FOUNTAIN HILLS AERIAL CONTROL

STREET PAVING PROJECT

HORIZONTAL CONTROL

Jim Gillespie
Project Manager

Anderson-Nelson, Inc.

- Engineering
- Surveying
- Site Grading Plans
- Subdivision Development
- Hydrology
- Construction Management
- Computer Services

17252 E. Falcon Dr., Suite 6, Fountain Hills, AZ 85268
(602) 837-9332

Phoenix, Arizona
(602) 273-1850

Bullhead City, Arizona
(602) 763-7372

BOOK 1

T	BS	FS	ΔRA	H.D	HI	HT
AL.	Sweat	5000	94-20-04	476.803	4.30	5.63
			-06	.802		
			00-00-00			
			m 94-20-05			
			94-20-04			
			-04	m94-20-04.5		
			00-00-00			
			m 94-20-04			
AL	5000	Sweat	265-39-58			
			-58			
			00-00-02			
			m 265-39-57			
			265-39-56	m.265-39-56		
			-56			
			00-00-02			
			m 265-39-55			

1 of 8/27/01

+/-	EL.	DESC.
+24.952		
+ .950		Set trav. pt North side Cerro Alto near lots 24/23

JE
JW

	T	BS	FS	∠Rt	HD	HI	HT
A	AL	Swat	1244	285-33-52	4427.270		
				-54	.261		
				00-00-04	.268		
				m 285-33-51			
				285-33-52			
				-52			
				00-00-00			
				m 285-33-52			
A	AL	1244	Swat	74-26-06			
				-06			
				359-59-56			
				m 74-26-08			
				74-26-08			
				-06			
				00-00-00			
				m 74-26-07			

V	EL	DESC
		BCD Int. Sierra Madre & Golden Eagle Panel Pt

⊼	BS	FS	∠ Rt.	HD	HI	HT	+/-	EL	Desc.
AL	Swent	1224	255-43-18	2443.500	4.30	5.51	-67.409		
			-20	.459			.467		BC @ Int. Golden Eagle
			00-00-00						& Jamaica Ln.
			m 255-43-19						Panel Pt.
			255-43-16						
			-18						
			359-59-58						
			m 255-43-18						
AL	1224	Swent	104-16-40						
			-40						
			00-00-00						
			m 104-16-40						
			104-16-42						
			-40						
			00-00-00						
			m 104-16-41						

T	BS	FS	∠Rt	HD	HI	HT
A	Sweat	5002	255-22-42	2510.617	4.30	5.53
			-42	.617		
			00-00-00			
			m 255-22-42			
			255-22-44			
			-44			
			00-00-00			
			m 255-22-44			
A	5002	Sweat	104-37-18			
			-18			
			00-00-00			
			m 104-37-18			
			104-37-16			
			-18			
			00-00-02			
			m 104-37-16			

+/-	EL	DESC
-62.1588		
.607		Set trav. pt NE cor Golden Eagle & Jamaica

255-22-43
104-37-17
360-00-00

⊼	BS	FS	∡Rt	HD	HI	HT	+/-	EL	Desc.
AL	Sweat	1225	227-00-00	1784.922	4.30	5.58	-27.539		
			226-59-58	.921			.567		BC Int Golden Eagle
			00-00-00						& Richwood
			m 226-59-59						Panel Pt.
			226-59-58						
			-58						
			00-00-00						
			m 226-59-58						
AL	1225	Sweat	133-00-00						
			-02						
			00-00-00						
			m 133-00-01						
			133-00-00						
			133-00-00						
			359-59-58						
			m 133-00-01						

T	BS	TS	∡Rt	HD	HI	HT	T/C	EL	DESC.
AL	Sweat	1217	190-29-52	1260970	4.30	10.54	-107.991		
			-50	.976			107.991		Boat Spike @ Int Aspen
			00-00-00						& Rusty Nail
			m 190-29-51						Panel Pt.
			190-29-48						
			-50						
			359-59-58						
			m 190-29-50						
AL	1217	Sweat	169-30-10						
			-08						
			00-00-02						
			m 169-30-08						
			169-30-10						
			-10						
			00-00-02						
			m 169-30-09						

X	BS	FS	∠Rt	HD	HI	HT	+/-	EL.	DESC
AL	Sweat	5003	241-08-48	1799.040	4.30	5.34	-74.906		
			-50	.039			.948		B.C. @ Int Golden Eagle
			00-00-00						& Nyack Drive
			m 241-08-49						trav. pt.
			241-08-50						
			-50						
			00-00-00						
			m 241-08-50						
AL	5003	Sweat	118-51-10						
			-10						
			00-00-00						
			m 118-51-10						
			118-51-08						
			-10						
			00-00-00						
			m 118-51-09						

⊼	BS	FS	∠Rt	H.D.	HI	LT	+/-	El	Desc.
AL.	Sweat	5004	284-46-22	2808.321	4.30	5.29	-157.375		
			-24	.320			.331		Set trav. pt. on
			00-00-00						retardation structure
			M 284-46-23						East of Plat 5006
			284-46-20						Ashbreak Wash
			-22						
			00-00-00						
			^ 284-46-21						
AL	5004	Sweat	75-13-38						
			-38						
			00-00-00						
			^ 75-13-38						
			75-13-38						
			-36						
			359-59-58						
			^ 75-13-38						

T	BS	FS	∠ Rt.	H.D	HI	HT	+/-	EL	DESC
AL	Sweat	5005	176-39-40	2319.080	4.30	5.25	-17.084		
			-36	.085			.120		Boat Spike trav. pt on
			359-59-58						Boxcar drive P.C., east of
			∩ 176-39-39						Pageland Cir
			176-39-38						
			-38						
			00-00-00						
			∩ 176-39-38						
AL	5005	Sweat	183-20-20						
			-18						
			359-59-56						
			∩ 183-20-21						
			183-20-22						
			-20						
			00-00-00						
			∩ 183-20-21						

⊼	BS.	F.S.	∡ RT	HD	HI	HI	+/-	ELEV.	Desc.
AL	Sweat	1213	153-33-00	3109.886	4.30	5.34	-4.858		
			-00	.884			.785		Boat spike @ Int of
			00-00-00						Aspen & Windyhill Rd.
			M 153-33-00						Panel Pt.
			153-33-00						
			-00						
			00-00-00						
			M 153-33-00						
AL	1213	Sweat	206-26-58						
			27-00						
			00-00-00						
			M 206-26-59						
			206-27-00						
			-00						
			00-00-00						
			M 206-27-00						

T	B.S.	F.S.	∡ RT.	H.D.	HI	HT	+/-	ELEV.	Desc
AL	Sweat	1212	158-01-20	2335.067	4.30	5.49	75915		
			-20	.068			.895		Boat spike @ Int. Marathon
			00-00-00						& Green Valley
			∧ 158-01-20						Panel Pt.
			158-01-20						
			-22						
			00-00-00						
			∧ 158-01-21						
AL	1212	Sweat	201-58-40						
			-42						
			00-00-02						
			∧ 201-58-40						
			201-58-38						
			-40						
			00-00-00						
			∧ 201-58-39						

T	BS	F.S	∠ RT	H.D.	H.I.	H.T	+/-	ELEV.	=
AL	Sweat	Deb	189-41-04						
			-04						
			00-00-00						
			^ 189-41-04						
			189-41-04						
			-04						
			00-00-00						
			^ 189-41-04						
AL	Deb	Sweat	170-18-56						
			-56						
			00-00-00						
			^ 170-18-56						
			170-18-56						
			-56						
			00-00-00						
			^ 170-18-56						

T	B.S.	F.S	∠ RT	H.D.	H.I	H.T
AL	Deb	5006	182-18-34	4167.488	A.30	
			-32	487		
			00-00-00			
			∧ 182-18-33			
			182-18-34			
			-34			
			00-00-00			
			∧ 182-18-34			
AL	5006	Deb	177-41-24			
			-26			
			00-00-00			
			∧ 177-41-25			
			177-41-28			
			-26			
			00-00-00			
			∧ 177-41-27			

+/-	ELEV	Desc.
		Set trav. pt. South end of Montezuma, East side of road

π	B.S.	F.S.	∡	Rt	H.D.	HI	Ht	+/-	ELEV	Desc.
AL.	Sweat	5007		182-37-38	1887.552	4.30	5.39	-61.827		
				-38	.552			.842		Boat spike @ Int. Golden Eagle & Aspen Panel Pt.
				00-00-00						
			∧	182-37-38						
				182-37-40						
				-40						
				00-00-00						
			M	182-37-40						
AL.	5007	Sweat		177-22-20						
				-20						
				00-00-00						
			∧	177-22-20						
				177-22-22						
				-22						
				00-00-00						
			M	177-22-22						

T	B.S.	F.S.	∠ RT	H.D.	HI	HT
AL	Sweat	5008	151-45-14	3274221	A.30	
			-16	.222		
			359-59-52			
			M 151-45-19			
			151-45-22			
			-20			
			00-00-00			
			M 151-45-21			
AL.	5008	Sweat	208-14-40			
			-38			
			00-00-00			
			M 208-14-39			
			208-14-40			
			-42			
			00-00-02			
			M 208-14-40			

+/-	ELEV	Desc.
		Set trav. pt. Windyhill Road
		Lot 16. (South Side of Road

π	B.S.	F.S.	∠	AT	H.D.	HI	HT	+/-	ELEV	Desc.
5000	Sweet	1205	327-27-10		133.080	5.59	5.38	-13.356		
			327-27-10		133.080			-13.353		Panel Pt. Cerro Alto
			0-0-0							East Side Lot 23
			m							
			327-27-08							
			327-27-10							
			359-59-58							
			m							
5000	1205	Sweet	32-32-50							
			32-32-50							
			0-0-0							
			m							
			32-32-48							
			32-32-52							
			359-59-58							
			m							

A	BS	FS	AZ	HD	HI	HT
5000	Sweat	1204	111-00-02	1007.120	5.59	9.47
			-00	.120		
			00-00-00			
			m 111-00-01			
			111-00-00			
			-00			
			00-00-00			
			m 111-00-00			
5000	1204	Sweat	248-59-58			
			249-00-00			
			359-59-58			
			m 249-00-00			
			248-59-56			
			-58			
			359-59-58			
			m 248-59-58			

+L	El.	Desc.
+34.13		
+34.156		Panel Pt. Cerro Alto's Alvarado

T	SS	FS	∡Rt.	HD	HI	HT
1217	ALLEN	1218	307-35-58	803.161	5.60	5.46
			307-35-58	803.161		
			0-0-0			
			m			
			307-35-58			
			307-30-00			
			0-0-0			
			m			
217	1218	ALLEN	52-2A-02			
			52-2A-02			
			0-0-0			
			m			
			52-2A-04			
			52-2A-00			
			0-00-00			
			m			

+/-	EL.	DESC
-20.984		
-21.009		Set random P.K. @ Int. Aspen & Quick Draw, Panel Pt (No Int. pt. existing)

307-35-58
52 2A-03
300-00-01

T	BS	FS	∡ Pt.	HD	HI	HT	+/-	El.	Desc.
5003	ALLEN	1219	334-24-28	292.661	5.66	5.15	-32.094		
			334-24-30	292.663			-32.096		Panel Pt. West side Nyack Drive, near P.C. lot-12
			0-0-0						
			m						
			334-24-28						
			334-24-30						
			0-0-0						
			m						
5003	1219	ALLEN	25-35-30						
			25-35-28						
			359-59-58						
			m						
			25-35-28						
			25-35-30						
			359-59-58						
			m						

T	BS	FS	∠Pt.	H.D	HI	HT	+/-	EL	DESC.
500A	Sweat	1223	173-45-42	829.730	5.47	5.35	+31.974		
			-40	.732			.961		B.C. ? Int. Golden Eagle & Aspen Panel Pt.
			00-00-02						
			m 173-45-40						
			173-45-42						
			-44						
			00-00-02						
			m 173-45-42						
500A	1223	Sweat	186-14-16						
			-20						
			359-59-56						
			m 186-14-20						
			186-14-18						
			-18						
			00-00-00						
			m 186-14-18						

T	BS	FS	∠R.	H.D.	HI	HT
5004	Sweat	5009	131-10-56	1205.822	5.47	5.28
			.58	.820		
			00-00-00			
			∧ 131-10-57			
			131-10-56			
			.56			
			00-00-00			
			∧			
5004	5009	Sweat	228-49-04			
			.02			
			359-59-58			
			∧ 228-49-04			
			228-49-04			
			.00			
			00-00-00			
			∧ 228-49-02			

±∠	EL.	DESC.
+53.629		
.629		Set trav. pt. s. side Eagles Nest Dr. w. of panel #222

T	BS	FS	∠Rt.	H.D.	HI	HT	+/-	EL	DESC.
5004	Sweat	1220	108-19-00	1450872	5.47	5.22	+7.483		
			-04	.877			+7.449		Panel Pt. S. side Aspen Dr. @ Int. w/ Eagles Nest
			00-00-00						
			M 108-19-02						
			108-19-02						
			-02						
			00-00-00						
			M 108-19-02						
5004	1220	Sweat	251-40-56						
			-58						
			00-00-00						
			M 251-40-57						
			251-40-56						
			-56						
			359-59-58						
			M 251-40-57						

108-19-02
251-40-57
359-59-59

T	BS	FS	HA	HD	HI	HT
3004	Sweat	1221	113-36-18	853660	5.47	5.13
			-18	.657		
			00-00-00			
			M 113-36-18			
			113-36-18			
			-18			
			00-00-00			
			M 113-36-18			
3004	1221	Sweat	246-23-40			
			-42			
			359-59-58			
			M 246-23-42			
			246-23-44			
			-42			
			00-00-00			
			M 246-23-43			

V	EL	DESC
40.919		
.926		Found Pt. North side Aspen Dr. P.C. lot 15.

T	BS	FS	∠Pt.	H.D	HI	HT	+/-	EL	DESC
5009	Sweat	1222	280-29-56	135.638	5.44	5.32	-3.959		
			280-29-56	135.639			-3.962		Pard Pt. South side Eagles Nest Drive
			0-0-0						
			m						
			286-29-56						
			286-29-58						
			0-0-02						
			m						
5009	1222	Sweat	73-30-06						
			73-30-06						
			0-0-02						
			m						
			73-30-02						
			73-30-04						
			359-59-58						
			m						

π	BS	FS	X Pt.	H.D	HI	HT	+/-	EL	DESC.
5005	ALLEN	12/5	139-30-40	264.968	5.60	5.3A	+8.682		
			139-30-38	264.968			+8.678		Boat spike @ P.C. west of Int.
			0-0-02						Boxcar & Pageland, Panel Pt
			m						
			139-30-38						
			139-30-36						
			359-59-56						
			m						
5005	12/5		220-29-20						
			220-29-18						
			359-59-56						
			m						
			220-29-20						
			220-29-20						
			0-0-0						
			m.						

T	ES	FS	∡Pt	HD	HI	HT	+/-	EL	Desc
5008	ALLEN	1211	03-17-50	437.501	5.54	9.37	-74.630		
			-50	437.497			.641		Panel Pt. N. side Greenbriar
			00-00-00						Near Lots 20/19
			m 03-17-50						
			03-17-52						
			-52						
			00-00-02						
			m 03-17-51						
5008	1211	AL	356-42-12						
			-12						
			00-00-02						
			m 356-42-11						
			356-42-10						
			-08						
			00-00-00						
			m 356-42-09						

π	BS	FS	∡Rt	HD	HI	HT	+/-	EL	Desc.
5008	AL	1210	92-58-22	524.494	5.54	5.32	-54.857		
			-20	.494			.856		Boat spike @ Int Aspen & Greenvalley Panel
			00-00-06						
			m 92-58-18						
			92-58-16						
			-16						
			00-00-00						
			m 92 58-16						
5008	1210	AL	267-01-44						
			-44						
			00-00-02						
			m 267-01-43						
			267-01-46						
			-42						
			00-00-00						
			m 267-01-44						

T	BS	FS	ARC	HD	HI	HT	V	EL	DEC
5008	AL	1209	78-50-48	833.810	5.54	5.31	-57.390		
			-43	.813			.370		
			00-00-02						
			m 78-50-47						
			78-50-48						
			-48						
			00-00-00						
			m 78-50-48						
5008	1209	AL	281-09-14						
			-10						
			00-00-00						
			m 281-09-12						
			281-09-16						
			-14						
			00-00-04						
			m 281-09-13						

Boot spike @ Int. Marathon & Aspen, Panel Pt

T	BS	FS	AZ	HD	HI	HT	EL	DESC.
2008	AL	1208	103-56-06	1219.507	5.54	525	-36.539	
			-06	.512			.530	Panel Pt. end of Marathon Dr.
			00-00-00					
			m 103-56-06					
			103-56-04					
			-04					
			00-00-00					
			m 103-56-04					
2008	1208	AL	256-04-00					
			256-03-58					
			00-00-04					
			m 256-03-57					
			256-03-54					
			-54					
			359-59-58					
			m 256-03-55					

∡	BS	FS	∡ Rt	HD	HI	HT	∡	El.	Desc
5008	AL	1207	38-11-16	1465.242	5.54	5.30	-3.891		
			-16	.244			-3.891		Panel Pt. N. end of Kit Fox Pl.
			00-00-00						
			M 38-11-16						
			38-11-16						
			-16						
			00-00-00						
			M 38-11-16						
5008	1207	AL	321-48-44						
			-44						
			00-00-00						
			M 321-48-44						
			321-48-46						
			-46						
			00-00-00						
			M 321-48-46						

⊼	BS	FS	∠Rt	H.D	HI	HT	∠	El	Desc.
					5.60	6.32			
5006	ALLEN	1109	328-37-06	1881.670			6.958		Panel Pt. on Zamora Plaza
			-08	.672			.974		
			00-00-02						
			m						
			328-37-06						
			-08						
			00-00-00						
			m						
5006	1109	ALLEN	31-22-54						
			-54						
			00-00-00						
			m						
			31-22-54						
			-56						
			00-00-00						
			m.						

⊼	B.S.	F.S.	∡ RT	H.D	HI	HT	+/-	ELEV.	Desc.
					5.60	4.91			
5006	AL	1108	18-40-56	2898.464			94.630		35- Sec Cor. 5 A / 819
			-56	.460			.713		
			00-00-00						BM#
			M						
			18-40-56						
			-56						
			00-00-00						
			M						
5006	1108	AL	341-19-04						
			-04						
			00-00-00						
			M						
			341-19-04						
			-04						
			00-00-00						
			M						

T	B.S.	F.S.	∡ H	H.D	HI	HT	+/-	ELEV	Desc
					5.60	5.21			
5005	AL	1110	232-57-56	761.770			+1.429		Panel PA near center of
			-54	.767			.435		section 8
			359-59-58						
			^						
			232-57-58						
			-56						
			00-00-00						
			^						
5006	1110	AL	127-02-02						
			-04						
			00-00-00						
			^						
			127-02-02						
			-00						
			359-59-56						
			^						

T	B.S.	F.S.	∠ RT	H.D.	HI	HT	+/-	ELEV.	Desc
					5.60	5.19			
1207	DEB	1103	225-22-46	2826.870			+212.596		Panel Pt. near NW cor. of Plat 5000
			-46	.886			.640		
			359-59-50						
			M						
			225-22-52						
			-52						
			00-00-00						
			M						
1207		DEB	134-37-06						
			-04						
			359-59-56						
			M						
			134-37-08						
			-10						
			00-00-00						
			M						

π	B.S.	F.S.	∡ RT.	H.D.	HI	HT.	+/-	ELEV.	Desc.
1207	Deb.	1206	350-51-30	228.014	5.60	5.52	-25.499		Boat Spike @ Int. Paradox &
			350-51-30	228.014			-25.497		Kit Fox Plaza
			0-0-02						Panel Pt.
			M						
			350-51-30						
			350-51-26						
			359-59-56						
			M						
207	1206	Deb	09-08-32						
			09-08-32						
			0-0-0						
			M						
			09-08-28						
			09-08-30						
			0-0-0						
			M						

⊼	BS	FS	∠RA	H.D	HI	HT	+/-	EL	DESC.
002	ALLEN	1240	132-31-54		5.44	5.35			
			-56	1671.211			-74.756		Boot spike @ Int. Tepee &
			359-59-54	.214			.756		Peace Pipe Pl., panel pt
			M						
			182-32-00						
			-02						
			00-00-02						
			M						
002	1240	ALLEN	177-28-02						
			-02						
			00-00-00						
			M						
			177-28-04						
			-00						
			00-00-04						
			M						

T	B.S.	FS	∡ RT	H.D.	HI	HT	+/-	ELEV.	Desc.
5002	AL.	12A2	202-29-14	264.362	5.44	5.35	-00.517		
			-16	.362			.538		Boat spike @ Int. Audobon & Blackbird, pavel pt
			00-00-00						
			M						
			202-29-14						
			-12						
			00-00-00						
			M						
5002	12A2	AL.	157-30-46						
			-46						
			00-00-00						
			M						
			157-30-44						
			-46						
			00-00-00						
			M						

∡	BS	FS	∡Rt	HD	HI	HT	+/-	Ex	DESC
					5.03	5.15			
5002	At	5010	139-38-32	2596031			-116.974		Set trav. pt. N. of Richwood
			-32	.031			.974		across from Bottleneck
			00-00-00						
			m 139-38-32						
			139-38-34						
			-34						
			00-00-02						
			m 139-38-33						
5002	5010	At	220-21-26						
			-24						
			359-59-56						
			m 220-21-27						
			220-21-26						
			-28						
			00-00-00						
			m 220-21-27						

T	BD	FD	∠Rt.	H.D.	HI	HT	+/-	El.	Desc.
					5.03	5.47			
5002	AL	1236	130-15-52	2979837			-65.545		Random point at east end of
			-52	.837			- .522		Centipede
			00-00-00						
			m 130-15-52						
			130-15-50						
			-52						
			00-00-00						
			m 130-15-52						
5002	1236	AL	229-44-06						
			-08						
			00-00-00						
			m 229-44-07						
			229-44-06						
			-06						
			359-59-56						
			m 229-44-08						

T	BS	FS	∠RA	HD	HI	HT	+/-	EL	DESC
					5.03	5.40			
002	AL	1235	113-14-10	2898.033			-16.830		Boat spike @ Int. Centipede &
			-10	.030			.921		Grassland \ pavel pt.
			359-59-58						
			m 113-14-11						
			113-14-12						
			-12						
			00-00-00						
			m 113-14-12						
002	1235	AL	246-45-46						
			-48						
			00-00-00						
			m 246-45-47						
			246-45-46						
			-46						
			359-59-54						
			m 246-45-49						

T	B.S.	F.S.	∡ RT	H.D.	HI	HT	+/-	ELEV.	Desc.
					5.43	5.43			
5002	AL	1234	98-18-50	324.709			+17.859		Random point at west end
			-50	.706			.985		of Centipede
			00-00-00						
			^						
			98-18-50						
			-50						
			00-00-00						
			^						
5002	1234	AL	261-41-10						
			-10						
			00-00-00						
			^						
			261-41-10						
			-10						
			00-00-00						
			^						

98-18-50
261-41 10
360-00-00

T	B.S.	F.S.	∡ RT	H.D.	HI	HT	+/-	ELEV	Desc.
					5.03	5.42			
5002	AL.	1232	107-32-52	2407.826			-81287		Bat. ~~spike~~ @ Int. Greenland &
			-48	.327			.249		Scorpion, panel pt.
			359-59-58						
			^						
			107-37-50						
			-52						
			00-00-00						
			^						
5002	1232	AL.	252-22-12						
			-12						
			00-00-02						
			^						
			252-22-12						
			-10						
			00-00-00						
			^						

π	B.S.	F.S.	∠ RT	HD	HI	H	+/-	ELEV.	Desc.
					5.63	5.37			
5002	AL	5011	122-19-50	2303.18			-96.217		Boat spike trav. pt. P.C. on
			-50	.183			.131		Cobblestone Lane
			00-00-00						
			∩ 122-19-50						
			122-19-52						
			-50						
			00-00-00						
			∩ 122-19-51						
5002	5011	AL	237-40-08						
			-10						
			00-00-00						
			∩ 237-40-09						
			237-40-10						
			-08						
			359-59-58						
			∩ 237-40-09						

AA.5

π	B.S.	F.S.	∡ RT	HD	HI	HT	+/-	ELEV	Desc.
				192.032	5.50	5.30	-3.524		
1240	5002	5012	133-20-02	192.034			-3.528		Set trav. pt. on Parcelice Pl.
			133-20-02						
			0-0-0						
			M						
			133-20-00						
			133-20-02						
			0-0-02						
			M						
1240	5012	5002	226-40-00						
			226-40-00						
			0-0-0						
			M						
			226-40-00						
			226-40-00						
			0-0-02						
			M						

T	BS	FS	∡Rt.	H.O.	VI	HT	+/-	El.	Desc.
				202.259	5.42	5.35	+11.004		
5012	1240	1239	122-29-00	202.258			+10.997		Set panel pt. end of Peace Pipe Pl.
			122-29-04						
			0-0-0						
			M						
			122-29-04						
			122-29-00						
			0-0-0						
			M						
5012	1239	1240	237-30-54						
			237-30-50						
			359-59-58						
			M						
			237-30-54						
			237-30-54						
			0-0-0						
			M						

T	BS	FS	∠ Rt	HD	HI	HT	+/-	EL	Desc
2A2	5002	5013	89-05-54	109.675	5.59	5.33	+0.557		
			89-05-52	109.676			+0.560		Set trav. W. side Audobon
			0-0-0						
			M						
			89-05-56						
			89-05-54						
			0-0-0						
			M						
2A2	5013	5002	270-54-08						
			270-54-06						
			0-0-0						
			M						
			270-54-06						
			270-54-06						
			0-0-02						
			M						

R	BS	FS	ARt	HD	HI	HT	V	EL	Desc.
5013	1242	1241	184-17-30	97.134	5.52	5.40	-9.569		
			184-17-30	97.133			-9.571		Random panel pt. North end of Hudoban
			0-0-0						
			M						
			184-17-34						
			184-17-34						
			0-0-0						
			M						
5013	1241	1242	175-42-24						
			175-42-26						
			0-0-0						
			M						
			175-42-24						
			175-42-24						
			359-59-58						
			M						

T	BS	FS	ARt	HD	HI	HT	+/-	EL.	Desc.
5010	5002	1237	326-21-34	61.894	5.27	5.50	-10.786		
			326-21-34	61.896			10.786		Boat spike @ Int. Richwood & Bottlebrush, panel pt.
			0-0-0						
			M						
			326-21-34						
			326-21-34						
			0-0-0						
			M						
5010	1237	5002	33-38-26						
			33-38-24						
			0-0-02						
			M						
			33-38-24						
			33-38-22						
			0-0-0						
			M						

T	BS	FS	ARP	HD	HI	HT	%	EL.	DESC.
					5.27	5.54			
5010	5002	1238	328-29-16	341.037			-5.145		Random panel pt. @ South end of Battlebrush
			328-29-16	.036			.138		
			0-0-0						
			M						
			328-29-1A						
			328-29-1B						
			0-0-0						
			M						
5010	1238	5002	31-30-AA						
			31-30-AA						
			0-0-0						
			M						
			31-30-AA						
			31-30-AA						
			352-59-58						
			M						

⊼	BS	FS	∠PT	H.D	HI	HT	∠	EL.	DESC.
				3394.648					
5002	ALLEN	501A	213-27-08	3394.648					
			213-27-08						
			359-59-58						
			M -09						
			213-27-10						
			213-27-10						
			0-0-0						
			M -10						
5002	501A	ALLEN	146-32-50						
			146-32-50						
			0-0-0						
			M -50						
			146-32-50						
			146-32-50						
			0-0-0						
			M -50						

Set trav pt. S. side of Blackmer near 4|3 / 9|10

(Dist too far for ∠)

213-27-09.5
146-32-50
359-59-59.5

PANEL 1100 = ECL 32-1 (F.H original control)

Record A1559.110 N. 17484.740 E.

Also is BM# 328

Record El = 2039.74

0.35' Above grd.

T	ES	FS	ΔRt	HD
SOA	SOOZ	1107	83-02-30	278.157
			83-03-30	278.057
			359-59-56	
			M -35	
			83-03-40	
			83-03-36	
			0-00-0	
			M -30	
SOA	1107	SOOZ	276-56-14	
			276-56-14	
			359-59-56	
			M -14	
			276-56-22	
			276-56-22	
			359-59-54	
			M -25	

DEL

B.C. Sec. Cor.

A	3
9	10

Flush

83-03-38
276-56-20.5

359-59-58.5

SAF

T	BS	FS	ΔPt	H.D.	HI	HT	Y	EL.	Desc.
					5.45	5.30			
5000	ALLEN	5015	192-01-10	894.220			+33.794		St. trav. pt. @ SE cor. Cerro
			192-01-10	894.229			.780		Alto & Alvarado to see Panel #104
			359-59-50						
			M -12						
			192-01-12						
			192-01-12						
			359-59-58						
			M -13						
5000	5015	ALLEN	167-58-48						
			167-58-50						
			0-0-0						192-01-12.5
			M -49						167-58-48.5
			167-58-50						360-00-01.0
			167-58-46						
			0-0-0						
			M 48						

T	BS	FS	∠ Pt.	HD	HI	HT	V	E	Desc.
					5.29	5.10			
5015	Sweat	110A	72-33-52	3016.267			+2.625		St random panel pt. on
			72-33-52	3016.256			+2.696		Ramon Dr. Plat 507E
			00-00-04						
			m 72-33-50						
			72-33-43						
			72-33-52						
			00-00-00						
			m 72-33-50						
5015	110A	Sweat	287-26-08						
			287-26-10						
			00-00-00						
			m 287-26-09						
			287-26-08						
			287-26-12						
			00-00-00						
			m 287-26-10						

72-33-50
287-26-09.5
359-59-59.5

⊼	BS	FS	∡ Rt.	H.D.	HI	HT
TBM#1	Sweat	1122	236-51-22	604.844	5.21	5.51
			236-51-24	604.844		
			0-0-0			
			M -23			
			236-51-22			
			236-51-24			
			0-0-0			
			M -23			
TBM#1	1122	Sweat	123-08-38			
			123-08-36			
			0-0-02			
			M -36			
			123-08-40			
			123-08-38			
			0-0-02			
			M -38			

STA	+	HI	−	EL.	DESC.
TBM#1				1777.936	1/2" rebar per plat 6010
	11.03	88.966			
#1122			12.35	1776.616	Panel Pt. flush
	12.17	88.786			
TBM#1			10.85	1777.936	

+/-	EL.	DESC.
-1.046		Panel pt. (flush) near Sec. cor. 9/10 16/15
-1.045		

TBM#1 = 31594.485 N. 24949.972 E.

236-51-23
123-08-37
360-00-00

⊼	BS	FS	∠Rt	H.D	HI	HT
JUD	Sweat	1123	289-59-54	6906.431	3.84	5.68
			-54	6906.426		
			00-00-00			
			∧			
			289-59-54			
			-54			
			00-00-00			
			∧			
JUD	1123	Sweat	70-00-08			
			-10			
			00-00-02			
			∧			
			70-00-04			
			-06			
			359-59-58			
			∧			

+/-	EL	DESC
~~-6.704~~	DO NOT	
~~-6.704~~	USE!	Set panel pt. west of #123
		(Flush)

JUD = BM #76 EL = 1681.0

1.65' above ground

π	B.S.	F.S.	∡ RT.	HD	HI	HT	+/-	ELEV.	Desc.
					3.84	3.95			
JuD	Sweat	1118	260·44·54	1930.687			-158.127		Panel pt. on B.C.
			-50	.690			.082		
			00·00·00						1.35' above grd.
			M 260·44·52						
			260·44·50						
			-50						
			359·59·58						
			M 260·44·51						
JuD	1118	Sweat	99·15·12						
			-12						
			00·00·00						
			M 99·15·12						
			99·15·12						
			-10						
			00·00·00						
			M 99·15·11						

1/16 S1 S12 C.C.
T3N R6E

π	B.S.	F.S.	∡ RT.	HD.	HI	HT	+/-	ELEV.	Desc.	
					3.84	4.07				59 ∡
JuD	Sweat	1115	157-56-14	1423 29[illegible]			-154.284		Panel Pt. on B.C.	2/1
			-12	.292			.284			1/A cor.
			00-00-00						1.15 above grd.	
			∧ 157-56-13							
			157-56-10							
			-12							
			00-00-00							
			∧ 157-56-11							
JuD	1115	Sweat	202-03-54							
			-54							
			00-00-08							
			∧ 202-03-50							
			202-03-50							
			-48							
			00-00-02							
			∧ 202-03-48							

Π	B.S.	F.S.	∠ RT	HD	HI	HT	+/-	ELEV.	Desc.
				3.88	3.88				
J.D.	Sweat	1114	137-47-12	4009.859			-20.349		Panel Pt. on B.C.
			-08	4009.873			-20.361		
			00-00-00						
			∧ 137-42-10						1.40' above grd.
			137-42-10						
			-10						
			00-00-00						
			M 137-42-10						
J.D.	1114	Sweat	222-17-52						
			-54						
			00-00-04						
			∧ 222-17-51						
			222-17-48						
			-50						
			00-00-00						
			∧ 222-17-49						

TAN
S 36 U

S 1 U
T3N

T	B.S	F.S.	∡ AT	HD.	HI	HT	+/-	ELEV.	Desc.
					3.84	4.58			
JuD	Sweat	1113	128-37-14	3784.792			~~.18651~~ ~~.823~~ DO NOT USE!		Panel Pt. on B.C.
			-14	.788					
			00-00-00						1.10' above grd.
			∩ 128-37-14						
			128-37-16						
			-12						
			00-00-02						
			∩ 128-37-13						
JuD	1113	Sweat	231-22-50						
			-46						
			00-00-00						
			∩ 231-22-48						
			231-22-46						
			-44						
			359-59-56						
			∩ 231-22-47						

35	36
2	1

T	B.S.	F.S.	∠ RT.	H.D.	HI	HT	+/-	ELEV	DESC.
					3.84	5.30			
JuD	Sweat	5016	61 59 42	2941.895			+85.719		Set trav. pt.
			-42	.899			.650		
			00-00-00						
			∧ 61-59-42						
			61-59-42						
			-42						
			00-00-00						
			∧ 61-59-42						
JuD	5016	Sweat	298-00-14						
			-16						
			359-59-56						
			∧ 298-00-17						
			298 00-18						
			-18						
			00-00-00						
			∧ 298-00-18						

T	BS	FS	∡Rt.	H.D.	HI	HT	+/-	EL	DESC
				2439.101					
123A	500Z	110Z	252-06-2A	2439.100					Panel on B.C. Sec. Cor. 33/34 4/3
			252-06-26						
			0-0-0						
			m. -25						
			252-06-2A						
			252-06-2A						
			359-59-58						
			m -25						
123A	110Z	500Z	107-53-3A						
			107-53-3A						
			0-0-0						
			m -3A						
			107-53-32						
			107-53-36						
			0-0-0						
			m -3A						

STA	+	HI	-	EL.	DESC.
				1890.04	PANEL #217
	17.92				
TP			0.55		
	24.27				
TP			1.03		
	11.73				
TP			1.97	1940.40 adj. 1940.41	PANEL @ CME & Aspen
	0.30				
T.P.			11.07		
	0.97				
T.P.			7.26		
	6.92				
			3.77	1926.50	PANEL #212
		+36.46			

Sta	+	Hi	-	El.	Desc.
				1552.89	Panel #276 Knuckle Vallecito
	10.645				
TP			7.047		
	2.523				
TP			0.349		
	8.403				
TP			0.250		
	10.072				
TP			0.920		Int Del Cambre & La Pasada
	8.238				
TP			0.521		
	13.395				
TP			5.945		
	0.430				
TP			13.462		Panel #119 Boat Spike Flush P.C.
	5.713				
TP			3.845		
	7.048				
TP			3.722		
	8.722				
TP			3.216		Int Deerskin & Del Cambre
	4.330				
TP			0.110		
	13.455				
TP			0.810		
	+94.174		-40.197	1606.807	Panel #265 check in
		+53.977			

1606.91 Calle Del Prado
#265 & Deerskin

119

West of Council Ct.

Sta.	+	Hi	-	El.	Desc.
				2038.20	Panel # 202
	9.49				
T.P.			24.04		
	1.14				
TP			22.18		Panel # 105 ODD NAIL FLUSH SW OF [illegible] & [illegible]
	8.84				
TP			6.93		
	22.38				
TP			1.55		
	20.01				
T.P.			0.58		
	22.99				
T.P.			5.38		Panel # 104 ODD NAIL FLUSH RAMON DRIVE
	5.36				
T.P.			22.97		
	0.81				
T.P.			7.48		
	10.50				
T.P.			23.70		
	0.32				
T.P.			22.57		
	0.65				
T.P.			22.02		
	2.67				
T.P.			8.84		Panel # 109 ODD NAIL FLUSH ZAMORA PLAZA
	1.14				
TP			17.43		
	1.65				
TP			20.83		
	2.56				
TP			17.57		
	0.29				
TP			11.36		

Sta	+	HI	-	El	Desc
	4.58				
TP			15.77		
	10.22				
TP			1.01		
	13.98				
TP			1.54		
	13.70				
TP			1.06		
	11.12				
TP			14.42		
	20.77				
T.P.			0.76		
	22.20				
T.P.			6.09		Panel # 110 600 Nail Flush
	5.74				
T.P.			17.43		
	0.16				
T.P.			23.39		
	14.72				
TP			14.28		
	0.50				
TP			16.50		
	1.91				
TP			24.03		
	0.42				
TP			15.99		
	5.64				
TP			7.94		Int. Montezuma & Tequesta B.C.
	(237.10)		1395.64		

2038.20
158.54
1879.66

Total Dist on Circuit 11,000 ft.

Record el. = 1879.72

⊼	ES	FS	∡Rt.	H.D.	HI	HT	⊼	EL	DESC.
					4.86	5.41			
DEB	SWEAT	1203	35-47-06	1041.147			+15.485		BC @ Int Golden Eagle &
			-06	.146			.174		Cerro Alto
			00-00-00						
			m 35-47-06						
			35-47-06						
			-06						
			00-00-00						
			m 35-47-06						
DEB	1203	Sweat	324-12-54						
			-52						
			00-00-00						
			n 324-12-53						
			324-12-54						
			-54						
			00-00-00						
			n 324-12-54						

☆	BS	FS	∠Rt.	H.D.	HI	HT
					4.86	5.52
Deb	Sweat		359-26-00	1739.181		
			-00	.186		
			00-00-00			
			∧ 359-26-00			
			359-26-00			
			-00			
			00-00-00			
			∧ 359-26-00			
Deb		Sweat	00-33-56			
			-58			
			359-59-58			
			∧ 00-33-58			
			00-34-00			
			-00			
			00-00-00			
			∧ 00-34-00			

☆	El.	DESC.
-122.556		Set P.K. on Aspen Dr. near
.584		SOSD - BLK 2 - LOT 26, no point number
		on map

⊼	BS	FS	XRT.	H.D.	HI	HT	⊼	EL.	DESC.
					4.86	5.45			
Deb	Sweat	1214	42-36-00	1871.713			-97.597		B.C. @ Int. of Aspen Dr.
			-00	.708			.641		& Sourdough
			00-00-00						
			M 42-36-00						
			42-36-00						
			-00						
			00-00-00						
			M 42-36-00						
Deb	1214	Sweat	317-24-02						
			317-23-58						
			00-00-00						
			M 317-24-00						
			317-23-58						
			-24-00						
			00-00-00						
			M 317-23-59						

⊼	BS	FS	∠Rt	HD	HI	HT	+/-	EL	DESC.
					4.86	5.35			
Deb	Sweat	5017	333-58-18	1796.342			-132.765		Set trav. pt. on DAM in
			-18	.341			.779		505 D
			359-59-58						
			M 333-58-19						
			333-58-18						
			-18						
			00-00-00						
			M 333-58-18						
Deb	5017	Sweat	26-01-42						
			-42						
			00-00-00						
			M 26-01-42						
			26-01-42						
			-42						
			00-00-00						
			M 26-01-42						

T	BS	FS	∠Rt.	H.D.	HI	HT
					5.50	5.48
507	DEB	1216	294·32·46	1276.826		
			-48	.824		
			359·59·58			
			m 294·32·48			
			294·32·50			
			-50			
			00·00·00			
			m 294·32·50			
507	1216	DEB	65·27·10			
			·08			
			359·59·56			
			m 65·27·11			
			65·27·10			
			-10			
			00·00·00			
			m 65·27·10			

Y	E	DESC.
+74.627		
.637		

?

9/5/91

CONT. FROM 9/4/91 1 OF 2

T	BS	ES	∠ Rt.	H.D.	HI	HT	+/-	EL.	DESC.
5046	JWD	5017	169-42-24	986.433	5.47	4.88	-2.125		TRAV Pt.
			-24	.432			.118		(ELL 2-3. BM# 385)
			00-00-00						Record El. = 1759.26
			m -24						
			169-42-28						
			-28						
			00-00-00						
			m -28						
5046	5017	JWD	190-17-32						
			190-17-32						
			0-0-0						
			m -32						169-42-26
			190-17-32						190-17-33
			190-17-32						359-59-59
			359-59-56						
			m -34						

Panel #111

BM el 1772.44

Gr 1772.34

BOOK 2

T	B.S.	F.S.	∠ RT.	HD.	HI	HT	+/-	EL.	Desc.
					5.49	5.15			
5017	Deb	1228	87-46-24	797.557					
			-28	.557			-36.286		Rep. Cor SW
			359-59-58				.286		return Lot: 66
			∧ 87-46-27						@ Int. of Dixie
			87-46-28						Mine & Aspen Trail
			-26						
			00-00-00						
			∧ 87-46-27						
5017	1228	Deb	272-13-32						
			-32						
			00-00-00						
			∧ 272-13-32						
			272-13-32						
			-32						
			00-00-00						
			∧ 272-13-32						

⊼	B.S.	F.S.	∠	RT	HD	HI	HT	+/-	ELEV	Desc.
						5.49	4.95			
5017	Deb	1226	62-02-30		628.323			-26.769		Prop corner @
			-30		.323			.774		West end of
			00-00-00							Agate Knoll
			∧ 62-02-30							
			62-02-30							
			-30							
			00-00-00							
			∧ 62-02-30							
5017	1226	Deb	297-57-32							
			-30							
			00-00-00							
			∧ 297-57-31							
			297-57-34							
			-32							
			00-00-06							
			∧ 297-57-30							

T	B.S.	F.S.	∡ RT.	HD.	HI	HT	+/-	ELEV	Desc.
					5.49	5.34			
5017	Deb	1229	110-15-58	793.351			-46.585		Set nail @
			-58	.353			.592		South end of
			00-00-00						Yellowstone
			∧ 110-15-58						
			110-15-54						
			-58						
			00-00-00						
			∧ 110-15-56						
5017	1229	Deb	249-44-02						
			-04						
			00-00-00						
			∧ 249-44-03						
			249-44-04						
			-04						
			00-00-00						
			∧ 249-44-04						

T	B.S.	F.S.	∠ RT.	H.D.	HI	HT.	+/-	ELEV.	Desc.
					5.49	9.52			
5017	Deb	1230	105-39-32	1006.087			-41.028		
			-34	.084			.027		Bent spike @ Int.
			00-00-00						Dixie Wine & Yellowstone
			∧ 105-39-33						
			105-39-34						
			-34						
			00-00-02						
			∧ 105-39-33						
5017	1230	Deb	254-20-26						
			-26						
			00-00-00						
			∧ 254-20-26						
			254-20-28						
			-30						
			359-59-58						
			∧ 254-20-30						

⊼	B.S.	F.S.	∡ RT.	H.D.	HI	HT	+/-	ELEV.	Desc.
					5.49	5.43			
5017	Deb	1232	91-12-20	1225.868			-37.260		
			-18	.868			279		Boat spike @ Int. of Grassland & Scorpion - Previously located (use this location)
			00-00-00						
			∩ 91-12-19						
			91-12-22						
			-24						
			00-00-02						
			∩ 91-12-22						
5017	1232	Deb	268-47-40						
			-38						
			00-00-02						
			∩ 268-47-38						
			268-47-42						
			-36						
			359-59-56						
			∩ 268-47-41						

T	BS	F.S.	∡RT	H.D	HI	HT	+/-	ELEV	Desc.
					5.59	13.56			
1232	1228	1231	255-08-40	485.881			-6.322		set nail @
			-36	.887			.341		East end of
			00-00-02						Scorpion in
			∧ 255-08-37						Cul-de-sac
			255-08-38						
			-38						
			00-00-00						
			∧ 255-08-38						
1232	1231	1228	104-51-20						
			-22						
			00-00-00						
			∧ 104-51-21						
			104-51-26						
			-24						
			00-00-04						
			∧ 104-51-23						

0/20/91
80

T	B.S.	F.S.	∠RT.	HD	HI	HT	+/-	ELEV.	Desc.
					5.56	9.46			
DewBaker	Jwo	1277	342-28-56	1245.599			-171.955		
			-58	.598			.964		
			359-59-56						
			∧ 342-28-59						
			342-29-00						
			-00						
			00-00-00						
			∧ 342-29-00						
NB.	1277	JwD	17-31-00						
			30-58						
			00-00-00						
			∧ 17-30-59						
			17-31-02						
			-00						
			00-00-00						
			∧ 17-31-01						

T	B.S.	F.S.	∡RT	H.D.	HI	HT	+/-	ELEV	Desc.
					5.56	5.20			
N.B.	JuD	1276	339-46-54	1581.196			-179.562		
			-52	.194			.575		
			359-59-56						
			M 339-46-55						
			339-46-54						
			-54						
			00-00-00						
			M 339-46-54						
NB	1276	JuD	20-13-04						
			-00						
			359-59-56						
			M 20-13-04						
			20-13-04						
			-04						
			00-00-00						
			M 20-13-04						

T	B.S.	F.S.	∠	RT	HD.	HI	HT	+/-	ELEV.	Desc.
						5.56	5.31			
NB	JuD	1275	01-23-06		1598.788			-183.753		
				-06	.792			.715		
			359-59-58							
			∧ 01-23-07							
			01-23-06							
				-06						
			00-00-00							
			∧ 01-23-06							
NB	1275	JuD	358-36-56							
				-56						
			00-00-00							
			∧ 358-36-56							
			358-36-54							
				-56						
			00-00-04							
			∧ 358-36-53							

T	B.S.	F.S.	∡ RT.	HD.	HI	HT	+/-	ELEV.	Desc.
					5.56	5.40			
NB	JuD	5018	26-48-38	1445.350			-193.651		
			-40	.347			.685		
			00-00-00						
			m 26-48-39						
			26-48-38						
			-42						
			00-00-02						
			m 26-48-39						
NB	5018	JuD	333-11-18						
			-18						
			359-59-56						
			m 333-11-20						
			333-11-20						
			-22						
			00-00-00						
			m 333-11-21						

T	B.S.	F.S.	∠ RT.	HD	HI	HT	+/-	ELEV.	Desc.
					5.56	5.45			
NB	JuD	1271	54-17-56	1677.369			-186.897		
			-54	.368			.937		
			00-00-00						
			∧ 54-17-55						
			54-17-56						
			-56						
			00-00-00						
			∧ 54-17-56						
NB	1271	JuD	305-42-06						
			-06						
			00-00-00						
			∧ 305-42-06						
			302-42-06						
			-08						
			00-00-04						
			∧ 302-42-05						

T	B.S.	F.S.	∡ RT.	HD
NB	JuD	1272	29-52-20	1118.694
			-20	.697
			359-59-58	
			∧ 29-52-21	
			29-52-20	
			-20	
			00-00-00	
			∧ 29-52-20	
NB	1272	JuD	330-07-40	
			-40	
			00-00-00	
			∧ 330-07-40	
			330-07-42	
			-42	
			00-00-00	
			∧ 330-07-42	

HI	HT	+/-	ELEV.	Desc.
5.56	5.40			
		+184.639		
		.622		

T	B.S.	F.S.	∠ RT.	HD
NB	JuD	1265	337-17-18	4544.745
			-18	.740
			00-00-00	
			∩ 337-17-18	
			337-17-18	
			-18	
			00-00-00	
			∩ 337-17-18	
NB	1265	JuD	22-42-40	
			-42	
			00-00-00	
			∩ 22-42-41	
			22-42-42	
			-44	
			00-00-00	
			∩ 22-42-43	

HI	HT	+/-	ELEV.	Desc.
5.56	5.33	-33.597		
		.607		

T	B.S.	F.S.	∡ RT.	HD	HI	HT	+/-	ELEV.	Desc.
					5.56	5.34			
NB	JuD	5019	336-20-04	5003.752			-32.064		
			-02	.751			.023		
			359-59-58						
			∧ 336-20-04						
			336-20-04						
			-04						
			00-00-00						
			∧ 336-20-04						
NB	5019	JuD	23-39-54						
			-54						
			359-59-58						
			∧ 23-39-55						
			23-39-56						
			-56						
			00-00-00						
			∧ 23-39-56						

T	B.S.	FS.	∠ RT	HD	HI	HT	+/-	ELEV.	Desc.
					5.56	5.20			
NB	JuD	1259	326-25-40	5565.610			-39	455	
			-42	.607				455	
			00-00-00						
			∧ 326-25-41						
			326-25-42						
			-42						
			00-00-00						
			∧ 326-25-42						
NB	1259	JuD	33-34-16						
			-18						
			359-59-58						
			∧ 33-34-18						
			33-34-18						
			-20						
			00-00-00						
			∧ 33-34-19						

T	BS	FS	∠	RT	HD	HI	HT	+/-	ELEV.	DESC.
						5.56	5.31			
NB	JWD	5020	322-35-32		5698.717			-38.401		
				-32	.724			363		
			00-00-02							
			M 322-53-31							
			322-35-30							
				-30						
			00-00-00							
			M 322-35-30							
NB	5020	JWD	37-24-28							
				-24						
			359-59-56							
			M 37-24-28							
			37-24-30							
				-28						
			00-00-00							
			M 37-24-29							

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc.
					5.70	5.34			
5018	NB	1273	23-54-32	30.937			+0.064		
			-34	.936			.064		
			00-00-00						
			M 23-54-33						
			23-54-36						
			-36						
			00-00-02						
			M 23-54-35						
5018	1273	NB	336-05-26						
			-26						
			00-00-00						
			M 336-05-26						
			336-05-28						
			-24						
			00-00-00						
			M 336-05-26						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	Desc.
					5.70	5.15			
5018	JwD	1274	140-16-58	231.098			-1.307		
			140-16-58	231.100			-1.311		
			0-0-0						
			M						
			140-16-50						
			140-16-58						
			0-0-0						
			M						
5018	1274	JwD	219-43-02						
			219-43-02						
			0-0-0						
			M						
			219-43-00						
			219-43-02						
			359-59-58						
			M						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc.
					5.79	5.31			
12105	NB	12100	147-18-34	417.067			+7.177		
			-36	.068			.174		
			00-00-00						
			M						
			147-18-36						
			-36						
			00-00-00						
			M						
12105	12100	NB	212-41-26						
			-24						
			00-00-00						
			M						
			212-41-24						
			-24						
			00-00-00						
			M						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc.
					5.79	5.38			
1265	NB	1263	61-22-42	507.353			-0.257		
			-42	.353			.257		
			00-00-00						
			M 61-22-42						
			61-22-42						
			-42						
			00-00-00						
			M 61-22-42						
1265	1263	NB	298-37-18						
			-18						
			00-00-00						
			M 298-37-18						
			298-37-16						
			-18						
			00-00-00						
			M 298-37-17						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	Desc
					5.53	5.30			
S019	NB	1267	284-06-52	501.745			-33.718		
			-54	.746			.714		
			00-00-00						
			M						
			284-06-54						
			-54						
			00-00-00						
			M						
S019	1267	NB	75-53-08						
			-08						
			00-00-02						
			M						
			75-53-06						
			-08						
			00-00-00						
			M						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc.
					5.53	5.38			
5019	NB	1202	69-45-58	596.743			-17.198		
			-46-00	.748			.212		
			00-00-00						
			^						
			69-46-00						
			-00						
			00-00-00						
			^						
5019	1207	NB	290-14-02						
			-00						
			359-59-58						
			^						
			290-14-02						
			-00						
			00-00-00						
			^						

T	BS	FS	∠ RT	HD	HT	HT	+/-	ELEV	Desc.
					5.53	5.43			
5019	NB	5021	68-13-46	1383.391			-15.313		
			-46	.390			.335		
			00-00-00						
			M 68-13-46						
			68-13-48						
			-46						
			00-00-00						
			M 68-13-47						
5019	5021	NB	291-46-14						
			-14						
			00-00-00						
			M 291-46-14						
			291-46-12						
			-12						
			359-59-58						
			M 291-46-13						

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T	BS	FS	∡ RT	HO	HI	HT	+/-	ELEV	Desc
					5.60	5.60			
5021	5019	1261	125-55-00	26.892			+0.220		
			-00	.894			.220		
			00-00-00						
			∧ 125-55-00						
			125-55-00						
			-00						
			00-00-00						
			∧ 125-55-00						
5021	1261	5019	234-04-56						
			-56						
			00-00-00						
			∧ 234-04-56						
			234-04-56						
			-58						
			00-00-00						
			∧ 234-04-57						

T	BS	FS	∡	RT	HD	HI	HT	+/-	ELEV.	Desc.
5020	NB	1257				5.69	5.42			
			06-42-42		476.008			-6.534		
				-42	.005			.534		
			359-59-50							
			∧ 06-42-47							
			06-42-48							
				-48						
			00-00-00							
			∧ 06-42-48							
5020	1257	NB	353-17-14							
				-12						
			00-00-00							
			∧ 353-17-13							
			353-17-10							
				-14						
			359-59-58							
			∧ 353-17-13							

T	BS	FS	* RT	HD	HI	HT	+/-	ELEV.	Desc.
5020	N.B	1258			5.69	5.40			
			233-32-08	558.065			+5.397		
			-06	.066			.397		
			00-00-00						
			^ 233-32-07						
			233-32-10						
			-08						
			00-00-00						
			^ 233-32-09						
5020	1258	NB	126-27-54						
			126-27-52						
			00-00-02						
			^ 126-27-52						
			126-27-52						
			-52						
			359-59-56						
			^ 126-27-54						

T	B.S.	FS	∠ RT	HD	HI	HT	+/-	ELEV	Desc.
1259	NB	1260			5.40	5.45			
			347-28-18	287.939			-6.783		
			-16	.939			.779		
			359-59-58						
			∧ 347-28-18						
			347-28-18						
			-18						
			00-00-00						
			∧ 347-28-18						
1259	1260	NB	12-31-42						
			-42						
			00-00-00						
			∧ 12-31-42						
			12-31-38						
			-40						
			359-59-58						
			∧ 12-31-40						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc.
JWD	NB	1270			4.05	5.90			
			335-28-10	2323.312			-145.454		
			-12	.307			.472		
			00-00-00						
			^ 335-28-11						
			335-28-12						
			-12						
			00-00-00						
			^ 335-28-12						
JWD	1270	NB	24-31-52						
			-52						
			359-59-56						
			^ 24-31-50						
			24-31-50						
			-50						
			00-00-02						
			^ 24-31-49						

∡	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc.
					4.05	5.50			
JWD	NB	1269	329-59-02	2346.001			-15.961		
			-04	.002			.942		
			00-00-04						
			M 329-59-01						
			329-58-58						
			-59-00						
			359-59-58						
			M 329-59-00						
JWD	1269	NB	30-01-00						
			-00						
			00-00-00						
			M 30-01-00						
			30-01-00						
			-02						
			00-00-02						
			M 30-01-00						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	Desc.
					4.05	0.24			
JUD	N.B	1268	324-25-52	1959.852			-1458.18		
			-54	.853			.834		
			00-00-02						
			∧ 324-25-52						
			324-25-52						
			-52						
			00-00-00						
			∧ 324-25-52						
JUD	1268	NB	35-34-06						
			-06						
			359-59-58						
			∧ 35-34-07						
			35-34-08						
			-08						
			00-00-02						
			∧ 35-34-07						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	Desc.
					3.81	5.58			
New Robert	JuD	1301	234-08-06	1551.089			-96.570		
			-04	.088			.570		
			00-00-00						
			M 234-08-05						
			234-08-06						
			-06						
			00-00-00						
			M 234-08-06						
NR	1301	JuD	125-51-54						
			-54						
			00-00-00						
			M 125-51-54						
			125-51-59						
			-54						
			359-59-58						
			M 125-51-55						

T	BS	FS	∡ RT	HD	HT	HT	+/-	ELEV.	Desc.
					3.81	5.57			
NR	JWD	1304	238-48-26	2035.175			+84	327	
			-26	.177				.343	
			359-59-58						
			∧ 238-48-27						
			238-48-30						
			-28						
			00-00-00						
			∧ 238-48-29						
NR	1304	JWD	121-11-30						
			-32						
			00-00-00						
			∧ 121-11-31						
			121-11-32						
			-30						
			359-59-58						
			∧ 121-11-32						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc
					3.81	5.57			
NR	JuD	1288	241-05-02	2877.957			-64.012		
			-00	.962			-63.944		
			359-59-58						
			∧ 241-05-02						
			241-05-08						
			-00						
			00-00-00						
			∧ 241-05-00						
NR	1288	JuD	118-54-58						
			-58						
			00-00-00						
			∧ 118-54-58						
			118-54-56						
			-56						
			359-59-56						
			∧ 118-54-58						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	DESC
					3.81	5.15			
NR	JuD	1303	250-47-56	1890.976			-81.542		
			-56	.971			.572		
			00-00-00						
			M 250-47-56						
			250-47-56						
			-56						
			00-00-00						
			M 250-47-56						
NR	1303	JuD	109-12-00						
			-02						
			359-59-58						
			M 109-12-02						
			109-12-04						
			-02						
			00-00-00						
			M 109-12-03						

T	BS	FS	∡	RT	HD	HI	HT	+/-	ELEV	Desc
						3.81	5.35			
NR	JuD	1300	276-24-18		1611.321			-117.659		
				-18	.319			.671		
			00-00-02							
			M 276-24-17							
			276-24-16							
				-16						
			00-00-00							
			M 276-24-16							
NR	1300	JuD	83-35-42							
				-44						
			00-00-00							
			M 83-35-43							
			83-35-44							
				-44						
			00-00-00							
			M 83-35-44							

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	Desc
					3.81	9.64			
NR	JWD	1297	283-02-46	2506.939			+106.217		
			-46	.939			.217		
			359-59-58						
			M 283-02-47						
			283-02-48						
			-48						
			00-00-00						
			M 283-02-48						
NR	1297	JWD	276-57-12						
			-12						
			00-00-00						
			M 276-57-12						
			276-57-12						
			-10						
			00-00-02						
			M 276-57-10						

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV.	Desc
					381	9.73			
NR	JuD	1299	278-27-44	2686.455			-98.387		
			-42	.458			345		
			359-59-58						
			∧ 278-27-44						
			278-27-42						
			-42						
			00-00-00						
			∧ 278-27-42						
NR	1299	JuD	81-32-14						
			-16						
			359-59-56						
			∧ 81-32-17						
			81-32-18						
			-16						
			00-00-00						
			∧ 81-32-17						

T	BS	FS	∡ RT	HD
NR	JWD	1298	282-59-50	2994.768
			-48	.764
			00-00-00	
			∩ 282-59-49	
			282-59-46	
			-48	
			359-59-58	
			∩ 282-59-48	
NR	1298	JWD	77-00-12	
			77-00-10	
			00-00-00	
			∩ 77-00-11	
			77-00-10	
			-10	
			00-00-00	
			∩ 77-00-10	

HI	HT	+/-	ELEV	Desc.
3.81	5.34			
		-00.540		
		.634		

T	BS	FS	∠ RT	HD	HI	HT	+/-	ELEV	DESC
					3.81	5.34			
NR	JWD	1292	269-58-04	3126.741			-89.778		
			-06	.743			.704		
			00-00-00						
			M 269-58-05						
			269-58-06						
			-06						
			00-00-00						
			M 269-58-06						
NR	1292	JWD	90-01-54						
			90-01-54						
			00-00-00						
			M 90-01-54						
			90-01-50						
			-54						
			359-59-58						
			M 90-01-53						

T	BS	FS	∡	RT	HD	HI	HT	+/-	ELEV	DESC.
						3.81	5.45			
NR	JuD	1289	260-34-46		3502.470			-5.787		
				-48	.473			.785		
			00-00-00							
			∧ 260-34-47							
			260-34-48							
				-48						
			00-00-00							
			∧ 260-34-48							
NR	1289	JuD	99-25-12							
				-12						
			00-00-00							
			∧ 99-25-12							
			99-25-12							
				-12						
			00-00-00							
			∧ 99-25-12							

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	DESC
					3.81	5.90			
NR	JuD	1294	281-35-24	3943.330			+0.222		
			-26	.334			.222		
			00-00-00						
			∩ 281-35-25						
			281-35-24						
			-24						
			00-00-00						
			∩ 281-35-24						
NR	1294	JuD	78-24-34						
			-36						
			00-00-00						
			∩ 78-24-35						
			78-24-34						
			-32						
			00-00-00						
			∩ 78-24-33						

T	BS	FS	∢	RT	HD	HI	HT	+/-	ELEV	Desc
						3.81	5.36			
NR	JuD	1296	294-43-52		3095.865			+106.928		
				-54	.871			.831		
			00-00-00							
			∩ 294-43-53							
			294-43-52							
				-54						
			00-00-00							
			∩ 294-43-53							
NR	1296	JuD	65-16-06							
				-06						
			00-00-00							
			∩ 65-16-06							
			65-16-08							
				-08						
			00-00-00							
			∩ 65-16-08							

T	BC	FS	∠	RT	HD	HI	HT	+/-	ELEV	line Desc
						3.81	5.49			
NR	JuD	1284	262-38-16		4988.815			-21.595		
				-14	.823			.608		
			359-59-58							
			M 262-38-16							
			262-38-16							
				-18						
			00-00-00							
			M 262-38-17							
NR	1284	JuD	97-21-46							
				-44						
			00-00-04							
			M 97-21-43							
			97-21-44							
				-44						
			00-00-00							
			M 97-21-44							

T	BS	FS	∡	RT	HD	HI	HT	+/-	ELEV.
						3.81	5.38		
NR	JuD	5022	254-30-42		3834.173			-5.762	
				-42	.174			.796	
			00-00-00						
			∧ 254-30-42						
			254-30-44						
				-40					
			00-00-02						
			∧ 254-30-41						
NR	5022	JuD	105-29-20						
				-18					
			00-00-00						
			∧ 105-29-19						
			105-29-18						
				-18					
			359-59-56						
			∧ 105-29-20						

T	BS	FS	∡	∠T	HD	HI	HT	+/-	ELEV	DESC
						5.37	5.49			
5022	NR	1290	244-47-42		1183.334			-30.257		
				-40	.335			.257		
			00-00-00							
			∧ 244-47-41							
			244-47-40							
				-40						
			00-00-00							
			∧ 244-47-40							
5022	1290	NR	115-12-20							
				-22						
			00-00-00							
			∧ 115-12-21							
			115-12-20							
				-20						
			00-00-00							
			∧ 115-12-20							

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	Desc
					5.37	5.49			
5022	NR	1291	262-41-10	1459.134			-8.047		
			-12	.138			.058		
			00-00-00						
			∧ 262-41-11						
			262-41-12						
			-12						
			00-00-00						
			∧ 262-41-12						
5022	1291	NR	97-18-50						
			-50						
			00-00-02						
			∧ 97-18-49						
			97-18-48						
			-48						
			00-00-00						
			∧ 97-18-48						

T	BS	FS	∠ RT	HD	HI	HT	+/-	ELEV	Desc
					5.37	5.50			
5022	NR		267-46-30	509.883			-44.341		
			-28	.885			.341		
			00-00-02						
			M 267-46-28						
			267-46-28						
			-28						
			00-00-00						
			M 267-46-28						
5022		NR	92-13-32						
			-30						
			00-00-00						
			M 92-13-31						
			92-13-32						
			-34						
			00-00-00						
			M 92-13-33						

BOOK 3

T	BS	FS	∠ RT	HC	HI	HT
5022	NR	1282			5.37	5.54
			217-51-48	1948.146		
			-46	.147		
			00-00-00			
			∧ 217-51-47			
			217-51-44			
			-46			
			00-00-00			
			∧ 217-51-45			
5022	1282	NR	142-08-16			
			-14			
			00-00-00			
			∧ 142-08-15			
			142-08-16			
			-16			
			00-00-00			
			∧ 142-08-16			

+/-	ELEV	DESC.
2.147		
.208		

⊼	BS	FS	∡Rt.	H.D.	DESC.
123A	Sweat	623A	D. 94-34-11		Set P.C. in punty
			R. 274-32-55		split prop. cor PC
			H. 180-00-10		
			M. 94-33-58	9.64	

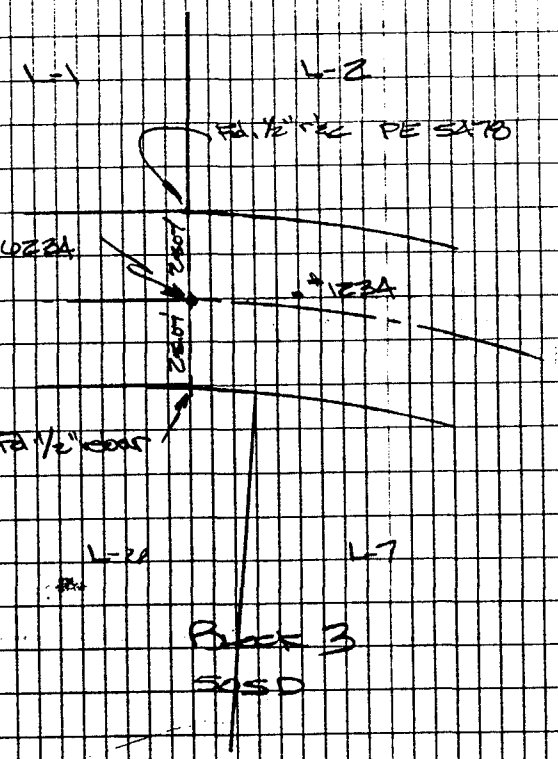
STA	+	HI	-	EL	DESC
123A					TBM
	5.81				
623A			5.35		T.P.
	5.41				
123A			5.88		TBM

123

Centipede \ West End 9/30/91

JF

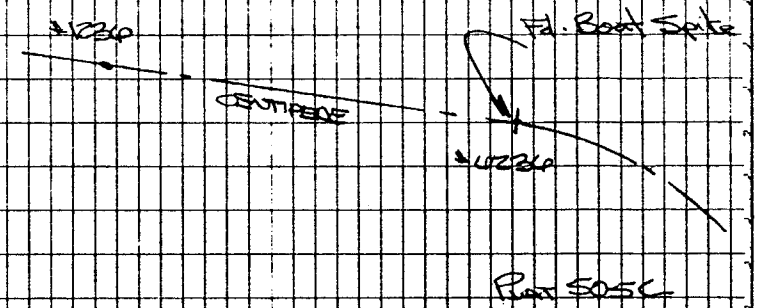
JW



T	BS	FS	∡Rt	H.D.	Desc.
1236	Sweat	6236	261-45-20	336.209	
			261-45-20	336-208	
			359-59-58		
			m. 261-45-21		
			261-45-24		
			261-45-24		
			0-0-0		
			m. 261-45-24		

STA	T	HI	—	EL.	DESC.
1236					TBM
	1.83				
6236			15.84		Boat Spike T.P.
	15.71				
1236			1.70		TBM

Centipede \\ East End 9/30/91

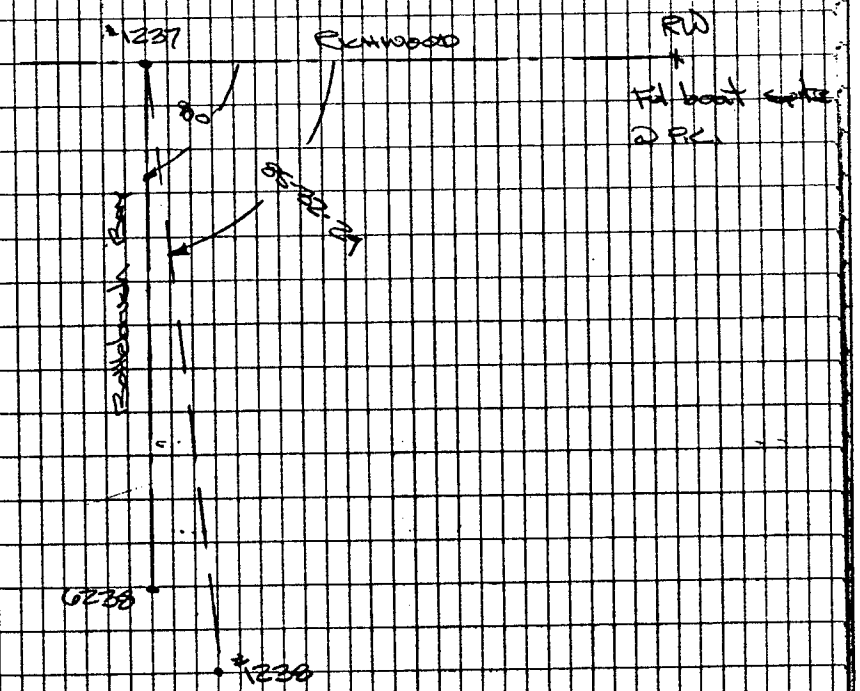


⊼	BS	FS	∠Rt.	H.D.	DESC.
1237	RW	1238	85-32-30		
			85-32-26		
			0-0-0		
			m. 85-32-28		
			85-32-30		
			85-32-28		
			359-59-58		
			m. 85-32-30		
1237	RW	6238	90-00-00	255.00	Set nail 0.20 below surface

STA	+	HI	-	EL.	DESC.
1238					TBM
	3.81				
6238			5.42		T.P.
	5.47				
1238			3.86		TBM

9/30/91

BOTTLEBRUSH BAY



A	BS	FS	∡Rt	H.D.	DESC.
1235	SWEAT	6235	281-07-12	248.570	Split returns N
			281-07-10	.572	end of Kim Dr.,
			359-59-56		set nail
			m.		
			281-07-10		
			281-07-12		
			0-0-0		
			m.		

STA	+	HI	−	EL.	DESC.
1235					TBM
	1.36				
6235			16.57		T.P.
	16.81				
1235			1.60		TBM

Kim Dr.

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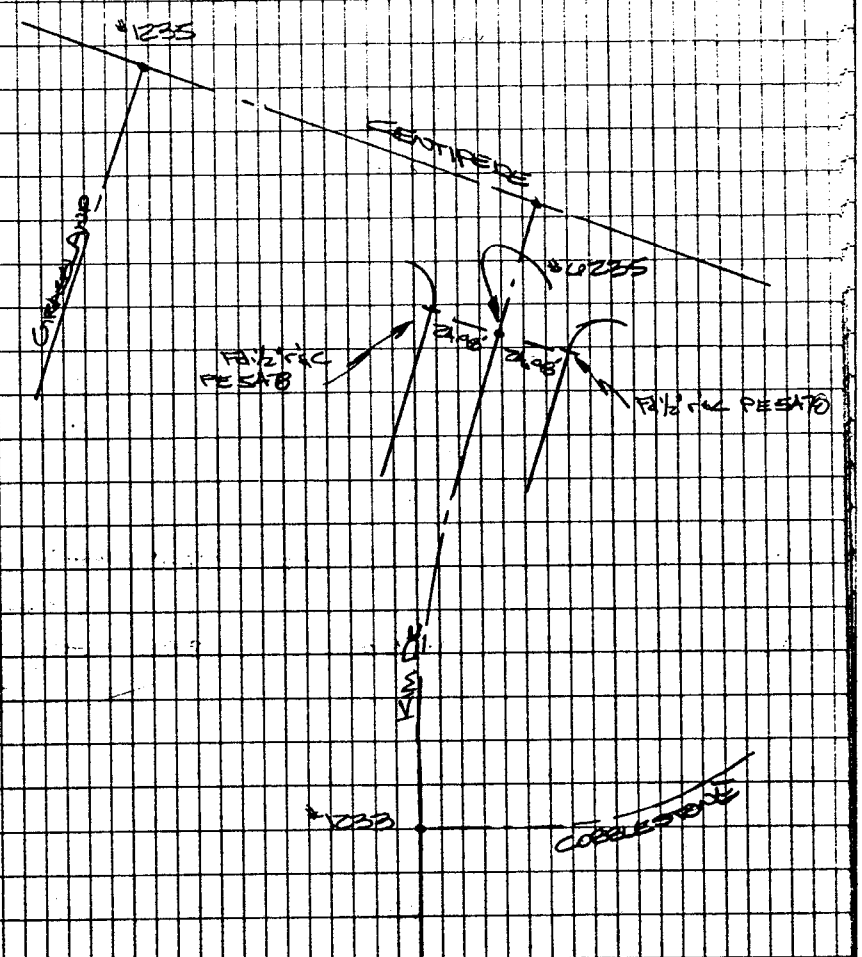
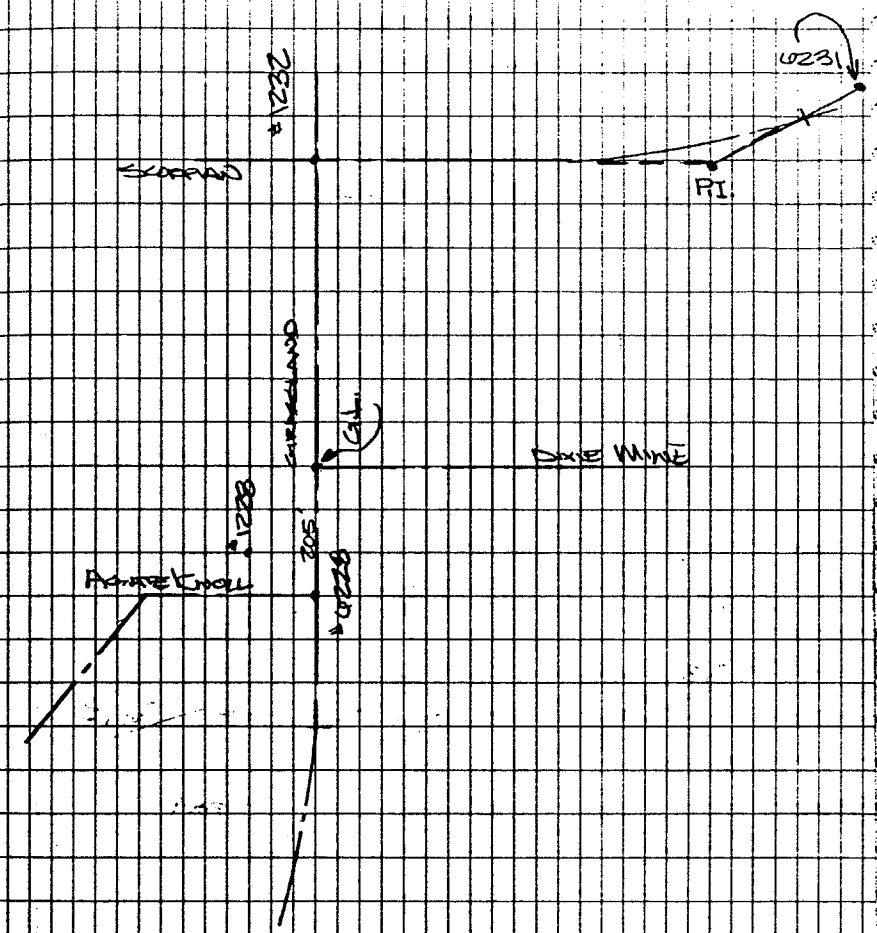


9/30/91

⊼	BS	FS	∠Rt	H.D.	DESC.
1232	1228	G.L.	354-01-28	250.044	Fd. Boat Spike @
			354-01-30	.043	Int.
			359-59-58		
			M.		
			354-01-30		
			354-01-30		
			0-0-0		
			M.		
1232	G.L.	6228	0-00-00	455.04	Set nail @ Int. Agate Knoll & Grassland
1232	G.L.	P.I.	270-00-00	357.31	Set nail @ P.I. on Scorpion
P.I.	1232	6231	103-00-00	128.88	Set nail @ Rad. Pt. Scorpion

STA	+	HI	−	EL	DESC
1231					TBM
	4.89				
6231			5.43		TP Rad Pt.
	5.58				
1231			5.04		TBM

GRASSLAND & SCORPION



STA	+	HI	−	EL	DESC.
1228					TBM
	1.98				
6228			5.12		T.P. Int.
	4.88				
1228			1.74		TBM

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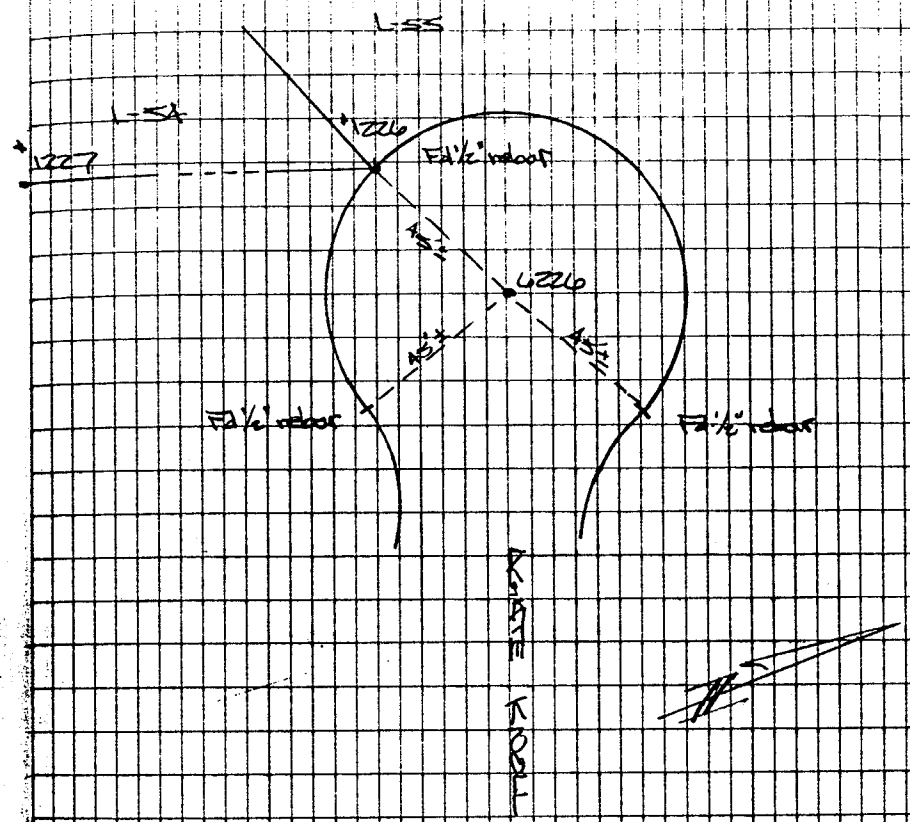
Π	BS	FS	∡Rt	H.D.	DESC.
1226	1227	6226	D 205-23-00	45.01	Set nail @ Rad Pt.
			R 25-23-12		of Agate Knoll
			H 180-00-14		
			M 205-22-59		
			D 205-23-02		
			R 205-22-49		
			H 179-49-48		
			M 205-23-01		

Sta	+	HI	-	El.	Desc.
1226					TBM
	4.39				
6226			5.46		TP Rad Pt.
	5.38				
1226			4.30		TBM



∡	BS	FS	∡ Rt.	HD	Desc.
1227	1226	6227	P 80-00-53	60.50	Set nail @ Rad Pt.
			R 260-00-17		Grassland
			H 180-00-13		
			M 80-00-29.5		
			P 80-00-00		
			R 260-00-51		
			H 179-59-48		
			M 80-00-31		

Sta	+	HI	−	EL	Desc.
1227					TBM
	2.63				
6227			5.55		TP Rad Pt
	5.49				
1227			2.56		TBM

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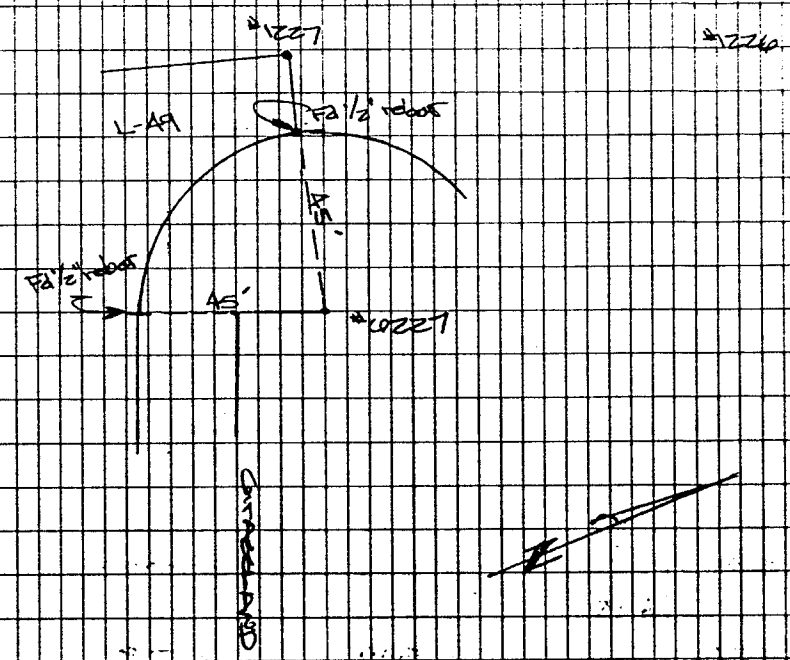
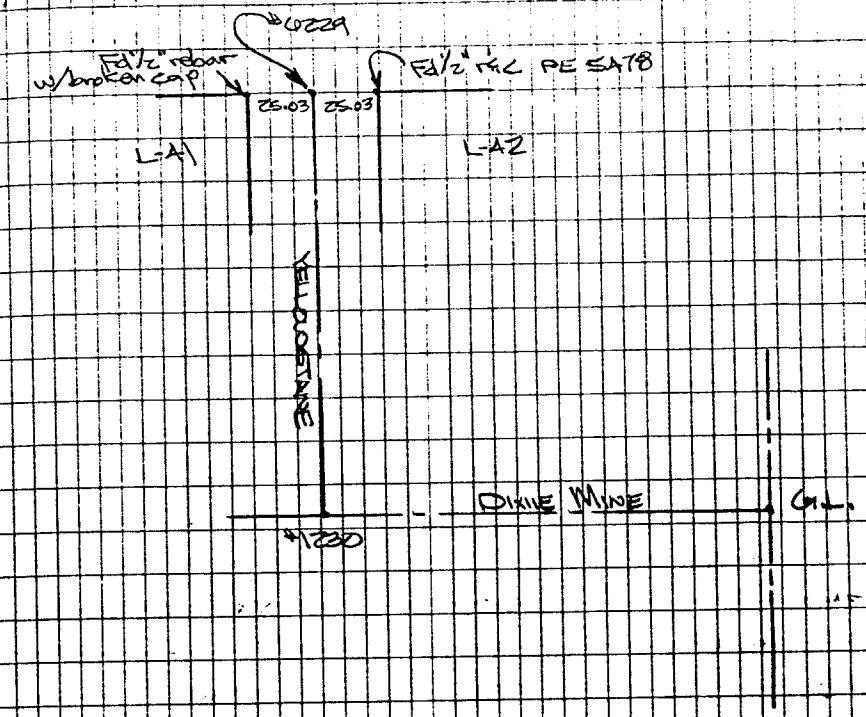


T	BS	FS	∡Rt.	HD	DESC.
1230	G.L.	6229	269-58-50	224.901	Set nail @ S.
			-52	.901	end Yellowstone,
			00-00-00		split prop. cors.
			m 269-58-51		
			269-58-52		
			269-58-50		
			0-0-0		
			m 269-58-51		

STA	+	HI	−	EL.	DESC.
1229					TBM
	4.95				
6229			5.10		TP
	5.32				
1229			5.17		TBM

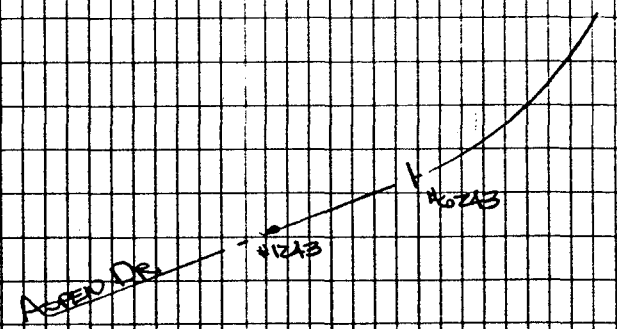
YELLOWSTONE 9/30/91



⊼	BS	FS	∡Rt	H.D	DESC
12A3	DEB	62A3	67-12-30	24.25	Fd. pvmt. nail @ ℄ P.C. Aspen Dr.

STA	+	HI	−	EL	DESC
12A3					TBM
	4.35				
62A3			6.03		T.P. ℄ P.C. Pvmt. nail
	5.97				
12A3			4.29		TBM

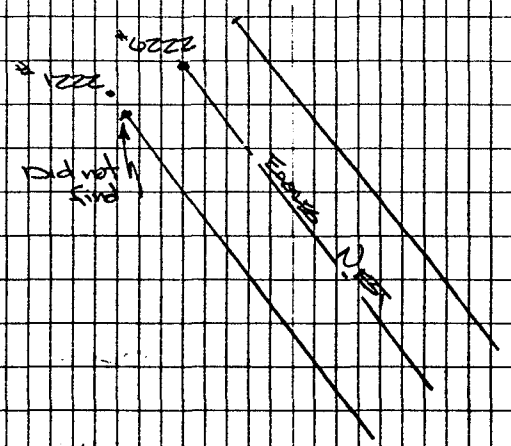
ASPEN DR. 9/30/91



$\bar{\pi}$	BS	FS	XPt.	HD	DESC.
1222	SWEAT	6222	220-18-06	24.38	Set nail @ record position

STA	+	HI	−	EL.	DESC
1222					TBM
	5.12				
6222			5.51		℄ P.C. T.P.
	5.64				
1222			5.25		TBM

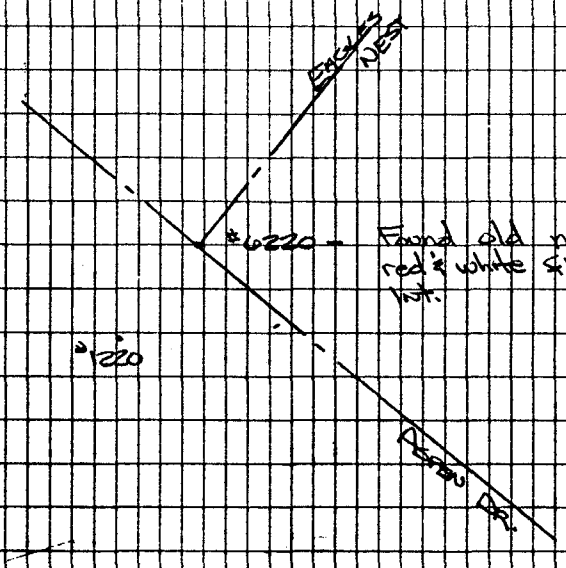
EAGLES NEST 10/1/91



T	BS	FS	X.Pt.	H.D.	DESC.
1220	Sweet	6220	D. 203-39-05	23-78	
			R. 23-39-14		
			H. 180-00-15		
			m. 203-39-02		
			D. 203-38-57		
			R. 23-38-47		
			H. 179-59-36		
			m. 203-38-04		

Sta	+	HI	-	El.	Desc.
1220					TBM
	A.33				
6220			A.78		T.P. Int.
	A.68				
1220			A.23		TBM

ASPEN & EAGLES NEST 10/1/91

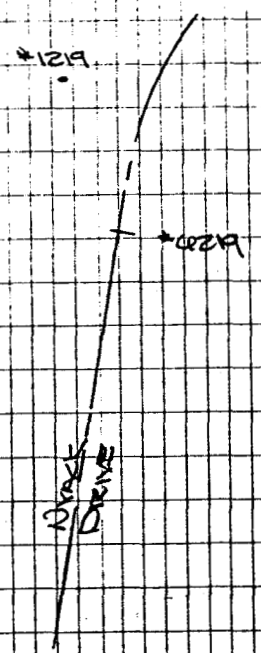


π	BS	FS	∡Rt.	H.D.	Desc.
1219	Sweat	6219	329-48-55	66.44	Set nail @ record position

STA	+	HI	−	EL.	DESC.
1219					TBM
	1.52				
6219			13.43		T.P. PC
	13.49				
1219			1.58		TBM

13A
10/1/91

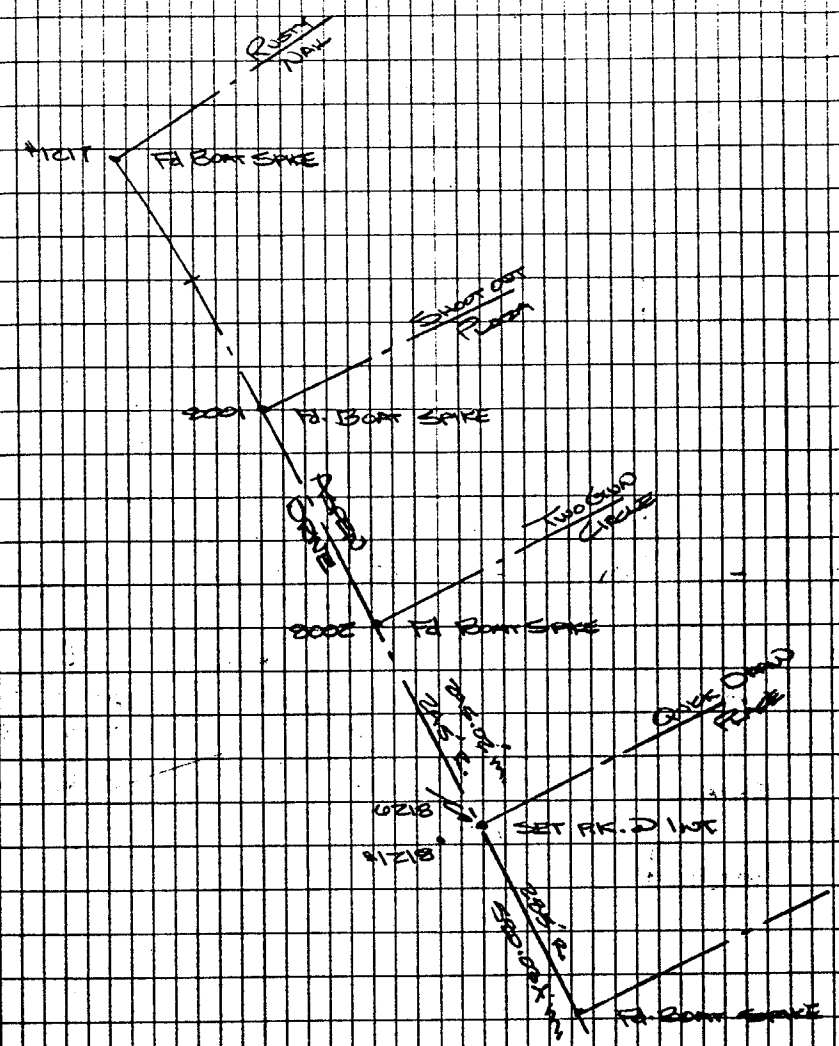
NYACK



A	BS	FS	∠R	HD	DESC.
1217	ALLED	6218	307-39-16	804.419	
			-16	.418	
			00-00-00		
			m 307-39-16		
			307-39-18		
			-18		
			00-00-00		
			m 307-39-18		
1217	ALLED	8002	307-33-12	509.426	
			-08	.425	
			00-00-00		
			m 307-33-10		
			307-33-12		
			-10		
			00-00-00		
			m 307-33-11		
1217	ALLED	8001	307-14-30	239.480	
			-30	.477	
			00-00-02		
			m 307-14-29		
			307-14-30		
			-30		
			00-00-02		
			m 307-14-29		

STA	+	HI	−	EL	DESC
1217	1.41				TBM
8001			8.76		JP
	2.29				
8002			8.64		JP
	1.43				
6218			8.100		JP
	8.82				
1218			8.79		TBM

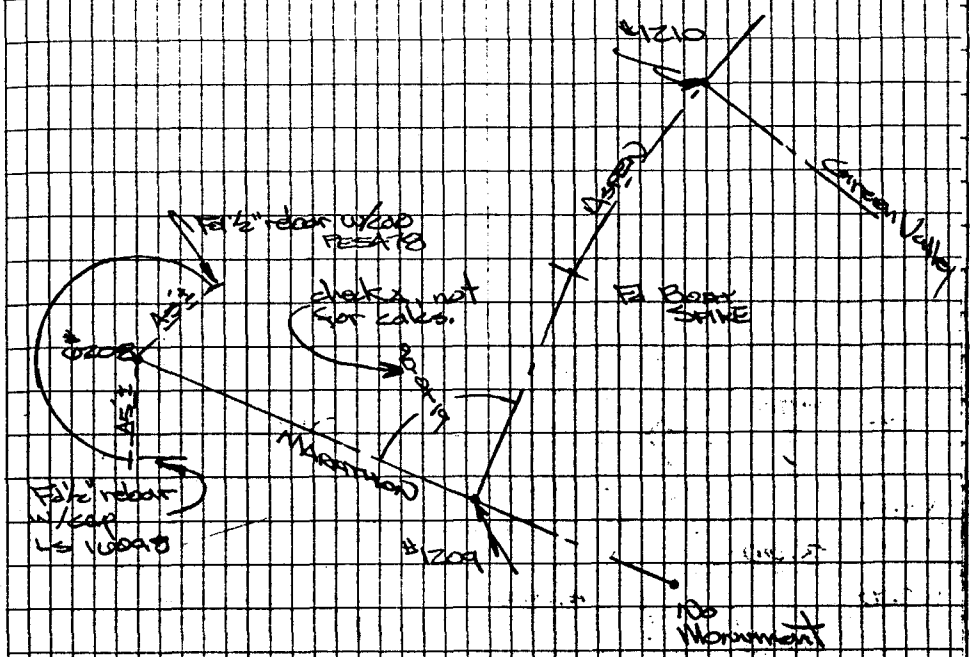
10/1/91



T	BS	FS	∠Rt.	H.D.	
1209	1210	1208	202-55-02	500.00	Set nail 2
			202-55-02	500.00	rad. pt.
			0-0-0		
			m.		
			202-55-00		
			202-55-00		
			359-59-58		
			m		

STA	+	H	−	El.	Desc.
1208					TBM
	4.50				
1208			5.53		
	5.04				
1208			4.02		

MARATHON 1/2/91



T	BS	FS	ΔPt	H.D	Desc.
1206	1207	6207	01-10-14	205.00	Set nail @
			-18		rad-pt. in line
			00-00-08		with prop corr
			m		17/18
			01-10-14		
			-14		
			00-00-00		
			m		

STA	+	HI	−	EL.	Desc.
1207					TBM
	3.60				
6206			5.55		TP. Rad Pt.
	5.45				
1207			3.50		TBM

KT FOX

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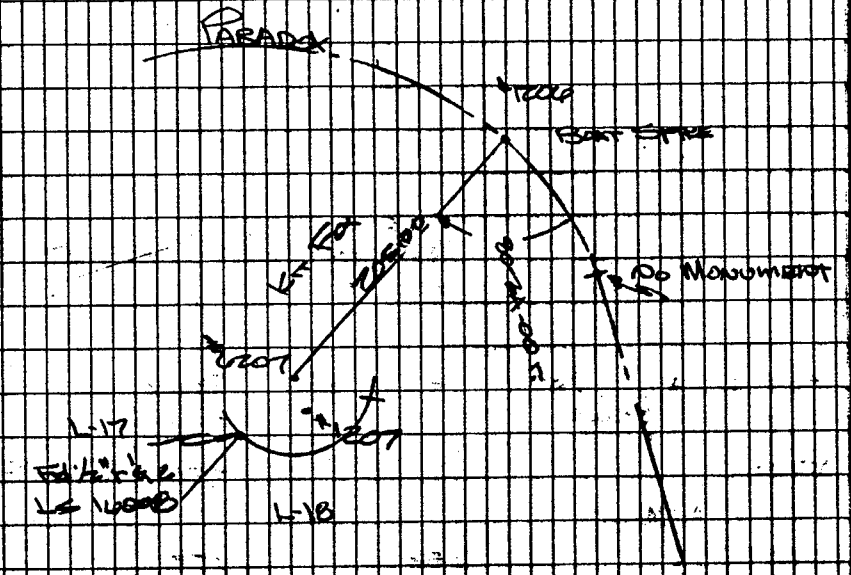
10/2/91

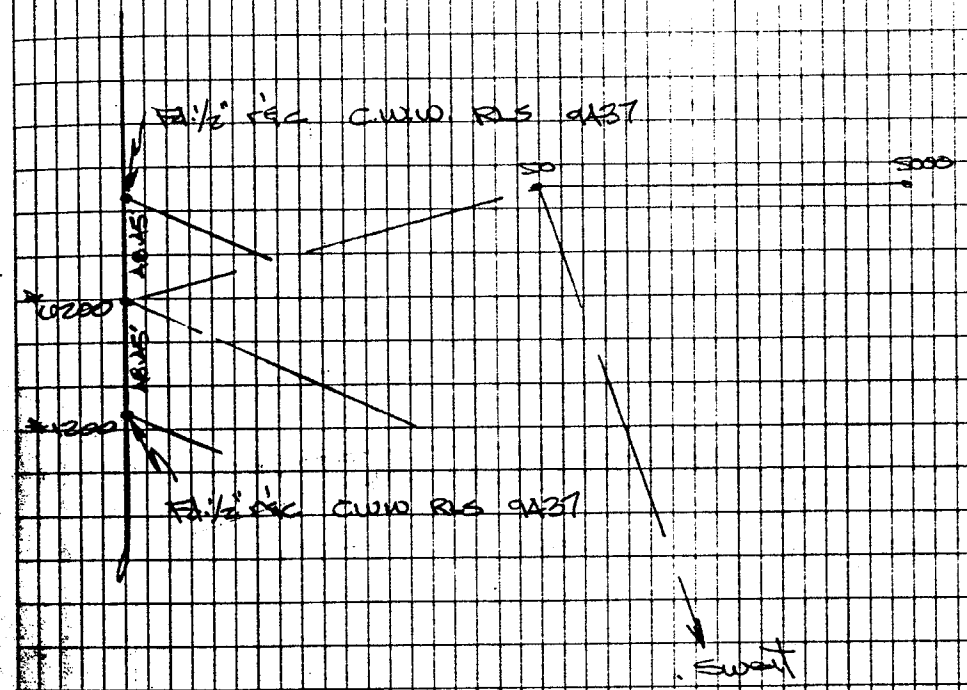


∧	BS	FS	∡Rt.	HD	Desc.
50	5000	6200	168-49-38	3390.364	Set nail @ West
			-40	3390.365	Bdry. of Plat 5000
			00-00-06		@ ℄ Golden Eagle
			m		
			168-49-30		
			-30		
			359-59-48		
			m		
50	Sweat	6200	104-39-38		
			-34		
			259-59-58		
			m		
			104-39-38		
			-38		
			00-00-00		
			m		

Sta	+	HI	-	El.	Desc.
1200					TBM - Panel Pt.
	4.74				
6200			6.58		T.P.
	6.50				
1200			4.64		TBM

GOLDEN EAGLE 138

10/2/91



⊼	BS	FS	∠Rt.	H.D.	
5000	ALLEN	205	A5-36-55	205.86	Set nail @ record position

STA	+	HI	−	EL	DESC.
1205					TBM
	1.96				
6205			8.02		T.P. P.C.
	7.92				
1205			1.86		TBM

CERRO ALTO

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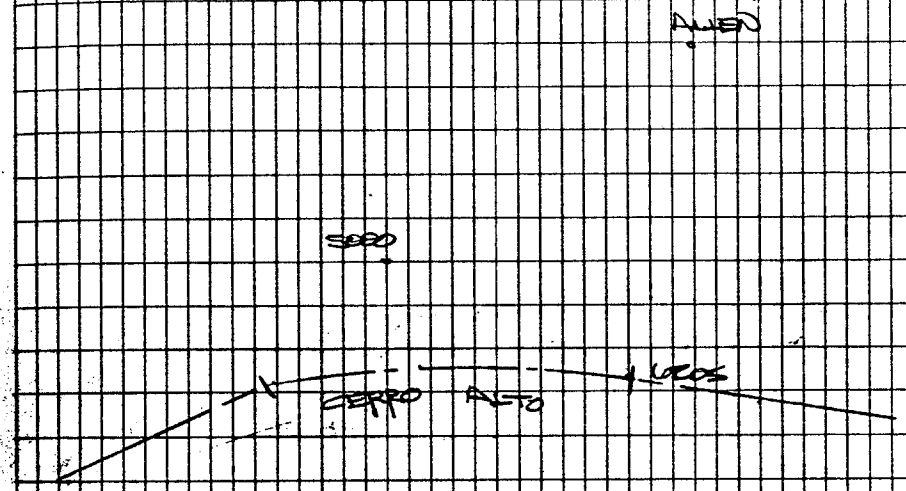
10/2/91



A	BS	FS	∡Pt.	HD	DESC.
1215	5000	6215	0-00-00	44.98	Int. Boxcar & Pageland, Bent Spike
1216	Sweat	6216	D 96-09-45	34.47	Set nail @ ℄
			R 276-09-59		∡pt. @ Rad. Pt
			H 180-00-20		
			M -A2		
			D 96-09-29		
			R 279-09-44		
			H 179-59-46		
			M -A3		

Sta	+	HI	-	El.	DESC.
1215					TBM
	4.39				
6215			5.71		T.P. Int.
	5.61				
1215			4.79		TBM
1216					TBM
	5.32				
6216			5.10		T.P. ℄ ∡pt.
	5.04				
1216			5.26		TBM

PAGELAND

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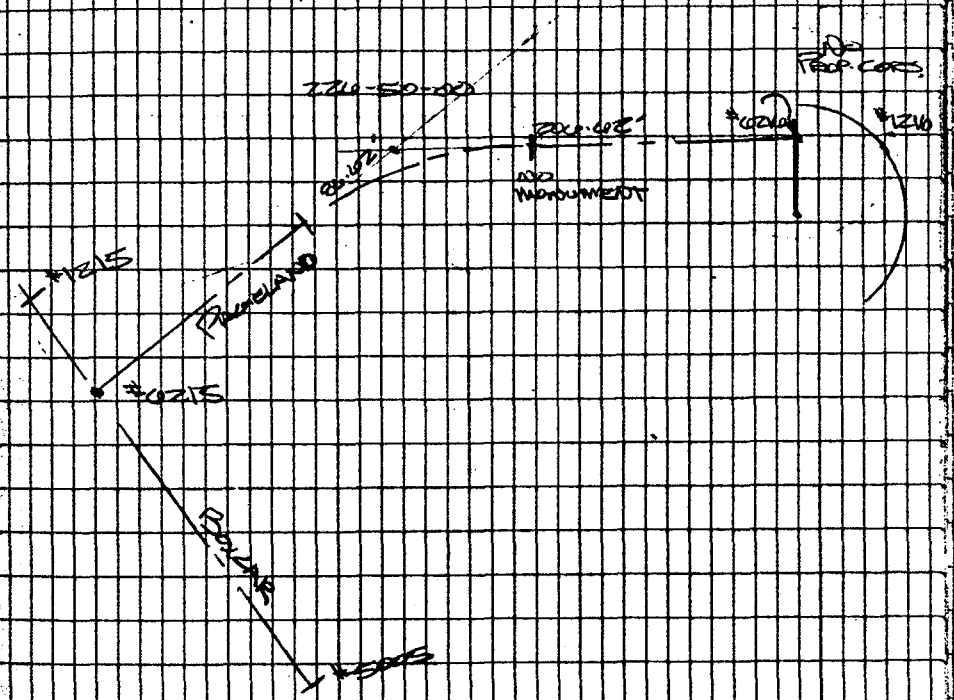
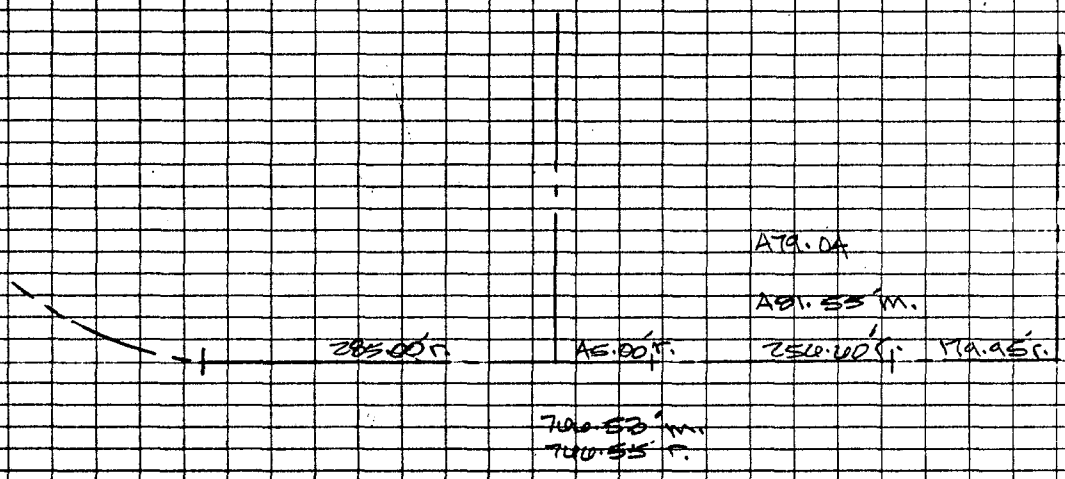
10/2/91
10/3/91



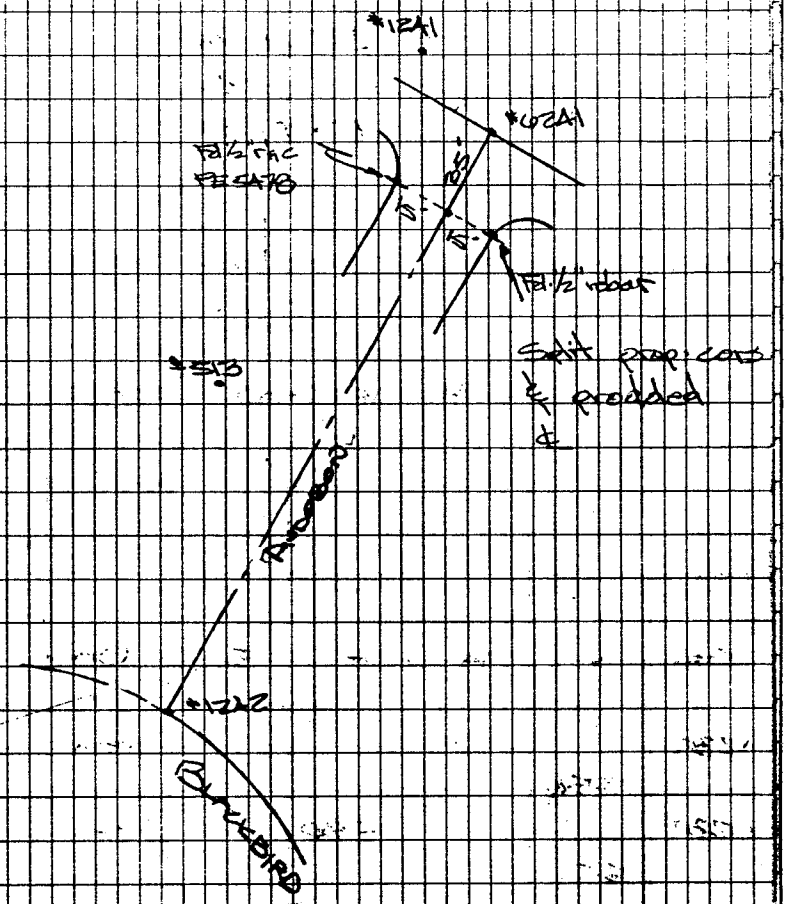

A79.04
A81.55 m.
285.00 r.
A5.00 r.
256.60 r.
179.95 r.
766.53 m.
766.55 r.

⊼	BS	FS	∡ Rt	H.D.	Desc
12A1	513	62A1	D 292-06-03	31.30	set nail @ ℄
			R 112-05-54		& pt. hammerhead
			H 180-00-09		
			M 292-06-04		
			D 292-06-04		
			R 112-05-51		
			H 179-59-59		
			M 292-05-58		

STA	+	HI	−	EL	Desc
12A1					TBM
	4.48				
62A1			5.31		TP
	5.24				
12A1			4.41		TBM

AUDUBON 142

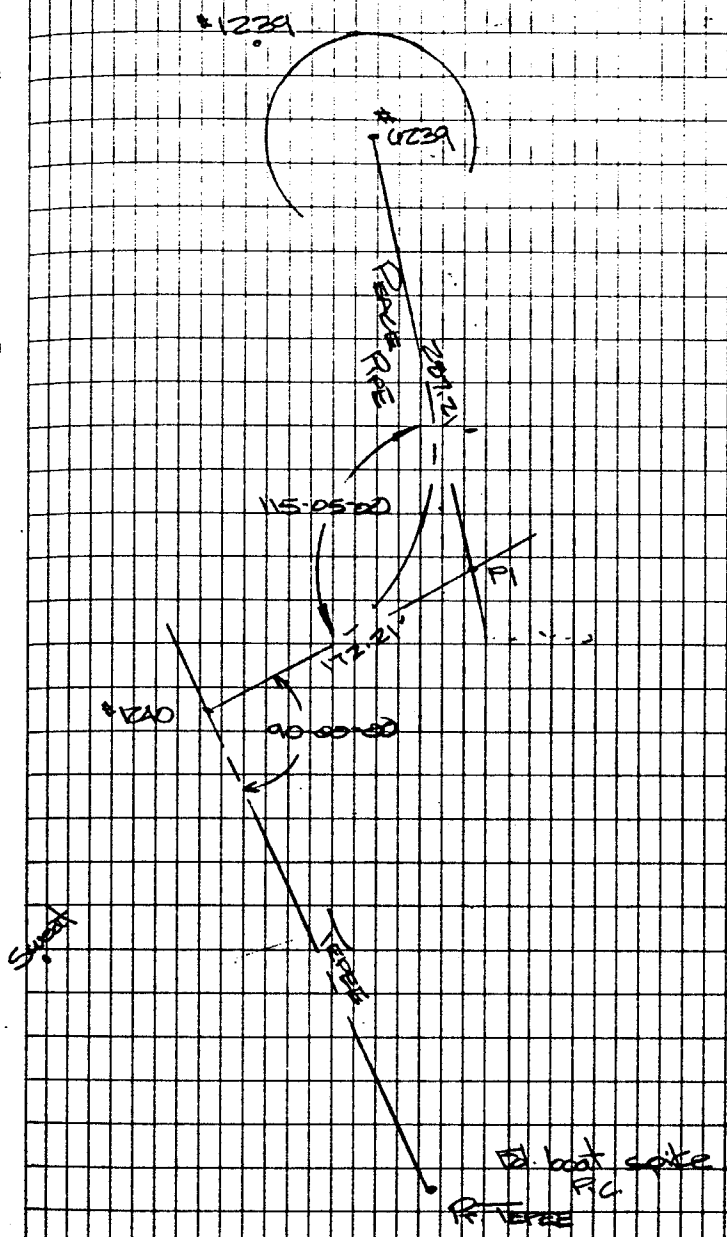
10/3/91



⊼	BS	FS	∠Rt.	HD	DESC
1240	Sweat	Tepee	285-21-26		
			-24		
			00-00-02		
			m		
			285-21-84		
			-24		
			00-00-00		
			m		
1240	Tepee	P1	270-00-00	172.21	Set P1
P1	1240	6239	115-05-00	287.21	Set nail @ rad. pt.

STA	+	HI	−	EL	DESC
1239					TBM
	2.54				
6239			5.80		TP
	5.71				
1239			2.45		TBM

Peace Pipe 10/3/91 143



T	BS	FS	∡R.	H.D.	DESC.
S017	S002	S023	149-12-14	2052.290	Fd. prop. cor
			-10	.289	P.C. N. side
			00-00-02		Glenbrook
			m		
			149-12-10		
			-10		
			359-59-58		
			m		
S017	Sweet	S023	220-05-12		
			-12		
			00-00-00		
			m		
			220-05-12		
			-12		
			259-59-58		
			m		

AA
6/3/91

T	BS	F.S.	∠RT	HD	Desc
5017	5002	5024	186-27-40	1072.088	Set hor. pt.
			-40	.093	Dogwood Ln.
			00-00-00		
			M		
			186-27-42		
			-42		
			00-00-02		
			M		
5017	Sweat	5024	257-20-44		
			-46		
			00-00-00		
			M		
			257-20-46		
			-44		
			00-00-00		
			M		

	π	B.S.	F.S.	∢ RT	HD	DESC.
S	5017	5002	1278	.203-52-12	2981.974	B.C. @ Int.
				-14	.973	Hampstead
				.00-00-00		& Montrose
				M		
				.203-52-12		
				-14		
				.359-59-58		
				M		
S	5017	SWEAT	1278	.275-45-16		
				-14		
				.00-00-02		
				M		
				.274-45-14		
				-12		
				.359-59-58		
				M		

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A	BS	F.S.	∠ RT	HD	DESC.
5017	5002	1281	.185-28-06	3841.170	Fd. bent spike
			. -06	.167	@ Int. Greenhurst
			.00-00-06		& Fairlyn
			M		
			.185-28-02		
			. -02		
			.00-00-00		
			M		
5017	SWEAT	1281	.256-20-52		
			. -50		
			.359-59-58		
			M		
			.256-20-52		
			. -54		
			.259-59-58		
			M		

⊼	BS	F.S.	∡ RT	HD	DESC.
1278	5017	1279	144-02-48	658.195	
			-48	.196	
			00-00-00		
			M		
			144-02-50		
			-48		
			00-00-00		
			M		

SA	+	HI	−	EL	DESC.	
			M			
1279					TBM	Panel Pt.
	2.23					
6279			10.66		T.P.,	P.C.
	10.56					
1279			2.13		TBM	

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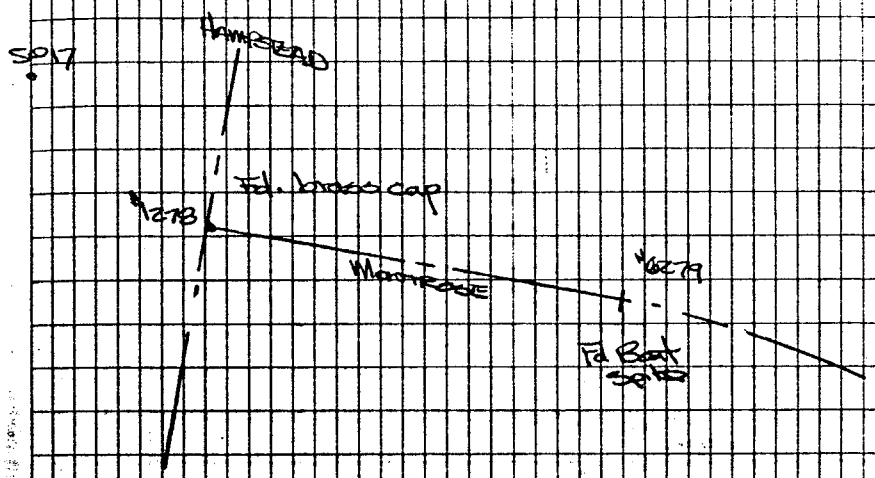
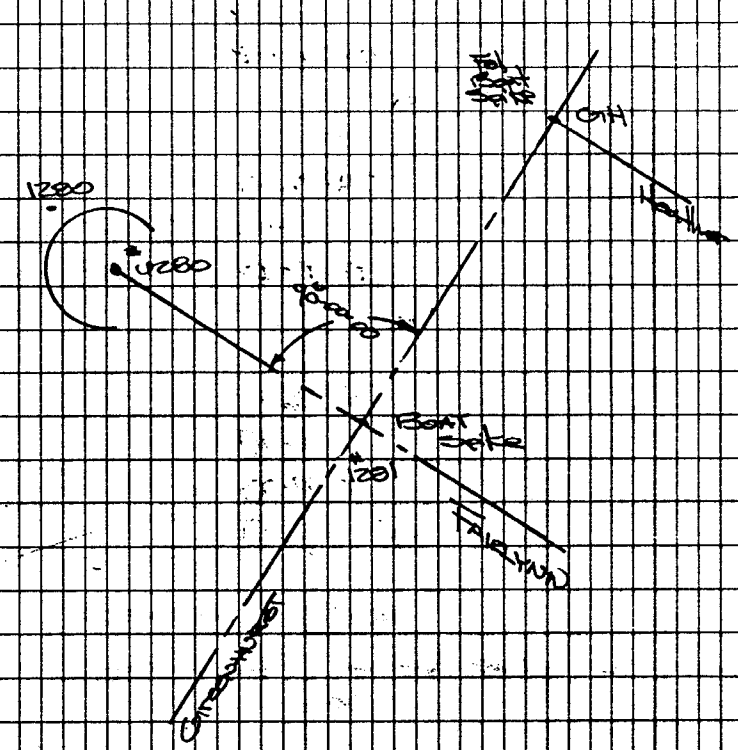
MONTROSE



T	BS	FS	Ht.	H.D.	Desc.
1281	GH	1280	270-00-00	215.00	Set nail @ Road Pt. 90° off ℄ Greenhouse
1281	5017	GH	87-27-16		
			87-27-18		
			0-00-00		
			87-27-14		
			87-27-16		
			0-0-02		

Sta	+	HI	−	El.	Desc.
1280					TBM Panel Pt.
	3.34				
1280			5.88		TP Road Pt.
	5.76				
1280			3.22		TBM



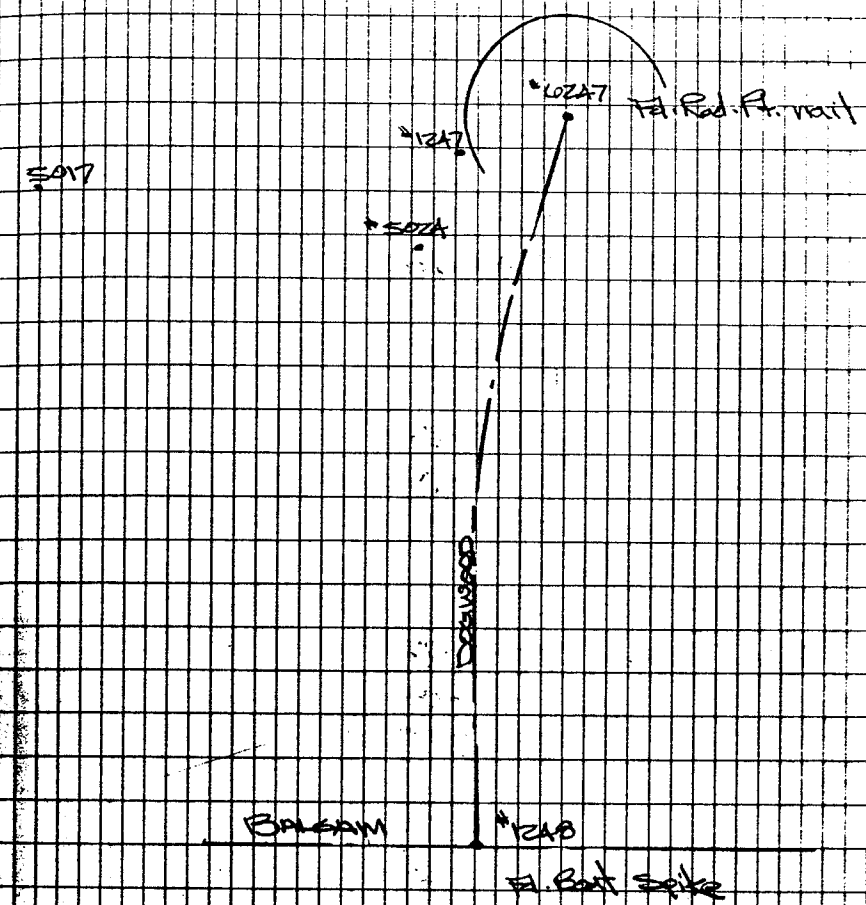
T	BS	FS	∠Rt.	H.D.	Desc.
502A	501A	102A7	108-54-54	81.004	Fd. nail @ Rad. Pt.
			-54	81.003	
			00-00-00		
			m		
			108-54-58		
			-54		
			00-00-02		
			m		
502A	501A	12A8	242-06-40		Fd. Bolt spiked
			-40	352.263	Int. Balsam &
			00-00-00	.263	Dogwood
			m		
			242-06-42		
			-40		
			00-00-00		
			m		

Sta	+	HI	–	El.	Desc.
12A7					TBM Panel Pt.
	3.46				
102A7			5.23		TP
	5.04				
12A7			3.47		TBM

Dogwood

150

10/3/91



TI	FS	FE	ZRT	HD	HI	HT
Fadukr	Pat	1148	155-41-24		3.22	2.83
			-36	3338287		
			00-00-00	.289		
			∩			
			155-41-30			
			-28			
			150-59-56			
			∩			
P.D.	1148	Pat	204-18-28			
			-26			
			00-00-00			
			∩			
			204-18-28			
			-28			
			00-00-00			
			∩			
P.D.	Rena	1148	308-24-24			
			-24			
			00-00-00			
			∩			
			308-24-24			
			-24			
			00-00-00			
			∩			
PD	1148	Rena	51-35-36			
			-36			
			00-00-00			
			∩			
			51-35-36			
			-36			
			00-00-00			

A/+	ELEV	Desc		Validity
-209.37				JF
-209.45	1075.08	Sec. Cor.	29/28 / 32/33	JW
		2.79' above ground		
		EW# A360		
		record elev. = 1075.82		

T	BS	FS	∡RT	HD	HI	HI	HI	ELEV	Dist
PD.	Pat	1150	12-07-52		3.22	4.55			
			12-07-52	2160384					
			359-59-52	.378					
			^						
			12-07-56						
			-56						
			00-00-00						
			^						
PD.	1150	Pat	347-52-04						
			-04						
			00-00-00						
			^						
			347-52-02						
			-00						
			359-59-58						
			^						
PD	Rena	1150	164-50-48						
			-50						
			00-00-00						
			^						
			164-50-52						
			-50						
			00-00-04						
			^						
PD	1150	Aena	195-09-06						
			-08						
			359-59-56						
			^						
			195-09-10						
			-08						
			359-59-58						

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HI	ELEV	Dist
292.564		
.615	1080.78	

Sec. Cor. 28/27 33/34

0.80' above ground
BM#153
record elev = 1080.71

T	BS	FS	∡ RT	HD	HI	HT	+/-	ELEV	K-CT
Pat	PD.	1153	153-47-42		3.33	8.65			
			-40	2230.129			-127.319		
			00-00-00	.126			.355		
			M						
			153-47-42						
			-42						
			00-00-00						
			M						
Pat	1153	PD.	206-12-20						
			-22						
			00-00-00						
			M						
			206-12-22						
			-22						
			00-00-02						
			M						
Pat	Sweat	1153	114-07-02						
			-04						
			359-59-58						
			M						
			114-07-02						
			-02						
			00-00-00						
			M						
Pat	1153	Sweat	245-52-56						
			-56						
			00-00-00						
			M						
			245-52-52						
			-56						
			359-59-56						

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T	BS	FS	∡ RT	HD	HI	HT	HI	ELEV	DESC	10/10/91
Pat	PD	5025	64-49-18		3.33	5.53				
			-20	5093.450			12.324		SET TRAV. PT. N. SIDE GREENBRIAR	
			00-00-00	.459			.324			
			M							
			64-49-20							
			-20							
			00-00-00							
			M							
Pat	5025	PD	295-10-38							
			-38							
			359-59-58							
			M							
			295-10-40							
			-40							
			00-00-02							
			M							
Pat	Sweat	5025	25-08-42							
			-44							
			359-59-58							
			M							
			25-08-44							
			-44							
			00-00-00							
			M							
Pat	5025	Sweat	334-51-16							
			-16							
			00-00-00							
			M							
			334-51-14							
			-14							
			00-00-00							

T	BS	FS	∡ Rc	HD	HI	HT
ΔPAT	PADIC	1144	104-56-36	6498.810	3.39	
			104-56-36	.806		
			359-59-58	.808		
			M.			
			104-56-36			
			104-56-36			
			0-0-02			
			M.			
PAT	1144		255-03-26			
			255-03-26			
			0-0-0			
			M			
			255-03-24			
			255-03-22			
			0-0-0			
			M			
PAT	Sweat	1144	65-15-48			
			65-15-44			
			359-59-58			
			M.			
			65-15-48			
			65-15-46			
			0-0-0			
			M			
PAT	1144	Sweat	294-44-10			
			294-44-12			
			0-0-0			
			M			
			294-44-12			
			294-44-12			
			0-0-0			
			M			

∡	El	Desc	

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JF
JW

T	BS	FS	∠ Right	HD	HI	HT
Pat	Paduc	5026	28-51-10	954.092	3.39	5.25
			-06	.092		
			00-00-00			
			M			
			28-51-03			
			-03			
			00-00-00			
			M			
Pat	5026	Paduc	331-08-52			
			-52			
			00-00-00			
			M			
			331-08-52			
			-50			
			00-00-00			
			M			
Pat	Sweat	5026	349-10-18			
			349-10-14			
			359-59-56			
			M			
			349-10-16			
			-18			
			00-00-00			
			M			
Pat	5026	Sweat	10-49-46			
			-44			
			00-00-00			
			M			
			10-49-42			
			-44			
			00-00-00			
			M			

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H/-	ELEV	Desc.	10/11/91
-90.146			
.161			

⊼	BS	FS	∠Pt.	HD	HI	HT	∠	EL	DESC
5026	PAT	1152	298-58-50	56.635	5.25	6.31	-0.479		
			298-58-50	.634			-0.477		
			359-59-58						
			m						
			298-58-50						
			298-58-50						
			0-0-0						
			m						
5026	1152	PAT	61-01-06						
			61-01-08						
			0-0-0						
			m						
			61-01-06						
			61-01-06						
			359-59-56						
			m						

T	BS	FS	∠RT	HD	HI	HT	+/-	ELEV	Desc
5025	Pat	11A3	243-00-44	886.491	5.76	5.46	-57.162		
			-42	.492			.155		
			00-00-00						
			^						
			243-00-42						
			-42						
			00-00-00						
			^						
5025	11A3	Pat	116-59-20						
			-20						
			00-00-00						
			^						
			116-59-22						
			-20						
			00-00-00						
			^						
5025	Padue	11A3	165-41-36						
			-38						
			00-00-00						
			^						
			165-41-36						
			-36						
			00-00-00						
			^						
5025	11A3	Padue	194-18-24						
			-22						
			00-00-00						
			^						
			194-18-24						
			-24						
			359-59-58						
			^						

10/11/01

10/11/91

T	BS	FS	∠ RT	HD	HI	HT	+/- ELEV	Desc.	
New Mick	M.F.	5027	103-16-00	9297.123			103-15-44	B.S. MF	
			103-15-58	.121			-42		
			00-00-00	.124			359-59-56		
			^				^ -45		103-15-44.5
			103-15-58				103-15-42		256-44-16
			-59		103-15-59		-40		360-00-00.5
			00-00-00		256-44-00		359-59-54		
			^		359-59-59		^ -44		
NM	5027	MF	256-44-00				256-44-14	BS. 5027	103-15-44.25
			-00				-18		
			00-00-00				0°		
			^				^ -16		
			256-44-00				256-44-16		
			256-43-58				-18		
			359-59-58				00-00-02		
			^ 43-59				^ -16		
NM	Sweat	5027	336-36-42		336-36-44		336-36-44	BS Sweat	
			-42		23-23-16		-44		
			359-59-56		360-00-00		00-00-02		336-36-42.5
			^				^ -43		23-23-17
			336-36-44				336-36-42		359-59-59.5
			-44				-44		
			00-00-00				00-00-02		
			^ 44				^ -42		
NM	5027	Sweat	23-23-16				23-23-24	BS. 5027	336-36-42.75
			-16				-20		
			00-00-00				00-00-06		
			^ 14				^ -19		
			23-23-16				23-23-14		
			-16				-16		
			00-00-02				0°		
			^ 15				^ -15		

T	DS	FS	∠ RT	HD	HI	HT	+/-	ELEV	Desc
NM	MF	5028	31-32-58	2684.248	5.52		-177.219		
			31 33-00	.251			.219		Set trav. pt.
			00-00-00						
			M						
			31-33-00						
			-00						
			00-00-00						
			n						
NM	5028	MF	328-26-58						
			328-27-00						
			00-00-00						
			n						
			328-27-00						
			-00						
			359-59-58						
			n						
NM	Sweat	5028	264-53-40						
			-40						
			00-00-02						
			M						
			264-53-40						
			-40						
			00-00-00						
			n						
NM	5028	Sweat	95-06-18						
			-20						
			00-00-00						
			n						
			95-06-18						
			-18						
			00-00-00						
			n						

1600
10/11/91

∠	BS	FS	∠Rt	H.D.	HI	HT
~~5027~~ 5028	N.M.	1138	83-53-18	385.237	5.65	
			-18	.237		
			00-00-00			
			^			
			83-53-18			
			-18			
			00-00-00			
			^			
~~5027~~	1138	NM	276-06-40			
			-42			
			00-00-00			
			^			
			276-06-40			
			-40			
			00-00-00			
			^			
~~5027~~	MF	1138	333-20-56			
			-56			
			00-00-00			
			^			
			333-20-56			
			-56			
			00-00-00			
			^			
~~5027~~	1138	MF	26-39-04			
			-04			
			00-00-00			
			^			
			26-39-06			
			-04			
			00-00-00			
			^			

10/14/91

+/-	EL	DESC.
-4.535		
.535		

T	BS	FS	X.R.	H.D.	HI	HT	+/-	EL	DESC.	10/14/91
~~5028~~ 5027	NewMick	1137	49-38-52	111.093						
			49-38-52	111.093						
			0-0-02							
			m							
			49-38-48							
			49-38-48							
			359-59-58							
			m							
~~5028~~	1137	NewMick	310-21-10							
			310-21-12							
			0-0-0							
			m							
			310-21-12							
			310-21-14							
			0-0-04							
			m							
~~5028~~	Sweat	1137	181-58-54							
			181-58-54							
			0-0-0							
			m							
			181-58-54							
			181-58-54							
			0-0-0							
			m							
~~5028~~	1137	Sweat	178-01-06							
			178-01-04							
			0-0-0							
			m							
			178-01-04							
			178-01-06							
			359-59-58							
			m							

Julie = 2174.53

π	BS	FS	∡ RT	HO	HI	HT
Julie	Sweat	5030	154-52-02	2016.394	4.50	5.22
			-06	.371		
			00-00-00			
			M			
			154-52-02			
			-02			
			00-00-00			
			M			
Julie	5030	Sweat	205-07-56			
			-58			
			00-00-00			
			M			
			205-07-58			
			-58			
			00-00-00			
			M			
Julie	Paduc	5030	17-11-42			
			17-11-42			
			0-0-0			
			M			
			17-11-42			
			17-11-42			
			359-59-58			
			M			
Julie	5030	Paduc	342-48-16			
			342-48-16			
			0-0-0			
			M			
			342-48-16			
			342-48-20			
			0-0-0			
			M			

+/-	ELEV	Desc.
-253.276		
.402		

M - 253.339

1920.47 Trav. pt.

163
10/14/91

5030 = 1920.47

T	BS	FC	∢ RT	HD	HI	HT	H/+	ELEV	ICPSC	10/4/91
5030	Julie	5021	00-32-00	248.631	5.101	5.15	+6.05			
			-02	.533			+6.03			
			359-59-58							
			M							
			00-32-00				M = +6.04			
			-00							
			00-00-00					1920.97	Tran. Pt.	
			M							
5030	5021	Julie	359-28-00							
			-00							
			00-00-00							
			M							
			359-28-02							
			-00							
			00-00-02							
			M							

5031 = 1926.97

T	BS	FS	∡HT	HI	HI	HT
5031	5030	11AZ	291-45-46	1429.600	5.45	5.30
			-48	.599		
			00-00-02			
			^			
			291-45-46			
			-46			
			00-00-00			
			^			
5031	11AZ	5030	68-14-16			
			-14			
			00-00-00			
			^			
			68-14-14			
			-14			
			00-00-00			
			^			

165

10/14/91

+/-	ELEV	DIST
-129.047		
.081		

M -129.064

1798.06

Sec. Cor. 20/21 / 29/28

1.15' above gr.

BM #430

record elev = 1797.75

JULIE = 2174.53

T	RS	FS	∡ RT	HD	HI	HT
Julie	Sweat	5032	15-21-48	3847.432	4.57	5.28
			-48	.49		
			00-00-00			
			M			
			15-21-48			
			-48			
			00-00-00			
			M			
Julie	5032	Sweat	344-38-14			
			-14			
			00-00-00			
			M			
			344-38-12			
			-12			
			00-00-00			
			M			
Julie	Paduc	5032	237-41-28			
			-26			
			359-59-58			
			M			
			237-41-30			
			-30			
			00-00-02			
			M			
Julie	5032	Paduc	122-18-30			
			-30			
			359-59-58			
			M			
			122-18-28			
			-30			
			359-59-58			
			M			

166

10/15/91

+/-	ELEV	Misc
-103.51		
-103.28		
M=-103.39		

2010.43 Trav. pt.

π	BS	FS	∡ HT	HI	HI	HT
Julie	Sweat	5033	12-19-40	3729.801	4.57	5.20
			-40	.793		
			00-00-00			
			M			
			12-19-42			
			-44			
			00-00-02			
			M			
Julie	5033	Sweat	347-40-18			
			-16			
			359-59-58			
			M			
			347-40-18			
			-18			
			00-00-00			
			M			
Julie	Paduc	5033	234-39-32			
			-30			
			00-00-04			
			M			
			234-39-28			
			-30			
			00-00-00			
			M			
Julie	5033	Paduc	125-20-32			
			-34			
			00-00-00			
			M			
			125-20-34			
			-34			
			00-00-00			
			M			

JULIE = 2174.53

167

10/15/91

H/-	ELEV.	Resc
-141.71		
-141.51		
M = -141.61		
	2032.29	TRAV. PT.

π	BC	FS	∢ RT	AD	HI	HT
5033	Julie	1135	82-44-40	1243.8[illegible]	5.59	5.10
			-40	.880		
			00-00-00			
			^			
			82-44-40			
			-40			
			00-00-00			
			^			
5033	1135	Julie	277-15-20			
			-20			
			00-00-00			
			^			
			271-15-20			
			-20			
			00-00-00			
			^			
5033	Sweat	1135	284-13-52			
			-52			
			359-59-58			
			^			
			284-13-54			
			-54			
			00-00-00			
			^			
5033	1135	Sweat	75-46-04			
			-04			
			359-59-58			
			^			
			75-46-06			
			-06			
			359-59-58			
			^			

5033 = 2032.29

168

10/15/91

+/-	ELEV	Desc
+10.03		
+10.06		
M = +10.045		
	2042.83	

1/4 cor. 17/20

1.18' above gr.

BM #417

rec. el. = 2042.94

π	BS	FS	∡ RT	HD	HI	HT
5032	Julie	1136	252-36-26	1173.976	5.63	5.15
			-30	.973		
			00-00-04			
			M			
			252-36-28			
			-26			
			00-00-00			
			M			
5032	1136	Julie	107-23-34			
			-34			
			00-00-02			
			M			
			107-23-34			
			-34			
			00-00-00			
			M			
5032	Sweat	1136	99-47-32			
			-34			
			359-59-58			
			M			
			99-47-34			
			-34			
			00-00-00			
			M			
5032	1136	Sweat	260-12-24			
			-24			
			00-00-00			
			M			
			260-12-26			
			-28			
			359-59-58			
			M			

5032 = 2010.43

169

10/15/91

+/-	ELEV.	Misc.
-86.14		
-86.33		

M = -86.24

1924.67

Sec. Cor. 17/16 / 20/21

0.75 above gr.

BM 289

rec. el. = 1924.33

⊼	BS	FS	ΔRt.	H.D.	Desc.
ΔSweat	ΔLoure	503A	D. 305-16-1A	3111.93	1/4 COR. 17/16
			R. 125-16-21	.92	
			H. 180-00-06	.92	
			M. 305-16-1A	.91	
			D. 305-16-1A		
			R. 125-16-25		
			H. 180-00-05		
			M. 305-16-17		

T	BS	FS	APP.	HD	DESC.
5034	Sweet	5035	D A5-15-08	216A2.25	Sec. Cor. 8/9 17/16
			R 225-15-10	.24	
			H 180-00-00	.26	
			M A5-15-00	.27	
				216A2.27	
			D A5-15-04		
			R 225-15-08		
			H 180-00-01		
			M A5-15-05.5		
			D A5-15-03		
			R 225-15-10		
			H 180-00-00		
			M A5-15-06.5		

Panel Pt., No # on map

T	BS	FS	∠ Rt.	H.D.	Desc.
503A	Sweat	5036	332-43-12	2A52.A25	Panel Pt. SW
			332-43-06	2A52.A26	
			0-0-0		
			m.		
			332-43-12		
			332-43-08		
			0-0-0		
			m.		
503A	5036	Sweat	27-16-50		
			27-16-50		
			0-0-02		
			m		
			27-16-50		
			27-16-48		
			359-59-58		
			m.		

of Sweat, No # on MAP

173 10/17/91
JF
JW

STA	+	HI	-	EL.	DESC.
BM446				1874.91	rec.
	2.37				
			10.22		
	1.16				
			12.13		
	2.89				
			15.77		
	3.56				
BM445			6.52	1840.25	PANEL 1147
	10.77				1/2" rebar in conc.
			2.84		0.20' above gr.
	15.69				rec. el=
			0.72		1840.24
	11.99				
BM447			1.88	1873.26	rec. el=
					1873.24

Π @ Δ John \\ BM #501 elev = 1098.15

FS. = Panel 1149 near S. 1/4 cor. sec. 28

	S.D.	Vertical ∡	+/-	HI	HT
	3341.456	89-07-30		3.94	5.13
	3341.450	89-07-32			
	3341.452	89-07-31			
m	3341.453	89-07-31	+51.01		

Π @ Panel 1149

FS. = Δ John

	S.D	Vert. ∡	+/-	HI	HT
	3341.449	90-53-27		5.13	3.94
	3341.451	90-53-31			
	3341.447	90-53-29			
m	3341.449	90-53-29	-51.98		

Panel 1149

174
10/18/91
JF
JW

EL

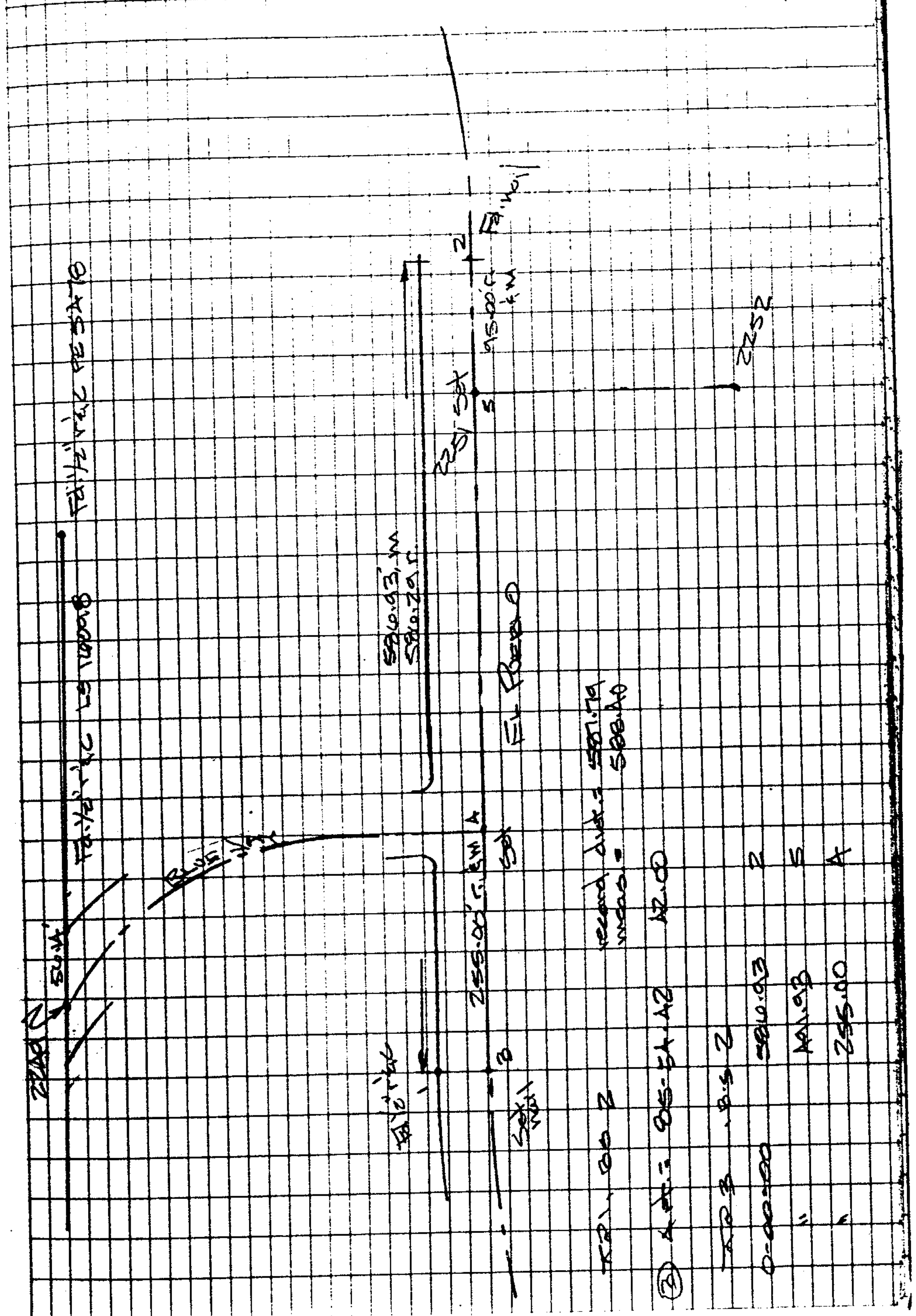
(+49.92 from Δ John)

(-50.79 from panel)

m = 50.31

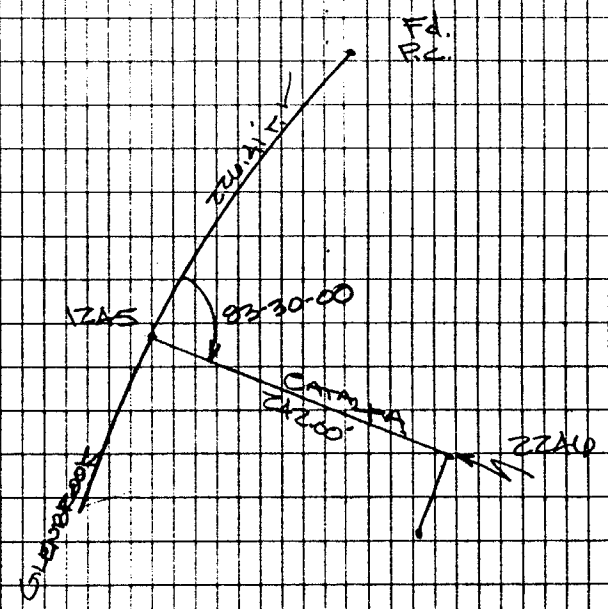
EL @ 1149 = 1748.46

Sta	+	HI	−	El.	Desc.
1249					Panel BM
	3.96				
2249			3.21		Set record pt.
	3.55				
1249			2.10		
1252					Panel BM
	2.05				
2252			4.43		Rec Pt
	4.63				
1252			2.25		
1251					Panel TBM
	4.04				
2251			3.99		Int.
	4.14				
1251			4.19		
1250					Panel TBM
	4.50				
2250			4.51		Int.
	4.61				
1250			4.60		



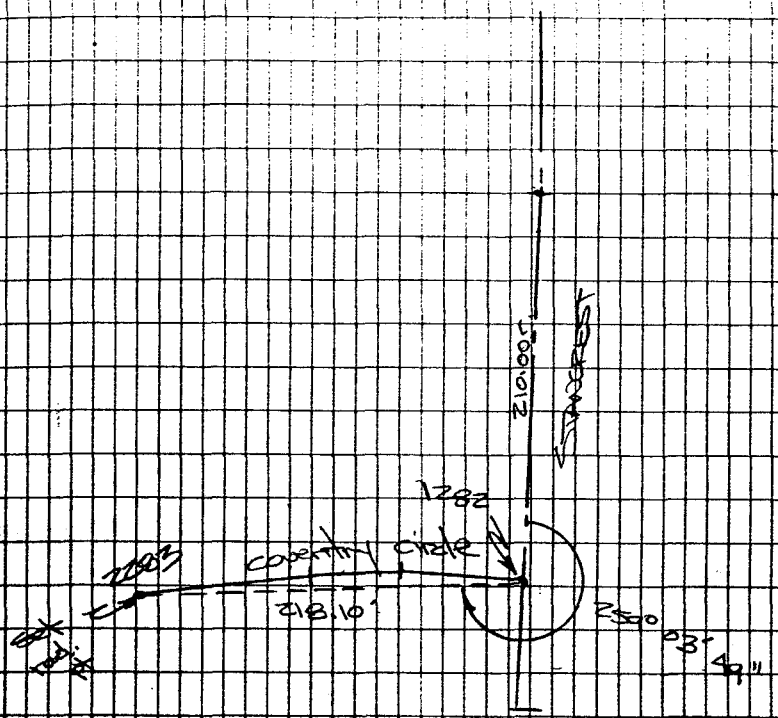
STA	+	HI	-	EL.	DESC.
1246					Panel TBM
	3.34				
2246			5.21		℄ & Pt.
	5.09				
1246			3.22		

176
10/21/91

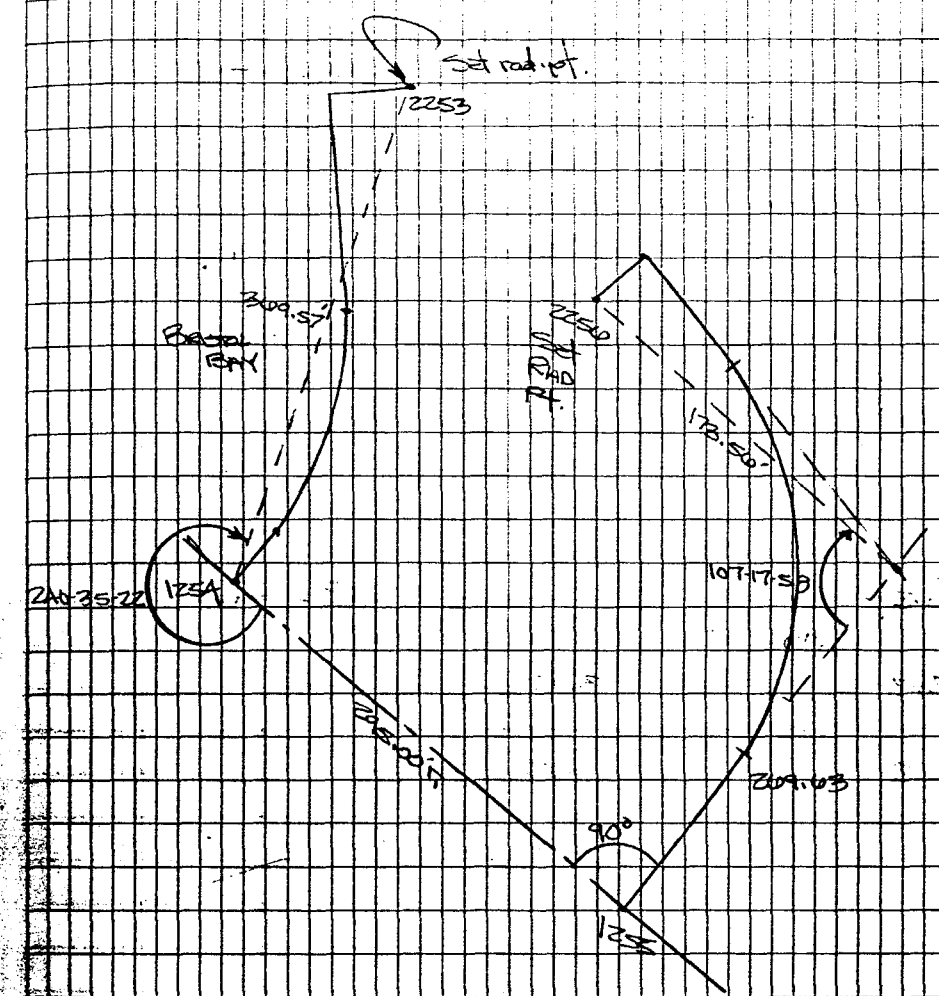


Sta	+	HI	−	El	Desc.
1283					Panel Trim
	1.61				
2283			4.95		Road Pt.
	5.07				
1283			1.73		

10/22/91



Sta	+	Hi	−	El	Desc.
1253					Panel TBM
	0.47				
2253			6.05		Rad Pt.
	5.91				
1253			2.33		
1256					Panel TBM
	3.79				
2256			3.94		Rad. Pt.
	3.716				
1256			3.601		



Sta.	+	HI	−	El.	Desc.
1259					Found TBM
	3.04				
2259			3.33		Rad. Pt.
	3.09				
1259			2.80		
1262					Found TBM
	1.910				
2262			3.77		Int.
	3.83				
1262			2.02		

Escondido

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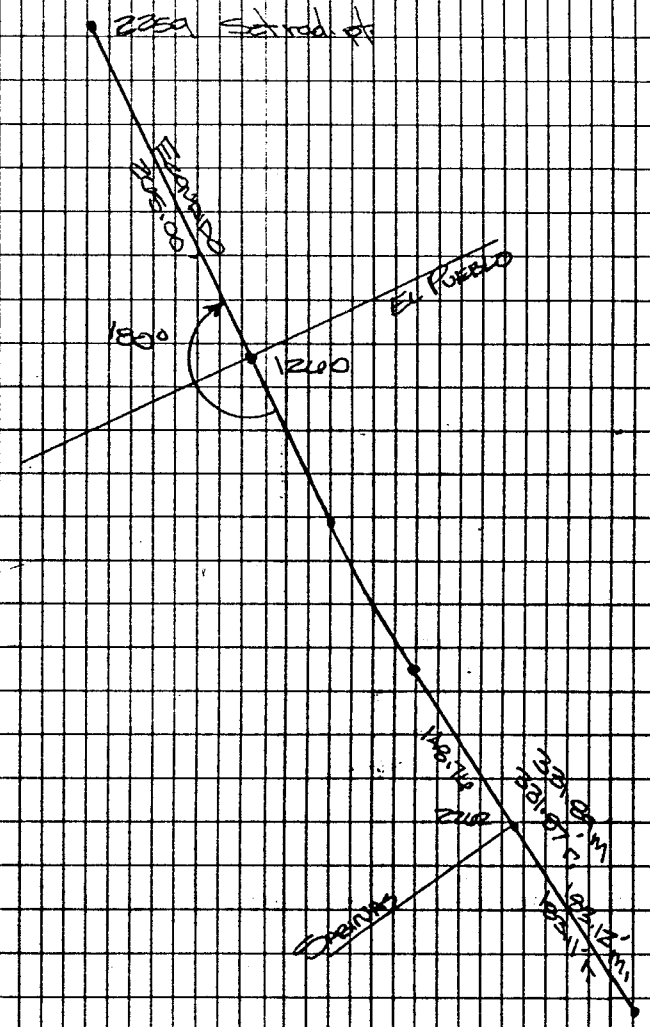
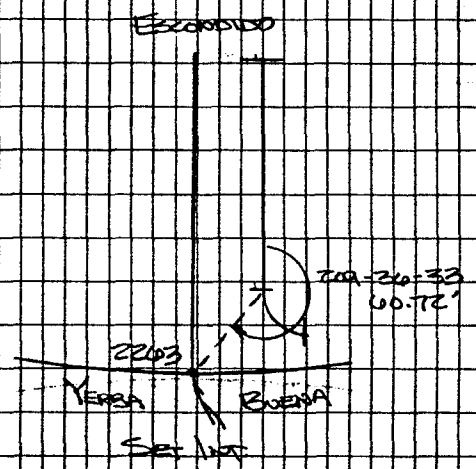
10/20/91



180
10/22/91

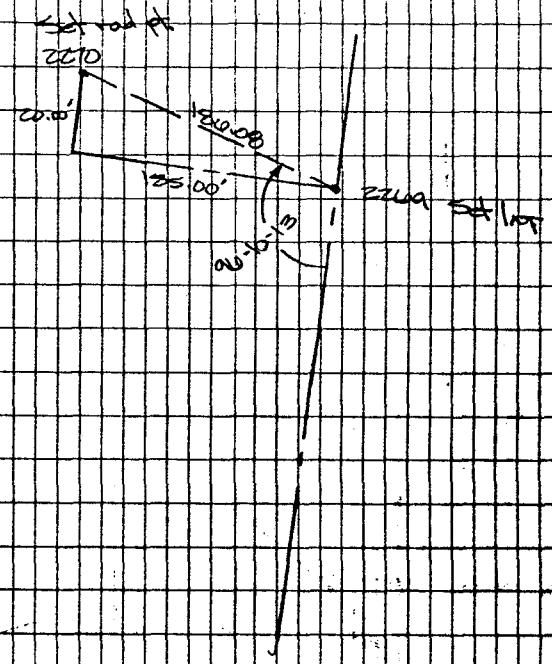


SAME ELEV. AS PANEL 12103

Sta	+	HI	−	EL	DESC.
1273					TBM Panel
	4.96				
2273			4.93		⊥ pt.
	4.78				
2274			10.41		INT.
	10.55				
1274			10.14		TBM Panel
1277					TBM Panel
	4.73				
2276			3.78		⊥ pt.
	3.94				
1277			4.84		

10/22/91

Sta	+	HI	−	El	Desc
1209					Panel TBM
	6.20				
2209			4.70		Int.
	4.82				
1209			4.32		
1270					Panel TBM
	2.33				
2270			5.30		Rad. Pt.
	5.24				
1270			2.19		



*	HI	-	EL	DESC.
				Panel TBM
6.20				
		4.70		INT.
4.82				
		4.32		
				Panel TBM
2.33				
		5.38		RAD. PT
5.24				
		2.19		

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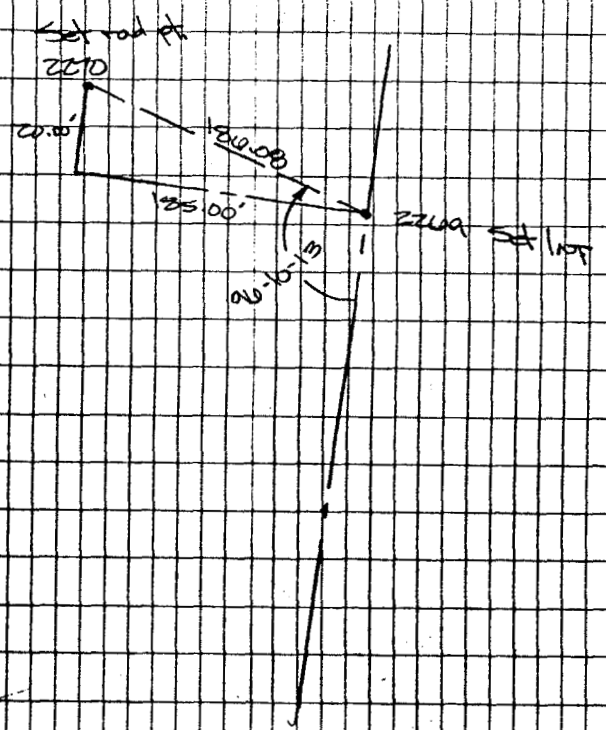
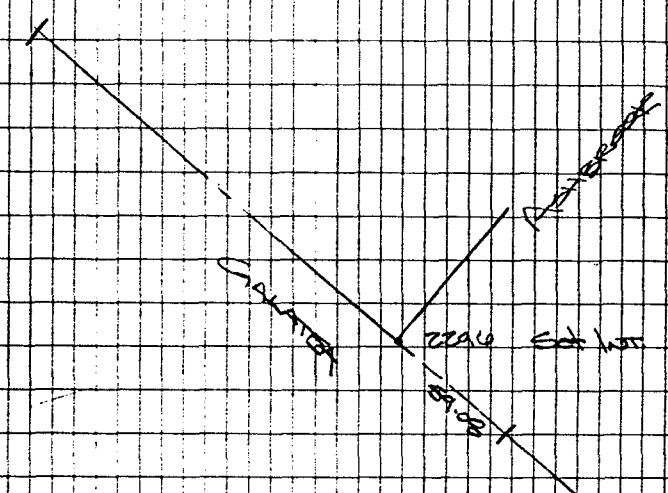
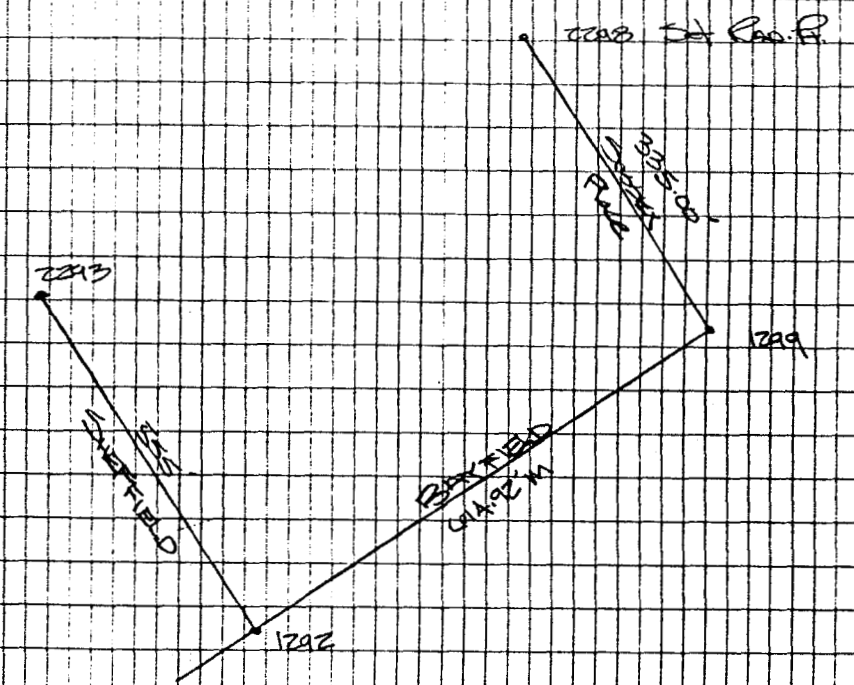


SA +	HI	-	EL	DESC.
1294				Panel TBM
	5.55			
2294		5.02		INT
	5.11			
1294		5.04		



Sta	+	HI	−	EL	Desc.
1298					Panel TBM
	2.20				
1298			5.21		RAD
	5.32				
1298			2.31		
1293					Panel TBM
	4.74				
2293			5.51		RAD
	5.42				
1293			4.87		

18A
10/23/91



PANEL 133

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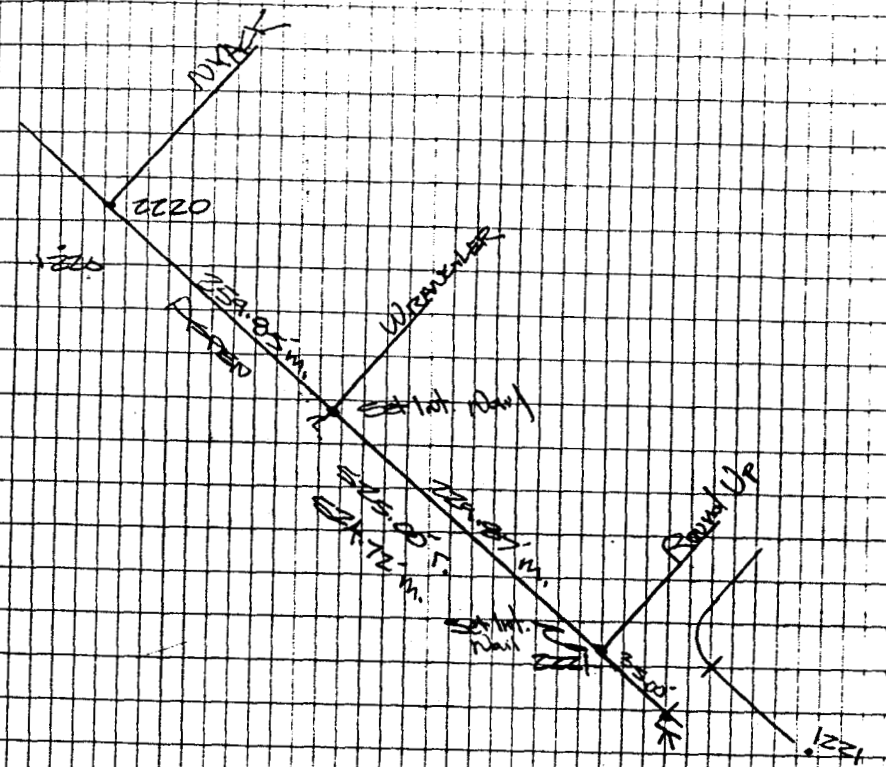
10/25/91

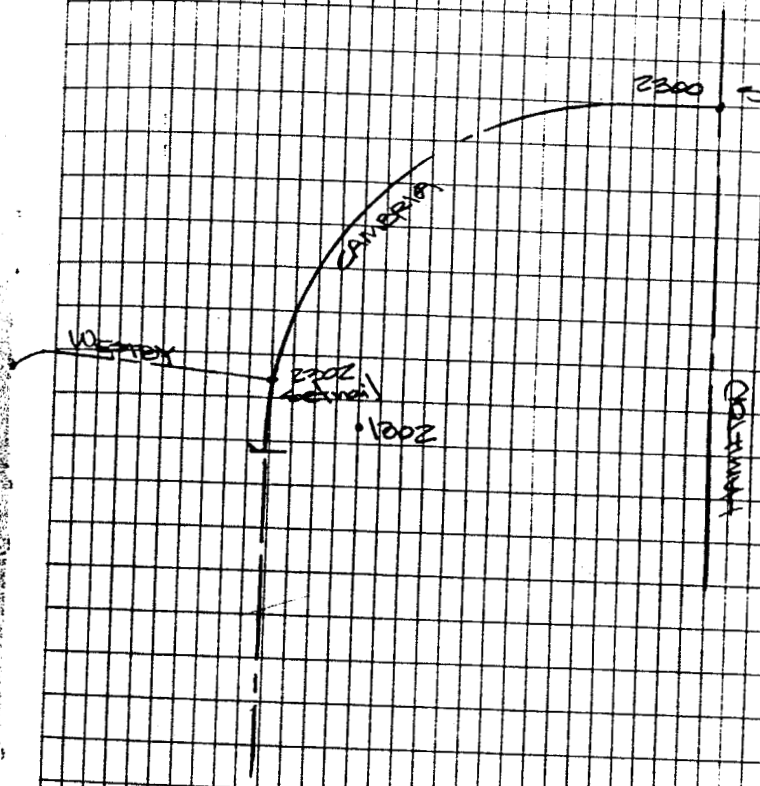
STA	+1	+2	HI1	HI2	-1	-2	EL1	EL3	DESC
							9.07.80	19.07.80	BM 255
TP	13.00		80.80		0.42		80.38		
TP		13.16		80.96		0.07		80.29	
	8.49		88.87						
		8.58		88.87					
TP					0.25		88.62		
TP						0.33		88.54	
	15.05		03.67						
		15.13		03.67					
TP					2.93		2000.74		
TP						2.98		2000.69	
	6.55		07.29						
		6.43		07.12					
TP					3.61		2003.68		PANEL 133 1/2" rebar 0.06' above gr
TP						3.44		2003.68	" "

Sta	+	HI	−	El	Desc.
1221					Panel TBM
	4.05				
2220			4.90		Set Int.
	4.01				
?			4.54		Set Int. Wrangler & Round Up
	7.58				
1220			1.69		Panel TBM

Aspen 10/20/91

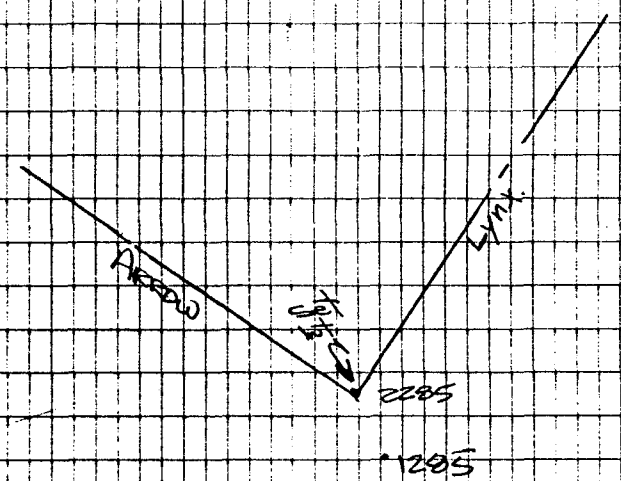


STA	+	HI	−	EL.	DESC.
1300					Panel TBM
	2.40				
2300			3.87		Int. nail
	3.66				
1300			2.19		
1302					Panel TBM
	3.50				
2302			5.03		Int. Nail
	4.85				
1302			3.31		



STA	+	HI	-	EL.	DESC.
1285					Panel TBM
	A.102				
2285			A.80		Int xpt
	A.107				
1285			A.49		

10/20/91



SA	+	H1	-	E.	DEK
1A05					Panel TBM
	5.13				
2A05			A.68		P.T. NAIL
	A.56				
1A05			5.01		