Flood Control District of Maricopa County
Contract FCD 89-79

# WICKENBURG AREA DRAINAGE MASTER STUDY

# TECHNICAL DOCUMENTATION REPORT

## HYDROLOGIC ANALYSES

## FLOODLAIN DELINEATION

Submitted to the
Federal Emergency Management Agency
on Behalf of the
Flood Control District of Maricopa County

BLACK & VEATCH
PROGRESS BY DESIGN

Project No. 17676

May 1994

COE & VAN LOO
PLANNING • ENGINEERING
LANDSCAPE ARCHITECTURE

CVL No. 1197-02

Flood Control District of Maricopa County
Contract FCD 89-79

# WICKENBURG AREA DRAINAGE MASTER STUDY

# TECHNICAL DOCUMENTATION REPORT

## Appendix 4.2: HEC-2 Models & Cross Section Plots for Sols Wash Area Wash
## FLYING E WASH & TRIBUTARIES (Wash ab)

Submitted to the
Federal Emergency Management Agency
on Behalf of the
Flood Control District of Maricopa County

N:\1197\02\ADMIN\119702RP.063

May 1994

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>RIVERINE HYDRAULIC ANALYSIS FORM | O.M.B. Burden No 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
|---|---|---|

## PUBLIC BURDEN DISCLOSURE NOTICE

Public reporting burden for this form is estimated to average 2.25 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing and reviewing the form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden, to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, S.W., Washington, DC 20472; and to the Office of Management and Budget, Paperwork Reduction Project (3067-0148), Washington, DC 20503.

Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AB: FLYING E WASH
*(One form for each flooding source)*

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. REACH TO BE REVISED

Downstream limit: Station 0.95

Upstream limit: Station 5.279

### 2. EFFECTIVE FIS

☐ Not studied

☒ Studied by approximate methods

Downstream limit of study: Sols Wash Confluence

Upstream limit of study: Maricopa County Line / Town of Wickenburg Limit

☒ Studied by detailed methods

Downstream limit of study: ~1,000' Downstream from U.S. Hwy 60

Upstream limit of study: ~2,000' Upstream from U.S. Hwy 60

☐ Floodway delineated

Downstream limit of Floodway: _____

Upstream limit of Floodway: _____

### 3. HYDRAULIC ANALYSIS

Why is the hydraulic analysis different from that used to develop the FIRM. *(Check all that apply)*

☐ Not studied in FIS

☒ Improved hydrologic data/analysis. Explain: Hydrologic Analysis procedures standardized by the Flood Control District of Maricopa County

☐ Improved hydraulic analysis. Explain: _____

☐ Flood control structure. Explain: _____

☐ Other. Explain: _____

Full input and output listings along with files on diskette *(if available)* for each of the models listed below and summary of the source of input parameters used in the models must be provided. The summary must include a complete description of any changes made from model to model *(e.g. duplicate effective model to corrected effective model)*. Only the Duplicate Effective and the Revised or Post-Project Conditions models must be submitted. See instructions for directions on when other models may be required. Only the 100-year flood profile is required for SFHAs with a Zone A designation. For areas which do not have detailed flooding, a hydraulic model is not required; however BFE's may not be added to the revised FIRM.

☐ Duplicate Effective Model — Natural ☐ Floodway ☐

Copies of the hydraulic analysis used in the effective FIS, referred to as the effective models *(10-, 50-, 100-, and 500-year multi-profile runs and the floodway run)* must be obtained and then reproduced on the requestor's equipment to produce the duplicate effective model. This is required to assure that the effective model input data has been transferred correctly to the requestor's equipment and to assure that the revised data will be integrated into the effective data to provide a continuous FIS model upstream and downstream of the revised reach.

☐ Corrected Effective Model — Natural ☐ Floodway ☐

The corrected effective model is the model that corrects any errors that occur in the duplicate effective model, adds any additional cross sections to the duplicate effective model, or incorporates more detailed topographic information than that used in the currently effective model. The corrected effective model must not reflect any man-made physical changes since the date of the effective model. An error could be a technical error in the modeling procedures, or any construction in the floodplain that occurred prior to the date of the effective model but was not incorporated into the effective model.

☐ Existing or Pre-Project Conditions Model — Natural ☐ Floodway ☐

The duplicate effective or corrected model is modified to produce the existing or pre-project conditions model to reflect any modifications that have occurred within the floodplain since the date of the effective model but prior to the construction of the project for which the revision is being requested. If no modification has occurred since the date of the effective model, then this model would be identical to the corrected effective or duplicate effective model.

☐ Revised or Post-Project Conditions Model — Natural ☐ Floodway ☐

The existing or pre-project conditions model *(or duplicate effective or corrected effective model, as appropriate)* is revised to reflect revised or post-project conditions. This model must incorporate any physical changes to the floodplain since the effective model was produced as well as the effects of the project. When the request is for proposed project this model should reflect proposed conditions.

☒ Other: Please attach a sheet describing all other models or calculations submitted. — Natural ☒ Floodway ☒

New Model
(Proposed Effective Model)

4. MODEL PARAMETERS *(from model used to revise 100-year water surface elevation)*

| Discharges: | Upstream Limit | Downstream Limit |
|---|---|---|
| 10-year | | |
| 50-year | | |
| 100-year | | |
| 500-year | | |

Attach diagram showing changes in 100-year discharge

2. Explain how the starting water surface elevations were determined Starting water surface elevation determined by the Slope-Area Method

3. Give range of friction loss coefficients (*Manning's "N"*) Channel .....

Overbanks .....

If friction loss coefficients are different anywhere along the revised reach from those used to develop the FIRM, give location, value used in the effective FIS, and revised values and an explanation as to how the revised values were determined.

| Location | FIS | Revised |
|---|---|---|
| NA | | |
| | | |
| | | |
| | | |

Explain:

4. Describe how the cross section geometry data were determined (*e.g., field survey, topographic map, taken from previous study*) and list cross sections that were added.

Data points for cross sections are based on the photogrammetric models for the topographic maps

5. Explain how reach lengths for channel and overbanks were determined:

All reach lengths were measured from floodplain work maps.

## 5. RESULTS (from model used to revise 100-year water surface elevations)

1. Do the results indicate:

a. Water surface elevations higher than end points of cross sections? ..... ☐ Yes ☒ No

b. Supercritical depth? ..... ☐ Yes ☒ No

c. Critical depth? ..... ☒ Yes ☐ No

d. Other unique situations ..... ☒ Yes ☐ No

(If yes, Special Problem Report attached)

If yes to any of the above, attach an explanation that discusses the situation and how it is presented on the profiles, tables, and maps.

2. What is the maximum change in energy gradient between cross-sections? ..... 10.86

Specify location ..... SECNO 3.950

3. What is the distance between the cross-sections in 2 above? ..... 590

Specify location ..... 3.950

4. What is the maximum distance between cross-sections? ..... 700

Specify location ..... 5.014

5. Floodway determination

a. What is the maximum surcharge allowed by the community or State? ..... 1 foot

b. What is the maximum surcharge for the revised conditions? ..... 0.5 foot

Specify location ..... Station 0.351

c. What is the maximum velocity? ..... 15.4 fps

Specify location ..... 2.109

Explain:

d. Are there any negeative surcharge values at any cross-section ☒ Yes ☐ No

If yes, the floodway may need to widen. If it is not widened, please explain and indicate the maximum negative surcharge.

The maximum negative surcharge is 0.4 ft at Section 2.342. This is a result of adjacent encroachment that increases velocity and lowers the water surface elevation at the section.

6. Is the discharge value used to determine the floodway anywhere different from that used to determine the natural 100-year flood elevations? ..... ☐ Yes ☒ No

If Yes, explain:

7. Do 100-year water surface elevations increase at any location? ..... ☐ Yes ☒ No

If yes, please attach a list of the locations where the increases occur, state whether or not the increases are located on the requestor's property, and provide an explanation of the reason for the increases.

NA- New Model

Please attach a completed comparison table entitled: Water Surface Elevation Check (See page 6)

## 6. REVISED FIRM/FBFM AND FLOOD PROFILES

A. The revised water surface elevations tie into those computed by the effective FIS Model *(10-, 50-, 100-, and 500-year)*, downstream of the project at cross-section NA within _____ feet and upstream of the project at cross section _____ within _____ feet.

B. The revised floodway elevations tie into those computed by the effective FIS model, dowstream of the project at cross section NA within _____ feet and upstream of the project at cross section _____ within NA feet.

C. Attach profiles, at the same vertical and horizontal scale as the profiles in the effective FIS report, showing stream bed and profiles of all floods studied (without encroachment). Also, label all cross sections, road crossings (including low chord and top-of-road data), culverts, tributaries, corporate limits, and study limits. If channel distance has changed, the stationing should be revised for all profile sheets.

D. Attach a Floodway Data Table showing data for each cross section listed in the published Floodway Data Table in the FIS report.

Proceed to Riverine/Coastal Mapping Form

FEDERAL EMERGENCY MANAGMENT AGENCY

# WATER SURFACE ELEVATION CHECK

COMMUNITY NAME: Unincorporated Maricopa County/ Town of Wickenburg

FLOODIND SOURCE: WASH AB. FLYING E WASH AND TRIBS

PROJECT NAME /IDENTIFIER: Wickenburg ADMS FCD 89-79

| | EFFECTIVE | | | DUPLICATE EFFECTIVE | | | CORRECTED EFFECTIVE | | | EXISTING/PRE-PROJECT | | | REVISED/PROJECT | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SECNO | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] |
| | | | | | | | | | | | | | | | |

COMMENTS: New Model - See following Floodway Data Tables

1-100-year (natural) Water Surface Elevation 2-Encroachment (floodway) Water Surface Elevation 3-Surcharge Value

Include all cross sections in the models between tie-in points. Any interpolated values should be indicated in parentheses.

Sheet 1 of 1

4.2

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>**HYDROLOGIC ANALYSIS FORM** | O.M.B. Burden No. 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
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Community Name: UNINCORPORATED MARICOPA COUNTY / TOWN OF WICKENBURG

Flooding Source: Wash AB: FLYING E WASH AND TRIBUTARIES
*(One form for each flooding source)*

Project Name /Identifier: WICKENBURG ADMS FCD 89-79

### 1. HYDROLOGIC ANALYSIS IN FIS

☒ Approximate study stream (Zone A)
☒ Detailed study stream (briefly explain methodology) Unknown

### 2. REASON FOR NEW HYDROLOGIC ANALYSIS

☐ No existing analysis
☐ Improved data *(see data revision on page 3)*
☐ Changed physical conditions of watershed *(explain)*

☐ Alternative methodology *(justify why the revised model is better than model used in the effective FIS)*

☐ Evaluation of proposed conditions (CLOMRs only) (explain)

☒ Other No existing analysis or analysis being updated to reflect existing conditions

If a computer program/model was used in revising the hydrologic analysis, please provide a diskette with the input files for the 10-, 50-, 100 - and 500-year recurrence intervals.

Only the 100-year recurrence interval need be included for SFHAs designated as Zone A.

### 3. APPROVAL OF ANALYSIS

☒ Approval of hydrologic analysis, including the resulting peak discharge value (s) has been provided by the appropriate local, state, or Federal Agency. (i.e., Flood Control District of Maricopa County )
Attach evidence of approval.

☐ Approval of the hydrologic analysis is not required by any local, State, or Federal Agency.

Stream: WASH AB: FLYING E WASH

Comparison of 100-year Discharges

| Location: | Drainage area (Sq mi.) | FIS (cfs): | Revised (cfs): |
|---|---|---|---|
| US HWY 60 | 8.4 / 8.5 | 6,500 | 6,943 |
| | | | |
| | | | |
| | | | |
| | | | |

Note: When revised discharges are not significantly different than FIS discharges, FEMA may require a confidence limits analysis on attachment D at a later date to complete the review.

As is often the case with revision requests, only a portion of a stream may actually be revised or be affected by a revision. Therefore, transition to the unrevised portion is important to maintain the continuity of the study. NFIP regulations stipulate that such a transition must be assured. What is the transition from the proposed discharges to the effective discharges? Please explain how the transition was made *(attach separate sheet if necessary)*

ATTACH A COMPLETED REVIEW OF RESULTS PAGE FOR EACH FLOODING SOURCE.

Is the new hydrologic analysis being developed solely to revise the flow values presented in the FIS *(i.e. no changed hydraulic conditions)*? ☐ Yes ☒ No

If yes, does the 100-year water surface elevation change by 1.0 foot or more? ☐ Yes ☐ No

FEMA does not normally revise NFIP maps solely due to insignificant flow changes where changes in 100-year water surface elevation are less than 1.0 foot.

## 5. HISTORICAL FLOODING INFORMATION

Is historical data available for the flooding source? ☐ Yes ☒ No

If yes, provide the following:

Location along flooding source: _____

Maximum peak discharge: _____ cfs

Second highest peak discharge: _____ cfs

Source of information: _____

## 6. GAGE RECORD INFORMATION

Location of nearest gage to project site *(along flooding source or similar watershed; specify)*

NA

Gaging Station: _____

Drainage area at gage: _____ $mi^2$

Number of years of data: _____

## 7. DATA REVISION

Please use the following table to list all the data and/or parameters affected by this request and identify them as new data (*New*) or as revising existing data (*Revised*). *(If necessary, attach a separate sheet.)*

| Data Parameter | New | Revised | Data Source |
|---|---|---|---|
| NA | ☐ | ☐ | |
| | ☐ | ☐ | |
| | ☐ | ☐ | |
| | ☐ | ☐ | |
| | ☐ | ☐ | |

- Data source can be from a Federal, State, or local government agency, or from a private source. Some State and local governments may have less strict data requirements than Federal agencies, in which case the hydrologic data may not be accepted by FEMA unless it is demonstrated that the data give a better estimate of the flood discharge.
- Attach documentation corroborating each data source *(i.e., certified statement, report, bibliographical reference to a published document)*. In the case of a published document or a government report, providing copies of the cover and pertinent pages may be helpful.

## 8. METHODOLOGY FOR NEW ANALYSIS

☐ Statistical Analysis of Gage Records (*use Attachment A*)

☐ Regional Regression Equations *(use Attachment B)*

☒ Precipitation/Runoff Model *(use Attachment C)*

☐ Other *(specify; attach backup computations and supporting data)* _____

Gaging Station: NA

Gage Location (latitude and longitude): _____

| | FIS: | Revised: |
|---|---|---|
| 1. Number of years of data | _____ | _____ |
| Systematic | _____ | _____ |
| Historical | _____ | _____ |
| 2. Homogeneous data | ☐ Yes ☐ No | ☐ Yes ☐ No |
| 3. Data adjustments | ☐ Yes ☐ No | ☐ Yes ☐ No |
| 4. Number of high outliers | _____ | _____ |
| Low outliers | _____ | _____ |
| Zero events | _____ | _____ |
| 5. Generalized skew | _____ | _____ |
| 6. Station skew | _____ | _____ |
| 7. Adopted skew | _____ | _____ |
| 8. Probability distribution used (justify if log-Pearson III was not used) | _____ | _____ |
| 9. Transfer equations to ungaged sites | | ☐ Yes ☐ No |

If yes, specify method

_____

_____

_____

10. Expected probability* ☐ Yes ☐ No

11. Comparison of results with other analyses ☐ Yes ☐ No

If yes, describe comparison

_____

_____

_____

*FEMA does not accept expected probability analyses for the purpose of reflecting flood hazard information in a FIS.

If any data is not available, indicate by N/A.

Attach analysis including plot of flood frequency curve.

1. Bibliographical Reference:

NA

*(Attach a copy of title page, table of contents, and pertinent pages including equations.)*

2. Gaged or ungaged stream: _____

3. Hydrologic region(s): _____
Attach backup map.

4. Provide parameters, values, and source of data used to define parameters.

| | FIS: | | Revised: | |
|---|---|---|---|---|
| 5. Urbanized conditions calculations ..... | ☐ Yes | ☐ No | ☐ Yes | ☐ No |
| 6 Percent of watershed urbanization ..... | _____ | | _____ | |
| 7. Is the watershed controlled? ..... | ☐ Yes | ☐ No | ☐ Yes | ☐ No |
| 8. Comparison with other analyses ..... | ☐ Yes | ☐ No | ☐ Yes | ☐ No |

If the answer to 5, 7, or 8 is yes, explain methodology in Comments.

If data is not available, indicate by N/A.

Comments

Attach computation and supporting maps, delineating the watershed boundary and drainage area divides.

| | | FIS: | Revised |
|---|---|---|---|
| 1. | Method or model used: | | HEC-1 |
| | Version: | | VER 3.0 |
| | Date: | | 02 AUG 88 |
| 2. | Source of rainfall depth: | | NOAA ATLAS 2 |
| 3. | Source of rainfall distribution: | | SCS TYPE II |
| 4. | Rainfall duration: | | 24 HOURS |
| 5. | Areal adjustment to precipitation (%): | | NWS HYDRO-40 |
| 6. | Hydrograph development method: | | S-GRAPH |
| 7. | Loss rate method: | | GREEN-AMPT |
| | Source of soils information: | | SCS |
| | Source of land use information | | TOWN of WICKENBURG |
| 8. | Channel routing method: | | NORMAL DEPTH |
| 9. | Reservoir routing: | ☐ Yes ☐ No | ☐ Yes ☐ No |
| 10. | Baseflow considerations: | ☐ Yes ☐ No | ☐ Yes ☒ No |

If yes, explain how baseflow was determined:

11. Snowmelt considerations: ☐ Yes ☐ No ☐ Yes ☒ No

12. Model calibration: ☐ Yes ☐ No ☒ Yes ☐ No

If yes, explain how calibration was performed Computed discharges were compared with DISCHARGE VS DRAINAGE AREA curves and envelopes prepared by the Flood Control District of Maricopa County

13. Future land use condition: ☐ Yes ☒ No

If yes, explain why

NOTE: FEMA policy is to base flooding on existing conditions.
If data is not available, indicate by N/A.

Attach precipitation/runoff model, hydrologic model schematic, curve number calculations, time of concentration calculations, and supporting maps, delineating the watershed boundary and drainage area divides.

eam: NA – NO FLOW RECORDS

Select one location for Confidence Limits Evaluation (*describe location*): _____

_____

Discharges for selected location:

| Exceedance Probability | | FIS | Revised |
|---|---|---|---|
| 10% | (10-year) ..... | _____ cfs | _____ cfs |
| 2% | (50-year) ..... | _____ cfs | _____ cfs |
| 1% | (100-year) ..... | _____ cfs | _____ cfs |
| 0.2% | (500-year) ..... | _____ cfs | _____ cfs |

1% (100-year) Flood Confidence Intervals

90% Confidence Interval: 5% limit _____ cfs

95% limit _____ cfs

50% Confidence Interval: 25% limit _____ cfs

75% limit _____ cfs

If the value of the 100-year frequency flood in the FIS is beyond the 50% confidence interval but within the 90% confidence interval, does the 100-year water surface elevation change by 1.0 foot or more? ☐ Yes ☐ No

An example of confidence limits analysis can be found in Appendix 9 of Bulletin 17B.

ttach Confidence Limits Analysis.

FLOODWAY DATA, WASH AB: FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| .095 | 121. | 328. | 9.2 | 2134.5 | 2134.5 | .0 |
| .125 | 128. | 331. | 9.1 | 2136.4 | 2136.4 | .0 |
| .131 | 138. | 565. | 5.3 | 2137.7 | 2137.7 | .0 |
| .134 | 138. | 753. | 4.0 | 2139.2 | 2139.2 | .0 |
| .160 | 318. | 670. | 6.3 | 2139.9 | 2139.9 | .0 |
| .220 | 658. | 1271. | 6.2 | 2143.8 | 2143.8 | .0 |
| .256 | 515. | 1255. | 6.2 | 2147.3 | 2147.2 | .1 |
| .351 | 310. | 1011. | 7.7 | 2153.8 | 2153.3 | .5 |
| .460 | 209. | 856. | 9.1 | 2161.2 | 2161.3 | -.1 |
| .540 | 259. | 857. | 9.1 | 2166.2 | 2166.0 | .2 |
| .576 | 311. | 949. | 8.2 | 2169.2 | 2169.2 | .0 |
| .640 | 431. | 1010. | 7.7 | 2174.2 | 2174.2 | .0 |
| .707 | 451. | 1134. | 6.9 | 2181.7 | 2181.7 | .0 |
| .801 | 442. | 1276. | 6.1 | 2187.6 | 2187.6 | .0 |
| .898 | 482. | 995. | 7.9 | 2193.9 | 2193.9 | .0 |
| .938 | 440. | 1115. | 7.0 | 2198.1 | 2198.1 | .0 |
| 1.012 | 583. | 1140. | 6.9 | 2204.1 | 2204.1 | .0 |
| 1.112 | 453. | 1033. | 7.6 | 2210.9 | 2210.9 | .0 |
| 1.180 | 667. | 1232. | 6.3 | 2216.9 | 2216.8 | .1 |
| 1.280 | 515. | 1102. | 7.1 | 2226.2 | 2226.2 | .0 |
| 1.353 | 482. | 1122. | 7.0 | 2233.6 | 2233.6 | .0 |
| 1.441 | 409. | 1025. | 7.6 | 2240.1 | 2240.1 | .0 |
| 1.545 | 475. | 1229. | 6.4 | 2247.0 | 2246.8 | .2 |
| 1.641 | 463. | 1162. | 6.7 | 2252.2 | 2252.1 | .1 |
| 1.725 | 291. | 947. | 8.3 | 2259.9 | 2259.9 | .0 |
| 1.829 | 503. | 1180. | 6.6 | 2267.5 | 2267.4 | .1 |
| 1.918 | 177. | 740. | 10.6 | 2274.6 | 2274.7 | -.1 |
| 2.011 | 126. | 674. | 11.6 | 2282.2 | 2282.3 | -.1 |
| 2.056 | 143. | 694. | 11.3 | 2284.3 | 2284.2 | .1 |
| 2.107 | 85. | 518. | 13.4 | 2287.3 | 2287.3 | .0 |
| 2.109 | 62. | 451. | 15.4 | 2289.4 | 2289.4 | .0 |
| 2.118 | 62. | 541. | 12.8 | 2290.8 | 2290.8 | .0 |
| 2.120 | 59. | 505. | 13.7 | 2290.7 | 2290.7 | .0 |
| 2.125 | 59. | 575. | 12.1 | 2292.4 | 2292.4 | .0 |
| 2.213 | 233. | 885. | 7.8 | 2298.3 | 2298.1 | .2 |
| 2.248 | 230. | 908. | 7.6 | 2300.3 | 2300.0 | .3 |
| 2.342 | 162. | 728. | 9.5 | 2305.6 | 2306.0 | -.4 |
| 2.435 | 144. | 684. | 10.1 | 2309.8 | 2309.8 | .0 |

FLOODWAY DATA, AB: UPPER FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| 2.435 | 144. | 701. | 9.9 | 2309.9 | 2309.9 | .0 |
| 2.539 | 549. | 844. | 8.2 | 2315.5 | 2315.5 | .0 |
| 2.630 | 137. | 453. | 4.8 | 2319.2 | 2319.2 | .0 |
| 2.725 | 244. | 281. | 7.7 | 2325.8 | 2325.8 | .0 |
| 2.812 | 434. | 517. | 4.2 | 2331.1 | 2331.1 | .0 |
| 2.922 | 352. | 427. | 5.0 | 2337.7 | 2337.7 | .0 |
| 3.005 | 480. | 497. | 4.3 | 2344.1 | 2344.1 | .0 |
| 3.047 | 228. | 396. | 5.4 | 2347.4 | 2347.4 | .0 |
| 3.113 | 73. | 245. | 8.8 | 2352.6 | 2352.6 | .0 |
| 3.200 | 240. | 383. | 5.6 | 2358.2 | 2358.2 | .0 |
| 3.261 | 274. | 580. | 3.7 | 2360.4 | 2360.4 | .0 |
| 3.308 | 302. | 435. | 4.9 | 2362.1 | 2362.1 | .0 |
| 3.355 | 413. | 503. | 4.3 | 2365.7 | 2365.7 | .0 |
| 3.454 | 596. | 425. | 5.1 | 2371.8 | 2371.8 | .0 |
| 3.549 | 351. | 275. | 3.3 | 2380.0 | 2380.0 | .0 |
| 3.643 | 332. | 238. | 3.8 | 2387.5 | 2387.5 | .0 |
| 3.740 | 280. | 255. | 3.5 | 2395.6 | 2395.6 | .0 |
| 3.838 | 383. | 263. | 3.4 | 2404.7 | 2404.7 | .0 |
| 3.950 | 92. | 160. | 5.6 | 2415.1 | 2415.1 | .0 |
| 3.980 | 83. | 148. | 6.1 | 2417.7 | 2417.7 | .0 |
| 4.032 | 97. | 151. | 5.9 | 2422.6 | 2422.6 | .0 |
| 4.103 | 151. | 198. | 4.5 | 2428.4 | 2428.4 | .0 |
| 4.168 | 189. | 209. | 4.3 | 2434.3 | 2434.3 | .0 |
| 4.213 | 168. | 330. | 2.7 | 2435.6 | 2435.6 | .0 |
| 4.301 | 171. | 189. | 4.7 | 2442.9 | 2442.9 | .0 |
| 4.384 | 106. | 162. | 5.5 | 2449.5 | 2449.5 | .0 |
| 4.493 | 324. | 254. | 3.5 | 2458.6 | 2458.6 | .0 |
| 4.594 | 539. | 207. | 4.3 | 2467.4 | 2467.4 | .0 |
| 4.688 | 221. | 227. | 3.9 | 2475.6 | 2475.6 | .0 |
| 4.787 | 396. | 252. | 3.6 | 2484.2 | 2484.2 | .0 |
| 4.881 | 374. | 197. | 4.6 | 2489.5 | 2489.5 | .0 |
| 5.014 | 130. | 179. | 5.0 | 2500.0 | 2500.0 | .0 |
| 5.082 | 282. | 257. | 3.5 | 2506.6 | 2506.6 | .0 |
| 5.175 | 295. | 194. | 4.6 | 2514.5 | 2514.5 | .0 |
| 5.279 | 173. | 192. | 4.7 | 2522.3 | 2522.3 | .0 |
| -3.454 | 596. | 425. | 5.1 | 2371.8 | 2371.8 | .0 |
| .198 | 106. | 232. | 5.9 | 2377.6 | 2377.5 | .1 |
| .291 | 89. | 199. | 6.9 | 2382.4 | 2382.4 | .0 |
| .387 | 53. | 159. | 8.6 | 2387.7 | 2387.7 | .0 |
| .482 | 85. | 205. | 6.6 | 2392.0 | 2392.0 | .0 |
| .559 | 44. | 135. | 10.1 | 2400.7 | 2400.7 | .0 |
| .607 | 55. | 163. | 8.4 | 2403.5 | 2403.5 | .0 |

A/194

EXPLANATORY NOTES FOR
FORM 4 SECTION 5 PARAGRAPH 1.C

This watercourse islocated in a mountainous area. It is common for this watercourse to flow in subcritical, supercritical, and transitional flow regimes. The subcritical profile has been used to delineate the 100 year floodplain and prepare maps, tables, etc.

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>RIVERINE/COASTAL MAPPING FORM | O.M.B. Burden No. 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
|---|---|---|

**PUBLIC BURDEN DISCLOSURE NOTICE**

Public reporting burden for this form is estimated to average 1.5 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing and reviewing the form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden, to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, S.W., Washington, DC 20472; and to the Office of Management and Budget, Paperwork Reduction Project (3067-0148), Washington, DC 20503.

Community Name: Unincorporated Maricopa County/Town of Wickenburg

Flooding Source: WASH AB FLYING E WASH AND TRIBUTARIES

Project Name/Identifier: Wickenburg ADMS FCD 89-79

**1. MAPPING CHANGES**

1. A topographic work map of suitable scale, contour interval, and planimetric definition must be submitted showing *(indicate N/A when not applicable)*:

| | | Included | | |
|---|---|---|---|---|
| A. | Revised approximate 100-year floodplain boundaries (Zone A) | ☒ Yes | ☐ No | ☐ N/A |
| B. | Revised detailed 100- and 500-year floodplain boundaries | ☒ Yes | ☐ No | ☐ N/A |
| C. | Revised 100-year floodway boundaries | ☒ Yes | ☐ No | ☐ N/A |
| D. | Location and alignment of all cross sections used in the revised hydraulic model with stationing control indicated | ☒ Yes | ☐ No | ☐ N/A |
| E. | Stream alignments, road and dam alignments | ☒ Yes | ☐ No | ☐ N/A |
| F. | Current community boundaries | ☒ Yes | ☐ No | ☐ N/A |
| G. | Effective 100- and 500-year floodplain and 100-year floodway boundaries from the FIRM/FBFM reduced or enlarged to the scale of the topographic work map | ☐ Yes | ☐ No | ☒ N/A |
| H. | Tie-ins between the effective and revised 100- and 500-year floodplains and 100-year floodway boundaries | ☐ Yes | ☐ No | ☒ N/A |
| I. | The requestor's property boundaries and community easements | ☐ Yes | ☐ No | ☒ N/A |
| J. | The signed certification of a registered professional engineer | ☒ Yes | ☐ No | ☐ N/A |
| K. | Location and description of reference marks | ☒ Yes | ☐ No | ☐ N/A |
| L. | Vertical datum (example: NGVD, NAVD etc.) | ☒ Yes | ☐ No | ☐ N/A |
| M. | Coastal zone designations tie into adjacent areas not being revised | ☐ Yes | ☐ No | ☒ N/A |
| N. | Location and alignment of all coastal transects used to revise the coastal analyses | ☐ Yes | ☐ No | ☒ N/A |

If any of the items above are marked no or N/A, please explain: No [redacted], 500-year, or coastal zones revised or delineated; Revised 100-year floodplains tie into effective Hassayampa River floodplain.

2. What is the source and date of the updated topographic information *(example: orthophoto maps, July 1985; field survey, May 1979, beach profiles, June 1987, etc.)*? Photo: Jan. 1991 (E), Oct 1990 (W); Maps 1992

3. What is the scale and contour interval of the following work maps?
   a. Effective FIS unknown scale unknown Contour interval
   b. Revision Request 1" = 200' scale 2 FT AND 4 FT Contour interval

NOTE: Revised topographic information must be of equal or greater detail.

4. Attach an annotated FIRM and FBFM at the scale of the effective FIRM and FBFM showing the revised 100-year and 500-year floodplains and the 100-year floodway boundaries and how they tie into those shown on the effective FIRM and FBFM downstream and upstream of the revision or adjacent to the area of revision for coastal studies.

Attach additional pages if needed.

5. Flood Boundaries and 100-year water surface elevations:

Has the 100-year floodplain been shifted or increased or the 100-year water surface elevation increased at any location on property other than the requestor's or community's? ☐ Yes ☒ No

If yes, please give the location of shift or increase and an explanation for the increase.

Revised detailed 100-year floodplain replaces effective zone AE and A floodplain.

a. Have the affected property owners been notified of this shift or increase and the effect it will have on their property? ..... ☐ Yes ☒ No

If yes, please attach letters from these property owners stating they have no objections to the revised flood boundaries if a LOMR is being requested.

b. What is the number of insurable structures that will be impacted by this shift or increase? _____

6. Have the floodway boundaries shifted or increased at any location compared to those shown on the effective FBFM or FIRM? ..... ☐ Yes ☒ No

If yes, explain:

7. If a V-zone has been designated, has it been delineated to extend landward to the heel of the primary frontal dune? ☐ Yes ☒ No

If no, explain:

NA

8. Manual or digital map submission:

☒ Manual

☐ Digital

Digital map submissions may be used to update digital FIRMs (DFIRMs). For updating DFIRMs, these submissions must be coordinated with FEMA Headquarters as far in advance of submission as possible.

## 2. EARTH FILL PLACEMENT

1. The fill is: ☐ Existing ☐ Proposed ☒ N/A

2. Has fill been/will be placed in the regulatory floodway? ..... ☐ Yes ☒ No
   If yes, please attach completed Riverine Hydraulic Analysis Form.

3. Has fill been/will be placed in floodway fringe *(area between the floodway and 100-year floodplain boundaries)*? ..... ☐ Yes ☒ No

   If yes, then complete A, B, C, and D below.

   A. Are fill slopes for granular materials steeper than one vertical on one-and-one-half horizontal? ..... ☐ Yes ☐ No

      If yes, justify steeper slopes_____

      B. Is adequate erosion protection provided for fill slopes exposed to moving flood waters? *(Slopes exposed to flows with velocities of up to 5 feet per second (fps) during the 100-year flood must, at a minimum, be protected by a cover of grass, vines, weeds, or similar vegetation; slopes exposed to flows with velocities greater than 5 fps during the 100-year flood must, at a minimum, be protected by stone or rock riprap.)* ..... ☐ Yes ☐ No

      If no, describe erosion protection provided_____

      C. Has all fill placed in revised 100-year floodplain been compacted to 95 percent of the maximum density obtainable with the Standard Proctor Test Method or acceptable equivalent method? ☐ Yes ☐ No

      D. Can structures conceivably be constructed on the fill at any time in the future? ☐ Yes ☐ No

      If yes, provide certification of fill compaction (item C. above) by the community's NFIP permit official, a registered professional engineer, or an accredited soils engineer.

4. Has fill been/will be placed in a V-zone? ☐ Yes ☒ No

   If yes, is the fill protected from erosion by a flood control structure such as a revetment or seawall? ☐ Yes ☐ No

   If yes, attach the coastal structures form.

BRIDGE

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>BRIDGE/CULVERT FORM | O.M.B. Burden No. 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
|---|---|---|

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Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AB: FLYING E WASH

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. IDENTIFIER

1. Name of roadway, railroad, etc.: AT & SF RAILWAY
2. Location of bridge/culvert along flooding source (in terms of stream distance or cross-section identifier): Station 0.131 to Station 0.134
3. This revision reflects *(check one of the following)*:
   - ☒ New bridge/culvert not modeled in the FIS
   - ☐ Modified bridge/culvert previously modeled in the FIS
   - ☐ New analysis of bridge/culvert previously modeled in the FIS

   *(Explain why new analysis was performed)*

### 2. BACKGROUND

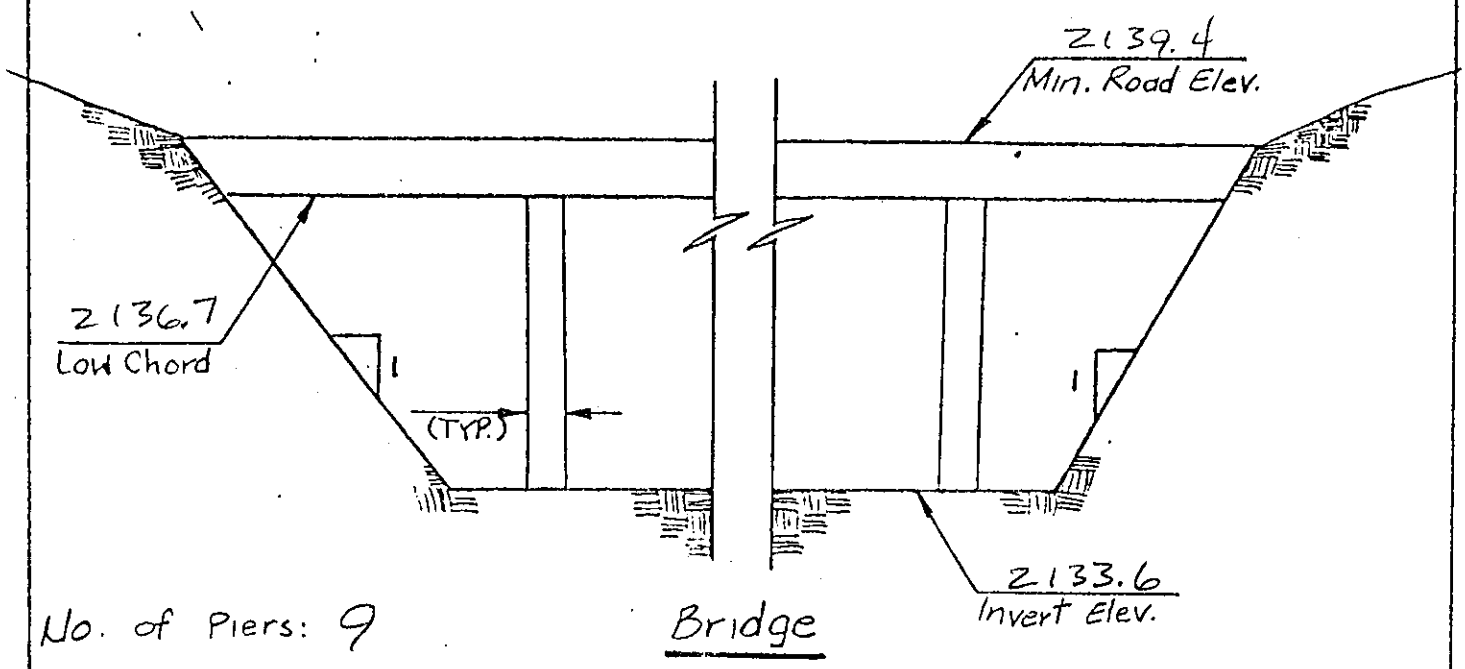
Provide the following information about the structure:

1. Dimension, material, and shape (e.g. two 10 x 5 feet reinforced concrete box culvert; three 30-foot span bridge with 2 rows of two 3- foot diameter circular piers; 40-foot wide ogee shape spillway) Ten 13-ft span wooden bridge with nine triple post bents of 1ft dia wood piles
2. Entrance geometry of culvert/type of bridge opening (e.g. 30° - 75° wing walls with square top edge, sloping embankments and vertical abutments) Sloping embankments and vertical abutments
3. Hydraulic model used to analyze the structure *(e.g., HEC-2 with special bridge routine, WSPRO, HY8)* HEC-2 with special bridge routine

If different than hydraulic analysis for the flooding source, justify why the hydraulic analysis used for the flooding source could not analyze the structure(s). *(Attach justification)*

Note: If any items do not apply to submitted hydraulic analysis, indicate by N/A
* One form per new/revised bridge/culvert

Sketch the downstream face of the structure together with the road profile. Show, at a minimum, the maximum low chord elevation, invert elevation, minimum top of road elevation, and ineffective flow widths.

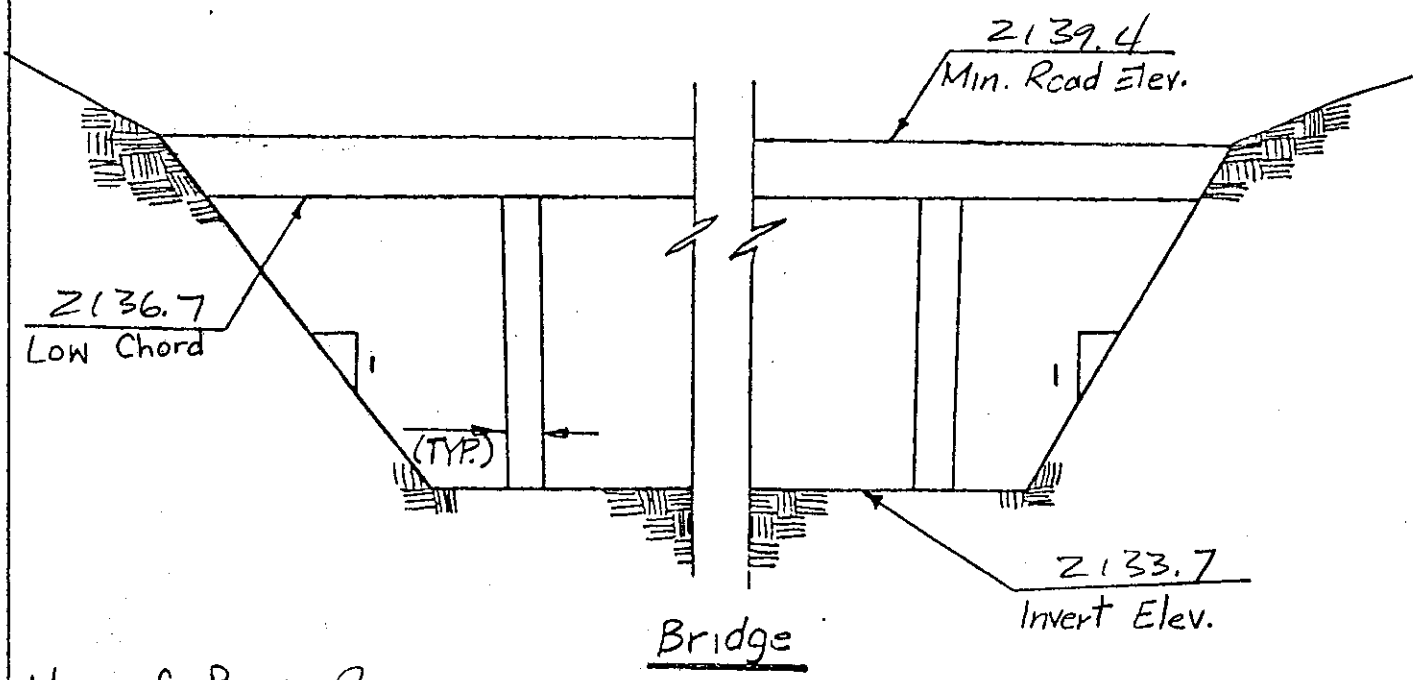



No. of Piers: 9

Total Width of Piers: 9 ft

See Cross Section #0.131

Sketch the upstream face of the structure together with the road profile. Show, at a minimum, the maximum low chord elevation, invert elevation, and minimum top of road elevation.

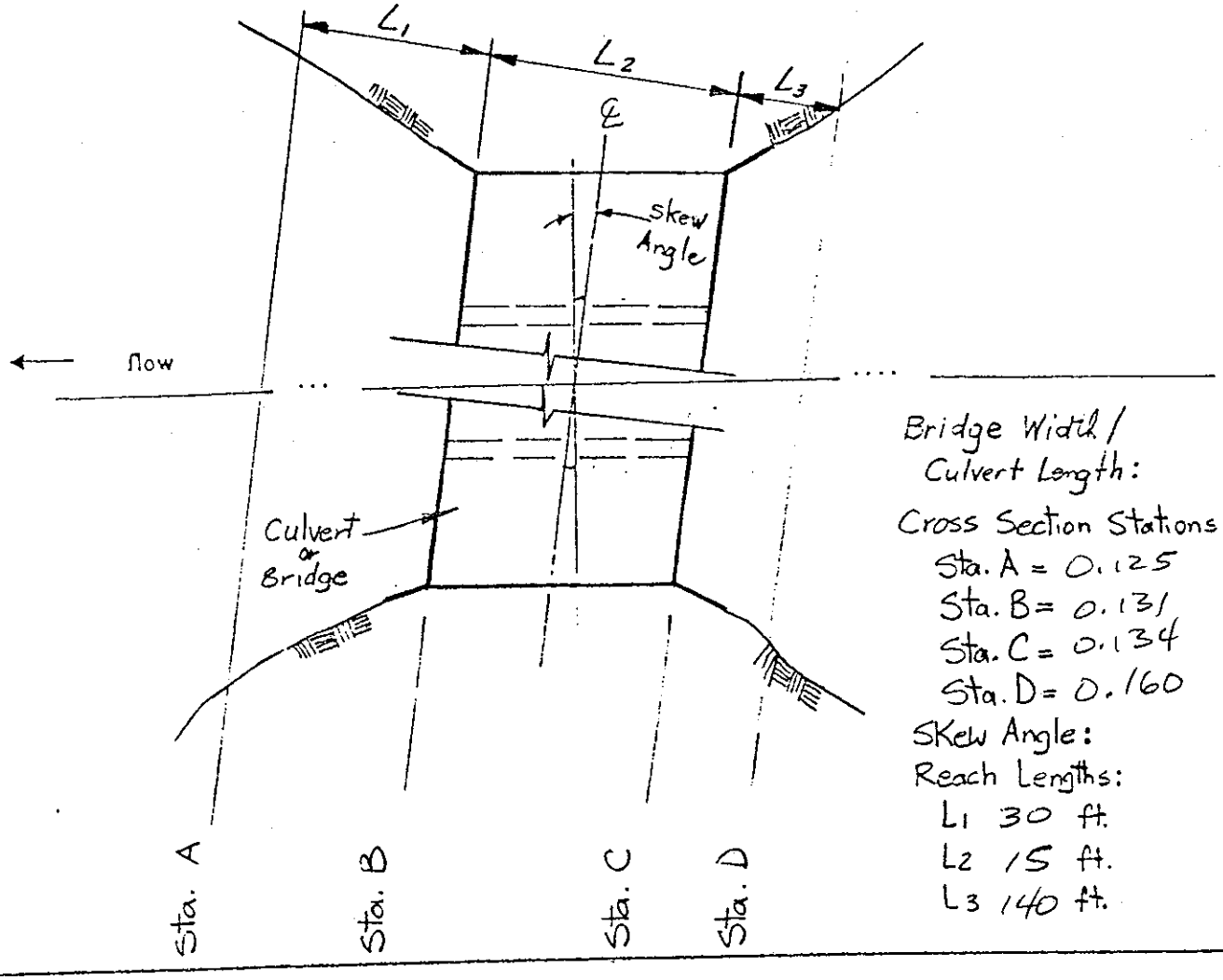



No. of Piers: 9

Total Width of Piers: 9 ft

See Cross Section #0.134

etch the plan view of the structure(s) Show, at a minimum, the skew angle, cross-section locations, distances tween cross sections, and length of structure (s).




Bridge Width / Culvert Length:

Cross Section Stations
Sta. A = 0.125
Sta. B = 0.131
Sta. C = 0.134
Sta. D = 0.160

Skew Angle:

Reach Lengths:
L1 30 ft.
L2 15 ft.
L3 140 ft.

Attach plans of the structure (s) certified by a registered Professional Engineer.

| | |
|---|---|
| Culvert length or bridge width (ft) | 138 |
| Calculated culvert/bridge area (ft²) by the hydraulic model, if applicable | 387 |
| Total culvert/bridge area (ft²) | 387 |

Elevations Above Which Flow is Effective for Overbanks

| | Left Overbank | Right Overbank |
|---|---|---|
| Upstream face | 2139.9 | 2139.4 |
| Downstream face | 2139.9 | 2139.4 |

Minimum Top of Road Elevation

| | Left Overbank | Right Overbank |
|---|---|---|
| Upstream face | 2139.4 | 2139.4 |
| Downstream face | 2139.4 | 2139.4 |

| 100-Year Elevations | Water Surface Elevations | Energy Gradient Elevations |
|---|---|---|
| Upstream face | 2139.16 | 2139.40 |
| Downstream face | 2137.70 | 2138.14 |

| Discharge | Low Flow | Pressure Flow | Weir Flow | Total Flow |
|---|---|---|---|---|
| Amount of flow through/over the structure (s) (cfs) | — | 2999 | 0 | 3002.4* |

The maximum depth of flow over the roadway/railroad (ft.) ..... —

Weir length (ft.) ..... —

Top Widths

| | Floodplain | Floodway |
|---|---|---|
| Upstream face | 138 | |
| Downstream face | 138 | |

Top Widths

| | Effective Flow | Effective and Ineffective Flow |
|---|---|---|
| Upstream face | 138 | |
| Downstream face | 138 | |

*Split flow option used to calculate flow diverted over low right bank berm upstream of bridge.

Loss Coefficients

| | |
|---|---|
| Entrance loss coefficient | — |
| Manning's "n" value assigned to the structure(s) | — |
| Friction loss coefficient through structure (s) | — |
| Other loss coefficients (e.g., bend manhole, etc.) | — |
| Total loss coefficient | 1.83 |
| Weir coefficient | 2.8 |
| Pier coefficient | 1.05 |
| Contraction loss coefficient | 0.3 |
| Expansion loss coefficient | 0.5 |

4. SEDIMENT TRANSPORT CONSIDERATIONS

1. A. Is there any indication from historical records that sediment transport *(including scour and deposition)* can affect the 100-year water surface elevations? ..... ☐ Yes ☐ No

B. Based on the conditions *(such as geomorphology, vegetative cover and development of the watershed and stream bed, and bank conditions)*, is there a potential for debris and sediment transport *(including scour and deposition)* to affect the 100-year water surface elevations and/or conveyance capacity through the bridge/culvert? ..... ☐ Yes ☐ No

.. If the answer to either 1A or 1B is yes:

A. What is the estimated sediment *(bed material)* load?
_____cfs *(attach gradation curve)*

Explain method used to estimate the sediment transport and the depth of scour and/or deposition NA - Sediment transport not considered in analysis.

B. Will sediment accumulate anywhere through the bridge/culvert? ☐ Yes ☐ No

If yes, explain the impact on the conveyance capacity through the bridge/culvert?

5. FLOODWAY ANALYSIS

Explain method of bridge encroachment (floodway run) No additional encroachment for floodway analysis

Comments (*explain any unusual situations*):

Flow is diverted over a low right bank berm. See attached special problem report

Attach analysis.

BRIDGE

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>BRIDGE/CULVERT FORM | O.M.B. Burden No. 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
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Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AE: FLYING E WASH

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. IDENTIFIER

1. Name of roadway, railroad, etc.: U.S HWY 60
2. Location of bridge/culvert along flooding source (in terms of stream distance or cross-section identifier): Station 2.109 to Station 2.118
3. This revision reflects *(check one of the following)*:
   - ☐ New bridge/culvert not modeled in the FIS
   - ☐ Modified bridge/culvert previously modeled in the FIS
   - ☒ New analysis of bridge/culvert previously modeled in the FIS

   *(Explain why new analysis was performed)* NEW TOPOGRAPHIC DATA

### 2. BACKGROUND

Provide the following information about the structure:

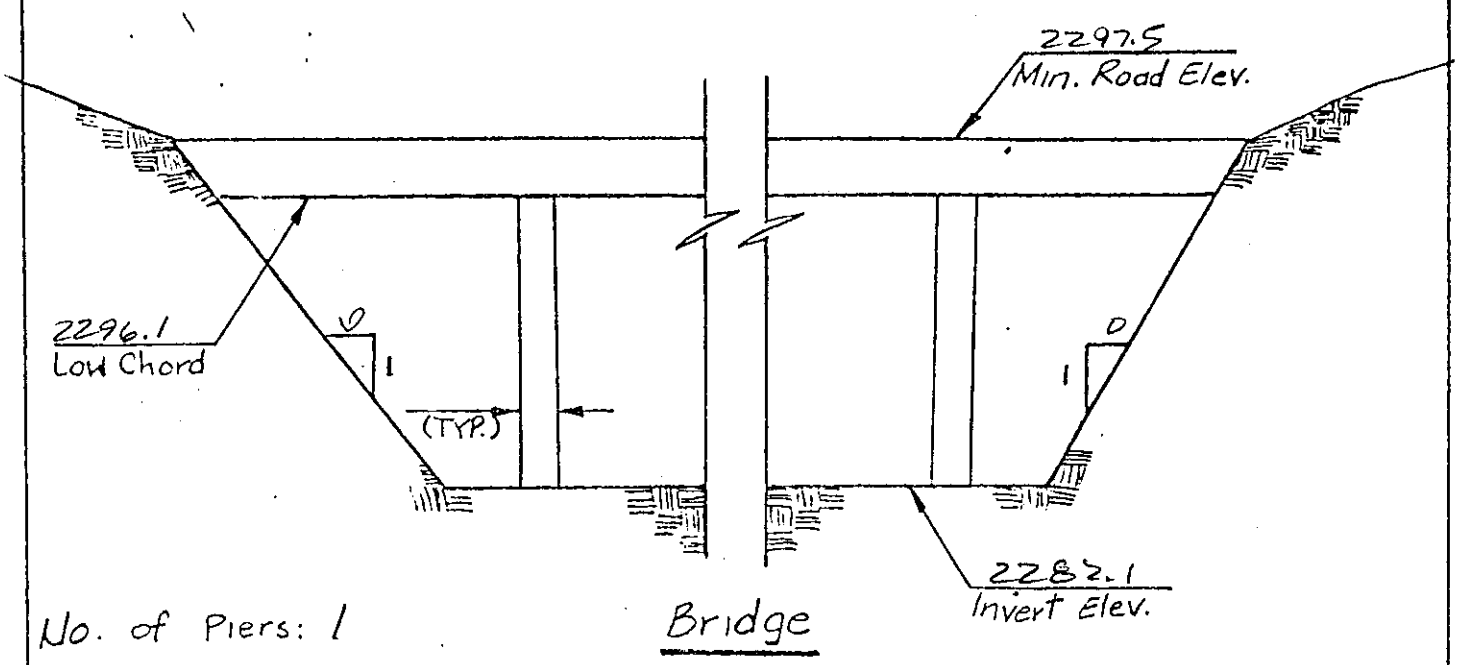
1. Dimension, material, and shape (e.g. two 10 x 5 feet reinforced concrete box culvert; three 30-foot span bridge with 2 rows of two 3- foot diameter circular piers; 40-foot wide ogee shape spillway) Two 30 foot span concrete bridge
2. Entrance geometry of culvert/type of bridge opening (e.g. 30° - 75° wing walls with square top edge, sloping embankments and vertical abutments) Sloping approach embankments to 30-70° Wingwalls and vertical abutments, Second bridge just upstream
3. Hydraulic model used to analyze the structure (*e.g., HEC-2 with special bridge routine, WSPRO, HY8*) HEC-2 with special bridge routine

If different than hydraulic analysis for the flooding source, justify why the hydraulic analysis used for the flooding source could not analyze the structure(s). *(Attach justification)*

Note: If any items do not apply to submitted hydraulic analysis, indicate by N/A

* One form per new/revised bridge/culvert

Sketch the downstream face of the structure together with the road profile. Show, at a minimum, the maximum low chord elevation, invert elevation, minimum top of road elevation, and ineffective flow widths.

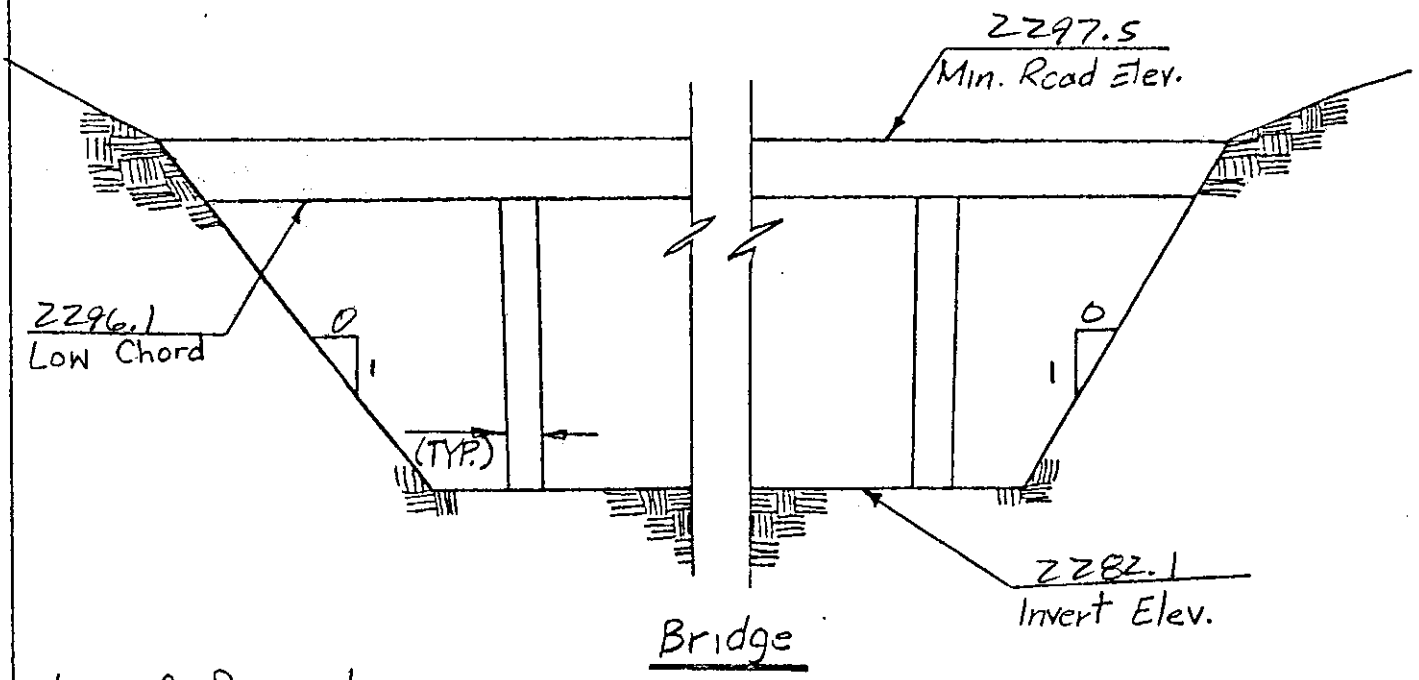



No. of Piers: 1

Total Width of Piers: 1.5 ft

See Cross Section #2.109

Sketch the upstream face of the structure together with the road profile. Show, at a minimum, the maximum low chord elevation, invert elevation, and minimum top of road elevation.

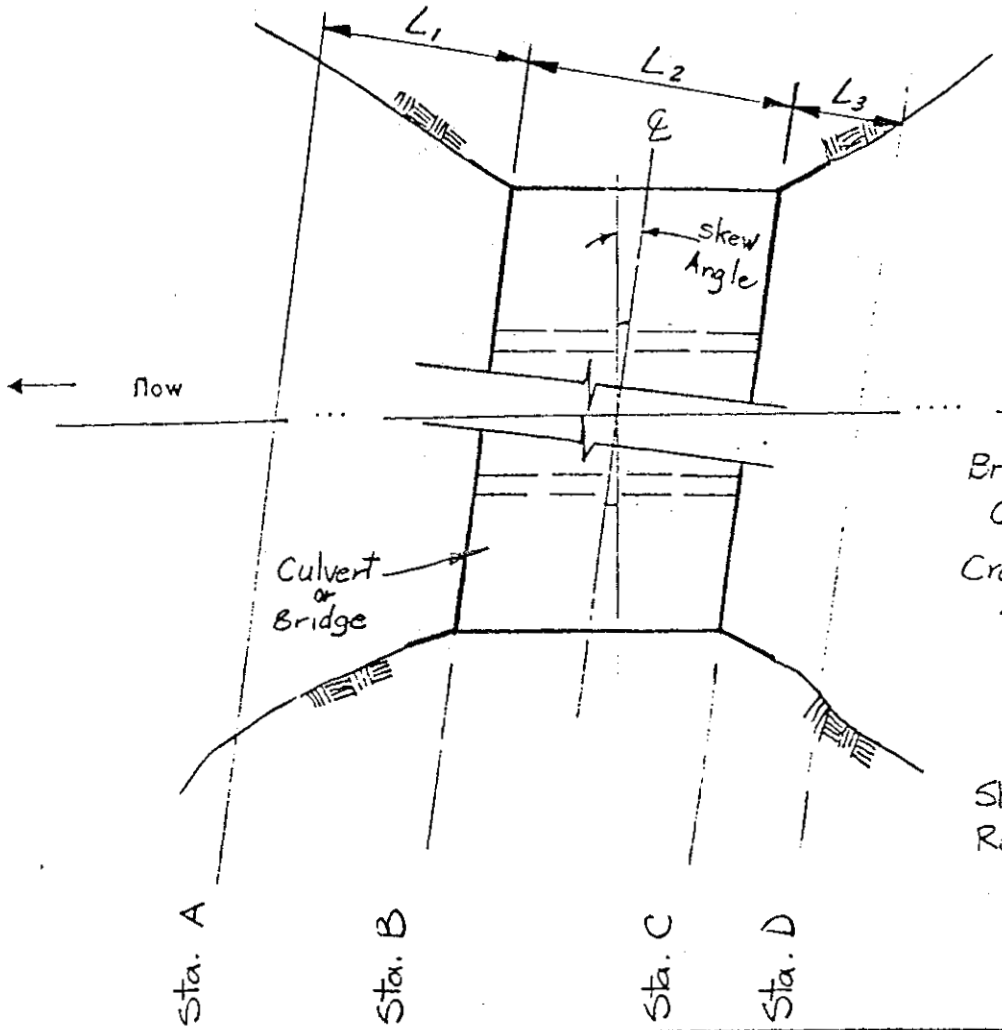



No. of Piers: 1

Total Width of Piers: 1.5 ft

See Cross Section #2.118

Sketch the plan view of the structure(s) Show, at a minimum, the skew angle, cross-section locations, distances between cross sections, and length of structure (s).




Bridge Width / Culvert Length: 45'

Cross Section Stations

Sta. A = 2.107

Sta. B = 2.109

Sta. C = 2.118

Sta. D = 2.120

Skew Angle: 0

Reach Lengths:

L1 10 ft.

L2 45 ft.

L3 10 ft.

Attach plans of the structure (s) certified by a registered Professional Engineer.

| | |
|---|---|
| Culvert length or bridge width (ft) | 61.9 |
| Calculated culvert/bridge area ($ft^2$) by the hydraulic model, if applicable | 845.6 |
| Total culvert/bridge area ($ft^2$) | 845.6 |

Elevations Above Which Flow is Effective for Overbanks

| | Left Overbank | Right Overbank |
|---|---|---|
| Upstream face | _____ | _____ |
| Downstream face | _____ | _____ |

Minimum Top of Road Elevation

| | Left Overbank | Right Overbank |
|---|---|---|
| Upstream face | _____ | _____ |
| Downstream face | _____ | _____ |

| 100-Year Elevations | Water Surface Elevations | Energy Gradient Elevations |
|---|---|---|
| Upstream face | _____ | _____ |
| Downstream face | _____ | _____ |

| Discharge | Low Flow | Pressure Flow | Weir Flow | Total Flow |
|---|---|---|---|---|
| Amount of flow through/over the structure (s) (cfs) | _____ | _____ | _____ | _____ |

The maximum depth of flow over the roadway/railroad (ft.) ..... _____

Weir length (ft.) ..... _____

Top Widths

| | Floodplain | Floodway |
|---|---|---|
| Upstream face | _____ | _____ |
| Downstream face | _____ | _____ |

Top Widths

| | Effective Flow | Effective and Ineffective Flow |
|---|---|---|
| Upstream face | _____ | _____ |
| Downstream face | _____ | _____ |

Loss Coefficients

| | |
|---|---|
| Entrance loss coefficient | — |
| Manning's "n" value assigned to the structure(s) | — |
| Friction loss coefficient through structure (s) | — |
| Other loss coefficients (e.g., bend manhole, etc.) | — |
| Total loss coefficient | 1.56 |
| Weir coefficient | 2.8 |
| Pier coefficient | 1.25 |
| Contraction loss coefficient | 0.30 |
| Expansion loss coefficient | 0.50 |

4. SEDIMENT TRANSPORT CONSIDERATIONS

1. A. Is there any indication from historical records that sediment transport *(including scour and deposition)* can affect the 100-year water surface elevations? ..... ☐ Yes ☐ No

B Based on the conditions *(such as geomorphology, vegetative cover and development of the watershed and stream bed, and bank conditions)*, is there a potential for debris and sediment transport *(including scour and deposition)* to affect the 100-year water surface elevations and/or conveyance capacity through the bridge/culvert? ..... ☐ Yes ☐ No

.. If the answer to either 1A or 1B is yes:

A. What is the estimated sediment *(bed material)* load?
_____cfs *(attach gradation curve)*

Explain method used to estimate the sediment transport and the depth of scour and/or deposition NA - Sediment transport not considered in analysis.

B. Will sediment accumulate anywhere through the bridge/culvert? ☐ Yes ☐ No

If yes, explain the impact on the conveyance capacity through the bridge/culvert?_____

5. FLOODWAY ANALYSIS

Explain method of bridge encroachment (floodway run) No additional encroachment at bridge

Comments *(explain any unusual situations)*:

Abandoned US60 bridge lies just upstream - see following FORM 7

Attach analysis.

BRIDGE

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>BRIDGE/CULVERT FORM | O.M.B. Burden No. 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
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Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AB: FLYING E WASH

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. IDENTIFIER

1. Name of roadway, railroad, etc.: ABANDONED U.S. HWY 60
2. Location of bridge/culvert along flooding source (in terms of stream distance or cross-section identifier): Station 2.120 to Station 2.125
3. This revision reflects (*check one of the following*):
   - ☐ New bridge/culvert not modeled in the FIS
   - ☐ Modified bridge/culvert previously modeled in the FIS
   - ☒ New analysis of bridge/culvert previously modeled in the FIS

   (*Explain why new analysis was performed*) NEW TOPOGRAPHIC DATA

### 2. BACKGROUND

Provide the following information about the structure:

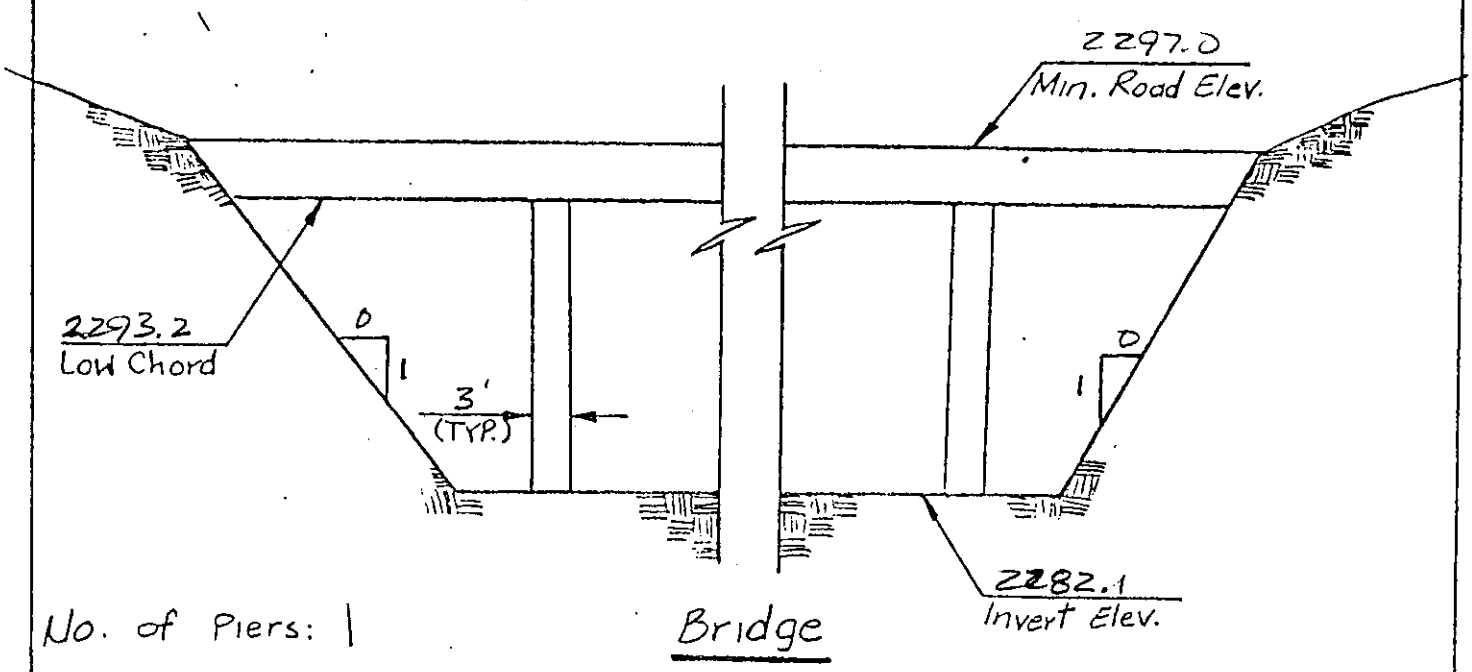
1. Dimension, material, and shape (e.g. two 10 x 5 feet reinforced concrete box culvert; three 30-foot span bridge with 2 rows of two 3- foot diameter circular piers; 40-foot wide ogee shape spillway) Two 28-ft span Concrete bridge
2. Entrance geometry of culvert/type of bridge opening (e.g. 30° - 75° wing walls with square top edge, sloping embankments and vertical abutments) Sloping approach embankments to 30-70° Wing walls and vertical abutments; Second bridge just downstream
3. Hydraulic model used to analyze the structure (*e.g., HEC-2 with special bridge routine, WSPRO, HY8*) HEC-2 with special bridge routine

If different than hydraulic analysis for the flooding source, justify why the hydraulic analysis used for the flooding source could not analyze the structure(s). (*Attach justification*)

Note: If any items do not apply to submitted hydraulic analysis, indicate by N/A

* One form per new/revised bridge/culvert

Sketch the downstream face of the structure together with the road profile. Show, at a minimum, the maximum low chord elevation, invert elevation, minimum top of road elevation, and ineffective flow widths.

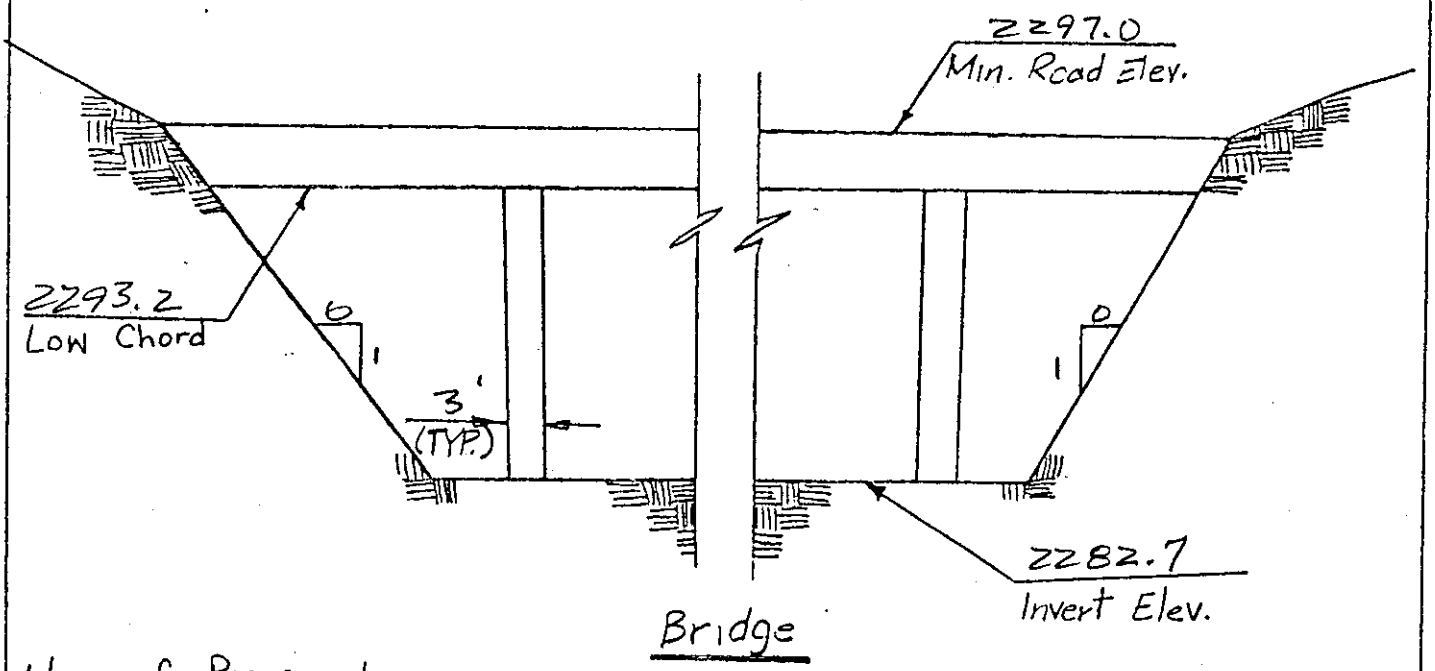



No. of Piers: 1

Total Width of Piers: 3 ft

See Cross Section # 2.120

Sketch the upstream face of the structure together with the road profile. Show, at a minimum, the maximum low chord elevation, invert elevation, and minimum top of road elevation.

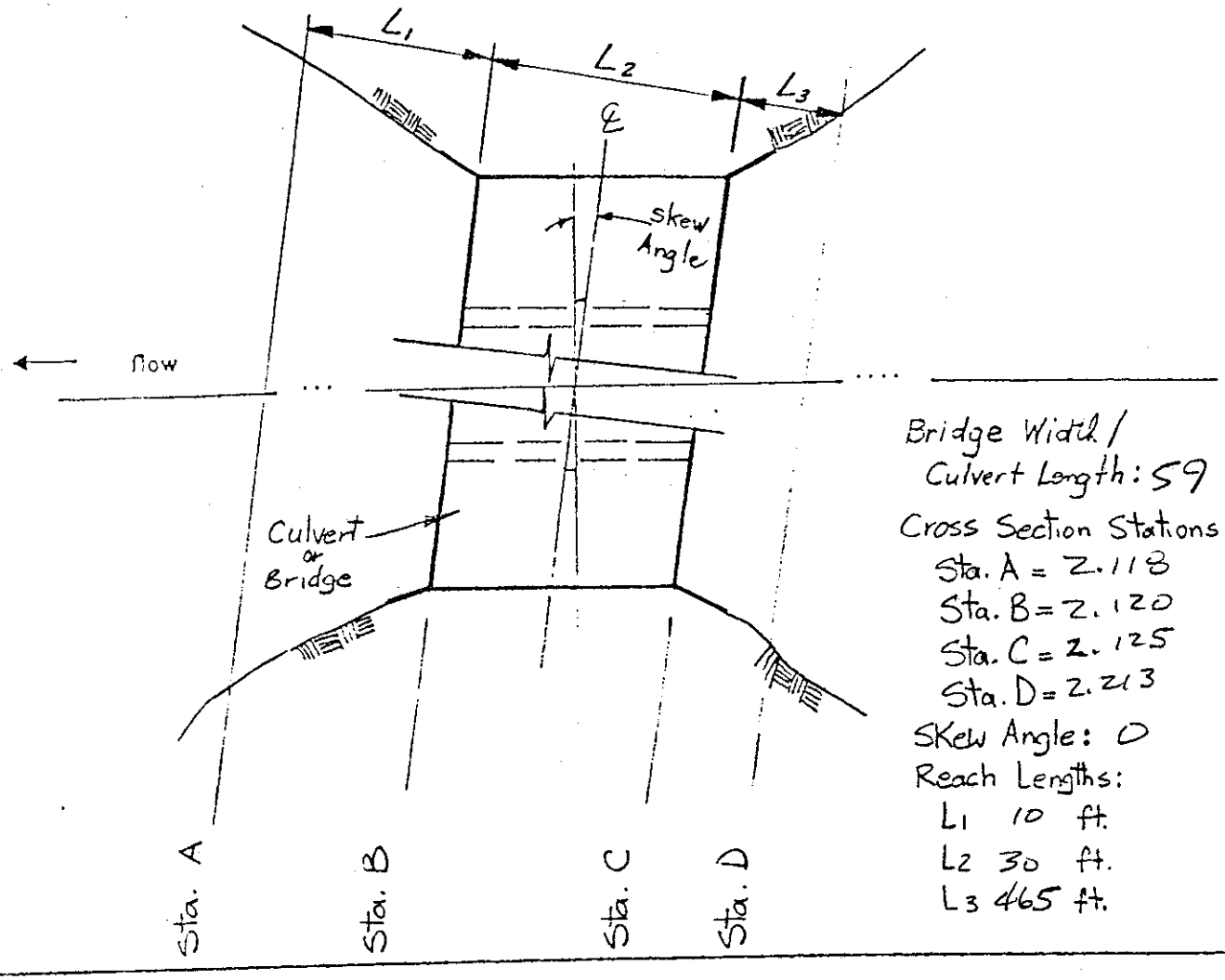



No. of Piers: 1

Total Width of Piers: 3 ft

See Cross Section # 2.125

Sketch the plan view of the structure(s) Show, at a minimum, the skew angle, cross-section locations, distances between cross sections, and length of structure (s).




Bridge Width / Culvert Length: 59

Cross Section Stations

Sta. A = 2.118

Sta. B = 2.120

Sta. C = 2.125

Sta. D = 2.213

Skew Angle: 0

Reach Lengths:

L1 10 ft.

L2 30 ft.

L3 465 ft.

Attach plans of the structure (s) certified by a registered Professional Engineer.

| | |
|---|---|
| Culvert length or bridge width (ft) | 59 |
| Calculated culvert/bridge area (ft²) by the hydraulic model, if applicable | 588 |
| Total culvert/bridge area (ft²) | 588 |

Elevations Above Which Flow is Effective for Overbanks

| | Left Overbank | Right Overbank |
|---|---|---|
| Upstream face | 2297.0 | 2297.5 |
| Downstream face | 2297.0 | 2297.5 |

Minimum Top of Road Elevation

| | Left Overbank | Right Overbank |
|---|---|---|
| Upstream face | 2297.0 | 2297.0 |
| Downstream face | 2297.0 | 2297.0 |

| 100-Year Elevations | Water Surface Elevations | Energy Gradient Elevations |
|---|---|---|
| Upstream face | 2292.45 | 2294.71 |
| Downstream face | 2290.67 | 2293.60 |

| Discharge | Low Flow | Pressure Flow | Weir Flow | Total Flow |
|---|---|---|---|---|
| Amount of flow through/over the structure (s) (cfs) | 6943 | — | — | 6943 |

The maximum depth of flow over the roadway/railroad (ft.) ..... —

Weir length (ft.) ..... —

Top Widths

| | Floodplain | Floodway |
|---|---|---|
| Upstream face | 59 | 59 |
| Downstream face | 59 | 59 |

Top Widths

| | Effective Flow | Effective and Ineffective Flow |
|---|---|---|
| Upstream face | 59 | 59 |
| Downstream face | 59 | 59 |

Loss Coefficients

| | |
|---|---|
| Entrance loss coefficient | — |
| Manning's "n" value assigned to the structure(s) | — |
| Friction loss coefficient through structure (s) | — |
| Other loss coefficients (e.g., bend manhole, etc.) | — |
| Total loss coefficient | 1.56 |
| Weir coefficient | 2.8 |
| Pier coefficient | 1.25 |
| Contraction loss coefficient | 0.30 |
| Expansion loss coefficient | 0.50 |

4. SEDIMENT TRANSPORT CONSIDERATIONS

1. A. Is there any indication from historical records that sediment transport (*including scour and deposition*) can affect the 100-year water surface elevations? ..... ☐ Yes ☐ No

B Based on the conditions (*such as geomorphology, vegetative cover and development of the watershed and stream bed, and bank conditions*), is there a potential for debris and sediment transport (*including scour and deposition*) to affect the 100-year water surface elevations and/or conveyance capacity through the bridge/culvert? ..... ☐ Yes ☐ No

.. If the answer to either 1A or 1B is yes:

A. What is the estimated sediment (*bed material*) load?
_____cfs (*attach gradation curve*)

Explain method used to estimate the sediment transport and the depth of scour and/or deposition NA - Sediment transport not considered in analysis.

B. Will sediment accumulate anywhere through the bridge/culvert? ☐ Yes ☐ No

If yes, explain the impact on the conveyance capacity through the bridge/culvert?_____

5. FLOODWAY ANALYSIS

Explain method of bridge encroachment (floodway run) NA

Comments *(explain any unusual situations)*:

Attach analysis.

89, 92 105, 113

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>RIVERINE HYDRAULIC ANALYSIS FORM | O.M.B. Burden No 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
|---|---|---|

## PUBLIC BURDEN DISCLOSURE NOTICE

Public reporting burden for this form is estimated to average 2.25 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing and reviewing the form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden, to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, S.W., Washington, DC 20472; and to the Office of Management and Budget, Paperwork Reduction Project (3067-0148), Washington, DC 20503.

Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AB: GEORGE'S TANK BREAKOUT FROM FLYING E WASH
*(One form for each flooding source)*

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. REACH TO BE REVISED

Downstream limit: Confluence with Flying E Wash

Upstream limit: West edge of George's Tank

### 2. EFFECTIVE FIS

☒ Not studied

☐ Studied by approximate methods

Downstream limit of study _____

Upstream limit of study _____

☐ Studied by detailed methods

Downstream limit of study _____

Upstream limit of study _____

☐ Floodway delineated

Downstream limit of Floodway _____

Upstream limit of Floodway _____

### 3. HYDRAULIC ANALYSIS

Why is the hydraulic analysis different from that used to develop the FIRM. *(Check all that apply)*

☒ Not studied in FIS

☒ Improved hydrologic data/analysis. Explain: Hydrologic Analysis procedures standardized by the Flood Control District of Maricopa County

☐ Improved hydraulic analysis. Explain: _____

☐ Flood control structure. Explain: _____

☐ Other. Explain: _____

Full input and output listings along with files on diskette *(if available)* for each of the models listed below and summary of the source of input parameters used in the models must be provided. The summary must include a complete description of any changes made from model to model (*e.g. duplicate effective model to corrected effective model)*. Only the Duplicate Effective and the Revised or Post-Project Conditions models must be submitted. See instructions for directions on when other models may be required. Only the 100-year flood profile is required for SFHAs with a Zone A designation. For areas which do not have detailed flooding, a hydraulic model is not required; however BFE's may not be added to the revised FIRM.

☐ Duplicate Effective Model — Natural ☐ Floodway ☐

Copies of the hydraulic analysis used in the effective FIS, referred to as the effective models *(10-, 50-, 100-, and 500-year multi-profile runs and the floodway run)* must be obtained and then reproduced on the requestor's equipment to produce the duplicate effective model. This is required to assure that the effective model input data has been transferred correctly to the requestor's equipment and to assure that the revised data will be integrated into the effective data to provide a continuous FIS model upstream and downstream of the revised reach.

☐ Corrected Effective Model — Natural ☐ Floodway ☐

The corrected effective model is the model that corrects any errors that occur in the duplicate effective model, adds any additional cross sections to the duplicate effective model, or incorporates more detailed topographic information than that used in the currently effective model. The corrected effective model must not reflect any man-made physical changes since the date of the effective model. An error could be a technical error in the modeling procedures, or any construction in the floodplain that occurred prior to the date of the effective model but was not incorporated into the effective model.

☐ Existing or Pre-Project Conditions Model — Natural ☐ Floodway ☐

The duplicate effective or corrected model is modified to produce the existing or pre-project conditions model to reflect any modifications that have occurred within the floodplain since the date of the effective model but prior to the construction of the project for which the revision is being requested. If no modification has occurred since the date of the effective model, then this model would be identical to the corrected effective or duplicate effective model.

☐ Revised or Post-Project Conditions Model — Natural ☐ Floodway ☐

The existing or pre-project conditions model *(or duplicate effective or corrected effective model, as appropriate)* is revised to reflect revised or post-project conditions. This model must incorporate any physical changes to the floodplain since the effective model was produced as well as the effects of the project. When the request is for proposed project this model should reflect proposed conditions.

☒ Other: Please attach a sheet describing all other models or calculations submitted. — Natural ☒ Floodway ☒

New Model
(Proposed Effective Model)

## 4. MODEL PARAMETERS *(from model used to revise 100-year water surface elevation)*

| Discharges: | Upstream Limit | Downstream Limit |
|---|---|---|
| 10-year | | |
| 50-year | | |
| 100-year | 1109 | 1586 |
| 500-year | | |

Attach diagram showing changes in 100-year discharge

2. Explain how the starting water surface elevations were determined Starting water surface elevation from Flying E Wash analysis at section/station No 2.630

3. Give range of friction loss coefficients (*Manning's "N"*) Channel ..... 0.030

Overbanks ..... 0.045

If friction loss coefficients are different anywhere along the revised reach from those used to develop the FIRM, give location, value used in the effective FIS, and revised values and an explanation as to how the revised values were determined.

| Location | FIS | Revised |
|---|---|---|
| NA | | |
| | | |
| | | |
| | | |

Explain:

4. Describe how the cross section geometry data were determined (*e.g., field survey, topographic map, taken from previous study*) and list cross sections that were added.

Data points for cross sections are based on the [redacted] topographic maps (2 ft and 4 ft contour intervals)

5. Explain how reach lengths for channel and overbanks were determined:

All reach lengths were measured from floodplain work maps.

## 5. RESULTS (from model used to revise 100-year water surface elevations)

1. Do the results indicate:

a. Water surface elevations higher than end points of cross sections? ..... ☐ Yes ☒ No

b. Supercritical depth? ..... ☐ Yes ☒ No

c. Critical depth? ..... ☐ Yes ☐ No

d. Other unique situations ..... ☒ Yes ☐ No

(If yes, Special Problem Report attached)

If yes to any of the above, attach an explanation that discusses the situation and how it is presented on the profiles, tables, and maps.

2. What is the maximum change in energy gradient between cross-sections? ..... See Special Problem Report Attached

Specify location .....

3. What is the distance between the cross-sections in 2 above? .....

Specify location .....

4. What is the maximum distance between cross-sections? ..... _____

Specify location ..... _____

5. Floodway determination

a. What is the maximum surcharge allowed by the community or State? ..... 1 foot

b. What is the maximum surcharge for the revised conditions? ..... _____ foot

Specify location ..... _____

c. What is the maximum velocity? ..... _____ fps

Specify location ..... _____

Explain: [redacted]

d. Are there any negeative surcharge values at any cross-section ☐ Yes ☐ No

If yes, the floodway may need to widen. If it is not widened, please explain and indicate the maximum negative surcharge.

6. Is the discharge value used to determine the floodway anywhere different from that used to determine the natural 100-year flood elevations? ..... ☐ Yes ☒ No

If Yes, explain:

7. Do 100-year water surface elevations increase at any location? ..... ☐ Yes ☒ No

If yes, please attach a list of the locations where the increases occur, state whether or not the increases are located on the requestor's property, and provide an explanation of the reason for the increases.

NA- New Model

Please attach a completed comparison table entitled: *Water Surface Elevation Check* (See page 6)

## 6. REVISED FIRM/FBFM AND FLOOD PROFILES

A. The revised water surface elevations tie into those computed by the effective FIS Model *(10-, 50-, 100-, and 500-year)*, downstream of the project at cross-section NA within _____ feet and upstream of the project at cross section _____ within _____ feet.

B. The revised floodway elevations tie into those computed by the effective FIS model, dowstream of the project at cross section NA within _____ feet and upstream of the project at cross section _____ within NA feet.

C. Attach profiles, at the same vertical and horizontal scale as the profiles in the effective FIS report, showing stream bed and profiles of all floods studied (without encroachment). Also, label all cross sections, road crossings (including low chord and top-of-road data), culverts, tributaries, corporate limits, and study limits. If channel distance has changed, the stationing should be revised for all profile sheets.

D. Attach a Floodway Data Table showing data for each cross section listed in the published Floodway Data Table in the FIS report.

Proceed to Riverine /Coastal Mapping Form

FEDERAL EMERGENCY MANAGMENT AGENCY

# WATER SURFACE ELEVATION CHECK

COMMUNITY NAME: Unincorporated Maricopa County/ Town of Wickenburg

FLOODIND SOURCE:

PROJECT NAME /IDENTIFIER: Wickenburg ADMS FCD89-79

| | EFFECTIVE | | | DUPLICATE EFFECTIVE | | | CORRECTED EFFECTIVE | | | EXISTING/PRE-PROJECT | | | REVISED/PROJECT | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SECNO | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] |
| | | | | | | | | | | | | | | | |
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COMMENTS: New Model - See following Floodway Data Table

1-100-year (natural) Water Surface Elevation 2-Encroachment (floodway) Water Surface Elevation 3-Surcharge Value

Include all cross sections in the models between tie-in points. Any interpolated values should be indicated in parentheses.

Sheet 1 of 1

Town of Wickenburg (CID 040056) and Unincorporated Maricopa County (CID 040037) Arizona.

November 1992.

Black & Veatch (PN 17676) / Coe & Van Loo for the Flood Control District of Maricopa County (Contract FCD 89-79).

Various Washes in and near the Town of Wickenburg.

Documentation Index Number 4.5. Special Problem Report.

PREPARER: Black & Veatch.

LOCATION/SPECIAL PROBLEM DESCRIPTION:

*GEORGE'S TANK BREAKOUT CHANNEL*

MAP SHEETS 87, 98, 108, 118

George's Tank Breakout Channel. The HEC-2 model pertaining to the area is UFEW.* on the FLYINGE diskette. Subdirectory GTANK contains several HEC-2 files used to calculate normal depth for Zone A determination in the George's Tank Breakout channel.

George's Tank is a small storage facility that was formed by damming Flying E Wash. The tank has a permitted water right for stock watering. No design or construction data is available. In keeping with FEMA policy, this structure is not considered dependable for flood risk planning, and is omitted from the base model used to establish regulatory floodplains.

Topographic maps prepared for this study indicate that the top of the dam is approximately 7 ft higher than an area along the west edge of the storage area. The general condition of the dam is good. From field reconnaissance and evaluation of the maximum 100-year water surface elevation in the tank, failure of the dam is unlikely.

As the runoff volume for the watershed above the dam is significantly higher than the storage volume, the peak flow is likely to "break out" of the Flying E Wash channel at the west edge and proceed downstream along a completely different channel. The Flood Control District of Maricopa County requested that this channel, which for purposes of this study is called the George's Tank Breakout Channel, be evaluated using approximate methods to establish a Zone A floodplain.

Hydrologic routing through the tank indicated insignificant peak flow attenuation due to storage, so the base breakout flow is assumed the same as the George's Tank inflow. Breakout flows receive supplemental inflow from adjacent and downstream watersheds.

Normal depth was evaluated using data taken from the topographic mapping prepared for this study. Sections A through J were defined for HEC-2 input by taking cross section data from the map at regular intervals and critical locations as shown on floodplain maps. Slopes were estimated for each cross section by establishing midpoints between upstream and downstream sections, measuring distances and taking elevation changes from the contour information. In each model, the cross section is repeated several times using fields 7 and 9 to establish slope. From this, normal depth was calculated for each cross section.

Depths and topwidths were used to establish floodplain limits at cross sections.

BLACK & VEATCH
CONSULTING ENGINEERS
KANSAS CITY DALLAS DENVER ORLANDO

SUBJECT: Dickenbore ADMS FOD 89-9 Upper Flume Wash: Zone A Determination for Breakout Area W. of George's Tank
WORK: Review/Assess Hydrology/Prepare Cross Sections for Normal Depth Analysis HEC-2
PROJECT NO. 17676.400
FILE NO.
DATE 5/29/92 19
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George's Tank is at the center of the north line of Section 20, T7N R5W. As the dam at George's Tank is approximately 7 ft higher than the ground surface on the west side, the District has requested that the channel below the Breakout area be submitted to FEMA as a Zone A. Assumptions are as follows:

1. George's Tank is full, i.e. no peak attenuation is considered.

2. Flow from the adjacent watershed is added at the George's Tank outlet and at the tributary entering the wash near the large pecan tree west of Flume 6 (which is upstream of George's Tank). Peak flows may be added, as lag times are not appreciably different.

3. Flowrates (100-year) from the HEC-1 model are:

| | | |
|---|---|---|
| George's Tank inflow (SAB200) | = | 896 cfs |
| SAB195 above major trib | = | 213 cfs * |
| SAB195 below major trib | = | 690 cfs * |

The flowrates are assumed additive. $Q_{100}$ above the corral is approx. 1109 cfs; $Q_{100}$ below the corral is approx. 1586 cfs.
Sections A through G lie below the corral; H through J lie above it.

4. Cross sections and slopes for normal depth calculations taken from topographic maps prepared by McLain-Harbers Sheets 89, 98, 102 and 118 of 137.

5. Mannings 'n' values from review of aerial photographs and general values from the report on Mannings 'n' values [illegible] previously [illegible] study.

* From ratio of tributary area to entire area in SAB195. See attached sheet/map from Hydrology Report.

BLACK & VEATCH
CONSULTING ENGINEERS
KANSAS CITY DALLAS DENVER ORLANDO

SUBJECT Wakenburg ADMS FCD 5979 Upper Plum E. West Zone A Determination for Breakout W. of George's Tank
WORK Hydrology / Cross Sections for HEC-2 Analysis
PROJECT No. D626400
FILE No.

DATE 5/29/92 19
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A

GR 850, 2332 865, 2330, 880, 2329 910, 2326 990, 2324
GR 2323, 1000 2320, 1005 2326, 1015 2322, 1022, 2330, 1032

Slope $\frac{6}{440}$ = 1.4% = .014

CHECK
THROUGH
Capacity 4.1 cfs.

B GR 2344, 900 2342, 920 2340, 945 2332, 975 2336, 990
GR 2335.8, 1000 2336, 1010 2332, 1045 2340, 1075 2342, 1100

Slope = $\frac{14}{1500}$ = .009 = 0.9%

C GR 2362, 900 2360, 910 2358, 920 2356, 930 2354, 950
2354, 1100 2356, 1130 2358, 1180 2360, 1190 2362, 1210
2354, 990 2354, 010

Slope = $\frac{20}{1320}$ = .015 = 1.5%

D GR 2376, 720 2374, 800 2372, 850 2372, 1010, 2374, 1030
2376, 1040
2372, 990

Slope = $\frac{14}{830}$ = .017 = 1.7%

E GR 2382, 760 2386, 903 2384, 908 2382, 930 2382, 945
2382, 990 2381.8, 1000 2382, 1010 2382, 1030 2382 1050
2382, 1070 2382, 1100 2384, 1150 2386, 1170 2388, 1180

Slope = $\frac{10}{750}$ = .013 = 1.3%

P-GN-024-A

BLACK & VEATCH
CONSULTING ENGINEERS
KANSAS CITY DALLAS DENVER ORLANDO

SUBJECT: Wichita Bus ADMS FOD 89-79 Upper Flying E Wash Zone A Determination Breakout W of George's Tank
WORK: Hydrology / Cross Sections
PROJECT No. 17676.400
FILE No.
DATE 5/29/92 19
SET UP BY: TKM
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CHECKED BY:
PAGE No. OF

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F GR 2400, 740 2398, 770 2396, 800 2394, 950 2394, 990
2393.2, 1000 2394, 1020 2396, 1036 2398, 1040 2400, 1050

$$Slope = \frac{14}{1050} = .013 = 1.3\%$$

G GR 2412, 960 2410, 975 2408, 980 2406, 990 2405.5 1000
2406, 1015 2408, 1030 2410, 1260 2412, 1275

$$Slope = \frac{14}{870} = .016 = 1.6\%$$

H GR 2424, 950 2422, 975 2420, 985 2418, 990 2417.5, 1000
2418, 1010 ~~2418, 1025~~ 2418, 1090 2420, 1160 2422, 1180 2424, 1260

$$Slope = \frac{8}{940} = .009 = 0.9\%$$

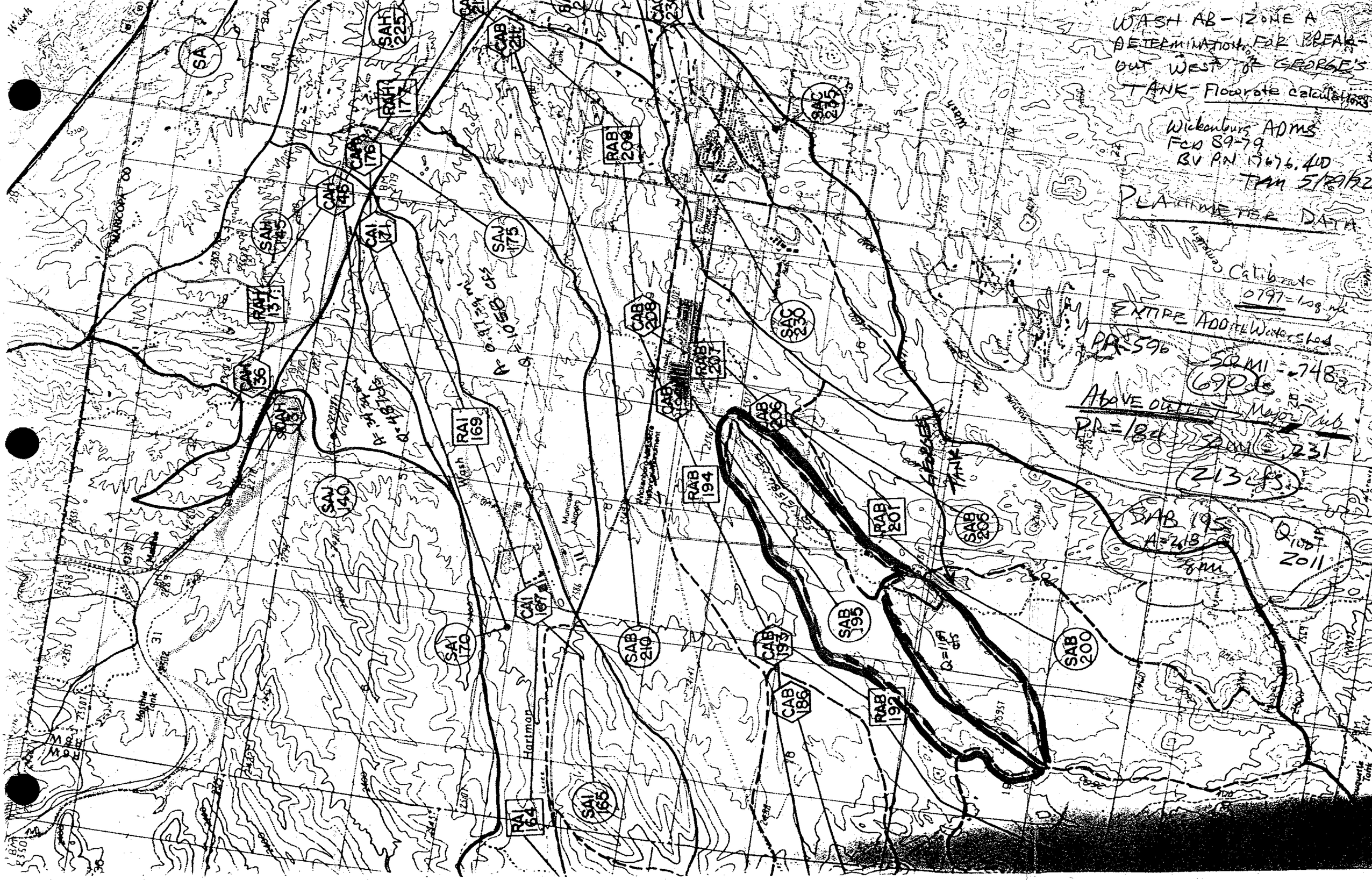
I GR 2436, 560 2434, 605 2432, 630 2430, 810 2428, 845
2426.5, 1000 2428, 1030 2430, 1040 2436, 1040
2427, 990 2427, 1010

$$Slope = \frac{12}{850} = .014 = 1.4\%$$

J GR 2448, 690 2446, 725 2444, 750 2444, 890 2442, 940
2441.8, 1000 2442, 1015 2444, 1020 2446, 1035 2448, 1050
2442, 995

$$Slope = \frac{10}{700} = .014 = 1.4\%$$

P-GN-024-A


WASH AB - ZONE A
DETERMINATION FOR BREAK-
OUT WEST OF GEORGE'S
TANK - Flowrate calculations
Wickenburg ADMS
FCD 89-79
BV PN 17676.4ID
TPM 5/20/92
PLANIMETER DATA
Calibrate
0797 = 1.08 mi
ENTIRE ADOTE Watershed
PA = 596
SQ MI = .748
(690 cfs)
ABOVE OUTLET
Major Trib
PA = 184
SQ MI = .231
(213 cfs)
SAB 195
A = 2.18
Q100 = 2011
Q = 1168 cfs
SAB 195
SAB 200
SAB 206
RAB 207
RAB 208
RAB 194
RAB 192
CAB 208
CAB 193
CAB 186
SAC 235
SAC 236
SAB 210
SAJ 175
SAJ 140
SAJ 170
SAI 165
RAI 164
CAI 167
RAI 169
SAH 225
CAB 216
RAH 174
CAB 176
CAI 146
CAI 121
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SAH 136
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| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>RIVERINE HYDRAULIC ANALYSIS FORM | O.M.B. Burden No 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
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Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: Wash AB: Holly Wash Tributary to Flying E Wash
*(One form for each flooding source)*

Project Name/Identifier: Wickenburg ADMS FCD 89-79

**1. REACH TO BE REVISED**

Downstream limit: Station Flying E Wash Confluence

Upstream limit: Station 1.873

**2. EFFECTIVE FIS**

☒ Not studied

☐ Studied by approximate methods

Downstream limit of study _____

Upstream limit of study _____

☐ Studied by detailed methods

Downstream limit of study _____

Upstream limit of study _____

☐ Floodway delineated

Downstream limit of Floodway _____

Upstream limit of Floodway _____

**3. HYDRAULIC ANALYSIS**

Why is the hydraulic analysis different from that used to develop the FIRM. *(Check all that apply)*

☒ Not studied in FIS

☒ Improved hydrologic data/analysis. Explain: Hydrologic Analysis procedures standardized by the Flood Control District of Maricopa County

☐ Improved hydraulic analysis. Explain: _____

☐ Flood control structure. Explain: _____

☐ Other. Explain: _____

Full input and output listings along with files on diskette *(if available)* for each of the models listed below and summary of the source of input parameters used in the models must be provided. The summary must include a complete description of any changes made from model to model *(e.g. duplicate effective model to corrected effective model)*. Only the Duplicate Effective and the Revised or Post-Project Conditions models must be submitted. See instructions for directions on when other models may be required. Only the 100-year flood profile is required for SFHAs with a Zone A designation. For areas which do not have detailed flooding, a hydraulic model is not required; however BFE's may not be added to the revised FIRM.

☐ Duplicate Effective Model — Natural ☐ Floodway ☐

Copies of the hydraulic analysis used in the effective FIS, referred to as the effective models *(10-, 50-, 100-, and 500-year multi-profile runs and the floodway run)* must be obtained and then reproduced on the requestor's equipment to produce the duplicate effective model. This is required to assure that the effective model input data has been transferred correctly to the requestor's equipment and to assure that the revised data will be integrated into the effective data to provide a continuous FIS model upstream and downstream of the revised reach.

☐ Corrected Effective Model — Natural ☐ Floodway ☐

The corrected effective model is the model that corrects any errors that occur in the duplicate effective model, adds any additional cross sections to the duplicate effective model, or incorporates more detailed topographic information than that used in the currently effective model. The corrected effective model must not reflect any man-made physical changes since the date of the effective model. An error could be a technical error in the modeling procedures, or any construction in the floodplain that occurred prior to the date of the effective model but was not incorporated into the effective model.

☐ Existing or Pre-Project Conditions Model — Natural ☐ Floodway ☐

The duplicate effective or corrected model is modified to produce the existing or pre-project conditions model to reflect any modifications that have occurred within the floodplain since the date of the effective model but prior to the construction of the project for which the revision is being requested. If no modification has occurred since the date of the effective model, then this model would be identical to the corrected effective or duplicate effective model.

☐ Revised or Post-Project Conditions Model — Natural ☐ Floodway ☐

The existing or pre-project conditions model *(or duplicate effective or corrected effective model, as appropriate)* is revised to reflect revised or post-project conditions. This model must incorporate any physical changes to the floodplain since the effective model was produced as well as the effects of the project. When the request is for proposed project this model should reflect proposed conditions.

☒ Other: Please attach a sheet describing all other models or calculations submitted. — Natural ☒ Floodway ☒

New Model
(Proposed Effective Model)

## 4. MODEL PARAMETERS *(from model used to revise 100-year water surface elevation)*

| Discharges: | Upstream Limit | Downstream Limit |
|---|---|---|
| 10-year | | |
| 50-year | | |
| 100-year | 1361 | 1361 |
| 500-year | | |

Attach diagram showing changes in 100-year discharge

2. Explain how the starting water surface elevations were determined Starting water surface elevation ~~determined by the Slope Area Method~~ taken from Flying E Wash section 3.454

3. Give range of friction loss coefficients (*Manning's "N"*) Channel ..... 0.030

Overbanks ..... 0.050

If friction loss coefficients are different anywhere along the revised reach from those used to develop the FIRM, give location, value used in the effective FIS, and revised values and an explanation as to how the revised values were determined.

| Location | FIS | Revised |
|---|---|---|
| NA | | |
| | | |
| | | |
| | | |

Explain:

4. Describe how the cross section geometry data were determined (*e.g., field survey, topographic map, taken from previous study*) and list cross sections that were added.

Data points for cross sections are based on the photogrammetric models for the topographic maps

5. Explain how reach lengths for channel and overbanks were determined:

All reach lengths were measured from floodplain work maps.

## 5. RESULTS (from model used to revise 100-year water surface elevations)

1. Do the results indicate:

a. Water surface elevations higher than end points of cross sections? ..... ☐ Yes ☒ No

b. Supercritical depth? ..... ☐ Yes ☒ No

c. Critical depth? ..... ☒ Yes ☐ No

d. Other unique situations ..... ☐ Yes ☒ No

(If yes, Special Problem Report attached)

If yes to any of the above, attach an explanation that discusses the situation and how it is presented on the profiles, tables, and maps.

2. What is the maximum change in energy gradient between cross-sections? ..... 12.38

Specify location ..... 0.954

3. What is the distance between the cross-sections in 2 above? ..... 530

Specify location ..... 0.954

4. What is the maximum distance between cross-sections? ..... 560

Specify location ..... .853, 1.767, 1.873

5. Floodway determination

a. What is the maximum surcharge allowed by the community or State? ..... 1 foot

b. What is the maximum surcharge for the revised conditions? ..... 0.4 foot

Specify location ..... 1.661

c. What is the maximum velocity? ..... 10.1 fps

Specify location ..... 0.559

Explain:

d. Are there any negeative surcharge values at any cross-section ☒ Yes ☐ No

If yes, the floodway may need to widen. If it is not widened, please explain and indicate the maximum negative surcharge.

The maximum negative surcharge is 0.1 ft at Section 1.473. This is a result of adjacent encroachment that increases velocity and lowers the water surface elevation at the section.

6. Is the discharge value used to determine the floodway anywhere different from that used to determine the natural 100-year flood elevations? ..... ☐ Yes ☒ No

If Yes, explain:

7. Do 100-year water surface elevations increase at any location? ..... ☐ Yes ☒ No

If yes, please attach a list of the locations where the increases occur, state whether or not the increases are located on the requestor's property, and provide an explanation of the reason for the increases.

NA- New Model

Please attach a completed comparison table entitled: Water Surface Elevation Check (See page 6)

## 6. REVISED FIRM/FBFM AND FLOOD PROFILES

A. The revised water surface elevations tie into those computed by the effective FIS Model (*10-, 50-, 100-, and 500-year*), downstream of the project at cross-section NA within _____ feet and upstream of the project at cross section _____ within _____ feet.

B. The revised floodway elevations tie into those computed by the effective FIS model, dowstream of the project at cross section NA within _____ feet and upstream of the project at cross section _____ within NA feet.

C. Attach profiles, at the same vertical and horizontal scale as the profiles in the effective FIS report, showing stream bed and profiles of all floods studied (without encroachment). Also, label all cross sections, road crossings (including low chord and top-of-road data), culverts, tributaries, corporate limits, and study limits. If channel distance has changed, the stationing should be revised for all profile sheets.

D. Attach a Floodway Data Table showing data for each cross section listed in the published Floodway Data Table in the FIS report.

Proceed to Riverine /Coastal Mapping Form

FEDERAL EMERGENCY MANAGMENT AGENCY

# WATER SURFACE ELEVATION CHECK

| COMMUNITY NAME | FLOODIND SOURCE | PROJECT NAME /IDENTIFIER |
|---|---|---|
| Unincorporated Maricopa County/ Town of Wickenburg | WASH AB: Holly Wash Trib to Flying E Wash | Wickenburg ADMS FCD 89-79 |

| | EFFECTIVE | | | DUPLICATE EFFECTIVE | | | CORRECTED EFFECTIVE | | | EXISTING/PRE-PROJECT | | | REVISED/PROJECT | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SECNO | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] |
| | | | | | | | | | | | | | | | |

COMMENTS: New Model - See following Floodway Data Table

1-100-year (natural) Water Surface Elevation 2-Encroachment (floodway) Water Surface Elevation 3-Surcharge Value

Include all cross sections in the models between tie-in points. Any interpolated values should be indicated in parentheses.

Sheet 1 of 1

FLOODWAY DATA, AB: UPPER FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| 2.435 | 144. | 701. | 9.9 | 2309.9 | 2309.9 | .0 |
| 2.539 | 549. | 844. | 8.2 | 2315.5 | 2315.5 | .0 |
| 2.630 | 137. | 453. | 4.8 | 2319.2 | 2319.2 | .0 |
| 2.725 | 244. | 281. | 7.7 | 2325.8 | 2325.8 | .0 |
| 2.812 | 434. | 517. | 4.2 | 2331.1 | 2331.1 | .0 |
| 2.922 | 352. | 427. | 5.0 | 2337.7 | 2337.7 | .0 |
| 3.005 | 480. | 497. | 4.3 | 2344.1 | 2344.1 | .0 |
| 3.047 | 228. | 396. | 5.4 | 2347.4 | 2347.4 | .0 |
| 3.113 | 73. | 245. | 8.8 | 2352.6 | 2352.6 | .0 |
| 3.200 | 240. | 383. | 5.6 | 2358.2 | 2358.2 | .0 |
| 3.261 | 274. | 580. | 3.7 | 2360.4 | 2360.4 | .0 |
| 3.308 | 302. | 435. | 4.9 | 2362.1 | 2362.1 | .0 |
| 3.355 | 413. | 503. | 4.3 | 2365.7 | 2365.7 | .0 |
| 3.454 | 596. | 425. | 5.1 | 2371.8 | 2371.8 | .0 |
| 3.549 | 351. | 275. | 3.3 | 2380.0 | 2380.0 | .0 |
| 3.643 | 332. | 238. | 3.8 | 2387.5 | 2387.5 | .0 |
| 3.740 | 280. | 255. | 3.5 | 2395.6 | 2395.6 | .0 |
| 3.838 | 383. | 263. | 3.4 | 2404.7 | 2404.7 | .0 |
| 3.950 | 92. | 160. | 5.6 | 2415.1 | 2415.1 | .0 |
| 3.980 | 83. | 148. | 6.1 | 2417.7 | 2417.7 | .0 |
| 4.032 | 97. | 151. | 5.9 | 2422.6 | 2422.6 | .0 |
| 4.103 | 151. | 198. | 4.5 | 2428.4 | 2428.4 | .0 |
| 4.168 | 189. | 209. | 4.3 | 2434.3 | 2434.3 | .0 |
| 4.213 | 168. | 330. | 2.7 | 2435.6 | 2435.6 | .0 |
| 4.301 | 171. | 189. | 4.7 | 2442.9 | 2442.9 | .0 |
| 4.384 | 106. | 162. | 5.5 | 2449.5 | 2449.5 | .0 |
| 4.493 | 324. | 254. | 3.5 | 2458.6 | 2458.6 | .0 |
| 4.594 | 539. | 207. | 4.3 | 2467.4 | 2467.4 | .0 |
| 4.688 | 221. | 227. | 3.9 | 2475.6 | 2475.6 | .0 |
| 4.787 | 396. | 252. | 3.6 | 2484.2 | 2484.2 | .0 |
| 4.881 | 374. | 197. | 4.6 | 2489.5 | 2489.5 | .0 |
| 5.014 | 130. | 179. | 5.0 | 2500.0 | 2500.0 | .0 |
| 5.082 | 282. | 257. | 3.5 | 2506.6 | 2506.6 | .0 |
| 5.175 | 295. | 194. | 4.6 | 2514.5 | 2514.5 | .0 |
| 5.279 | 173. | 192. | 4.7 | 2522.3 | 2522.3 | .0 |
| -3.454 | 596. | 425. | 5.1 | 2371.8 | 2371.8 | .0 |
| .198 | 106. | 232. | 5.9 | 2377.6 | 2377.5 | .1 |
| .291 | 89. | 199. | 6.9 | 2382.4 | 2382.4 | .0 |
| .387 | 53. | 159. | 8.6 | 2387.7 | 2387.7 | .0 |
| .482 | 85. | 205. | 6.6 | 2392.0 | 2392.0 | .0 |
| .559 | 44. | 135. | 10.1 | 2400.7 | 2400.7 | .0 |
| .607 | 55. | 163. | 8.4 | 2403.5 | 2403.5 | .0 |

Upper Flying E Wash

FLOODWAY DATA, AB: UPPER FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| .681 | 83. | 196. | 6.9 | 2406.9 | 2406.9 | .0 |
| .747 | 48. | 152. | 9.0 | 2411.1 | 2411.1 | .0 |
| .853 | 103. | 214. | 6.4 | 2420.8 | 2420.8 | .0 |
| .954 | 73. | 186. | 7.3 | 2433.0 | 2433.0 | .0 |
| 1.005 | 88. | 342. | 4.0 | 2435.0 | 2434.9 | .1 |
| 1.101 | 75. | 185. | 7.4 | 2438.7 | 2438.7 | .0 |
| 1.202 | 96. | 212. | 6.4 | 2449.6 | 2449.6 | .0 |
| 1.295 | 106. | 217. | 6.3 | 2455.6 | 2455.6 | .0 |
| 1.399 | 111. | 219. | 6.2 | 2464.0 | 2464.0 | .0 |
| 1.473 | 93. | 206. | 6.6 | 2469.4 | 2469.5 | -.1 |
| 1.576 | 100. | 195. | 7.0 | 2476.3 | 2476.0 | .3 |
| 1.615 | 65. | 174. | 7.8 | 2482.1 | 2481.9 | .2 |
| 1.661 | 131. | 282. | 4.8 | 2485.1 | 2484.7 | .4 |
| 1.767 | 90. | 204. | 6.7 | 2493.4 | 2493.2 | .2 |
| 1.873 | 155. | 291. | 4.7 | 2499.2 | 2498.9 | .3 |

EXPLANATORY NOTES FOR
FORM 4 SECTION 5 PARAGRAPH 1.C

This watercourse islocated in a mountainous area. It is common for this watercourse to flow in subcritical, supercritical, and transitional flow regimes. The subcritical profile has been used to delineate the 100 year floodplain and prepare maps, tables, etc.

Flat 39 93 99 101 10

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>RIVERINE HYDRAULIC ANALYSIS FORM | O.M.B. Burden No 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
|---|---|---|

## PUBLIC BURDEN DISCLOSURE NOTICE

lic reporting burden for this form is estimated to average 2.25 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing and reviewing the form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden, to: Information Collections Management, Federal Emergency Management Agency, 500 C Street, S.W., Washington, DC 20472; and to the Office of Management and Budget, Paperwork Reduction Project (3067-0148), Washington, DC 20503.

Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AB: YUCCA FLAT WASH TRIBUTARY TO FLYING E WASH
*(One form for each flooding source)*

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. REACH TO BE REVISED

Downstream limit: Station 0.000 (Flying E Wash Confluence)

Upstream limit: Station 2.965

### 2. EFFECTIVE FIS

☐ Not studied

☒ Studied by approximate methods

Downstream limit of study: Same

Upstream limit of study: Approximately 0.697

☐ Studied by detailed methods

Downstream limit of study: _____

Upstream limit of study: _____

☐ Floodway delineated

Downstream limit of Floodway: _____

Upstream limit of Floodway: _____

### 3. HYDRAULIC ANALYSIS

Why is the hydraulic analysis different from that used to develop the FIRM. *(Check all that apply)*

☐ Not studied in FIS

☒ Improved hydrologic data/analysis. Explain: Hydrologic Analysis procedures standardized by the Flood Control District of Maricopa County

☐ Improved hydraulic analysis. Explain: _____

☐ Flood control structure. Explain: _____

☐ Other. Explain: _____

Full input and output listings along with files on diskette *(if available)* for each of the models listed below and summary of the source of input parameters used in the models must be provided. The summary must include a complete description of any changes made from model to model *(e.g. duplicate effective model to corrected effective model)*. Only the Duplicate Effective and the Revised or Post-Project Conditions models must be submitted. See instructions for directions on when other models may be required. Only the 100-year flood profile is required for SFHAs with a Zone A designation. For areas which do not have detailed flooding, a hydraulic model is not required; however BFE's may not be added to the revised FIRM.

☐ Duplicate Effective Model — Natural ☐ Floodway ☐

Copies of the hydraulic analysis used in the effective FIS, referred to as the effective models *(10-, 50-, 100-, and 500-year multi-profile runs and the floodway run)* must be obtained and then reproduced on the requestor's equipment to produce the duplicate effective model. This is required to assure that the effective model input data has been transferred correctly to the requestor's equipment and to assure that the revised data will be integrated into the effective data to provide a continuous FIS model upstream and downstream of the revised reach.

☐ Corrected Effective Model — Natural ☐ Floodway ☐

The corrected effective model is the model that corrects any errors that occur in the duplicate effective model, adds any additional cross sections to the duplicate effective model, or incorporates more detailed topographic information than that used in the currently effective model. The corrected effective model must not reflect any man-made physical changes since the date of the effective model. An error could be a technical error in the modeling procedures, or any construction in the floodplain that occurred prior to the date of the effective model but was not incorporated into the effective model.

☐ Existing or Pre-Project Conditions Model — Natural ☐ Floodway ☐

The duplicate effective or corrected model is modified to produce the existing or pre-project conditions model to reflect any modifications that have occurred within the floodplain since the date of the effective model but prior to the construction of the project for which the revision is being requested. If no modification has occurred since the date of the effective model, then this model would be identical to the corrected effective or duplicate effective model.

☐ Revised or Post-Project Conditions Model — Natural ☐ Floodway ☐

The existing or pre-project conditions model *(or duplicate effective or corrected effective model, as appropriate)* is revised to reflect revised or post-project conditions. This model must incorporate any physical changes to the floodplain since the effective model was produced as well as the effects of the project. When the request is for proposed project this model should reflect proposed conditions.

☒ Other: Please attach a sheet describing all other models or calculations submitted. — Natural ☒ Floodway ☒

New Model
(Proposed Effective Model)

**4. MODEL PARAMETERS** *(from model used to revise 100-year water surface elevation)*

| Discharges: | Upstream Limit | Downstream Limit |
|---|---|---|
| 10-year | | |
| 50-year | | |
| 100-year | 2189 | 5152 |
| 500-year | | |

Attach diagram showing changes in 100-year discharge

2. Explain how the starting water surface elevations were determined Starting water surface elevation determined ~~by the Slope Area Method~~ from Flying E Wash analysis

3. Give range of friction loss coefficients (*Manning's "N"*) Channel .....

Overbanks .....

If friction loss coefficients are different anywhere along the revised reach from those used to develop the FIRM, give location, value used in the effective FIS, and revised values and an explanation as to how the revised values were determined.

| Location | FIS | Revised |
|---|---|---|
| NA | | |
| | | |
| | | |
| | | |

Explain:

4. Describe how the cross section geometry data were determined (*e.g., field survey, topographic map, taken from previous study*) and list cross sections that were added.

Data points for cross sections are based on the photogrammetric models for the topographic maps

5. Explain how reach lengths for channel and overbanks were determined:

All reach lengths were measured from floodplain work maps.

## 5. RESULTS (from model used to revise 100-year water surface elevations)

1. Do the results indicate:

a. Water surface elevations higher than end points of cross sections? ..... ☐ Yes ☒ No

b. Supercritical depth? ..... ☐ Yes ☒ No

c. Critical depth? ..... ☒ Yes ☐ No

d. Other unique situations ..... ☐ Yes ☒ No

(If yes, Special Problem Report attached)

If yes to any of the above, attach an explanation that discusses the situation and how it is presented on the profiles, tables, and maps.

2. What is the maximum change in energy gradient between cross-sections? ..... 8.72

Specify location ..... 0.578

3. What is the distance between the cross-sections in 2 above? ..... 530 ft

Specify location ..... 0.578

4. What is the maximum distance between cross-sections? ..... 680

Specify location ..... 1.367

5. Floodway determination

a. What is the maximum surcharge allowed by the community or State? ..... 1 foot

b. What is the maximum surcharge for the revised conditions? ..... 0.5 foot

Specify location ..... 0.390, 2.091

c. What is the maximum velocity? ..... 11.5 fps

Specify location ..... 1.070

Explain:

d. Are there any negeative surcharge values at any cross-section ☒ Yes ☐ No

If yes, the floodway may need to widen. If it is not widened, please explain and indicate the maximum negative surcharge.

The maximum negative surcharge is 0.2 ft at Section 1.646. This is a result of adjacent encroachment that increases velocity and lowers the water surface elevation at the section.

6. Is the discharge value used to determine the floodway anywhere different from that used to determine the natural 100-year flood elevations? ..... ☐ Yes ☒ No

If Yes, explain:

7. Do 100-year water surface elevations increase at any location? ..... ☐ Yes ☒ No

If yes, please attach a list of the locations where the increases occur, state whether or not the increases are located on the requestor's property, and provide an explanation of the reason for the increases.

NA- New Model

Please attach a completed comparison table entitled: Water Surface Elevation Check (See page 6)

## 6. REVISED FIRM/FBFM AND FLOOD PROFILES

A. The revised water surface elevations tie into those computed by the effective FIS Model *(10-, 50-, 100-, and 500-year)*, downstream of the project at cross-section NA within _____ feet and upstream of the project at cross section _____ within _____ feet.

B. The revised floodway elevations tie into those computed by the effective FIS model, dowstream of the project at cross section NA within _____ feet and upstream of the project at cross section _____ within NA feet.

C. Attach profiles, at the same vertical and horizontal scale as the profiles in the effective FIS report, showing stream bed and profiles of all floods studied (without encroachment). Also, label all cross sections, road crossings (including low chord and top-of-road data), culverts, tributaries, corporate limits, and study limits. If channel distance has changed, the stationing should be revised for all profile sheets.

D. Attach a Floodway Data Table showing data for each cross section listed in the published Floodway Data Table in the FIS report.

Proceed to Riverine /Coastal Mapping Form

FEDERAL EMERGENCY MANAGMENT AGENCY

# WATER SURFACE ELEVATION CHECK

COMMUNITY NAME: Unincorporated Maricopa County/ Town of Wickenburg

FLOODIND SOURCE: Yucca Flat Wash Tributary to Flying E Wash

PROJECT NAME /IDENTIFIER: Wickenburg ADMS FCD 89-79

| | EFFECTIVE | | | DUPLICATE EFFECTIVE | | | CORRECTED EFFECTIVE | | | EXISTING/PRE-PROJECT | | | REVISED/PROJECT | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SECNO | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] |
| | | | | | | | | | | | | | | | |

COMMENTS: New Model - See following Floodway Data Table

1-100-year (natural) Water Surface Elevation 2-Encroachment (floodway) Water Surface Elevation 3-Surcharge Value

Include all cross sections in the models between tie-in points. Any interpolated values should be indicated in parentheses.

Sheet 1 of 1

FLOODWAY DATA, AB: YUCCA FLAT WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| 2.435 | 144. | 701. | 9.9 | 2309.9 | 2309.9 | .0 |
| 2.539 | 549. | 844. | 8.2 | 2315.5 | 2315.5 | .0 |
| .191 | 533. | 873. | 5.9 | 2322.4 | 2322.4 | .0 |
| .290 | 389. | 746. | 6.9 | 2328.8 | 2328.8 | .0 |
| .390 | 379. | 849. | 6.1 | 2336.8 | 2336.3 | .5 |
| .477 | 390. | 716. | 7.2 | 2343.6 | 2343.3 | .3 |
| .578 | 341. | 843. | 6.1 | 2352.0 | 2351.8 | .2 |
| .697 | 213. | 684. | 7.5 | 2359.0 | 2358.8 | .2 |
| .788 | 174. | 625. | 8.2 | 2364.9 | 2364.9 | .0 |
| .883 | 94. | 472. | 10.9 | 2370.6 | 2370.7 | -.1 |
| .972 | 158. | 585. | 8.8 | 2375.5 | 2375.5 | .0 |
| 1.070 | 89. | 449. | 11.5 | 2381.8 | 2381.9 | -.1 |
| 1.163 | 130. | 662. | 7.8 | 2386.1 | 2385.7 | .4 |
| 1.239 | 129. | 549. | 9.4 | 2390.3 | 2390.4 | -.1 |
| 1.367 | 321. | 813. | 6.3 | 2394.9 | 2394.9 | .0 |
| 1.462 | 187. | 637. | 8.1 | 2401.3 | 2401.4 | -.1 |
| 1.551 | 144. | 542. | 9.5 | 2407.0 | 2406.9 | .1 |
| 1.646 | 163. | 599. | 8.6 | 2412.4 | 2412.6 | -.2 |
| 1.718 | 260. | 1114. | 4.6 | 2415.5 | 2415.4 | .1 |
| 1.808 | 328. | 431. | 4.8 | 2420.3 | 2420.3 | .0 |
| 1.905 | 245. | 405. | 5.1 | 2425.8 | 2425.8 | .0 |
| 2.003 | 268. | 430. | 4.8 | 2432.8 | 2432.8 | .0 |
| 2.091 | 215. | 385. | 5.4 | 2437.5 | 2437.0 | .5 |
| 2.172 | 219. | 394. | 5.3 | 2442.3 | 2442.0 | .3 |
| 2.284 | 196. | 376. | 5.5 | 2450.6 | 2450.6 | .0 |
| 2.384 | 199. | 376. | 5.5 | 2456.7 | 2456.7 | .0 |
| 2.477 | 397. | 460. | 4.5 | 2462.3 | 2462.3 | .0 |
| 2.562 | 278. | 350. | 5.9 | 2467.4 | 2467.4 | .0 |
| 2.672 | 220. | 357. | 5.8 | 2475.3 | 2475.3 | .0 |
| 2.761 | 279. | 403. | 5.2 | 2480.3 | 2480.3 | .0 |
| 2.857 | 356. | 459. | 4.5 | 2488.2 | 2488.2 | .0 |
| 2.965 | 331. | 408. | 5.1 | 2496.7 | 2496.7 | .0 |
| -1.718 | 260. | 1116. | 4.6 | 2415.5 | 2415.4 | .1 |
| .098 | 233. | 355. | 5.9 | 2418.8 | 2418.8 | .0 |
| .190 | 81. | 263. | 8.0 | 2423.9 | 2423.9 | .0 |
| .301 | 118. | 308. | 6.8 | 2431.5 | 2431.3 | .2 |
| .384 | 93. | 328. | 6.4 | 2434.5 | 2434.0 | .5 |
| .473 | 102. | 273. | 7.7 | 2440.9 | 2440.7 | .2 |
| .581 | 112. | 314. | 6.7 | 2448.6 | 2448.4 | .2 |
| .669 | 129. | 327. | 6.4 | 2452.7 | 2452.2 | .5 |
| .765 | 67. | 239. | 8.8 | 2458.4 | 2458.3 | .1 |
| .866 | 123. | 333. | 6.3 | 2463.2 | 2463.0 | .2 |

Yucca Flat Wash

Twin Springs Wash (Tributary)

EXPLANATORY NOTES FOR
FORM 4 SECTION 5 PARAGRAPH 1.C

This watercourse islocated in a mountainous area. It is common for this watercourse to flow in subcritical, supercritical, and transitional flow regimes. The subcritical profile has been used to delineate the 100 year floodplain and prepare maps, tables, etc.

| FEDERAL EMERGENCY MANAGEMENT AGENCY<br>**RIVERINE HYDRAULIC ANALYSIS FORM** | O.M.B. Burden No 3067-0148<br>Expires July 31, 1994 | FEMA USE ONLY |
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Community Name: Unincorporated Maricopa County / Town of Wickenburg

Flooding Source: WASH AB: TWIN PEAKS WASH TRIBUTARY TO YUCCA FLAT WASH
*(One form for each flooding source)*

Project Name/Identifier: Wickenburg ADMS FCD 89-79

### 1. REACH TO BE REVISED

Downstream limit: Station 0.000 (YUCCA FLAT WASH CONFLUENCE)

Upstream limit: Station 2.183

### 2. EFFECTIVE FIS

☒ Not studied

☐ Studied by approximate methods

Downstream limit of study _____

Upstream limit of study _____

☐ Studied by detailed methods

Downstream limit of study _____

Upstream limit of study _____

☐ Floodway delineated

Downstream limit of Floodway _____

Upstream limit of Floodway _____

### 3. HYDRAULIC ANALYSIS

Why is the hydraulic analysis different from that used to develop the FIRM. *(Check all that apply)*

☒ Not studied in FIS

☒ Improved hydrologic data/analysis. Explain: Hydrologic Analysis procedures standardized by the Flood Control District of Maricopa County

☐ Improved hydraulic analysis. Explain: _____

☐ Flood control structure. Explain: _____

☐ Other. Explain: _____

Full input and output listings along with files on diskette *(if available)* for each of the models listed below and summary of the source of input parameters used in the models must be provided. The summary must include a complete description of any changes made from model to model *(e.g. duplicate effective model to corrected effective model)*. Only the Duplicate Effective and the Revised or Post-Project Conditions models must be submitted. See instructions for directions on when other models may be required. Only the 100-year flood profile is required for SFHAs with a Zone A designation. For areas which do not have detailed flooding, a hydraulic model is not required; however BFE's may not be added to the revised FIRM.

| | Natural | Floodway |
|---|---|---|
| ☐ Duplicate Effective Model | ☐ | ☐ |

Copies of the hydraulic analysis used in the effective FIS, referred to as the effective models *(10-, 50-, 100-, and 500-year multi-profile runs and the floodway run)* must be obtained and then reproduced on the requestor's equipment to produce the duplicate effective model. This is required to assure that the effective model input data has been transferred correctly to the requestor's equipment and to assure that the revised data will be integrated into the effective data to provide a continuous FIS model upstream and downstream of the revised reach.

| | Natural | Floodway |
|---|---|---|
| ☐ Corrected Effective Model | ☐ | ☐ |

The corrected effective model is the model that corrects any errors that occur in the duplicate effective model, adds any additional cross sections to the duplicate effective model, or incorporates more detailed topographic information than that used in the currently effective model. The corrected effective model must not reflect any man-made physical changes since the date of the effective model. An error could be a technical error in the modeling procedures, or any construction in the floodplain that occurred prior to the date of the effective model but was not incorporated into the effective model.

| | Natural | Floodway |
|---|---|---|
| ☐ Existing or Pre-Project Conditions Model | ☐ | ☐ |

The duplicate effective or corrected model is modified to produce the existing or pre-project conditions model to reflect any modifications that have occurred within the floodplain since the date of the effective model but prior to the construction of the project for which the revision is being requested. If no modification has occurred since the date of the effective model, then this model would be identical to the corrected effective or duplicate effective model.

| | Natural | Floodway |
|---|---|---|
| ☐ Revised or Post-Project Conditions Model | ☐ | ☐ |

The existing or pre-project conditions model *(or duplicate effective or corrected effective model, as appropriate)* is revised to reflect revised or post-project conditions. This model must incorporate any physical changes to the floodplain since the effective model was produced as well as the effects of the project. When the request is for proposed project this model should reflect proposed conditions.

| | Natural | Floodway |
|---|---|---|
| ☒ Other: Please attach a sheet describing all other models or calculations submitted. | ☒ | ☒ |

New Model
(Proposed Effective Model)

## 4. MODEL PARAMETERS *(from model used to revise 100-year water surface elevation)*

| Discharges: | Upstream Limit | Downstream Limit |
|---|---|---|
| 10-year | | |
| 50-year | | |
| 100-year | 1650 | 2099 |
| 500-year | | |

Attach diagram showing changes in 100-year discharge

2. Explain how the starting water surface elevations were determined Starting water surface elevation ~~determined by the Slope Area Method~~ from YUCCA FLAT WASH analysis

3. Give range of friction loss coefficients (*Manning's "N"*) Channel ..... 0.030

Overbanks ..... 0.050

If friction loss coefficients are different anywhere along the revised reach from those used to develop the FIRM, give location, value used in the effective FIS, and revised values and an explanation as to how the revised values were determined.

| Location | FIS | Revised |
|---|---|---|
| NA | | |
| | | |
| | | |
| | | |

Explain:

4. Describe how the cross section geometry data were determined (*e.g., field survey, topographic map, taken from previous study*) and list cross sections that were added.

Data points for cross sections are based on the photogrammetric models for the topographic maps

5. Explain how reach lengths for channel and overbanks were determined:

All reach lengths were measured from floodplain work maps.

5. RESULTS (from model used to revise 100-year water surface elevations)

1. Do the results indicate:

a. Water surface elevations higher than end points of cross sections? ..... ☐ Yes ☒ No

b. Supercritical depth? ..... ☐ Yes ☒ No

c. Critical depth? ..... ☒ Yes ☐ No

d. Other unique situations ..... ☐ Yes ☒ No

(If yes, Special Problem Report attached)

If yes to any of the above, attach an explanation that discusses the situation and how it is presented on the profiles, tables, and maps.

2. What is the maximum change in energy gradient between cross-sections? ..... 9.26

Specify location ..... 1.343

3. What is the distance between the cross-sections in 2 above? ..... 530

Specify location ..... 1.343

4. What is the maximum distance between cross-sections? ..... 580

Specify location ..... 0.301

5. Floodway determination

a. What is the maximum surcharge allowed by the community or State? ..... 1 foot

b. What is the maximum surcharge for the revised conditions? ..... 0.5 foot

Specify location ..... 0.384

c. What is the maximum velocity? ..... 9.1 fps

Specify location ..... 1.802

Explain:

d. Are there any negeative surcharge values at any cross-section ☐ Yes ☒ No

If yes, the floodway may need to widen. If it is not widened, please explain and indicate the maximum negative surcharge.

6. Is the discharge value used to determine the floodway anywhere different from that used to determine the natural 100-year flood elevations? ..... ☐ Yes ☒ No

If Yes, explain:

7. Do 100-year water surface elevations increase at any location? ..... ☐ Yes ☒ No

If yes, please attach a list of the locations where the increases occur, state whether or not the increases are located on the requestor's property, and provide an explanation of the reason for the increases.

NA- New Model

Please attach a completed comparison table entitled: Water Surface Elevation Check (See page 6)

## 6. REVISED FIRM/FBFM AND FLOOD PROFILES

A. The revised water surface elevations tie into those computed by the effective FIS Model *(10-, 50-, 100-, and 500-year)*, downstream of the project at cross-section NA within _____ feet and upstream of the project at cross section _____ within _____ feet.

B. The revised floodway elevations tie into those computed by the effective FIS model, dowstream of the project at cross section NA within _____ feet and upstream of the project at cross section _____ within NA feet.

C. Attach profiles, at the same vertical and horizontal scale as the profiles in the effective FIS report, showing stream bed and profiles of all floods studied (without encroachment). Also, label all cross sections, road crossings (including low chord and top-of-road data), culverts, tributaries, corporate limits, and study limits. If channel distance has changed, the stationing should be revised for all profile sheets.

D. Attach a Floodway Data Table showing data for each cross section listed in the published Floodway Data Table in the FIS report.

Proceed to Riverine /Coastal Mapping Form

FEDERAL EMERGENCY MANAGMENT AGENCY

# WATER SURFACE ELEVATION CHECK

COMMUNITY NAME: Unincorporated Maricopa County/ Town of Wickenburg

FLOODIND SOURCE: WASH AB: TWIN PEAKS WASH TRIBUTARY TO YUCCA FLAT WASH

PROJECT NAME /IDENTIFIER: Wickenburg ADMS FCD 89-79

| | EFFECTIVE | | | DUPLICATE EFFECTIVE | | | CORRECTED EFFECTIVE | | | EXISTING/PRE-PROJECT | | | REVISED/PROJECT | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| SECNO | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] | NCWSEL[1] | FCWSEL[2] | SURC.[3] |
| | | | | | | | | | | | | | | | |

COMMENTS: New Model - See following Floodway Data Table

1-100-year (natural) Water Surface Elevation 2-Encroachment (floodway) Water Surface Elevation 3-Surcharge Value

Include all cross sections in the models between tie-in points. Any interpolated values should be indicated in parentheses.

Sheet 1 of 1

FLOODWAY DATA, AB: YUCCA FLAT WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| 2.435 | 144. | 701. | 9.9 | 2309.9 | 2309.9 | .0 |
| 2.539 | 549. | 844. | 8.2 | 2315.5 | 2315.5 | .0 |
| .191 | 533. | 873. | 5.9 | 2322.4 | 2322.4 | .0 |
| .290 | 389. | 746. | 6.9 | 2328.8 | 2328.8 | .0 |
| .390 | 379. | 849. | 6.1 | 2336.8 | 2336.3 | .5 |
| .477 | 390. | 716. | 7.2 | 2343.6 | 2343.3 | .3 |
| .578 | 341. | 843. | 6.1 | 2352.0 | 2351.8 | .2 |
| .697 | 213. | 684. | 7.5 | 2359.0 | 2358.8 | .2 |
| .788 | 174. | 625. | 8.2 | 2364.9 | 2364.9 | .0 |
| .883 | 94. | 472. | 10.9 | 2370.6 | 2370.7 | -.1 |
| .972 | 158. | 585. | 8.8 | 2375.5 | 2375.5 | .0 |
| 1.070 | 89. | 449. | 11.5 | 2381.8 | 2381.9 | -.1 |
| 1.163 | 130. | 662. | 7.8 | 2386.1 | 2385.7 | .4 |
| 1.239 | 129. | 549. | 9.4 | 2390.3 | 2390.4 | -.1 |
| 1.367 | 321. | 813. | 6.3 | 2394.9 | 2394.9 | .0 |
| 1.462 | 187. | 637. | 8.1 | 2401.3 | 2401.4 | -.1 |
| 1.551 | 144. | 542. | 9.5 | 2407.0 | 2406.9 | .1 |
| 1.646 | 163. | 599. | 8.6 | 2412.4 | 2412.6 | -.2 |
| 1.718 | 260. | 1114. | 4.6 | 2415.5 | 2415.4 | .1 |
| 1.808 | 328. | 431. | 4.8 | 2420.3 | 2420.3 | .0 |
| 1.905 | 245. | 405. | 5.1 | 2425.8 | 2425.8 | .0 |
| 2.003 | 268. | 430. | 4.8 | 2432.8 | 2432.8 | .0 |
| 2.091 | 215. | 385. | 5.4 | 2437.5 | 2437.0 | .5 |
| 2.172 | 219. | 394. | 5.3 | 2442.3 | 2442.0 | .3 |
| 2.284 | 196. | 376. | 5.5 | 2450.6 | 2450.6 | .0 |
| 2.384 | 199. | 376. | 5.5 | 2456.7 | 2456.7 | .0 |
| 2.477 | 397. | 460. | 4.5 | 2462.3 | 2462.3 | .0 |
| 2.562 | 278. | 350. | 5.9 | 2467.4 | 2467.4 | .0 |
| 2.672 | 220. | 357. | 5.8 | 2475.3 | 2475.3 | .0 |
| 2.761 | 279. | 403. | 5.2 | 2480.3 | 2480.3 | .0 |
| 2.857 | 356. | 459. | 4.5 | 2488.2 | 2488.2 | .0 |
| 2.965 | 331. | 408. | 5.1 | 2496.7 | 2496.7 | .0 |
| -1.718 | 260. | 1116. | 4.6 | 2415.5 | 2415.4 | .1 |
| .098 | 233. | 355. | 5.9 | 2418.8 | 2418.8 | .0 |
| .190 | 81. | 263. | 8.0 | 2423.9 | 2423.9 | .0 |
| .301 | 118. | 308. | 6.8 | 2431.5 | 2431.3 | .2 |
| .384 | 93. | 328. | 6.4 | 2434.5 | 2434.0 | .5 |
| .473 | 102. | 273. | 7.7 | 2440.9 | 2440.7 | .2 |
| .581 | 112. | 314. | 6.7 | 2448.6 | 2448.4 | .2 |
| .669 | 129. | 327. | 6.4 | 2452.7 | 2452.2 | .5 |
| .765 | 67. | 239. | 8.8 | 2458.4 | 2458.3 | .1 |
| .866 | 123. | 333. | 6.3 | 2463.2 | 2463.0 | .2 |

Twin Pass Wash (Trib. Thru)

FLOODWAY DATA, AB: YUCCA FLAT WASH
PROFILE NO. 2

TWIN PEAKS WASH (TRIBUTARY)

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| .949 | 74. | 245. | 8.6 | 2469.5 | 2469.4 | .1 |
| 1.045 | 170. | 361. | 5.8 | 2474.5 | 2474.5 | .0 |
| 1.148 | 77. | 244. | 8.6 | 2481.0 | 2481.0 | .0 |
| 1.242 | 114. | 293. | 7.2 | 2487.1 | 2487.1 | .0 |
| 1.343 | 70. | 237. | 8.9 | 2496.0 | 2496.0 | .0 |
| 1.428 | 91. | 271. | 7.7 | 2500.7 | 2500.7 | .0 |
| 1.525 | 97. | 280. | 7.5 | 2506.3 | 2506.3 | .0 |
| 1.619 | 92. | 269. | 7.8 | 2515.1 | 2515.1 | .0 |
| 1.719 | 102. | 280. | 7.5 | 2522.9 | 2522.9 | .0 |
| 1.802 | 68. | 230. | 9.1 | 2529.6 | 2529.6 | .0 |
| 1.897 | 93. | 228. | 7.2 | 2538.9 | 2538.9 | .0 |
| 1.993 | 122. | 246. | 6.7 | 2543.1 | 2543.1 | .0 |
| 2.094 | 86. | 224. | 7.4 | 2549.3 | 2549.3 | .0 |
| 2.183 | 61. | 192. | 8.6 | 2552.8 | 2552.8 | .0 |

EXPLANATORY NOTES FOR
FORM 4 SECTION 5 PARAGRAPH 1.C

This watercourse islocated in a mountainous area. It is common for this watercourse to flow in subcritical, supercritical, and transitional flow regimes. The subcritical profile has been used to delineate the 100 year floodplain and prepare maps, tables, etc.

```
*********************************************
*  HEC-2 WATER SURFACE PROFILES             *
*                                           *
*  Version   4.6.2;  May 1991               *
*                                           *
*  RUN DATE    15JUL92    TIME   14:58:54   *
*********************************************
```

```
*************************************
*  U.S. ARMY CORPS OF ENGINEERS     *
*  HYDROLOGIC ENGINEERING CENTER    *
*  609 SECOND STREET, SUITE D       *
*  DAVIS, CALIFORNIA 95616-4687     *
*         (916) 756-1104            *
*************************************
```

```
X     X  XXXXXXX   XXXXX              XXXXX
X     X  X        X     X            X     X
X     X  X        X                        X
XXXXXXX  XXXX     X         XXXXX    XXXXX
X     X  X        X                  X
X     X  X        X     X            X
X     X  XXXXXXX   XXXXX             XXXXXXX
```

THIS RUN EXECUTED 15JUL92 14:58:54

```
************************************
 HEC-2 WATER SURFACE PROFILES

 Version   4.6.2;  May 1991
************************************
```

SPLIT FLOW BEING PERFORMED

SF RIGHT BANK LEVEE US FROM AT&SF RAILROAD

JC ENERGY GRADE LINE USED TO DETERMINE WEIR FLOW
JP 1

TW RIGHT BANK LEVEE BETWEEN SECTIONS 0.134 & 0.160

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| WS | 17 | 0.134 | 0.160 | -1 | 2.8 | | | | | |
| WC | 0 | 2139.4 | 3.9 | 2138.9 | 7.8 | 2138.8 | 11.7 | 2138.7 | 15.6 | 2138.6 |
| WC | 19.5 | 2138.6 | 23.5 | 2138.4 | 27.4 | 2138.4 | 31.3 | 2138.3 | 35.2 | 2138.2 |
| [illegible] | [illegible]9.1 | 2138.1 | 43.0 | 2138.0 | 123.9 | 2138.0 | 127.9 | 2138.1 | 139.7 | 2138.1 |
| [illegible] | [illegible].7 | 2138.2 | 151.6 | 2138.2 | | | | | | |

TW RIGHT BANK LEVEE BETWEEN SECTIONS 0.160 & 0.220

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| WS | 57 | 0.160 | 0.220 | -1 | 2.8 | | | | | |
| WC | 0 | 2138.2 | 3.9 | 2138.3 | 15.7 | 2138.3 | 19.7 | 2138.4 | 31.5 | 2138.4 |
| WC | 35.5 | 2138.5 | 43.5 | 2138.5 | 47.5 | 2138.6 | 55.7 | 2138.6 | 59.7 | 2138.7 |
| WC | 67.9 | 2138.7 | 71.9 | 2138.8 | 80.1 | 2138.8 | 84.1 | 2138.9 | 92.3 | 2138.9 |
| WC | 96.3 | 2139.0 | 100.4 | 2139.0 | 104.4 | 2139.1 | 108.4 | 2139.1 | 112.4 | 2139.2 |
| WC | 116.4 | 2139.2 | 120.4 | 2139.3 | 124.4 | 2139.3 | 128.4 | 2139.4 | 132.4 | 2139.4 |
| WC | 136.4 | 2139.5 | 140.4 | 2139.6 | 144.4 | 2139.6 | 148.4 | 2139.7 | 152.4 | 2139.7 |
| WC | 156.4 | 2139.8 | 160.4 | 2139.8 | 164.4 | 2139.9 | 168.4 | 2139.9 | 172.4 | 2140.0 |
| WC | 176.4 | 2140.1 | 180.4 | 2140.3 | 184.4 | 2140.5 | 188.4 | 2140.6 | 192.4 | 2140.8 |
| WC | 196.4 | 2140.9 | 200.4 | 2141.1 | 204.4 | 2141.2 | 208.4 | 2141.4 | 212.4 | 2141.5 |
| WC | 216.4 | 2141.7 | 220.4 | 2141.9 | 224.4 | 2142.0 | 228.7 | 2142.1 | 232.9 | 2142.1 |
| WC | 237.2 | 2142.2 | 241.4 | 2142.3 | 245.7 | 2142.3 | 249.9 | 2142.4 | 254.2 | 2142.4 |
| WC | 258.4 | 2142.5 | 318.4 | 2142.3 | | | | | | |

```
      WICKENBURG ADMS: CONTRACT FCD 89-79
      BLACK & VEATCH PN 17676  COE & VAN LOO JN 1197-02
T3    WASH AB: FLYING E WASH            (FILE LFEW.DAT)

J1  ICHECK   INQ     NINV    IDIR    STRT    METRIC  HVINS   Q       WSEL    FQ

              2                                                    2134.50

J2  NPROF    IPLOT   PRFVS   XSECV   XSECH   FN      ALLDC   IBW     CHNIM   ITRACE

     1               -1                              -1                      15


J3  VARIABLE CODES FOR SUMMARY PRINTOUT

    150      200

NC   0.050    0.050   0.030     0.1     0.3
QT       2    7820.   7820.
ET                     9.1                                                  905.0   1026.31
            CONFLUENCE OF WASH AB: FLYING E WASH
            AND SOLS WASH BETWEEN CROSS-SECTIONS
                V (SOLS WASH RIVER MILE 1.97)
                W (SOLS WASH RIVER MILE 2.06)
            CROSS-SECTION DESIGNATION FROM
                SOLS WASH FLOODPLAIN DLINEATION
                HASSAYAMPA RIVER TO MARICOPA COUNTY LINE
                CELLA BARR ASSOCIATES

            SWSE DETERMINED BY SLOPE AREA METHOD

            SPLIT FLOW OPTION USED FROM XSECT 0.134 TO XSECT 0.220
            TO MODEL OVERFLOW LEVEE IN RIGHT OVERBANK.  THE PROGRAM
            WILL USE THE ENERGY GRADE LINE TO DETERMINE OVERFLOW.
X1   0.095      95    919.7   1011.0       0       0       0
GR  2140.0    842.0  2139.9    844.0  2139.7   846.0  2139.6   848.0  2139.4   850.0
GR  2139.3    852.0  2139.1    854.0  2139.0   856.0  2138.9   858.0  2138.7   860.0
GR  2138.6    862.0  2138.4    864.0  2138.3   866.0  2138.1   868.0  2138.0   870.0
GR  2137.8    872.0  2137.6    874.0  2137.4   876.0  2137.2   878.0  2137.0   880.0
GR  2136.8    882.0  2136.6    884.0  2136.4   886.0  2136.2   888.0  2136.0   890.0
GR  2135.8    892.0  2135.6    894.0  2135.4   896.0  2135.2   898.0  2135.0   900.0
GR  2134.8    902.0  2134.6    904.0  2134.4   906.0  2134.2   908.0  2134.0   910.0
GR  2133.9    911.9  2133.8    913.9  2133.7   915.8  2133.6   917.8  2132.0   919.7
GR  2131.8    921.7  2131.7    923.6  2131.5   925.6  2131.3   927.5  2131.2   929.4
GR  2131.1    931.4  2131.2    933.3  2131.3   935.3  2131.2   937.2  2131.3   939.2
GR  2131.2    941.1  2131.1    943.1  2131.0   945.0  2131.0   947.0  2131.1   949.0
GR  2131.2    953.0  2131.3    955.0  2131.2   961.0  2131.1   963.0  2131.2   967.0
GR  2131.2    969.0  2131.1    973.0  2131.2   975.0  2131.3   978.9  2131.2   980.8
GR  2131.1    982.8  2131.2    984.7  2131.3   988.5  2131.2   990.4  2131.1   992.3
GR  2131.1    994.3  2131.0    996.2  2131.0   998.1  2131.0  1000.0  2131.2  1001.8
GR  2131.3   1003.7  2131.5   1005.5  2131.7  1007.3  2131.8  1009.2  2132.0  1011.0
GR  2132.3   1013.0  2132.6   1015.0  2132.9  1017.0  2133.1  1019.0  2133.4  1021.0
GR  2133.7   1023.0  2134.0   1025.0  2134.8  1027.1  2135.5  1029.3  2136.3  1031.4
GR  2137.0   1033.5  2137.8   1035.6  2138.5  1037.8  2139.3  1039.9  2140.0  1042.0
```

```
N      0.050     0.050     0.030       0.3       0.5
ET                         9.1                                                  885.00    1012.87
X1     0.125        75     899.0    1011.0       130       160       160
GR    2140.5     860.0    2140.4     861.8    2140.3     863.7    2140.3     865.5    2140.2     867.3
GR    2140.1     869.2    2140.0     871.0    2139.5     873.3    2139.0     875.5    2138.5     877.8
GR    2138.0     880.0    2137.4     881.9    2136.8     883.8    2136.2     885.7    2136.1     887.6
GR    2136.0     889.5    2135.4     891.4    2134.8     893.3    2134.2     895.2    2134.1     897.1
GR    2134.0     899.0    2133.9     901.0    2133.8     903.0    2133.8     907.0    2133.8     909.0
GR    2133.7     915.0    2133.7     917.0    2133.6     921.0    2133.6     923.0    2133.5     927.0
GR    2133.5     929.0    2133.5     931.0    2133.6     932.9    2133.6     936.7    2133.7     938.6
GR    2133.8     940.5    2133.8     942.4    2133.9     944.3    2133.9     948.1    2134.0     950.0
GR    2134.0     966.0    2133.9     968.0    2133.9     970.0    2133.8     972.0    2133.8     974.0
GR    2133.7     976.0    2133.6     978.0    2133.6     980.0    2133.5     982.0    2133.5     984.0
GR    2133.4     986.0    2133.4     988.0    2133.3     990.0    2133.2     992.0    2133.2     994.0
GR    2133.1     996.0    2133.1     998.0    2133.0    1000.0    2133.1    1004.9    2133.2    1008.8
GR    2134.0    1011.0    2135.9    1012.3    2137.0    1013.5    2138.5    1019.8    2140.0    1028.0
GR    2140.1    1030.0    2140.1    1032.0    2140.1    1034.0    2140.2    1036.0    2140.3    1038.0
GR    2140.3    1040.0    2140.4    1042.0    2140.4    1044.0    2140.4    1046.0    2140.5    1048.0

            DS FACE: AT&SF RAILROAD BRIDGE (STRUCTURE AB-3)

                NOTE:  CENTERLINE SECTION OF AT&SF RAILROAD WAS
                       USED TO CREATE THE DS FACE CROSS-SECTION
X1     0.131        46       875.     1013.        30        30        30
X3        10                                                            2139.9    2139.4
GR    2141.5     230.0    2141.5     243.1    2141.4     256.1    2141.4     282.3    2141.3     295.4
GR    2141.3     308.5    2141.2     321.5    2141.2     334.6    2141.1     347.7    2141.1     373.9
GR    2141.0     386.9    2141.0     400.0    2140.9     412.9    2140.9     438.7    2140.8     451.6
GR    2140.8     464.5    2140.7     477.5    2140.7     490.4    2140.6     503.3    2140.6     529.1
GR    2140.5     542.0    2140.5     555.7    2140.4     569.3    2140.4     583.0    2140.3     596.7
GR    2140.3     624.0    2140.2     637.7    2140.2     651.3    2140.1     665.0    2140.1     678.7
GR    2140.0     692.3    2140.0     850.0    2139.9     863.6    2139.9     874.99   2133.6     875.0
GR    2133.6     890.9    2133.6     904.5    2133.6     918.2    2133.6     931.8    2133.6     945.5
GR    2133.6     959.1    2133.6     986.4    2133.6    1000.0    2133.6    1013.0    2139.4    1013.01
GR    2140.0    1043.0

SB       1.05       1.83       2.8         0       138         9       387         0    2133.7    2133.6
            US FACE: AT&SF RAILROAD BRIDGE (STRUCTURE AB-3)
                NOTE:  CENTERLINE SECTION OF AT&SF RAILROAD WAS
                       USED TO CREATE THE US FACE CROSS-SECTION
X1     0.134        46       875.     1013.      14.7      14.7      14.7
X2                           1     2136.7    2139.4
X3        10                                                            2139.9    2139.4
BT       -46     230.0    2141.5               243.1    2141.5               256.1    2141.4
BT               282.3    2141.4               295.4    2141.3               308.5    2141.3
BT               321.5    2141.2               334.6    2141.2               347.7    2141.1
BT               373.9    2141.1               386.9    2141.0               400.0    2141.0
BT               412.9    2140.9               438.7    2140.9               451.6    2140.8
BT               464.5    2140.8               477.5    2140.7               490.4    2140.7
BT               503.3    2140.6               529.1    2140.6               542.0    2140.5
                 555.7    2140.5               569.3    2140.4               583.0    2140.4
                 596.7    2140.3               624.0    2140.3               637.7    2140.2
BT               651.3    2140.2               665.0    2140.1               678.7    2140.1
```

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                692.3    2140.0              850.0    2140.0              863.6    2139.9
                874.99   2139.9              875.0    2139.9              890.9    2139.9
BT              904.5    2139.8              918.2    2139.8              931.8    2139.7
BT              945.5    2139.7              959.1    2139.6              986.4    2139.6
BT              1000.0   2139.5              1013.0   2139.4              1013.01  2139.4
BT              1043.0   2140.0
GR   2141.5     230.0    2141.5    243.1     2141.4   256.1     2141.4    282.3    2141.3    295.4
GR   2141.3     308.5    2141.2    321.5     2141.2   334.6     2141.1    347.7    2141.1    373.9
GR   2141.0     386.9    2141.0    400.0     2140.9   412.9     2140.9    438.7    2140.8    451.6
GR   2140.8     464.5    2140.7    477.5     2140.7   490.4     2140.6    503.3    2140.6    529.1
GR   2140.5     542.0    2140.5    555.7     2140.4   569.3     2140.4    583.0    2140.3    596.7
GR   2140.3     624.0    2140.2    637.7     2140.2   651.3     2140.1    665.0    2140.1    678.7
GR   2140.0     692.3    2140.0    850.0     2139.9   863.6     2139.9    874.99   2133.7    875.0
GR   2133.7     890.9    2133.7    904.5     2133.7   918.2     2133.7    931.8    2133.7    945.5
GR   2133.7     959.1    2133.7    986.4     2133.7   1000.0    2133.7    1013.0   2139.4    1013.01
GR   2140.0     1043.0

ET                9.1      9.1                                                    730.      1048
                ET RECORD:  STATION 730. MODEL 1 TO 1
                            FLOW CONTRACTION UPSTREAM
                            OF AT&SF BRIDGE

                ET RECORD:  STATION 1048. TOP OF OVERFLOW
                            LEVEE IN RIGHT OVERBANK
X1   0.160        95       941.8    1011.6    140      140       140
GR   2142.0     290.5    2141.5    296.3     2139.5   319.6     2139.0    325.4    2139.5    331.2
GR   2139.2     347.4    2138.7    374.5     2139.0   379.9     2139.0    385.6    2139.1    419.9
GR   2138.9     430.7    2137.9    473.8     2138.5   490.0     2138.5    500.5    2138.4    526.6
GR   2138.3     552.8    2138.2    579.0     2138.4   599.9     2138.2    610.8    2138.0    627.1
GR   2137.5     659.8    2137.3    676.1     2138.0   687.0     2137.8    697.5    2137.5    713.3
GR   2137.1     734.4    2137.0    739.6     2137.5   744.9     2137.6    750.3    2137.9    766.7
GR   2138.2     783.0    2138.0    788.5     2138.2   794.5     2139.0    818.5    2139.0    824.5
GR   2139.1     830.7    2139.5    855.3     2139.5   861.5     2139.1    872.6    2138.7    883.8
GR   2138.5     889.3    2138.5    894.9     2138.4   902.5     2138.0    910.1    2137.6    915.4
GR   2137.2     920.7    2136.8    926.0     2136.6   941.8     2136.2    947.1    2136.0    952.4
GR   2136.4     957.7    2136.6    968.3     2136.2   973.6     2136.1    978.8    2136.0    984.1
GR   2136.0     989.4    2136.0    994.7     2136.0   1000.0    2136.0    1005.8   2136.5    1011.6
GR   2137.2     1017.4   2137.6    1023.2    2137.9   1029.0    2138.0    1036.1   2138.1    1043.1
GR   2138.2     1048.0   2138.1    1058.1    2138.2   1066.0    2138.3    1071.4   2138.2    1076.9
GR   2138.3     1082.3   2138.4    1098.6    2138.5   1115.0    2138.5    1120.4   2138.7    1126.3
GR   2138.9     1132.1   2139.1    1143.9    2139.4   1155.6    2139.5    1161.5   2139.5    1167.0
GR   2139.4     1178.0   2139.4    1200.1    2139.5   1206.0    2139.6    1211.9   2139.9    1229.7
GR   2139.9     1248.5   2140.0    1254.9    2140.0   1261.4    2140.4    1266.6   2141.2    1277.1
GR   2142.4     1292.8   2143.6    1308.6    2144.4   1319.0    2144.8    1324.3   2142.0    1329.5

NC   0.050      0.050    0.030     0.1       0.3
QT       2      7820.    7820.
ET                5.1      9.1                360.     1092.50                     434.96    1092.50
                ET RECORD:  STATION 1092.5 TOP OF OVERFLOW
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LEVEE IN RIGHT OVERBANK

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 0.220 | 88 | 965.0 | 1030.0 | 295 | 320 | 315 | | | |
| GR | 2150.0 | 359.0 | 2149.3 | 366.0 | 2148.7 | 373.0 | 2148.0 | 380.0 | 2147.5 | 387.5 |
| GR | 2147.0 | 395.0 | 2146.5 | 402.5 | 2146.0 | 410.0 | 2145.3 | 417.0 | 2144.7 | 424.0 |
| GR | 2144.0 | 431.0 | 2143.5 | 439.5 | 2143.0 | 448.0 | 2142.5 | 456.5 | 2142.0 | 465.0 |
| GR | 2141.8 | 473.3 | 2141.7 | 481.7 | 2141.5 | 490.0 | 2141.4 | 498.3 | 2141.3 | 506.7 |
| GR | 2141.3 | 515.0 | 2141.2 | 523.3 | 2141.1 | 531.7 | 2141.0 | 540.0 | 2141.1 | 547.8 |
| GR | 2141.1 | 555.6 | 2141.2 | 563.4 | 2141.3 | 571.3 | 2141.3 | 579.1 | 2141.4 | 586.9 |
| GR | 2141.4 | 594.7 | 2141.5 | 602.5 | 2141.6 | 610.3 | 2141.6 | 618.1 | 2141.7 | 625.9 |
| GR | 2141.8 | 633.8 | 2141.8 | 641.6 | 2141.9 | 649.4 | 2141.9 | 657.2 | 2142.0 | 665.0 |
| GR | 2142.1 | 672.5 | 2142.2 | 680.0 | 2142.3 | 687.5 | 2142.3 | 695.0 | 2142.4 | 702.5 |
| GR | 2142.5 | 710.0 | 2142.5 | 832.0 | 2142.4 | 840.1 | 2142.4 | 848.3 | 2142.3 | 856.4 |
| GR | 2142.2 | 864.6 | 2142.1 | 872.7 | 2142.1 | 880.9 | 2142.0 | 889.0 | 2141.9 | 896.7 |
| GR | 2141.8 | 904.3 | 2141.8 | 912.0 | 2141.7 | 919.7 | 2141.6 | 927.3 | 2141.5 | 935.0 |
| GR | 2141.4 | 942.5 | 2141.3 | 950.0 | 2141.1 | 957.5 | 2141.0 | 965.0 | 2140.9 | 973.8 |
| GR | 2140.8 | 982.5 | 2140.6 | 991.3 | 2140.5 | 1000.0 | 2140.6 | 1007.5 | 2140.8 | 1015.0 |
| GR | 2140.9 | 1022.5 | 2141.0 | 1030.0 | 2141.5 | 1038.0 | 2142.0 | 1046.0 | 2142.0 | 1053.8 |
| GR | 2142.1 | 1061.5 | 2142.1 | 1069.3 | 2142.2 | 1077.0 | 2142.2 | 1084.8 | 2142.3 | 1092.5 |
| GR | 2142.3 | 1108.0 | 2142.4 | 1115.8 | 2142.4 | 1123.5 | 2142.5 | 1131.3 | 2142.5 | 1139.0 |
| GR | 2144.0 | 1142.0 | 2147.0 | 1151.5 | 2150.0 | 1161.0 | | | | |
| ET | | | 9.1 | | | | | | 570. | 1084.96 |
| X1 | 0.256 | 68 | 961.0 | 1000.0 | 200 | 200 | 190 | | | |
| GR | 2155.0 | 381.0 | 2154.0 | 392.0 | 2153.0 | 401.0 | 2152.0 | 410.0 | 2151.5 | 418.0 |
| GR | 2151.0 | 426.0 | 2150.5 | 434.0 | 2150.0 | 442.0 | 2149.0 | 450.5 | 2148.0 | 459.0 |
| GR | 2147.0 | 467.0 | 2146.0 | 475.0 | 2145.8 | 483.5 | 2145.5 | 492.0 | 2145.4 | 500.4 |
| GR | 2145.4 | 508.8 | 2145.3 | 517.1 | 2145.3 | 525.5 | 2145.2 | 533.9 | 2145.1 | 542.3 |
| GR | 2145.1 | 550.6 | 2145.0 | 559.0 | 2145.0 | 790.2 | 2145.1 | 798.3 | 2145.1 | 806.5 |
| GR | 2145.2 | 814.7 | 2145.2 | 822.8 | 2145.3 | 831.0 | 2145.3 | 847.3 | 2145.4 | 855.5 |
| GR | 2145.4 | 863.7 | 2145.5 | 871.8 | 2145.5 | 880.0 | 2145.4 | 887.8 | 2145.3 | 895.6 |
| GR | 2145.2 | 903.4 | 2145.1 | 911.2 | 2145.0 | 919.0 | 2145.0 | 942.0 | 2144.0 | 953.0 |
| GR | 2143.0 | 961.0 | 2143.0 | 1000.0 | 2144.0 | 1010.0 | 2146.0 | 1019.0 | 2145.5 | 1025.5 |
| GR | 2145.0 | 1032.0 | 2145.2 | 1039.8 | 2145.4 | 1047.6 | 2145.6 | 1055.4 | 2145.8 | 1063.2 |
| GR | 2146.0 | 1071.0 | 2146.7 | 1078.3 | 2147.3 | 1085.7 | 2148.0 | 1093.0 | 2148.3 | 1100.8 |
| GR | 2148.5 | 1108.5 | 2148.8 | 1116.3 | 2149.0 | 1124.0 | 2149.3 | 1131.8 | 2149.5 | 1139.5 |
| GR | 2149.8 | 1147.3 | 2150.0 | 1155.0 | 2151.0 | 1164.0 | 2152.0 | 1173.0 | 2153.0 | 1182.0 |
| GR | 2154.0 | 1191.0 | 2155.0 | 1200.0 | 2156.0 | 1209.0 | | | | |
| ET | | | 9.1 | | | | | | 800. | 1110. |
| X1 | 0.351 | 47 | 917.0 | 1000.0 | 470 | 505 | 500 | | | |
| GR | 2162.0 | 680.0 | 2161.3 | 686.7 | 2160.7 | 693.3 | 2160.0 | 700.0 | 2158.9 | 706.1 |
| GR | 2157.7 | 712.3 | 2156.6 | 718.4 | 2155.4 | 724.6 | 2154.3 | 730.7 | 2153.1 | 736.9 |
| GR | 2152.0 | 743.0 | 2150.0 | 750.0 | 2150.0 | 804.0 | 2150.1 | 809.6 | 2150.3 | 815.3 |
| GR | 2150.4 | 820.9 | 2150.5 | 826.5 | 2150.6 | 832.1 | 2150.8 | 837.8 | 2150.9 | 843.4 |
| GR | 2151.0 | 849.0 | 2151.0 | 904.0 | 2150.5 | 909.5 | 2150.0 | 915.0 | 2149.0 | 917.0 |
| GR | 2149.0 | 1000.0 | 2150.0 | 1004.0 | 2152.0 | 1010.0 | 2151.9 | 1015.5 | 2151.8 | 1021.0 |
| GR | 2151.8 | 1026.5 | 2151.7 | 1032.0 | 2151.6 | 1037.5 | 2151.5 | 1043.0 | 2151.5 | 1200.0 |
| GR | 2152.0 | 1204.0 | 2156.0 | 1211.5 | 2160.0 | 1219.0 | 2160.7 | 1224.3 | 2161.3 | 1229.7 |
| GR | 2162.0 | 1235.0 | 2162.3 | 1241.2 | 2162.7 | 1247.3 | 2163.0 | 1253.5 | 2163.3 | 1259.7 |
| GR | 2163.7 | 1265.8 | 2164.0 | 1272.0 | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 973.55 | 1183. |
| X1 | 0.460 | 70 | 982.3 | 1016.3 | 580 | 590 | 575 | | | |
| GR | 2169.0 | 961.0 | 2156.0 | 982.3 | 2155.9 | 985.8 | 2155.8 | 988.4 | 2155.7 | 991.9 |
| GR | 2155.6 | 994.5 | 2155.5 | 1000.0 | 2155.6 | 1008.2 | 2156.0 | 1016.3 | 2156.2 | 1022.5 |
| GR | 2156.4 | 1028.7 | 2157.0 | 1034.9 | 2157.1 | 1040.4 | 2157.2 | 1046.0 | 2157.3 | 1051.5 |
| GR | 2157.4 | 1057.1 | 2157.5 | 1062.6 | 2157.6 | 1068.1 | 2157.7 | 1073.7 | 2157.5 | 1079.2 |
| GR | 2157.4 | 1085.0 | 2157.3 | 1090.7 | 2157.2 | 1096.5 | 2157.1 | 1102.2 | 2157.0 | 1108.0 |
| GR | 2156.9 | 1113.7 | 2156.8 | 1119.5 | 2156.7 | 1125.2 | 2157.0 | 1131.0 | 2157.1 | 1139.5 |
| GR | 2157.5 | 1148.0 | 2157.7 | 1155.0 | 2157.9 | 1162.0 | 2158.5 | 1169.0 | 2158.8 | 1175.8 |
| GR | 2159.1 | 1182.7 | 2160.0 | 1189.5 | 2160.2 | 1195.1 | 2160.4 | 1200.7 | 2160.6 | 1206.3 |
| GR | 2160.8 | 1211.9 | 2161.0 | 1217.4 | 2161.2 | 1223.1 | 2161.4 | 1228.6 | 2161.6 | 1234.2 |
| GR | 2161.8 | 1239.8 | 2162.0 | 1245.4 | 2161.0 | 1251.0 | 2161.1 | 1256.3 | 2161.2 | 1261.6 |
| GR | 2161.3 | 1266.9 | 2161.4 | 1272.2 | 2161.5 | 1277.4 | 2161.6 | 1282.8 | 2161.7 | 1288.0 |
| GR | 2161.8 | 1293.3 | 2161.9 | 1298.6 | 2162.0 | 1303.9 | 2161.5 | 1309.2 | 2161.6 | 1314.9 |
| GR | 2161.7 | 1320.6 | 2161.7 | 1326.3 | 2161.8 | 1332.1 | 2161.9 | 1337.8 | 2161.9 | 1353.5 |
| GR | 2163.7 | 1359.7 | 2165.5 | 1365.8 | 2167.4 | 1372.0 | 2169.2 | 1378.1 | 2171.0 | 1384.3 |
| ET | | | 9.1 | | | | | | 822.80 | 1082. |
| X1 | 0.540 | 35 | 966.6 | 1000.0 | 390 | 295 | 425 | | | |
| GR | 2172.0 | 805.5 | 2171.9 | 806.5 | 2171.0 | 810.2 | 2166.1 | 821.8 | 2164.0 | 841.5 |
| GR | 2163.9 | 857.0 | 2163.0 | 872.5 | 2162.9 | 883.5 | 2162.8 | 894.6 | 2162.7 | 905.7 |
| GR | 2162.0 | 916.7 | 2162.0 | 928.2 | 2162.1 | 939.6 | 2162.1 | 944.4 | 2162.1 | 955.5 |
| GR | 2162.2 | 966.6 | 2162.2 | 977.8 | 2162.2 | 988.9 | 2162.4 | 1000.0 | 2162.5 | 1010.3 |
| GR | 2162.6 | 1020.6 | 2162.7 | 1030.8 | 2162.8 | 1041.1 | 2163.4 | 1051.4 | 2163.4 | 1066.7 |
| [illegible] | 2163.5 | 1082.0 | 2163.6 | 1092.7 | 2163.6 | 1103.4 | 2163.7 | 1114.2 | 2164.0 | 1124.9 |
| [illegible] | 2164.7 | 1140.6 | 2170.0 | 1156.2 | 2171.1 | 1168.0 | 2172.2 | 1179.7 | 2180.0 | 1191.5 |
| ET | | | 9.1 | | | | | | 717.46 | 1028.94 |
| X1 | 0.576 | 78 | 958.3 | 1000.0 | 200 | 165 | 190 | | | |
| GR | 2176.0 | 621.2 | 2174.5 | 630.5 | 2174.3 | 636.3 | 2174.1 | 642.2 | 2173.9 | 648.0 |
| GR | 2173.7 | 653.8 | 2173.5 | 659.6 | 2173.3 | 665.5 | 2173.5 | 671.3 | 2172.7 | 677.0 |
| GR | 2171.9 | 682.7 | 2171.1 | 688.4 | 2170.3 | 694.1 | 2169.7 | 699.8 | 2169.5 | 705.5 |
| GR | 2169.5 | 711.2 | 2169.2 | 717.5 | 2168.9 | 723.9 | 2168.5 | 730.3 | 2167.9 | 736.6 |
| GR | 2167.6 | 742.1 | 2167.3 | 747.6 | 2167.1 | 753.0 | 2166.8 | 758.5 | 2166.5 | 764.0 |
| GR | 2166.5 | 769.5 | 2166.6 | 775.0 | 2166.7 | 780.5 | 2166.8 | 786.0 | 2166.9 | 791.5 |
| GR | 2167.0 | 797.0 | 2167.1 | 802.5 | 2167.2 | 808.0 | 2167.3 | 813.5 | 2167.4 | 819.0 |
| GR | 2167.0 | 824.5 | 2166.8 | 830.0 | 2166.6 | 835.6 | 2166.4 | 841.2 | 2166.2 | 846.7 |
| GR | 2166.0 | 852.3 | 2165.8 | 857.8 | 2165.6 | 863.3 | 2165.4 | 868.9 | 2165.2 | 874.5 |
| GR | 2166.0 | 880.0 | 2165.9 | 885.6 | 2165.8 | 891.1 | 2165.7 | 896.7 | 2165.6 | 902.3 |
| GR | 2165.5 | 907.8 | 2165.4 | 913.4 | 2165.3 | 918.9 | 2165.5 | 924.5 | 2165.4 | 930.1 |
| GR | 2165.3 | 935.8 | 2165.2 | 941.4 | 2165.1 | 947.0 | 2165.0 | 952.6 | 2164.9 | 958.3 |
| GR | 2164.8 | 963.9 | 2165.0 | 969.5 | 2165.0 | 975.6 | 2165.0 | 981.7 | 2164.9 | 987.8 |
| GR | 2164.9 | 993.9 | 2164.9 | 1000.0 | 2165.1 | 1006.1 | 2165.3 | 1012.2 | 2165.6 | 1018.2 |
| GR | 2166.0 | 1024.3 | 2170.0 | 1030.1 | 2174.0 | 1035.8 | 2178.0 | 1041.6 | 2182.0 | 1047.4 |
| GR | 2186.0 | 1053.2 | 2190.0 | 1058.9 | 2186.0 | 1064.7 | | | | |
| ET | | | 9.1 | | | | | | 690.53 | 1121.64 |
| X1 | 0.640 | 65 | 991.1 | 1020.9 | 350 | 340 | 340 | | | |
| GR | 2181.0 | 650.5 | 2177.0 | 664.9 | 2177.0 | 668.0 | 2175.8 | 679.2 | 2174.0 | 691.7 |
| GR | 2173.9 | 701.6 | 2173.7 | 711.5 | 2174.2 | 719.9 | 2174.2 | 728.2 | 2174.1 | 736.6 |
| [illegible] | 2174.0 | 743.5 | 2173.8 | 750.3 | 2173.8 | 757.2 | 2174.2 | 764.1 | 2174.3 | 770.9 |
| [illegible] | 2174.0 | 777.8 | 2174.5 | 784.6 | 2174.3 | 791.3 | 2174.1 | 798.1 | 2174.0 | 801.9 |
| GR | 2173.8 | 812.2 | 2172.5 | 819.5 | 2172.3 | 826.9 | 2172.1 | 834.2 | 2171.9 | 846.5 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2171.6 | 850.4 | 2171.0 | 859.3 | 2171.2 | 866.8 | 2171.3 | 874.2 | 2171.5 | 881.7 |
| | 2171.0 | 889.1 | 2171.0 | 896.4 | 2171.0 | 903.8 | 2171.9 | 911.1 | 2171.9 | 918.2 |
| GR | 2171.9 | 925.3 | 2171.9 | 932.3 | 2172.0 | 939.4 | 2171.6 | 947.0 | 2169.5 | 954.5 |
| GR | 2169.6 | 963.8 | 2170.0 | 973.2 | 2169.9 | 982.1 | 2169.8 | 991.1 | 2169.5 | 1000.0 |
| GR | 2169.6 | 1007.0 | 2169.7 | 1013.9 | 2169.8 | 1020.9 | 2169.8 | 1027.9 | 2169.9 | 1034.8 |
| GR | 2170.0 | 1041.8 | 2170.2 | 1048.5 | 2170.3 | 1055.2 | 2170.5 | 1061.9 | 2170.7 | 1068.6 |
| GR | 2171.0 | 1075.3 | 2171.1 | 1081.8 | 2171.2 | 1088.4 | 2171.3 | 1094.9 | 2171.3 | 1101.4 |
| GR | 2171.4 | 1108.0 | 2171.5 | 1114.5 | 2174.6 | 1122.8 | 2177.7 | 1131.2 | 2190.0 | 1139.5 |
| ET | | | 9.1 | | | | | | 746.02 | 1196.82 |
| X1 | 0.707 | 79 | 980.0 | 1010.0 | 320 | 365 | 350 | | | |
| GR | 2190.0 | 590.0 | 2189.0 | 600.0 | 2188.0 | 610.0 | 2187.0 | 620.0 | 2186.3 | 630.3 |
| GR | 2185.5 | 640.5 | 2184.8 | 650.8 | 2184.0 | 661.0 | 2183.6 | 671.3 | 2183.3 | 681.5 |
| GR | 2182.9 | 691.8 | 2182.5 | 702.0 | 2182.3 | 711.6 | 2182.1 | 721.3 | 2181.9 | 730.9 |
| GR | 2181.8 | 740.5 | 2181.6 | 750.1 | 2181.4 | 759.8 | 2181.2 | 769.4 | 2181.0 | 779.0 |
| GR | 2180.9 | 788.5 | 2180.8 | 798.0 | 2180.6 | 807.5 | 2180.5 | 817.0 | 2180.4 | 826.5 |
| GR | 2180.3 | 836.0 | 2180.1 | 845.5 | 2180.0 | 855.0 | 2179.7 | 864.5 | 2179.3 | 874.0 |
| GR | 2179.0 | 883.5 | 2178.7 | 893.0 | 2178.3 | 902.5 | 2178.0 | 912.0 | 2177.7 | 921.6 |
| GR | 2177.4 | 931.2 | 2177.1 | 940.8 | 2176.8 | 950.4 | 2176.5 | 960.0 | 2176.4 | 970.0 |
| GR | 2176.3 | 980.0 | 2176.1 | 990.0 | 2176.0 | 1000.0 | 2176.3 | 1010.0 | 2176.5 | 1020.0 |
| GR | 2177.4 | 1029.5 | 2178.3 | 1039.0 | 2179.1 | 1048.5 | 2180.0 | 1058.0 | 2180.0 | 1066.8 |
| GR | 2180.0 | 1075.5 | 2180.0 | 1084.3 | 2180.0 | 1093.0 | 2180.0 | 1101.0 | 2180.0 | 1109.0 |
| GR | 2180.0 | 1119.7 | 2180.0 | 1130.3 | 2180.0 | 1141.0 | 2180.0 | 1151.7 | 2180.0 | 1162.3 |
| GR | 2180.0 | 1173.0 | 2180.7 | 1182.3 | 2181.3 | 1191.7 | 2182.0 | 1201.0 | 2182.7 | 1210.3 |
| GR | 2183.3 | 1219.7 | 2184.0 | 1229.0 | 2184.0 | 1239.3 | 2184.0 | 1249.5 | 2184.0 | 1259.8 |
| GR | 2184.0 | 1270.0 | 2184.7 | 1280.0 | 2185.3 | 1290.0 | 2186.0 | 1300.0 | 2188.0 | 1310.0 |
| | 2190.0 | 1320.0 | 2192.0 | 1330.0 | 2196.0 | 1340.0 | 2200.0 | 1350.0 | | |
| ET | | | 9.1 | | | | | | 952.26 | 1393.86 |
| X1 | 0.801 | 87 | 967.0 | 1002.0 | 460 | 540 | 500 | | | |
| GR | 2208.0 | 812.0 | 2206.0 | 821.5 | 2204.0 | 831.0 | 2202.0 | 840.5 | 2200.0 | 850.0 |
| GR | 2199.3 | 860.3 | 2198.7 | 870.7 | 2198.0 | 881.0 | 2197.6 | 889.8 | 2197.3 | 898.5 |
| GR | 2196.9 | 907.3 | 2196.5 | 916.0 | 2196.0 | 930.0 | 2195.3 | 931.9 | 2194.5 | 933.8 |
| GR | 2193.8 | 935.6 | 2193.0 | 937.5 | 2192.3 | 939.4 | 2191.5 | 941.3 | 2190.8 | 943.1 |
| GR | 2190.0 | 945.0 | 2189.3 | 947.0 | 2188.7 | 949.0 | 2188.0 | 951.0 | 2187.3 | 953.0 |
| GR | 2186.7 | 955.0 | 2186.0 | 957.0 | 2185.3 | 959.0 | 2184.7 | 961.0 | 2184.0 | 963.0 |
| GR | 2183.3 | 965.0 | 2182.7 | 967.0 | 2182.0 | 969.0 | 2181.9 | 971.0 | 2181.9 | 973.0 |
| GR | 2181.8 | 975.0 | 2181.7 | 977.0 | 2181.6 | 979.0 | 2181.6 | 981.0 | 2181.5 | 983.0 |
| GR | 2181.3 | 985.0 | 2181.0 | 987.0 | 2180.8 | 989.0 | 2180.5 | 991.0 | 2180.3 | 993.0 |
| GR | 2180.0 | 995.0 | 2180.5 | 997.5 | 2181.0 | 1000.0 | 2182.5 | 1002.0 | 2184.0 | 1004.0 |
| GR | 2184.1 | 1006.0 | 2184.1 | 1008.0 | 2184.2 | 1010.0 | 2184.3 | 1012.0 | 2184.3 | 1014.0 |
| GR | 2184.4 | 1016.0 | 2184.4 | 1018.0 | 2184.5 | 1020.0 | 2184.5 | 1022.0 | 2184.5 | 1024.0 |
| GR | 2184.5 | 1026.0 | 2184.5 | 1028.0 | 2184.5 | 1030.0 | 2184.5 | 1032.0 | 2184.5 | 1034.0 |
| GR | 2184.5 | 1036.0 | 2184.5 | 1038.0 | 2184.5 | 1040.0 | 2184.8 | 1060.5 | 2185.0 | 1081.0 |
| GR | 2185.0 | 1101.3 | 2185.0 | 1121.7 | 2185.0 | 1142.0 | 2185.3 | 1165.5 | 2185.5 | 1189.0 |
| GR | 2185.5 | 1210.0 | 2185.3 | 1229.7 | 2185.2 | 1249.3 | 2185.0 | 1269.0 | 2185.0 | 1290.5 |
| GR | 2185.0 | 1312.0 | 2184.8 | 1331.3 | 2184.7 | 1350.7 | 2184.5 | 1370.0 | 2183.5 | 1382.0 |
| GR | 2190.0 | 1401.0 | 2198.0 | 1430.0 | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 818.44 | 1300.60 |
| X1 | 0.898 | 79 | 986.5 | 1013.3 | 470 | 480 | 510 | | | |
| GR | 2204.0 | 748.0 | 2202.0 | 760.0 | 2200.0 | 772.0 | 2198.7 | 783.0 | 2197.3 | 794.0 |
| GR | 2196.0 | 805.0 | 2194.0 | 817.5 | 2192.0 | 830.0 | 2191.0 | 840.0 | 2191.5 | 850.0 |
| GR | 2192.0 | 854.0 | 2192.0 | 862.7 | 2192.0 | 871.3 | 2192.0 | 880.0 | 2192.2 | 890.0 |
| GR | 2192.3 | 900.0 | 2192.5 | 910.0 | 2192.4 | 915.0 | 2192.4 | 920.0 | 2192.3 | 925.0 |
| GR | 2192.3 | 930.0 | 2192.2 | 935.0 | 2192.2 | 940.0 | 2192.1 | 945.0 | 2192.1 | 950.0 |
| GR | 2192.0 | 955.0 | 2192.0 | 960.2 | 2192.0 | 965.4 | 2192.0 | 970.6 | 2192.0 | 975.8 |
| GR | 2192.0 | 981.0 | 2191.8 | 986.5 | 2191.5 | 992.0 | 2191.5 | 996.0 | 2191.5 | 1000.0 |
| GR | 2191.5 | 1004.0 | 2191.7 | 1008.7 | 2191.8 | 1013.3 | 2192.0 | 1018.0 | 2192.1 | 1026.8 |
| GR | 2192.3 | 1035.5 | 2192.4 | 1044.3 | 2192.5 | 1053.0 | 2192.3 | 1062.7 | 2192.2 | 1072.3 |
| GR | 2192.0 | 1082.0 | 2192.2 | 1090.7 | 2192.3 | 1099.3 | 2192.5 | 1108.0 | 2192.3 | 1118.7 |
| GR | 2192.2 | 1129.3 | 2192.0 | 1140.0 | 2191.8 | 1149.2 | 2191.7 | 1158.3 | 2191.5 | 1167.5 |
| GR | 2191.3 | 1176.7 | 2191.2 | 1185.8 | 2191.0 | 1195.0 | 2191.0 | 1203.8 | 2191.0 | 1212.5 |
| GR | 2191.0 | 1221.3 | 2191.0 | 1230.0 | 2190.8 | 1241.0 | 2190.5 | 1252.0 | 2190.3 | 1263.0 |
| GR | 2190.0 | 1274.0 | 2191.0 | 1283.0 | 2192.0 | 1292.0 | 2194.0 | 1301.3 | 2196.0 | 1310.7 |
| GR | 2198.0 | 1320.0 | 2199.0 | 1328.0 | 2200.0 | 1336.0 | 2201.2 | 1346.8 | 2202.3 | 1357.7 |
| GR | 2203.5 | 1368.5 | 2204.7 | 1379.3 | 2205.8 | 1390.2 | 2207.0 | 1401.0 | | |
| ET | | | 9.1 | | | | | | 907.60 | 1347.88 |
| X1 | 0.938 | 91 | 986.0 | 1011.0 | 195 | 235 | 210 | | | |
| GR | 2210.0 | 872.0 | 2206.7 | 881.3 | 2203.3 | 890.7 | 2200.0 | 900.0 | 2197.5 | 910.0 |
| GR | 2195.0 | 920.0 | 2195.0 | 942.1 | 2194.9 | 944.2 | 2194.9 | 946.3 | 2194.8 | 948.3 |
| GR | 2194.8 | 952.5 | 2194.7 | 954.6 | 2194.7 | 956.7 | 2194.6 | 958.8 | 2194.6 | 960.8 |
| GR | 2194.5 | 962.9 | 2194.5 | 965.0 | 2194.4 | 967.1 | 2194.4 | 971.3 | 2194.3 | 973.4 |
| [illegible] | 2194.3 | 975.5 | 2194.2 | 977.6 | 2194.1 | 979.7 | 2194.1 | 983.9 | 2194.0 | 986.0 |
| [illegible] | 2193.8 | 988.0 | 2193.8 | 990.0 | 2193.6 | 992.0 | 2193.6 | 998.0 | 2193.5 | 1000.0 |
| GR | 2193.6 | 1001.8 | 2193.7 | 1003.7 | 2193.8 | 1005.5 | 2193.8 | 1007.3 | 2193.9 | 1009.2 |
| GR | 2194.0 | 1011.0 | 2194.1 | 1013.1 | 2194.3 | 1015.3 | 2194.4 | 1017.4 | 2194.5 | 1019.5 |
| GR | 2194.6 | 1021.6 | 2194.8 | 1023.8 | 2194.9 | 1025.9 | 2195.0 | 1028.0 | 2195.1 | 1030.0 |
| GR | 2195.2 | 1032.0 | 2195.3 | 1034.0 | 2195.4 | 1036.0 | 2195.4 | 1038.0 | 2195.6 | 1040.0 |
| GR | 2195.6 | 1042.0 | 2195.7 | 1044.0 | 2195.8 | 1046.0 | 2195.9 | 1048.0 | 2196.0 | 1050.0 |
| GR | 2196.0 | 1052.0 | 2196.1 | 1054.0 | 2196.1 | 1056.0 | 2196.2 | 1058.0 | 2196.2 | 1062.0 |
| GR | 2196.3 | 1064.0 | 2196.3 | 1066.0 | 2196.4 | 1068.0 | 2196.4 | 1072.0 | 2196.5 | 1074.0 |
| GR | 2196.5 | 1076.0 | 2196.6 | 1078.0 | 2196.6 | 1082.0 | 2196.7 | 1084.0 | 2196.7 | 1086.0 |
| GR | 2196.8 | 1088.0 | 2196.8 | 1092.0 | 2196.9 | 1094.0 | 2196.9 | 1096.0 | 2197.0 | 1098.0 |
| GR | 2197.0 | 1100.0 | 2196.8 | 1118.3 | 2196.5 | 1136.5 | 2196.3 | 1154.8 | 2196.0 | 1173.0 |
| GR | 2196.0 | 1192.5 | 2196.0 | 1212.0 | 2195.0 | 1220.0 | 2195.1 | 1241.6 | 2195.2 | 1263.2 |
| GR | 2195.3 | 1284.8 | 2195.4 | 1306.4 | 2195.5 | 1328.0 | 2196.0 | 1340.0 | 2200.0 | 1355.0 |
| GR | 2210.0 | 1370.0 | | | | | | | | |
| ET | | | 9.1 | | | | | | 902.50 | 1485.97 |
| X1 | 1.012 | 74 | 987.0 | 1009.0 | 380 | 420 | 390 | | | |
| GR | 2214.0 | 870.0 | 2210.0 | 885.0 | 2208.7 | 889.3 | 2207.3 | 893.7 | 2206.0 | 898.0 |
| GR | 2204.0 | 902.7 | 2202.0 | 907.3 | 2200.0 | 912.0 | 2200.2 | 917.0 | 2200.3 | 922.0 |
| GR | 2200.5 | 927.0 | 2200.7 | 932.0 | 2200.8 | 937.0 | 2201.0 | 942.0 | 2201.1 | 946.8 |
| GR | 2201.3 | 951.5 | 2201.4 | 956.3 | 2201.5 | 961.0 | 2201.5 | 966.3 | 2201.5 | 971.7 |
| GR | 2201.5 | 977.0 | 2201.3 | 982.0 | 2201.2 | 987.0 | 2201.0 | 992.0 | 2200.5 | 996.0 |
| GR | 2200.0 | 1000.0 | 2201.0 | 1004.0 | 2201.2 | 1009.0 | 2201.3 | 1014.0 | 2201.5 | 1019.0 |
| GR | 2201.8 | 1024.5 | 2202.0 | 1030.0 | 2202.1 | 1035.3 | 2202.3 | 1040.5 | 2202.4 | 1045.8 |
| [illegible] | 2202.5 | 1051.0 | 2202.3 | 1057.0 | 2202.0 | 1063.0 | 2202.2 | 1068.7 | 2202.3 | 1074.3 |
| [illegible] | 2202.5 | 1080.0 | 2202.5 | 1084.8 | 2202.5 | 1089.6 | 2202.5 | 1094.4 | 2202.5 | 1099.2 |
| GR | 2202.5 | 1104.0 | 2202.5 | 1108.8 | 2202.5 | 1113.6 | 2202.5 | 1118.4 | 2202.5 | 1123.2 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2202.5 | 1128.0 | 2202.5 | 1150.5 | 2202.5 | 1173.0 | 2202.3 | 1190.3 | 2202.2 | 1207.7 |
| | 2202.0 | 1225.0 | 2201.8 | 1243.3 | 2201.7 | 1261.7 | 2201.5 | 1280.0 | 2201.3 | 1297.5 |
| GR | 2201.0 | 1315.0 | 2201.5 | 1332.0 | 2202.0 | 1349.0 | 2202.5 | 1372.0 | 2203.0 | 1395.0 |
| GR | 2203.3 | 1413.3 | 2203.5 | 1431.5 | 2203.8 | 1449.8 | 2204.0 | 1468.0 | 2204.0 | 1485.0 |
| GR | 2206.0 | 1507.5 | 2208.0 | 1530.0 | 2210.0 | 1549.0 | 2210.0 | 1565.0 | | |
| ET | | | 9.1 | | | | | | 569.59 | 1022.12 |
| X1 | 1.112 | 76 | 977.0 | 1009.0 | 465 | 540 | 530 | | | |
| GR | 2220.0 | 555.0 | 2210.0 | 571.0 | 2205.5 | 592.0 | 2206.0 | 605.0 | 2206.5 | 629.0 |
| GR | 2207.0 | 653.0 | 2207.3 | 675.5 | 2207.5 | 698.0 | 2208.0 | 718.0 | 2208.5 | 738.0 |
| GR | 2209.0 | 756.7 | 2209.5 | 775.3 | 2210.0 | 794.0 | 2210.1 | 813.0 | 2210.3 | 832.0 |
| GR | 2210.4 | 851.0 | 2210.5 | 870.0 | 2210.3 | 890.3 | 2210.2 | 910.7 | 2210.0 | 931.0 |
| GR | 2209.9 | 932.9 | 2209.8 | 934.9 | 2209.7 | 936.8 | 2209.6 | 938.8 | 2209.5 | 940.7 |
| GR | 2209.4 | 942.6 | 2209.3 | 944.6 | 2209.3 | 946.5 | 2209.2 | 948.4 | 2209.1 | 950.4 |
| GR | 2209.0 | 952.3 | 2208.9 | 954.3 | 2208.8 | 956.2 | 2208.7 | 958.1 | 2208.6 | 960.1 |
| GR | 2208.5 | 962.0 | 2208.4 | 963.9 | 2208.3 | 965.8 | 2208.1 | 967.6 | 2208.0 | 969.5 |
| GR | 2207.9 | 971.4 | 2207.8 | 973.3 | 2207.6 | 975.1 | 2207.5 | 977.0 | 2207.4 | 978.9 |
| GR | 2207.4 | 980.8 | 2207.3 | 982.6 | 2207.3 | 984.5 | 2207.2 | 986.4 | 2207.1 | 988.3 |
| GR | 2207.1 | 990.1 | 2207.0 | 992.0 | 2207.0 | 994.0 | 2207.0 | 996.0 | 2207.0 | 998.0 |
| GR | 2207.0 | 1000.0 | 2207.1 | 1002.3 | 2207.3 | 1004.5 | 2207.4 | 1006.8 | 2207.5 | 1009.0 |
| GR | 2207.9 | 1010.8 | 2208.3 | 1012.7 | 2208.8 | 1014.5 | 2209.2 | 1016.3 | 2209.6 | 1018.2 |
| GR | 2210.0 | 1020.0 | 2210.8 | 1021.9 | 2211.5 | 1023.8 | 2212.3 | 1025.6 | 2213.0 | 1027.5 |
| GR | 2213.8 | 1029.4 | 2214.5 | 1031.3 | 2215.3 | 1033.1 | 2216.0 | 1035.0 | 2218.0 | 1042.5 |
| GR | 2220.0 | 1050.0 | | | | | | | | |
| ET | | 7.1 | 9.1 | | | | 620. | 1442. | 659.36 | 1326.11 |
| | | ET RECORD: STA 620. ELIMINATE INEFFECTIVE | | | | | | | | |
| | | | FLOW AREA IN LEFT OVERBANK | | | | | | | |
| X1 | 1.180 | 86 | 980.0 | 1005.0 | 330 | 365 | 360 | | | |
| GR | 2226.0 | 200.0 | 2223.0 | 215.0 | 2221.5 | 230.5 | 2220.0 | 246.0 | 2219.3 | 266.3 |
| GR | 2218.7 | 286.7 | 2218.0 | 307.0 | 2217.0 | 328.0 | 2216.0 | 349.0 | 2215.5 | 370.0 |
| GR | 2215.3 | 390.7 | 2215.2 | 411.3 | 2215.0 | 432.0 | 2214.8 | 454.7 | 2214.7 | 477.3 |
| GR | 2214.5 | 500.0 | 2214.8 | 520.7 | 2215.2 | 541.3 | 2215.5 | 562.0 | 2218.0 | 583.0 |
| GR | 2222.0 | 595.0 | 2226.0 | 620.0 | 2222.0 | 640.0 | 2218.0 | 655.0 | 2214.0 | 670.0 |
| GR | 2212.0 | 685.0 | 2214.0 | 708.0 | 2214.5 | 722.0 | 2213.5 | 750.0 | 2214.5 | 775.0 |
| GR | 2214.8 | 793.3 | 2215.2 | 811.7 | 2215.5 | 830.0 | 2216.5 | 850.0 | 2216.3 | 865.0 |
| GR | 2216.0 | 880.0 | 2216.5 | 900.0 | 2216.0 | 910.0 | 2214.0 | 930.0 | 2215.5 | 950.0 |
| GR | 2216.0 | 970.0 | 2213.5 | 980.0 | 2213.5 | 992.0 | 2213.0 | 1000.0 | 2213.5 | 1005.0 |
| GR | 2214.0 | 1018.0 | 2214.5 | 1034.0 | 2215.0 | 1050.0 | 2215.5 | 1065.0 | 2216.0 | 1080.0 |
| GR | 2216.3 | 1090.0 | 2216.7 | 1100.0 | 2217.0 | 1110.0 | 2216.5 | 1120.0 | 2216.0 | 1130.0 |
| GR | 2216.0 | 1140.0 | 2216.0 | 1150.0 | 2216.0 | 1160.0 | 2216.0 | 1170.0 | 2215.2 | 1180.0 |
| GR | 2214.3 | 1190.0 | 2213.5 | 1200.0 | 2213.5 | 1210.0 | 2213.5 | 1220.0 | 2213.8 | 1229.0 |
| GR | 2214.0 | 1238.0 | 2215.3 | 1249.0 | 2216.5 | 1260.0 | 2216.0 | 1270.0 | 2215.5 | 1280.0 |
| GR | 2216.0 | 1291.0 | 2216.5 | 1302.0 | 2216.7 | 1313.0 | 2216.8 | 1324.0 | 2217.0 | 1335.0 |
| GR | 2217.1 | 1343.8 | 2217.3 | 1352.5 | 2217.4 | 1361.3 | 2217.5 | 1370.0 | 2218.3 | 1380.0 |
| GR | 2219.2 | 1390.0 | 2220.0 | 1400.0 | 2222.5 | 1410.5 | 2225.0 | 1421.0 | 2227.5 | 1431.5 |
| GR | 2230.0 | 1442.0 | | | | | | | | |
| ET | | | 9.1 | | | | | | 791.27 | 1306.35 |

VULTURE MINE ROAD

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 1.280 | 17 | 980 | 1020 | 570 | 480 | 525 | | | |
| GR | 2234 | 520 | 2232 | 575 | 2230.4 | 645 | 2230 | 695 | 2228 | 748 |
| GR | 2226 | 795 | 2224 | 865 | 2223 | 980 | 2223 | 1000 | 2223 | 1020 |
| GR | 2223.3 | 1090 | 2224 | 1190 | 2226 | 1300 | 2228 | 1380 | 2230 | 1430 |
| GR | 2232 | 1492 | 2234 | 1570 | | | | | | |
| | | | | | | | | | | |
| ET | | | 9.1 | | | | | | 869.70 | 1351.53 |
| X1 | 1.353 | 77 | 976.7 | 1018.0 | 365 | 400 | 390 | | | |
| GR | 2250.0 | 825.0 | 2247.3 | 831.3 | 2244.5 | 837.5 | 2241.8 | 843.8 | 2239.0 | 850.0 |
| GR | 2237.1 | 856.8 | 2235.3 | 863.5 | 2233.4 | 870.3 | 2231.5 | 877.0 | 2231.6 | 882.8 |
| GR | 2231.8 | 888.5 | 2231.9 | 894.3 | 2232.0 | 900.0 | 2231.8 | 905.7 | 2231.6 | 911.4 |
| GR | 2231.4 | 917.1 | 2231.1 | 922.9 | 2230.9 | 928.6 | 2230.7 | 934.3 | 2230.5 | 940.0 |
| GR | 2230.5 | 965.0 | 2230.4 | 970.8 | 2230.3 | 976.7 | 2230.3 | 982.5 | 2230.2 | 988.3 |
| GR | 2230.1 | 994.2 | 2230.0 | 1000.0 | 2230.1 | 1006.0 | 2230.2 | 1012.0 | 2230.3 | 1018.0 |
| GR | 2230.4 | 1024.0 | 2230.5 | 1030.0 | 2230.6 | 1035.6 | 2230.7 | 1041.2 | 2230.8 | 1046.8 |
| GR | 2230.9 | 1052.4 | 2231.0 | 1058.0 | 2231.1 | 1063.8 | 2231.1 | 1069.6 | 2231.2 | 1075.3 |
| GR | 2231.2 | 1081.1 | 2231.3 | 1086.9 | 2231.3 | 1092.7 | 2231.4 | 1098.4 | 2231.4 | 1104.2 |
| GR | 2231.5 | 1110.0 | 2231.5 | 1231.1 | 2231.4 | 1237.3 | 2231.4 | 1249.6 | 2231.3 | 1255.7 |
| GR | 2231.3 | 1268.0 | 2231.2 | 1274.1 | 2231.2 | 1280.3 | 2231.1 | 1286.4 | 2231.1 | 1298.7 |
| GR | 2231.0 | 1304.9 | 2231.0 | 1311.0 | 2231.4 | 1317.1 | 2231.8 | 1323.2 | 2232.1 | 1329.2 |
| GR | 2232.5 | 1335.3 | 2232.9 | 1341.4 | 2233.3 | 1347.5 | 2233.7 | 1353.5 | 2234.1 | 1359.6 |
| GR | 2234.5 | 1365.7 | 2234.9 | 1371.8 | 2235.2 | 1377.8 | 2235.6 | 1383.9 | 2236.0 | 1390.0 |
| GR | 2236.8 | 1395.5 | 2237.5 | 1401.0 | 2238.3 | 1406.5 | 2239.0 | 1412.0 | 2242.0 | 1418.3 |
| GR | 2245.0 | 1424.7 | 2248.0 | 1431.0 | | | | | | |
| | | | | | | | | | | |
| | | | 9.1 | | | | | | 914.10 | 1322.97 |
| X1 | 1.441 | 83 | 981.0 | 1012.0 | 435 | 470 | 460 | | | |
| GR | 2260.0 | 855.0 | 2257.5 | 861.0 | 2255.0 | 867.0 | 2252.5 | 873.0 | 2250.0 | 879.0 |
| GR | 2248.4 | 884.6 | 2246.9 | 890.1 | 2245.3 | 895.7 | 2243.7 | 901.3 | 2242.1 | 906.9 |
| GR | 2240.6 | 912.4 | 2239.0 | 918.0 | 2237.8 | 924.0 | 2236.5 | 930.0 | 2236.5 | 981.0 |
| GR | 2236.3 | 987.3 | 2236.2 | 993.7 | 2236.0 | 1000.0 | 2236.3 | 1006.0 | 2236.5 | 1012.0 |
| GR | 2236.5 | 1041.0 | 2236.6 | 1046.4 | 2236.6 | 1051.9 | 2236.7 | 1057.3 | 2236.7 | 1062.8 |
| GR | 2236.8 | 1068.2 | 2236.8 | 1073.7 | 2236.9 | 1079.1 | 2236.9 | 1084.6 | 2237.0 | 1090.0 |
| GR | 2236.9 | 1095.0 | 2236.8 | 1100.0 | 2236.7 | 1105.0 | 2236.6 | 1110.0 | 2236.5 | 1115.0 |
| GR | 2236.8 | 1121.3 | 2237.2 | 1127.7 | 2237.5 | 1134.0 | 2237.6 | 1139.8 | 2237.6 | 1145.5 |
| GR | 2237.7 | 1151.3 | 2237.8 | 1157.0 | 2237.8 | 1162.8 | 2237.9 | 1168.5 | 2237.9 | 1174.3 |
| GR | 2238.0 | 1180.0 | 2238.1 | 1185.5 | 2238.1 | 1190.9 | 2238.2 | 1196.4 | 2238.3 | 1201.8 |
| GR | 2238.4 | 1207.3 | 2238.5 | 1212.8 | 2238.5 | 1218.2 | 2238.6 | 1223.7 | 2238.7 | 1229.2 |
| GR | 2238.8 | 1234.6 | 2238.9 | 1240.1 | 2238.9 | 1245.5 | 2239.0 | 1251.0 | 2239.1 | 1256.4 |
| GR | 2239.1 | 1261.7 | 2239.1 | 1267.1 | 2239.2 | 1272.4 | 2239.2 | 1277.8 | 2239.3 | 1283.2 |
| GR | 2239.3 | 1288.6 | 2239.4 | 1293.9 | 2239.4 | 1304.6 | 2239.5 | 1310.0 | 2239.8 | 1316.0 |
| GR | 2240.0 | 1322.0 | 2240.7 | 1328.0 | 2241.3 | 1334.0 | 2242.0 | 1340.0 | 2243.6 | 1346.0 |
| GR | 2245.2 | 1352.0 | 2246.8 | 1358.0 | 2248.4 | 1364.0 | 2250.0 | 1370.0 | 2250.3 | 1375.0 |
| GR | 2250.5 | 1380.0 | 2250.8 | 1385.0 | 2251.0 | 1390.0 | | | | |
| | | | | | | | | | | |
| ET | | | 9.1 | | | | | | 619.32 | 1094. |
| X1 | 1.545 | 73 | 975.0 | 1019.0 | 605 | 445 | 550 | | | |
| GR | 2260.0 | 585.0 | 2256.7 | 593.7 | 2253.3 | 602.3 | 2250.0 | 611.0 | 2246.5 | 620.0 |
| GR | 2244.5 | 644.0 | 2244.0 | 655.0 | 2244.0 | 663.0 | 2244.0 | 671.0 | 2244.3 | 681.0 |
| GR | 2244.7 | 691.0 | 2245.0 | 701.0 | 2244.5 | 713.5 | 2244.0 | 726.0 | 2241.8 | 738.0 |
| GR | 2243.9 | 750.0 | 2242.0 | 762.0 | 2244.5 | 774.0 | 2244.4 | 783.0 | 2244.3 | 792.0 |
| GR | 2244.1 | 801.0 | 2244.0 | 810.0 | 2244.2 | 820.3 | 2244.3 | 830.7 | 2244.5 | 841.0 |
| GR | 2244.6 | 850.8 | 2244.7 | 860.6 | 2244.8 | 870.4 | 2244.9 | 880.2 | 2245.0 | 890.0 |

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GR   2244.9    900.0   2244.8    910.0   2244.6    920.0   2244.5    930.0   2244.4    941.3
GR   2244.3    952.5   2244.1    963.8   2244.0    975.0   2244.0    987.5   2244.0   1000.0
GR   2244.0   1009.5   2244.0   1019.0   2244.3   1027.0   2244.5   1035.0   2244.3   1042.5
GR   2244.0   1050.0   2244.5   1060.5   2245.0   1071.0   2245.1   1082.3   2245.3   1093.5
GR   2245.4   1104.8   2245.5   1116.0   2245.3   1127.3   2245.2   1138.7   2245.0   1150.0
GR   2245.1   1158.8   2245.3   1167.5   2245.4   1176.3   2245.5   1185.0   2245.5   1195.0
GR   2245.5   1205.0   2245.5   1215.0   2245.5   1225.0   2245.5   1235.0   2245.5   1245.0
GR   2245.5   1255.0   2245.5   1265.0   2245.5   1275.0   2245.5   1285.0   2245.5   1295.5
GR   2245.5   1306.0   2249.0   1310.0   2260.0   1335.0

ET              9.1      9.1                                                   600.     1089.
            ET RECORD: STA 600. ELIMINATE INEFFECTIVE
                       FLOW AREA IN LEFT OVERBANK
X1   1.641       76    945.0   1000.0    490      520      510
GR   2264.0    185.0   2261.8    198.0   2259.5    211.0   2258.8    220.5   2258.0    230.0
GR   2257.5    242.5   2257.0    255.0   2256.5    267.5   2256.0    280.0   2255.7    293.3
GR   2255.3    306.7   2255.0    320.0   2254.7    333.3   2254.3    346.7   2254.0    360.0
GR   2253.5    373.3   2253.0    386.7   2252.5    400.0   2252.0    412.0   2252.5    430.0
GR   2252.3    442.3   2252.2    454.7   2252.0    467.0   2251.5    482.0   2252.5    498.0
GR   2252.8    509.0   2253.0    520.0   2252.8    530.0   2252.5    540.0   2252.8    555.0
GR   2253.0    570.0   2253.0    600.0   2250.0    610.0   2249.5    627.0   2249.3    639.0
GR   2249.0    651.0   2249.3    665.5   2249.5    680.0   2249.5    775.0   2249.6    787.0
GR   2249.7    799.0   2249.8    811.0   2249.9    823.0   2250.0    835.0   2250.0    900.0
GR   2249.8    911.3   2249.5    922.5   2249.3    933.8   2249.0    945.0   2249.0   1000.0
GR   2249.5   1010.5   2250.0   1021.0   2251.0   1037.0   2251.5   1055.0   2252.3   1066.3
GR   2253.2   1077.7   2254.0   1089.0   2253.9   1102.3   2253.9   1115.6   2253.8   1128.9
GR   2253.7   1142.1   2253.6   1155.4   2253.6   1168.7   2253.5   1182.0   2253.5   1290.0
GR   2253.8   1304.5   2254.0   1319.0   2254.8   1333.0   2255.7   1347.0   2256.5   1361.0
GR   2257.4   1373.8   2258.3   1386.5   2259.1   1399.3   2260.0   1412.0   2261.0   1426.0
GR   2262.0   1440.0

ET              9.1      9.1                                                   795.     1170.
            ET RECORD: STA 795. ELIMINATE INEFFECTIVE
                       FLOW AREA IN LEFT OVERBANK
X1   1.725       86    970.0   1028.0    460      420      440
GR   2269.0    290.0   2267.3    299.3   2265.7    308.7   2264.0    318.0   2263.3    327.3
GR   2262.5    336.5   2261.8    345.8   2261.0    355.0   2260.7    366.7   2260.3    378.3
GR   2260.0    390.0   2259.8    400.0   2259.7    410.0   2259.5    420.0   2259.3    430.0
GR   2259.2    440.0   2259.0    450.0   2259.1    460.3   2259.3    470.5   2259.4    480.8
GR   2259.5    491.0   2259.7    501.0   2259.8    511.0   2260.0    521.0   2259.9    532.0
GR   2259.8    543.0   2259.6    554.0   2259.5    565.0   2260.0    580.0   2260.1    590.0
GR   2260.3    600.0   2260.4    610.0   2260.5    620.0   2260.5    665.0   2260.3    675.0
GR   2260.0    685.0   2260.3    695.0   2260.5    705.0   2260.5    795.0   2260.0    804.3
GR   2259.5    813.7   2259.0    823.0   2258.5    831.0   2258.0    839.0   2257.0    850.0
GR   2257.0    890.0   2256.9    900.2   2256.8    910.4   2256.7    920.6   2256.6    930.8
GR   2256.5    941.0   2256.2    950.7   2255.8    960.3   2255.5    970.0   2255.3    980.0
GR   2255.2    990.0   2255.0   1000.0   2255.2   1009.3   2255.3   1018.7   2255.5   1028.0
GR   2256.0   1039.0   2256.5   1050.0   2256.3   1060.7   2256.2   1071.3   2256.0   1082.0
GR   2258.5   1091.5   2261.0   1101.0   2262.0   1110.5   2263.0   1120.0   2264.0   1130.0
GR   2265.0   1140.0   2266.0   1150.0   2267.0   1160.0   2268.0   1170.0   2268.3   1181.7
GR   2268.7   1193.3   2269.0   1205.0   2269.1   1215.5   2269.2   1226.0   2269.3   1236.5
GR   2269.3   1247.0   2269.4   1257.5   2269.5   1268.0   2269.5   1320.0   2269.8   1329.5
GR   2270.0   1339.0
```

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 656.79 | 1160. |
| X1 | 1.829 | 61 | 895.0 | 1000.0 | 570 | 540 | 550 | | | |
| GR | 2276.0 | 441.0 | 2274.0 | 451.0 | 2272.0 | 456.0 | 2270.0 | 468.0 | 2268.0 | 610.0 |
| GR | 2266.0 | 754.0 | 2265.8 | 763.0 | 2265.5 | 772.0 | 2265.7 | 781.3 | 2265.8 | 790.7 |
| GR | 2266.0 | 800.0 | 2265.5 | 809.5 | 2265.0 | 819.0 | 2265.5 | 827.0 | 2266.0 | 835.0 |
| GR | 2266.0 | 870.0 | 2264.5 | 882.5 | 2263.0 | 895.0 | 2263.1 | 905.0 | 2263.3 | 915.0 |
| GR | 2263.4 | 925.0 | 2263.5 | 935.0 | 2263.5 | 970.0 | 2263.3 | 980.0 | 2263.2 | 990.0 |
| GR | 2263.0 | 1000.0 | 2264.0 | 1012.0 | 2264.3 | 1021.0 | 2264.5 | 1030.0 | 2264.6 | 1039.7 |
| GR | 2264.6 | 1049.4 | 2264.7 | 1059.1 | 2264.8 | 1068.9 | 2264.9 | 1078.6 | 2264.9 | 1088.3 |
| GR | 2265.0 | 1098.0 | 2265.1 | 1108.3 | 2265.1 | 1118.6 | 2265.2 | 1128.9 | 2265.3 | 1139.1 |
| GR | 2265.4 | 1149.4 | 2265.4 | 1159.7 | 2265.5 | 1170.0 | 2266.1 | 1180.0 | 2266.2 | 1190.0 |
| GR | 2266.5 | 1200.0 | 2266.4 | 1210.0 | 2266.3 | 1220.0 | 2266.1 | 1230.0 | 2266.0 | 1240.0 |
| GR | 2266.4 | 1248.0 | 2266.7 | 1256.0 | 2268.0 | 1270.0 | 2270.0 | 1300.0 | 2270.0 | 1350.0 |
| GR | 2268.0 | 1355.0 | 2268.0 | 1365.0 | 2270.0 | 1375.0 | 2272.0 | 1412.0 | 2274.0 | 1440.0 |
| GR | 2276.0 | 1460.0 | | | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 882. | 1061.25 |
| X1 | 1.918 | 88 | 931.0 | 1007.5 | 560 | 420 | 470 | | | |
| GR | 2281.0 | 319.0 | 2280.8 | 328.0 | 2280.5 | 337.0 | 2280.3 | 346.0 | 2280.0 | 355.0 |
| GR | 2279.9 | 364.8 | 2279.8 | 374.5 | 2279.6 | 384.3 | 2279.5 | 394.0 | 2279.4 | 403.8 |
| GR | 2279.3 | 413.5 | 2279.1 | 423.3 | 2279.0 | 433.0 | 2278.9 | 442.5 | 2278.8 | 452.0 |
| GR | 2278.6 | 461.5 | 2278.5 | 471.0 | 2278.4 | 480.5 | 2278.3 | 490.0 | 2278.1 | 499.5 |
| GR | 2278.0 | 509.0 | 2277.8 | 518.9 | 2277.5 | 528.8 | 2277.3 | 538.6 | 2277.0 | 548.5 |
| GR | 2276.8 | 558.4 | 2276.5 | 568.3 | 2276.3 | 578.1 | 2276.0 | 588.0 | 2275.5 | 600.0 |
| [illegible] | 2275.5 | 610.0 | 2275.8 | 619.5 | 2276.0 | 629.0 | 2276.3 | 640.0 | 2276.7 | 651.0 |
| [illegible] | 2277.0 | 662.0 | 2277.0 | 720.0 | 2276.8 | 730.0 | 2276.7 | 740.0 | 2276.5 | 750.0 |
| GR | 2276.3 | 760.0 | 2276.2 | 770.0 | 2276.0 | 780.0 | 2275.6 | 789.8 | 2275.2 | 799.6 |
| GR | 2274.8 | 809.4 | 2274.4 | 819.2 | 2274.0 | 829.0 | 2273.7 | 837.9 | 2273.4 | 846.7 |
| GR | 2273.1 | 855.6 | 2272.9 | 864.4 | 2272.6 | 873.3 | 2272.3 | 882.1 | 2272.0 | 891.0 |
| GR | 2270.8 | 902.0 | 2269.5 | 913.0 | 2269.4 | 922.0 | 2269.3 | 931.0 | 2269.2 | 940.0 |
| GR | 2269.1 | 949.0 | 2269.0 | 958.0 | 2269.0 | 1000.0 | 2269.3 | 1007.5 | 2269.5 | 1015.0 |
| GR | 2271.0 | 1023.0 | 2272.5 | 1031.0 | 2274.0 | 1039.0 | 2274.3 | 1050.0 | 2274.7 | 1061.0 |
| GR | 2275.0 | 1072.0 | 2275.2 | 1081.3 | 2275.3 | 1090.7 | 2275.5 | 1100.0 | 2275.6 | 1110.2 |
| GR | 2275.7 | 1120.4 | 2275.8 | 1130.6 | 2275.9 | 1140.8 | 2276.0 | 1151.0 | 2276.3 | 1160.8 |
| GR | 2276.7 | 1170.7 | 2277.0 | 1180.5 | 2277.3 | 1190.3 | 2277.7 | 1200.2 | 2278.0 | 1210.0 |
| GR | 2279.7 | 1220.7 | 2281.3 | 1231.3 | 2283.0 | 1242.0 | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 900. | 1025.95 |
| X1 | 2.011 | 73 | 949.7 | 1011.0 | 490 | 495 | 490 | | | |
| GR | 2290.0 | 152.0 | 2289.5 | 161.0 | 2289.0 | 170.0 | 2288.8 | 178.8 | 2288.5 | 187.5 |
| GR | 2288.3 | 196.3 | 2288.0 | 205.0 | 2287.5 | 213.3 | 2287.0 | 221.7 | 2286.5 | 230.0 |
| GR | 2286.0 | 238.3 | 2285.5 | 246.7 | 2285.0 | 255.0 | 2285.1 | 264.4 | 2285.1 | 273.9 |
| GR | 2285.2 | 283.3 | 2285.2 | 292.8 | 2285.3 | 302.2 | 2285.3 | 311.7 | 2285.4 | 321.1 |
| GR | 2285.4 | 330.6 | 2285.5 | 340.0 | 2285.7 | 350.0 | 2285.8 | 360.0 | 2286.0 | 370.0 |
| GR | 2285.7 | 377.7 | 2285.3 | 385.3 | 2285.0 | 393.0 | 2284.5 | 405.0 | 2284.0 | 412.5 |
| GR | 2283.5 | 420.0 | 2283.5 | 619.0 | 2283.4 | 628.3 | 2283.4 | 646.8 | 2283.3 | 656.1 |
| GR | 2283.3 | 665.4 | 2283.2 | 674.6 | 2283.2 | 683.9 | 2283.1 | 693.2 | 2283.1 | 711.7 |
| GR | 2283.0 | 721.0 | 2282.7 | 729.0 | 2282.3 | 737.0 | 2282.0 | 745.0 | 2280.8 | 753.5 |
| GR | 2279.5 | 762.0 | 2279.5 | 803.0 | 2280.0 | 811.0 | 2280.5 | 819.0 | 2280.8 | 827.2 |
| GR | 2281.1 | 835.4 | 2281.4 | 843.6 | 2281.7 | 851.8 | 2282.0 | 860.0 | 2282.0 | 880.0 |
| [illegible] | 2281.3 | 889.3 | 2280.7 | 898.7 | 2280.0 | 908.0 | 2279.0 | 914.0 | 2278.0 | 921.5 |
| [illegible] | 2277.0 | 929.0 | 2276.5 | 939.3 | 2276.0 | 949.7 | 2275.5 | 960.0 | 2275.4 | 970.0 |
| GR | 2275.3 | 980.0 | 2275.1 | 990.0 | 2275.0 | 1000.0 | 2276.0 | 1011.0 | 2280.0 | 1020.5 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2284.0 | 1030.0 | 2288.0 | 1039.5 | 2292.0 | 1049.0 | | | | |
| NC | 0.050 | 0.050 | 0.030 | 0.3 | 0.5 | | | | | |
| ET | | | 9.1 | | | | | | 899.05 | 1041.74 |
| X1 | 2.056 | 80 | 926.5 | 1000.0 | 215 | 240 | 240 | | | |
| GR | 2294.0 | 250.0 | 2291.5 | 260.5 | 2289.0 | 271.0 | 2288.8 | 279.8 | 2288.5 | 288.5 |
| GR | 2288.3 | 297.3 | 2288.0 | 306.0 | 2287.2 | 315.7 | 2286.3 | 325.3 | 2285.5 | 335.0 |
| GR | 2285.4 | 343.5 | 2285.4 | 360.6 | 2285.3 | 369.2 | 2285.3 | 377.7 | 2285.2 | 386.3 |
| GR | 2285.2 | 394.8 | 2285.1 | 403.4 | 2285.1 | 420.5 | 2285.0 | 429.0 | 2285.0 | 437.6 |
| GR | 2285.1 | 446.2 | 2285.1 | 454.8 | 2285.2 | 463.3 | 2285.2 | 471.9 | 2285.3 | 480.5 |
| GR | 2285.3 | 497.7 | 2285.4 | 506.3 | 2285.4 | 514.8 | 2285.5 | 523.4 | 2285.5 | 532.0 |
| GR | 2285.6 | 540.0 | 2285.7 | 548.0 | 2285.8 | 556.0 | 2285.8 | 564.0 | 2285.9 | 572.0 |
| GR | 2286.0 | 580.0 | 2285.8 | 588.3 | 2285.7 | 596.7 | 2285.5 | 605.0 | 2285.6 | 614.3 |
| GR | 2285.8 | 623.5 | 2285.9 | 632.8 | 2286.0 | 642.0 | 2285.9 | 650.7 | 2285.9 | 659.4 |
| GR | 2285.8 | 668.1 | 2285.7 | 676.9 | 2285.6 | 685.6 | 2285.6 | 694.3 | 2285.5 | 703.0 |
| GR | 2285.4 | 711.4 | 2285.3 | 719.8 | 2285.2 | 728.2 | 2285.1 | 736.6 | 2285.0 | 745.0 |
| GR | 2285.1 | 753.8 | 2285.2 | 762.6 | 2285.3 | 771.4 | 2285.4 | 780.2 | 2285.5 | 789.0 |
| GR | 2285.5 | 893.0 | 2278.5 | 926.5 | 2278.5 | 955.0 | 2278.1 | 964.0 | 2277.7 | 973.0 |
| GR | 2277.3 | 982.0 | 2276.9 | 991.0 | 2276.5 | 1000.0 | 2280.0 | 1012.0 | 2281.0 | 1020.0 |
| GR | 2282.0 | 1028.0 | 2283.4 | 1036.6 | 2284.8 | 1045.2 | 2286.2 | 1053.8 | 2287.6 | 1062.4 |
| GR | 2289.0 | 1071.0 | 2289.8 | 1079.0 | 2290.5 | 1087.0 | 2291.3 | 1095.0 | 2292.0 | 1103.0 |
| QT | 6 | 6943 | 6943 | 6943 | 6943 | 6943 | 6943 | | | |
| ET | | | 9.1 | | | | | | 952.21 | 1037.53 |
| X1 | 2.107 | 80 | 965.0 | 1029.0 | 275 | 240 | 270 | | | |
| GR | 2292.0 | 650.0 | 2291.9 | 656.5 | 2291.8 | 663.0 | 2291.7 | 669.4 | 2291.6 | 675.9 |
| | 2291.5 | 682.4 | 2291.4 | 688.8 | 2291.3 | 695.3 | 2291.2 | 701.8 | 2291.1 | 708.3 |
| | 2290.9 | 714.7 | 2290.8 | 721.2 | 2290.7 | 727.7 | 2290.6 | 734.2 | 2290.5 | 740.6 |
| GR | 2290.4 | 747.1 | 2290.3 | 753.6 | 2290.2 | 760.0 | 2290.1 | 766.5 | 2290.0 | 773.0 |
| GR | 2290.0 | 913.0 | 2289.8 | 919.0 | 2289.7 | 925.0 | 2289.5 | 931.0 | 2289.3 | 937.0 |
| GR | 2289.2 | 943.0 | 2289.0 | 949.0 | 2284.8 | 957.0 | 2280.5 | 965.0 | 2280.5 | 1000.0 |
| GR | 2280.4 | 1007.3 | 2280.3 | 1014.5 | 2280.1 | 1021.8 | 2280.0 | 1029.0 | 2286.0 | 1036.0 |
| GR | 2292.0 | 1043.0 | 2291.7 | 1049.5 | 2291.3 | 1056.0 | 2291.0 | 1062.5 | 2290.7 | 1069.0 |
| GR | 2290.3 | 1075.5 | 2290.0 | 1082.0 | 2290.4 | 1088.4 | 2290.9 | 1094.9 | 2291.3 | 1101.3 |
| GR | 2291.8 | 1107.8 | 2292.2 | 1114.2 | 2292.7 | 1120.7 | 2293.1 | 1127.1 | 2293.6 | 1133.6 |
| GR | 2294.0 | 1140.0 | 2294.1 | 1146.5 | 2294.1 | 1153.0 | 2294.2 | 1159.6 | 2294.3 | 1166.1 |
| GR | 2294.3 | 1172.6 | 2294.4 | 1179.1 | 2294.5 | 1185.7 | 2294.5 | 1192.2 | 2294.6 | 1198.7 |
| GR | 2294.6 | 1205.2 | 2294.7 | 1211.7 | 2294.8 | 1218.3 | 2294.9 | 1224.8 | 2294.9 | 1231.3 |
| GR | 2295.0 | 1237.8 | 2295.0 | 1244.3 | 2295.1 | 1250.9 | 2295.2 | 1257.4 | 2295.2 | 1263.9 |
| GR | 2295.3 | 1270.4 | 2295.4 | 1277.0 | 2295.4 | 1283.5 | 2295.5 | 1290.0 | 2295.4 | 1297.0 |
| GR | 2295.3 | 1304.0 | 2295.3 | 1311.0 | 2295.2 | 1318.0 | 2295.1 | 1325.0 | 2295.0 | 1332.0 |
| NC | 0.050 | 0.050 | 0.020 | 0.3 | 0.5 | | | | | |
| | | DOWNSTREAM FACE OF US HWY 60 CONC BRIDGE (STRUCTURE A8-2) | | | | | | | | |
| X1 | 2.109 | 52 | 968.1 | 1030.0 | 10 | 10 | 10 | | | |
| X3 | 10 | | | | | | | 2299.2 | 2297.5 | |
| GR | 2300.0 | 695.0 | 2300.0 | 700.9 | 2299.9 | 706.7 | 2299.9 | 718.4 | 2299.8 | 724.3 |
| GR | 2299.8 | 736.0 | 2299.7 | 741.9 | 2299.7 | 747.7 | 2299.6 | 753.6 | 2299.6 | 765.3 |
| GR | 2299.5 | 771.1 | 2299.5 | 908.1 | 2299.4 | 914.3 | 2299.4 | 926.5 | 2299.3 | 932.6 |
| GR | 2299.3 | 951.0 | 2299.2 | 957.1 | 2299.2 | 968.09 | 2282.1 | 968.1 | 2282.1 | 969.4 |
| GR | 2282.1 | 975.5 | 2282.1 | 987.8 | 2282.1 | 993.9 | 2282.1 | 1000.0 | 2282.1 | 1006.0 |
| | 2282.1 | 1018.0 | 2282.1 | 1024.0 | 2282.1 | 1030.0 | 2298.8 | 1030.01 | 2298.7 | 1036.0 |
| | 2298.6 | 1042.0 | 2298.6 | 1054.0 | 2298.5 | 1060.0 | 2298.5 | 1145.9 | 2298.4 | 1151.8 |
| GR | 2298.4 | 1169.4 | 2298.3 | 1175.3 | 2298.3 | 1187.1 | 2298.2 | 1192.9 | 2298.2 | 1204.7 |

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GR   2298.1   1210.6   2298.1   1228.2   2298.0   1234.1   2298.0   1240.0   2297.9   1246.0
GR   2297.9   1258.0   2297.8   1264.0   2297.8   1270.0   2297.7   1276.0   2297.6   1282.0
GR   2297.6   1294.0   2297.5   1300.0

SB   1.25     1.56     2.8      0        61.9     1.5      845.6    0        2282.1   2282.1
          UPSTREAM FACE OF US HWY 60 CONC BRIDGE (STRUCTURE AB-2)
X1   2.118    52       968.1    1030.0   45       45       45
X2                     1        2296.1   2297.5
X3   10                                                               2299.2   2297.5
BT   -52      695.0    2300.0            700.9    2300.0            706.7    2299.9
BT            718.4    2299.9            724.3    2299.8            736.0    2299.8
BT            741.9    2299.7            747.7    2299.7            753.6    2299.6
BT            765.3    2299.6            771.1    2299.5            908.1    2299.5
BT            914.3    2299.4            926.5    2299.4            932.6    2299.3
BT            951.0    2299.3            957.1    2299.2            968.09   2299.2
BT            968.10   2299.2            969.4    2299.2            975.5    2299.1
BT            987.8    2299.1            993.9    2299.0            1000.0   2299.0
BT            1006.0   2298.9            1018.0   2298.9            1024.0   2298.8
BT            1030.0   2298.8            1030.01  2298.8            1036.0   2298.7
BT            1042.0   2298.6            1054.0   2298.6            1060.0   2298.5
BT            1145.9   2298.5            1151.8   2298.4            1169.4   2298.4
BT            1175.3   2298.3            1187.1   2298.3            1192.9   2298.2
BT            1204.7   2298.2            1210.6   2298.1            1228.2   2298.1
BT            1234.1   2298.0            1240.0   2298.0            1246.0   2297.9
BT            1258.0   2297.9            1264.0   2297.8            1270.0   2297.8
              1276.0   2297.7            1282.0   2297.6            1294.0   2297.6
              1300.0   2297.5
GR   2300.0   695.0    2300.0   700.9    2299.9   706.7    2299.9   718.4    2299.8   724.3
GR   2299.8   736.0    2299.7   741.9    2299.7   747.7    2299.6   753.6    2299.6   765.3
GR   2299.5   771.1    2299.5   908.1    2299.4   914.3    2299.4   926.5    2299.3   932.6
GR   2299.3   951.0    2299.2   957.1    2299.2   968.09   2282.1   968.1    2282.1   969.4
GR   2282.1   975.5    2282.1   987.8    2282.1   993.9    2282.1   1000.0   2282.1   1006.0
GR   2282.1   1018.0   2282.1   1024.0   2282.1   1030.0   2298.8   1030.01  2298.7   1036.0
GR   2298.6   1042.0   2298.6   1054.0   2298.5   1060.0   2298.5   1145.9   2298.4   1151.8
GR   2298.4   1169.4   2298.3   1175.3   2298.3   1187.1   2298.2   1192.9   2298.2   1204.7
GR   2298.1   1210.6   2298.1   1228.2   2298.0   1234.1   2298.0   1240.0   2297.9   1246.0
GR   2297.9   1258.0   2297.8   1264.0   2297.8   1270.0   2297.7   1276.0   2297.6   1282.0
GR   2297.6   1294.0   2297.5   1300.0

          DOWNSTREAM FACE OF OLD US HWY 60 CONC BRIDGE (STRUCTURE AB-1)
X1   2.120    72       970.5    1029.5   10       10       10
X3   10                                                               2297.0   2297.5
GR   2298.5   655.0    2298.5   661.5    2298.4   668.0    2298.4   687.6    2298.3   694.2
GR   2298.3   713.7    2298.2   720.3    2298.2   739.8    2298.1   746.4    2298.1   766.0
GR   2298.0   772.5    2298.0   779.0    2297.9   785.4    2297.9   798.2    2297.8   804.6
GR   2297.8   811.0    2297.7   817.5    2297.7   823.9    2297.6   830.3    2297.6   843.1
GR   2297.5   849.5    2297.4   855.9    2297.4   868.7    2297.3   875.1    2297.3   881.5
GR   2297.2   888.0    2297.2   894.4    2297.1   900.8    2297.1   913.6    2297.0   920.0
GR   2297.1   926.7    2297.2   933.3    2297.3   940.0    2297.3   946.7    2297.4   953.3
GR   2297.5   960.0    2297.6   966.7    2297.7   970.49   2282.1   970.5    2282.1   973.3
GR   2282.1   980.0    2282.1   986.7    2282.1   993.3    2282.1   1000.0   2282.1   1006.6
GR   2282.1   1013.2   2282.1   1029.5   2298.1   1029.51  2298.1   1039.6   2298.2   1046.2
GR   2298.2   1059.4   2298.3   1066.0   2298.3   1085.8   2298.4   1092.4   2298.4   1118.8
GR   2298.5   1125.4   2298.5   1138.6   2298.4   1145.1   2298.4   1164.8   2298.3   1171.3
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| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2298.3 | 1191.0 | 2298.2 | 1197.6 | 2298.2 | 1210.7 | 2298.1 | 1217.2 | 2298.1 | 1236.9 |
| GR | 2298.0 | 1243.4 | 2298.0 | 1250.0 | 2297.9 | 1256.0 | 2297.8 | 1262.0 | 2297.7 | 1268.0 |
| GR | 2297.6 | 1274.0 | 2297.5 | 1280.0 | | | | | | |
| SB | 1.25 | 1.56 | 2.8 | 0 | 59 | 3.0 | 588.0 | 0 | 2282.7 | 2282.1 |
| | | UPSTREAM FACE OF OLD US HWY 60 CONC BRIDGE (STRUCTURE AB-1) | | | | | | | | |
| X1 | 2.125 | 72 | 970.5 | 1029.5 | 30.3 | 30.3 | 30.3 | | | |
| X2 | | | 1 | 2293.2 | 2297.0 | | | | | |
| X3 | 10 | | | | | | | 2297.0 | 2297.5 | |
| BT | -72 | 655.0 | 2298.5 | | 661.5 | 2298.5 | | 668.0 | 2298.4 | |
| BT | | 687.6 | 2298.4 | | 694.2 | 2298.3 | | 713.7 | 2298.3 | |
| BT | | 720.3 | 2298.2 | | 739.8 | 2298.2 | | 746.4 | 2298.1 | |
| BT | | 766.0 | 2298.1 | | 772.5 | 2298.0 | | 779.0 | 2298.0 | |
| BT | | 785.4 | 2297.9 | | 798.2 | 2297.9 | | 804.6 | 2297.8 | |
| BT | | 811.0 | 2297.8 | | 817.5 | 2297.7 | | 823.9 | 2297.7 | |
| BT | | 830.3 | 2297.6 | | 843.1 | 2297.6 | | 849.5 | 2297.5 | |
| BT | | 855.9 | 2297.4 | | 868.7 | 2297.4 | | 875.1 | 2297.3 | |
| BT | | 881.5 | 2297.3 | | 888.0 | 2297.2 | | 894.4 | 2297.2 | |
| BT | | 900.8 | 2297.1 | | 913.6 | 2297.1 | | 920.0 | 2297.0 | |
| BT | | 926.7 | 2297.1 | | 933.3 | 2297.2 | | 940.0 | 2297.3 | |
| BT | | 946.7 | 2297.3 | | 953.3 | 2297.4 | | 960.0 | 2297.5 | |
| BT | | 966.7 | 2297.6 | | 970.49 | 2297.7 | | 970.5 | 2297.7 | |
| BT | | 973.3 | 2297.7 | | 980.0 | 2297.8 | | 986.7 | 2297.8 | |
| BT | | 993.3 | 2297.9 | | 1000.0 | 2298.0 | | 1006.6 | 2298.0 | |
| BT | | 1013.2 | 2298.1 | | 1029.5 | 2298.1 | | 1029.51 | 2298.1 | |
| | | 1039.6 | 2298.1 | | 1046.2 | 2298.2 | | 1059.4 | 2298.2 | |
| | | 1066.0 | 2298.3 | | 1085.8 | 2298.3 | | 1092.4 | 2298.4 | |
| BT | | 1118.8 | 2298.4 | | 1125.4 | 2298.5 | | 1138.6 | 2298.5 | |
| BT | | 1145.1 | 2298.4 | | 1164.8 | 2298.4 | | 1171.3 | 2298.3 | |
| BT | | 1191.0 | 2298.3 | | 1197.6 | 2298.2 | | 1210.7 | 2298.2 | |
| BT | | 1217.2 | 2298.1 | | 1236.9 | 2298.1 | | 1243.4 | 2298.0 | |
| BT | | 1250.0 | 2298.0 | | 1256.0 | 2297.9 | | 1262.0 | 2297.8 | |
| BT | | 1268.0 | 2297.7 | | 1274.0 | 2297.6 | | 1280.0 | 2297.5 | |
| GR | 2298.5 | 655.0 | 2298.5 | 661.5 | 2298.4 | 668.0 | 2298.4 | 687.6 | 2298.3 | 694.2 |
| GR | 2298.3 | 713.7 | 2298.2 | 720.3 | 2298.2 | 739.8 | 2298.1 | 746.4 | 2298.1 | 766.0 |
| GR | 2298.0 | 772.5 | 2298.0 | 779.0 | 2297.9 | 785.4 | 2297.9 | 798.2 | 2297.8 | 804.6 |
| GR | 2297.8 | 811.0 | 2297.7 | 817.5 | 2297.7 | 823.9 | 2297.6 | 830.3 | 2297.6 | 843.1 |
| GR | 2297.5 | 849.5 | 2297.4 | 855.9 | 2297.4 | 868.7 | 2297.3 | 875.1 | 2297.3 | 881.5 |
| GR | 2297.2 | 888.0 | 2297.2 | 894.4 | 2297.1 | 900.8 | 2297.1 | 913.6 | 2297.0 | 920.0 |
| GR | 2297.1 | 926.7 | 2297.2 | 933.3 | 2297.3 | 940.0 | 2297.3 | 946.7 | 2297.4 | 953.3 |
| GR | 2297.5 | 960.0 | 2297.6 | 966.7 | 2297.7 | 970.49 | 2282.7 | 970.5 | 2282.7 | 973.3 |
| GR | 2282.7 | 980.0 | 2282.7 | 986.7 | 2282.7 | 993.3 | 2282.7 | 1000.0 | 2282.7 | 1006.6 |
| GR | 2282.7 | 1013.2 | 2282.7 | 1029.5 | 2298.1 | 1029.51 | 2298.1 | 1039.6 | 2298.2 | 1046.2 |
| GR | 2298.2 | 1059.4 | 2298.3 | 1066.0 | 2298.3 | 1085.8 | 2298.4 | 1092.4 | 2298.4 | 1118.8 |
| GR | 2298.5 | 1125.4 | 2298.5 | 1138.6 | 2298.4 | 1145.1 | 2298.4 | 1164.8 | 2298.3 | 1171.3 |
| GR | 2298.3 | 1191.0 | 2298.2 | 1197.6 | 2298.2 | 1210.7 | 2298.1 | 1217.2 | 2298.1 | 1236.9 |
| GR | 2298.0 | 1243.4 | 2298.0 | 1250.0 | 2297.9 | 1256.0 | 2297.8 | 1262.0 | 2297.7 | 1268.0 |
| GR | 2297.6 | 1274.0 | 2297.5 | 1280.0 | | | | | | |

```
NC    0.050     0.050     0.030     0.1       0.3
ET                        9.1                                                 829.96    1062.63
X1    2.213     84        982.0     1027.5    415       525       465
GR    2301.0    739.0     2300.5    744.5     2300.0    750.0     2299.0    755.0     2298.0    760.0
GR    2297.5    766.7     2297.0    773.3     2296.5    780.0     2295.8    787.0     2295.0    794.0
GR    2294.3    801.0     2293.5    808.0     2294.0    815.3     2294.5    822.7     2295.0    830.0
GR    2295.3    837.0     2295.5    844.0     2295.8    851.0     2296.0    858.0     2296.0    890.0
GR    2296.1    896.7     2296.2    903.3     2296.3    910.0     2296.3    916.7     2296.4    923.3
GR    2296.5    930.0     2296.1    936.5     2295.7    943.0     2295.3    949.5     2294.8    956.0
GR    2294.4    962.5     2294.0    969.0     2293.0    975.5     2292.0    982.0     2290.0    990.0
GR    2289.8    995.0     2289.5    1000.0    2290.0    1009.0    2290.5    1014.5    2291.0    1020.0
GR    2292.5    1027.5    2294.0    1035.0    2294.8    1041.0    2295.7    1047.0    2296.5    1053.0
GR    2296.5    1059.5    2296.6    1066.1    2296.6    1079.2    2296.7    1085.7    2296.7    1092.2
GR    2296.8    1098.8    2296.8    1105.3    2296.9    1111.8    2296.9    1124.9    2297.0    1131.5
GR    2297.0    1138.0    2297.2    1145.0    2297.3    1152.0    2297.5    1159.0    2297.5    1221.0
GR    2297.3    1227.3    2297.2    1233.7    2297.0    1240.0    2297.0    1260.0    2297.2    1266.7
GR    2297.3    1273.3    2297.5    1280.0    2297.4    1286.5    2297.3    1293.0    2297.1    1299.5
GR    2297.0    1306.0    2297.2    1312.8    2297.3    1319.7    2297.5    1326.5    2297.7    1333.3
GR    2297.8    1340.2    2298.0    1347.0    2300.0    1356.0    2300.5    1363.0    2301.0    1370.0
GR    2301.3    1375.8    2301.5    1381.5    2301.8    1387.3    2302.0    1393.0

ET                        9.1                                                 829.96    1060.00
X1    2.248     77        988.0     1031.0    130       245       180
GR    2305.0    734.0     2304.8    742.0     2304.5    750.0     2303.1    758.0     2301.8    766.0
GR    2300.4    774.0     2299.0    782.0     2298.4    789.6     2297.8    797.2     2297.2    804.8
GR    2296.6    812.4     2296.0    820.0     2295.5    831.0     2295.8    838.5     2296.0    846.0
GR    2296.1    853.7     2296.3    861.5     2296.4    869.2     2296.6    876.9     2296.7    884.6
GR    2296.8    892.4     2296.9    900.1     2297.1    907.8     2297.2    915.5     2297.4    923.3
GR    2297.5    931.0     2297.5    972.0     2296.8    980.0     2296.0    988.0     2293.0    995.0
GR    2292.0    1000.0    2293.0    1011.0    2294.8    1021.0    2296.5    1031.0    2296.9    1038.5
GR    2297.3    1046.0    2297.6    1053.5    2298.0    1061.0    2298.1    1069.1    2298.2    1077.2
GR    2298.3    1085.3    2298.4    1093.4    2298.5    1101.5    2298.6    1109.6    2298.7    1117.7
GR    2298.8    1125.8    2298.9    1133.9    2299.0    1142.0    2299.0    1261.0    2299.2    1269.7
GR    2299.3    1278.3    2299.5    1287.0    2299.8    1295.5    2300.0    1304.0    2300.5    1312.0
GR    2301.0    1320.0    2301.1    1328.5    2301.3    1337.0    2301.4    1345.5    2301.5    1354.0
GR    2301.6    1362.5    2301.8    1371.0    2301.9    1379.5    2302.0    1388.0    2302.1    1396.1
GR    2302.1    1412.3    2302.2    1420.4    2302.3    1428.5    2302.3    1436.6    2302.4    1444.7
GR    2302.4    1460.9    2302.5    1469.0    2302.6    1477.4    2302.7    1485.8    2302.8    1494.2
GR    2302.9    1502.6    2303.0    1511.0

ET                7.1       9.1                                   940.      1475.     946.06    1109.00
                ET RECORD: STA 1475. ELIMINATE INEFFECTIVE
                           FLOW AREA IN RIGHT OVERBANK
X1    2.342     85        970.0     1010.0    515       450       500
GR    2310.0    940.0     2305.0    947.5     2300.0    955.0     2299.0    962.5     2298.0    970.0
GR    2297.8    977.5     2297.5    985.0     2297.3    992.5     2297.0    1000.0    2298.0    1010.0
GR    2300.0    1020.0    2302.0    1030.0    2302.5    1038.8    2303.0    1047.5    2303.5    1056.3
GR    2304.0    1065.0    2303.8    1075.0    2303.5    1085.0    2303.8    1092.5    2304.0    1100.0
GR    2304.1    1109.2    2304.2    1118.4    2304.3    1127.6    2304.4    1136.8    2304.5    1146.1
GR    2304.6    1155.3    2304.7    1164.5    2304.8    1173.7    2304.9    1182.9    2305.1    1192.1
GR    2305.2    1201.3    2305.3    1210.5    2305.4    1219.7    2305.5    1228.9    2305.6    1238.2
GR    2305.7    1247.4    2305.8    1256.6    2305.9    1265.8    2306.0    1275.0    2306.1    1284.1
GR    2306.1    1302.3    2306.2    1311.4    2306.2    1320.4    2306.3    1329.6    2306.3    1338.6
```

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2306.4 | 1347.7 | 2306.4 | 1365.9 | 2306.5 | 1375.0 | 2306.6 | 1384.1 | 2306.6 | 1402.3 |
| | 2306.7 | 1411.4 | 2306.7 | 1420.4 | 2306.8 | 1429.6 | 2306.8 | 1438.6 | 2306.9 | 1447.7 |
| GR | 2306.9 | 1465.9 | 2307.0 | 1475.0 | 2306.9 | 1484.1 | 2306.9 | 1493.2 | 2306.8 | 1502.3 |
| GR | 2306.8 | 1511.5 | 2306.7 | 1520.6 | 2306.6 | 1529.7 | 2306.6 | 1538.8 | 2306.5 | 1547.9 |
| GR | 2306.5 | 1557.1 | 2306.4 | 1566.2 | 2306.4 | 1575.3 | 2306.3 | 1584.4 | 2306.2 | 1593.5 |
| GR | 2306.2 | 1602.7 | 2306.1 | 1611.8 | 2306.1 | 1620.9 | 2306.0 | 1630.0 | 2305.8 | 1638.8 |
| GR | 2305.5 | 1647.5 | 2305.3 | 1656.3 | 2305.0 | 1665.0 | 2305.5 | 1720.0 | 2305.0 | 1770.0 |
| GR | 2306.0 | 1790.0 | 2307.0 | 1810.0 | 2308.0 | 1830.0 | 2309.0 | 1837.5 | 2310.0 | 1845.0 |
| ET | | 7.1 | 9.1 | | | | 952. | 1228.0 | 957.69 | 1102 |

CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH

ET RECORD: STA 1288. ELIMINATE INEFFECTIVE
FLOW AREA IN RIGHT OVERBANK

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 2.435 | 93 | 991.0 | 1027.0 | 500 | 455 | 490 | | | |
| GR | 2318.0 | 952.0 | 2308.0 | 959.0 | 2307.0 | 967.5 | 2306.0 | 976.0 | 2304.0 | 991.0 |
| GR | 2303.8 | 1000.0 | 2303.5 | 1009.0 | 2303.8 | 1018.0 | 2304.0 | 1027.0 | 2304.3 | 1037.0 |
| GR | 2304.6 | 1047.0 | 2304.9 | 1057.0 | 2305.2 | 1067.0 | 2305.5 | 1077.0 | 2306.0 | 1092.0 |
| GR | 2306.8 | 1102.0 | 2307.7 | 1108.0 | 2308.5 | 1112.0 | 2308.6 | 1112.7 | 2308.8 | 1117.4 |
| GR | 2308.9 | 1120.1 | 2309.1 | 1124.8 | 2309.3 | 1135.5 | 2309.4 | 1136.2 | 2309.6 | 1136.9 |
| GR | 2309.7 | 1137.6 | 2309.9 | 1138.3 | 2310.0 | 1139.0 | 2311.0 | 1183.5 | 2312.0 | 1228.0 |
| GR | 2312.0 | 1258.3 | 2311.9 | 1268.7 | 2311.9 | 1279.0 | 2311.8 | 1289.3 | 2311.8 | 1310.0 |
| GR | 2311.7 | 1320.3 | 2311.7 | 1330.7 | 2311.6 | 1341.0 | 2311.6 | 1351.3 | 2311.5 | 1361.7 |
| GR | 2311.5 | 1372.0 | 2311.3 | 1384.5 | 2311.0 | 1397.0 | 2311.0 | 1429.0 | 2311.2 | 1438.0 |
| GR | 2311.3 | 1447.0 | 2311.5 | 1456.0 | 2311.6 | 1466.9 | 2311.6 | 1488.7 | 2311.7 | 1499.6 |
| | 2311.7 | 1510.6 | 2311.8 | 1521.4 | 2311.8 | 1532.4 | 2311.9 | 1543.3 | 2311.9 | 1565.1 |
| | 2312.0 | 1576.0 | 2311.5 | 1586.0 | 2311.0 | 1596.0 | 2311.0 | 1609.0 | 2311.3 | 1618.5 |
| | 2311.5 | 1628.0 | 2311.3 | 1640.0 | 2311.0 | 1652.0 | 2311.3 | 1664.5 | 2311.5 | 1677.0 |
| GR | 2311.3 | 1687.0 | 2311.1 | 1697.0 | 2310.9 | 1707.0 | 2310.7 | 1717.0 | 2310.5 | 1727.0 |
| GR | 2310.3 | 1737.0 | 2310.0 | 1747.0 | 2309.8 | 1757.0 | 2309.7 | 1767.0 | 2309.5 | 1777.0 |
| GR | 2309.7 | 1788.7 | 2309.8 | 1800.3 | 2310.0 | 1812.0 | 2309.7 | 1821.0 | 2309.3 | 1830.0 |
| GR | 2309.0 | 1839.0 | 2308.0 | 1880.0 | 2308.7 | 1889.0 | 2309.3 | 1898.0 | 2310.0 | 1907.0 |
| GR | 2311.3 | 1917.0 | 2312.7 | 1927.0 | 2314.0 | 1937.0 | 2315.3 | 1947.0 | 2316.7 | 1957.0 |
| GR | 2318.0 | 1967.0 | 2320.0 | 1977.0 | 2322.0 | 1991.0 | | | | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

```
*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS
0

CCHV=     .100 CEHV=     .300
*SECNO  .095
            CONFLUENCE OF WASH AB: FLYING E WASH
            AND SOLS WASH BETWEEN CROSS-SECTIONS
                V (SOLS WASH RIVER MILE 1.97)
                W (SOLS WASH RIVER MILE 2.06)
            CROSS-SECTION DESIGNATION FROM
                SOLS WASH FLOODPLAIN DLINEATION
                HASSAYAMPA RIVER TO MARICOPA COUNTY LINE
                CELLA BARR ASSOCIATES

            SWSE DETERMINED BY SLOPE AREA METHOD

            SPLIT FLOW OPTION USED FROM XSECT 0.134 TO XSECT 0.220
            TO MODEL OVERFLOW LEVEE IN RIGHT OVERBANK.  THE PROGRAM
            WILL USE THE ENERGY GRADE LINE TO DETERMINE OVERFLOW.
     .095      3.50   2134.50   2134.47   2134.50   2135.94      1.44       .00       .00   2132.00
   3002.4      23.5    2899.7      79.2      10.0     296.5      21.3        .0        .0   2132.00
      .00      2.37      9.78      3.71      .050      .030      .050      .000   2131.00    905.00
  .008120        0.        0.        0.         0         4         0       .00    121.31   1026.31


FLOW DISTRIBUTION FOR SECNO=       .09          CWSEL=   2134.50

STA=     905.     920.    1011.    1026.
  PER Q=       .8     96.6      2.6
   AREA=      9.9    296.5     21.3
    VEL=      2.4      9.8      3.7
  DEPTH=       .7      3.2      1.4

CCHV=     .300 CEHV=     .500
*SECNO  .125
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
     .125      3.42   2136.42   2136.42       .00   2137.76      1.34      1.38       .03   2134.00
   3002.4      72.7    2924.8       5.0      17.6     311.3       2.1       1.2        .4   2134.00
      .00      4.12      9.40      2.41      .050      .030      .050      .000   2133.00    885.00
  .009227      130.      160.      160.         0         8         0       .00    127.87   1012.87
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .13 CWSEL= 2136.42

| STA= | 885. | 888. | 890. | 891. | 893. | 895. | 897. | 899. | 1011. | 1012. | 1013. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .0 | .0 | .1 | .3 | .5 | .7 | .8 | 97.4 | .2 | .0 | |
| AREA= | .5 | .7 | 1.4 | 2.5 | 3.6 | 4.3 | 4.5 | 311.3 | 1.9 | .1 | |
| VEL= | 1.2 | 1.5 | 2.2 | 3.3 | 4.3 | 4.9 | 5.1 | 9.4 | 2.5 | .9 | |
| DEPTH= | .2 | .4 | .7 | 1.3 | 1.9 | 2.3 | 2.4 | 2.8 | 1.5 | .3 | |

*SECNO .131

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.29

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2139.90 ELREA= 2139.40

DS FACE: AT&SF RAILROAD BRIDGE (STRUCTURE AB-3)

NOTE: CENTERLINE SECTION OF AT&SF RAILROAD WAS
USED TO CREATE THE DS FACE CROSS-SECTION

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .131 | 4.10 | 2137.70 | 2136.05 | .00 | 2138.14 | .44 | .10 | .27 | 2133.60 |
| 3002.4 | .0 | 3002.4 | .0 | .0 | 565.0 | .0 | 1.5 | .5 | 2133.60 |
| .01 | .00 | 5.31 | .00 | .000 | .030 | .000 | .000 | 2133.60 | 875.00 |
| .001757 | 30. | 30. | 30. | 3 | 15 | 0 | .00 | 138.00 | 1013.00 |

FLOW DISTRIBUTION FOR SECNO= .13 CWSEL= 2137.70

| STA= | 875. | 1013. |
|---|---|---|
| PER Q= | 100.0 | |
| AREA= | 565.0 | |
| VEL= | 5.3 | |
| DEPTH= | 4.1 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

SPECIAL BRIDGE

| SB | XK | XKOR | COFQ | RDLEN | BWC | BWP | BAREA | SS | ELCHU | ELCHD |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1.05 | 1.83 | 2.80 | .00 | 138.00 | 9.00 | 387.00 | .00 | 2133.70 | 2133.60 |

*SECNO .134

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.61

PRESSURE AND WEIR FLOW, Weir Submergence Based on TRAPEZOIDAL Shape

| EGPRS | EGLWC | H3 | QWEIR | QPR | BAREA | TRAPEZOID AREA | ELLC | ELTRD | WEIRLN |
|---|---|---|---|---|---|---|---|---|---|
| 2139.41 | 2138.23 | .09 | 0. | 2999. | 387. | 387. | 2136.70 | 2139.40 | 1. |

OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2139.90 ELREA= 2139.40

US FACE: AT&SF RAILROAD BRIDGE (STRUCTURE AB-3)
NOTE: CENTERLINE SECTION OF AT&SF RAILROAD WAS
USED TO CREATE THE US FACE CROSS-SECTION

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .134 | 5.46 | 2139.16 | .00 | .00 | 2139.40 | .25 | 1.27 | .00 | 2133.70 |
| 3002.4 | .0 | 3002.4 | .0 | .0 | 753.2 | .0 | 1.7 | .6 | 2133.70 |
| .01 | .00 | 3.99 | .00 | .000 | .030 | .000 | .000 | 2133.70 | 875.00 |
| .000674 | 15. | 15. | 15. | 2 | 0 | 0 | .00 | 138.00 | 1013.00 |

FLOW DISTRIBUTION FOR SECNO= .13 CWSEL= 2139.16

STA= 875. 1013.
PER Q= 100.0
AREA= 753.2
VEL= 4.0
DEPTH= 5.5

*SECNO .160

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3470 ENCROACHMENT STATIONS= 730.0 1048.0 TYPE= 1 TARGET= 318.000

ET RECORD: STATION 730. MODEL 1 TO 1
FLOW CONTRACTION UPSTREAM
OF AT&SF BRIDGE

ET RECORD: STATION 1048. TOP OF OVERFLOW
LEVEE IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .160 | 3.85 | 2139.85 | 2139.85 | 2139.85 | 2140.92 | 1.07 | .27 | .41 | 2136.60 |
| 4245.8 | 1326.5 | 2583.7 | 335.7 | 336.0 | 255.3 | 78.3 | 4.0 | 1.3 | 2136.50 |
| .01 | 3.95 | 10.12 | 4.29 | .050 | .030 | .050 | .000 | 2136.00 | 730.00 |
| .007419 | 140. | 140. | 140. | 0 | 19 | 0 | .00 | 318.00 | 1048.00 |

FLOW DISTRIBUTION FOR SECNO= .16 CWSEL= 2139.85

| STA= | 730. | 745. | 767. | 789. | 819. | 895. | 921. | 942. | 1012. | 1023. | 1043. | 1048. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.3 | 4.7 | 3.5 | 3.0 | 3.1 | 4.3 | 8.3 | 60.9 | 3.7 | 3.6 | .6 | |
| AREA= | 40.3 | 46.9 | 39.0 | 40.6 | 57.1 | 47.1 | 64.9 | 255.3 | 31.6 | 38.3 | 8.3 | |
| VEL= | 4.6 | 4.3 | 3.8 | 3.2 | 2.3 | 3.9 | 5.4 | 10.1 | 5.0 | 4.0 | 3.0 | |
| TH= | 2.7 | 2.2 | 1.8 | 1.4 | .7 | 1.8 | 3.1 | 3.7 | 2.7 | 1.9 | 1.7 | |

CCHV= .100 CEHV= .300
*SECNO .220
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 360.0 1092.5 TYPE= 1 TARGET= 732.500

ET RECORD: STATION 1092.5 TOP OF OVERFLOW
LEVEE IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .220 | 3.27 | 2143.77 | 2143.77 | 2143.77 | 2144.66 | .89 | 3.14 | .02 | 2141.00 |
| 7820.0 | 5006.5 | 2255.3 | 558.2 | 961.6 | 195.3 | 112.7 | 10.7 | 4.7 | 2141.00 |
| .02 | 5.21 | 11.55 | 4.96 | .050 | .030 | .050 | .000 | 2140.50 | 434.96 |
| .012537 | 295. | 315. | 320. | 0 | 15 | 0 | .00 | 657.54 | 1092.50 |

FLOW DISTRIBUTION FOR SECNO= .22 CWSEL= 2143.77

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 435. | 482. | 507. | 523. | 540. | 556. | 571. | 595. | 618. | 642. | 673. | 710. | 832. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.4 | 4.3 | 3.2 | 3.6 | 3.5 | 3.2 | 4.3 | 3.8 | 3.3 | 3.6 | 3.0 | 7.7 | |
| AREA= | 59.0 | 57.5 | 41.4 | 44.5 | 42.0 | 40.3 | 56.6 | 52.3 | 47.8 | 56.6 | 55.0 | 154.6 | |
| VEL= | 4.5 | 5.8 | 6.1 | 6.4 | 6.4 | 6.2 | 6.0 | 5.7 | 5.3 | 5.0 | 4.3 | 3.9 | |
| DEPTH= | 1.3 | 2.3 | 2.5 | 2.7 | 2.7 | 2.6 | 2.4 | 2.2 | 2.0 | 1.8 | 1.5 | 1.3 | |

| STA= | 832. | 873. | 904. | 927. | 950. | 965. | 1030. | 1054. | 1085. | 1092. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 3.5 | 3.2 | 3.9 | 3.2 | 28.8 | 3.5 | 3.0 | .6 | |
| AREA= | 58.9 | 56.1 | 46.8 | 52.6 | 39.6 | 195.3 | 50.1 | 50.9 | 11.7 | |
| VEL= | 4.3 | 4.9 | 5.3 | 5.8 | 6.4 | 11.5 | 5.5 | 4.6 | 3.9 | |
| DEPTH= | 1.4 | 1.8 | 2.0 | 2.3 | 2.6 | 3.0 | 2.1 | 1.6 | 1.5 | |

*SECNO .256
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .256 | 4.24 | 2147.24 | 2147.24 | 2147.24 | 2148.14 | .90 | 2.11 | .00 | 2143.00 |
| 7820.0 | 5006.6 | 2061.8 | 751.6 | 1047.4 | 165.4 | 156.4 | 16.8 | 7.6 | 2143.00 |
| .03 | 4.78 | 12.47 | 4.81 | .050 | .030 | .050 | .000 | 2143.00 | 465.08 |
| .009231 | 200. | 190. | 200. | 0 | 11 | 0 | .00 | 619.88 | 1084.96 |

W DISTRIBUTION FOR SECNO= .26 CWSEL= 2147.24

| STA= | 465. | 509. | 542. | 790. | 815. | 847. | 880. | 911. | 942. | 961. | 1000. | 1010. | 1040. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.0 | 3.8 | 34.6 | 3.2 | 3.7 | 3.2 | 3.4 | 4.3 | 4.8 | 26.4 | 3.3 | 3.5 | |
| AREA= | 61.6 | 66.3 | 554.1 | 52.4 | 64.5 | 59.4 | 60.5 | 68.6 | 60.1 | 165.4 | 37.4 | 59.5 | |
| VEL= | 3.8 | 4.5 | 4.9 | 4.7 | 4.5 | 4.3 | 4.5 | 4.9 | 6.2 | 12.5 | 6.9 | 4.5 | |
| DEPTH= | 1.4 | 2.0 | 2.2 | 2.1 | 2.0 | 1.8 | 1.9 | 2.2 | 3.2 | 4.2 | 3.7 | 2.0 | |

| STA= | 1040. | 1085. |
|---|---|---|
| PER Q= | 2.9 | |
| AREA= | 59.5 | |
| VEL= | 3.8 | |
| DEPTH= | 1.3 | |

*SECNO .351
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .351 | 4.28 | 2153.28 | 2153.28 | 2153.28 | 2154.43 | 1.15 | 4.00 | .08 | 2149.00 |
| 7820.0 | 2454.3 | 3977.3 | 1388.4 | 485.5 | 355.2 | 365.9 | 31.0 | 13.6 | 2149.00 |
| .05 | 5.05 | 11.20 | 3.79 | .050 | .030 | .050 | .000 | 2149.00 | 735.98 |
| .007357 | 470. | 500. | 505. | 0 | 5 | 0 | .00 | 470.42 | 1206.40 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .35 CWSEL= 2153.28

| STA= | 736. | 804. | 821. | 843. | 904. | 917. | 1000. | 1032. | 1200. | 1206. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 13.7 | 3.6 | 3.7 | 7.8 | 2.5 | 50.9 | 3.2 | 14.2 | .3 | |
| AREA= | 197.5 | 52.0 | 59.4 | 138.4 | 38.1 | 355.2 | 60.5 | 297.8 | 7.6 | |
| VEL= | 5.4 | 5.4 | 4.9 | 4.4 | 5.2 | 11.2 | 4.2 | 3.7 | 3.0 | |
| DEPTH= | 2.9 | 3.1 | 2.6 | 2.3 | 2.9 | 4.3 | 1.9 | 1.8 | 1.2 | |

*SECNO .460

3265 DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .460 | 5.84 | 2161.34 | 2161.34 | 2161.34 | 2163.02 | 1.68 | 4.68 | .16 | 2156.00 |
| 7820.0 | 112.9 | 2824.6 | 4882.5 | 23.4 | 191.7 | 707.9 | 45.3 | 18.6 | 2156.00 |
| .07 | 4.84 | 14.74 | 6.90 | .050 | .030 | .050 | .000 | 2155.50 | 973.55 |
| 008828 | 580. | 575. | 590. | 0 | 11 | 0 | .00 | 273.25 | 1268.97 |

FLOW DISTRIBUTION FOR SECNO= .46 CWSEL= 2161.34

| STA= | 974. | 982. | 1016. | 1023. | 1029. | 1040. | 1052. | 1063. | 1074. | 1085. | 1097. | 1108. | 1120. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 1.4 | 36.1 | 3.5 | 3.3 | 5.1 | 4.2 | 3.9 | 3.6 | 3.8 | 4.2 | 4.6 | 4.9 | |
| AREA= | 23.4 | 191.7 | 32.5 | 31.2 | 52.4 | 45.9 | 43.7 | 41.5 | 43.1 | 46.5 | 48.8 | 51.1 | |
| VEL= | 4.8 | 14.7 | 8.4 | 8.2 | 7.6 | 7.2 | 7.0 | 6.7 | 6.8 | 7.1 | 7.3 | 7.5 | |
| DEPTH= | 2.7 | 5.6 | 5.2 | 5.0 | 4.5 | 4.1 | 3.9 | 3.7 | 3.8 | 4.0 | 4.2 | 4.4 | |

| STA= | 1120. | 1131. | 1140. | 1148. | 1162. | 1183. | 1269. |
|---|---|---|---|---|---|---|---|
| PER Q= | 5.1 | 3.4 | 3.1 | 4.3 | 4.0 | 1.5 | |
| AREA= | 52.2 | 36.5 | 34.3 | 50.9 | 56.7 | 40.6 | |
| VEL= | 7.7 | 7.4 | 7.1 | 6.6 | 5.5 | 2.9 | |
| DEPTH= | 4.5 | 4.3 | 4.0 | 3.6 | 2.7 | .5 | |

*SECNO .540
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .540 | 3.99 | 2165.99 | 2165.99 | 2166.00 | 2167.41 | 1.41 | 3.94 | .03 | 2162.20 |
| 7820.0 | 3382.6 | 1807.1 | 2630.3 | 429.7 | 125.6 | 376.2 | 52.6 | 20.9 | 2162.40 |
| .08 | 7.87 | 14.39 | 6.99 | .050 | .030 | .050 | .000 | 2162.00 | 822.80 |
| .014427 | 390. | 425. | 295. | 0 | 19 | 0 | .00 | 321.61 | 1144.41 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .54 CWSEL= 2165.99

| STA= | 823. | 857. | 873. | 884. | 895. | 906. | 917. | 928. | 940. | 956. | 967. | 1000. | 1010. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 3.4 | 3.2 | 3.4 | 3.6 | 4.3 | 5.3 | 5.1 | 7.0 | 4.8 | 23.1 | 3.9 | |
| AREA= | 50.3 | 39.4 | 33.5 | 34.9 | 36.0 | 40.1 | 45.9 | 45.0 | 61.9 | 42.7 | 125.6 | 36.5 | |
| VEL= | 4.9 | 6.6 | 7.5 | 7.7 | 7.8 | 8.4 | 9.0 | 8.9 | 8.8 | 8.8 | 14.4 | 8.3 | |
| DEPTH= | 1.5 | 2.5 | 3.0 | 3.1 | 3.2 | 3.6 | 4.0 | 3.9 | 3.9 | 3.8 | 3.8 | 3.5 | |

| STA= | 1010. | 1021. | 1031. | 1041. | 1067. | 1082. | 1103. | 1125. | 1144. |
|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 3.5 | 3.3 | 6.2 | 3.3 | 4.3 | 3.8 | 1.7 | |
| AREA= | 35.5 | 34.1 | 33.4 | 69.5 | 38.9 | 51.8 | 48.2 | 28.3 | |
| VEL= | 8.1 | 8.0 | 7.8 | 7.0 | 6.7 | 6.4 | 6.1 | 4.8 | |
| DEPTH= | 3.4 | 3.3 | 3.2 | 2.7 | 2.5 | 2.4 | 2.2 | 1.4 | |

*SECNO .576
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .576 | 4.40 | 2169.20 | 2169.20 | 2169.20 | 2170.67 | 1.47 | 2.44 | .02 | 2164.90 |
| 7820.0 | 4568.4 | 2491.8 | 759.8 | 672.3 | 178.1 | 100.7 | 56.7 | 22.3 | 2164.90 |
| .08 | 6.79 | 13.99 | 7.54 | .050 | .030 | .050 | .000 | 2164.80 | 717.46 |
| 11505 | 200. | 190. | 165. | 0 | 8 | 0 | .00 | 311.48 | 1028.94 |

FLOW DISTRIBUTION FOR SECNO= .58 CWSEL= 2169.20

| STA= | 717. | 764. | 781. | 803. | 830. | 847. | 858. | 869. | 880. | 891. | 902. | 913. | 925. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 3.4 | 3.6 | 3.7 | 3.6 | 3.1 | 3.8 | 4.1 | 3.3 | 3.7 | 4.0 | 4.2 | |
| AREA= | 65.3 | 43.5 | 50.6 | 55.9 | 45.1 | 35.5 | 40.0 | 41.7 | 36.6 | 39.2 | 41.1 | 42.5 | |
| VEL= | 4.8 | 6.1 | 5.6 | 5.1 | 6.2 | 6.9 | 7.5 | 7.7 | 7.1 | 7.4 | 7.6 | 7.8 | |
| DEPTH= | 1.4 | 2.6 | 2.3 | 2.0 | 2.7 | 3.2 | 3.6 | 3.8 | 3.3 | 3.5 | 3.7 | 3.8 | |

| STA= | 925. | 936. | 947. | 958. | 1000. | 1012. | 1024. | 1029. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.3 | 4.6 | 5.0 | 31.9 | 5.2 | 4.1 | .4 | |
| AREA= | 43.0 | 44.8 | 47.5 | 178.1 | 50.0 | 43.3 | 7.4 | |
| VEL= | 7.8 | 8.0 | 8.3 | 14.0 | 8.2 | 7.5 | 3.8 | |
| DEPTH= | 3.8 | 4.0 | 4.2 | 4.3 | 4.1 | 3.6 | 1.6 | |

*SECNO .640

3265 DIVIDED FLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .640 | 4.67 | 2174.17 | 2174.17 | 2174.17 | 2175.47 | 1.30 | 3.87 | .02 | 2169.80 |
| 7820.0 | 3481.3 | 1906.0 | 2432.6 | 537.3 | 134.6 | 338.4 | 64.4 | 25.1 | 2169.80 |
| .09 | 6.48 | 14.16 | 7.19 | .050 | .030 | .050 | .000 | 2169.50 | 690.53 |
| .010939 | 350. | 340. | 340. | 0 | 8 | 0 | .00 | 393.49 | 1121.64 |

FLOW DISTRIBUTION FOR SECNO= .64 CWSEL= 2174.17

| STA= | 691. | 847. | 867. | 882. | 896. | 911. | 932. | 955. | 964. | 973. | 982. | 991. | 1021. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 4.6 | 3.4 | 3.7 | 3.5 | 3.3 | 4.8 | 4.7 | 4.4 | 3.9 | 4.1 | 24.4 | |
| AREA= | 79.5 | 58.0 | 42.4 | 44.7 | 43.3 | 48.1 | 60.9 | 42.9 | 41.1 | 37.5 | 38.9 | 134.6 | |
| VEL= | 4.0 | 6.3 | 6.2 | 6.5 | 6.4 | 5.4 | 6.2 | 8.6 | 8.3 | 8.1 | 8.2 | 14.2 | |
| DEPTH= | .5 | 2.9 | 2.8 | 3.0 | 2.9 | 2.3 | 2.7 | 4.6 | 4.4 | 4.2 | 4.3 | 4.5 | |

| STA= | 1021. | 1028. | 1035. | 1042. | 1055. | 1069. | 1082. | 1095. | 1115. | 1122. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 3.1 | 3.1 | 5.4 | 4.6 | 3.7 | 3.2 | 4.3 | .4 | |
| AREA= | 30.6 | 29.8 | 29.5 | 53.5 | 49.2 | 42.5 | 38.9 | 54.9 | 9.5 | |
| VEL= | 8.3 | 8.2 | 8.1 | 7.8 | 7.4 | 6.8 | 6.4 | 6.2 | 3.6 | |
| DEPTH= | 4.4 | 4.3 | 4.2 | 4.0 | 3.7 | 3.2 | 3.0 | 2.8 | 1.3 | |

*SECNO .707
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .707 | 5.69 | 2181.69 | 2181.69 | 2181.69 | 2182.93 | 1.25 | 3.17 | .01 | 2176.30 |
| 7820.0 | 3481.3 | 2312.1 | 2026.6 | 572.0 | 166.6 | 396.5 | 72.8 | 28.4 | 2176.30 |
| .11 | 6.09 | 13.88 | 5.11 | .050 | .030 | .050 | .000 | 2176.00 | 746.02 |
| .007992 | 320. | 350. | 365. | 0 | 11 | 0 | .00 | 450.79 | 1196.82 |

FLOW DISTRIBUTION FOR SECNO= .71 CWSEL= 2181.69

| STA= | 746. | 855. | 884. | 903. | 922. | 931. | 941. | 950. | 960. | 970. | 980. | 1010. | 1020. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 3.6 | 4.1 | 5.7 | 3.5 | 3.9 | 4.4 | 4.8 | 5.4 | 5.5 | 29.6 | 5.4 | |
| AREA= | 100.4 | 62.3 | 57.2 | 70.4 | 39.7 | 42.6 | 45.5 | 48.3 | 52.4 | 53.4 | 166.6 | 52.9 | |
| VEL= | 2.9 | 4.5 | 5.5 | 6.3 | 6.8 | 7.2 | 7.5 | 7.8 | 8.0 | 8.1 | 13.9 | 8.1 | |
| DEPTH= | .9 | 2.2 | 3.0 | 3.7 | 4.1 | 4.4 | 4.7 | 5.0 | 5.2 | 5.3 | 5.6 | 5.3 | |

| STA= | 1020. | 1030. | 1039. | 1058. | 1101. | 1141. | 1182. | 1197. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.3 | 3.0 | 3.1 | 3.5 | 3.2 | 3.1 | .2 | |
| AREA= | 45.0 | 36.4 | 48.6 | 72.5 | 67.4 | 66.3 | 7.4 | |
| VEL= | 7.5 | 6.5 | 5.0 | 3.8 | 3.8 | 3.7 | 1.9 | |
| DEPTH= | 4.7 | 3.8 | 2.6 | 1.7 | 1.7 | 1.6 | .5 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .801
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .801 | 7.56 | 2187.56 | 2187.56 | 2187.56 | 2188.83 | 1.27 | 3.67 | .01 | 2182.70 |
| 7820.0 | 179.9 | 2959.6 | 4680.4 | 35.9 | 220.0 | 1019.2 | 87.0 | 33.6 | 2182.50 |
| .12 | 5.01 | 13.45 | 4.59 | .050 | .030 | .050 | .000 | 2180.00 | 952.26 |
| .006555 | 460. | 500. | 540. | 0 | 14 | 0 | .00 | 441.60 | 1393.86 |

FLOW DISTRIBUTION FOR SECNO= .80 CWSEL= 2187.56

| STA= | 952. | 967. | 1002. | 1016. | 1032. | 1061. | 1081. | 1122. | 1166. | 1210. | 1249. | 1291. | 1312. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 2.3 | 37.8 | 3.4 | 3.2 | 5.3 | 3.2 | 6.0 | 6.1 | 4.8 | 4.6 | 5.9 | 3.2 | |
| AREA= | 35.8 | 220.0 | 48.9 | 49.2 | 84.1 | 54.5 | 104.1 | 108.5 | 93.9 | 87.8 | 103.4 | 55.0 | |
| VEL= | 5.0 | 13.5 | 5.4 | 5.1 | 5.0 | 4.6 | 4.5 | 4.4 | 4.0 | 4.1 | 4.4 | 4.5 | |
| DEPTH= | 2.4 | 6.3 | 3.5 | 3.1 | 3.0 | 2.7 | 2.6 | 2.5 | 2.1 | 2.2 | 2.5 | 2.6 | |

| STA= | 1312. | 1331. | 1351. | 1370. | 1382. | 1394. |
|---|---|---|---|---|---|---|
| PER Q= | 3.0 | 3.3 | 3.6 | 3.1 | 1.1 | |
| AREA= | 51.3 | 54.5 | 57.1 | 42.7 | 24.1 | |
| VEL= | 4.6 | 4.8 | 5.0 | 5.6 | 3.7 | |
| DEPTH= | 2.7 | 2.8 | 3.0 | 3.6 | 2.0 | |

*SECNO .898
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .898 | 3.85 | 2193.85 | 2193.85 | 2193.85 | 2194.91 | 1.06 | 5.35 | .02 | 2191.80 |
| 7820.0 | 1952.1 | 769.1 | 5098.8 | 295.5 | 60.5 | 638.5 | 99.6 | 38.7 | 2191.80 |
| .14 | 6.61 | 12.70 | 7.99 | .050 | .030 | .050 | .000 | 2190.00 | 818.44 |
| .022209 | 470. | 510. | 480. | 0 | 11 | 0 | .00 | 482.17 | 1300.60 |

FLOW DISTRIBUTION FOR SECNO= .90 CWSEL= 2193.85

| STA= | 818. | 850. | 871. | 900. | 930. | 955. | 976. | 987. | 1013. | 1036. | 1072. | 1099. | 1129. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.7 | 3.5 | 4.1 | 3.2 | 3.4 | 3.3 | 1.8 | 9.8 | 3.3 | 4.1 | 3.7 | 3.4 | |
| AREA= | 60.2 | 40.4 | 49.6 | 44.0 | 42.5 | 38.5 | 20.3 | 60.5 | 39.4 | 54.8 | 46.0 | 45.1 | |
| VEL= | 7.4 | 6.8 | 6.4 | 5.7 | 6.3 | 6.7 | 6.8 | 12.7 | 6.5 | 5.8 | 6.3 | 5.8 | |
| DEPTH= | 1.9 | 1.9 | 1.7 | 1.5 | 1.7 | 1.9 | 1.9 | 2.3 | 1.8 | 1.5 | 1.7 | 1.5 | |

| STA= | 1129. | 1149. | 1168. | 1186. | 1204. | 1221. | 1241. | 1252. | 1263. | 1274. | 1283. | 1301. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 3.8 | 4.9 | 5.7 | 5.7 | 6.6 | 4.3 | 4.9 | 5.5 | 3.8 | 2.5 | |
| AREA= | 36.7 | 39.8 | 46.2 | 50.4 | 49.9 | 57.2 | 35.2 | 38.0 | 40.7 | 30.2 | 29.1 | |
| VEL= | 6.7 | 7.4 | 8.2 | 8.8 | 8.9 | 9.0 | 9.6 | 10.1 | 10.6 | 9.9 | 6.8 | |
| DEPTH= | 1.8 | 2.2 | 2.5 | 2.8 | 2.9 | 2.9 | 3.2 | 3.5 | 3.7 | 3.4 | 1.7 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .938
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .938 | 4.60 | 2198.10 | 2198.10 | 2198.10 | 2199.25 | 1.15 | 3.53 | .03 | 2194.00 |
| 7820.0 | 1770.3 | 1589.4 | 4460.3 | 245.6 | 109.7 | 760.2 | 105.0 | 41.1 | 2194.00 |
| .15 | 7.21 | 14.49 | 5.87 | .050 | .030 | .050 | .000 | 2193.50 | 907.60 |
| .011943 | 195. | 210. | 235. | 0 | 11 | 0 | .00 | 440.28 | 1347.88 |

FLOW DISTRIBUTION FOR SECNO= .94 CWSEL= 2198.10

| STA= | 908. | 942. | 953. | 963. | 971. | 980. | 986. | 1011. | 1020. | 1030. | 1044. | 1068. | 1118. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.2 | 3.1 | 3.4 | 3.0 | 3.3 | 2.7 | 20.3 | 3.3 | 3.2 | 3.0 | 3.2 | 3.4 | |
| AREA= | 87.7 | 33.7 | 35.9 | 30.8 | 32.2 | 25.3 | 109.7 | 32.6 | 34.5 | 37.6 | 48.1 | 67.4 | |
| VEL= | 6.4 | 7.1 | 7.4 | 7.7 | 8.0 | 8.2 | 14.5 | 8.0 | 7.2 | 6.3 | 5.2 | 4.0 | |
| DEPTH= | 2.5 | 3.2 | 3.4 | 3.7 | 3.8 | 4.0 | 4.4 | 3.8 | 3.3 | 2.7 | 2.0 | 1.3 | |

| STA= | 1118. | 1155. | 1193. | 1220. | 1242. | 1263. | 1285. | 1306. | 1328. | 1348. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 5.1 | 4.4 | 5.8 | 5.4 | 5.1 | 4.8 | 4.6 | 2.4 | |
| AREA= | 57.5 | 76.5 | 61.8 | 65.9 | 63.7 | 61.6 | 59.4 | 57.2 | 36.5 | |
| VEL= | 4.4 | 5.2 | 5.6 | 6.8 | 6.7 | 6.5 | 6.4 | 6.2 | 5.2 | |
| DEPTH= | 1.6 | 2.0 | 2.2 | 3.1 | 3.0 | 2.9 | 2.8 | 2.7 | 1.8 | |

*SECNO 1.012
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.012 | 4.09 | 2204.09 | 2204.09 | 2204.09 | 2205.04 | .96 | 5.53 | .02 | 2201.20 |
| 7820.0 | 1963.9 | 1001.3 | 4854.8 | 249.8 | 72.9 | 817.7 | 115.6 | 45.9 | 2201.20 |
| .16 | 7.86 | 13.73 | 5.94 | .050 | .030 | .050 | .000 | 2200.00 | 902.50 |
| .015744 | 380. | 390. | 420. | 0 | 15 | 0 | .00 | 583.48 | 1485.97 |

FLOW DISTRIBUTION FOR SECNO= 1.01 CWSEL= 2204.09

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 902. | 917. | 927. | 937. | 947. | 961. | 977. | 987. | 1009. | 1025. | 1046. | 1074. | 1104. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 4.3 | 3.7 | 3.1 | 3.7 | 3.7 | 2.6 | 12.8 | 3.7 | 3.1 | 3.7 | 3.1 | |
| AREA= | 39.4 | 37.6 | 34.1 | 30.5 | 39.1 | 41.4 | 27.6 | 72.9 | 41.0 | 41.8 | 51.9 | 47.7 | |
| VEL= | 8.0 | 9.0 | 8.5 | 8.0 | 7.3 | 7.0 | 7.3 | 13.7 | 7.1 | 5.9 | 5.6 | 5.1 | |
| DEPTH= | 2.7 | 3.8 | 3.4 | 3.1 | 2.8 | 2.6 | 2.8 | 3.3 | 2.6 | 2.0 | 1.8 | 1.6 | |

| STA= | 1104. | 1151. | 1190. | 1225. | 1243. | 1262. | 1280. | 1298. | 1315. | 1332. | 1349. | 1372. | 1432. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.8 | 4.3 | 4.9 | 3.2 | 3.6 | 4.0 | 4.3 | 5.0 | 4.6 | 3.3 | 3.0 | 3.0 | |
| AREA= | 73.8 | 64.9 | 66.3 | 40.0 | 43.0 | 45.5 | 47.0 | 51.4 | 48.2 | 39.7 | 42.2 | 60.4 | |
| VEL= | 5.1 | 5.2 | 5.7 | 6.3 | 6.6 | 6.8 | 7.2 | 7.6 | 7.5 | 6.6 | 5.6 | 3.9 | |
| DEPTH= | 1.6 | 1.6 | 1.9 | 2.2 | 2.3 | 2.5 | 2.7 | 2.9 | 2.8 | 2.3 | 1.8 | 1.0 | |

| STA= | 1432. | 1486. |
|---|---|---|
| PER Q= | .3 | |
| AREA= | 12.9 | |
| VEL= | 1.7 | |
| DEPTH= | .2 | |

*SECNO 1.112

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.112 | 5.38 | 2210.88 | 2210.80 | 2210.88 | 2211.99 | 1.11 | 6.90 | .05 | 2207.50 |
| 20.0 | 6145.5 | 1540.2 | 134.3 | 890.6 | 117.9 | 24.3 | 128.0 | 51.9 | 2207.50 |
| .18 | 6.90 | 13.06 | 5.54 | .050 | .030 | .050 | .000 | 2205.50 | 569.59 |
| .012220 | 465. | 530. | 540. | 2 | 11 | 0 | .00 | 452.52 | 1022.12 |

FLOW DISTRIBUTION FOR SECNO= 1.11 CWSEL= 2210.88

| STA= | 570. | 592. | 605. | 629. | 653. | 676. | 698. | 718. | 738. | 775. | 911. | 960. | 975. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.8 | 8.3 | 13.0 | 10.7 | 8.5 | 7.6 | 5.6 | 4.2 | 4.5 | 3.1 | 3.3 | 3.4 | |
| AREA= | 66.3 | 66.7 | 111.1 | 99.1 | 83.9 | 78.3 | 62.6 | 52.6 | 70.1 | 90.6 | 61.8 | 41.1 | |
| VEL= | 6.9 | 9.8 | 9.1 | 8.5 | 7.9 | 7.5 | 7.0 | 6.3 | 5.1 | 2.7 | 4.1 | 6.5 | |
| DEPTH= | 3.0 | 5.1 | 4.6 | 4.1 | 3.7 | 3.5 | 3.1 | 2.6 | 1.9 | .7 | 1.3 | 2.7 | |

| STA= | 975. | 977. | 1009. | 1022. |
|---|---|---|---|---|
| PER Q= | .6 | 19.7 | 1.7 | |
| AREA= | 6.3 | 117.9 | 24.3 | |
| VEL= | 7.3 | 13.1 | 5.5 | |
| DEPTH= | 3.3 | 3.7 | 1.8 | |

*SECNO 1.180

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 620.0 1442.0 TYPE= 1 TARGET= 822.000
ET RECORD: STA 620. ELIMINATE INEFFECTIVE
FLOW AREA IN LEFT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.180 | 4.84 | 2216.84 | 2216.84 | 2216.84 | 2217.76 | .92 | 4.48 | .02 | 2213.50 |
| 7820.0 | 3944.0 | 1167.9 | 2708.1 | 621.3 | 86.7 | 464.1 | 136.6 | 56.3 | 2213.50 |
| .19 | 6.35 | 13.47 | 5.84 | .050 | .030 | .050 | .000 | 2212.00 | 659.36 |
| .014113 | 330. | 360. | 365. | 0 | 15 | 0 | .00 | 658.13 | 1326.11 |

FLOW DISTRIBUTION FOR SECNO= 1.18 CWSEL= 2216.84

| STA= | 659. | 685. | 708. | 722. | 750. | 775. | 793. | 830. | 930. | 950. | 980. | 1005. | 1018. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.2 | 9.7 | 3.1 | 7.2 | 6.4 | 3.0 | 3.9 | 4.2 | 3.1 | 2.5 | 14.9 | 3.8 | |
| AREA= | 72.7 | 88.3 | 36.2 | 79.5 | 71.0 | 40.0 | 61.1 | 88.1 | 41.8 | 42.7 | 86.7 | 40.1 | |
| VEL= | 7.7 | 8.6 | 6.7 | 7.1 | 7.1 | 6.0 | 5.0 | 3.8 | 5.8 | 4.7 | 13.5 | 7.5 | |
| DEPTH= | 2.8 | 3.8 | 2.6 | 2.8 | 2.8 | 2.2 | 1.7 | .9 | 2.1 | 1.4 | 3.5 | 3.1 | |

| STA= | 1018. | 1034. | 1065. | 1180. | 1200. | 1210. | 1220. | 1238. | 1291. | 1326. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.5 | 3.9 | 3.3 | 4.3 | 3.4 | 3.4 | 5.3 | 3.5 | .3 | |
| AREA= | 41.4 | 57.2 | 79.9 | 50.3 | 33.4 | 33.4 | 55.1 | 63.1 | 10.1 | |
| VEL= | 6.7 | 5.4 | 3.2 | 6.6 | 7.9 | 7.9 | 7.5 | 4.4 | 2.0 | |
| DEPTH= | 2.6 | 1.8 | .7 | 2.5 | 3.3 | 3.3 | 3.1 | 1.2 | .3 | |

*SECNO 1.280
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
VULTURE MINE ROAD

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.280 | 3.16 | 2226.16 | 2226.16 | 2226.16 | 2227.19 | 1.03 | 7.55 | .03 | 2223.00 |
| 7820.0 | 2434.4 | 1631.9 | 3753.7 | 387.2 | 126.3 | 589.4 | 150.3 | 63.3 | 2223.00 |
| .21 | 6.29 | 12.92 | 6.37 | .050 | .030 | .050 | .000 | 2223.00 | 791.27 |
| .014670 | 570. | 525. | 480. | 0 | 14 | 0 | .00 | 515.08 | 1306.35 |

FLOW DISTRIBUTION FOR SECNO= 1.28 CWSEL= 2226.16

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 791. | 865. | 980. | 1020. | 1090. | 1190. | 1300. | 1306. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.1 | 27.0 | 20.9 | 20.2 | 21.3 | 6.5 | .0 | |
| AREA= | 81.4 | 305.7 | 126.3 | 210.6 | 250.9 | 127.5 | .5 | |
| VEL= | 4.0 | 6.9 | 12.9 | 7.5 | 6.6 | 4.0 | .7 | |
| DEPTH= | 1.1 | 2.7 | 3.2 | 3.0 | 2.5 | 1.2 | .1 | |

*SECNO 1.353
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.353 | 3.57 | 2233.57 | 2233.57 | 2233.57 | 2234.63 | 1.06 | 5.46 | .01 | 2230.30 |
| 7820.0 | 1647.4 | 1823.7 | 4348.8 | 255.6 | 140.3 | 727.0 | 160.3 | 67.8 | 2230.30 |
| .23 | 6.45 | 13.00 | 5.98 | .050 | .030 | .050 | .000 | 2230.00 | 869.70 |
| .013484 | 365. | 390. | 400. | 0 | 8 | 0 | .00 | 481.83 | 1351.53 |

FLOW DISTRIBUTION FOR SECNO= 1.35 CWSEL= 2233.57

| STA= | 870. | 900. | 923. | 940. | 965. | 977. | 1018. | 1030. | 1041. | 1058. | 1075. | 1093. | 1231. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 3.2 | 4.1 | 7.1 | 3.5 | 23.3 | 3.6 | 3.0 | 3.9 | 3.4 | 3.1 | 20.7 | |
| AREA= | 49.0 | 45.4 | 47.3 | 76.7 | 37.1 | 140.3 | 38.0 | 33.2 | 45.7 | 42.7 | 40.3 | 288.0 | |
| VEL= | 4.9 | 5.5 | 6.8 | 7.3 | 7.4 | 13.0 | 7.4 | 7.1 | 6.7 | 6.3 | 6.0 | 5.6 | |
| DEPTH= | 1.6 | 2.0 | 2.8 | 3.1 | 3.2 | 3.4 | 3.2 | 3.0 | 2.7 | 2.5 | 2.3 | 2.1 | |

| STA= | 1231. | 1256. | 1274. | 1299. | 1317. | 1352. |
|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 3.2 | 4.8 | 3.7 | 2.1 | |
| AREA= | 53.3 | 42.0 | 59.8 | 45.7 | 38.1 | |
| VEL= | 5.8 | 6.0 | 6.2 | 6.3 | 4.3 | |
| DEPTH= | 2.2 | 2.3 | 2.4 | 2.5 | 1.1 | |

*SECNO 1.441
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.441 | 4.11 | 2240.11 | 2240.11 | 2240.11 | 2241.32 | 1.21 | 6.09 | .05 | 2236.50 |
| 7820.0 | 1645.6 | 1656.5 | 4517.8 | 214.5 | 119.5 | 690.8 | 171.6 | 72.5 | 2236.50 |
| .24 | 7.67 | 13.87 | 6.54 | .050 | .030 | .050 | .000 | 2236.00 | 914.10 |
| .012983 | 435. | 460. | 470. | 0 | 8 | 0 | .00 | 408.86 | 1322.97 |

FLOW DISTRIBUTION FOR SECNO= 1.44 CWSEL= 2240.11

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 914. | 981. | 1012. | 1041. | 1052. | 1063. | 1074. | 1085. | 1095. | 1105. | 1115. | 1128. | 1146. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 21.0 | 21.2 | 10.7 | 3.9 | 3.7 | 3.5 | 3.3 | 3.1 | 3.2 | 3.5 | 4.0 | 3.8 | |
| AREA= | 214.5 | 119.5 | 104.8 | 38.6 | 37.5 | 36.4 | 35.3 | 32.9 | 33.1 | 35.1 | 41.7 | 46.6 | |
| VEL= | 7.7 | 13.9 | 8.0 | 7.9 | 7.7 | 7.6 | 7.4 | 7.3 | 7.5 | 7.8 | 7.5 | 6.4 | |
| DEPTH= | 3.2 | 3.9 | 3.6 | 3.5 | 3.4 | 3.3 | 3.2 | 3.2 | 3.3 | 3.5 | 3.3 | 2.6 | |

| STA= | 1146. | 1163. | 1186. | 1213. | 1256. | 1323. |
|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 3.6 | 3.3 | 3.1 | 1.9 | |
| AREA= | 41.2 | 49.4 | 50.6 | 58.3 | 49.3 | |
| VEL= | 6.0 | 5.7 | 5.1 | 4.2 | 2.9 | |
| DEPTH= | 2.4 | 2.2 | 1.9 | 1.3 | .7 | |

*SECNO 1.545

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.545 | 4.96 | 2246.76 | 2246.41 | 2246.76 | 2247.33 | .57 | 5.95 | .06 | 2244.00 |
| 7820.0 | 4791.8 | 1174.4 | 1853.8 | 867.3 | 121.6 | 450.1 | 186.5 | 79.0 | 2244.00 |
| .27 | 5.53 | 9.66 | 4.12 | .050 | .030 | .050 | .000 | 2241.80 | 619.32 |
| 009801 | 605. | 550. | 445. | 4 | 8 | 0 | .00 | 688.12 | 1307.44 |

FLOW DISTRIBUTION FOR SECNO= 1.54 CWSEL= 2246.76

| STA= | 619. | 655. | 671. | 691. | 726. | 738. | 750. | 762. | 774. | 801. | 820. | 841. | 870. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.3 | 3.3 | 3.3 | 4.8 | 4.2 | 4.3 | 4.2 | 3.6 | 4.5 | 3.8 | 3.4 | 3.9 | |
| AREA= | 58.0 | 44.2 | 48.8 | 75.7 | 46.4 | 47.0 | 45.8 | 42.2 | 65.6 | 51.9 | 50.5 | 62.1 | |
| VEL= | 4.4 | 5.8 | 5.3 | 5.0 | 7.2 | 7.2 | 7.1 | 6.7 | 5.3 | 5.7 | 5.3 | 4.8 | |
| DEPTH= | 1.6 | 2.8 | 2.4 | 2.2 | 3.9 | 3.9 | 3.8 | 3.5 | 2.4 | 2.7 | 2.4 | 2.1 | |

| STA= | 870. | 900. | 930. | 953. | 975. | 1019. | 1043. | 1061. | 1094. | 1150. | 1195. | 1255. | 1307. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 3.8 | 3.6 | 4.3 | 15.0 | 3.9 | 3.2 | 3.2 | 4.0 | 3.2 | 3.3 | 2.9 | |
| AREA= | 54.7 | 61.9 | 53.2 | 59.4 | 121.6 | 57.5 | 46.0 | 58.0 | 82.2 | 65.2 | 75.8 | 65.4 | |
| VEL= | 4.4 | 4.8 | 5.2 | 5.6 | 9.7 | 5.4 | 5.5 | 4.3 | 3.8 | 3.8 | 3.4 | 3.4 | |
| DEPTH= | 1.8 | 2.1 | 2.4 | 2.6 | 2.8 | 2.4 | 2.6 | 1.8 | 1.5 | 1.4 | 1.3 | 1.2 | |

*SECNO 1.641

3470 ENCROACHMENT STATIONS= 600.0 1089.0 TYPE= 1 TARGET= 489.000
ET RECORD: STA 600. ELIMINATE INEFFECTIVE
FLOW AREA IN LEFT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| 1.641 | 3.09 | 2252.09 | 2252.01 | 2252.09 | 2253.13 | 1.04 | 5.66 | .14 | 2249.00 |
| 7820.0 | 5237.1 | 2060.7 | 522.2 | 834.7 | 170.1 | 97.5 | 201.0 | 85.6 | 2249.00 |
| .28 | 6.27 | 12.12 | 5.35 | .050 | .030 | .050 | .000 | 2249.00 | 603.03 |
| .013284 | 490. | 510. | 520. | 3 | 14 | 0 | .00 | 460.34 | 1063.36 |

FLOW DISTRIBUTION FOR SECNO= 1.64 CWSEL= 2252.09

| STA= | 603. | 627. | 651. | 666. | 680. | 775. | 799. | 823. | 900. | 923. | 945. | 1000. | 1021. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.4 | 5.9 | 3.8 | 3.3 | 20.4 | 4.8 | 4.2 | 11.6 | 4.0 | 5.5 | 26.4 | 4.5 | |
| AREA= | 47.1 | 67.6 | 42.7 | 39.0 | 246.2 | 59.8 | 55.0 | 161.7 | 52.1 | 63.4 | 170.1 | 54.4 | |
| VEL= | 5.6 | 6.8 | 7.0 | 6.6 | 6.5 | 6.3 | 6.0 | 5.6 | 6.0 | 6.8 | 12.1 | 6.5 | |
| DEPTH= | 2.0 | 2.8 | 2.9 | 2.7 | 2.6 | 2.5 | 2.3 | 2.1 | 2.3 | 2.8 | 3.1 | 2.6 | |

| STA= | 1021. | 1063. |
|---|---|---|
| PER Q= | 2.2 | |
| AREA= | 43.1 | |
| VEL= | 3.9 | |
| DEPTH= | 1.0 | |

O 1.725

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 795.0 1170.0 TYPE= 1 TARGET= 375.000
ET RECORD: STA 795. ELIMINATE INEFFECTIVE
FLOW AREA IN LEFT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.725 | 4.91 | 2259.91 | 2259.91 | 2259.91 | 2261.48 | 1.58 | 4.90 | .16 | 2255.50 |
| 7820.0 | 2698.3 | 3577.7 | 1544.0 | 447.2 | 270.1 | 232.0 | 211.6 | 89.4 | 2255.50 |
| .30 | 6.03 | 13.25 | 6.66 | .050 | .030 | .050 | .000 | 2255.00 | 806.05 |
| .009197 | 460. | 440. | 420. | 0 | 14 | 0 | .00 | 290.79 | 1096.85 |

FLOW DISTRIBUTION FOR SECNO= 1.73 CWSEL= 2259.91

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 806. | 890. | 910. | 931. | 951. | 960. | 970. | 1028. | 1039. | 1050. | 1061. | 1071. | 1082. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 11.6 | 4.7 | 5.2 | 5.7 | 3.4 | 4.0 | 45.8 | 4.3 | 3.5 | 3.2 | 3.4 | 3.6 | |
| AREA= | 172.9 | 61.3 | 65.4 | 68.7 | 37.5 | 41.3 | 270.1 | 45.7 | 40.2 | 37.5 | 38.8 | 40.7 | |
| VEL= | 5.2 | 5.9 | 6.2 | 6.5 | 7.1 | 7.5 | 13.2 | 7.4 | 6.8 | 6.6 | 6.8 | 6.9 | |
| DEPTH= | 2.1 | 3.0 | 3.2 | 3.5 | 3.9 | 4.3 | 4.7 | 4.2 | 3.7 | 3.5 | 3.7 | 3.8 | |

| STA= | 1082. | 1097. |
|---|---|---|
| PER Q= | 1.8 | |
| AREA= | 29.0 | |
| VEL= | 4.9 | |
| DEPTH= | 2.0 | |

*SECNO 1.829

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.829 | 4.35 | 2267.35 | 2267.35 | 2267.35 | 2268.42 | 1.07 | 4.41 | .05 | 2263.00 |
| 7820.0 | 1129.3 | 4402.5 | 2288.1 | 322.0 | 421.3 | 528.5 | 225.7 | 95.2 | 2263.00 |
| .32 | 3.51 | 10.45 | 4.33 | .050 | .030 | .050 | .000 | 2263.00 | 656.79 |
| 006983 | 570. | 550. | 540. | 0 | 15 | 0 | .00 | 606.21 | 1263.00 |

FLOW DISTRIBUTION FOR SECNO= 1.83 CWSEL= 2267.35

| STA= | 657. | 781. | 827. | 883. | 895. | 1000. | 1012. | 1030. | 1049. | 1069. | 1098. | 1129. | 1160. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.6 | 3.8 | 3.7 | 3.3 | 56.3 | 3.6 | 3.7 | 3.4 | 3.1 | 4.1 | 3.8 | 3.2 | |
| AREA= | 110.2 | 80.5 | 86.3 | 45.0 | 421.3 | 46.2 | 55.4 | 53.8 | 51.7 | 71.3 | 69.5 | 62.1 | |
| VEL= | 2.5 | 3.7 | 3.4 | 5.8 | 10.5 | 6.1 | 5.3 | 4.9 | 4.8 | 4.5 | 4.3 | 4.0 | |
| DEPTH= | .9 | 1.8 | 1.6 | 3.6 | 4.0 | 3.9 | 3.1 | 2.8 | 2.6 | 2.5 | 2.3 | 2.0 | |

| STA= | 1160. | 1230. | 1263. |
|---|---|---|---|
| PER Q= | 3.3 | 1.0 | |
| AREA= | 87.6 | 30.9 | |
| VEL= | 3.0 | 2.6 | |
| DEPTH= | 1.2 | .9 | |

*SECNO 1.918

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.918 | 5.71 | 2274.71 | 2274.71 | 2274.71 | 2276.63 | 1.93 | 3.24 | .26 | 2269.30 |
| 7820.0 | 1624.4 | 5507.8 | 687.8 | 294.0 | 431.4 | 119.2 | 237.4 | 100.0 | 2269.30 |
| .33 | 5.53 | 12.77 | 5.77 | .050 | .030 | .050 | .000 | 2269.00 | 811.68 |
| .006619 | 560. | 470. | 420. | 0 | 11 | 0 | .00 | 249.57 | 1061.25 |

FLOW DISTRIBUTION FOR SECNO= 1.92 CWSEL= 2274.71

| STA= | 812. | 882. | 902. | 913. | 922. | 931. | 1008. | 1015. | 1031. | 1061. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 3.8 | 4.2 | 4.4 | 4.6 | 70.4 | 3.7 | 4.4 | .6 | |
| AREA= | 89.2 | 59.1 | 50.1 | 47.3 | 48.2 | 431.4 | 39.8 | 59.3 | 20.1 | |
| VEL= | 3.3 | 5.0 | 6.6 | 7.3 | 7.4 | 12.8 | 7.4 | 5.9 | 2.4 | |
| DEPTH= | 1.3 | 3.0 | 4.6 | 5.3 | 5.4 | 5.6 | 5.3 | 3.7 | .7 | |

*SECNO 2.011
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.011 | 7.29 | 2282.29 | 2282.29 | 2282.29 | 2284.17 | 1.88 | 2.84 | .01 | 2276.00 |
| 7820.0 | 2159.6 | 5429.9 | 230.5 | 464.4 | 423.4 | 47.1 | 247.4 | 103.0 | 2276.00 |
| .34 | 4.65 | 12.82 | 4.90 | .050 | .030 | .050 | .000 | 2275.00 | 737.14 |
| .005101 | 490. | 490. | 495. | 0 | 11 | 0 | .00 | 288.81 | 1025.95 |

FLOW DISTRIBUTION FOR SECNO= 2.01 CWSEL= 2282.29

| STA= | 737. | 803. | 860. | 922. | 939. | 950. | 1011. | 1026. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.2 | 3.1 | 4.1 | 7.6 | 5.7 | 69.4 | 2.9 | |
| AREA= | 141.6 | 79.5 | 87.4 | 93.1 | 62.9 | 423.4 | 47.1 | |
| VEL= | 4.0 | 3.0 | 3.7 | 6.4 | 7.0 | 12.8 | 4.9 | |
| DEPTH= | 2.1 | 1.4 | 1.4 | 5.2 | 6.0 | 6.9 | 3.1 | |

CCHV= .300 CEHV= .500
*SECNO 2.056

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.056 | 7.74 | 2284.24 | 2284.24 | 2284.24 | 2286.88 | 2.65 | 1.38 | .38 | 2278.50 |
| 7820.0 | 384.7 | 6543.3 | 892.0 | 78.8 | 466.7 | 139.0 | 251.7 | 104.1 | 2276.50 |
| .35 | 4.89 | 14.02 | 6.42 | .050 | .030 | .050 | .000 | 2276.50 | 899.05 |
| .006821 | 215. | 240. | 240. | 0 | 8 | 0 | .00 | 142.70 | 1041.74 |

FLOW DISTRIBUTION FOR SECNO= 2.06 CWSEL= 2284.24

| STA= | 899. | 927. | 1000. | 1012. | 1020. | 1028. | 1037. | 1042. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.9 | 83.7 | 7.2 | 2.2 | 1.3 | .5 | .0 | |
| AREA= | 78.8 | 466.7 | 71.8 | 29.9 | 21.9 | 13.2 | 2.2 | |
| VEL= | 4.9 | 14.0 | 7.9 | 5.9 | 4.8 | 3.2 | 1.4 | |
| DEPTH= | 2.9 | 6.3 | 6.0 | 3.7 | 2.7 | 1.5 | .4 | |

*SECNO 2.107

3301 HV CHANGED MORE THAN HVINS

MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.107 | 7.31 | 2287.31 | 2287.31 | 2287.31 | 2290.52 | 3.20 | 1.82 | .28 | 2280.50 |
| 6943.0 | 248.8 | 6530.5 | 163.7 | 43.3 | 442.9 | 31.2 | 255.4 | 104.8 | 2280.00 |
| .35 | 5.74 | 14.74 | 5.25 | .050 | .030 | .050 | .000 | 2280.00 | 952.21 |
| .006719 | 275. | 270. | 240. | 0 | 11 | 0 | .00 | 85.32 | 1037.53 |

FLOW DISTRIBUTION FOR SECNO= 2.11 CWSEL= 2287.31

| STA= | 952. | 957. | 965. | 1029. | 1036. | 1038. |
|---|---|---|---|---|---|---|
| PER Q= | .2 | 3.4 | 94.1 | 2.3 | .0 | |
| AREA= | 6.0 | 37.3 | 442.9 | 30.2 | 1.0 | |
| VEL= | 2.6 | 6.2 | 14.7 | 5.4 | 1.5 | |
| DEPTH= | 1.3 | 4.7 | 6.9 | 4.3 | .7 | |

CCHV= .300 CEHV= .500
*SECNO 2.109
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2299.20 ELREA= 2297.50

DOWNSTREAM FACE OF US HWY 60 CONC BRIDGE (STRUCTURE AB-2)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.109 | 7.28 | 2289.38 | 2289.38 | 2289.38 | 2293.07 | 3.68 | .04 | .24 | 2282.10 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 450.9 | .0 | 255.5 | 104.8 | 2282.10 |
| .35 | .00 | 15.40 | .00 | .000 | .020 | .000 | .000 | 2282.10 | 968.10 |
| .003041 | 10. | 10. | 10. | 0 | 5 | 0 | .00 | 61.90 | 1030.00 |

FLOW DISTRIBUTION FOR SECNO= 2.11 CWSEL= 2289.38

STA= 968. 1030.
PER Q= 100.0
AREA= 450.9
VEL= 15.4
DEPTH= 7.3

SPECIAL BRIDGE

DOWNSTREAM ELEV IS 2288.56 , NOT 2289.38 HYDRAULIC JUMP OCCURS DOWNSTREAM (IF LOW FLOW CONTROLS)

| SB | XK | XKOR | COFQ | RDLEN | BWC | BWP | BAREA | SS | ELCHU | ELCHD |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1.25 | 1.56 | 2.80 | .00 | 61.90 | 1.50 | 845.60 | .00 | 2282.10 | 2282.10 |

*SECNO 2.118

3301 HV CHANGED MORE THAN HVINS

CLASS B LOW FLOW

3420 BRIDGE W.S.= 2289.53 BRIDGE VELOCITY= 15.47 CALCULATED CHANNEL AREA= 449.

| EGPRS | EGLWC | H3 | QWEIR | QLOW | BAREA | TRAPEZOID AREA | ELLC | ELTRD | WEIRLN |
|---|---|---|---|---|---|---|---|---|---|
| .00 | 2293.39 | .00 | 0. | 6943. | 846. | 846. | 2296.10 | 2297.50 | 0. |

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2299.20 ELREA= 2297.50

UPSTREAM FACE OF US HWY 60 CONC BRIDGE (STRUCTURE AB-2)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.118 | 8.73 | 2290.83 | .00 | 2290.83 | 2293.39 | 2.56 | .33 | .00 | 2282.10 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 540.5 | .0 | 256.0 | 104.9 | 2282.10 |
| .36 | .00 | 12.84 | .00 | .000 | .020 | .000 | .000 | 2282.10 | 968.10 |
| 01662 | 45. | 45. | 45. | 0 | 0 | 0 | .00 | 61.90 | 1030.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 2.12 CWSEL= 2290.83

STA= 968. 1030.
PER Q= 100.0
AREA= 540.5
VEL= 12.8
DEPTH= 8.7

*SECNO 2.120

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2297.00 ELREA= 2297.50

DOWNSTREAM FACE OF OLD US HWY 60 CONC BRIDGE (STRUCTURE AB-1)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.120 | 8.57 | 2290.67 | 2289.63 | 2290.67 | 2293.60 | 2.93 | .02 | .18 | 2282.10 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 505.5 | .0 | 256.2 | 104.9 | 2282.10 |
| .36 | .00 | 13.74 | .00 | .000 | .020 | .000 | .000 | 2282.10 | 970.50 |
| .001949 | 10. | 10. | 10. | 2 | 11 | 0 | .00 | 59.00 | 1029.50 |

FLOW DISTRIBUTION FOR SECNO= 2.12 CWSEL= 2290.67

STA= 971. 1030.
PER Q= 100.0
AREA= 505.5
VEL= 13.7
DEPTH= 8.6

SPECIAL BRIDGE

5227 DOWNSTREAM ELEV IS 2288.42 , NOT 2290.67 HYDRAULIC JUMP OCCURS DOWNSTREAM (IF LOW FLOW CONTROLS)

| SB | XK | XKOR | COFQ | RDLEN | BWC | BWP | BAREA | SS | ELCHU | ELCHD |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1.25 | 1.56 | 2.80 | .00 | 59.00 | 3.00 | 588.00 | .00 | 2282.70 | 2282.10 |

*SECNO 2.125

3301 HV CHANGED MORE THAN HVINS

CLASS B LOW FLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3420 BRIDGE W.S.= 2290.21 BRIDGE VELOCITY= 15.87 CALCULATED CHANNEL AREA= 421.

| EGPRS | EGLWC | H3 | QWEIR | QLOW | BAREA | TRAPEZOID AREA | ELLC | ELTRD | WEIRLN |
|---|---|---|---|---|---|---|---|---|---|
| 2294.04 | 2294.71 | .00 | 0. | 6943. | 588. | 588. | 2293.20 | 2297.00 | 0. |

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2297.00 ELREA= 2297.50

UPSTREAM FACE OF OLD US HWY 60 CONC BRIDGE (STRUCTURE AB-1)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.125 | 9.75 | 2292.45 | .00 | 2292.45 | 2294.71 | 2.26 | 1.11 | .00 | 2282.70 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 575.0 | .0 | 256.5 | 104.9 | 2282.70 |
| .36 | .00 | 12.07 | .00 | .000 | .020 | .000 | .000 | 2282.70 | 970.50 |
| .001269 | 30. | 30. | 30. | 0 | 0 | 0 | .00 | 59.00 | 1029.50 |

FLOW DISTRIBUTION FOR SECNO= 2.13 CWSEL= 2292.45

971. 1030.
Q= 100.0
AREA= 575.0
VEL= 12.1
DEPTH= 9.7

CCHV= .100 CEHV= .300
*SECNO 2.213

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.213 | 8.58 | 2298.08 | 2298.08 | 2298.08 | 2299.32 | 1.24 | .93 | .10 | 2292.00 |
| 6943.0 | 2126.3 | 3965.4 | 851.3 | 573.4 | 345.5 | 352.6 | 266.3 | 108.5 | 2292.50 |
| .37 | 3.71 | 11.48 | 2.41 | .050 | .030 | .050 | .000 | 2289.50 | 759.60 |
| .003646 | 415. | 465. | 525. | 0 | 9 | 0 | .00 | 587.76 | 1347.36 |

FLOW DISTRIBUTION FOR SECNO= 2.21 CWSEL= 2298.08

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| CNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 760. | 801. | 815. | 830. | 858. | 897. | 943. | 963. | 976. | 982. | 1028. | 1041. | 1086. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.3 | 4.1 | 3.2 | 3.5 | 3.4 | 3.3 | 3.2 | 3.7 | 2.9 | 57.1 | 4.0 | 3.0 | |
| AREA= | 72.9 | 60.9 | 52.6 | 71.5 | 80.2 | 85.0 | 59.1 | 55.0 | 36.3 | 345.5 | 58.3 | 77.9 | |
| VEL= | 3.2 | 4.7 | 4.2 | 3.4 | 2.9 | 2.7 | 3.8 | 4.7 | 5.6 | 11.5 | 4.8 | 2.7 | |
| DEPTH= | 1.8 | 4.3 | 3.6 | 2.6 | 2.1 | 1.8 | 3.0 | 4.2 | 5.6 | 7.6 | 4.3 | 1.7 | |

| STA= | 1086. | 1227. | 1347. |
|---|---|---|---|
| PER Q= | 3.0 | 2.2 | |
| AREA= | 121.7 | 94.7 | |
| VEL= | 1.7 | 1.6 | |
| DEPTH= | .9 | .8 | |

*SECNO 2.248
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.248 | 8.02 | 2300.02 | 2300.02 | 2300.02 | 2301.06 | 1.04 | .72 | .02 | 2296.00 |
| 6943.0 | 2931.1 | 3023.5 | 988.4 | 643.5 | 264.0 | 352.6 | 271.4 | 111.0 | 2296.50 |
| .38 | 4.56 | 11.45 | 2.80 | .050 | .030 | .050 | .000 | 2292.00 | 776.15 |
| .004910 | 130. | 180. | 245. | 0 | 10 | 0 | .00 | 528.24 | 1304.39 |

DISTRIBUTION FOR SECNO= 2.25 CWSEL= 2300.02

| STA= | 776. | 812. | 831. | 846. | 862. | 877. | 892. | 908. | 931. | 972. | 988. | 1031. | 1046. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 5.7 | 5.0 | 4.5 | 3.9 | 3.4 | 3.0 | 3.7 | 5.8 | 3.4 | 43.5 | 3.0 | |
| AREA= | 70.6 | 75.3 | 63.7 | 60.4 | 55.4 | 51.5 | 47.7 | 63.2 | 103.5 | 52.0 | 264.0 | 46.9 | |
| VEL= | 3.6 | 5.3 | 5.5 | 5.2 | 4.9 | 4.6 | 4.4 | 4.1 | 3.9 | 4.6 | 11.5 | 4.5 | |
| DEPTH= | 1.9 | 4.0 | 4.2 | 3.9 | 3.6 | 3.3 | 3.1 | 2.7 | 2.5 | 3.2 | 6.1 | 3.1 | |

| STA= | 1046. | 1077. | 1134. | 1261. | 1304. |
|---|---|---|---|---|---|
| PER Q= | 3.4 | 3.3 | 4.0 | .6 | |
| AREA= | 67.2 | 83.6 | 130.6 | 24.4 | |
| VEL= | 3.5 | 2.7 | 2.1 | 1.6 | |
| DEPTH= | 2.2 | 1.5 | 1.0 | .6 | |

*SECNO 2.342

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3470 ENCROACHMENT STATIONS= 940.0 1475.0 TYPE= 1 TARGET= 535.000

ET RECORD: STA 1475. ELIMINATE INEFFECTIVE

FLOW AREA IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.342 | 8.96 | 2305.96 | 2305.96 | 2305.96 | 2307.72 | 1.76 | 2.18 | .22 | 2298.00 |
| 6943.0 | 810.9 | 4370.5 | 1761.7 | 131.1 | 337.7 | 467.9 | 283.6 | 115.6 | 2298.00 |
| .39 | 6.19 | 12.94 | 3.77 | .050 | .030 | .050 | .000 | 2297.00 | 946.06 |
| .003978 | 515. | 500. | 450. | 0 | 8 | 0 | .00 | 325.44 | 1271.50 |

FLOW DISTRIBUTION FOR SECNO= 2.34 CWSEL= 2305.96

| STA= | 946. | 963. | 970. | 1010. | 1020. | 1030. | 1048. | 1075. | 1109. | 1165. | 1271. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.9 | 5.7 | 62.9 | 6.8 | 3.8 | 3.8 | 3.0 | 3.3 | 3.2 | 1.5 | |
| AREA= | 75.1 | 56.0 | 337.7 | 69.6 | 49.6 | 60.6 | 63.7 | 73.5 | 86.4 | 64.4 | |
| VEL= | 5.5 | 7.1 | 12.9 | 6.7 | 5.4 | 4.3 | 3.3 | 3.1 | 2.5 | 1.6 | |
| DEPTH= | 4.6 | 7.5 | 8.4 | 7.0 | 5.0 | 3.5 | 2.3 | 2.1 | 1.6 | .6 | |

*SECNO 2.435

MINIMUM SPECIFIC ENERGY

CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 952.0 1228.0 TYPE= 1 TARGET= 276.000

CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH

ET RECORD: STA 1288. ELIMINATE INEFFECTIVE

FLOW AREA IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.435 | 6.34 | 2309.84 | 2309.84 | 2309.84 | 2311.91 | 2.07 | 2.67 | .09 | 2304.00 |
| 6943.0 | 826.9 | 3276.8 | 2839.3 | 122.1 | 218.3 | 393.2 | 292.7 | 118.3 | 2304.00 |
| .40 | 6.77 | 15.01 | 7.22 | .050 | .030 | .050 | .000 | 2303.50 | 957.71 |
| .008304 | 500. | 490. | 455. | 0 | 19 | 0 | .00 | 180.38 | 1138.09 |

FLOW DISTRIBUTION FOR SECNO= 2.43 CWSEL= 2309.84

| STA= | 958. | 976. | 991. | 1027. | 1037. | 1047. | 1057. | 1067. | 1077. | 1092. | 1102. | 1138. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 8.1 | 47.2 | 7.1 | 6.5 | 5.9 | 5.3 | 4.8 | 6.1 | 3.1 | 2.2 | |
| AREA= | 49.5 | 72.6 | 218.3 | 56.9 | 53.9 | 50.9 | 47.9 | 44.9 | 61.3 | 34.4 | 43.0 | |
| VEL= | 5.4 | 7.7 | 15.0 | 8.6 | 8.3 | 8.0 | 7.7 | 7.4 | 6.9 | 6.2 | 3.6 | |
| DEPTH= | 2.7 | 4.8 | 6.1 | 5.7 | 5.4 | 5.1 | 4.8 | 4.5 | 4.1 | 3.4 | 1.2 | |

RIGHT BANK LEVEE BETWEEN SECTIONS 0.134 & 0.160

| ASQ | QCOMP | ERRAC | TASQ | TCQ | TABER | NITER | DSWS | USWS | DSSNO | USSNO |
|---|---|---|---|---|---|---|---|---|---|---|
| 1243.40 | 1243.89 | .04 | 1243.40 | 1243.89 | .04 | 7 | 2139.404 | 2140.919 | .134 | .160 |

TW RIGHT BANK LEVEE BETWEEN SECTIONS 0.160 & 0.220

| ASQ | QCOMP | ERRAC | TASQ | TCQ | TABER | NITER | DSWS | USWS | DSSNO | USSNO |
|---|---|---|---|---|---|---|---|---|---|---|
| 3574.16 | 3574.18 | .00 | 4817.56 | 4818.07 | .01 | 7 | 2140.919 | 2144.661 | .160 | .220 |

FLOODWAY DETERMINATION
1.0 FT TARGET INCREASE
T3 WASH AB: FLYING E WASH

| J1 | ICHECK | INQ | NINV | IDIR | STRT | METRIC | HVINS | Q | WSEL | FQ |
|---|---|---|---|---|---|---|---|---|---|---|
| | | 3 | | | | | | | 2134.50 | |

| J2 | NPROF | IPLOT | PRFVS | XSECV | XSECH | FN | ALLDC | IBW | CHNIM | ITRACE |
|---|---|---|---|---|---|---|---|---|---|---|
| | 15 | | -1 | | | | -1 | | | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*PROF 2

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS
0

CCHV= .100 CEHV= .300
*SECNO .095

3470 ENCROACHMENT STATIONS= 905.0 1026.3 TYPE= 1 TARGET= 121.310
CONFLUENCE OF WASH AB: FLYING E WASH
AND SOLS WASH BETWEEN CROSS-SECTIONS
V (SOLS WASH RIVER MILE 1.97)
W (SOLS WASH RIVER MILE 2.06)
CROSS-SECTION DESIGNATION FROM
SOLS WASH FLOODPLAIN DLINEATION
HASSAYAMPA RIVER TO MARICOPA COUNTY LINE
CELLA BARR ASSOCIATES

SWSE DETERMINED BY SLOPE AREA METHOD

SPLIT FLOW OPTION USED FROM XSECT 0.134 TO XSECT 0.220
TO MODEL OVERFLOW LEVEE IN RIGHT OVERBANK. THE PROGRAM
WILL USE THE ENERGY GRADE LINE TO DETERMINE OVERFLOW.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .095 | 3.50 | 2134.50 | 2134.48 | 2134.50 | 2135.94 | 1.44 | .00 | .00 | 2132.00 |
| 3002.5 | 23.5 | 2899.8 | 79.2 | 10.0 | 296.5 | 21.3 | .0 | .0 | 2132.00 |
| .00 | 2.37 | 9.78 | 3.71 | .050 | .030 | .050 | .000 | 2131.00 | 905.00 |
| .008120 | 0. | 0. | 0. | 0 | 4 | 0 | .00 | 121.31 | 1026.31 |

CCHV= .300 CEHV= .500
*SECNO .125
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 885.0 1012.9 TYPE= 1 TARGET= 127.870

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .125 | 3.42 | 2136.42 | 2136.42 | 2136.42 | 2137.76 | 1.34 | 1.38 | .03 | 2134.00 |
| 3002.5 | 72.7 | 2924.8 | 5.0 | 17.6 | 311.3 | 2.1 | 1.2 | .4 | 2134.00 |
| .00 | 4.12 | 9.40 | 2.41 | .050 | .030 | .050 | .000 | 2133.00 | 885.00 |
| .009225 | 130. | 160. | 160. | 0 | 8 | 0 | .00 | 127.87 | 1012.87 |

*SECNO .131

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.29

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2139.90 ELREA= 2139.40

DS FACE: AT&SF RAILROAD BRIDGE (STRUCTURE AB-3)

NOTE: CENTERLINE SECTION OF AT&SF RAILROAD WAS
USED TO CREATE THE DS FACE CROSS-SECTION

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .131 | 4.10 | 2137.70 | 2136.05 | 2137.70 | 2138.14 | .44 | .10 | .27 | 2133.60 |
| 3002.5 | .0 | 3002.5 | .0 | .0 | 565.0 | .0 | 1.5 | .5 | 2133.60 |
| .01 | .00 | 5.31 | .00 | .000 | .030 | .000 | .000 | 2133.60 | 875.00 |
| .001757 | 30. | 30. | 30. | 3 | 15 | 0 | .00 | 138.00 | 1013.00 |

AL BRIDGE

| SB | XK | XKOR | COFQ | RDLEN | BWC | BWP | BAREA | SS | ELCHU | ELCHD |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1.05 | 1.83 | 2.80 | .00 | 138.00 | 9.00 | 387.00 | .00 | 2133.70 | 2133.60 |

*SECNO .134

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.61

PRESSURE AND WEIR FLOW, Weir Submergence Based on TRAPEZOIDAL Shape

| EGPRS | EGLWC | H3 | QWEIR | QPR | BAREA | TRAPEZOID AREA | ELLC | ELTRD | WEIRLN |
|---|---|---|---|---|---|---|---|---|---|
| 2139.41 | 2138.23 | .09 | 0. | 2999. | 387. | 387. | 2136.70 | 2139.40 | 1. |

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2139.90 ELREA= 2139.40

US FACE: AT&SF RAILROAD BRIDGE (STRUCTURE AB-3)

NOTE: CENTERLINE SECTION OF AT&SF RAILROAD WAS
USED TO CREATE THE US FACE CROSS-SECTION

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .134 | 5.46 | 2139.16 | .00 | 2139.16 | 2139.40 | .25 | 1.27 | .00 | 2133.70 |
| 3002.5 | .0 | 3002.5 | .0 | .0 | 753.2 | .0 | 1.7 | .6 | 2133.70 |
| .01 | .00 | 3.99 | .00 | .000 | .030 | .000 | .000 | 2133.70 | 875.00 |
| 00674 | 15. | 15. | 15. | 2 | 0 | 0 | .00 | 138.00 | 1013.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .160

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 730.0 1048.0 TYPE= 1 TARGET= 318.000
ET RECORD: STATION 730. MODEL 1 TO 1
FLOW CONTRACTION UPSTREAM
OF AT&SF BRIDGE

ET RECORD: STATION 1048. TOP OF OVERFLOW
LEVEE IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .160 | 3.85 | 2139.85 | 2139.85 | 2139.85 | 2140.92 | 1.07 | .27 | .41 | 2136.60 |
| 4245.8 | 1326.5 | 2583.7 | 335.7 | 336.0 | 255.3 | 78.3 | 4.0 | 1.3 | 2136.50 |
| .01 | 3.95 | 10.12 | 4.29 | .050 | .030 | .050 | .000 | 2136.00 | 730.00 |
| .007419 | 140. | 140. | 140. | 0 | 19 | 0 | .00 | 318.00 | 1048.00 |

.100 CEHV= .300
*SECNO .220
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 435.0 1092.5 TYPE= 1 TARGET= 657.540
ET RECORD: STATION 1092.5 TOP OF OVERFLOW
LEVEE IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .220 | 3.27 | 2143.77 | 2143.77 | 2143.77 | 2144.66 | .89 | 3.13 | .02 | 2141.00 |
| 7820.0 | 5007.2 | 2254.5 | 558.3 | 962.5 | 195.4 | 112.8 | 10.7 | 4.7 | 2141.00 |
| .02 | 5.20 | 11.54 | 4.95 | .050 | .030 | .050 | .000 | 2140.50 | 434.96 |
| .012504 | 295. | 315. | 320. | 0 | 15 | 0 | .00 | 657.54 | 1092.50 |

*SECNO .256
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 570.0 1085.0 TYPE= 1 TARGET= 514.960

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .256 | 4.38 | 2147.38 | 2147.38 | 2147.39 | 2148.43 | 1.05 | 2.16 | .05 | 2143.00 |
| 7820.0 | 4730.5 | 2231.2 | 858.3 | 915.0 | 171.0 | 168.6 | 16.5 | 7.4 | 2143.00 |
| .03 | 5.17 | 13.05 | 5.09 | .050 | .030 | .050 | .000 | 2143.00 | 570.00 |
| .009672 | 200. | 190. | 200. | 0 | 14 | 0 | .00 | 514.96 | 1084.96 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .351
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 800.0 1110.0 TYPE= 1 TARGET= 310.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .351 | 4.78 | 2153.78 | 2153.78 | 2153.78 | 2155.31 | 1.53 | 4.09 | .14 | 2149.00 |
| 7820.0 | 1915.5 | 4778.1 | 1126.4 | 360.1 | 397.0 | 253.7 | 29.1 | 11.9 | 2149.00 |
| .05 | 5.32 | 12.03 | 4.44 | .050 | .030 | .050 | .000 | 2149.00 | 800.00 |
| .007322 | 470. | 500. | 505. | 0 | 8 | 0 | .00 | 310.00 | 1110.00 |

*SECNO .460
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 973.5 1183.0 TYPE= 1 TARGET= 209.450

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .460 | 5.71 | 2161.21 | 2161.21 | 2161.21 | 2163.12 | 1.91 | 4.95 | .12 | 2156.00 |
| 7820.0 | 112.7 | 2895.3 | 4812.0 | 22.2 | 187.2 | 646.1 | 41.6 | 15.4 | 2156.00 |
| .06 | 5.07 | 15.47 | 7.45 | .050 | .030 | .050 | .000 | 2155.50 | 973.77 |
| .010035 | 580. | 575. | 590. | 0 | 11 | 0 | .00 | 209.23 | 1183.00 |

*SECNO .540
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 822.8 1082.0 TYPE= 1 TARGET= 259.200

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .540 | 4.20 | 2166.20 | 2166.20 | 2166.20 | 2167.84 | 1.64 | 4.31 | .03 | 2162.20 |
| 7820.0 | 3771.2 | 1985.9 | 2062.9 | 459.4 | 132.5 | 264.8 | 48.4 | 17.3 | 2162.40 |
| .07 | 8.21 | 14.99 | 7.79 | .050 | .030 | .050 | .000 | 2162.00 | 822.80 |
| .014576 | 390. | 425. | 295. | 0 | 19 | 0 | .00 | 259.20 | 1082.00 |

*SECNO .576
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 717.5 1028.9 TYPE= 1 TARGET= 311.480

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .576 | 4.40 | 2169.20 | 2169.20 | 2169.20 | 2170.67 | 1.48 | 2.47 | .02 | 2164.90 |
| 7820.0 | 4566.5 | 2493.5 | 760.0 | 670.7 | 177.9 | 100.5 | 52.3 | 18.5 | 2164.90 |
| .08 | 6.81 | 14.02 | 7.56 | .050 | .030 | .050 | .000 | 2164.80 | 717.60 |
| .011581 | 200. | 190. | 165. | 0 | 8 | 0 | .00 | 311.33 | 1028.93 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .640

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 690.5 1121.6 TYPE= 1 TARGET= 431.110

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .640 | 4.67 | 2174.17 | 2174.17 | 2174.17 | 2175.47 | 1.30 | 3.89 | .02 | 2169.80 |
| 7820.0 | 3481.1 | 1906.2 | 2432.6 | 537.1 | 134.6 | 338.3 | 60.1 | 21.3 | 2169.80 |
| .09 | 6.48 | 14.16 | 7.19 | .050 | .030 | .050 | .000 | 2169.50 | 690.54 |
| .010947 | 350. | 340. | 340. | 0 | 8 | 0 | .00 | 393.34 | 1121.64 |

*SECNO .707
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 746.0 1196.8 TYPE= 1 TARGET= 450.800

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .707 | 5.68 | 2181.68 | 2181.68 | 2181.68 | 2182.93 | 1.25 | 3.17 | .01 | 2176.30 |
| 7820.0 | 3481.1 | 2313.1 | 2025.7 | 571.5 | 166.5 | 396.1 | 68.5 | 24.6 | 2176.30 |
| .10 | 6.09 | 13.89 | 5.11 | .050 | .030 | .050 | .000 | 2176.00 | 746.14 |
| .008011 | 320. | 350. | 365. | 0 | 11 | 0 | .00 | 450.65 | 1196.78 |

*SECNO .801
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 952.3 1393.9 TYPE= 1 TARGET= 441.600

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .801 | 7.56 | 2187.56 | 2187.56 | 2187.56 | 2188.83 | 1.27 | 3.67 | .00 | 2182.70 |
| 7820.0 | 179.9 | 2957.8 | 4682.2 | 36.0 | 220.1 | 1020.2 | 82.7 | 29.9 | 2182.50 |
| .12 | 5.01 | 13.44 | 4.59 | .050 | .030 | .050 | .000 | 2180.00 | 952.26 |
| .006538 | 460. | 500. | 540. | 0 | 14 | 0 | .00 | 441.60 | 1393.86 |

*SECNO .898
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 818.4 1300.6 TYPE= 1 TARGET= 482.160

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .898 | 3.85 | 2193.85 | 2193.85 | 2193.85 | 2194.91 | 1.06 | 5.34 | .02 | 2191.80 |
| 7820.0 | 1952.2 | 769.1 | 5098.7 | 295.6 | 60.5 | 638.6 | 95.3 | 35.0 | 2191.80 |
| .14 | 6.60 | 12.70 | 7.98 | .050 | .030 | .050 | .000 | 2190.00 | 818.44 |
| .022200 | 470. | 510. | 480. | 0 | 11 | 0 | .00 | 482.16 | 1300.60 |

```
 SECNO     DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
 Q         QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
 TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
 SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


*SECNO  .938
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      907.6    1347.9  TYPE=      1  TARGET=      440.280
      .938      4.60   2198.10   2198.10   2198.10   2199.25      1.15      3.53       .03   2194.00
    7820.0    1770.3    1589.4    4460.2     245.6     109.7     760.1     100.7      37.3   2194.00
       .14      7.21     14.49      5.87      .050      .030      .050      .000   2193.50    907.60
   .011946      195.      210.      235.         0        11         0       .00    440.27   1347.87


*SECNO 1.012
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      902.5    1486.0  TYPE=      1  TARGET=      583.470
     1.012      4.09   2204.09   2204.09   2204.09   2205.04       .96      5.54       .02   2201.20
    7820.0    1964.2    1001.4    4854.4     249.7      72.9     817.3     111.2      42.2   2201.20
       .16      7.87     13.74      5.94      .050      .030      .050      .000   2200.00    902.50
   .015761      380.      390.      420.         0        15         0       .00    583.46   1485.96


*SECNO 1.112

3470 ENCROACHMENT STATIONS=      569.6    1022.1  TYPE=      1  TARGET=      452.530
     1.112      5.38   2210.88   2210.80   2210.88   2211.99      1.11      6.90       .05   2207.50
    7820.0    6145.6    1540.1     134.3     890.9     118.0      24.3     123.7      48.2   2207.50
       .18      6.90     13.05      5.53      .050      .030      .050      .000   2205.50    569.59
   .012210      465.      530.      540.         2        11         0       .00    452.53   1022.12


*SECNO 1.180

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      659.4    1326.1  TYPE=      1  TARGET=      666.750
            ET RECORD: STA 620. ELIMINATE INEFFECTIVE
                       FLOW AREA IN LEFT OVERBANK
     1.180      4.93   2216.93   2216.93   2216.93   2217.76       .83      4.21       .03   2213.50
    7820.0    3941.9    1143.3    2734.7     650.2      89.0     492.5     132.6      52.5   2213.50
       .19      6.06     12.85      5.55      .050      .030      .050      .000   2212.00    659.36
   .012414      330.      360.      365.         0        10         0       .00    662.95   1326.11
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.280
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 791.3 1306.3 TYPE= 1 TARGET= 515.080
VULTURE MINE ROAD

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.280 | 3.16 | 2226.16 | 2226.16 | 2226.16 | 2227.19 | 1.04 | 7.08 | .06 | 2223.00 |
| 7820.0 | 2434.2 | 1632.3 | 3753.4 | 386.8 | 126.3 | 588.9 | 146.6 | 59.6 | 2223.00 |
| .21 | 6.29 | 12.93 | 6.37 | .050 | .030 | .050 | .000 | 2223.00 | 791.31 |
| .014704 | 570. | 525. | 480. | 0 | 14 | 0 | .00 | 514.97 | 1306.28 |

*SECNO 1.353
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 869.7 1351.5 TYPE= 1 TARGET= 481.830

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.353 | 3.57 | 2233.57 | 2233.57 | 2233.57 | 2234.63 | 1.06 | 5.47 | .01 | 2230.30 |
| 7820.0 | 1647.4 | 1824.0 | 4348.5 | 255.5 | 140.3 | 726.7 | 156.5 | 64.0 | 2230.30 |
| .22 | 6.45 | 13.00 | 5.98 | .050 | .030 | .050 | .000 | 2230.00 | 869.70 |
| 13502 | 365. | 390. | 400. | 0 | 8 | 0 | .00 | 481.81 | 1351.51 |

*SECNO 1.441
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 914.1 1323.0 TYPE= 1 TARGET= 408.870

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.441 | 4.11 | 2240.11 | 2240.11 | 2240.11 | 2241.32 | 1.21 | 6.10 | .05 | 2236.50 |
| 7820.0 | 1645.6 | 1656.5 | 4517.8 | 214.5 | 119.5 | 690.8 | 167.9 | 68.8 | 2236.50 |
| .24 | 7.67 | 13.87 | 6.54 | .050 | .030 | .050 | .000 | 2236.00 | 914.10 |
| .012983 | 435. | 460. | 470. | 0 | 8 | 0 | .00 | 408.86 | 1322.97 |

*SECNO 1.545

3470 ENCROACHMENT STATIONS= 619.3 1094.0 TYPE= 1 TARGET= 474.680

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.545 | 5.13 | 2246.93 | 2246.50 | 2246.93 | 2247.66 | .74 | 6.30 | .05 | 2244.00 |
| 7820.0 | 5525.7 | 1343.7 | 950.6 | 925.7 | 128.8 | 174.6 | 181.8 | 74.1 | 2244.00 |
| .26 | 5.97 | 10.43 | 5.44 | .050 | .030 | .050 | .000 | 2241.80 | 619.32 |
| .010584 | 605. | 550. | 445. | 4 | 8 | 0 | .00 | 474.68 | 1094.00 |

```
 SECNO     DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
 Q         QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
 TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
 SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


*SECNO 1.641

3470 ENCROACHMENT STATIONS=      600.0    1089.0  TYPE=      1  TARGET=      489.000
            ET RECORD: STA 600. ELIMINATE INEFFECTIVE
                       FLOW AREA IN LEFT OVERBANK
    1.641      3.22   2252.22   2252.01   2252.22   2253.15       .93      5.43       .06   2249.00
   7820.0    5250.4    2032.1     537.4     878.8     177.2     105.8     195.4      79.5   2249.00
      .28      5.97     11.47      5.08      .050      .030      .050      .000   2249.00    602.60
  .011271     490.      510.      520.         4        14         0       .00    462.59   1065.19


*SECNO 1.725

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      795.0    1170.0  TYPE=      1  TARGET=      375.000
            ET RECORD: STA 795. ELIMINATE INEFFECTIVE
                       FLOW AREA IN LEFT OVERBANK
    1.725      4.90   2259.90   2259.90   2259.90   2261.48      1.59      4.56       .20   2255.50
   7820.0    2696.2    3580.1    1543.7     446.0     269.7     231.4     206.3      83.4   2255.50
      .29      6.05     13.28      6.67      .050      .030      .050      .000   2255.00    806.20
  .009260     460.      440.      420.         0        14         0       .00    290.62   1096.82


*SECNO 1.829
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      656.8    1160.0  TYPE=      1  TARGET=      503.210
    1.829      4.40   2267.40   2267.40   2267.40   2268.57      1.17      4.50       .04   2263.00
   7820.0    1209.1    4568.0    2043.0     334.3     426.7     418.8     219.8      88.5   2263.00
      .31      3.62     10.71      4.88      .050      .030      .050      .000   2263.00    656.79
  .007204     570.      550.      540.         0        15         0       .00    503.21   1160.00


*SECNO 1.918

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 882.0 1061.3 TYPE= 1 TARGET= 179.250

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.918 | 5.62 | 2274.62 | 2274.62 | 2274.62 | 2276.88 | 2.26 | 3.51 | .33 | 2269.30 |
| 7820.0 | 1377.1 | 5737.4 | 705.5 | 200.8 | 424.8 | 114.7 | 230.4 | 92.3 | 2269.30 |
| .32 | 6.86 | 13.50 | 6.15 | .050 | .030 | .050 | .000 | 2269.00 | 882.00 |
| .007559 | 560. | 470. | 420. | 0 | 11 | 0 | .00 | 176.83 | 1058.83 |

*SECNO 2.011

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 900.0 1025.9 TYPE= 1 TARGET= 125.950

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.011 | 7.18 | 2282.18 | 2282.18 | 2282.18 | 2284.95 | 2.77 | 3.52 | .15 | 2276.00 |
| 7820.0 | 1448.0 | 6117.9 | 254.1 | 211.6 | 416.6 | 45.4 | 238.4 | 94.0 | 2276.00 |
| .33 | 6.84 | 14.69 | 5.60 | .050 | .030 | .050 | .000 | 2275.00 | 900.00 |
| 06836 | 490. | 490. | 495. | 0 | 11 | 0 | .00 | 125.68 | 1025.68 |

CCHV= .300 CEHV= .500
*SECNO 2.056
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 899.0 1041.7 TYPE= 1 TARGET= 142.690

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.056 | 7.80 | 2284.30 | 2284.30 | 2284.30 | 2286.88 | 2.58 | 1.59 | .06 | 2278.50 |
| 7820.0 | 391.5 | 6530.1 | 898.4 | 80.6 | 471.6 | 141.8 | 242.1 | 94.7 | 2276.50 |
| .34 | 4.86 | 13.85 | 6.34 | .050 | .030 | .050 | .000 | 2276.50 | 899.05 |
| .006559 | 215. | 240. | 240. | 0 | 8 | 0 | .00 | 142.69 | 1041.74 |

*SECNO 2.107

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 952.2 1037.5 TYPE= 1 TARGET= 85.320

| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
|---|---|---|---|---|---|---|---|---|---|
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| 2.107 | 7.32 | 2287.32 | 2287.32 | 2287.32 | 2290.52 | 3.20 | 1.78 | .31 | 2280.50 |
| 6943.0 | 248.9 | 6530.3 | 163.8 | 43.3 | 443.0 | 31.2 | 245.8 | 95.4 | 2280.00 |
| .34 | 5.74 | 14.74 | 5.25 | .050 | .030 | .050 | .000 | 2280.00 | 952.21 |
| .006711 | 275. | 270. | 240. | 0 | 11 | 0 | .00 | 85.32 | 1037.53 |

CCHV= .300 CEHV= .500
*SECNO 2.109
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2299.20 ELREA= 2297.50

DOWNSTREAM FACE OF US HWY 60 CONC BRIDGE (STRUCTURE AB-2)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.109 | 7.28 | 2289.38 | 2289.38 | 2289.38 | 2293.07 | 3.68 | .04 | .24 | 2282.10 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 450.9 | .0 | 245.9 | 95.4 | 2282.10 |
| .34 | .00 | 15.40 | .00 | .000 | .020 | .000 | .000 | 2282.10 | 968.10 |
| .003041 | 10. | 10. | 10. | 0 | 5 | 0 | .00 | 61.90 | 1030.00 |

IAL BRIDGE

5227 DOWNSTREAM ELEV IS 2288.56 , NOT 2289.38 HYDRAULIC JUMP OCCURS DOWNSTREAM (IF LOW FLOW CONTROLS)

| SB | XK | XKOR | COFQ | RDLEN | BWC | BWP | BAREA | SS | ELCHU | ELCHD |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1.25 | 1.56 | 2.80 | .00 | 61.90 | 1.50 | 845.60 | .00 | 2282.10 | 2282.10 |

*SECNO 2.118

3301 HV CHANGED MORE THAN HVINS

CLASS B LOW FLOW

3420 BRIDGE W.S.= 2289.53 BRIDGE VELOCITY= 15.47 CALCULATED CHANNEL AREA= 449.

| EGPRS | EGLWC | H3 | QWEIR | QLOW | BAREA | TRAPEZOID AREA | ELLC | ELTRD | WEIRLN |
|---|---|---|---|---|---|---|---|---|---|
| .00 | 2293.39 | .00 | 0. | 6943. | 846. | 846. | 2296.10 | 2297.50 | 0. |

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2299.20 ELREA= 2297.50

UPSTREAM FACE OF US HWY 60 CONC BRIDGE (STRUCTURE AB-2)

| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
|---|---|---|---|---|---|---|---|---|---|
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| 2.118 | 8.73 | 2290.83 | .00 | 2290.83 | 2293.39 | 2.56 | .33 | .00 | 2282.10 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 540.5 | .0 | 246.4 | 95.5 | 2282.10 |
| .34 | .00 | 12.84 | .00 | .000 | .020 | .000 | .000 | 2282.10 | 968.10 |
| .001662 | 45. | 45. | 45. | 0 | 0 | 0 | .00 | 61.90 | 1030.00 |

*SECNO 2.120

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2297.00 ELREA= 2297.50

DOWNSTREAM FACE OF OLD US HWY 60 CONC BRIDGE (STRUCTURE AB-1)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.120 | 8.57 | 2290.67 | 2289.63 | 2290.67 | 2293.60 | 2.93 | .02 | .18 | 2282.10 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 505.5 | .0 | 246.5 | 95.5 | 2282.10 |
| .34 | .00 | 13.74 | .00 | .000 | .020 | .000 | .000 | 2282.10 | 970.50 |
| .001949 | 10. | 10. | 10. | 2 | 11 | 0 | .00 | 59.00 | 1029.50 |

SPECIAL BRIDGE

DOWNSTREAM ELEV IS 2288.42 , NOT 2290.67 HYDRAULIC JUMP OCCURS DOWNSTREAM (IF LOW FLOW CONTROLS)

| SB | XK | XKOR | COFQ | RDLEN | BWC | BWP | BAREA | SS | ELCHU | ELCHD |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1.25 | 1.56 | 2.80 | .00 | 59.00 | 3.00 | 588.00 | .00 | 2282.70 | 2282.10 |

*SECNO 2.125

3301 HV CHANGED MORE THAN HVINS

CLASS B LOW FLOW

3420 BRIDGE W.S.= 2290.21 BRIDGE VELOCITY= 15.87 CALCULATED CHANNEL AREA= 421.

| EGPRS | EGLWC | H3 | QWEIR | QLOW | BAREA | TRAPEZOID AREA | ELLC | ELTRD | WEIRLN |
|---|---|---|---|---|---|---|---|---|---|
| 2294.04 | 2294.71 | .00 | 0. | 6943. | 588. | 588. | 2293.20 | 2297.00 | 0. |

3495 OVERBANK AREA ASSUMED NON-EFFECTIVE, ELLEA= 2297.00 ELREA= 2297.50

UPSTREAM FACE OF OLD US HWY 60 CONC BRIDGE (STRUCTURE AB-1)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.125 | 9.75 | 2292.45 | .00 | 2292.45 | 2294.71 | 2.26 | 1.11 | .00 | 2282.70 |
| 6943.0 | .0 | 6943.0 | .0 | .0 | 575.0 | .0 | 246.9 | 95.5 | 2282.70 |
| .35 | .00 | 12.07 | .00 | .000 | .020 | .000 | .000 | 2282.70 | 970.50 |
| .001269 | 30. | 30. | 30. | 0 | 0 | 0 | .00 | 59.00 | 1029.50 |

```
 SECNO     DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
 Q         QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
 TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
 SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


CCHV=     .100 CEHV=     .300
*SECNO 2.213
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      830.0    1062.6  TYPE=      1  TARGET=      232.670
    2.213      8.79   2298.29   2298.29   2298.29   2300.19      1.90      1.01       .04   2292.00
   6943.0    1768.6    4668.6     505.8     419.8     355.3     109.8     254.5      97.0   2292.50
      .36      4.21     13.14      4.61      .050      .030      .050      .000   2289.50    829.96
  .004605      415.      465.      525.         0        15         0       .00    232.67   1062.63


*SECNO 2.248
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      830.0    1060.0  TYPE=      1  TARGET=      230.040
    2.248      8.29   2300.29   2300.29   2300.29   2301.89      1.60       .88       .03   2296.00
   6943.0    2904.3    3615.8     422.9     544.3     275.5      88.5     257.8      97.9   2296.50
      .36      5.34     13.12      4.78      .050      .030      .050      .000   2292.00    829.96
  .006094      130.      180.      245.         0        10         0       .00    230.04   1060.00


*SECNO 2.342

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      946.1    1109.0  TYPE=      1  TARGET=      162.940
            ET RECORD: STA 1475. ELIMINATE INEFFECTIVE
                       FLOW AREA IN RIGHT OVERBANK
    2.342      8.61   2305.61   2305.61   2305.61   2307.99      2.38      2.82       .23   2298.00
   6943.0     848.4    4695.8    1398.8     122.8     323.6     281.9     267.1     100.1   2298.00
      .37      6.91     14.51      4.96      .050      .030      .050      .000   2297.00    946.59
  .005293      515.      500.      450.         0         8         0       .00    162.41   1109.00


*SECNO 2.435
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3470 ENCROACHMENT STATIONS= 957.7 1102.0 TYPE= 1 TARGET= 144.310

CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH

ET RECORD: STA 1288. ELIMINATE INEFFECTIVE
FLOW AREA IN RIGHT OVERBANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.435 | 6.29 | 2309.79 | 2309.79 | 2309.79 | 2312.09 | 2.30 | 3.27 | .01 | 2304.00 |
| 6943.0 | 846.3 | 3376.1 | 2720.6 | 120.6 | 216.7 | 346.9 | 274.8 | 101.7 | 2304.00 |
| .39 | 7.02 | 15.58 | 7.84 | .050 | .030 | .050 | .000 | 2303.50 | 957.74 |
| .009036 | 500. | 490. | 455. | 0 | 19 | 0 | .00 | 144.26 | 1102.00 |

RIGHT BANK LEVEE BETWEEN SECTIONS 0.134 & 0.160

| ASQ | QCOMP | ERRAC | TASQ | TCQ | TABER | NITER | DSWS | USWS | DSSNO | USSNO |
|---|---|---|---|---|---|---|---|---|---|---|
| 1243.30 | 1243.87 | .05 | 1243.30 | 1243.87 | .05 | 7 | 2139.404 | 2140.919 | .134 | .160 |

TW RIGHT BANK LEVEE BETWEEN SECTIONS 0.160 & 0.220

| ASQ | QCOMP | ERRAC | TASQ | TCQ | TABER | NITER | DSWS | USWS | DSSNO | USSNO |
|---|---|---|---|---|---|---|---|---|---|---|
| 3574.17 | 3574.18 | .00 | 4817.47 | 4818.05 | .01 | 7 | 2140.919 | 2144.661 | .160 | .220 |

THIS RUN EXECUTED 15JUL92 15:04:44

**********
HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991
**********

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

WASH AB: FLYING E WASH

SUMMARY PRINTOUT TABLE 150

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | .095 | .00 | .00 | .00 | 2131.00 | 3002.44 | 2134.50 | 2134.47 | 2135.94 | 81.20 | 9.78 | 327.80 | 333.20 |
| | .095 | .00 | .00 | .00 | 2131.00 | 3002.53 | 2134.50 | 2134.48 | 2135.94 | 81.20 | 9.78 | 327.80 | 333.20 |
| * | .125 | 160.00 | .00 | .00 | 2133.00 | 3002.44 | 2136.42 | 2136.42 | 2137.76 | 92.27 | 9.40 | 330.99 | 312.56 |
| * | .125 | 160.00 | .00 | .00 | 2133.00 | 3002.53 | 2136.42 | 2136.42 | 2137.76 | 92.25 | 9.40 | 331.02 | 312.61 |
| | .131 | 30.00 | .00 | .00 | 2133.60 | 3002.44 | 2137.70 | 2136.05 | 2138.14 | 17.57 | 5.31 | 565.00 | 716.28 |
| | .131 | 30.00 | .00 | .00 | 2133.60 | 3002.53 | 2137.70 | 2136.05 | 2138.14 | 17.57 | 5.31 | 565.00 | 716.28 |
| * | .134 | 14.70 | 2139.40 | 2136.70 | 2133.70 | 3002.44 | 2139.16 | .00 | 2139.40 | 6.74 | 3.99 | 753.17 | 1156.54 |
| * | .134 | 14.70 | 2139.40 | 2136.70 | 2133.70 | 3002.53 | 2139.16 | .00 | 2139.40 | 6.74 | 3.99 | 753.21 | 1156.62 |
| * | .160 | 140.00 | .00 | .00 | 2136.00 | 4245.84 | 2139.85 | 2139.85 | 2140.92 | 74.19 | 10.12 | 669.54 | 492.94 |
| * | .160 | 140.00 | .00 | .00 | 2136.00 | 4245.83 | 2139.85 | 2139.85 | 2140.92 | 74.19 | 10.12 | 669.54 | 492.94 |
| * | .220 | 315.00 | .00 | .00 | 2140.50 | 7820.00 | 2143.77 | 2143.77 | 2144.66 | 125.37 | 11.55 | 1269.59 | 698.40 |
| * | .220 | 315.00 | .00 | .00 | 2140.50 | 7820.00 | 2143.77 | 2143.77 | 2144.66 | 125.04 | 11.54 | 1270.71 | 699.33 |
| * | .256 | 190.00 | .00 | .00 | 2143.00 | 7820.00 | 2147.24 | 2147.24 | 2148.14 | 92.31 | 12.47 | 1369.12 | 813.93 |
| * | .256 | 190.00 | .00 | .00 | 2143.00 | 7820.00 | 2147.38 | 2147.38 | 2148.43 | 96.72 | 13.05 | 1254.55 | 795.14 |
| * | .351 | 500.00 | .00 | .00 | 2149.00 | 7820.00 | 2153.28 | 2153.28 | 2154.43 | 73.57 | 11.20 | 1206.63 | 911.73 |
| * | .351 | 500.00 | .00 | .00 | 2149.00 | 7820.00 | 2153.78 | 2153.78 | 2155.31 | 73.22 | 12.03 | 1010.87 | 913.87 |
| * | .460 | 575.00 | .00 | .00 | 2155.50 | 7820.00 | 2161.34 | 2161.34 | 2163.02 | 88.28 | 14.74 | 922.95 | 832.29 |
| * | .460 | 575.00 | .00 | .00 | 2155.50 | 7820.00 | 2161.21 | 2161.21 | 2163.12 | 100.35 | 15.47 | 855.50 | 780.65 |
| * | .540 | 425.00 | .00 | .00 | 2162.00 | 7820.00 | 2165.99 | 2165.99 | 2167.41 | 144.27 | 14.39 | 931.43 | 651.05 |
| * | .540 | 425.00 | .00 | .00 | 2162.00 | 7820.00 | 2166.20 | 2166.20 | 2167.84 | 145.76 | 14.99 | 856.75 | 647.72 |
| * | .576 | 190.00 | .00 | .00 | 2164.80 | 7820.00 | 2169.20 | 2169.20 | 2170.67 | 115.05 | 13.99 | 951.23 | 729.07 |
| | .576 | 190.00 | .00 | .00 | 2164.80 | 7820.00 | 2169.20 | 2169.20 | 2170.67 | 115.81 | 14.02 | 949.10 | 726.66 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | .640 | 340.00 | .00 | .00 | 2169.50 | 7820.00 | 2174.17 | 2174.17 | 2175.47 | 109.39 | 14.16 | 1010.32 | 747.67 |
| * | .640 | 340.00 | .00 | .00 | 2169.50 | 7820.00 | 2174.17 | 2174.17 | 2175.47 | 109.47 | 14.16 | 1010.03 | 747.40 |
| * | .707 | 350.00 | .00 | .00 | 2176.00 | 7820.00 | 2181.69 | 2181.69 | 2182.93 | 79.92 | 13.88 | 1135.11 | 874.74 |
| * | .707 | 350.00 | .00 | .00 | 2176.00 | 7820.00 | 2181.68 | 2181.68 | 2182.93 | 80.11 | 13.89 | 1134.01 | 873.71 |
| * | .801 | 500.00 | .00 | .00 | 2180.00 | 7820.00 | 2187.56 | 2187.56 | 2188.83 | 65.55 | 13.45 | 1275.15 | 965.88 |
| * | .801 | 500.00 | .00 | .00 | 2180.00 | 7820.00 | 2187.56 | 2187.56 | 2188.83 | 65.38 | 13.44 | 1276.33 | 967.16 |
| * | .898 | 510.00 | .00 | .00 | 2190.00 | 7820.00 | 2193.85 | 2193.85 | 2194.91 | 222.09 | 12.70 | 994.60 | 524.74 |
| * | .898 | 510.00 | .00 | .00 | 2190.00 | 7820.00 | 2193.85 | 2193.85 | 2194.91 | 222.00 | 12.70 | 994.72 | 524.84 |
| * | .938 | 210.00 | .00 | .00 | 2193.50 | 7820.00 | 2198.10 | 2198.10 | 2199.25 | 119.43 | 14.49 | 1115.53 | 715.57 |
| * | .938 | 210.00 | .00 | .00 | 2193.50 | 7820.00 | 2198.10 | 2198.10 | 2199.25 | 119.46 | 14.49 | 1115.42 | 715.47 |
| * | 1.012 | 390.00 | .00 | .00 | 2200.00 | 7820.00 | 2204.09 | 2204.09 | 2205.04 | 157.44 | 13.73 | 1140.35 | 623.23 |
| * | 1.012 | 390.00 | .00 | .00 | 2200.00 | 7820.00 | 2204.09 | 2204.09 | 2205.04 | 157.61 | 13.74 | 1139.92 | 622.90 |
| | 1.112 | 530.00 | .00 | .00 | 2205.50 | 7820.00 | 2210.88 | 2210.80 | 2211.99 | 122.20 | 13.06 | 1032.82 | 707.40 |
| | 1.112 | 530.00 | .00 | .00 | 2205.50 | 7820.00 | 2210.88 | 2210.80 | 2211.99 | 122.10 | 13.05 | 1033.16 | 707.69 |
| * | 1.180 | 360.00 | .00 | .00 | 2212.00 | 7820.00 | 2216.84 | 2216.84 | 2217.76 | 141.13 | 13.47 | 1172.04 | 658.26 |
| * | 1.180 | 360.00 | .00 | .00 | 2212.00 | 7820.00 | 2216.93 | 2216.93 | 2217.76 | 124.14 | 12.85 | 1231.71 | 701.85 |
| | 1.280 | 525.00 | .00 | .00 | 2223.00 | 7820.00 | 2226.16 | 2226.16 | 2227.19 | 146.70 | 12.92 | 1102.93 | 645.65 |
| | 1.280 | 525.00 | .00 | .00 | 2223.00 | 7820.00 | 2226.16 | 2226.16 | 2227.19 | 147.04 | 12.93 | 1102.05 | 644.89 |
| * | 1.353 | 390.00 | .00 | .00 | 2230.00 | 7820.00 | 2233.57 | 2233.57 | 2234.63 | 134.84 | 13.00 | 1122.94 | 673.43 |
| * | 1.353 | 390.00 | .00 | .00 | 2230.00 | 7820.00 | 2233.57 | 2233.57 | 2234.63 | 135.02 | 13.00 | 1122.47 | 673.00 |
| * | 1.441 | 460.00 | .00 | .00 | 2236.00 | 7820.00 | 2240.11 | 2240.11 | 2241.32 | 129.83 | 13.87 | 1024.71 | 686.31 |
| * | 1.441 | 460.00 | .00 | .00 | 2236.00 | 7820.00 | 2240.11 | 2240.11 | 2241.32 | 129.83 | 13.87 | 1024.71 | 686.31 |
| | 1.545 | 550.00 | .00 | .00 | 2241.80 | 7820.00 | 2246.76 | 2246.41 | 2247.33 | 98.01 | 9.66 | 1438.95 | 789.89 |
| | 1.545 | 550.00 | .00 | .00 | 2241.80 | 7820.00 | 2246.93 | 2246.50 | 2247.66 | 105.84 | 10.43 | 1229.15 | 760.13 |
| | 1.641 | 510.00 | .00 | .00 | 2249.00 | 7820.00 | 2252.09 | 2252.01 | 2253.13 | 132.84 | 12.12 | 1102.25 | 678.50 |
| | 1.641 | 510.00 | .00 | .00 | 2249.00 | 7820.00 | 2252.22 | 2252.01 | 2253.15 | 112.71 | 11.47 | 1161.85 | 736.59 |
| * | 1.725 | 440.00 | .00 | .00 | 2255.00 | 7820.00 | 2259.91 | 2259.91 | 2261.48 | 91.97 | 13.25 | 949.26 | 815.41 |
| * | 1.725 | 440.00 | .00 | .00 | 2255.00 | 7820.00 | 2259.90 | 2259.90 | 2261.48 | 92.60 | 13.28 | 947.06 | 812.66 |
| * | 1.829 | 550.00 | .00 | .00 | 2263.00 | 7820.00 | 2267.35 | 2267.35 | 2268.42 | 69.83 | 10.45 | 1271.74 | 935.82 |
| * | 1.829 | 550.00 | .00 | .00 | 2263.00 | 7820.00 | 2267.40 | 2267.40 | 2268.57 | 72.04 | 10.71 | 1179.79 | 921.31 |
| * | 1.918 | 470.00 | .00 | .00 | 2269.00 | 7820.00 | 2274.71 | 2274.71 | 2276.63 | 66.19 | 12.77 | 844.52 | 961.18 |
| * | 1.918 | 470.00 | .00 | .00 | 2269.00 | 7820.00 | 2274.62 | 2274.62 | 2276.88 | 75.59 | 13.50 | 740.32 | 899.46 |
| * | 2.011 | 490.00 | .00 | .00 | 2275.00 | 7820.00 | 2282.29 | 2282.29 | 2284.17 | 51.01 | 12.82 | 934.92 | 1094.96 |
| | 2.011 | 490.00 | .00 | .00 | 2275.00 | 7820.00 | 2282.18 | 2282.18 | 2284.95 | 68.36 | 14.69 | 673.56 | 945.79 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 2.056 | 240.00 | .00 | .00 | 2276.50 | 7820.00 | 2284.24 | 2284.24 | 2286.88 | 68.21 | 14.02 | 684.41 | 946.88 |
| * | 2.056 | 240.00 | .00 | .00 | 2276.50 | 7820.00 | 2284.30 | 2284.30 | 2286.88 | 65.59 | 13.85 | 693.99 | 965.58 |
| * | 2.107 | 270.00 | .00 | .00 | 2280.00 | 6943.00 | 2287.31 | 2287.31 | 2290.52 | 67.19 | 14.74 | 517.42 | 847.04 |
| * | 2.107 | 270.00 | .00 | .00 | 2280.00 | 6943.00 | 2287.32 | 2287.32 | 2290.52 | 67.11 | 14.74 | 517.61 | 847.51 |
| * | 2.109 | 10.00 | .00 | .00 | 2282.10 | 6943.00 | 2289.38 | 2289.38 | 2293.07 | 30.41 | 15.40 | 450.91 | 1259.02 |
| * | 2.109 | 10.00 | .00 | .00 | 2282.10 | 6943.00 | 2289.38 | 2289.38 | 2293.07 | 30.41 | 15.40 | 450.91 | 1259.02 |
| * | 2.118 | 45.00 | 2297.50 | 2296.10 | 2282.10 | 6943.00 | 2290.83 | .00 | 2293.39 | 16.62 | 12.84 | 540.54 | 1703.21 |
| * | 2.118 | 45.00 | 2297.50 | 2296.10 | 2282.10 | 6943.00 | 2290.83 | .00 | 2293.39 | 16.62 | 12.84 | 540.54 | 1703.21 |
| | 2.120 | 10.00 | .00 | .00 | 2282.10 | 6943.00 | 2290.67 | 2289.63 | 2293.60 | 19.49 | 13.74 | 505.46 | 1572.53 |
| | 2.120 | 10.00 | .00 | .00 | 2282.10 | 6943.00 | 2290.67 | 2289.63 | 2293.60 | 19.49 | 13.74 | 505.46 | 1572.53 |
| * | 2.125 | 30.30 | 2297.00 | 2293.20 | 2282.70 | 6943.00 | 2292.45 | .00 | 2294.71 | 12.69 | 12.07 | 574.99 | 1949.34 |
| * | 2.125 | 30.30 | 2297.00 | 2293.20 | 2282.70 | 6943.00 | 2292.45 | .00 | 2294.71 | 12.69 | 12.07 | 574.99 | 1949.34 |
| * | 2.213 | 465.00 | .00 | .00 | 2289.50 | 6943.00 | 2298.08 | 2298.08 | 2299.32 | 36.46 | 11.48 | 1271.51 | 1149.88 |
| * | 2.213 | 465.00 | .00 | .00 | 2289.50 | 6943.00 | 2298.29 | 2298.29 | 2300.19 | 46.05 | 13.14 | 884.88 | 1023.11 |
| * | 2.248 | 180.00 | .00 | .00 | 2292.00 | 6943.00 | 2300.02 | 2300.02 | 2301.06 | 49.10 | 11.45 | 1260.04 | 990.87 |
| * | 2.248 | 180.00 | .00 | .00 | 2292.00 | 6943.00 | 2300.29 | 2300.29 | 2301.89 | 60.94 | 13.12 | 908.36 | 889.36 |
| | 2.342 | 500.00 | .00 | .00 | 2297.00 | 6943.00 | 2305.96 | 2305.96 | 2307.72 | 39.78 | 12.94 | 936.71 | 1100.77 |
| | 2.342 | 500.00 | .00 | .00 | 2297.00 | 6943.00 | 2305.61 | 2305.61 | 2307.99 | 52.93 | 14.51 | 728.25 | 954.29 |
| * | 2.435 | 490.00 | .00 | .00 | 2303.50 | 6943.00 | 2309.84 | 2309.84 | 2311.91 | 83.04 | 15.01 | 733.60 | 761.90 |
| * | 2.435 | 490.00 | .00 | .00 | 2303.50 | 6943.00 | 2309.79 | 2309.79 | 2312.09 | 90.36 | 15.58 | 684.15 | 730.39 |

AB: FLYING E WASH

SUMMARY PRINTOUT TABLE 150

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| | .095 | 3002.44 | 2134.50 | .00 | .00 | .00 | 121.31 | .00 |
| | .095 | 3002.53 | 2134.50 | .00 | .00 | .00 | 121.31 | .00 |
| * | .125 | 3002.44 | 2136.42 | .00 | 1.92 | .00 | 127.87 | 160.00 |
| * | .125 | 3002.53 | 2136.42 | .00 | 1.92 | .00 | 127.87 | 160.00 |
| * | .131 | 3002.44 | 2137.70 | .00 | 1.28 | .00 | 138.00 | 30.00 |
| * | .131 | 3002.53 | 2137.70 | .00 | 1.28 | .00 | 138.00 | 30.00 |
| * | .134 | 3002.44 | 2139.16 | .00 | 1.46 | .00 | 138.00 | 14.70 |
| * | .134 | 3002.53 | 2139.16 | .00 | 1.46 | .00 | 138.00 | 14.70 |
| * | .160 | 4245.84 | 2139.85 | .00 | .70 | .00 | 318.00 | 140.00 |
| * | .160 | 4245.83 | 2139.85 | .00 | .70 | .00 | 318.00 | 140.00 |
| * | .220 | 7820.00 | 2143.77 | .00 | 3.91 | .00 | 657.54 | 315.00 |
| * | .220 | 7820.00 | 2143.77 | .00 | 3.92 | .00 | 657.54 | 315.00 |
| | .256 | 7820.00 | 2147.24 | .00 | 3.47 | .00 | 619.88 | 190.00 |
| | .256 | 7820.00 | 2147.38 | .14 | 3.61 | .00 | 514.96 | 190.00 |
| * | .351 | 7820.00 | 2153.28 | .00 | 6.04 | .00 | 470.42 | 500.00 |
| * | .351 | 7820.00 | 2153.78 | .50 | 6.40 | .00 | 310.00 | 500.00 |
| * | .460 | 7820.00 | 2161.34 | .00 | 8.06 | .00 | 273.25 | 575.00 |
| * | .460 | 7820.00 | 2161.21 | -.13 | 7.42 | .00 | 209.23 | 575.00 |
| * | .540 | 7820.00 | 2165.99 | .00 | 4.65 | .00 | 321.61 | 425.00 |
| * | .540 | 7820.00 | 2166.20 | .21 | 4.99 | .00 | 259.20 | 425.00 |
| * | .576 | 7820.00 | 2169.20 | .00 | 3.21 | .00 | 311.48 | 190.00 |
| * | .576 | 7820.00 | 2169.20 | -.01 | 2.99 | .00 | 311.33 | 190.00 |
| * | .640 | 7820.00 | 2174.17 | .00 | 4.97 | .00 | 393.49 | 340.00 |
| * | .640 | 7820.00 | 2174.17 | .00 | 4.97 | .00 | 393.34 | 340.00 |
| * | .707 | 7820.00 | 2181.69 | .00 | 7.52 | .00 | 450.79 | 350.00 |
| * | .707 | 7820.00 | 2181.68 | .00 | 7.52 | .00 | 450.65 | 350.00 |
| * | .801 | 7820.00 | 2187.56 | .00 | 5.87 | .00 | 441.60 | 500.00 |
| * | .801 | 7820.00 | 2187.56 | .00 | 5.88 | .00 | 441.60 | 500.00 |
| * | .898 | 7820.00 | 2193.85 | .00 | 6.29 | .00 | 482.17 | 510.00 |
| * | .898 | 7820.00 | 2193.85 | .00 | 6.29 | .00 | 482.16 | 510.00 |
| | .938 | 7820.00 | 2198.10 | .00 | 4.25 | .00 | 440.28 | 210.00 |
| * | .938 | 7820.00 | 2198.10 | .00 | 4.25 | .00 | 440.27 | 210.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 1.012 | 7820.00 | 2204.09 | .00 | 5.99 | .00 | 583.48 | 390.00 |
| * | 1.012 | 7820.00 | 2204.09 | .00 | 5.99 | .00 | 583.46 | 390.00 |
| | 1.112 | 7820.00 | 2210.88 | .00 | 6.79 | .00 | 452.52 | 530.00 |
| | 1.112 | 7820.00 | 2210.88 | .00 | 6.79 | .00 | 452.53 | 530.00 |
| * | 1.180 | 7820.00 | 2216.84 | .00 | 5.96 | .00 | 658.13 | 360.00 |
| * | 1.180 | 7820.00 | 2216.93 | .09 | 6.05 | .00 | 662.95 | 360.00 |
| * | 1.280 | 7820.00 | 2226.16 | .00 | 9.32 | .00 | 515.08 | 525.00 |
| * | 1.280 | 7820.00 | 2226.16 | .00 | 9.23 | .00 | 514.97 | 525.00 |
| * | 1.353 | 7820.00 | 2233.57 | .00 | 7.41 | .00 | 481.83 | 390.00 |
| * | 1.353 | 7820.00 | 2233.57 | .00 | 7.41 | .00 | 481.81 | 390.00 |
| * | 1.441 | 7820.00 | 2240.11 | .00 | 6.54 | .00 | 408.86 | 460.00 |
| * | 1.441 | 7820.00 | 2240.11 | .00 | 6.55 | .00 | 408.86 | 460.00 |
| | 1.545 | 7820.00 | 2246.76 | .00 | 6.65 | .00 | 688.12 | 550.00 |
| | 1.545 | 7820.00 | 2246.93 | .16 | 6.81 | .00 | 474.68 | 550.00 |
| | 1.641 | 7820.00 | 2252.09 | .00 | 5.33 | .00 | 460.34 | 510.00 |
| | 1.641 | 7820.00 | 2252.22 | .13 | 5.29 | .00 | 462.59 | 510.00 |
| | 1.725 | 7820.00 | 2259.91 | .00 | 7.82 | .00 | 290.79 | 440.00 |
| * | 1.725 | 7820.00 | 2259.90 | -.01 | 7.68 | .00 | 290.62 | 440.00 |
| * | 1.829 | 7820.00 | 2267.35 | .00 | 7.44 | .00 | 606.21 | 550.00 |
| * | 1.829 | 7820.00 | 2267.40 | .05 | 7.50 | .00 | 503.21 | 550.00 |
| * | 1.918 | 7820.00 | 2274.71 | .00 | 7.36 | .00 | 249.57 | 470.00 |
| * | 1.918 | 7820.00 | 2274.62 | -.09 | 7.22 | .00 | 176.83 | 470.00 |
| * | 2.011 | 7820.00 | 2282.29 | .00 | 7.59 | .00 | 288.81 | 490.00 |
| * | 2.011 | 7820.00 | 2282.18 | -.11 | 7.56 | .00 | 125.68 | 490.00 |
| * | 2.056 | 7820.00 | 2284.24 | .00 | 1.94 | .00 | 142.70 | 240.00 |
| * | 2.056 | 7820.00 | 2284.30 | .07 | 2.12 | .00 | 142.69 | 240.00 |
| * | 2.107 | 6943.00 | 2287.31 | .00 | 3.08 | .00 | 85.32 | 270.00 |
| * | 2.107 | 6943.00 | 2287.32 | .00 | 3.01 | .00 | 85.32 | 270.00 |
| * | 2.109 | 6943.00 | 2289.38 | .00 | 2.07 | .00 | 61.90 | 10.00 |
| * | 2.109 | 6943.00 | 2289.38 | .00 | 2.07 | .00 | 61.90 | 10.00 |
| * | 2.118 | 6943.00 | 2290.83 | .00 | 1.45 | .00 | 61.90 | 45.00 |
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| | 2.120 | 6943.00 | 2290.67 | .00 | -.17 | .00 | 59.00 | 10.00 |
| | 2.120 | 6943.00 | 2290.67 | .00 | -.17 | .00 | 59.00 | 10.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 2.125 | 6943.00 | 2292.45 | .00 | 1.78 | .00 | 59.00 | 30.30 |
| * | 2.125 | 6943.00 | 2292.45 | .00 | 1.78 | .00 | 59.00 | 30.30 |
| * | 2.213 | 6943.00 | 2298.08 | .00 | 5.63 | .00 | 587.76 | 465.00 |
| * | 2.213 | 6943.00 | 2298.29 | .21 | 5.85 | .00 | 232.67 | 465.00 |
| * | 2.248 | 6943.00 | 2300.02 | .00 | 1.94 | .00 | 528.24 | 180.00 |
| * | 2.248 | 6943.00 | 2300.29 | .27 | 2.00 | .00 | 230.04 | 180.00 |
| * | 2.342 | 6943.00 | 2305.96 | .00 | 5.94 | .00 | 325.44 | 500.00 |
| * | 2.342 | 6943.00 | 2305.61 | -.35 | 5.32 | .00 | 162.41 | 500.00 |
| * | 2.435 | 6943.00 | 2309.84 | .00 | 3.88 | .00 | 180.38 | 490.00 |
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FLOODWAY DATA, WASH AB: FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| .095 | 121. | 328. | 9.2 | 2134.5 | 2134.5 | .0 |
| .125 | 128. | 331. | 9.1 | 2136.4 | 2136.4 | .0 |
| .131 | 138. | 565. | 5.3 | 2137.7 | 2137.7 | .0 |
| .134 | 138. | 753. | 4.0 | 2139.2 | 2139.2 | .0 |
| .160 | 318. | 670. | 6.3 | 2139.9 | 2139.9 | .0 |
| .220 | 658. | 1271. | 6.2 | 2143.8 | 2143.8 | .0 |
| .256 | 515. | 1255. | 6.2 | 2147.3 | 2147.2 | .1 |
| .351 | 310. | 1011. | 7.7 | 2153.8 | 2153.3 | .5 |
| .460 | 209. | 856. | 9.1 | 2161.2 | 2161.3 | -.1 |
| .540 | 259. | 857. | 9.1 | 2166.2 | 2166.0 | .2 |
| .576 | 311. | 949. | 8.2 | 2169.2 | 2169.2 | .0 |
| .640 | 431. | 1010. | 7.7 | 2174.2 | 2174.2 | .0 |
| .707 | 451. | 1134. | 6.9 | 2181.7 | 2181.7 | .0 |
| .801 | 442. | 1276. | 6.1 | 2187.6 | 2187.6 | .0 |
| .898 | 482. | 995. | 7.9 | 2193.9 | 2193.9 | .0 |
| .938 | 440. | 1115. | 7.0 | 2198.1 | 2198.1 | .0 |
| .012 | 583. | 1140. | 6.9 | 2204.1 | 2204.1 | .0 |
| 1.112 | 453. | 1033. | 7.6 | 2210.9 | 2210.9 | .0 |
| 1.180 | 667. | 1232. | 6.3 | 2216.9 | 2216.8 | .1 |
| 1.280 | 515. | 1102. | 7.1 | 2226.2 | 2226.2 | .0 |
| 1.353 | 482. | 1122. | 7.0 | 2233.6 | 2233.6 | .0 |
| 1.441 | 409. | 1025. | 7.6 | 2240.1 | 2240.1 | .0 |
| 1.545 | 475. | 1229. | 6.4 | 2247.0 | 2246.8 | .2 |
| 1.641 | 463. | 1162. | 6.7 | 2252.2 | 2252.1 | .1 |
| 1.725 | 291. | 947. | 8.3 | 2259.9 | 2259.9 | .0 |
| 1.829 | 503. | 1180. | 6.6 | 2267.5 | 2267.4 | .1 |
| 1.918 | 177. | 740. | 10.6 | 2274.6 | 2274.7 | -.1 |
| 2.011 | 126. | 674. | 11.6 | 2282.2 | 2282.3 | -.1 |
| 2.056 | 143. | 694. | 11.3 | 2284.3 | 2284.2 | .1 |
| 2.107 | 85. | 518. | 13.4 | 2287.3 | 2287.3 | .0 |
| 2.109 | 62. | 451. | 15.4 | 2289.4 | 2289.4 | .0 |
| 2.118 | 62. | 541. | 12.8 | 2290.8 | 2290.8 | .0 |
| 2.120 | 59. | 505. | 13.7 | 2290.7 | 2290.7 | .0 |
| 2.125 | 59. | 575. | 12.1 | 2292.4 | 2292.4 | .0 |
| 2.213 | 233. | 885. | 7.8 | 2298.3 | 2298.1 | .2 |
| 2.248 | 230. | 908. | 7.6 | 2300.3 | 2300.0 | .3 |
| 2.342 | 162. | 728. | 9.5 | 2305.6 | 2306.0 | -.4 |
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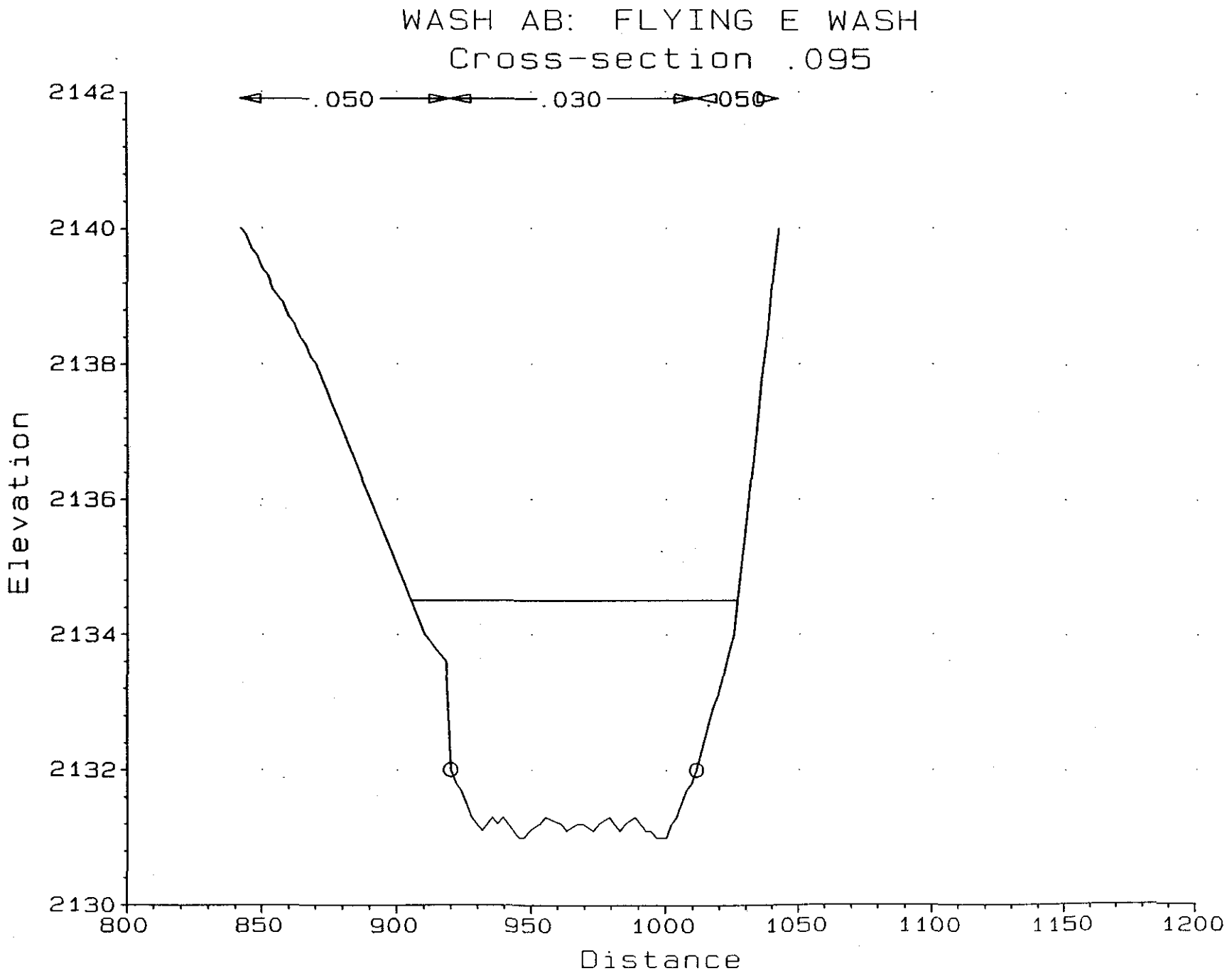
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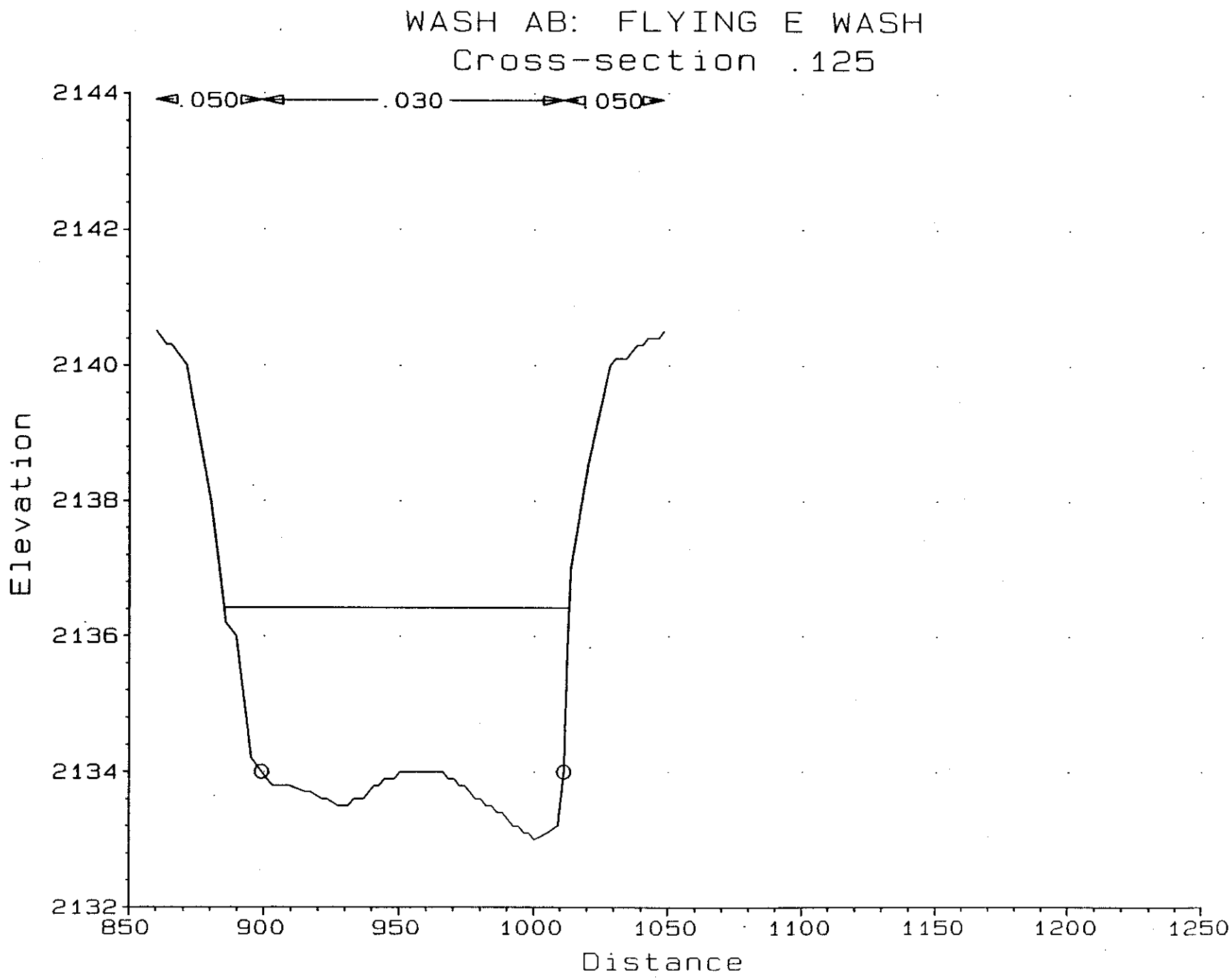
Distance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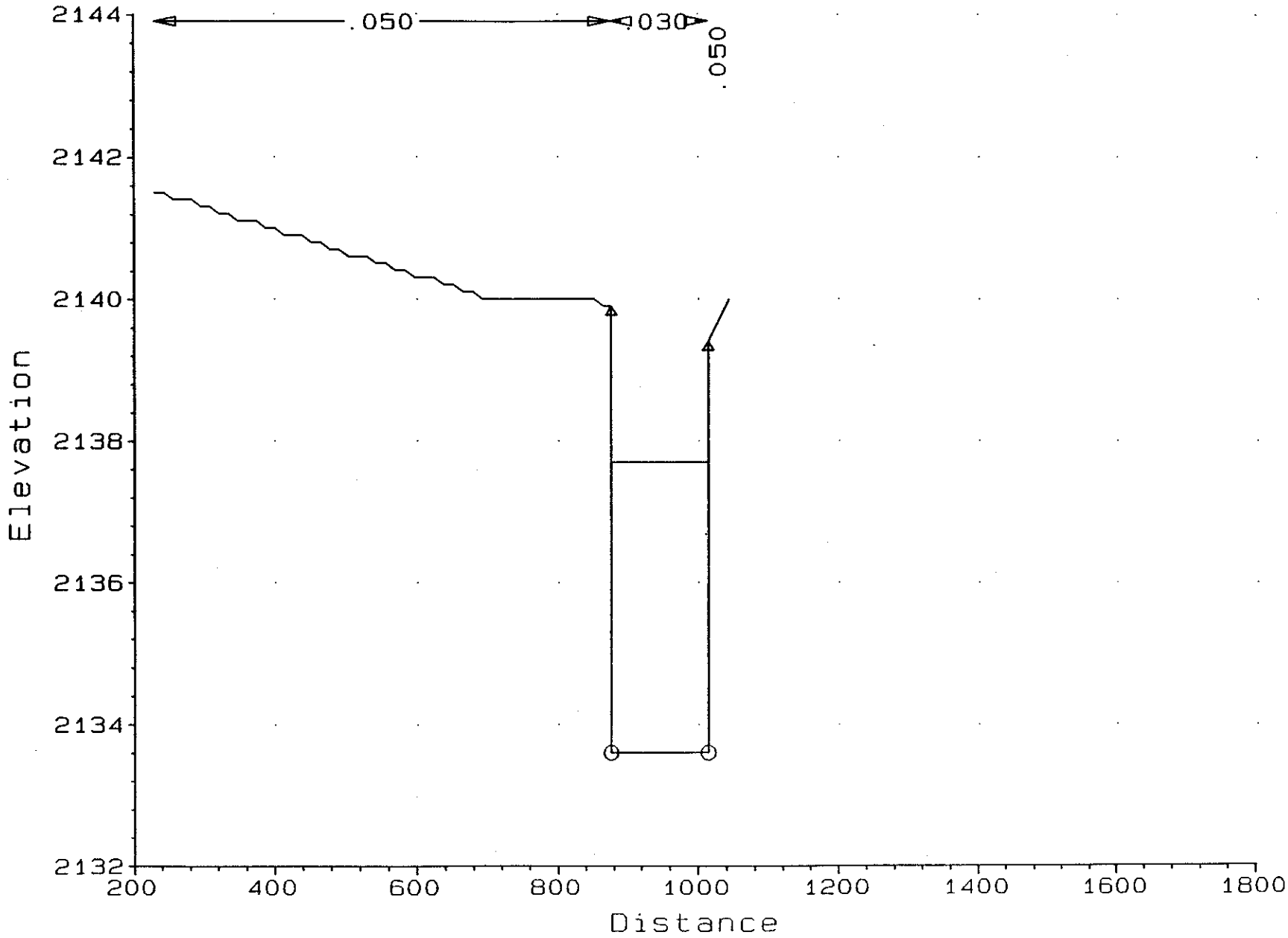
Cross-section .131



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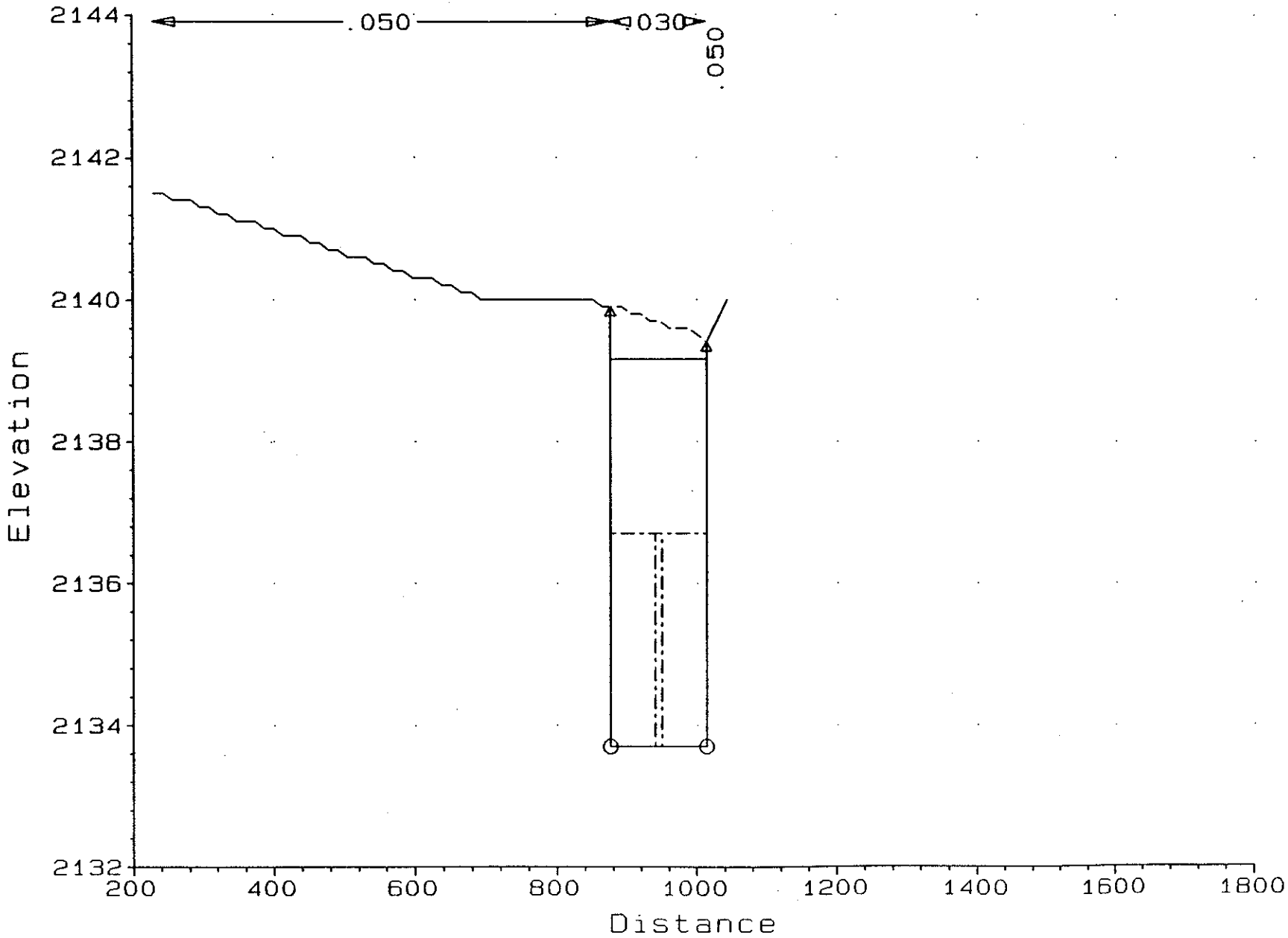

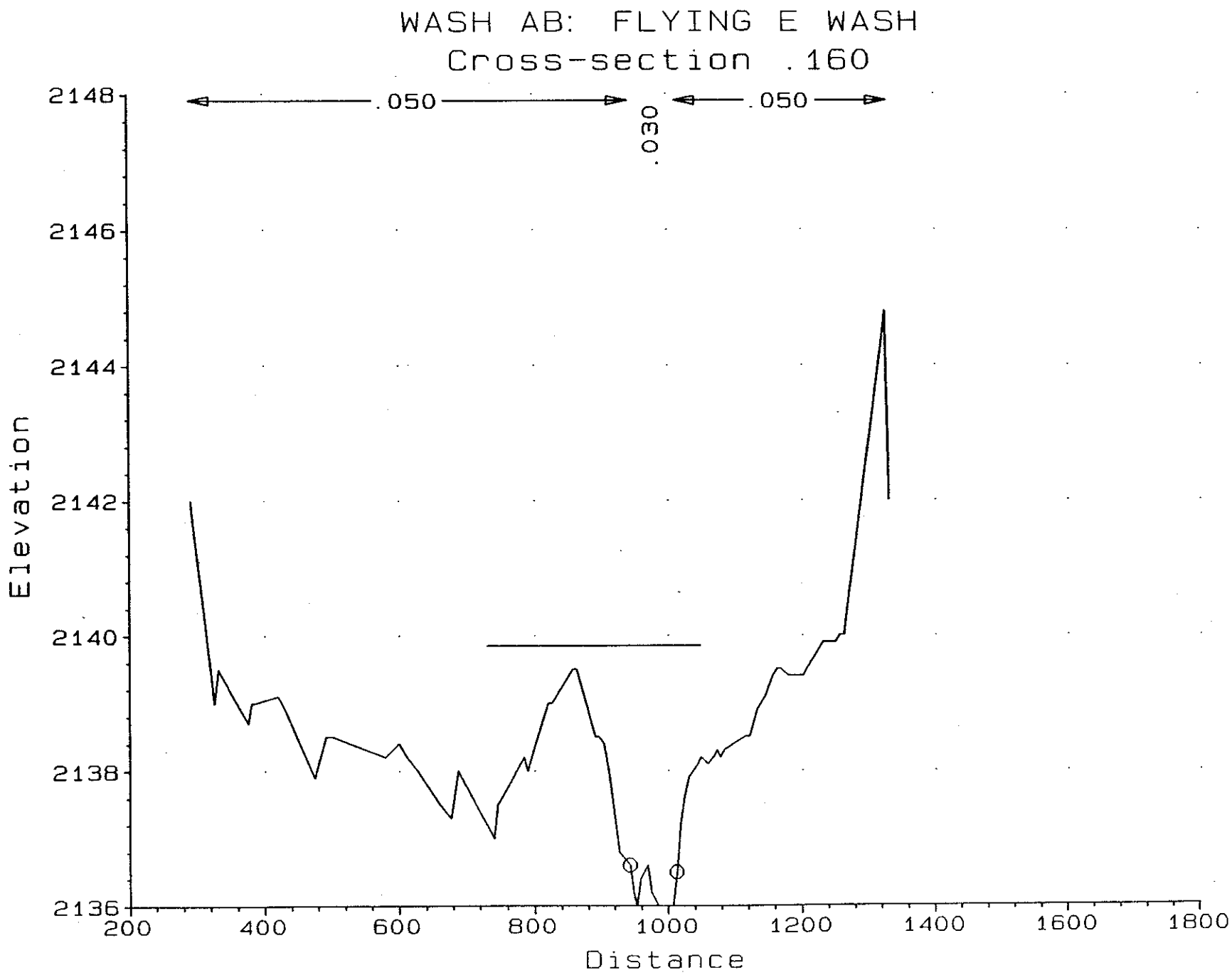
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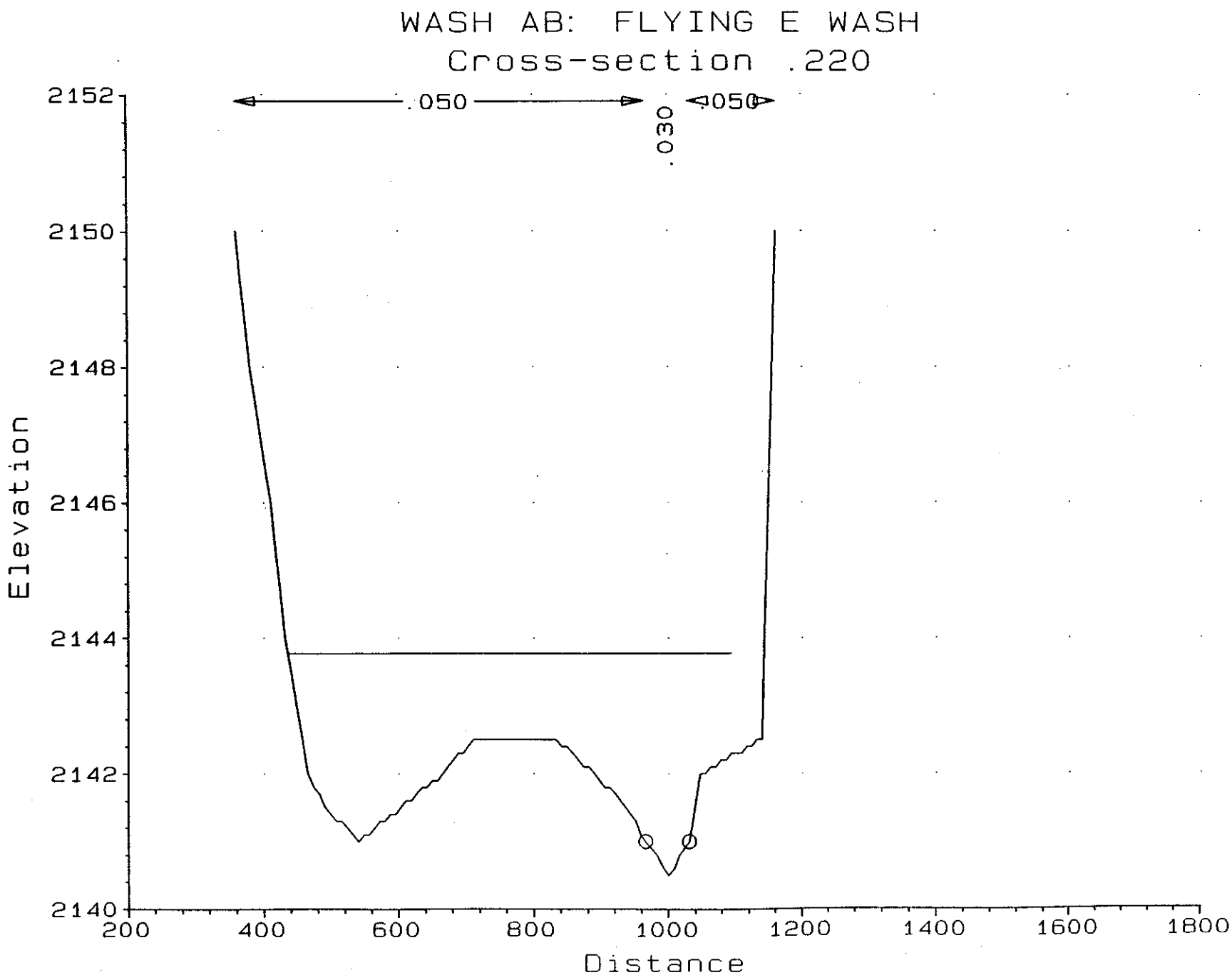
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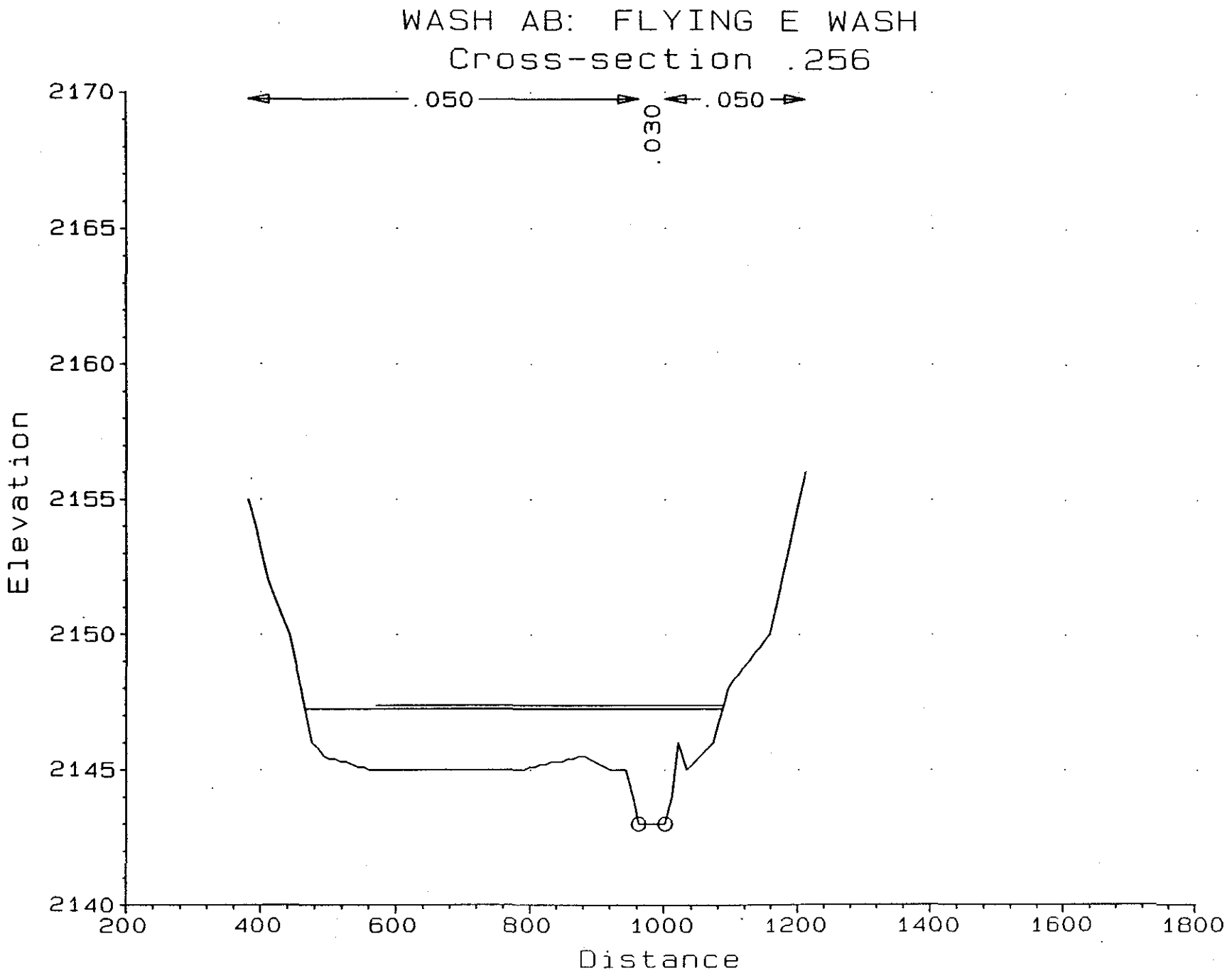
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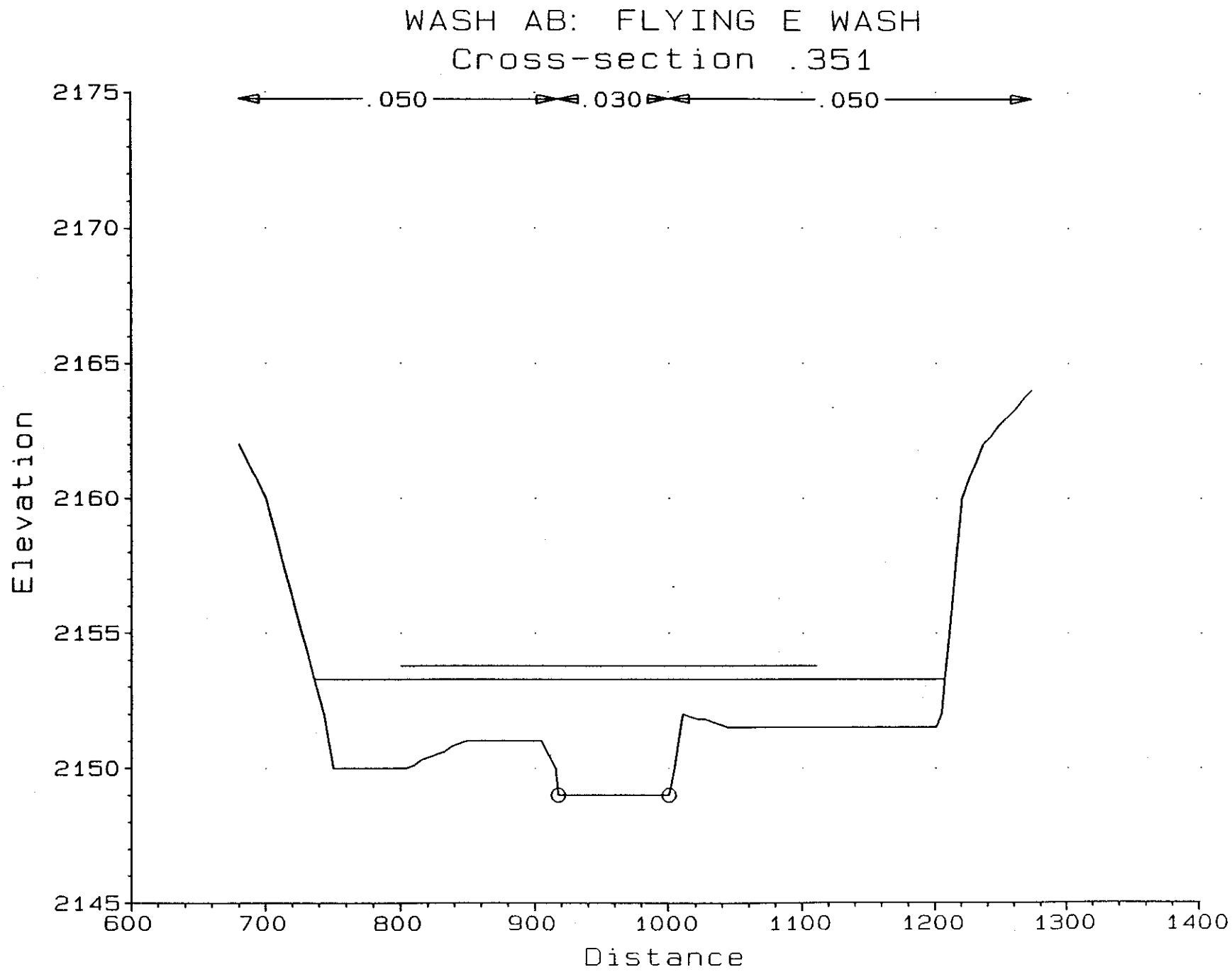
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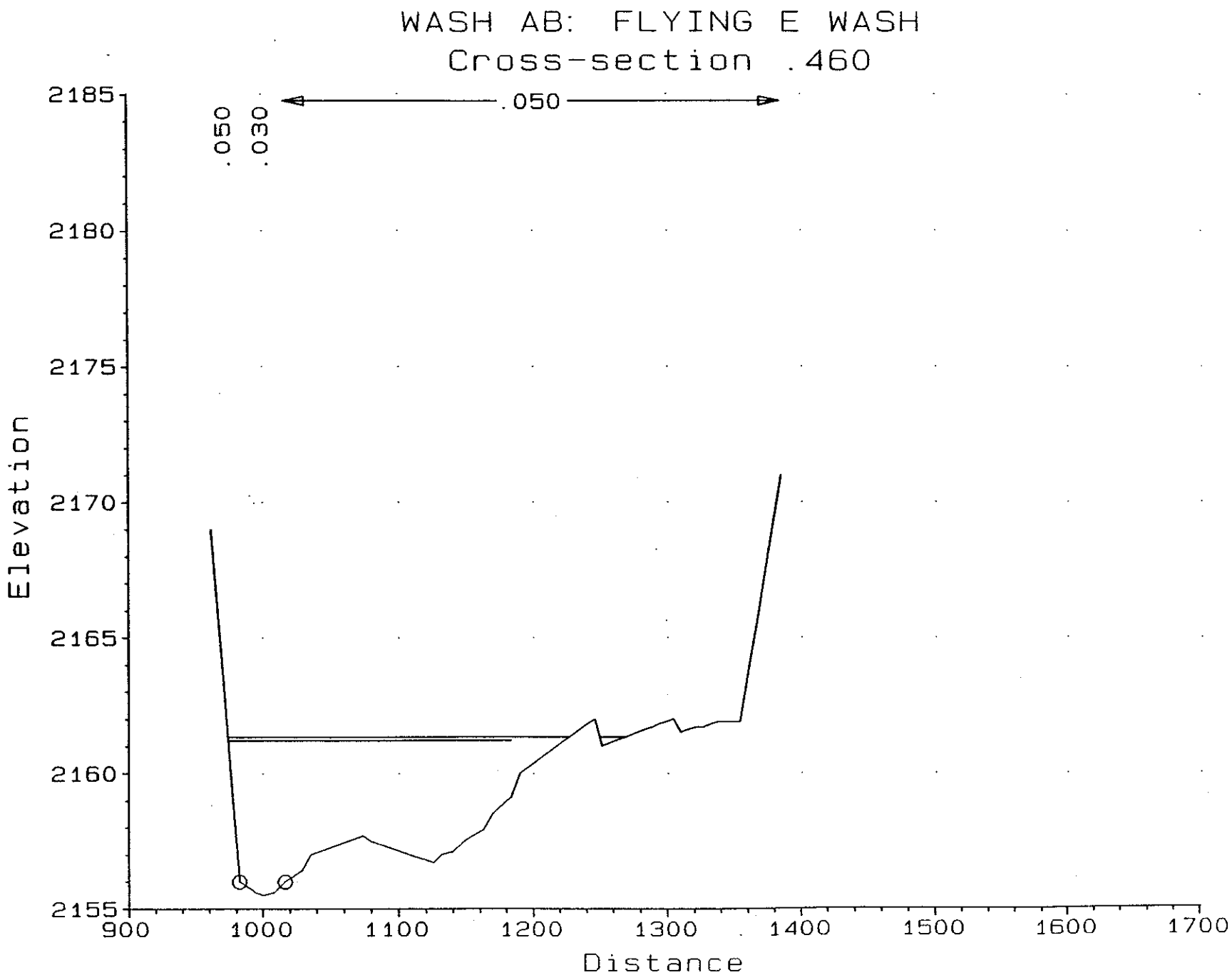
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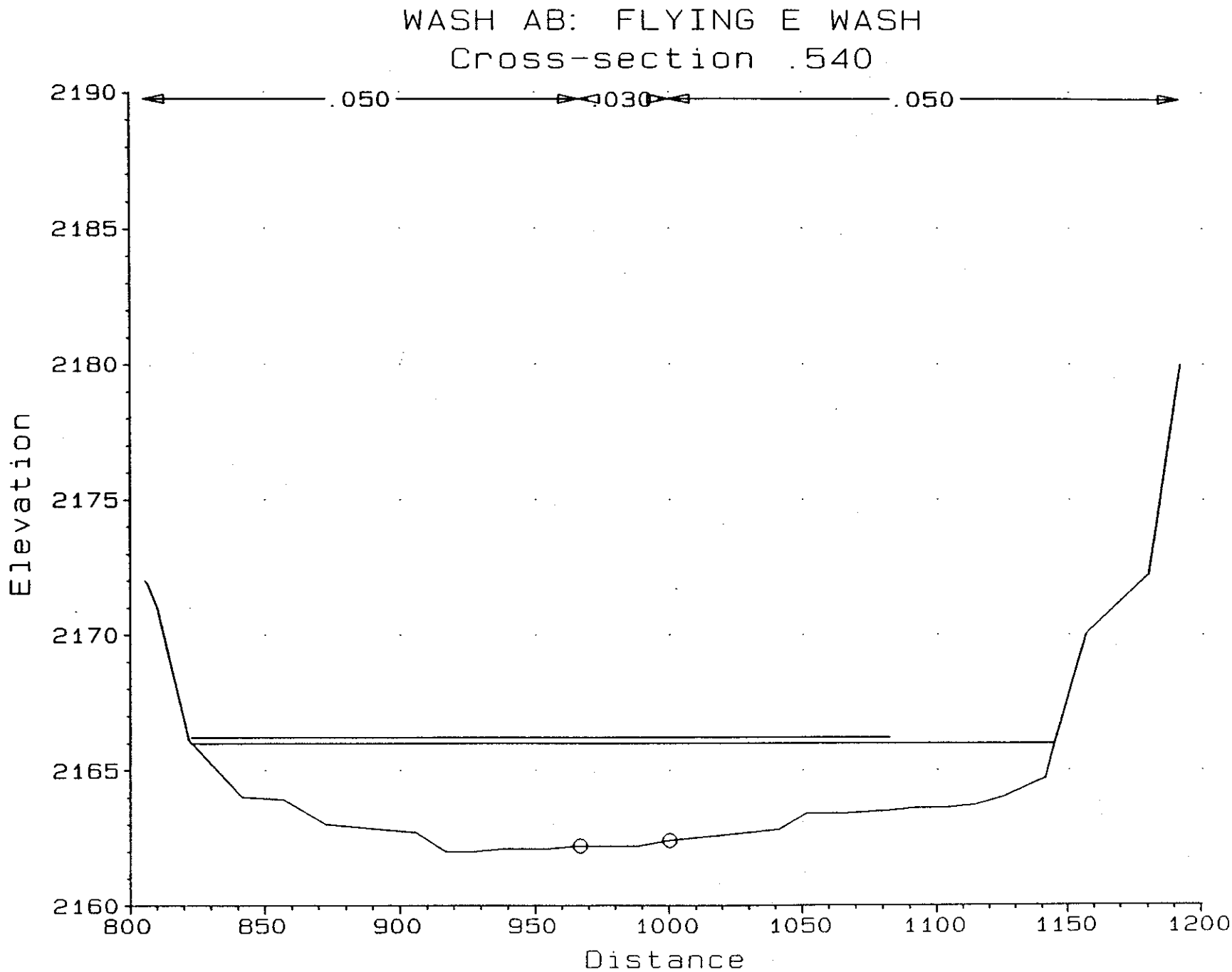
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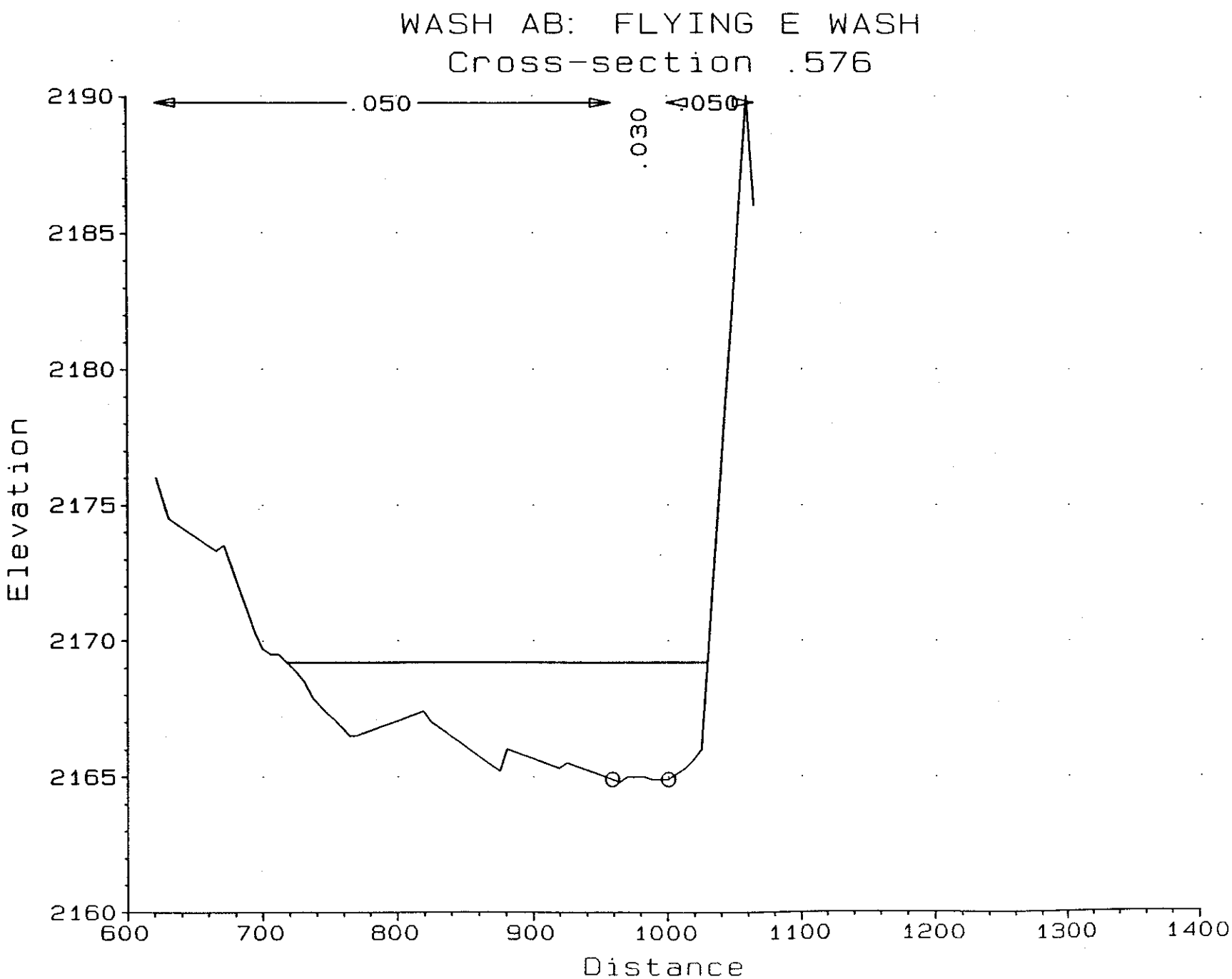
Distance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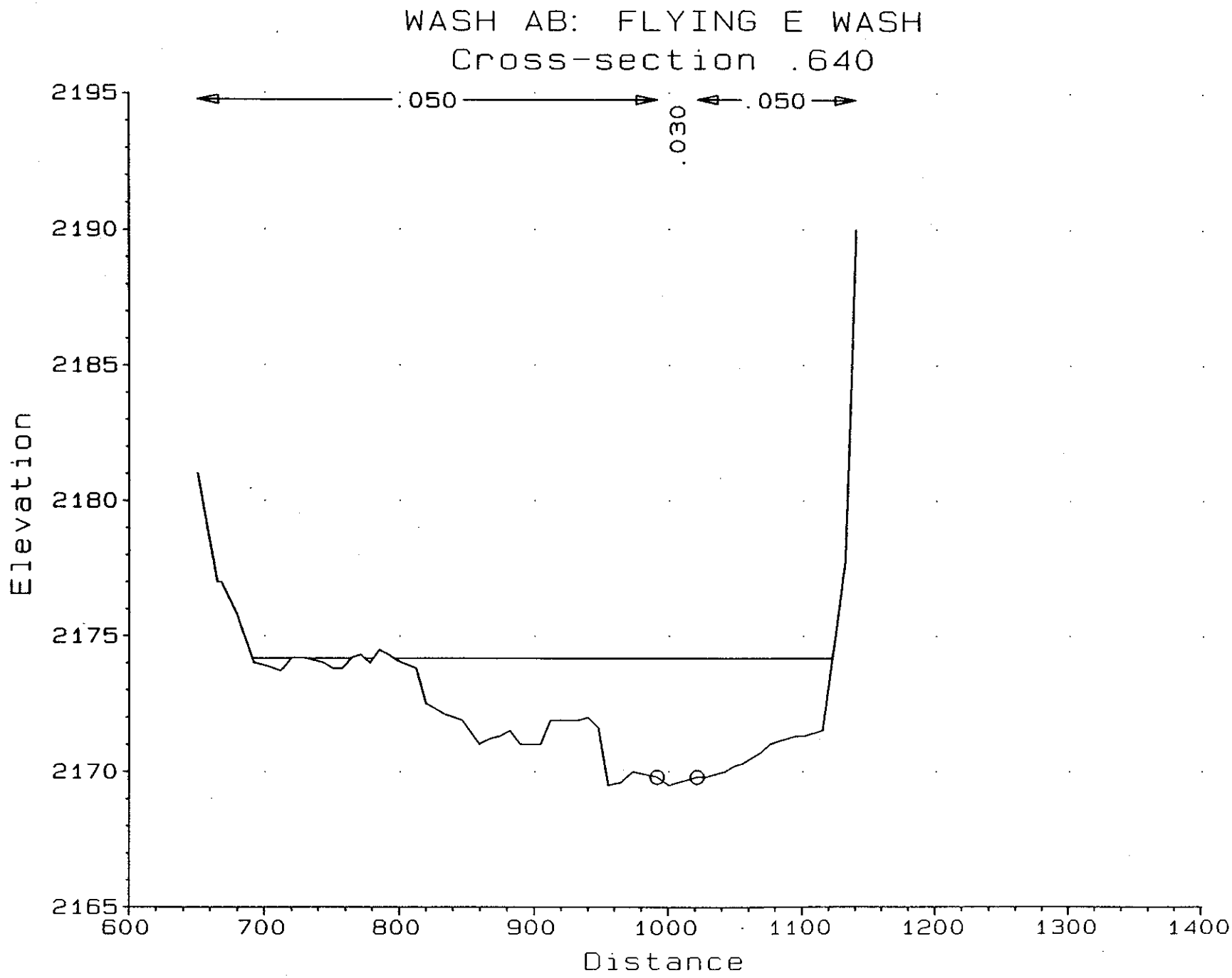
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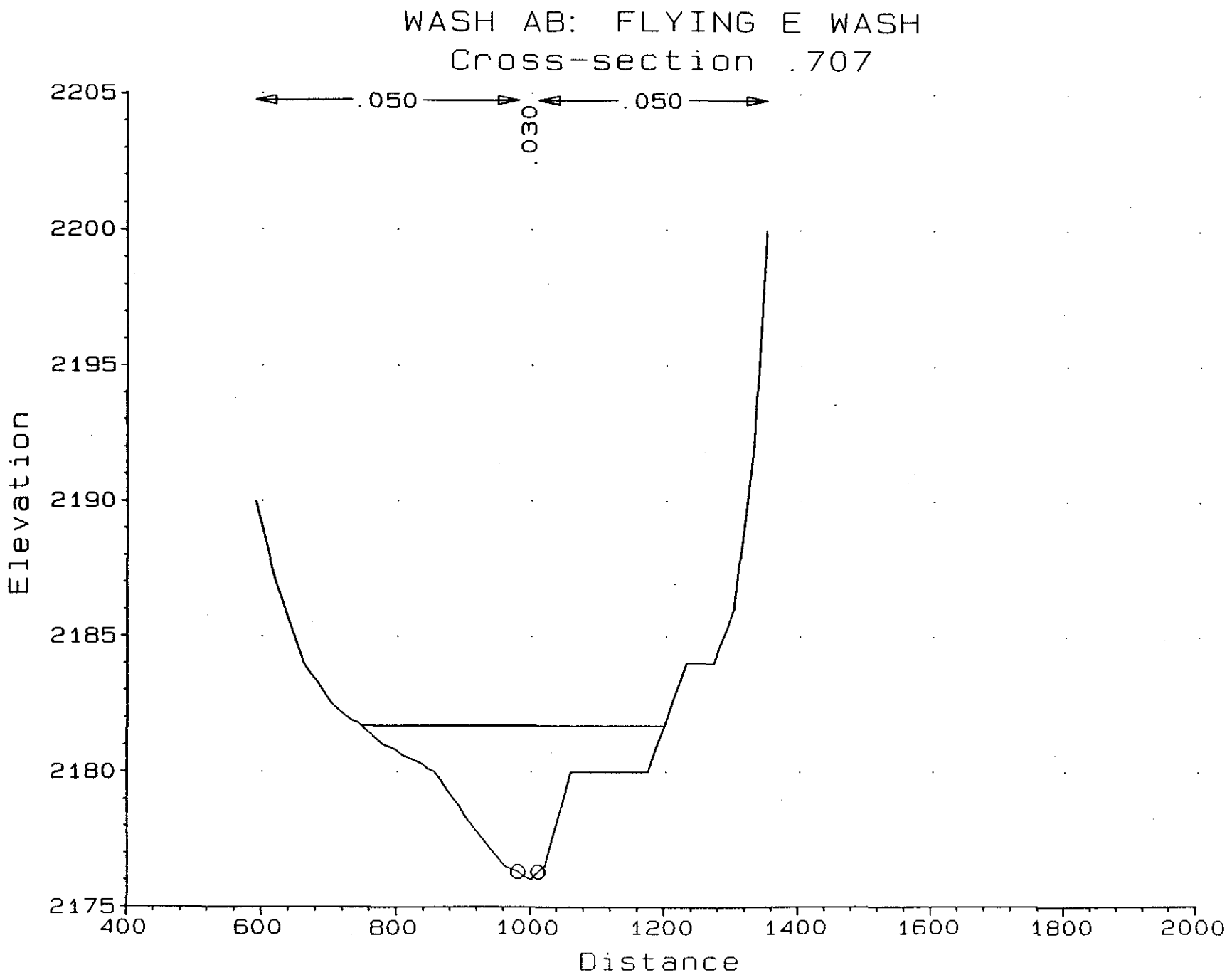
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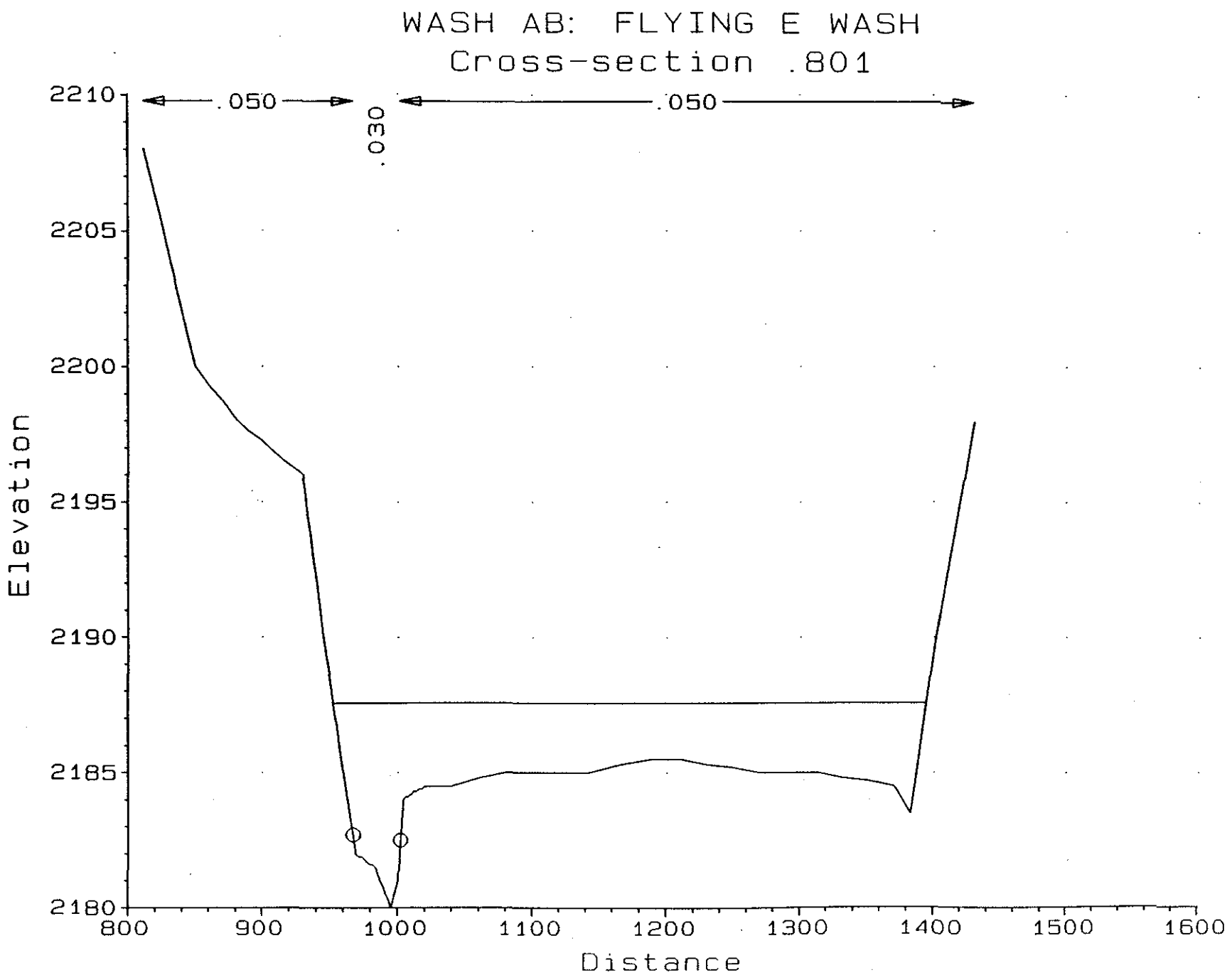
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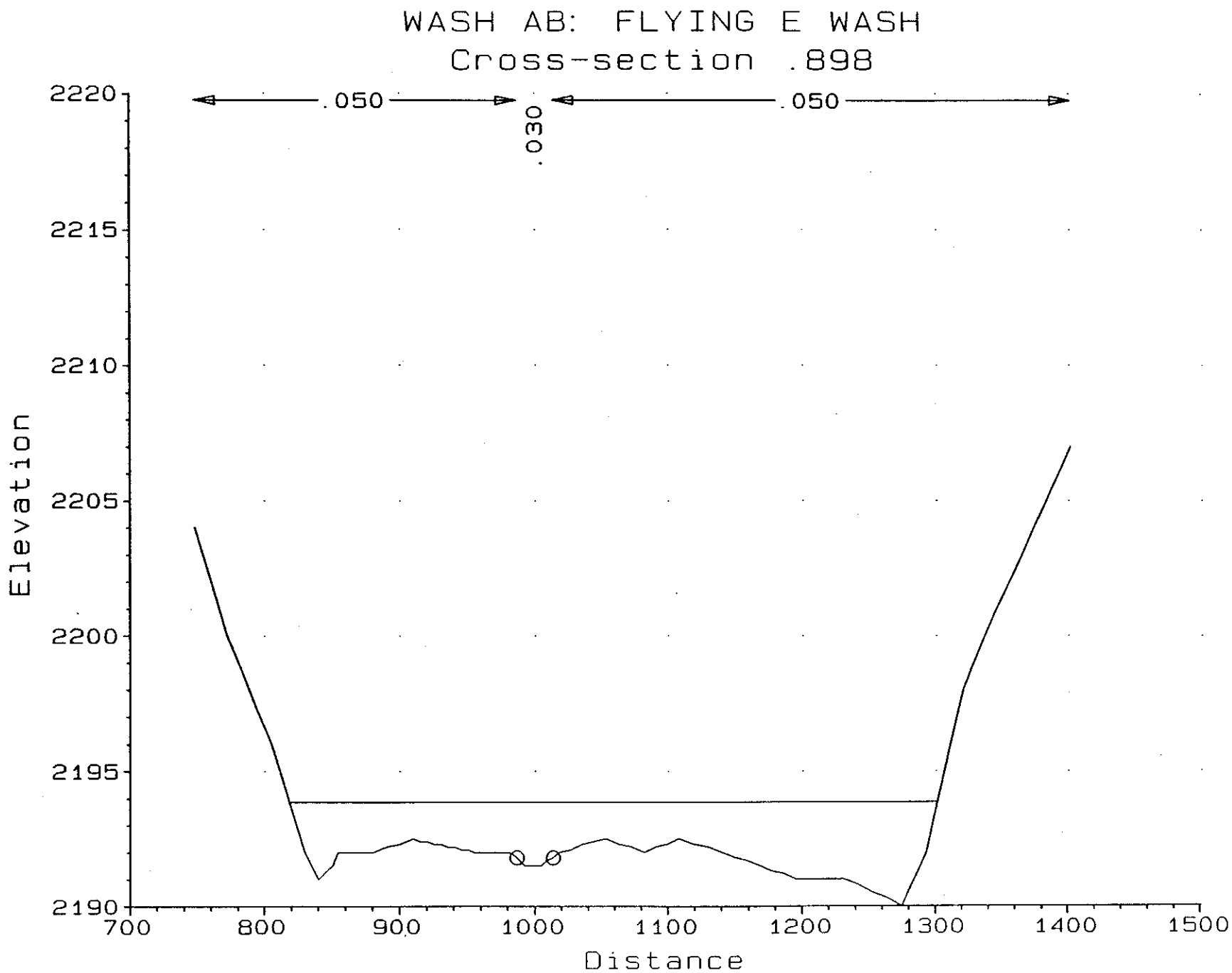
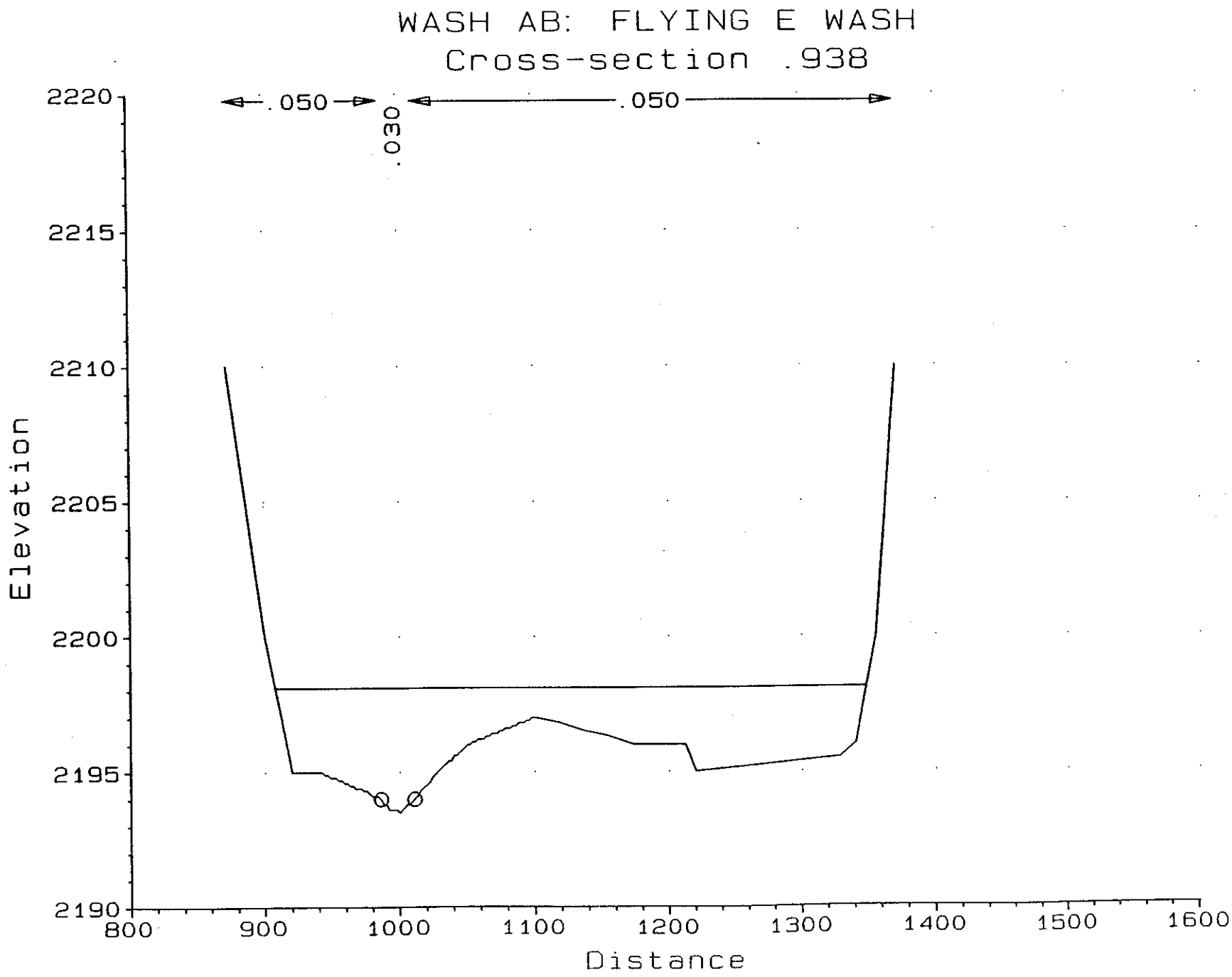
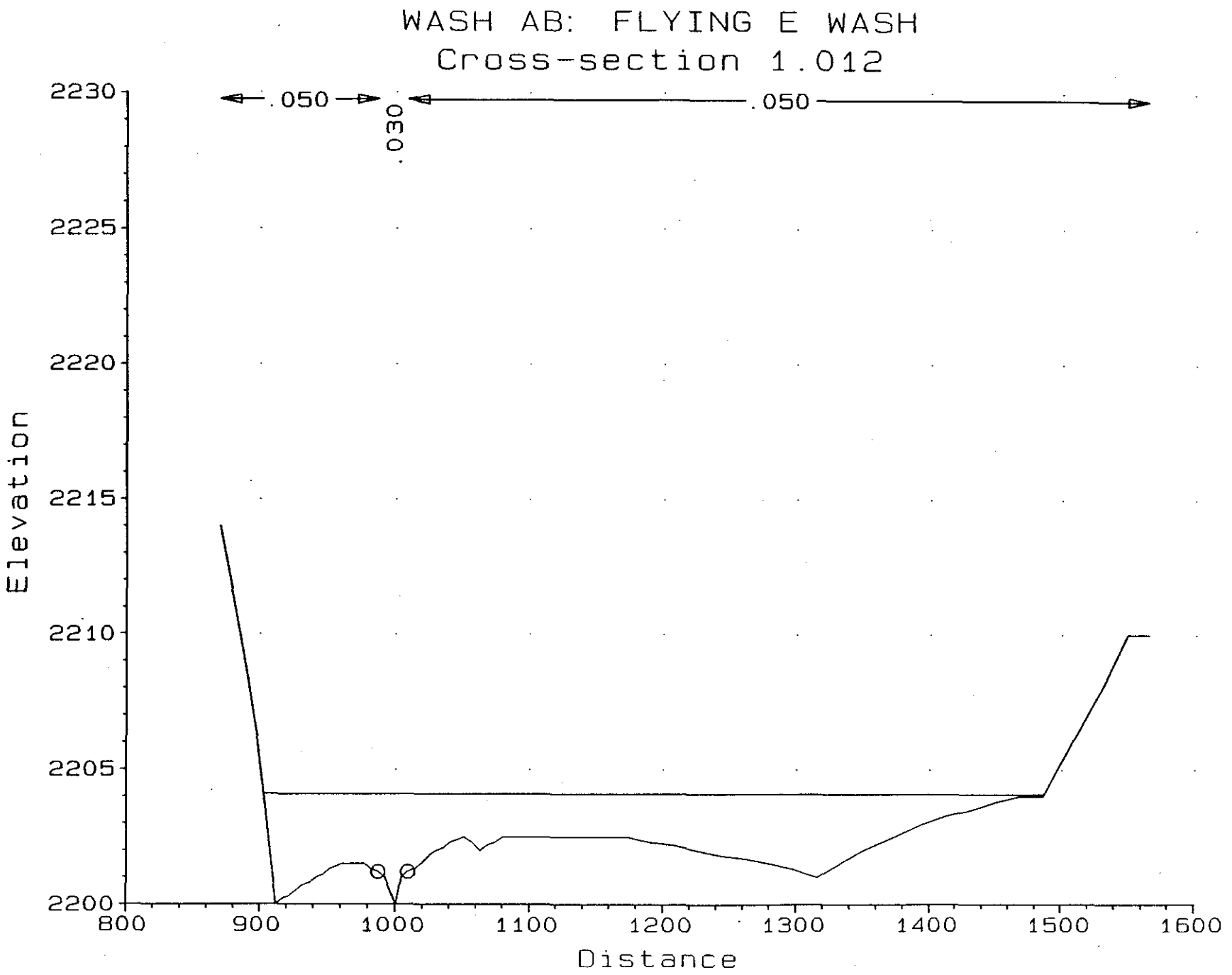
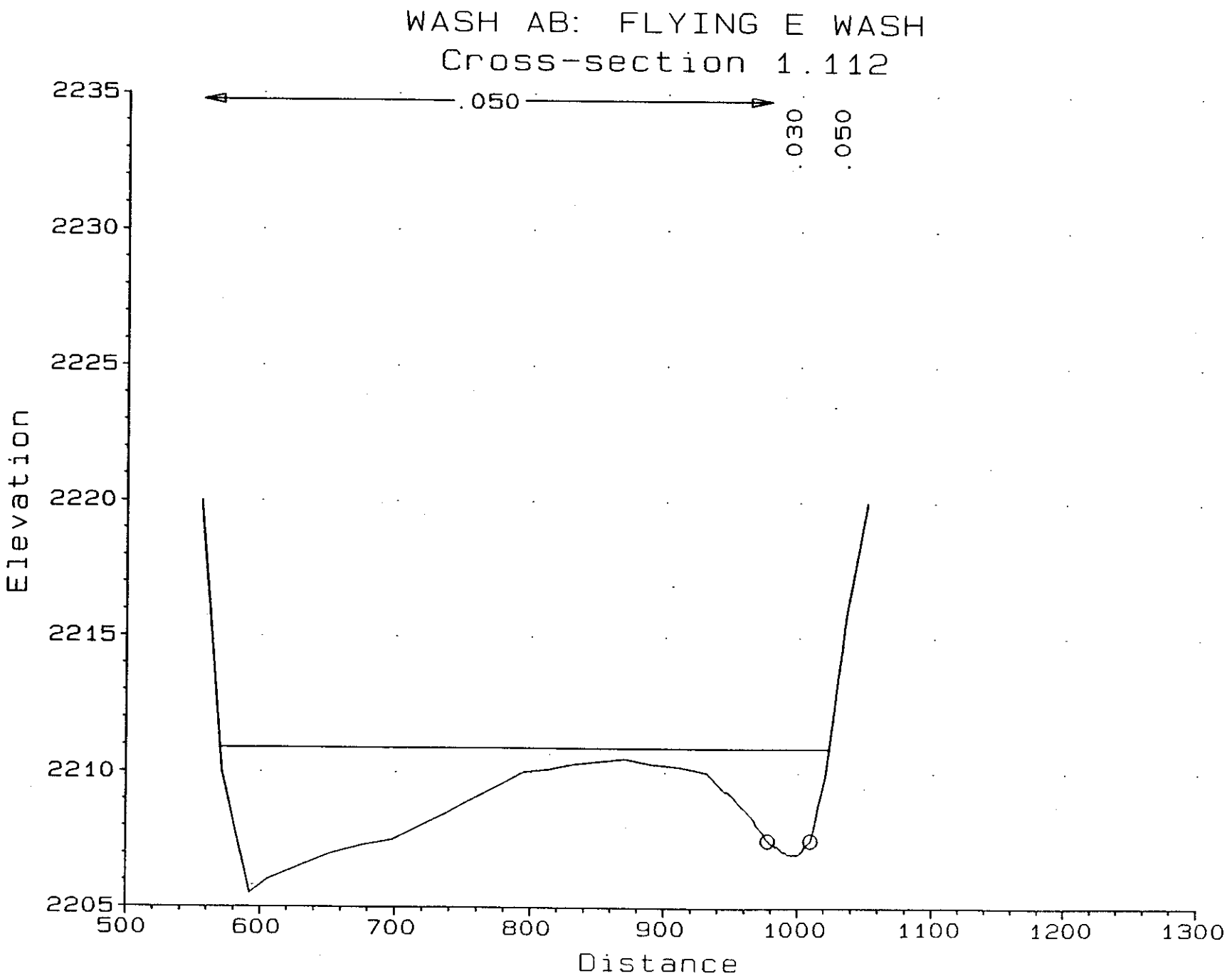
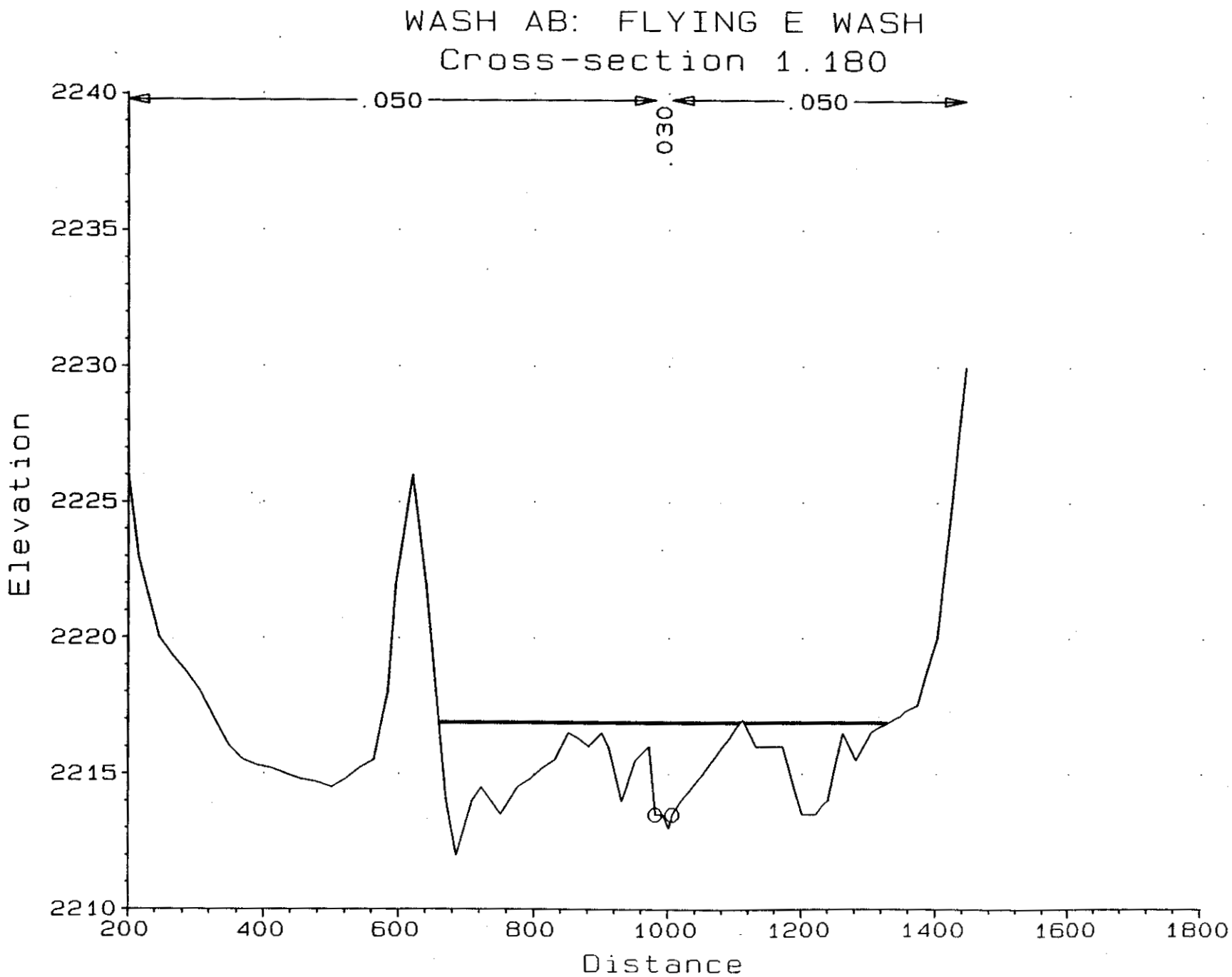
Cross-section .801
.050
.030
.050
Elevation
2210
2205
2200
2195
2190
2185
2180
800
900
1000
1100
1200
1300
1400
1500
1600
Distance

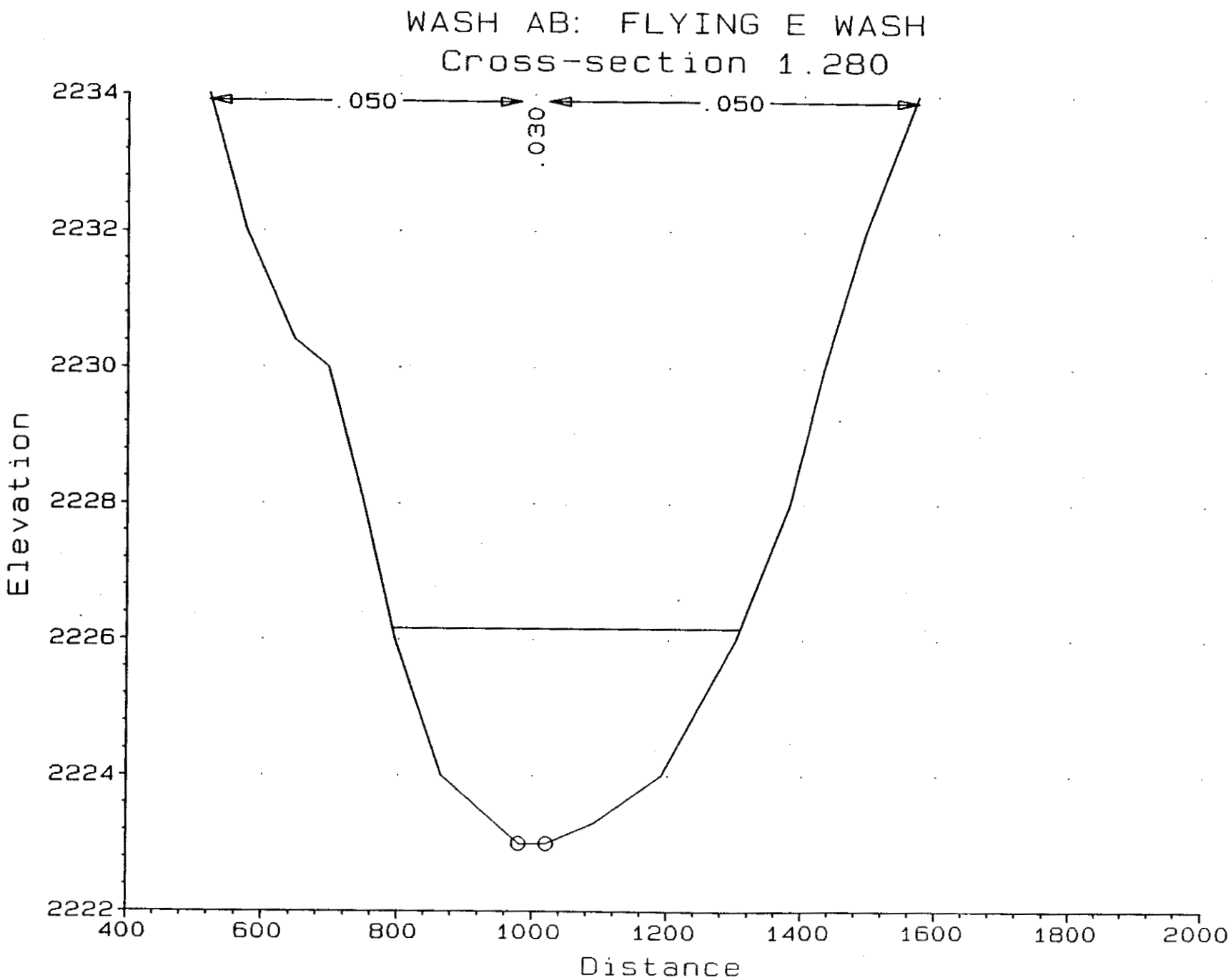

WASH AB: FLYING E WASH
Cross-section .898
.050
.030
.050
2220
2215
2210
2205
2200
2195
2190
Elevation
700
800
900
1000
1100
1200
1300
1400
1500
Distance

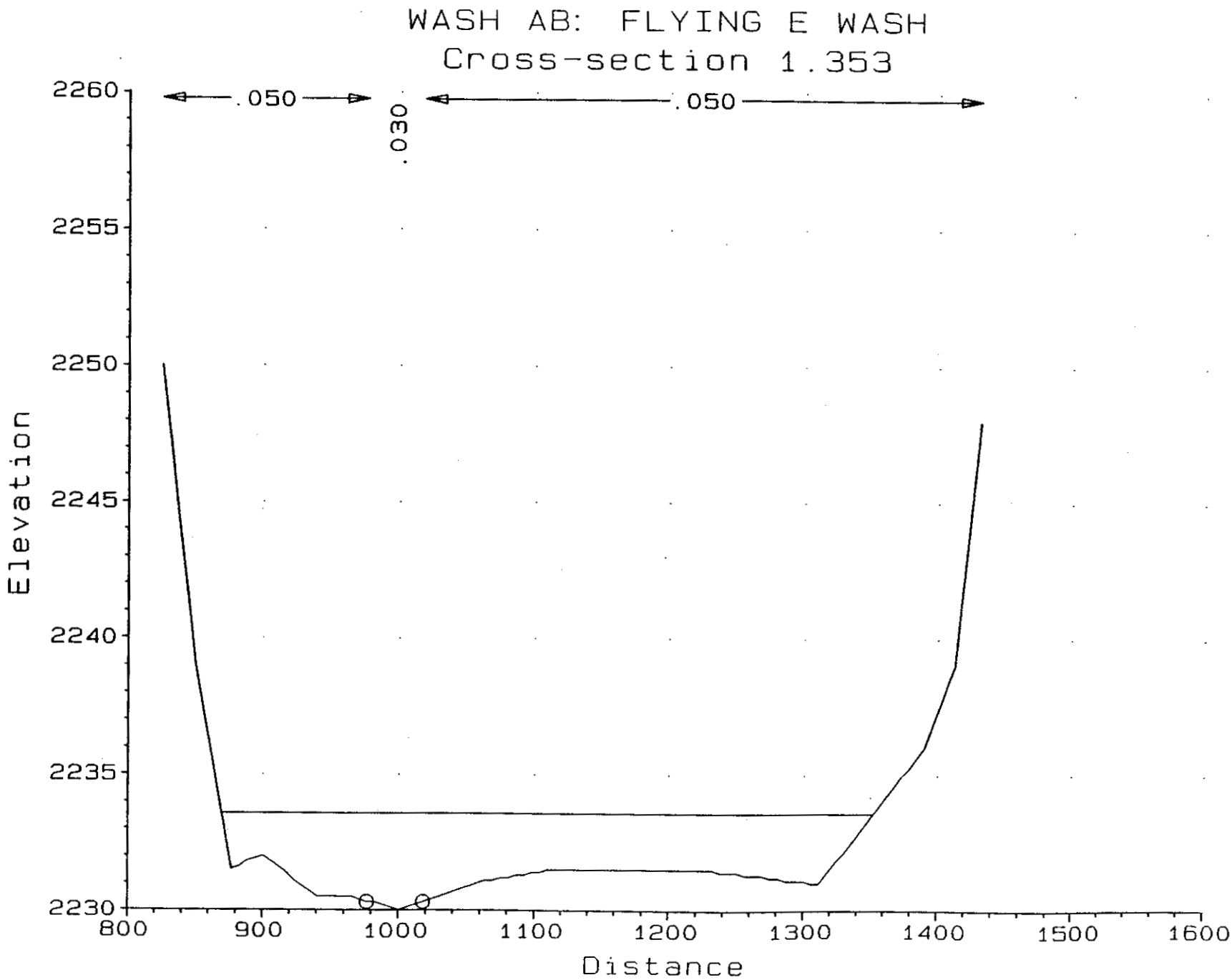

WASH AB: FLYING E WASH
Cross-section .938
.050
.030
.050
2220
2215
2210
2205
2200
2195
2190
Elevation
800
900
1000
1100
1200
1300
1400
1500
1600
Distance

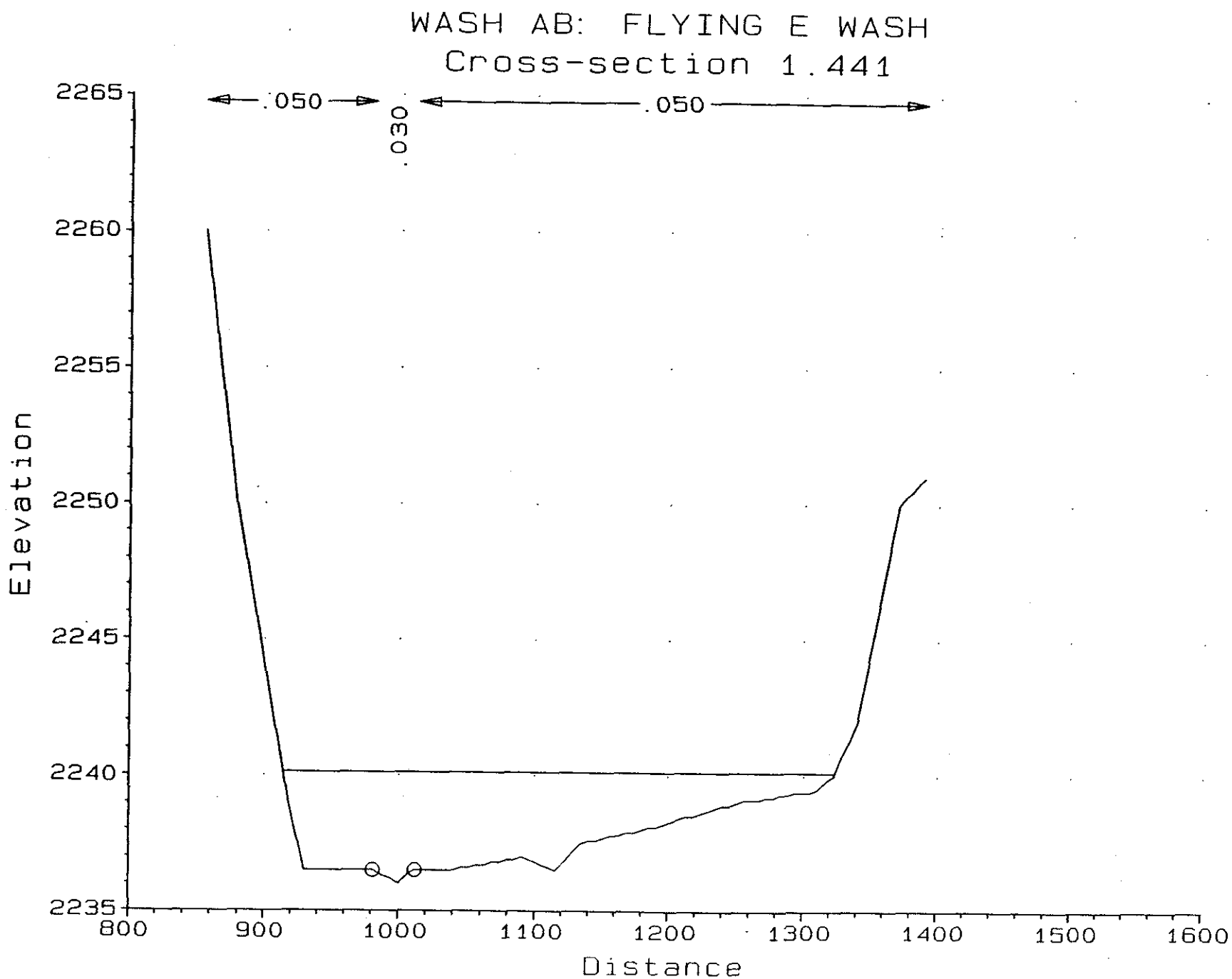

WASH AB: FLYING E WASH
Cross-section 1.012
.050
.030
.050
Elevation
2230
2225
2220
2215
2210
2205
2200
800
900
1000
1100
1200
1300
1400
1500
1600
Distance

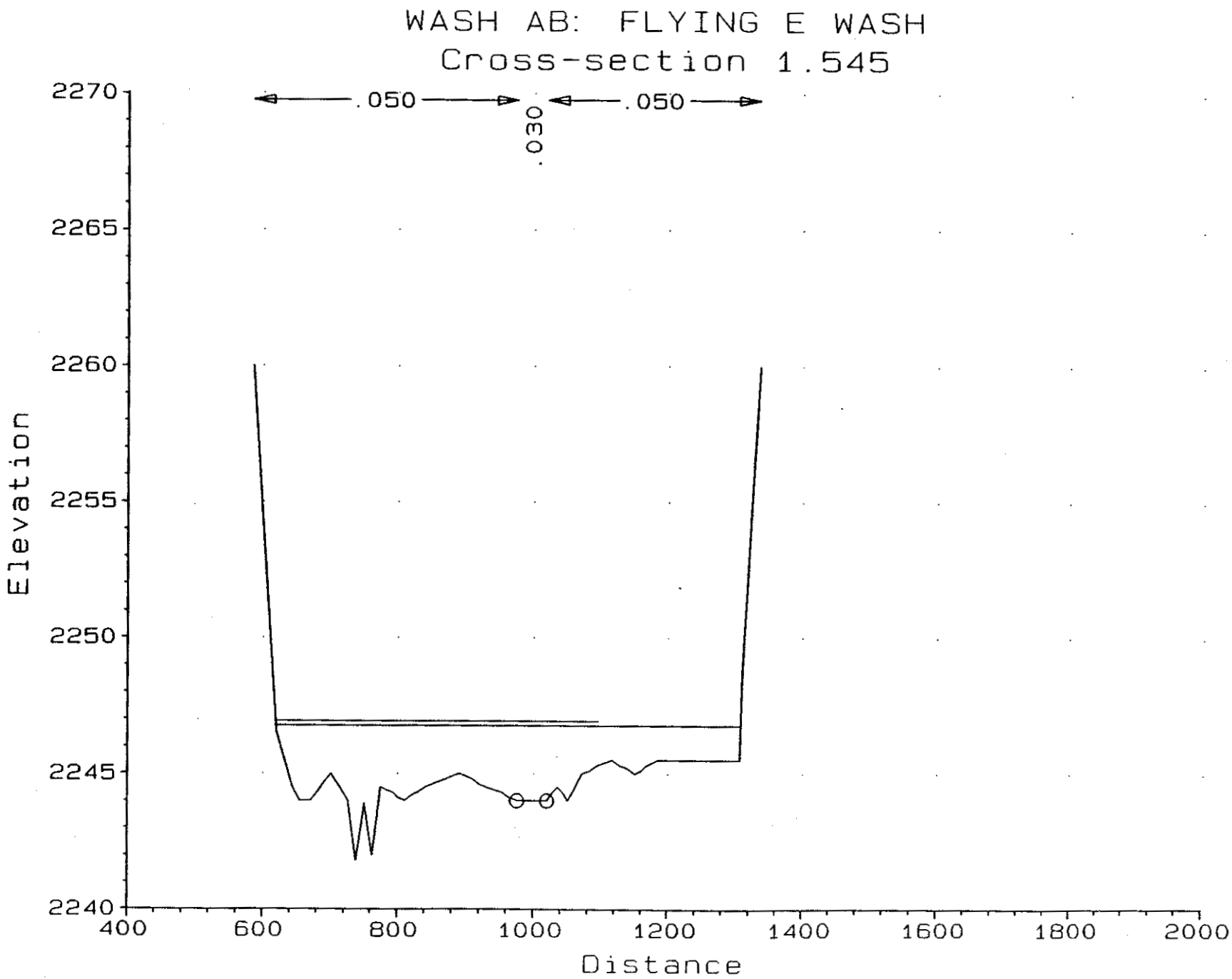

WASH AB: FLYING E WASH
Cross-section 1.112
.050
.030
.050
Elevation
2235
2230
2225
2220
2215
2210
2205
500
600
700
800
900
1000
1100
1200
1300
Distance

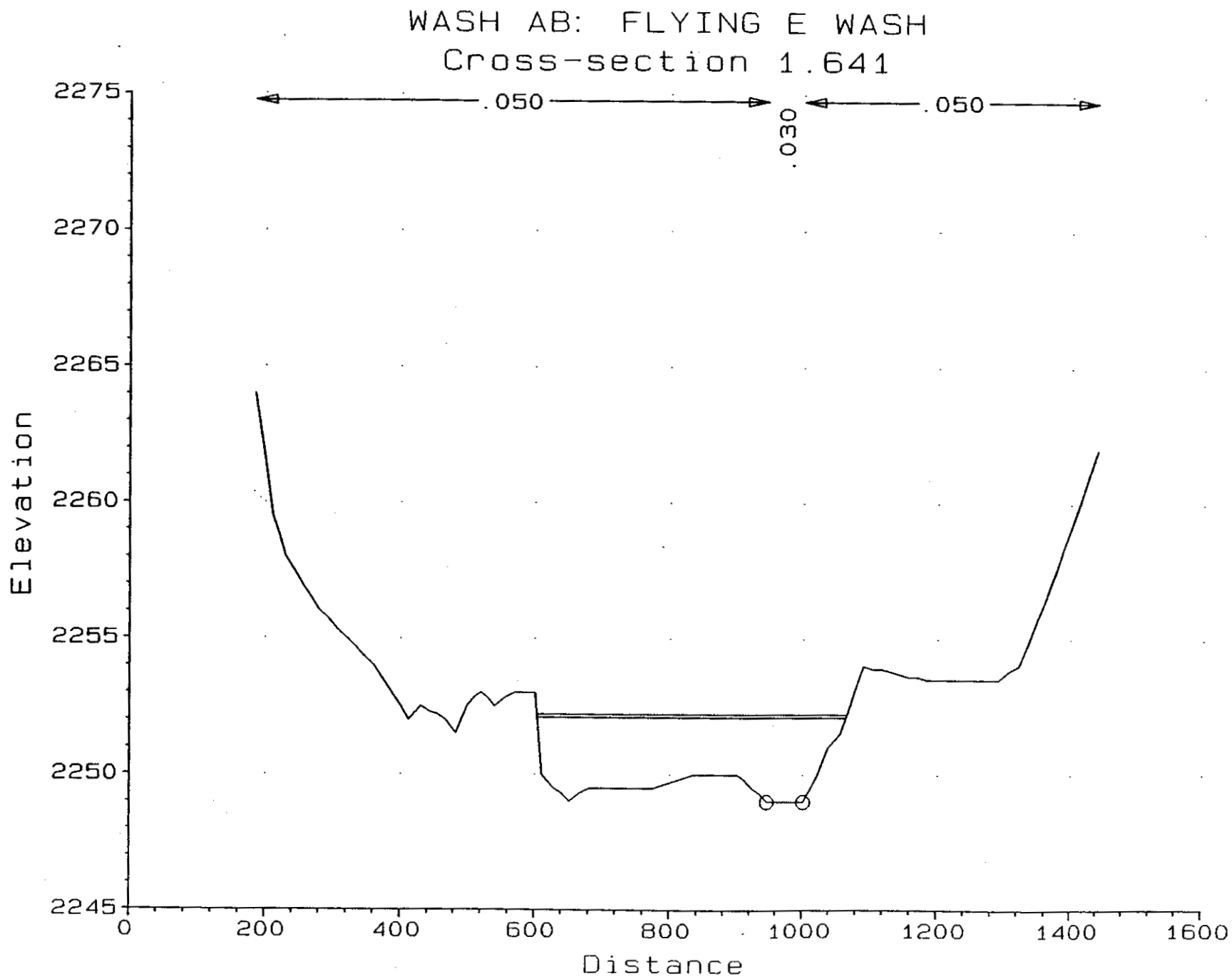

WASH AB: FLYING E WASH
Cross-section 1.180
.050
.030
.050
Elevation
2240
2235
2230
2225
2220
2215
2210
200
400
600
800
1000
1200
1400
1600
1800
Distance

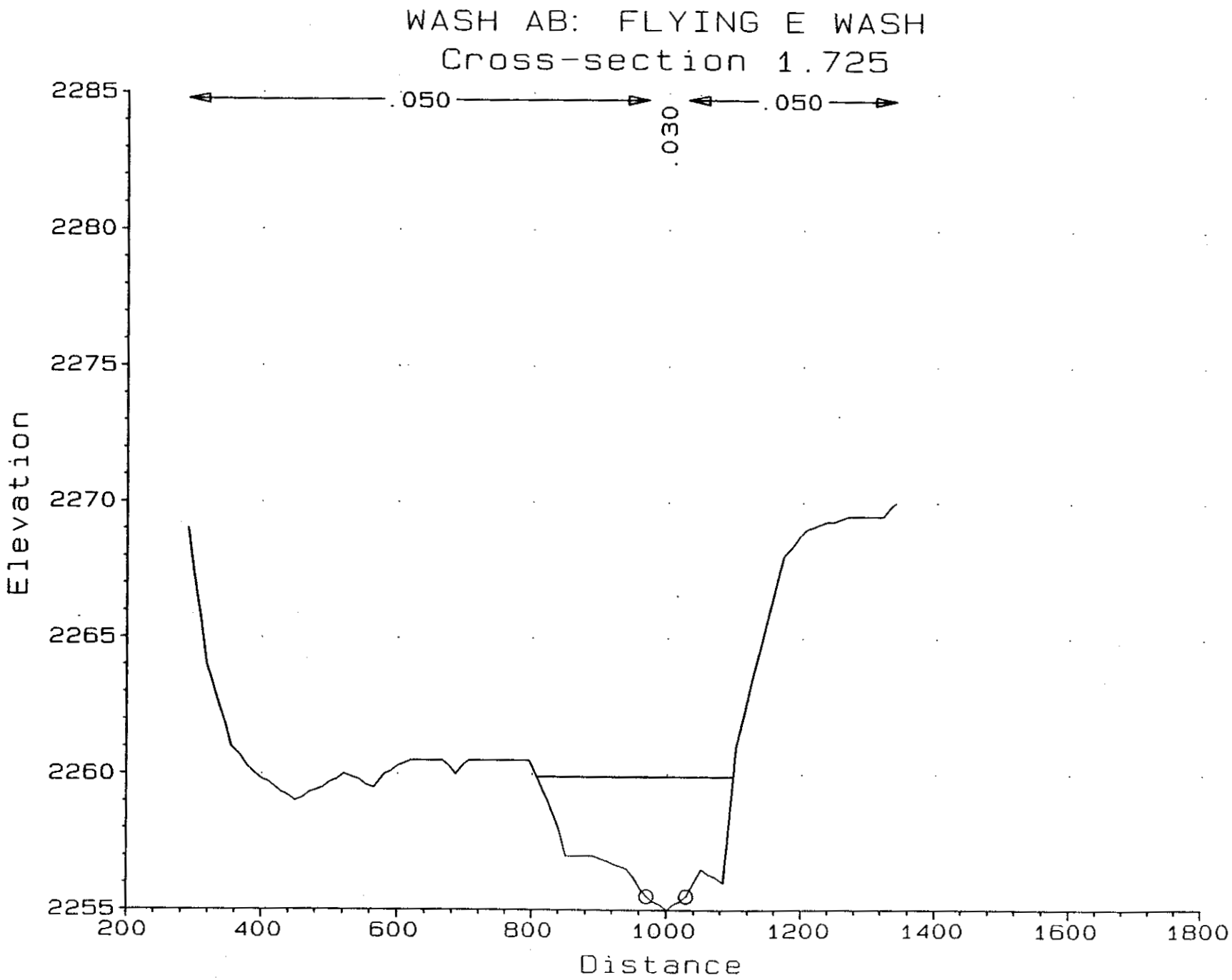

WASH AB: FLYING E WASH
Cross-section 1.280
.050
.030
.050
2234
2232
2230
2228
2226
2224
2222
Elevation
400
600
800
1000
1200
1400
1600
1800
2000
Distance

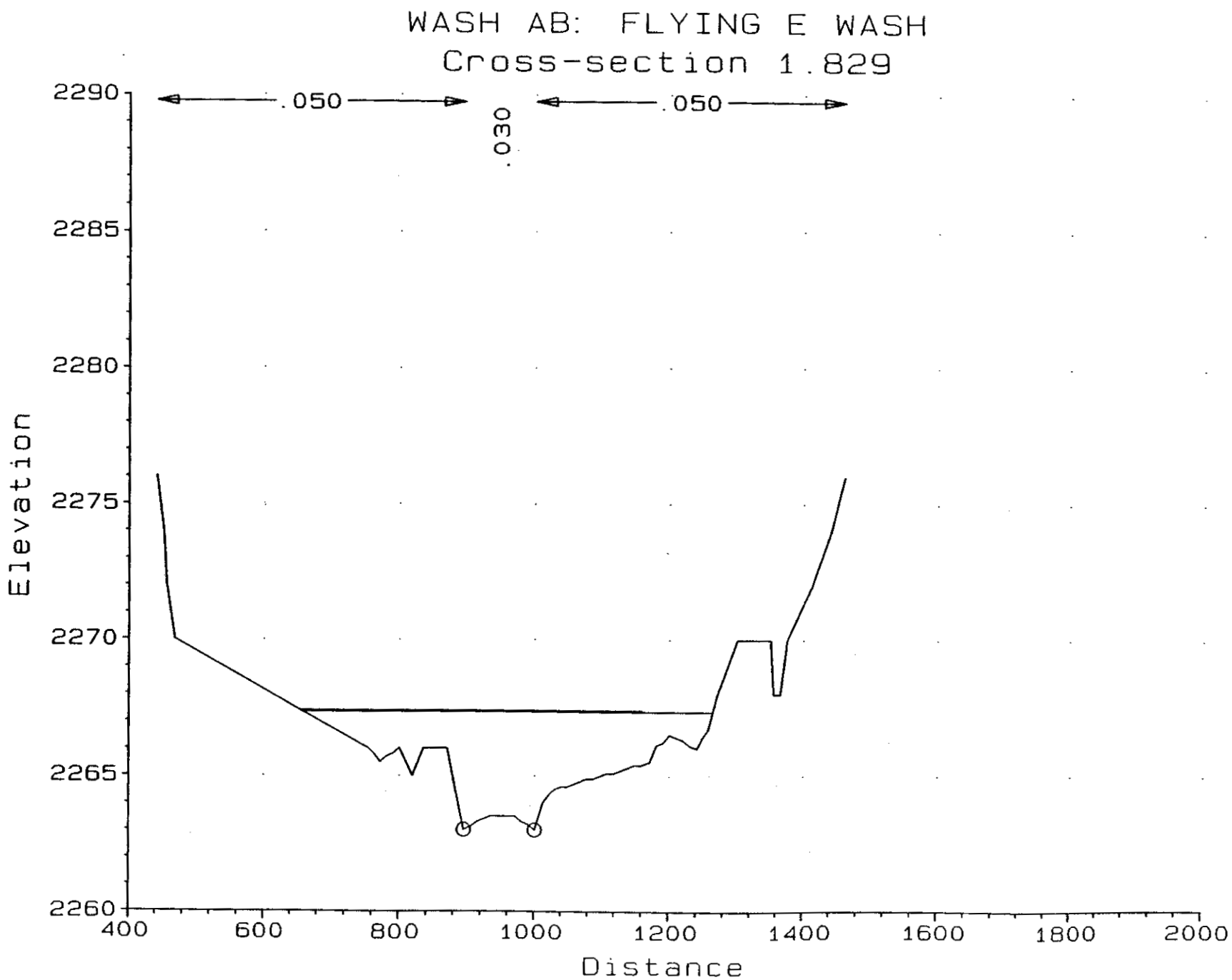

WASH AB: FLYING E WASH
Cross-section 1.353
.050
.030
.050
Elevation
2260
2255
2250
2245
2240
2235
2230
800
900
1000
1100
1200
1300
1400
1500
1600
Distance


WASH AB: FLYING E WASH
Cross-section 1.441
.050
.030
.050
Elevation
2265
2260
2255
2250
2245
2240
2235
800
900
1000
1100
1200
1300
1400
1500
1600
Distance

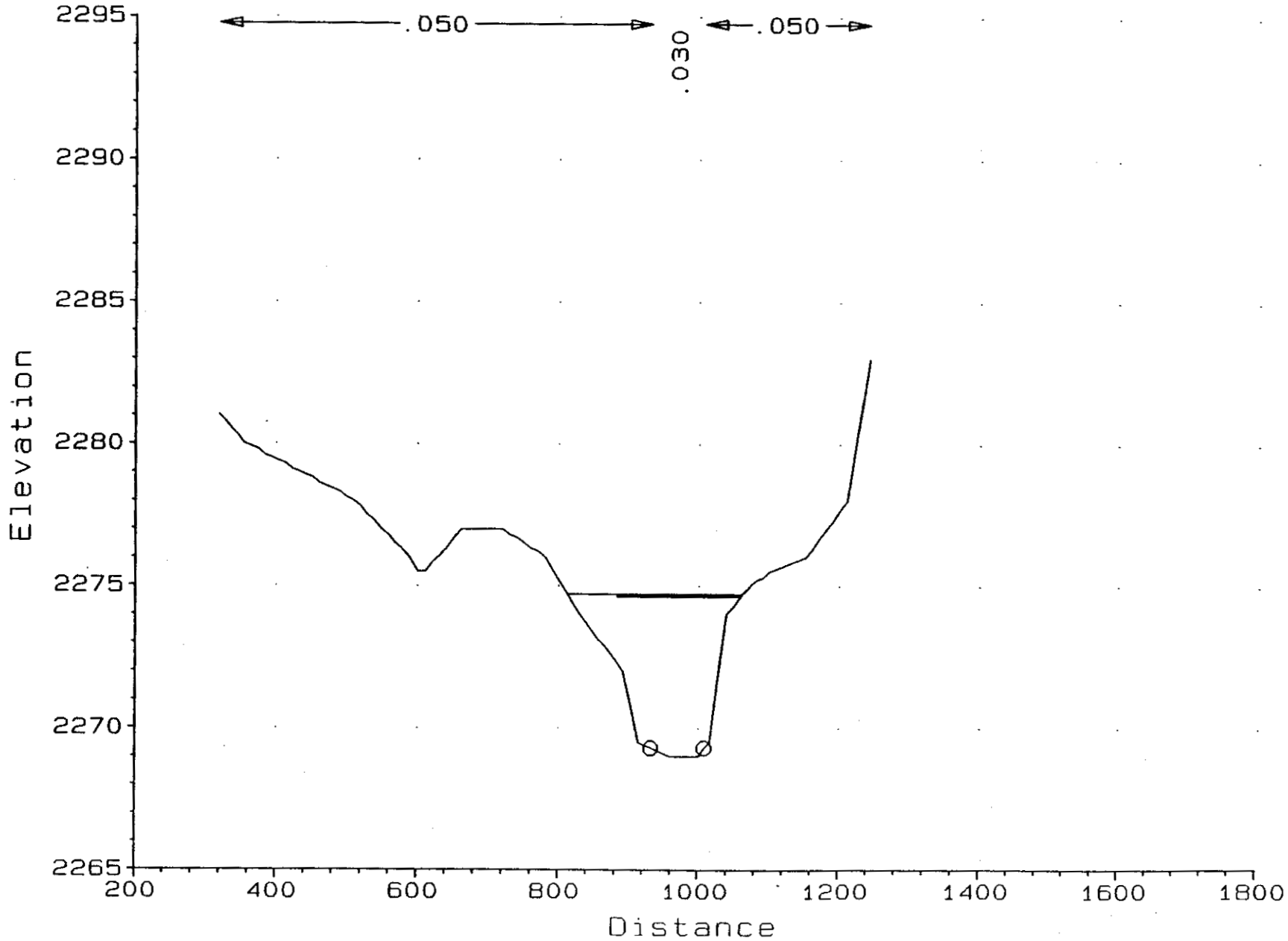

WASH AB: FLYING E WASH
Cross-section 1.545
.050
.050
.030
Elevation
2270
2265
2260
2255
2250
2245
2240
400
600
800
1000
1200
1400
1600
1800
2000
Distance

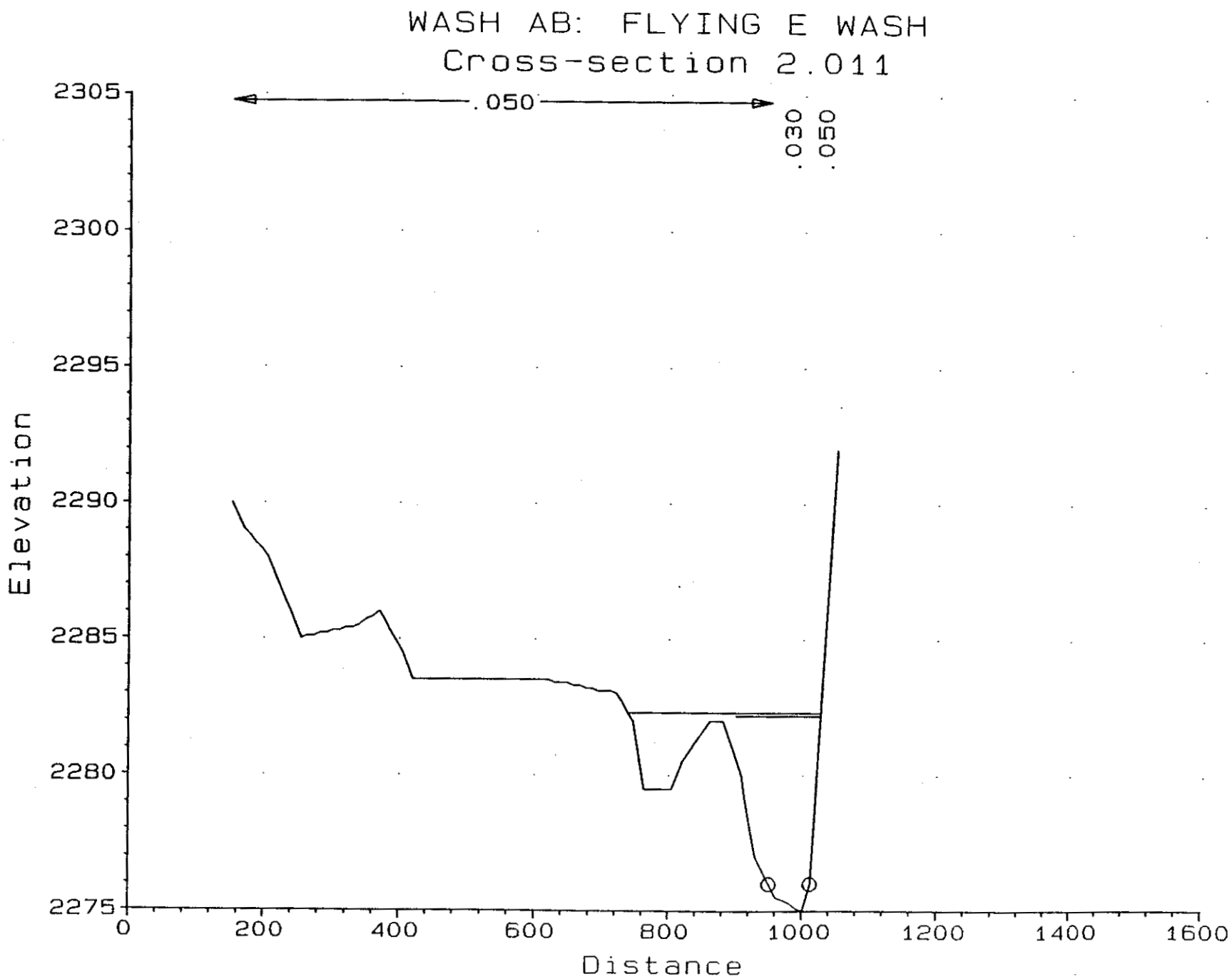

WASH AB: FLYING E WASH
Cross-section 1.641
.050
.030
.050
Elevation
2275
2270
2265
2260
2255
2250
2245
0
200
400
600
800
1000
1200
1400
1600
Distance

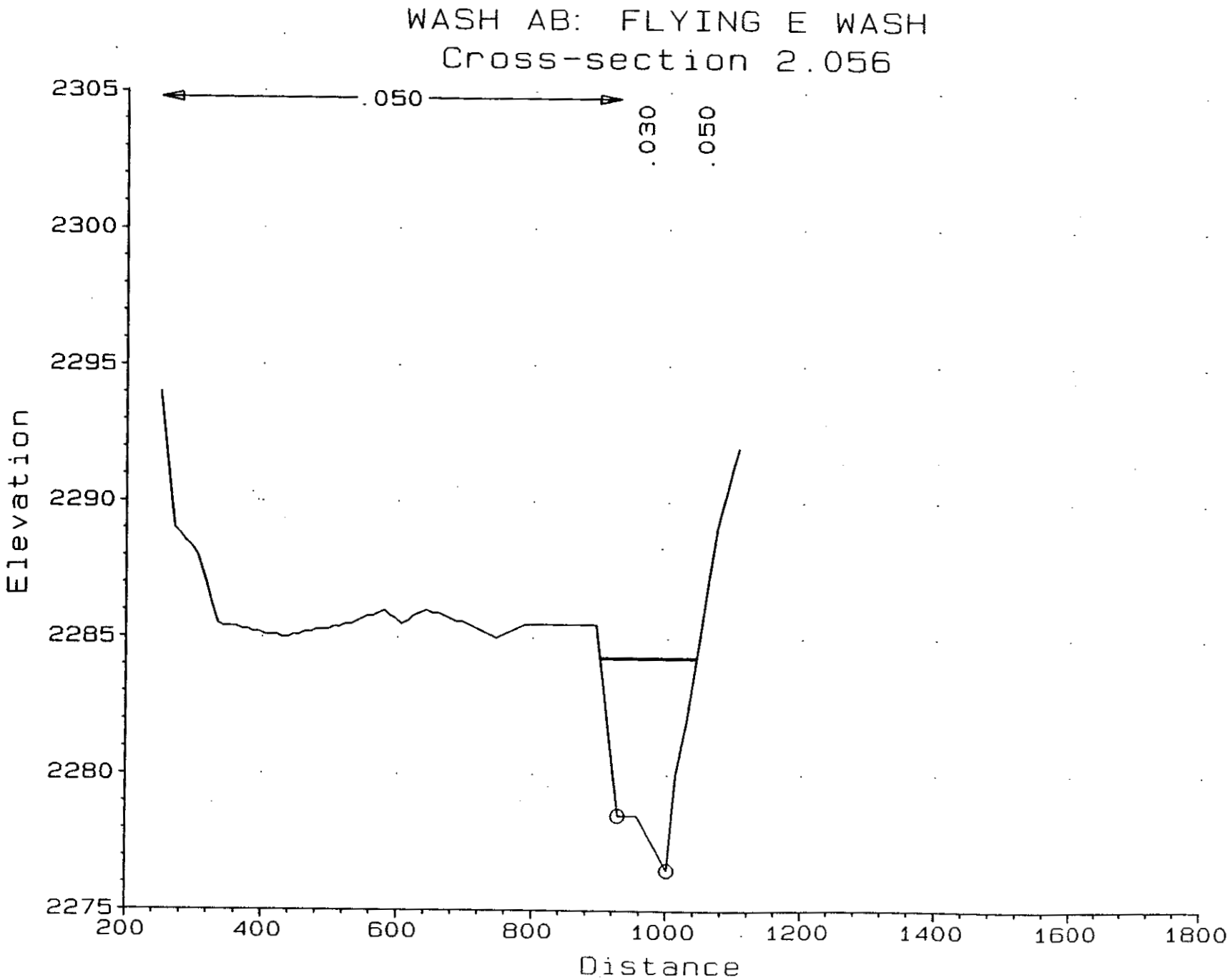

WASH AB: FLYING E WASH
Cross-section 1.725
.050
.030
.050
Elevation
2285
2280
2275
2270
2265
2260
2255
200
400
600
800
1000
1200
1400
1600
1800
Distance

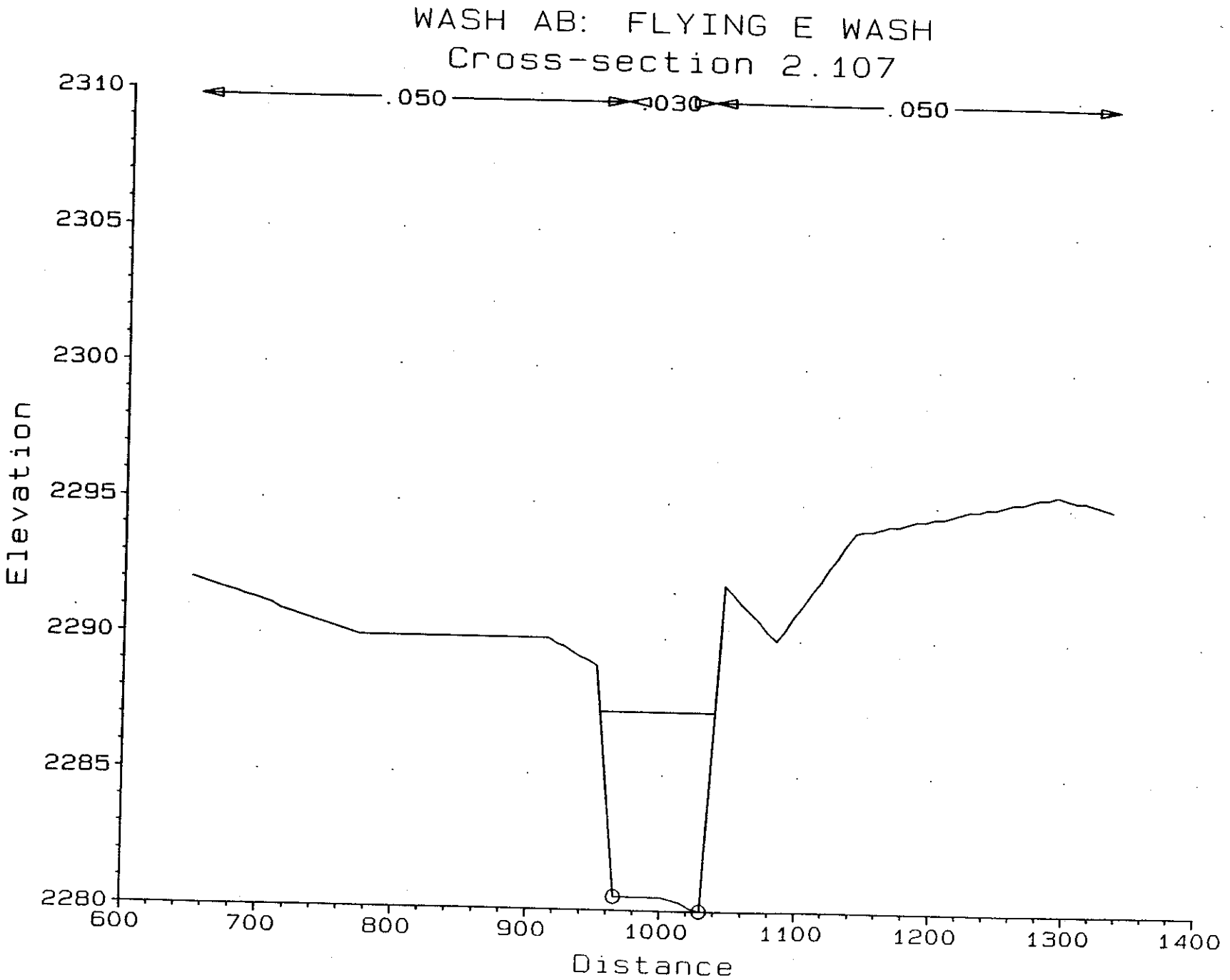

WASH AB: FLYING E WASH
Cross-section 1.829
.050
.050
.030
2290
2285
2280
2275
2270
2265
2260
Elevation
400
600
800
1000
1200
1400
1600
1800
2000
Distance

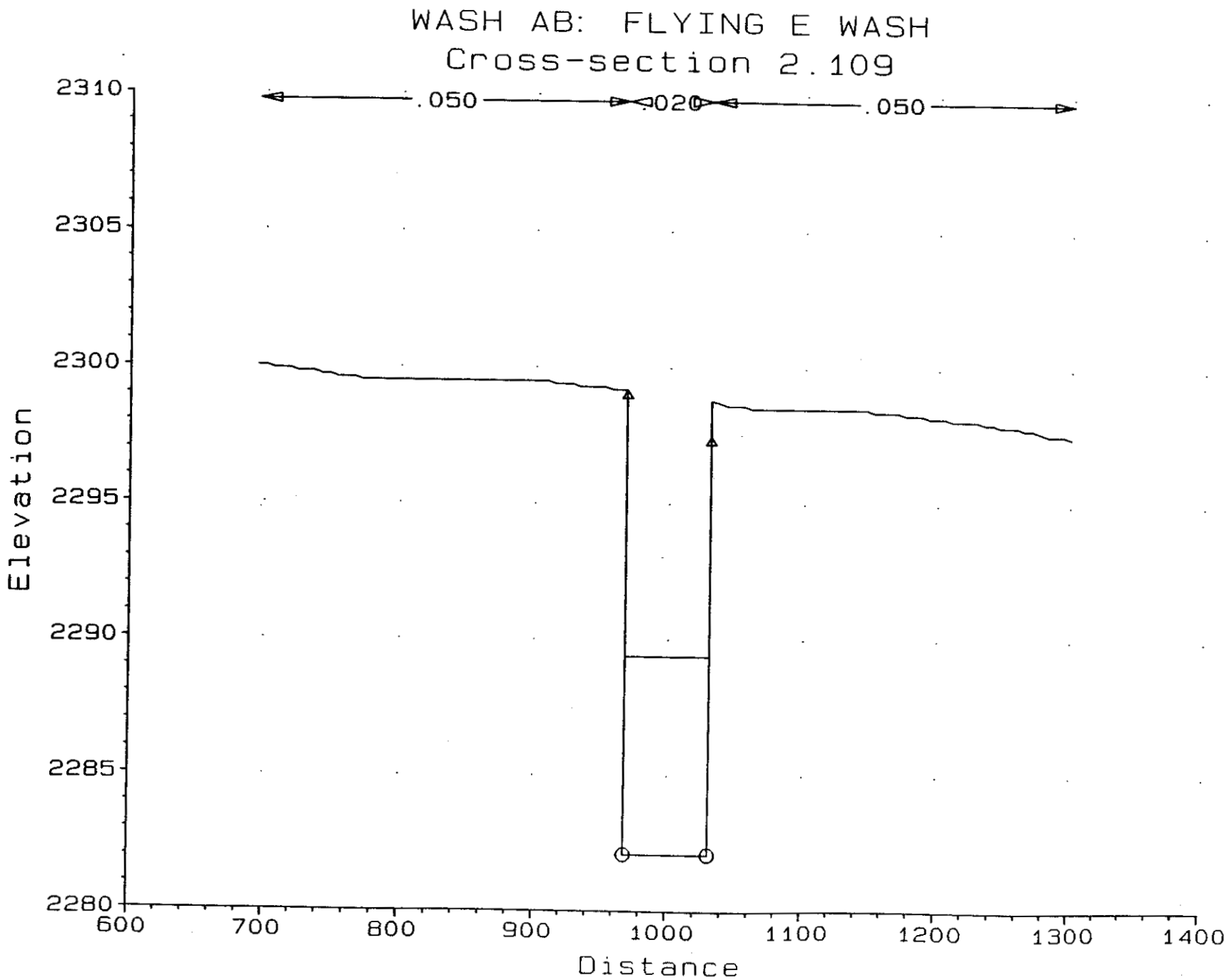
WASH AB: FLYING E WASH
Cross-section 1.918

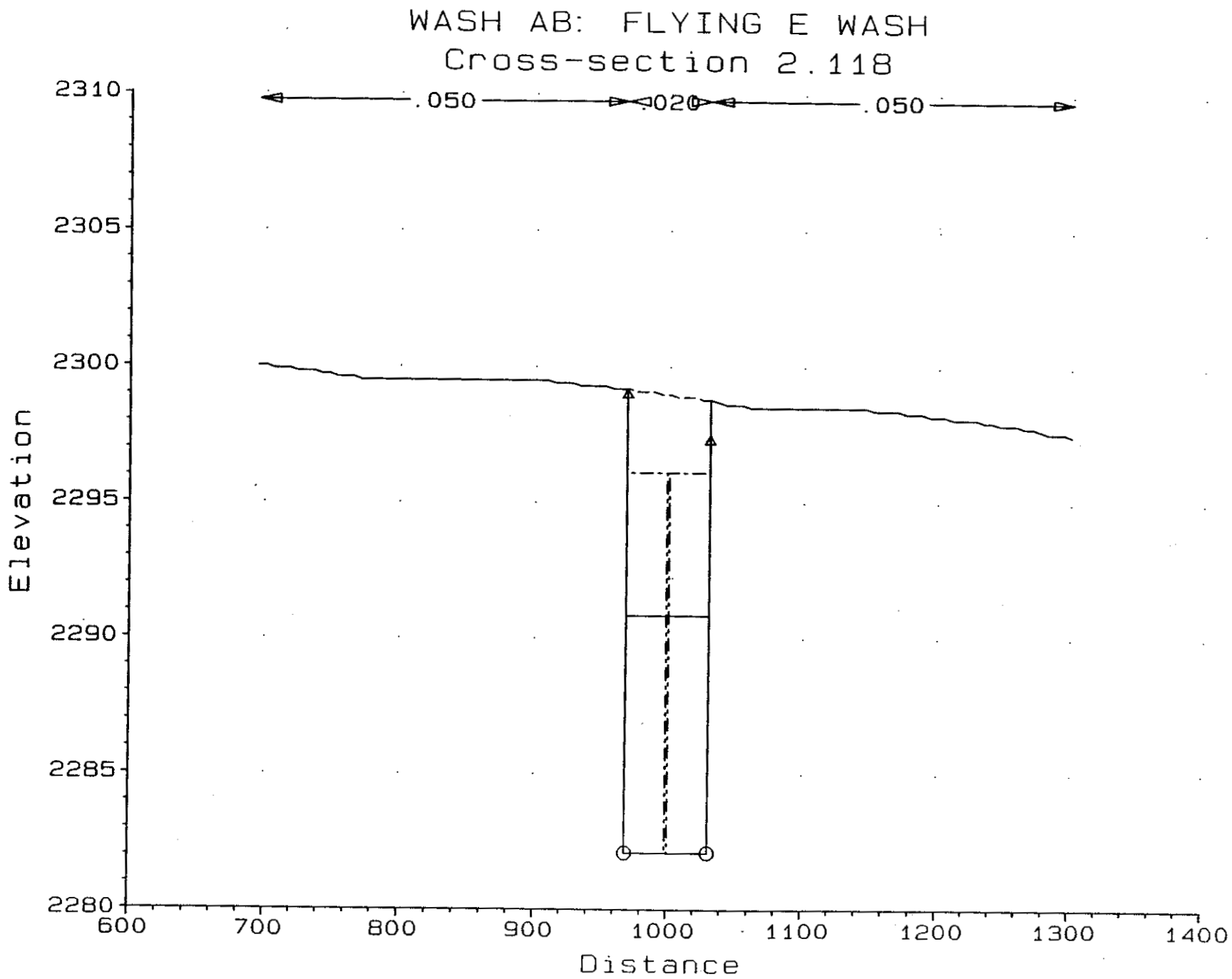


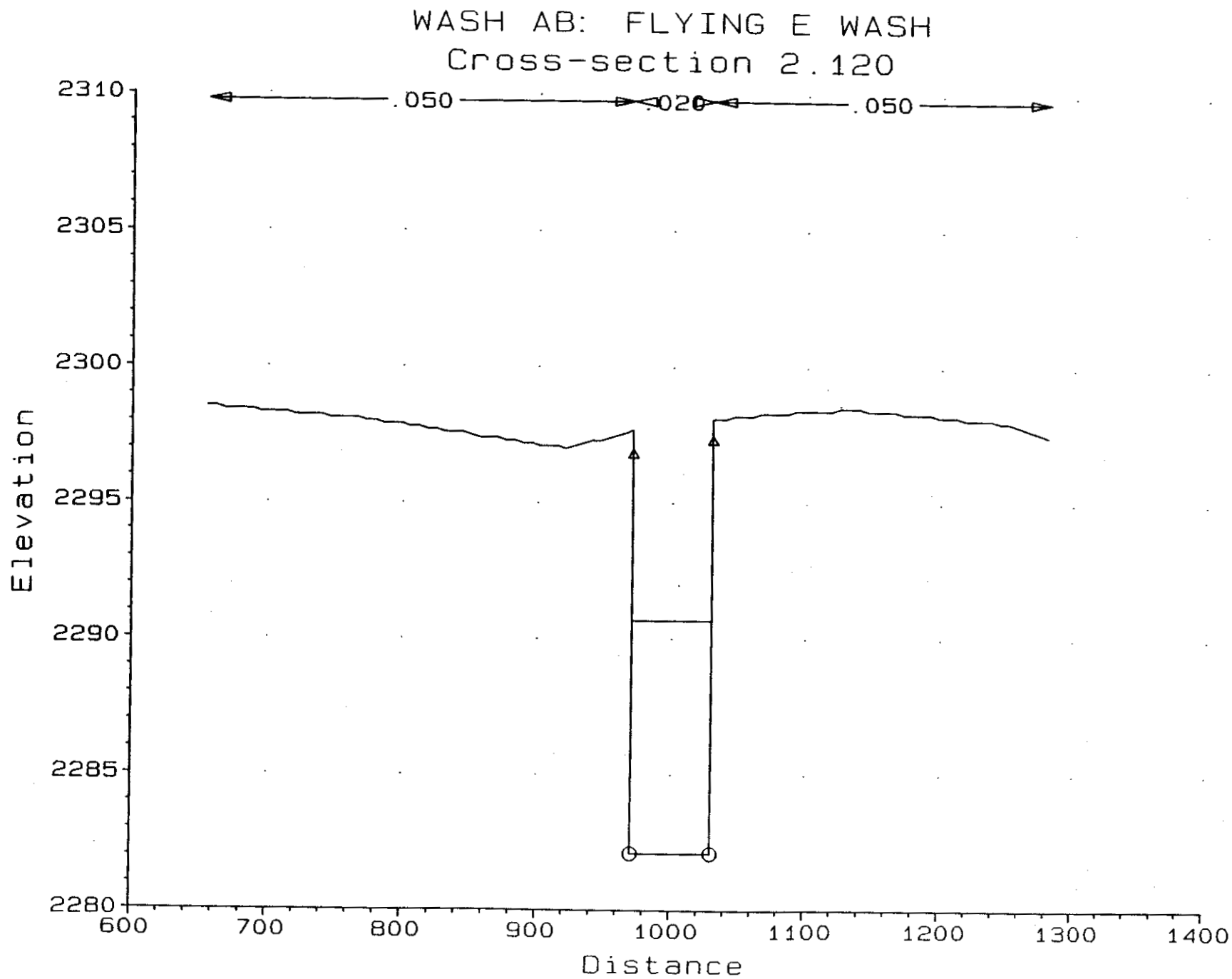

WASH AB: FLYING E WASH
Cross-section 2.011
.050
.030
.050
2305
2300
2295
2290
2285
2280
2275
Elevation
0
200
400
600
800
1000
1200
1400
1600
Distance

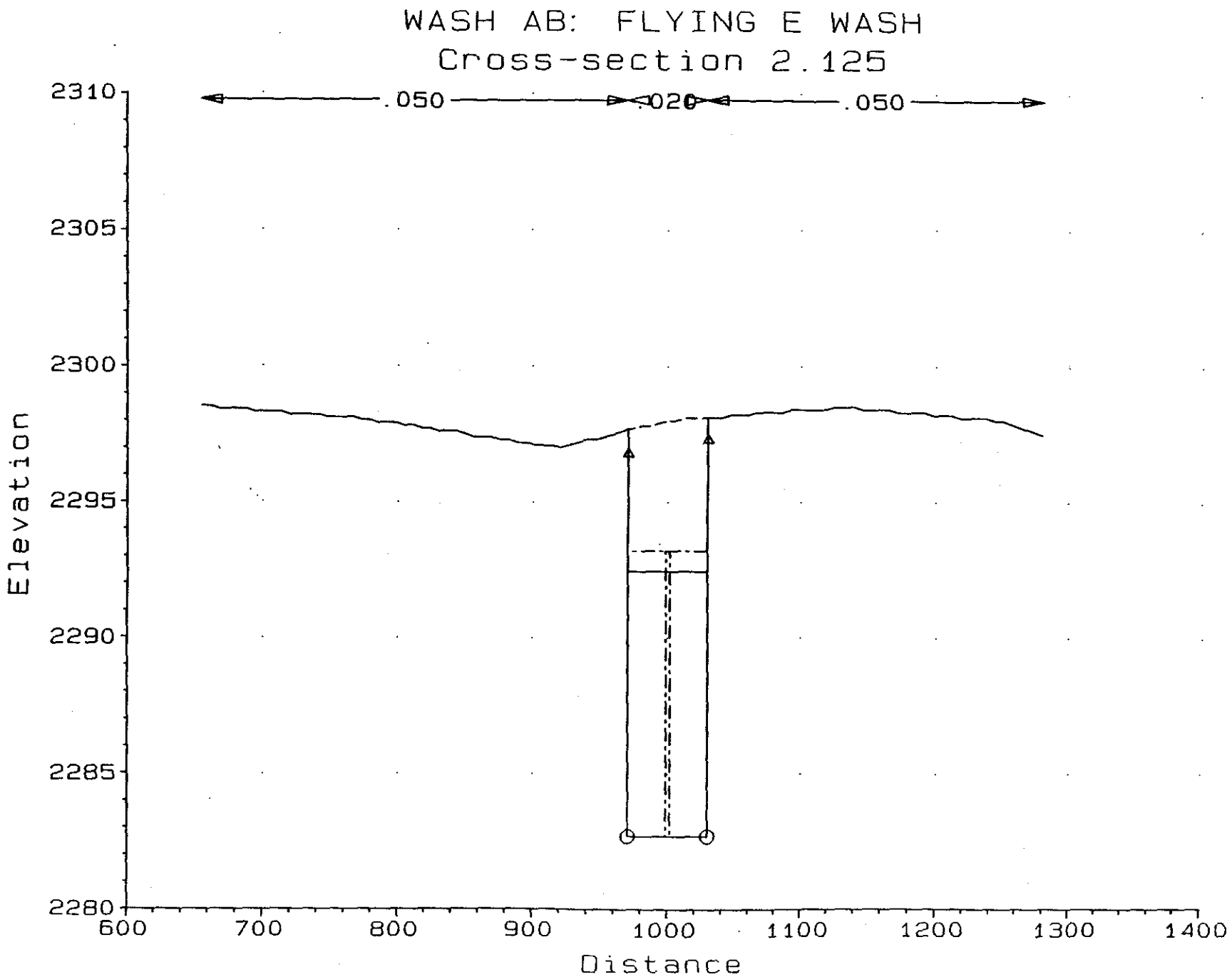

WASH AB: FLYING E WASH
Cross-section 2.056
.050
.030
.050
Elevation
2305
2300
2295
2290
2285
2280
2275
200
400
600
800
1000
1200
1400
1600
1800
Distance

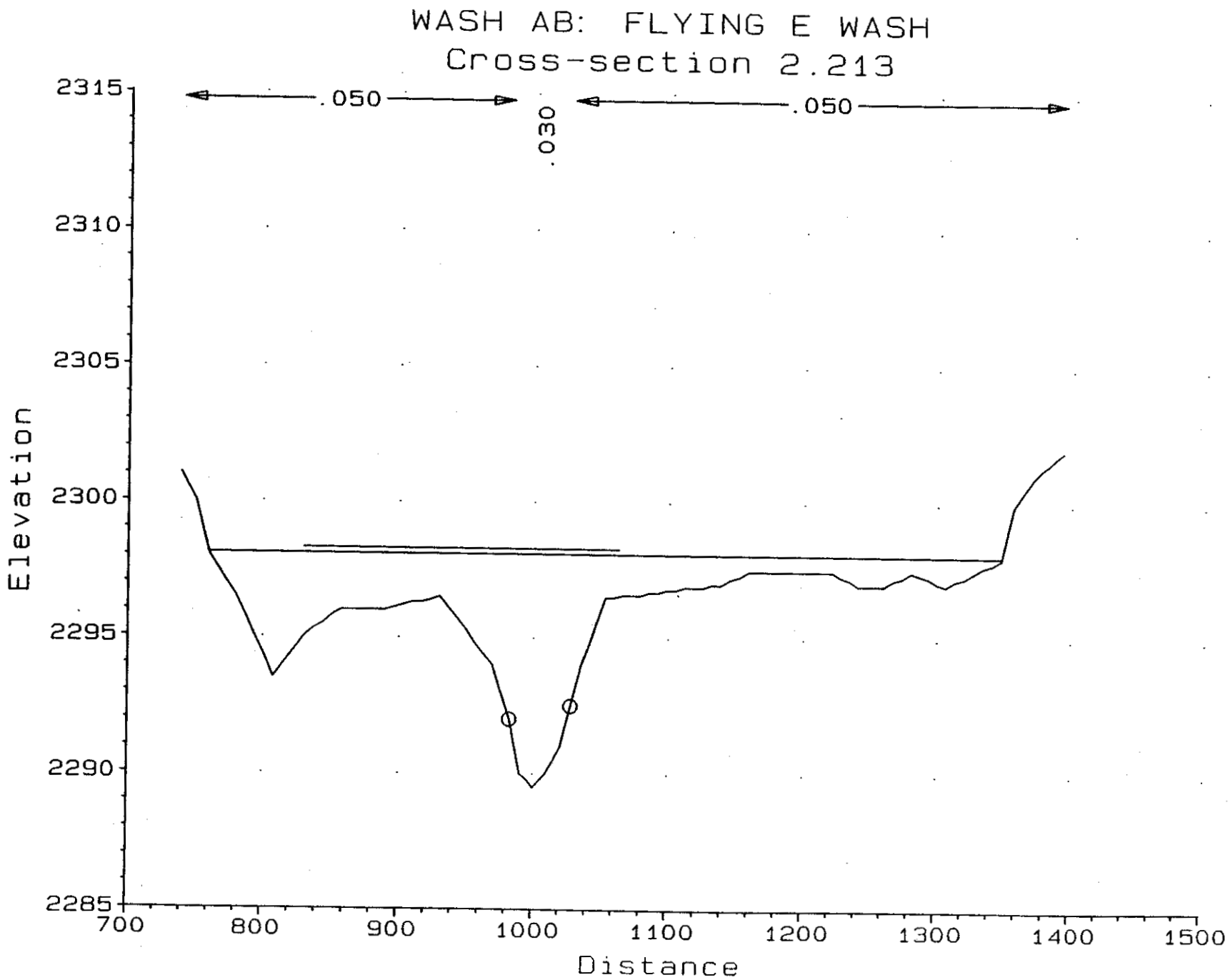

WASH AB: FLYING E WASH
Cross-section 2.107
.050
.030
.050
2310
2305
2300
2295
2290
2285
2280
Elevation
600
700
800
900
1000
1100
1200
1300
1400
Distance

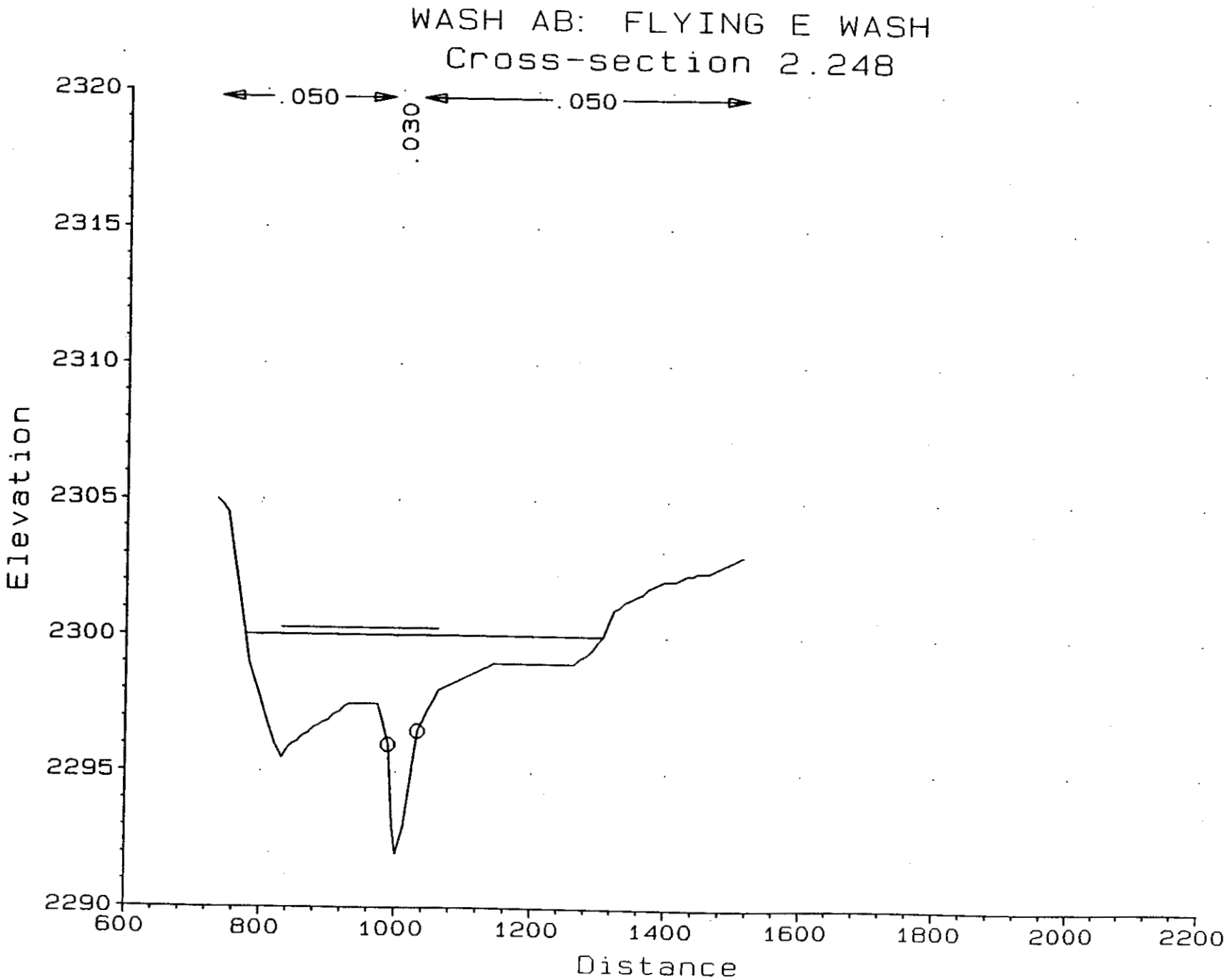

WASH AB: FLYING E WASH
Cross-section 2.109
.050
.020
.050
2310
2305
2300
2295
2290
2285
2280
Elevation
600
700
800
900
1000
1100
1200
1300
1400
Distance

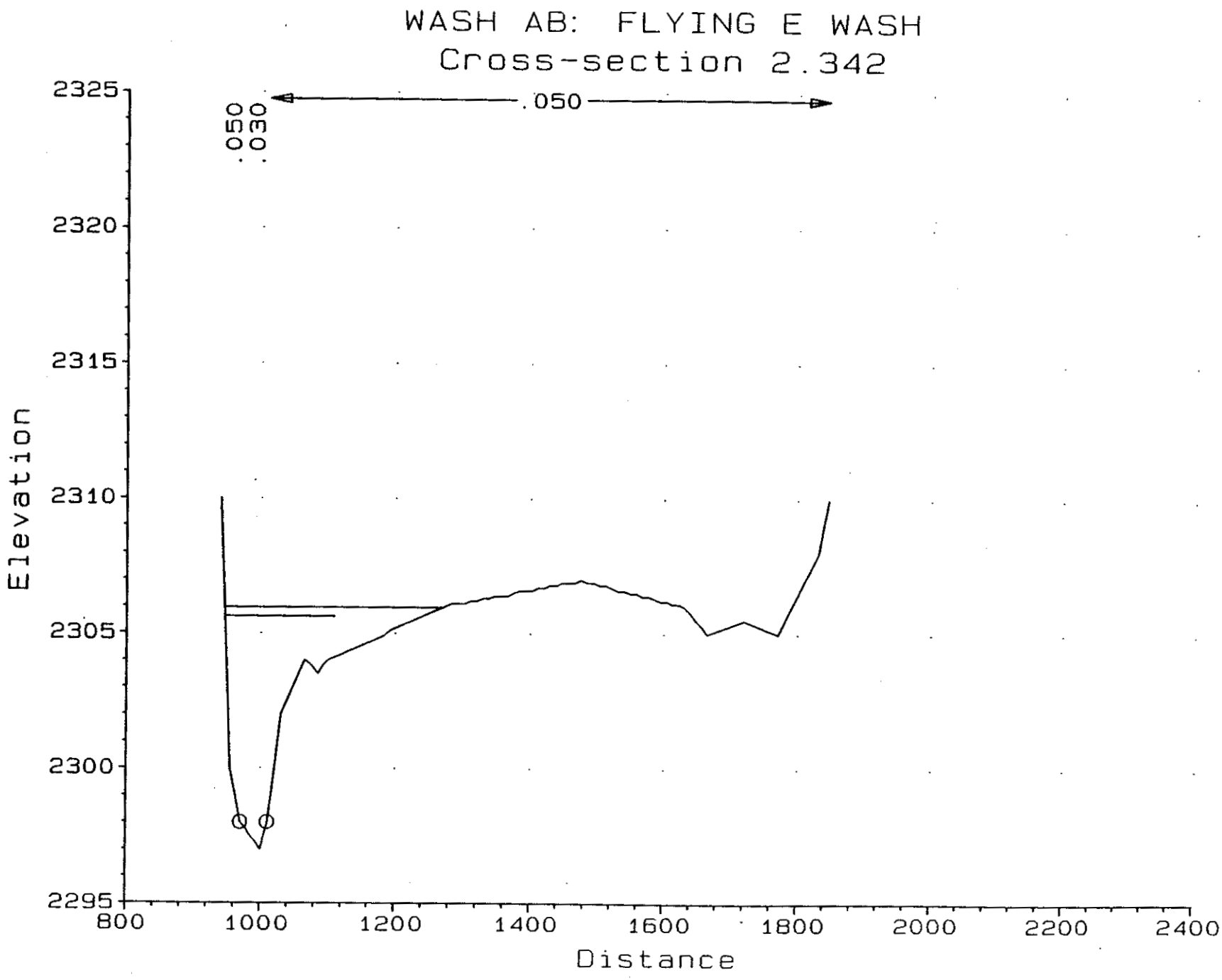

WASH AB: FLYING E WASH
Cross-section 2.118
.050
.020
.050
2310
2305
2300
2295
2290
2285
2280
Elevation
600
700
800
900
1000
1100
1200
1300
1400
Distance

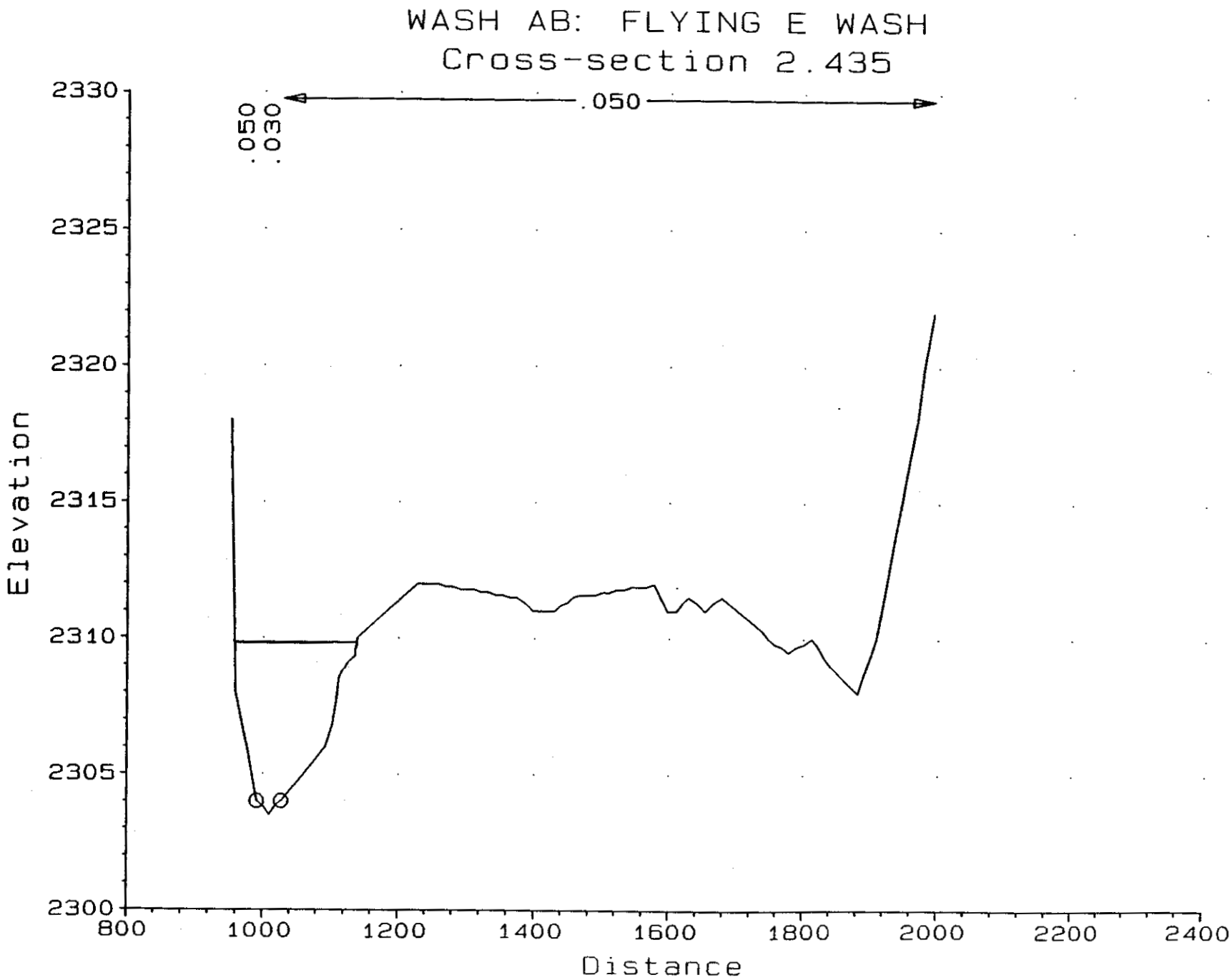

WASH AB: FLYING E WASH
Cross-section 2.120
.050
.020
.050
2310
2305
2300
2295
2290
2285
2280
Elevation
600
700
800
900
1000
1100
1200
1300
1400
Distance


WASH AB: FLYING E WASH
Cross-section 2.125
.050
.020
.050
2310
2305
2300
2295
2290
2285
2280
Elevation
600
700
800
900
1000
1100
1200
1300
1400
Distance


WASH AB: FLYING E WASH
Cross-section 2.213
.050
.030
.050
2315
2310
2305
2300
2295
2290
2285
Elevation
700
800
900
1000
1100
1200
1300
1400
1500
Distance


WASH AB: FLYING E WASH
Cross-section 2.248
.050
.030
.050
Elevation
2320
2315
2310
2305
2300
2295
2290
600
800
1000
1200
1400
1600
1800
2000
2200
Distance


WASH AB: FLYING E WASH
Cross-section 2.342
.050
.050
.030
Elevation
2325
2320
2315
2310
2305
2300
2295
800
1000
1200
1400
1600
1800
2000
2200
2400
Distance


WASH AB: FLYING E WASH
Cross-section 2.435
.050
.050
.030
Elevation
2330
2325
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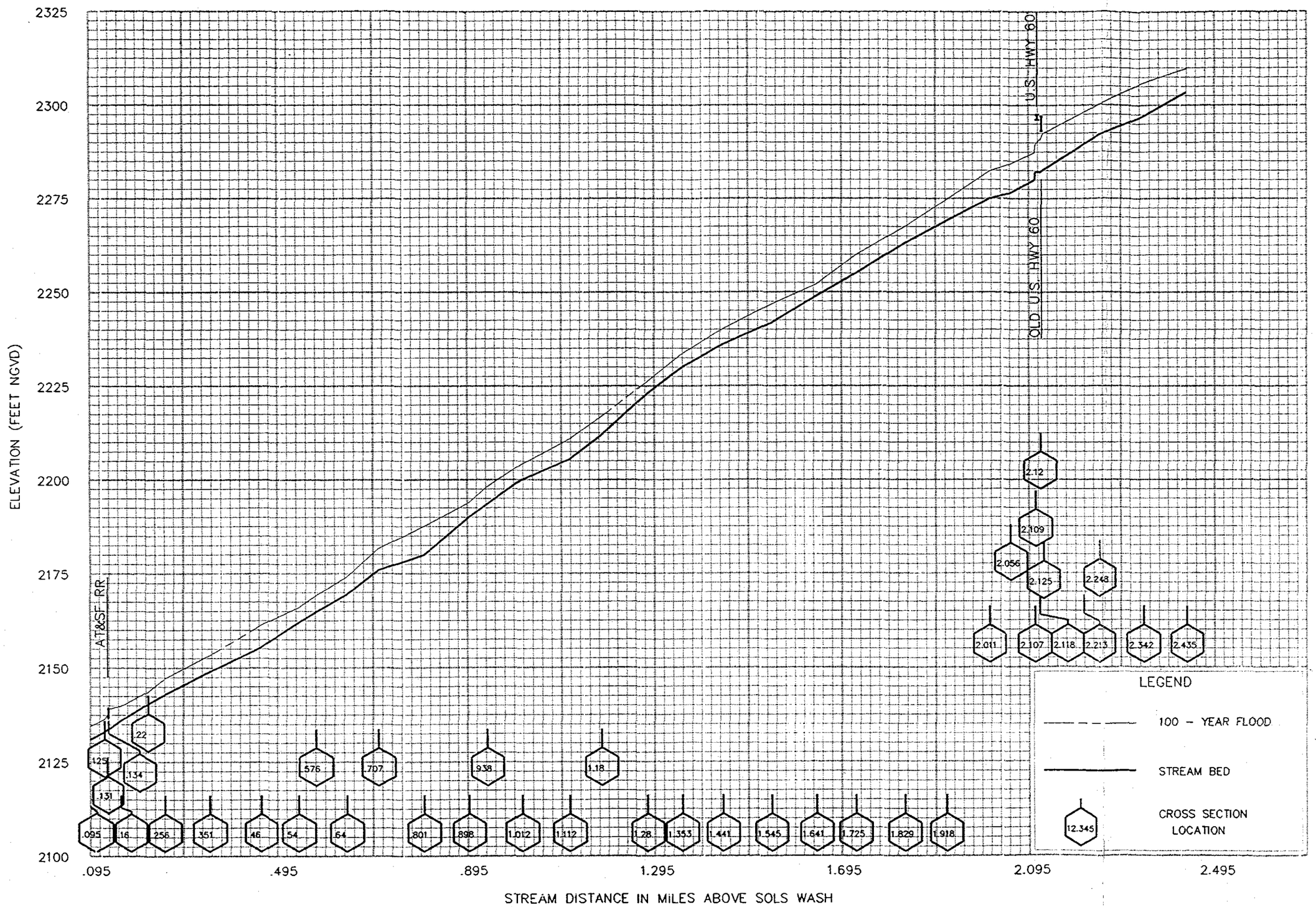
2315
2310
2305
2300
800
1000
1200
1400
1600
1800
2000
2200
2400
Distance




FLOOD PROFILES

FLYING E WASH (AB) (LOWER)

FEDERAL EMERGENCY MANAGEMENT AGENCY

MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

02/17/94 11:15:27 ACD-12_

PC FILE:LFEW.DWG

Upper
Flying E
Wash

```
*********************************************
*  HEC-2 WATER SURFACE PROFILES             *
*                                           *
*  Version   4.6.2;  May 1991               *
*                                           *
*  RUN DATE    05AUG92    TIME   11:42:35   *
*********************************************
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***************************************
*  U.S. ARMY CORPS OF ENGINEERS       *
*  HYDROLOGIC ENGINEERING CENTER      *
*  609 SECOND STREET, SUITE D         *
*  DAVIS, CALIFORNIA 95616-4687       *
*          (916) 756-1104             *
***************************************
```

```
X     X  XXXXXXX   XXXXX              XXXXX
X     X  X        X     X            X     X
X     X  X        X                        X
XXXXXXX  XXXX     X          XXXXX    XXXXX
X     X  X        X                  X
X     X  X        X     X            X
X     X  XXXXXXX   XXXXX             XXXXXXX
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THIS RUN EXECUTED 05AUG92 11:42:35

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************************************
 HEC-2 WATER SURFACE PROFILES

 Version   4.6.2;  May 1991
************************************


T1   WICKENBURG ADMS: CONTRACT FCD 89-79
T2   BLACK & VEATCH PN 17676; COE & VAN LOO JN 1197-02
T3       AB: UPPER FLYING E WASH          (FILE UFEW.DAT)

J1  ICHECK    INQ      NINV     IDIR     STRT     METRIC   HVINS    Q        WSEL     FQ

      0        2        0        0     .008304     0        0        0     2309.8     0

J2  NPROF    IPLOT    PRFVS    XSECV    XSECH    FN       ALLDC    IBW      CHNIM    ITRACE

     1        0       -1        0        0        0       -1        0        0        15


J3  VARIABLE CODES FOR SUMMARY PRINTOUT

     150      200

NC    0.050    0.050    0.030      0.1      0.3
QT        2   6943.0   6943.0

ET              7.1      9.1                                   952.     1228.0   957.69     1102
          CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH
X1    2.435       93    991.0   1027.0      500      455      490
X5        2   2309.8   2309.8
GR   2318.0    952.0   2308.0    959.0   2307.0    967.5   2306.0    976.0   2304.0    991.0
GR   2303.8   1000.0   2303.5   1009.0   2303.8   1018.0   2304.0   1027.0   2304.3   1037.0
GR   2304.6   1047.0   2304.9   1057.0   2305.2   1067.0   2305.5   1077.0   2306.0   1092.0
GR   2306.8   1102.0   2307.7   1108.0   2308.5   1112.0   2308.6   1112.7   2308.8   1117.4
GR   2308.9   1120.1   2309.1   1124.8   2309.3   1135.5   2309.4   1136.2   2309.6   1136.9
GR   2309.7   1137.6   2309.9   1138.3   2310.0   1139.0   2311.0   1183.5   2312.0   1228.0
GR   2312.0   1258.3   2311.9   1268.7   2311.9   1279.0   2311.8   1289.3   2311.8   1310.0
GR   2311.7   1320.3   2311.7   1330.7   2311.6   1341.0   2311.6   1351.3   2311.5   1361.7
GR   2311.5   1372.0   2311.3   1384.5   2311.0   1397.0   2311.0   1429.0   2311.2   1438.0
GR   2311.3   1447.0   2311.5   1456.0   2311.6   1466.9   2311.6   1488.7   2311.7   1499.6
GR   2311.7   1510.6   2311.8   1521.4   2311.8   1532.4   2311.9   1543.3   2311.9   1565.1
GR   2312.0   1576.0   2311.5   1586.0   2311.0   1596.0   2311.0   1609.0   2311.3   1618.5
GR   2311.5   1628.0   2311.3   1640.0   2311.0   1652.0   2311.3   1664.5   2311.5   1677.0
GR   2311.3   1687.0   2311.1   1697.0   2310.9   1707.0   2310.7   1717.0   2310.5   1727.0
GR   2310.3   1737.0   2310.0   1747.0   2309.8   1757.0   2309.7   1767.0   2309.5   1777.0
GR   2309.7   1788.7   2309.8   1800.3   2310.0   1812.0   2309.7   1821.0   2309.3   1830.0
GR   2309.0   1839.0   2308.0   1880.0   2308.7   1889.0   2309.3   1898.0   2310.0   1907.0
GR   2311.3   1917.0   2312.7   1927.0   2314.0   1937.0   2315.3   1947.0   2316.7   1957.0
GR   2318.0   1967.0   2320.0   1977.0   2322.0   1991.0
```

```
[illegible]    2     6943     6943
NH     5     .05    821.5     .03    880.9     .05      980     .03     1012     .05
NH  1142
          AT HIGH FLOW, BOTH YUCCA FLAT WASH AND FLYING E WASH CHANNELS
          ARE USED.  SECTION REPEATED FOR BOTH MODELS. NH CARD DEFINES CHANNELS
X1  2.539      63    821.5    880.9     570     490     550
X3                           465.3    2317.3   1100.   2317.0

GR   2322     320     2321    340.5    2320     361   2319.3   381.3   2318.7   401.7
GR   2318     422   2317.7    443.7   2317.3   465.3    2317     487   2315.5     510
GR   2315   527.7   2314.5    545.3    2314     563    2313     575     2316     596
GR 2316.5     619     2317      642  2316.5   666.5    2316     691   2316.5     710
GR   2316     730   2315.5      747    2315     764   2315.5     790   2315.2   795.2
GR 2314.9   800.4   2314.6    805.6   2314.3   810.8    2314     816   2313.5   821.5
GR   2313     827   2312.5      832    2312     837   2311.7   841.3   2311.3   845.7
GR   2311     850   2311.7      855   2312.3     860    2313     865   2313.1   870.3
GR 2313.1   875.6   2313.2    880.9   2313.3   886.1   2313.4   891.4   2313.4   896.7
GR 2313.5     902   2313.8    906.5    2314     911   2314.3   915.5   2314.5     920
GR 2314.3     941     2314      962    2312     977   2309.5     980     2309    1000
GR 2309.5    1012     2310     1027   2312.5    1035    2316    1063   2316.5  1081.5
GR   2317    1100     2317     1121    2317    1142

QT     2    2152     2152
NC   .05     .05     0.03
[illegible]           9.1                                                 893.34  1030.49
          UPPER FLYING E WASH FULLY DEFINED CHANNEL
X1  2.630      94    976.0   1016.0     480     460     480
GR 2327.5   820.0   2327.2    824.2   2326.9   828.4   2326.6   832.6   2326.3   836.8
GR 2326.0   841.0   2325.7    845.2   2325.4   849.4   2325.1   853.6   2324.8   857.8
GR 2324.5   862.0   2323.2    866.3   2321.8   870.7   2320.5   875.0   2320.2   879.1
GR 2319.9   883.3   2319.6    887.4   2319.3   891.5   2318.9   895.6   2318.6   899.8
GR 2318.3   903.9   2318.0    908.0   2315.5   911.0   2315.5   968.0   2315.4   972.0
GR 2315.4   976.0   2315.3    980.0   2315.3   984.0   2315.2   988.0   2315.1   992.0
GR 2315.1   996.0   2315.0   1000.0   2315.1  1004.0   2315.2  1008.0   2315.3  1012.0
GR 2315.4  1016.0   2315.5   1020.0   2316.8  1023.7   2318.0  1027.3   2319.3  1031.0
GR 2320.5  1034.7   2321.8   1038.3   2323.0  1042.0   2323.1  1045.8   2323.1  1049.5
GR 2323.2  1053.3   2323.3   1057.0   2323.3  1060.8   2323.4  1064.5   2323.4  1068.3
GR 2323.5  1072.0   2323.6   1075.9   2323.6  1079.8   2323.7  1083.7   2323.7  1087.6
GR 2323.8  1091.4   2323.8   1095.3   2323.9  1099.2   2323.9  1103.1   2324.0  1107.0
GR 2324.1  1111.2   2324.2   1115.3   2324.3  1119.5   2324.3  1123.7   2324.4  1127.8
GR 2324.5  1132.0   2324.4   1135.8   2324.4  1143.4   2324.3  1147.2   2324.3  1151.0
GR 2324.2  1154.8   2324.1   1158.6   2324.1  1166.2   2324.0  1170.0   2323.8  1174.2
GR 2323.6  1178.4   2323.4   1182.6   2323.2  1186.8   2323.0  1191.0   2323.2  1195.0
GR 2323.3  1199.0   2323.5   1203.0   2323.7  1207.0   2323.8  1211.0   2324.0  1215.0
GR 2324.3  1218.9   2324.7   1222.8   2325.0  1226.7   2325.3  1230.6   2325.7  1234.4
GR 2326.0  1238.3   2326.3   1242.2   2326.7  1246.1   2327.0  1250.0

ET                   9.1                                                 907.30  1151.54
X1  2.725      53    981.0   1020.0     515     485     500
GR 2332.0   860.0   2331.0    865.5   2330.0   871.0   2329.1   876.3   2328.3   881.5
[illegible]2327.4   886.8   2326.5    892.0   2326.3   897.0   2326.0   902.0   2325.8   906.8
[illegible]2325.5   911.5   2325.3    916.3   2325.0   921.0   2325.3   925.8   2325.5   930.5
GR 2325.8   935.3   2326.0    940.0   2327.0   944.5   2328.0   949.0   2328.0   955.0
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| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2326.0 | 962.0 | 2325.5 | 966.0 | 2325.0 | 970.0 | 2324.3 | 975.5 | 2323.5 | 981.0 |
| | 2323.4 | 985.8 | 2323.3 | 990.5 | 2323.1 | 995.3 | 2323.0 | 1000.0 | 2323.1 | 1005.0 |
| GR | 2323.3 | 1010.0 | 2323.4 | 1015.0 | 2323.5 | 1020.0 | 2327.0 | 1025.0 | 2330.5 | 1030.0 |
| GR | 2331.3 | 1035.5 | 2332.0 | 1041.0 | 2332.0 | 1046.7 | 2332.0 | 1052.3 | 2332.0 | 1058.0 |
| GR | 2332.3 | 1064.0 | 2332.5 | 1070.0 | 2330 | 1079 | 2328 | 1082 | 2326 | 1089 |
| GR | 2324 | 1106 | 2322 | 1121 | 2322 | 1138 | 2324 | 1148 | 2326 | 1152 |
| GR | 2328 | 1160 | 2330 | 1169 | 2332 | 1173 | | | | |
| ET | | 7.1 | 9.1 | | | | 895. | 1425. | 942.05 | 1375.90 |
| X1 | 2.812 | 75 | 976.7 | 1013.3 | 440 | 480 | 460 | | | |
| GR | 2334 | 785 | 2333.3 | 791.7 | 2332.7 | 798.3 | 2332 | 805 | 2331.5 | 812.5 |
| GR | 2331 | 820 | 2331.3 | 826.7 | 2331.7 | 833.3 | 2332 | 840 | 2332.7 | 846.1 |
| GR | 2333.3 | 852.2 | 2334 | 858.3 | 2334.7 | 864.4 | 2335.3 | 870.6 | 2336 | 876.7 |
| GR | 2336.7 | 882.8 | 2337.3 | 888.9 | 2338 | 895 | 2337 | 901.3 | 2336 | 907.5 |
| GR | 2335 | 913.8 | 2334 | 920 | 2333.2 | 926 | 2332.4 | 932 | 2331.6 | 938 |
| GR | 2330.8 | 944 | 2330 | 950 | 2329 | 957.5 | 2328 | 965 | 2327.8 | 976.7 |
| GR | 2327.7 | 988.3 | 2327.5 | 1000 | 2327.8 | 1013.3 | 2328 | 1020 | 2328.4 | 1026 |
| GR | 2328.8 | 1032 | 2329.2 | 1038 | 2329.6 | 1044 | 2330 | 1050 | 2330.1 | 1062.3 |
| GR | 2330.3 | 1074.6 | 2330.5 | 1086.9 | 2330.6 | 1099.2 | 2330.8 | 1111.5 | 2330.9 | 1123.8 |
| GR | 2330.9 | 1136.3 | 2330.8 | 1148.8 | 2330.7 | 1161.3 | 2330.6 | 1173.8 | 2330.4 | 1186.3 |
| GR | 2330.3 | 1198.8 | 2330.2 | 1211.3 | 2330.1 | 1223.8 | 2330.1 | 1236.7 | 2330.3 | 1250 |
| GR | 2330.4 | 1263.3 | 2330.4 | 1276.4 | 2330.3 | 1289.3 | 2330.1 | 1302.1 | 2330 | 1315 |
| GR | 2329.8 | 1327.5 | 2329.5 | 1340 | 2329.8 | 1353.3 | 2330 | 1360 | 2330.4 | 1366 |
| GR | 2330.8 | 1372 | 2331.2 | 1378 | 2331.6 | 1384 | 2332 | 1390 | 2332.8 | 1395.8 |
| GR | 2333.7 | 1401.7 | 2334.5 | 1407.5 | 2335.3 | 1413.3 | 2336.2 | 1419.2 | 2337 | 1425 |
| | | | 9.1 | | | | | | 695.41 | 1047.64 |
| X1 | 2.922 | 58 | 989.0 | 1020.0 | 585 | 525 | 580 | | | |
| GR | 2345.5 | 612.0 | 2344.5 | 636.0 | 2343.5 | 660.0 | 2340.0 | 670.0 | 2338.5 | 680.0 |
| GR | 2338.0 | 690.0 | 2336.5 | 715.0 | 2336.5 | 737.0 | 2336.5 | 759.0 | 2336.3 | 774.5 |
| GR | 2336.0 | 790.0 | 2335.5 | 814.0 | 2336.0 | 838.0 | 2336.7 | 855.3 | 2337.3 | 872.7 |
| GR | 2338.0 | 890.0 | 2338.3 | 905.5 | 2338.5 | 921.0 | 2338.5 | 940.0 | 2338.4 | 943.5 |
| GR | 2338.3 | 947.0 | 2338.3 | 950.5 | 2338.2 | 954.0 | 2338.1 | 957.5 | 2338.0 | 961.0 |
| GR | 2337.6 | 964.8 | 2337.2 | 968.6 | 2336.8 | 972.4 | 2336.4 | 976.2 | 2336.0 | 980.0 |
| GR | 2335.5 | 984.5 | 2335.0 | 989.0 | 2334.7 | 992.7 | 2334.3 | 996.3 | 2334.0 | 1000.0 |
| GR | 2334.2 | 1004.0 | 2334.4 | 1008.0 | 2334.6 | 1012.0 | 2334.8 | 1016.0 | 2335.0 | 1020.0 |
| GR | 2335.1 | 1023.5 | 2335.2 | 1027.0 | 2335.3 | 1030.5 | 2335.3 | 1034.0 | 2335.4 | 1037.5 |
| GR | 2335.5 | 1041.0 | 2336.6 | 1044.5 | 2337.8 | 1048.0 | 2338.9 | 1051.5 | 2340.0 | 1055.0 |
| GR | 2340.1 | 1059.0 | 2340.3 | 1063.0 | 2340.4 | 1067.0 | 2340.5 | 1071.0 | 2340.8 | 1088.0 |
| GR | 2341.0 | 1105.0 | 2343.5 | 1121.5 | 2346.0 | 1138.0 | | | | |
| ET | | | 9.1 | | | | | | 936.55 | 1416.51 |
| X1 | 3.005 | 60 | 983.3 | 1021.0 | 425 | 490 | 440 | | | |
| GR | 2350.0 | 900.0 | 2346.0 | 914.0 | 2344.0 | 938.0 | 2343.0 | 954.0 | 2342.8 | 957.2 |
| GR | 2342.6 | 960.4 | 2342.4 | 963.6 | 2342.2 | 966.8 | 2342.0 | 970.0 | 2341.7 | 973.3 |
| GR | 2341.3 | 976.7 | 2341.0 | 980.0 | 2340.9 | 983.3 | 2340.8 | 986.7 | 2340.8 | 990.0 |
| GR | 2340.7 | 993.3 | 2340.6 | 996.7 | 2340.5 | 1000.0 | 2340.6 | 1003.5 | 2340.6 | 1007.0 |
| GR | 2340.7 | 1010.5 | 2340.8 | 1014.0 | 2340.8 | 1017.5 | 2340.9 | 1021.0 | 2340.9 | 1024.5 |
| GR | 2341.0 | 1028.0 | 2341.3 | 1031.7 | 2341.7 | 1035.3 | 2342.0 | 1039.0 | 2342.7 | 1042.0 |
| GR | 2343.3 | 1045.0 | 2344.0 | 1048.0 | 2344.1 | 1051.5 | 2344.3 | 1055.0 | 2344.4 | 1058.5 |
| GR | 2344.5 | 1062.0 | 2344.5 | 1079.0 | 2344.0 | 1091.0 | 2343.0 | 1110.0 | 2343.5 | 1130.0 |
| | 2343.0 | 1160.0 | 2343.0 | 1190.0 | 2344.0 | 1215.0 | 2346.0 | 1234.0 | 2346.5 | 1246.0 |
| | 2346.0 | 1260.0 | 2344.0 | 1270.0 | 2343.0 | 1295.0 | 2343.0 | 1313.0 | 2342.0 | 1321.0 |
| GR | 2343.0 | 1330.0 | 2343.3 | 1348.5 | 2343.5 | 1367.0 | 2343.0 | 1395.0 | 2344.0 | 1415.0 |

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    2346.0    1440.0    2349.0    1470.0    2350.0    1491.0    2351.3    1508.0    2352.5    1525.0

ET                        9.1                                                         980.77    1208.34
X1   3.047      48     987.0    1008.5       205       265       220
GR  2364.0     890.0   2363.0     910.0    2362.0     930.0    2360.0     945.0    2355.0     960.5
GR  2350.0     976.0   2348.8     978.2    2347.6     980.4    2346.4     982.6    2345.2     984.8
GR  2344.0     987.0   2343.5     990.0    2343.4     992.0    2343.3     994.0    2343.2     996.0
GR  2343.1     998.0   2343.0    1000.0    2343.2    1002.0    2343.3    1004.0    2343.5    1006.0
GR  2344.0    1008.5   2344.5    1011.0    2344.6    1013.1    2344.6    1015.2    2344.7    1017.3
GR  2344.7    1019.4   2344.8    1021.6    2344.8    1023.7    2344.9    1025.8    2344.9    1027.9
GR  2345.0    1030.0   2345.0    1044.0    2344.5    1058.0    2345.0    1079.0    2346.0    1099.0
GR  2346.5    1120.0   2346.5    1145.0    2347.0    1170.0    2347.0    1185.0    2347.0    1200.0
GR  2348.0    1221.0   2349.0    1243.0    2350.0    1265.0    2350.7    1285.0    2351.3    1305.0
GR  2352.0    1325.0   2353.0    1345.0    2354.0    1365.0

ET                7.1       9.1                                   950      1100     973.52    1046.28
          FLYING E TANK - NO DESIGN OR CONSTRUCTION INFORMATION AVAILABLE FOR
          LOW DAM FORMING TANK:  NOT DEPENDABLE FOR FLOOD RISK PLANNING.
          SECTION 3.200 IS CONTROL SECTION FOR PONDING IN TANK.
          MAP PROVIDES TWO WATER SURFACE ELEVATIONS.  TANK WSEL IS THE
          EG ELEVATION AT THE CONTROL SECTION (2359.00 FT).  CHANNEL WSELs
          FROM NORMAL ANALYSIS WITH ENCROACHMENT AT 950 (THIS SECTION) TO
          OMIT TANK FROM FLOW AREA.
          ENTIRE INUNDATED AREA AND DAM INCLUDED IN AE ZONE.
X1   3.113      64    1000.0    1020.0       370       270       350
GR  2358.0     760.0   2356.0     771.0    2354.0     782.0    2352.0     790.0    2351.0     797.5
GR  2350.0     805.0   2349.8     813.0    2349.5     821.0    2349.5     830.8    2349.5     840.7
GR  2349.5     850.5   2349.5     860.3    2349.5     870.2    2349.5     880.0    2349.8     887.5
GR  2350.0     895.0   2351.0     903.0    2352.0     911.0    2358.0     921.0    2358.1     924.6
GR  2358.2     928.2   2358.3     931.8    2358.4     935.4    2358.5     939.0    2358.5     942.7
GR  2358.5     946.3   2358.5     950.0    2358.3     953.3    2358.2     956.7    2358.0     960.0
GR  2356.7     963.3   2355.3     966.7    2354.0     970.0    2352.7     973.3    2351.3     976.7
GR  2350.0     980.0   2349.3     983.0    2348.7     986.0    2348.0     989.0    2347.8     992.7
GR  2347.7     996.3   2347.5    1000.0    2347.5    1003.3    2347.5    1006.7    2347.5    1010.0
GR  2347.5    1013.3   2347.5    1016.7    2347.5    1020.0    2348.8    1022.5    2350.0    1025.0
GR  2350.4    1028.4   2350.8    1031.8    2351.2    1035.2    2351.6    1038.6    2352.0    1042.0
GR  2352.5    1045.5   2353.0    1049.0    2353.5    1052.5    2354.0    1056.0    2354.5    1065.5
GR  2355.0    1075.0   2355.3    1083.3    2355.7    1091.7    2356.0    1100.0

ET                        9.1                                                         924.94    1164.89
          FLYING E TANK OVERFLOW
X1   3.200      28    1000.0    1030.0       390       590       460
GR     2359     660   2358.8     685    2358.5     710    2358.5     728.3    2358.5     746.7
GR  2358.5     765   2358.5     790    2358.5     815    2358.5     839.5    2358.5     864
GR  2358.5     881   2358.5     898    2358.5     915    2357.8     935      2357.2     955
GR  2356.5     975     2356     980      2355    1000      2355     1030     2355.5    1040
GR     2356    1060   2356.5    1085      2357    1100    2357.5     1120     2357.8    1141
GR     2358    1162     2359    1181      2360    1200
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                                9.1                                                   815.46    1089.86
X1    3.261        44     990.0     1022.     330     250     320
GR    2370.0     692.0    2369.0    713.0    2368.0   734.0   2367.0   754.5    2366.0    775.0
GR    2363.0     796.5    2360.0    818.0    2358.0   840.0   2357.0   851.0    2357.0    860.0
GR    2358.0     875.0    2357.0    890.0    2357.0   903.0   2358.0   918.0    2358.5    932.0
GR    2359.0     958.0    2358.5    980.0    2358.3   983.3   2358.2   986.7    2358.0    990.0
GR    2357.0     994.0    2356.8    997.0    2356.5  1000.0   2356.6  1003.6    2356.7   1007.2
GR    2356.8    1010.8    2356.9   1014.4    2357.0  1018.0   2358.0  1022.0    2358.3   1026.0
GR    2358.5    1030.0    2358.6   1033.3    2358.7  1036.7   2358.8  1040.0    2358.8   1043.3
GR    2358.9    1046.7    2359.0   1050.0    2359.5  1071.0   2360.0  1088.0    2364.0   1109.0
GR    2366.0    1125.0    2368.0   1141.0    2368.5  1160.5   2369.0  1180.0

ET                              9.1                                                   720.38    1022.57
X1    3.308        61     980.0     1007.3    250     250     250
GR    2370.0     690.0    2364.0    712.0    2362.0   721.0   2361.0   732.0    2360.0    762.0
GR    2361.5     783.0    2361.5    795.0    2361.0   810.0   2361.5   830.0    2361.5    843.0
GR    2361.5     861.0    2361.5    890.0    2361.4   893.3   2361.3   896.5    2361.3    899.8
GR    2361.2     903.0    2361.1    906.3    2361.0   909.5   2360.9   912.8    2360.8    916.0
GR    2360.8     919.3    2360.7    922.5    2360.6   925.8   2360.5   929.0    2360.4    932.4
GR    2360.3     935.8    2360.2    939.2    2360.1   942.6   2360.0   946.0    2359.9    949.5
GR    2359.8     953.0    2359.6    956.5    2359.5   960.0   2359.5   963.3    2359.4    966.7
GR    2359.4     970.0    2359.3    973.3    2359.3   976.7   2359.3   980.0    2359.2    983.3
GR    2359.2     986.7    2359.1    990.0    2359.1   993.3   2359.0   996.7    2359.0   1000.0
GR    2359.2    1003.7    2359.3   1007.3    2359.5  1011.0   2360.0  1015.0    2361.0   1018.0
GR    2362.0    1021.0    2362.3   1024.4    2362.6  1027.9   2362.9  1031.3    2363.1   1034.7
GR    2363.4    1038.1    2363.7   1041.6    2364.0  1045.0   2368.0  1073.0    2369.0   1091.0
GR    2369.0    1100.0

ET                              9.1                                                   648.70    1062.19
          CONFLUENCE OF UPPER FLYING E WASH AND HOLLY WASH
X1    3.355        60     990.0     1013.3    240     245     250
GR    2376.0     560.0    2373.0    579.0    2370.0   598.0   2368.0   622.0    2366.0    645.0
GR    2364.0     670.0    2364.0    690.0    2364.5   710.0   2364.0   728.0    2363.5    738.0
GR    2364.0     747.0    2364.5    760.0    2365.0   780.0   2365.0   800.0    2364.5    815.0
GR    2365.0     835.0    2365.0    853.3    2365.0   871.7   2365.0   890.0    2365.0    905.5
GR    2365.0     921.0    2366.0    950.0    2366.0   953.3   2366.0   956.7    2366.0    960.0
GR    2365.5     963.3    2365.0    966.5    2364.5   969.8   2364.0   973.0    2363.5    976.5
GR    2363.0     980.0    2362.9    983.3    2362.8   986.7   2362.8   990.0    2362.7    993.3
GR    2362.6     996.7    2362.5   1000.0    2362.6  1003.3   2362.7  1006.7    2362.8   1010.0
GR    2362.8    1013.3    2362.9   1016.7    2363.0  1020.0   2363.2  1023.0    2363.3   1026.0
GR    2363.5    1029.0    2364.5   1032.0    2364.4  1035.5   2364.3  1039.0    2364.1   1042.5
GR    2364.0    1046.0    2364.4   1049.8    2364.8  1053.6   2365.2  1057.4    2365.6   1061.2
GR    2366.0    1065.0    2370.0   1105.0    2374.0  1130.0   2376.0  1165.0    2378.0   1185.0

ET                              9.1                                                   626.24    1222.47
          UPPER FLYING E WASH/HOLLY WASH CONFLUENCE
          HYDRAULIC CONTROL LINE IS AT STATION 1000.0
X1    3.454        91     1000.0    1017.0    450     530     520
GR    2385.0     500.0    2384.0    516.0    2382.0   532.0   2380.0   550.0    2378.0    565.5
GR    2376.0     581.0    2374.0    600.5    2372.0   620.0   2371.3   640.0    2370.5    660.0
GR    2370.0     680.0    2369.5    691.0    2370.0   704.0   2371.0   730.0    2372.0    751.0
GR    2371.0     770.0    2371.0    787.5    2371.0   805.0   2370.8   822.5    2370.5    840.0
GR    2370.8     856.0    2371.0    872.0    2371.3   895.5   2371.5   919.0    2372.0    930.0
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| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2372.3 | 933.7 | 2372.7 | 937.3 | 2373.0 | 941.0 | 2372.5 | 945.5 | 2372.0 | 950.0 |
| | 2371.8 | 953.6 | 2371.6 | 957.2 | 2371.4 | 960.8 | 2371.2 | 964.4 | 2371.0 | 968.0 |
| GR | 2370.9 | 971.6 | 2370.9 | 975.1 | 2370.8 | 978.7 | 2370.8 | 982.2 | 2370.7 | 985.8 |
| GR | 2370.7 | 989.3 | 2370.6 | 992.9 | 2370.6 | 996.4 | 2370.5 | 1000.0 | 2370.5 | 1003.4 |
| GR | 2370.5 | 1006.8 | 2370.5 | 1010.2 | 2370.5 | 1013.6 | 2370.5 | 1017.0 | 2371.0 | 1021.0 |
| GR | 2371.5 | 1025.0 | 2372.0 | 1029.0 | 2372.1 | 1032.9 | 2372.1 | 1036.8 | 2372.2 | 1040.6 |
| GR | 2372.3 | 1044.5 | 2372.3 | 1048.4 | 2372.4 | 1052.3 | 2372.4 | 1056.1 | 2372.5 | 1060.0 |
| GR | 2371.0 | 1081.0 | 2372.0 | 1100.0 | 2372.5 | 1115.0 | 2373.0 | 1130.0 | 2372.8 | 1150.0 |
| GR | 2372.5 | 1170.0 | 2372.3 | 1173.3 | 2372.2 | 1176.7 | 2372.0 | 1180.0 | 2371.4 | 1183.6 |
| GR | 2370.8 | 1187.2 | 2370.2 | 1190.8 | 2369.6 | 1194.4 | 2369.0 | 1198.0 | 2368.8 | 1201.0 |
| GR | 2368.7 | 1204.0 | 2368.5 | 1207.0 | 2368.8 | 1209.5 | 2369.0 | 1212.0 | 2369.5 | 1215.0 |
| GR | 2370.0 | 1218.0 | 2371.3 | 1221.3 | 2372.7 | 1224.7 | 2374.0 | 1228.0 | 2374.8 | 1231.4 |
| GR | 2375.6 | 1234.8 | 2376.4 | 1238.2 | 2377.2 | 1241.6 | 2378.0 | 1245.0 | 2380.0 | 1260.0 |
| GR | 2382.5 | 1280.0 | | | | | | | | |
| QT | 2 | 896 | 896 | | | | | | | |
| ET | | | 9.1 | | | | | | 804.32 | 1155.18 |
| | UPPER FLYING E WASH | | | | | | | | | |
| X1 | 3.549 | 78 | 990.0 | 1005.5 | 525 | 500 | 500 | | | |
| GR | 2392.0 | 525.0 | 2390.0 | 540.0 | 2390.0 | 555.0 | 2389.0 | 578.0 | 2388.5 | 596.5 |
| GR | 2388.0 | 615.0 | 2387.0 | 637.5 | 2386.0 | 660.0 | 2385.0 | 677.5 | 2384.0 | 695.0 |
| GR | 2383.3 | 712.5 | 2382.5 | 730.0 | 2382.3 | 752.5 | 2382.0 | 775.0 | 2381.7 | 780.0 |
| GR | 2381.3 | 785.0 | 2381.0 | 790.0 | 2380.7 | 795.0 | 2380.3 | 800.0 | 2380.0 | 805.0 |
| GR | 2379.6 | 810.2 | 2379.2 | 815.4 | 2378.8 | 820.6 | 2378.4 | 825.8 | 2378.0 | 831.0 |
| GR | 2378.0 | 835.5 | 2378.0 | 840.0 | 2378.7 | 845.0 | 2379.3 | 850.0 | 2380.0 | 855.0 |
| | 2379.8 | 860.0 | 2379.7 | 865.0 | 2379.5 | 870.0 | 2379.5 | 875.0 | 2379.5 | 880.0 |
| | 2379.5 | 885.0 | 2379.5 | 890.0 | 2379.5 | 895.0 | 2379.5 | 900.0 | 2379.5 | 905.0 |
| | 2379.5 | 910.0 | 2379.5 | 915.0 | 2379.5 | 920.0 | 2379.5 | 925.0 | 2379.5 | 930.0 |
| GR | 2379.5 | 935.0 | 2379.5 | 940.0 | 2379.6 | 944.5 | 2379.8 | 949.0 | 2379.9 | 953.5 |
| GR | 2380.0 | 958.0 | 2380.0 | 964.0 | 2380.0 | 970.0 | 2379.5 | 975.0 | 2379.0 | 980.0 |
| GR | 2378.9 | 985.0 | 2378.8 | 990.0 | 2378.6 | 995.0 | 2378.5 | 1000.0 | 2378.8 | 1005.5 |
| GR | 2379.0 | 1011.0 | 2379.3 | 1016.5 | 2379.5 | 1022.0 | 2379.5 | 1027.3 | 2379.5 | 1032.7 |
| GR | 2379.5 | 1038.0 | 2379.4 | 1043.3 | 2379.3 | 1048.5 | 2379.1 | 1053.8 | 2379.0 | 1059.0 |
| GR | 2379.0 | 1077.0 | 2379.0 | 1095.0 | 2379.0 | 1112.5 | 2379.0 | 1130.0 | 2380.0 | 1155.0 |
| GR | 2385.0 | 1177.5 | 2390.0 | 1200.0 | 2392.0 | 1220.0 | | | | |
| ET | | | 9.1 | | | | | | 719.31 | 1051.29 |
| X1 | 3.643 | 95 | 995.0 | 1015.0 | 505 | 495 | 500 | | | |
| GR | 2396.0 | 590.0 | 2395.0 | 601.7 | 2394.0 | 613.3 | 2393.0 | 625.0 | 2392.0 | 636.7 |
| GR | 2391.0 | 648.3 | 2390.0 | 660.0 | 2389.8 | 665.6 | 2389.6 | 671.1 | 2389.3 | 676.7 |
| GR | 2389.1 | 682.2 | 2388.9 | 687.8 | 2388.7 | 693.3 | 2388.4 | 698.9 | 2388.2 | 704.4 |
| GR | 2388.0 | 710.0 | 2387.8 | 715.0 | 2387.5 | 720.0 | 2387.3 | 725.0 | 2387.0 | 730.0 |
| GR | 2387.3 | 736.3 | 2387.5 | 742.5 | 2387.8 | 748.8 | 2388.0 | 755.0 | 2388.3 | 760.0 |
| GR | 2388.5 | 765.0 | 2388.3 | 770.0 | 2388.0 | 775.0 | 2387.5 | 780.0 | 2387.0 | 785.0 |
| GR | 2386.5 | 790.0 | 2386.0 | 795.0 | 2385.8 | 800.0 | 2385.5 | 805.0 | 2386.0 | 810.0 |
| GR | 2386.3 | 816.0 | 2386.6 | 822.0 | 2386.9 | 828.0 | 2387.2 | 834.0 | 2387.5 | 840.0 |
| GR | 2387.4 | 845.8 | 2387.3 | 851.7 | 2387.3 | 857.5 | 2387.2 | 863.3 | 2387.1 | 869.2 |
| GR | 2387.0 | 875.0 | 2387.0 | 895.0 | 2386.9 | 900.7 | 2386.7 | 906.4 | 2386.6 | 912.1 |
| GR | 2386.4 | 917.9 | 2386.3 | 923.6 | 2386.1 | 929.3 | 2386.0 | 935.0 | 2386.5 | 940.0 |
| GR | 2387.0 | 945.0 | 2387.5 | 950.0 | 2388.0 | 955.0 | 2388.2 | 960.3 | 2388.3 | 965.7 |
| GR | 2388.5 | 971.0 | 2388.3 | 975.5 | 2388.0 | 980.0 | 2387.0 | 985.0 | 2386.0 | 990.0 |
| | 2385.5 | 995.0 | 2385.0 | 1000.0 | 2385.0 | 1010.0 | 2385.5 | 1015.0 | 2386.0 | 1020.0 |
| | 2386.3 | 1025.7 | 2386.6 | 1031.4 | 2386.9 | 1037.1 | 2387.1 | 1042.9 | 2387.4 | 1048.6 |
| GR | 2387.7 | 1054.3 | 2388.0 | 1060.0 | 2388.3 | 1065.7 | 2388.6 | 1071.4 | 2388.9 | 1077.1 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| [illegible] | 2389.1 | 1082.9 | 2389.4 | 1088.6 | 2389.7 | 1094.3 | 2390.0 | 1100.0 | 2390.6 | 1105.9 |
| [illegible] | 2391.3 | 1111.8 | 2391.9 | 1117.7 | 2392.6 | 1123.6 | 2393.2 | 1129.6 | 2393.8 | 1135.4 |
| GR | 2394.4 | 1141.4 | 2395.1 | 1147.3 | 2395.7 | 1153.2 | 2396.4 | 1159.1 | 2397.0 | 1165.0 |
| ET | | | 9.1 | | | | | | 746.92 | 1027.08 |
| X1 | 3.740 | 60 | 990.0 | 1010.0 | 505 | 510 | 510 | | | |
| GR | 2407.0 | 605.0 | 2404.7 | 624.0 | 2402.3 | 643.0 | 2400.0 | 662.0 | 2399.0 | 681.0 |
| GR | 2398.0 | 700.0 | 2396.5 | 705.0 | 2396.5 | 731.0 | 2395.5 | 748.0 | 2395.0 | 771.0 |
| GR | 2394.8 | 794.3 | 2394.7 | 817.7 | 2394.5 | 841.0 | 2394.5 | 860.7 | 2394.5 | 880.3 |
| GR | 2394.5 | 900.0 | 2394.7 | 918.3 | 2394.8 | 936.7 | 2395.0 | 955.0 | 2396.0 | 960.0 |
| GR | 2396.1 | 962.5 | 2396.3 | 965.0 | 2396.4 | 967.5 | 2396.5 | 970.0 | 2396.3 | 972.7 |
| GR | 2396.2 | 975.3 | 2396.0 | 978.0 | 2395.3 | 980.3 | 2394.7 | 982.7 | 2394.0 | 985.0 |
| GR | 2393.8 | 987.5 | 2393.5 | 990.0 | 2393.4 | 992.5 | 2393.3 | 995.0 | 2393.1 | 997.5 |
| GR | 2393.0 | 1000.0 | 2393.1 | 1002.5 | 2393.3 | 1005.0 | 2393.4 | 1007.5 | 2393.5 | 1010.0 |
| GR | 2393.6 | 1012.5 | 2393.8 | 1015.0 | 2393.9 | 1017.5 | 2394.0 | 1020.0 | 2394.5 | 1022.3 |
| GR | 2395.0 | 1024.5 | 2395.5 | 1026.8 | 2396.0 | 1029.0 | 2396.5 | 1031.4 | 2397.0 | 1033.8 |
| GR | 2397.5 | 1036.1 | 2398.0 | 1038.5 | 2398.5 | 1040.9 | 2399.0 | 1043.3 | 2399.5 | 1045.6 |
| GR | 2400.0 | 1048.0 | 2402.0 | 1060.0 | 2406.0 | 1075.0 | 2408.0 | 1089.0 | 2408.5 | 1105.0 |
| ET | | | 9.1 | | | | | | 638.53 | 1021.60 |
| X1 | 3.838 | 80 | 990.0 | 1010.0 | 525 | 515 | 520 | | | |
| GR | 2418.0 | 500.0 | 2416.0 | 520.0 | 2414.0 | 540.0 | 2412.0 | 560.0 | 2410.0 | 579.7 |
| GR | 2408.0 | 599.3 | 2406.0 | 619.0 | 2405.0 | 634.5 | 2404.0 | 650.0 | 2403.0 | 660.0 |
| GR | 2403.5 | 687.0 | 2404.0 | 702.0 | 2403.8 | 718.0 | 2403.7 | 734.0 | 2403.5 | 750.0 |
| GR | 2404.0 | 773.0 | 2404.3 | 791.5 | 2404.5 | 810.0 | 2404.5 | 829.5 | 2404.5 | 849.0 |
| [illegible] | 2404.5 | 868.5 | 2404.5 | 888.0 | 2404.3 | 904.0 | 2404.0 | 920.0 | 2404.0 | 940.0 |
| [illegible] | 2406.0 | 960.0 | 2406.5 | 965.0 | 2406.4 | 967.0 | 2406.3 | 969.0 | 2406.1 | 971.0 |
| [illegible] | 2406.0 | 973.0 | 2405.5 | 975.0 | 2405.0 | 977.0 | 2404.5 | 979.0 | 2404.0 | 981.0 |
| GR | 2403.8 | 983.3 | 2403.5 | 985.5 | 2403.3 | 987.8 | 2403.0 | 990.0 | 2402.9 | 992.0 |
| GR | 2402.8 | 994.0 | 2402.7 | 996.0 | 2402.6 | 998.0 | 2402.5 | 1000.0 | 2402.6 | 1002.0 |
| GR | 2402.7 | 1004.0 | 2402.8 | 1006.0 | 2402.9 | 1008.0 | 2403.0 | 1010.0 | 2403.3 | 1012.0 |
| GR | 2403.6 | 1014.0 | 2403.9 | 1016.0 | 2404.2 | 1018.0 | 2404.5 | 1020.0 | 2404.8 | 1022.0 |
| GR | 2405.1 | 1024.0 | 2405.4 | 1026.0 | 2405.7 | 1028.0 | 2406.0 | 1030.0 | 2406.2 | 1032.1 |
| GR | 2406.4 | 1034.3 | 2406.5 | 1036.4 | 2406.7 | 1038.6 | 2406.9 | 1040.7 | 2407.1 | 1042.9 |
| GR | 2407.3 | 1045.0 | 2407.4 | 1047.1 | 2407.6 | 1049.3 | 2407.8 | 1051.4 | 2408.0 | 1053.6 |
| GR | 2408.1 | 1055.7 | 2408.3 | 1057.9 | 2408.5 | 1060.0 | 2408.0 | 1085.0 | 2407.5 | 1100.0 |
| GR | 2408.0 | 1125.0 | 2412.0 | 1150.0 | 2413.0 | 1170.0 | 2414.0 | 1190.0 | 2414.0 | 1210.0 |
| ET | | | 9.1 | | | | | | 989.23 | 1081.46 |
| X1 | 3.950 | 45 | 995.0 | 1008.0 | 600 | 600 | 590 | | | |
| GR | 2427.0 | 921.0 | 2425.5 | 938.0 | 2424.0 | 955.0 | 2423.5 | 958.1 | 2423.0 | 961.3 |
| GR | 2422.5 | 964.4 | 2422.0 | 967.5 | 2421.5 | 970.6 | 2421.0 | 973.8 | 2420.5 | 976.9 |
| GR | 2420.0 | 980.0 | 2418.4 | 983.0 | 2416.8 | 986.0 | 2415.2 | 989.0 | 2413.6 | 992.0 |
| GR | 2412.0 | 995.0 | 2411.8 | 997.5 | 2411.5 | 1000.0 | 2411.7 | 1002.7 | 2411.8 | 1005.3 |
| GR | 2412.0 | 1008.0 | 2412.1 | 1011.1 | 2412.3 | 1014.3 | 2412.4 | 1017.4 | 2412.6 | 1020.6 |
| GR | 2412.7 | 1023.7 | 2412.9 | 1026.9 | 2413.0 | 1030.0 | 2413.3 | 1033.3 | 2413.7 | 1036.7 |
| GR | 2414.0 | 1040.0 | 2414.0 | 1042.9 | 2414.0 | 1045.8 | 2414.0 | 1048.6 | 2414.0 | 1051.5 |
| GR | 2414.0 | 1054.4 | 2414.0 | 1057.3 | 2414.0 | 1060.1 | 2414.0 | 1063.0 | 2415.0 | 1080.0 |
| GR | 2415.8 | 1094.8 | 2416.0 | 1113.0 | 2419.0 | 1142.0 | 2423.5 | 1166.0 | 2426.0 | 1190.0 |

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ET                      9.1                                                983.07    1065.80
X1   3.980        55   991.8   1013.0      160       150       160
GR  2430.0     958.0  2428.0    961.4   2426.0     964.8    2424.0    968.2  2422.0     971.6
GR  2420.0     975.0  2419.0    978.5   2418.0     982.0    2417.0    985.3  2416.0     988.5
GR  2415.0     991.8  2414.0    995.0   2413.8     997.5    2413.5   1000.0  2414.0    1002.0
GR  2414.3    1004.8  2414.5   1007.5   2414.8    1010.3    2415.0   1013.0  2415.3    1015.8
GR  2415.5    1018.5  2415.8   1021.3   2416.0    1024.0    2416.1   1027.1  2416.2    1030.2
GR  2416.3    1033.3  2416.4   1036.4   2416.5    1039.5    2416.6   1042.6  2416.7    1045.7
GR  2416.8    1048.8  2416.9   1051.9   2417.0    1055.0    2417.2   1058.2  2417.4    1061.4
GR  2417.6    1064.6  2417.8   1067.8   2418.0    1071.0    2418.4   1073.8  2418.8    1076.6
GR  2419.2    1079.4  2419.6   1082.2   2420.0    1085.0    2420.4   1088.1  2420.7    1091.2
GR  2421.1    1094.3  2421.4   1097.4   2421.8    1100.5    2422.1   1103.6  2424.5    1106.8
GR  2425.9    1109.9  2426.2   1113.0   2426.6    1116.1    2427.9   1119.2  2430.3    1122.3

ET                      9.1                                                934.21    1031.51
X1   4.032        57   995.0   1011.0      290       235       270
GR  2435.0     868.0  2434.4    871.4   2433.8     874.8    2433.1    878.1  2432.5     881.5
GR  2431.9     884.9  2431.3    888.3   2430.6     891.6    2430.0    895.0  2429.3     898.1
GR  2428.5     901.3  2427.8    904.4   2427.0     907.5    2426.3    910.6  2425.5     913.8
GR  2424.8     916.9  2424.0    920.0   2423.7     923.3    2423.3    926.7  2423.0     930.0
GR  2422.7     933.3  2422.3    936.7   2422.0     940.0    2422.1    943.3  2422.2     946.7
GR  2422.3     950.0  2422.3    953.3   2422.4     956.7    2422.5    960.0  2422.4     963.0
GR  2422.3     966.0  2422.1    969.0   2422.0     972.0    2421.6    975.6  2421.2     979.2
GR  2420.8     982.8  2420.4    986.4   2420.0     990.0    2419.8    992.5  2419.5     995.0
GR  2419.3     997.5  2419.0   1000.0   2419.2    1003.7    2419.3   1007.3  2419.5    1011.0
GR  2419.7    1014.0  2419.8   1017.0   2420.0    1020.0    2420.7   1023.3  2421.3    1026.7
GR  2422.0    1030.0  2423.3   1033.3   2424.7    1036.7    2426.0   1040.0  2427.3    1043.3
GR  2428.7    1046.7  2430.0   1050.0

ET                      9.1                                                922.23    1073.70
          DOWNSTREAM OF GEORGE'S TANK DAM EMBANKMENT
X1   4.103        13   990.0   1010.0      355       405       375
GR  2436.0     870.0  2434.0    877.0   2432.0     890.0    2430.0    910.0  2428.0     925.0
GR  2426.3     990.0  2426.0   1000.0   2426.3    1010.0    2428.0   1070.0  2430.0    1090.0
GR  2432.0    1096.0  2434.0   1102.0   2436.0    1108.0

ET                      9.1                                                875.75    1064.72
          UPSTREAM OF GEORGE'S TANK DAM EMBANKMENT
          GEORGE'S TANK - NO DESIGN OR CONSTRUCTION DATA AVAILABLE FOR
          DAM FORMING TANK:  NOT DEPENDABLE FOR FLOOD RISK PLANNING.
          EXCESS FLOWS BREAK INTO SMALL CHANNEL ALONG WEST EDGE OF TANK OVER
          A WIDE, FLAT SADDLE.  SMALL CHANNEL ANALYZED AND SUBMITTED SEPARATELY
          AS A ZONE A UNDER THE TITLE "GEORGE'S TANK BREAKOUT".
X1   4.168        13   990.0   1010.0      345       345       345
GR  2442.0     810.0  2440.0    825.0   2438.0     845.0    2436.0    855.0  2434.0     880.0
GR  2432.5     990.0  2432.4   1000.0   2432.7    1010.0    2434.0   1062.0  2436.0    1078.0
GR  2438.0    1085.0  2440.0   1092.0   2442.0    1100.0
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                                9.1                                                    888.16    1056.14
          LOWER PORTION OF GEORGE'S TANK
X1    4.213       33     995.0    1010.0     270     195     235
GR   2450.0    665.0    2448.0     678.3  2446.0   691.7  2444.0    705.0  2442.0     722.5
GR   2440.0    740.0    2439.3     753.0  2438.7   766.0  2438.0    779.0  2437.7     794.0
GR   2437.3    809.0    2437.0     824.0  2436.8   838.3  2436.5    852.5  2436.3     866.8
GR   2436.0    881.0    2435.3     894.0  2434.7   907.0  2434.0    920.0  2433.5     935.0
GR   2434.0    955.0    2434.0     970.0  2433.0   982.5  2432.0    995.0  2431.5    1000.0
GR   2432.0   1010.0    2433.0    1025.0  2434.0  1040.0  2436.0   1060.0  2440.0    1075.0
GR   2450.0   1095.0    2455.0    1107.5  2460.0  1120.0

ET                              9.1                                                    900.30    1071.34
          UPPER PORTION OF GEORGE'S TANK
X1    4.301       24     989.0    1009.0     465     465     465
GR   2452.0    731.0    2450.7     749.0  2449.3   767.0  2448.0    785.0  2447.0     805.3
GR   2446.0    825.5    2445.0     845.8  2444.0   866.0  2443.3    886.0  2442.7     906.0
GR   2442.0    926.0    2441.8     944.5  2441.5   963.0  2441.3    981.5  2441.2     989.0
GR   2441.0   1000.0    2441.2    1009.0  2441.5  1025.0  2442.0   1050.0  2443.0    1074.5
GR   2444.0   1099.0    2448.0    1129.0  2452.0  1150.0  2456.0   1180.0

ET                              9.1                                                    935.37    1041.17
X1    4.384       33     988.0    1008.0     405     430     440
GR   2462.0    537.0    2461.6     558.0  2461.2   579.0  2460.8    600.0  2460.4     621.0
GR   2460.0    642.0    2459.5     664.3  2459.0   686.5  2458.5    708.8  2458.0     731.0
GR   2457.5    751.5    2457.0     772.0  2456.5   792.5  2456.0    813.0  2456.0     832.5
GR   2456.0    852.0    2454.7     869.3  2453.3   886.7  2452.0    904.0  2451.0     915.0
GR   2449.0    942.0    2448.0     963.0  2447.5   981.5  2447.3    988.0  2447.0    1000.0
GR   2447.3   1008.0    2448.0    1027.0  2450.0  1046.0  2452.0   1065.0  2456.0    1092.0
GR   2460.0   1117.0    2466.0    1139.5  2472.0  1162.0

ET                              9.1                                                    941.83    1265.84
X1    4.493       48     986.2    1006.2     465     600     575
GR   2469.0    595.0    2468.0     615.0  2467.6   636.2  2467.2    657.4  2466.8     678.6
GR   2466.4    699.8    2466.0     721.0  2465.6   742.8  2465.2    764.6  2464.8     786.4
GR   2464.4    808.2    2464.0     830.0  2462.0   847.0  2460.0    864.0  2459.7     886.0
GR   2459.3    908.0    2459.0     930.0  2458.3   953.3  2457.7    976.7  2457.4     986.2
GR   2457.0   1000.0    2457.1    1006.2  2457.3  1022.3  2457.5   1044.5  2457.8    1066.8
GR   2458.0   1089.0    2458.0    1109.2  2458.0  1129.3  2458.0   1149.5  2458.0    1169.7
GR   2458.0   1189.8    2458.0    1210.0  2458.3  1232.5  2458.5   1255.0  2458.8    1277.5
GR   2459.0   1300.0    2459.5    1317.5  2460.0  1335.0  2460.7   1360.0  2461.3    1385.0
GR   2462.0   1410.0    2463.0    1430.0  2464.0  1450.0  2465.3   1475.0  2466.7    1500.0
GR   2468.0   1525.0    2470.0    1543.0  2472.0  1561.0

ET                              9.1                                                    795.83    1337.36
X1    4.594       49     992.0    1012.5     520     530     530
GR   2472.0    700.0    2470.7     724.0  2469.3   748.0  2468.0    772.0  2467.5     791.5
GR   2467.0    811.0    2466.7     835.7  2466.3   860.3  2466.0    885.0  2467.0     909.5
GR   2468.0    934.0    2468.5     944.5  2469.0   955.0  2468.5    965.5  2468.0     976.0
GR   2467.1    986.5    2467.0     988.0  2466.5   992.0  2466.0   1000.0  2466.3    1006.5
GR   2466.5   1012.5    2467.0    1025.0  2467.2  1038.0  2467.3   1051.0  2467.5    1064.0
GR   2467.7   1077.0    2467.8    1090.0  2468.0  1103.0  2468.5   1114.5  2469.0    1126.0
GR   2468.0   1155.0    2467.0    1172.5  2466.0  1190.0  2466.0   1211.0  2467.0    1228.0
GR   2468.0   1245.0    2469.0    1265.0  2468.0  1290.0  2466.0   1320.0  2468.0    1345.0
```

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2469.0 | 1360.0 | 2468.0 | 1390.0 | 2468.7 | 1413.3 | 2469.3 | 1436.7 | 2470.0 | 1460.0 |
| | 2470.5 | 1482.8 | 2471.0 | 1505.5 | 2471.5 | 1528.3 | 2472.0 | 1551.0 | | |
| ET | | | 9.1 | | | | | | 791.68 | 1013.02 |
| X1 | 4.688 | 42 | 986.1 | 1004.3 | 440 | 530 | 500 | | | |
| GR | 2480.0 | 480.0 | 2479.3 | 506.7 | 2478.7 | 533.3 | 2478.0 | 560.0 | 2477.8 | 581.0 |
| GR | 2477.6 | 602.0 | 2477.4 | 623.0 | 2477.2 | 644.0 | 2477.0 | 665.0 | 2476.8 | 688.0 |
| GR | 2476.6 | 711.0 | 2476.4 | 734.0 | 2476.2 | 757.0 | 2476.0 | 780.0 | 2475.0 | 810.0 |
| GR | 2474.5 | 832.5 | 2474.0 | 855.0 | 2474.5 | 878.5 | 2475.0 | 902.0 | 2475.0 | 925.5 |
| GR | 2475.0 | 949.0 | 2474.0 | 979.0 | 2473.9 | 986.1 | 2473.8 | 993.2 | 2473.0 | 1000.0 |
| GR | 2473.5 | 1002.3 | 2473.9 | 1004.3 | 2476.0 | 1015.0 | 2478.0 | 1049.0 | 2477.0 | 1080.0 |
| GR | 2478.0 | 1091.0 | 2478.2 | 1115.0 | 2478.4 | 1139.0 | 2478.6 | 1163.0 | 2478.8 | 1187.0 |
| GR | 2479.0 | 1211.0 | 2479.3 | 1232.3 | 2479.7 | 1253.7 | 2480.0 | 1275.0 | 2480.3 | 1301.7 |
| GR | 2480.7 | 1328.3 | 2481.0 | 1355.0 | | | | | | |
| ET | | | 9.1 | | | | | | 637.91 | 1035.56 |
| X1 | 4.787 | 64 | 990.0 | 1010.7 | 580 | 470 | 520 | | | |
| GR | 2488.0 | 460.0 | 2487.7 | 483.7 | 2487.3 | 507.3 | 2487.0 | 531.0 | 2486.3 | 553.7 |
| GR | 2485.7 | 576.3 | 2485.0 | 599.0 | 2484.5 | 624.5 | 2484.0 | 650.0 | 2483.5 | 675.0 |
| GR | 2483.0 | 700.0 | 2483.0 | 725.0 | 2483.0 | 750.0 | 2483.5 | 777.5 | 2484.0 | 805.0 |
| GR | 2485.0 | 832.0 | 2484.0 | 864.0 | 2483.0 | 890.0 | 2484.0 | 915.0 | 2485.0 | 936.0 |
| GR | 2484.9 | 940.9 | 2484.7 | 945.7 | 2484.6 | 950.6 | 2484.4 | 955.4 | 2484.3 | 960.3 |
| GR | 2484.1 | 965.1 | 2484.0 | 970.0 | 2483.7 | 975.0 | 2483.3 | 980.0 | 2483.0 | 985.0 |
| GR | 2482.7 | 990.0 | 2482.3 | 995.0 | 2482.0 | 1000.0 | 2482.3 | 1005.3 | 2482.7 | 1010.7 |
| GR | 2483.0 | 1016.0 | 2483.3 | 1021.3 | 2483.7 | 1026.7 | 2484.0 | 1032.0 | 2484.3 | 1036.5 |
| | 2484.5 | 1041.0 | 2484.8 | 1045.5 | 2485.0 | 1050.0 | 2485.0 | 1055.0 | 2485.0 | 1060.0 |
| | 2485.0 | 1065.0 | 2485.0 | 1070.0 | 2485.0 | 1075.0 | 2485.0 | 1080.0 | 2485.0 | 1085.0 |
| | 2485.3 | 1112.3 | 2485.5 | 1139.5 | 2485.8 | 1166.8 | 2486.0 | 1194.0 | 2486.2 | 1220.2 |
| GR | 2486.4 | 1246.4 | 2486.6 | 1272.6 | 2486.8 | 1298.8 | 2487.0 | 1325.0 | 2487.0 | 1354.0 |
| GR | 2487.0 | 1383.0 | 2487.0 | 1412.0 | 2487.5 | 1431.0 | 2488.0 | 1450.0 | | |
| ET | | | 9.1 | | | | | | 971.98 | 1346.20 |
| X1 | 4.881 | 96 | 988.0 | 1007.7 | 470 | 495 | 500 | | | |
| GR | 2496.0 | 737.2 | 2495.9 | 744.1 | 2495.8 | 750.9 | 2495.7 | 757.8 | 2495.6 | 760.1 |
| GR | 2495.5 | 767.0 | 2495.4 | 773.8 | 2495.3 | 780.7 | 2495.2 | 785.3 | 2495.1 | 789.8 |
| GR | 2495.0 | 796.7 | 2494.9 | 803.6 | 2494.8 | 808.2 | 2494.8 | 810.5 | 2494.7 | 812.8 |
| GR | 2494.7 | 815.1 | 2494.6 | 817.4 | 2494.6 | 822.0 | 2494.5 | 824.3 | 2494.5 | 826.7 |
| GR | 2494.4 | 829.0 | 2494.4 | 833.6 | 2494.3 | 835.9 | 2494.3 | 838.2 | 2494.2 | 840.5 |
| GR | 2494.2 | 842.8 | 2494.1 | 845.1 | 2494.1 | 847.4 | 2494.0 | 849.7 | 2494.0 | 854.3 |
| GR | 2493.9 | 856.6 | 2493.9 | 858.9 | 2493.8 | 861.2 | 2493.8 | 863.5 | 2493.7 | 865.8 |
| GR | 2493.7 | 868.1 | 2493.6 | 870.4 | 2493.6 | 875.0 | 2493.5 | 877.3 | 2493.5 | 879.7 |
| GR | 2493.4 | 882.0 | 2493.4 | 886.6 | 2493.3 | 888.9 | 2493.3 | 891.2 | 2493.2 | 893.5 |
| GR | 2493.2 | 895.8 | 2493.1 | 898.1 | 2493.1 | 900.4 | 2493.0 | 902.7 | 2493.0 | 905.0 |
| GR | 2492.9 | 912.3 | 2492.7 | 919.6 | 2492.6 | 926.9 | 2492.4 | 934.1 | 2492.3 | 941.4 |
| GR | 2492.1 | 948.7 | 2492.0 | 956.0 | 2491.0 | 962.5 | 2490.0 | 969.0 | 2489.0 | 975.5 |
| GR | 2488.0 | 982.0 | 2487.7 | 988.0 | 2487.3 | 994.0 | 2487.0 | 1000.0 | 2487.5 | 1005.5 |
| GR | 2487.7 | 1007.7 | 2488.0 | 1011.0 | 2489.3 | 1017.3 | 2490.7 | 1023.7 | 2492.0 | 1030.0 |
| GR | 2492.3 | 1036.0 | 2492.7 | 1042.0 | 2493.0 | 1048.0 | 2492.0 | 1060.0 | 2490.0 | 1080.0 |
| GR | 2488.0 | 1100.0 | 2488.0 | 1120.0 | 2490.0 | 1140.0 | 2492.0 | 1160.0 | 2493.0 | 1185.0 |
| GR | 2493.0 | 1220.0 | 2492.5 | 1237.5 | 2492.0 | 1255.0 | 2490.0 | 1277.5 | 2488.0 | 1300.0 |
| GR | 2488.0 | 1325.0 | 2490.0 | 1352.5 | 2492.0 | 1380.0 | 2492.5 | 1401.3 | 2493.0 | 1422.5 |
| | 2493.5 | 1443.8 | 2494.0 | 1465.0 | 2494.8 | 1490.0 | 2495.5 | 1515.0 | 2496.3 | 1540.0 |
| | 2497.0 | 1565.0 | | | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 959.98 | 1090.10 |
| X1 | 5.014 | 46 | 990.0 | 1009.5 | 485 | 850 | 700 | | | |
| GR | 2505.0 | 925.0 | 2504.8 | 930.5 | 2504.5 | 936.0 | 2504.3 | 941.5 | 2504.0 | 947.0 |
| GR | 2502.7 | 951.3 | 2501.3 | 955.7 | 2500.0 | 960.0 | 2499.5 | 965.0 | 2499.0 | 970.0 |
| GR | 2498.5 | 975.0 | 2498.0 | 980.0 | 2497.8 | 985.0 | 2497.5 | 990.0 | 2497.3 | 995.0 |
| GR | 2497.0 | 1000.0 | 2497.3 | 1004.8 | 2497.5 | 1009.5 | 2497.8 | 1014.3 | 2498.0 | 1019.0 |
| GR | 2498.5 | 1024.5 | 2499.0 | 1030.0 | 2499.0 | 1035.0 | 2499.0 | 1040.0 | 2499.0 | 1045.0 |
| GR | 2499.0 | 1050.0 | 2499.0 | 1055.0 | 2499.0 | 1060.0 | 2499.2 | 1065.0 | 2499.3 | 1070.0 |
| GR | 2499.5 | 1075.0 | 2499.7 | 1080.0 | 2499.8 | 1085.0 | 2500.0 | 1090.0 | 2500.3 | 1095.0 |
| GR | 2500.7 | 1100.0 | 2501.0 | 1105.0 | 2501.3 | 1110.0 | 2501.7 | 1115.0 | 2502.0 | 1120.0 |
| GR | 2502.3 | 1125.0 | 2502.7 | 1130.0 | 2503.0 | 1135.0 | 2503.3 | 1140.0 | 2503.7 | 1145.0 |
| GR | 2504.0 | 1150.0 | | | | | | | | |
| ET | | | 9.1 | | | | | | 766.80 | 1048.75 |
| X1 | 5.082 | 72 | 990.0 | 1011.5 | 410 | 310 | 360 | | | |
| GR | 2508.0 | 750.0 | 2507.6 | 755.0 | 2507.1 | 760.0 | 2506.7 | 765.0 | 2506.3 | 770.0 |
| GR | 2505.9 | 775.0 | 2505.4 | 780.0 | 2505.0 | 785.0 | 2505.1 | 790.3 | 2505.3 | 795.6 |
| GR | 2505.4 | 800.9 | 2505.6 | 806.1 | 2505.7 | 811.4 | 2505.9 | 816.7 | 2506.0 | 822.0 |
| GR | 2506.0 | 826.9 | 2506.0 | 831.8 | 2506.0 | 836.7 | 2506.0 | 841.6 | 2506.0 | 846.4 |
| GR | 2506.0 | 851.3 | 2506.0 | 856.2 | 2506.0 | 861.1 | 2506.0 | 866.0 | 2506.0 | 870.9 |
| GR | 2506.0 | 875.8 | 2506.0 | 880.7 | 2506.0 | 885.6 | 2506.0 | 890.4 | 2506.0 | 895.3 |
| GR | 2506.0 | 900.2 | 2506.0 | 905.1 | 2506.0 | 910.0 | 2506.0 | 915.0 | 2506.0 | 920.0 |
| GR | 2506.0 | 925.0 | 2506.0 | 930.0 | 2506.0 | 935.0 | 2506.0 | 940.0 | 2506.0 | 945.0 |
| GR | 2506.0 | 950.0 | 2506.0 | 955.0 | 2506.0 | 960.0 | 2506.0 | 965.0 | 2505.7 | 970.0 |
| [illegible] | 2505.3 | 975.0 | 2505.0 | 980.0 | 2504.8 | 985.0 | 2504.5 | 990.0 | 2504.3 | 995.0 |
| [illegible] | 2504.0 | 1000.0 | 2504.2 | 1004.6 | 2504.4 | 1009.2 | 2504.5 | 1011.5 | 2504.6 | 1013.8 |
| [illegible] | 2504.8 | 1018.4 | 2505.0 | 1023.0 | 2505.3 | 1028.7 | 2505.7 | 1034.3 | 2506.0 | 1040.0 |
| GR | 2506.3 | 1045.3 | 2506.7 | 1050.7 | 2507.0 | 1056.0 | 2507.3 | 1061.3 | 2507.7 | 1066.7 |
| GR | 2508.0 | 1072.0 | 2508.3 | 1076.7 | 2508.7 | 1081.3 | 2509.0 | 1086.0 | 2509.3 | 1090.7 |
| GR | 2509.7 | 1095.3 | 2510.0 | 1100.0 | | | | | | |
| ET | | | 9.1 | | | | | | 732.80 | 1027.56 |
| X1 | 5.175 | 39 | 990.0 | 1007.5 | 530 | 460 | 490 | | | |
| GR | 2516.0 | 709.0 | 2515.0 | 725.0 | 2514.0 | 741.0 | 2514.5 | 755.5 | 2515.0 | 770.0 |
| GR | 2515.0 | 785.0 | 2515.0 | 800.0 | 2515.0 | 815.0 | 2515.0 | 830.0 | 2514.8 | 848.8 |
| GR | 2514.5 | 867.5 | 2514.3 | 886.3 | 2514.0 | 905.0 | 2514.0 | 923.3 | 2514.0 | 941.7 |
| GR | 2514.0 | 960.0 | 2513.5 | 965.0 | 2513.0 | 970.0 | 2512.5 | 975.0 | 2512.0 | 980.0 |
| GR | 2511.8 | 985.0 | 2511.5 | 990.0 | 2511.3 | 995.0 | 2511.0 | 1000.0 | 2511.3 | 1005.0 |
| GR | 2511.5 | 1007.5 | 2511.7 | 1010.0 | 2512.0 | 1015.0 | 2513.0 | 1020.0 | 2514.0 | 1025.0 |
| GR | 2515.0 | 1030.0 | 2515.1 | 1035.0 | 2515.3 | 1040.0 | 2515.4 | 1045.0 | 2515.5 | 1050.0 |
| GR | 2515.6 | 1055.0 | 2515.8 | 1060.0 | 2515.9 | 1065.0 | 2516.0 | 1070.0 | | |
| ET | | | 9.1 | | | | | | 976.30 | 1148.96 |
| X1 | 5.279 | 45 | 990.0 | 1010.0 | 540 | 550 | 550 | | | |
| GR | 2524.0 | 960.0 | 2523.5 | 964.8 | 2523.0 | 969.5 | 2522.5 | 974.3 | 2522.0 | 979.0 |
| GR | 2520.5 | 984.5 | 2519.0 | 990.0 | 2518.5 | 995.0 | 2518.0 | 1000.0 | 2518.5 | 1005.0 |
| GR | 2519.0 | 1010.0 | 2519.7 | 1015.0 | 2520.3 | 1020.0 | 2521.0 | 1025.0 | 2521.1 | 1030.0 |
| GR | 2521.2 | 1035.0 | 2521.3 | 1040.0 | 2521.4 | 1045.0 | 2521.4 | 1050.0 | 2521.6 | 1055.0 |
| GR | 2521.6 | 1060.0 | 2521.7 | 1065.0 | 2521.8 | 1070.0 | 2521.9 | 1075.0 | 2522.0 | 1080.0 |
| GR | 2522.0 | 1084.9 | 2522.0 | 1089.8 | 2522.0 | 1094.8 | 2522.0 | 1099.7 | 2522.0 | 1104.6 |
| [illegible] | 2522.0 | 1109.5 | 2522.0 | 1114.4 | 2522.0 | 1119.3 | 2522.0 | 1124.3 | 2522.0 | 1129.2 |
| [illegible] | 2522.0 | 1134.1 | 2522.0 | 1139.0 | 2522.1 | 1144.1 | 2522.3 | 1149.3 | 2522.4 | 1154.4 |
| GR | 2522.6 | 1159.6 | 2522.7 | 1164.7 | 2522.9 | 1169.9 | 2523.0 | 1175.0 | 2524.0 | 1205.0 |

```
NT        2      2152      2152
ET                         9.1                                                    626.24    1222.47
          HOLLY WASH/FLYING E WASH CONFLUENCE
          HYDRAULIC CONTROL LINE IS AT STATION 1207.0
X1     -3.454       91    1198.0    1212.0       450       530       545
GR     2385.0    500.0    2384.0     516.0    2382.0     532.0    2380.0     550.0    2378.0     565.5
GR     2376.0    581.0    2374.0     600.5    2372.0     620.0    2371.3     640.0    2370.5     660.0
GR     2370.0    680.0    2369.5     691.0    2370.0     704.0    2371.0     730.0    2372.0     751.0
GR     2371.0    770.0    2371.0     787.5    2371.0     805.0    2370.8     822.5    2370.5     840.0
GR     2370.8    856.0    2371.0     872.0    2371.3     895.5    2371.5     919.0    2372.0     930.0
GR     2372.3    933.7    2372.7     937.3    2373.0     941.0    2372.5     945.5    2372.0     950.0
GR     2371.8    953.6    2371.6     957.2    2371.4     960.8    2371.2     964.4    2371.0     968.0
GR     2370.9    971.6    2370.9     975.1    2370.8     978.7    2370.8     982.2    2370.7     985.8
GR     2370.7    989.3    2370.6     992.9    2370.6     996.4    2370.5    1000.0    2370.5    1003.4
GR     2370.5   1006.8    2370.5    1010.2    2370.5    1013.6    2370.5    1017.0    2371.0    1021.0
GR     2371.5   1025.0    2372.0    1029.0    2372.1    1032.9    2372.1    1036.8    2372.2    1040.6
GR     2372.3   1044.5    2372.3    1048.4    2372.4    1052.3    2372.4    1056.1    2372.5    1060.0
GR     2371.0   1081.0    2372.0    1100.0    2372.5    1115.0    2373.0    1130.0    2372.8    1150.0
GR     2372.5   1170.0    2372.3    1173.3    2372.2    1176.7    2372.0    1180.0    2371.4    1183.6
GR     2370.8   1187.2    2370.2    1190.8    2369.6    1194.4    2369.0    1198.0    2368.8    1201.0
GR     2368.7   1204.0    2368.5    1207.0    2368.8    1209.5    2369.0    1212.0    2369.5    1215.0
GR     2370.0   1218.0    2371.3    1221.3    2372.7    1224.7    2374.0    1228.0    2374.8    1231.4
GR     2375.6   1234.8    2376.4    1238.2    2377.2    1241.6    2378.0    1245.0    2380.0    1260.0
GR     2382.5   1280.0

NT        2      1361      1361
ET                         9.1                                                    906.79    1012.82
          HOLLY WASH
          HOLLY WASH RIVER MILES MEASURED FROM CONFLUENCE AT SECTION 3.355
X1      0.198       55     987.0    1007.0       500       510       500
GR     2386.0    650.0    2384.0     670.0    2383.0     687.5    2382.0     705.0    2381.5     722.0
GR     2381.0    739.0    2380.5     756.0    2380.3     778.0    2380.0     800.0    2379.5     821.0
GR     2379.1    839.5    2378.8     858.0    2378.4     876.5    2378.0     895.0    2374.6       972
GR       2375      974    2374.9     975.8    2374.8     977.7    2374.8     979.5    2374.7     981.3
GR     2374.5    983.2    2374.5       985    2374.3     987.0    2374.0     989.0    2373.8     991.0
GR     2373.5    993.0    2373.4     994.8    2373.3     996.5    2373.1     998.3    2373.0    1000.0
GR     2373.3   1002.5    2373.5    1005.0    2374.3    1007.0    2375.2    1009.0    2376.0    1011.0
GR     2376.3   1013.1    2376.5    1015.3    2376.8    1017.4    2377.0    1019.5    2377.3    1021.6
GR     2377.5   1023.8    2377.8    1025.9    2378.0    1028.0    2378.1    1030.0    2378.2    1032.0
GR     2378.3   1034.0    2378.4    1036.0    2378.6    1038.0    2378.7    1040.0    2378.8    1042.0
GR     2378.9   1044.0    2379.0    1046.0    2380.0    1057.0    2383.0    1074.5    2386.0    1092.0

ET                         9.1                                                    935.66    1024.74
X1      0.291       70     993.0    1010.0       485       490       490
GR     2396.0    800.0    2395.0     809.3    2394.0     818.7    2393.0     828.0    2391.3     837.0
GR     2389.7    846.0    2388.0     855.0    2386.7     863.3    2385.3     871.7    2384.0     880.0
GR     2383.5    890.0    2383.8     902.0    2384.0     914.0    2383.3     923.0    2382.7     932.0
GR     2382.0    941.0    2381.8     942.8    2381.7     944.7    2381.5     946.5    2381.3     948.3
GR     2381.2    950.2    2381.0     952.0    2380.8     954.0    2380.5     956.0    2380.3     958.0
GR     2380.0    960.0    2379.9     962.0    2379.8     964.0    2379.7     966.0    2379.6     968.0
       2379.5    970.0    2379.6     971.9    2379.6     973.8    2379.7     975.6    2379.8     977.5
       2379.8    979.4    2379.9     981.3    2379.9     983.1    2380.0     985.0    2379.8     987.0
GR     2379.5    989.0    2379.3     991.0    2379.0     993.0    2378.9     994.8    2378.8     996.5
```

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2378.6 | 998.3 | 2378.5 | 1000.0 | 2378.6 | 1002.0 | 2378.7 | 1004.0 | 2378.8 | 1006.0 |
| | 2378.9 | 1008.0 | 2379.0 | 1010.0 | 2379.6 | 1012.0 | 2380.2 | 1014.0 | 2380.8 | 1016.0 |
| GR | 2381.4 | 1018.0 | 2382.0 | 1020.0 | 2382.2 | 1021.8 | 2382.3 | 1023.7 | 2382.5 | 1025.5 |
| GR | 2382.7 | 1027.3 | 2382.8 | 1029.2 | 2383.0 | 1031.0 | 2383.3 | 1041.0 | 2383.7 | 1051.0 |
| GR | 2384.0 | 1061.0 | 2385.0 | 1070.5 | 2386.0 | 1080.0 | 2390.0 | 1090.0 | 2394.0 | 1100.0 |
| ET | | | 9.1 | | | | | | 975.64 | 1028.66 |
| X1 | 0.387 | 38 | 991.0 | 1006.7 | 510 | 510 | 510 | | | |
| GR | 2396.0 | 880.0 | 2395.0 | 895.5 | 2394.0 | 911.0 | 2392.0 | 930.0 | 2390.0 | 955.0 |
| GR | 2389.7 | 958.2 | 2389.4 | 961.4 | 2389.1 | 964.6 | 2388.8 | 967.8 | 2388.5 | 971.0 |
| GR | 2388.0 | 975.0 | 2386.5 | 978.3 | 2385.0 | 981.7 | 2383.5 | 985.0 | 2383.4 | 988.0 |
| GR | 2383.3 | 991.0 | 2383.2 | 994.0 | 2383.1 | 997.0 | 2383.0 | 1000.0 | 2383.2 | 1003.3 |
| GR | 2383.3 | 1006.7 | 2383.5 | 1010.0 | 2384.8 | 1012.5 | 2386.0 | 1015.0 | 2386.4 | 1018.2 |
| GR | 2386.8 | 1021.4 | 2387.2 | 1024.6 | 2387.6 | 1027.8 | 2388.0 | 1031.0 | 2388.3 | 1046.0 |
| GR | 2388.5 | 1061.0 | 2389.3 | 1077.5 | 2390.0 | 1094.0 | 2390.0 | 1114.3 | 2390.0 | 1134.7 |
| GR | 2390.0 | 1155.0 | 2396.0 | 1182.0 | 2400.0 | 1200.0 | | | | |
| ET | | | 9.1 | | | | | | 932.01 | 1016.89 |
| X1 | 0.482 | 76 | 989.0 | 1011.0 | 485 | 485 | 500 | | | |
| GR | 2401.0 | 840.0 | 2400.8 | 849.5 | 2400.5 | 859.0 | 2400.3 | 868.5 | 2400.0 | 878.0 |
| GR | 2399.0 | 889.0 | 2398.0 | 900.0 | 2397.6 | 902.0 | 2397.2 | 904.0 | 2396.8 | 906.0 |
| GR | 2396.4 | 908.0 | 2396.0 | 910.0 | 2395.6 | 912.0 | 2395.2 | 914.0 | 2394.8 | 916.0 |
| GR | 2394.4 | 918.0 | 2394.0 | 920.0 | 2393.7 | 922.0 | 2393.3 | 924.0 | 2393.0 | 926.0 |
| GR | 2392.7 | 928.0 | 2392.3 | 930.0 | 2392.0 | 932.0 | 2391.3 | 934.2 | 2390.7 | 936.3 |
| GR | 2390.0 | 938.5 | 2389.3 | 940.7 | 2388.7 | 942.8 | 2388.0 | 945.0 | 2388.0 | 947.5 |
| | 2388.0 | 950.0 | 2388.3 | 951.8 | 2388.7 | 953.7 | 2389.0 | 955.5 | 2389.3 | 957.3 |
| | 2389.7 | 959.2 | 2390.0 | 961.0 | 2390.3 | 962.8 | 2390.5 | 964.7 | 2390.8 | 966.5 |
| | 2391.0 | 968.3 | 2391.3 | 970.2 | 2391.5 | 972.0 | 2391.3 | 974.1 | 2391.1 | 976.3 |
| GR | 2390.9 | 978.4 | 2390.8 | 980.5 | 2390.6 | 982.6 | 2390.4 | 984.8 | 2390.2 | 986.9 |
| GR | 2390.0 | 989.0 | 2387.0 | 996.0 | 2387.0 | 998.0 | 2387.0 | 1000.0 | 2387.3 | 1002.5 |
| GR | 2387.5 | 1005.0 | 2388.3 | 1007.0 | 2389.2 | 1009.0 | 2390.0 | 1011.0 | 2390.7 | 1013.1 |
| GR | 2391.4 | 1015.1 | 2392.1 | 1017.2 | 2392.9 | 1019.3 | 2393.6 | 1021.4 | 2394.3 | 1023.4 |
| GR | 2395.0 | 1025.5 | 2395.7 | 1027.6 | 2396.4 | 1029.6 | 2397.1 | 1031.7 | 2397.9 | 1033.8 |
| GR | 2398.6 | 1035.9 | 2399.3 | 1037.9 | 2400.0 | 1040.0 | 2400.7 | 1048.3 | 2401.3 | 1056.7 |
| GR | 2402.0 | 1065.0 | | | | | | | | |
| ET | | 9.1 | 9.1 | | | | | | 978 | 1022 |
| X1 | 0.559 | 21 | 978 | 1022 | 405 | 405 | 405 | | | |
| GR | 2404 | 715 | 2402 | 730 | 2400 | 745 | 2398 | 795 | 2396 | 820 |
| GR | 2396 | 825 | 2398 | 828 | 2400 | 830 | 2402 | 845 | 2404 | 855 |
| GR | 2406 | 872 | 2406 | 940 | 2404 | 960 | 2402 | 965 | 2400 | 978 |
| GR | 2398 | 985 | 2396 | 1000 | 2398 | 1015 | 2400 | 1022 | 2402 | 1030 |
| GR | 2404 | 1043 | | | | | | | | |
| ET | | | 9.1 | | | | | | 972.01 | 1027.23 |
| X1 | 0.607 | 75 | 991.0 | 1009.0 | 290 | 265 | 255 | | | |
| GR | 2410.0 | 850.0 | 2409.9 | 853.0 | 2409.8 | 856.0 | 2409.7 | 859.0 | 2409.6 | 862.0 |
| GR | 2409.5 | 865.0 | 2409.6 | 868.3 | 2409.7 | 871.7 | 2409.8 | 875.0 | 2409.8 | 878.3 |
| GR | 2409.9 | 881.7 | 2410.0 | 885.0 | 2409.8 | 888.3 | 2409.7 | 891.7 | 2409.5 | 895.0 |
| GR | 2409.3 | 898.3 | 2409.2 | 901.7 | 2409.0 | 905.0 | 2408.8 | 908.3 | 2408.7 | 911.7 |
| | 2408.5 | 915.0 | 2408.3 | 918.3 | 2408.2 | 921.7 | 2408.0 | 925.0 | 2407.7 | 928.3 |
| | 2407.3 | 931.7 | 2407.0 | 935.0 | 2406.7 | 938.3 | 2406.3 | 941.7 | 2406.0 | 945.0 |
| GR | 2405.8 | 948.1 | 2405.5 | 951.3 | 2405.3 | 954.4 | 2405.0 | 957.5 | 2404.8 | 960.6 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2404.5 | 963.8 | 2404.3 | 966.9 | 2404.0 | 970.0 | 2403.2 | 973.0 | 2402.4 | 976.0 |
| | 2401.6 | 979.0 | 2400.8 | 982.0 | 2400.0 | 985.0 | 2399.8 | 988.0 | 2399.6 | 991.0 |
| GR | 2399.4 | 994.0 | 2399.2 | 997.0 | 2399.0 | 1000.0 | 2399.2 | 1003.0 | 2399.4 | 1006.0 |
| GR | 2399.6 | 1009.0 | 2399.8 | 1012.0 | 2400.0 | 1015.0 | 2400.9 | 1018.2 | 2401.8 | 1021.4 |
| GR | 2402.7 | 1024.6 | 2403.6 | 1027.7 | 2404.6 | 1030.9 | 2405.4 | 1034.1 | 2406.4 | 1037.3 |
| GR | 2407.3 | 1040.4 | 2408.2 | 1043.6 | 2409.1 | 1046.8 | 2410.0 | 1050.0 | 2410.9 | 1053.2 |
| GR | 2411.8 | 1056.4 | 2412.7 | 1059.6 | 2413.6 | 1062.7 | 2414.6 | 1065.9 | 2415.4 | 1069.1 |
| GR | 2416.4 | 1072.3 | 2417.3 | 1075.4 | 2418.2 | 1078.6 | 2419.1 | 1081.8 | 2420.0 | 1085.0 |
| ET | | | 9.1 | | | | | | 966.83 | 1050.17 |
| X1 | 0.681 | 15 | 987.3 | 1012.5 | 390 | 390 | 390 | | | |
| GR | 2420.0 | 945.0 | 2416.0 | 946.0 | 2412.0 | 958.0 | 2408.0 | 960.0 | 2404.0 | 985.0 |
| GR | 2403.3 | 987.3 | 2403.0 | 1000.0 | 2403.5 | 1012.5 | 2404.0 | 1015.0 | 2405.3 | 1036.7 |
| GR | 2406.7 | 1048.3 | 2408.0 | 1060.0 | 2412.0 | 1080.0 | 2416.0 | 1110.0 | 2420.0 | 1135.0 |
| ET | | | 9.1 | | | | | | 973.30 | 1021.70 |
| X1 | 0.747 | 52 | 988.0 | 1008.0 | 370 | 320 | 350 | | | |
| GR | 2422.0 | 910.0 | 2421.7 | 912.9 | 2421.4 | 915.7 | 2421.1 | 918.6 | 2420.9 | 921.4 |
| GR | 2420.6 | 924.3 | 2420.3 | 927.1 | 2420.0 | 930.0 | 2419.5 | 933.1 | 2419.0 | 936.3 |
| GR | 2418.5 | 939.4 | 2418.0 | 942.5 | 2417.5 | 945.6 | 2417.0 | 948.8 | 2416.5 | 951.9 |
| GR | 2416.0 | 955.0 | 2415.2 | 958.0 | 2414.4 | 961.0 | 2413.6 | 964.0 | 2412.8 | 967.0 |
| GR | 2412.0 | 970.0 | 2411.2 | 973.0 | 2410.4 | 976.0 | 2409.6 | 979.0 | 2408.8 | 982.0 |
| GR | 2408.0 | 985.0 | 2407.4 | 988.0 | 2406.8 | 991.0 | 2406.2 | 994.0 | 2405.6 | 997.0 |
| GR | 2405.0 | 1000.0 | 2406.0 | 1003.3 | 2407.0 | 1006.7 | 2407.4 | 1008.0 | 2408.0 | 1010.0 |
| GR | 2408.8 | 1013.0 | 2409.6 | 1016.0 | 2410.4 | 1019.0 | 2411.2 | 1022.0 | 2412.0 | 1025.0 |
| | 2413.6 | 1028.0 | 2415.2 | 1031.0 | 2416.8 | 1034.0 | 2418.4 | 1037.0 | 2420.0 | 1040.0 |
| | 2422.6 | 1042.9 | 2425.1 | 1045.7 | 2427.7 | 1048.6 | 2430.3 | 1051.4 | 2432.9 | 1054.3 |
| | 2435.4 | 1057.1 | 2438.0 | 1060.0 | | | | | | |
| ET | | | 9.1 | | | | | | 929.63 | 1032.36 |
| X1 | 0.853 | 53 | 995.5 | 1010.0 | 510 | 560 | 560 | | | |
| GR | 2440.0 | 825.0 | 2439.0 | 830.4 | 2438.0 | 835.8 | 2437.0 | 841.1 | 2436.0 | 846.5 |
| GR | 2435.0 | 851.9 | 2434.0 | 857.3 | 2433.0 | 862.6 | 2432.0 | 868.0 | 2430.0 | 873.5 |
| GR | 2428.0 | 879.0 | 2426.0 | 884.5 | 2424.0 | 890.0 | 2423.6 | 894.9 | 2423.2 | 899.8 |
| GR | 2422.8 | 904.7 | 2422.4 | 909.6 | 2422.0 | 914.5 | 2421.6 | 919.4 | 2421.2 | 924.3 |
| GR | 2420.8 | 929.2 | 2420.4 | 934.1 | 2420.0 | 939.0 | 2419.8 | 944.3 | 2419.5 | 949.5 |
| GR | 2419.3 | 954.8 | 2419.0 | 960.0 | 2418.8 | 965.2 | 2418.7 | 970.3 | 2418.5 | 975.5 |
| GR | 2418.3 | 980.7 | 2418.2 | 985.8 | 2418.0 | 991.0 | 2417.5 | 995.5 | 2417.0 | 1000.0 |
| GR | 2417.3 | 1005.0 | 2417.5 | 1010.0 | 2417.8 | 1015.0 | 2418.0 | 1020.0 | 2419.0 | 1025.5 |
| GR | 2420.0 | 1031.0 | 2422.7 | 1035.8 | 2425.3 | 1040.7 | 2428.0 | 1045.5 | 2430.7 | 1050.3 |
| GR | 2433.3 | 1055.2 | 2436.0 | 1060.0 | 2436.7 | 1065.3 | 2437.3 | 1070.7 | 2438.0 | 1076.0 |
| GR | 2438.7 | 1081.3 | 2439.3 | 1086.7 | 2440.0 | 1092.0 | | | | |
| ET | | | 9.1 | | | | | | 962 | 1035 |
| X1 | 0.954 | 56 | 986.5 | 1008.0 | 440 | 605 | 530 | | | |
| GR | 2443.0 | 900.0 | 2442.7 | 905.0 | 2442.3 | 910.0 | 2442.0 | 915.0 | 2441.6 | 920.0 |
| GR | 2441.2 | 925.0 | 2440.8 | 930.0 | 2440.4 | 935.0 | 2440.0 | 940.0 | 2438.4 | 945.0 |
| GR | 2436.8 | 950.0 | 2435.2 | 955.0 | 2433.6 | 960.0 | 2432.0 | 965.0 | 2431.3 | 970.7 |
| GR | 2430.7 | 976.3 | 2430.0 | 982.0 | 2429.8 | 986.5 | 2429.5 | 991.0 | 2429.3 | 995.5 |
| GR | 2429.0 | 1000.0 | 2429.5 | 1005.0 | 2429.8 | 1008.0 | 2430.0 | 1010.0 | 2430.3 | 1015.0 |
| GR | 2430.7 | 1020.0 | 2431.0 | 1025.0 | 2431.3 | 1030.0 | 2431.7 | 1035.0 | 2432.0 | 1040.0 |
| | 2432.6 | 1044.7 | 2433.1 | 1049.4 | 2433.7 | 1054.1 | 2434.3 | 1058.9 | 2434.9 | 1063.6 |
| | 2435.4 | 1068.3 | 2436.0 | 1073.0 | 2436.6 | 1078.3 | 2437.1 | 1083.6 | 2437.7 | 1088.9 |
| GR | 2438.3 | 1094.1 | 2438.9 | 1099.4 | 2439.4 | 1104.7 | 2440.0 | 1110.0 | 2441.0 | 1115.0 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2442.0 | 1120.0 | 2443.0 | 1125.0 | 2444.0 | 1130.0 | 2445.0 | 1135.0 | 2446.0 | 1140.0 |
| | 2447.0 | 1145.0 | 2448.0 | 1150.0 | 2449.0 | 1155.0 | 2450.0 | 1160.0 | 2451.0 | 1165.0 |
| GR | 2452.0 | 1170.0 | | | | | | | | |
| ET | | | 9.1 | | | | | | 941 | 1029 |
| X1 | 1.005 | 39 | 990.5 | 1007.5 | 280 | 255 | 270 | | | |
| GR | 2445.0 | 650.0 | 2442.0 | 681.0 | 2441.0 | 701.3 | 2440.0 | 721.7 | 2439.0 | 742.0 |
| GR | 2438.3 | 761.5 | 2437.5 | 781.0 | 2436.8 | 800.5 | 2436.0 | 820.0 | 2435.3 | 840.2 |
| GR | 2434.7 | 860.3 | 2434.0 | 880.5 | 2433.3 | 900.7 | 2432.7 | 920.8 | 2432.0 | 941.0 |
| GR | 2431.9 | 946.0 | 2431.8 | 951.0 | 2431.6 | 956.0 | 2431.5 | 961.0 | 2431.4 | 966.0 |
| GR | 2431.3 | 971.0 | 2431.1 | 976.0 | 2431.0 | 981.0 | 2430.8 | 985.8 | 2430.5 | 990.5 |
| GR | 2430.3 | 995.3 | 2430.0 | 1000.0 | 2430.3 | 1005.0 | 2430.5 | 1007.5 | 2430.7 | 1010.0 |
| GR | 2431.0 | 1015.0 | 2431.3 | 1019.7 | 2431.7 | 1024.3 | 2432.0 | 1029.0 | 2433.0 | 1034.3 |
| GR | 2434.0 | 1039.5 | 2435.0 | 1044.8 | 2436.0 | 1050.0 | 2440.0 | 1075.0 | | |
| ET | | | 9.1 | | | | | | 968 | 1043 |
| X1 | 1.101 | 54 | 990.0 | 1010.0 | 485 | 515 | 510 | | | |
| GR | 2450.0 | 870.0 | 2449.5 | 875.0 | 2449.0 | 880.0 | 2448.5 | 885.0 | 2448.0 | 890.0 |
| GR | 2447.2 | 895.2 | 2446.4 | 900.4 | 2445.6 | 905.6 | 2444.8 | 910.8 | 2444.0 | 916.0 |
| GR | 2443.6 | 920.9 | 2443.1 | 925.8 | 2442.7 | 930.7 | 2442.2 | 935.6 | 2441.8 | 940.4 |
| GR | 2441.3 | 945.3 | 2440.9 | 950.2 | 2440.4 | 955.1 | 2440.0 | 960.0 | 2439.2 | 965.0 |
| GR | 2438.4 | 970.0 | 2437.6 | 975.0 | 2436.8 | 980.0 | 2436.0 | 985.0 | 2435.7 | 990.0 |
| GR | 2435.3 | 995.0 | 2435.0 | 1000.0 | 2435.3 | 1005.0 | 2435.7 | 1010.0 | 2436.0 | 1015.0 |
| GR | 2436.0 | 1020.7 | 2436.0 | 1026.3 | 2436.0 | 1032.0 | 2436.5 | 1037.4 | 2437.0 | 1042.8 |
| GR | 2437.5 | 1048.1 | 2438.0 | 1053.5 | 2438.5 | 1058.9 | 2439.0 | 1064.3 | 2439.5 | 1069.6 |
| | 2440.0 | 1075.0 | 2440.6 | 1080.0 | 2441.1 | 1085.0 | 2441.7 | 1090.0 | 2442.3 | 1095.0 |
| | 2442.9 | 1100.0 | 2443.4 | 1105.0 | 2444.0 | 1110.0 | 2445.3 | 1115.0 | 2446.7 | 1120.0 |
| | 2448.0 | 1125.0 | 2449.3 | 1130.0 | 2450.7 | 1135.0 | 2452.0 | 1140.0 | | |
| ET | | | 9.1 | | | | | | 934 | 1030 |
| X1 | 1.202 | 44 | 992.0 | 1014.3 | 510 | 540 | 530 | | | |
| GR | 2461.0 | 900.0 | 2459.2 | 905.0 | 2457.4 | 910.0 | 2455.6 | 915.0 | 2453.8 | 920.0 |
| GR | 2452.0 | 925.0 | 2450.7 | 930.0 | 2449.3 | 935.0 | 2448.0 | 940.0 | 2448.0 | 945.2 |
| GR | 2448.0 | 950.3 | 2448.0 | 955.5 | 2448.0 | 960.7 | 2448.0 | 965.8 | 2448.0 | 971.0 |
| GR | 2447.8 | 975.8 | 2447.5 | 980.5 | 2447.3 | 985.3 | 2447.0 | 990.0 | 2446.8 | 992.0 |
| GR | 2446.5 | 995.0 | 2446.0 | 1000.0 | 2446.3 | 1004.8 | 2446.5 | 1009.5 | 2446.8 | 1014.3 |
| GR | 2447.0 | 1019.0 | 2447.5 | 1024.5 | 2448.0 | 1030.0 | 2448.5 | 1035.3 | 2449.0 | 1040.5 |
| GR | 2449.5 | 1045.8 | 2450.0 | 1051.0 | 2450.5 | 1056.3 | 2451.0 | 1061.5 | 2451.5 | 1066.8 |
| GR | 2452.0 | 1072.0 | 2453.0 | 1076.8 | 2454.0 | 1081.5 | 2455.0 | 1086.3 | 2456.0 | 1091.0 |
| GR | 2457.0 | 1095.8 | 2458.0 | 1100.5 | 2459.0 | 1105.3 | 2460.0 | 1110.0 | | |
| ET | | | 9.1 | | | | | | 952 | 1058 |
| X1 | 1.295 | 54 | 991.3 | 1013.5 | 490 | 495 | 490 | | | |
| GR | 2464.0 | 888.0 | 2463.2 | 893.4 | 2462.4 | 898.8 | 2461.6 | 904.2 | 2460.8 | 909.6 |
| GR | 2460.0 | 915.0 | 2459.3 | 920.2 | 2458.7 | 925.3 | 2458.0 | 930.5 | 2457.3 | 935.7 |
| GR | 2456.7 | 940.8 | 2456.0 | 946.0 | 2455.6 | 951.1 | 2455.3 | 956.3 | 2454.9 | 961.4 |
| GR | 2454.5 | 966.5 | 2454.1 | 971.6 | 2453.8 | 976.8 | 2453.4 | 981.9 | 2453.0 | 987.0 |
| GR | 2452.7 | 991.3 | 2452.3 | 995.7 | 2452.0 | 1000.0 | 2452.3 | 1004.5 | 2452.5 | 1009.0 |
| GR | 2452.8 | 1013.5 | 2453.0 | 1018.0 | 2453.2 | 1023.0 | 2453.3 | 1028.0 | 2453.5 | 1033.0 |
| GR | 2453.7 | 1038.0 | 2453.8 | 1043.0 | 2454.0 | 1048.0 | 2454.1 | 1053.2 | 2454.3 | 1058.3 |
| GR | 2454.5 | 1063.5 | 2454.6 | 1068.6 | 2454.8 | 1073.8 | 2454.9 | 1078.9 | 2455.1 | 1084.1 |
| | 2455.2 | 1089.2 | 2455.4 | 1094.4 | 2455.5 | 1099.5 | 2455.7 | 1104.7 | 2455.9 | 1109.8 |
| | 2456.0 | 1115.0 | 2457.1 | 1120.0 | 2458.3 | 1125.0 | 2459.4 | 1130.0 | 2460.6 | 1135.0 |
| GR | 2461.7 | 1140.0 | 2462.9 | 1145.0 | 2464.0 | 1150.0 | 2466.0 | 1178.0 | | |

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|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 919 | 1030 |
| X1 | 1.399 | 33 | 985.5 | 1010.0 | 580 | 530 | 550 | | | |
| GR | 2479.0 | 819.0 | 2476.0 | 827.7 | 2474.0 | 836.3 | 2472.0 | 845.0 | 2470.7 | 853.3 |
| GR | 2469.3 | 861.7 | 2464.0 | 870.0 | 2463.8 | 880.0 | 2463.5 | 890.0 | 2463.3 | 900.0 |
| GR | 2463.0 | 910.0 | 2462.9 | 918.7 | 2462.7 | 927.4 | 2462.6 | 936.1 | 2462.4 | 944.9 |
| GR | 2462.3 | 953.6 | 2462.1 | 962.3 | 2462.0 | 971.0 | 2461.7 | 980.7 | 2461.5 | 985.5 |
| GR | 2461.3 | 990.3 | 2461.0 | 1000.0 | 2461.5 | 1010.0 | 2462.0 | 1020.0 | 2462.5 | 1030.0 |
| GR | 2463.0 | 1040.0 | 2463.5 | 1050.0 | 2464.0 | 1060.0 | 2466.0 | 1070.5 | 2468.0 | 1081.0 |
| GR | 2473.3 | 1090.7 | 2478.7 | 1100.3 | 2484.0 | 1110.0 | | | | |
| ET | | | 9.1 | | | | | | 957 | 1050 |
| X1 | 1.473 | 40 | 987.5 | 1010.0 | 420 | 370 | 395 | | | |
| GR | 2480.0 | 608.0 | 2478.7 | 629.0 | 2477.3 | 650.0 | 2476.0 | 671.0 | 2475.3 | 692.3 |
| GR | 2474.7 | 713.7 | 2474.0 | 735.0 | 2473.3 | 754.0 | 2472.7 | 773.0 | 2472.0 | 792.0 |
| GR | 2471.5 | 811.5 | 2471.0 | 831.0 | 2470.5 | 850.5 | 2470.0 | 870.0 | 2469.7 | 890.0 |
| GR | 2469.3 | 910.0 | 2469.0 | 930.0 | 2468.8 | 939.0 | 2468.6 | 948.0 | 2468.4 | 957.0 |
| GR | 2468.2 | 966.0 | 2468.0 | 975.0 | 2467.3 | 983.3 | 2466.5 | 987.5 | 2466.7 | 991.7 |
| GR | 2466.0 | 1000.0 | 2466.5 | 1010.0 | 2467.0 | 1020.0 | 2467.3 | 1030.0 | 2467.7 | 1040.0 |
| GR | 2468.0 | 1050.0 | 2469.6 | 1059.0 | 2471.2 | 1068.0 | 2472.8 | 1077.0 | 2474.4 | 1086.0 |
| GR | 2476.0 | 1095.0 | 2477.0 | 1115.0 | 2478.0 | 1135.0 | 2479.0 | 1152.5 | 2480.0 | 1170.0 |
| ET | | | 9.1 | | | | | | 970 | 1070 |
| X1 | 1.576 | 44 | 1000.0 | 1019.0 | 520 | 545 | 540 | | | |
| GR | 2488.0 | 440.0 | 2487.0 | 461.3 | 2486.0 | 482.5 | 2485.0 | 503.8 | 2484.0 | 525.0 |
| | 2483.8 | 545.0 | 2483.5 | 565.0 | 2483.3 | 585.0 | 2483.0 | 605.0 | 2482.8 | 626.5 |
| | 2482.5 | 648.0 | 2482.3 | 669.5 | 2482.0 | 691.0 | 2481.7 | 710.7 | 2481.3 | 730.3 |
| | 2481.0 | 750.0 | 2481.7 | 772.7 | 2482.3 | 795.3 | 2483.0 | 818.0 | 2483.5 | 844.0 |
| GR | 2484.0 | 870.0 | 2482.7 | 888.3 | 2481.3 | 906.7 | 2480.0 | 925.0 | 2479.0 | 936.3 |
| GR | 2478.0 | 947.5 | 2477.0 | 958.8 | 2476.0 | 970.0 | 2475.5 | 977.5 | 2475.0 | 985.0 |
| GR | 2474.5 | 992.5 | 2474.0 | 1000.0 | 2474.0 | 1009.5 | 2474.0 | 1019.0 | 2474.0 | 1029.3 |
| GR | 2474.0 | 1039.7 | 2474.0 | 1050.0 | 2474.3 | 1070.0 | 2474.7 | 1090.0 | 2475.0 | 1110.0 |
| GR | 2476.0 | 1125.0 | 2480.0 | 1150.0 | 2488.0 | 1175.0 | 2496.0 | 1200.0 | | |
| ET | | | 9.1 | | | | | | 960 | 1025 |
| | | SECTION TAKEN FROM TOPOGRAPHIC MAP | | | | | | | | |
| X1 | 1.615 | 9 | 990 | 1010 | 205 | 205 | 205 | | | |
| GR | 2485 | 800 | 2484 | 940 | 2480 | 960 | 2479 | 990 | 2479 | 1000 |
| GR | 2479 | 1010 | 2480 | 1025 | 2484 | 1190 | 2488 | 1205 | | |
| ET | | | 9.1 | | | | | | 910 | 1041 |
| X1 | 1.661 | 38 | 990.5 | 1011.0 | 255 | 215 | 245 | | | |
| GR | 2497.0 | 290.0 | 2496.0 | 312.0 | 2495.5 | 336.5 | 2495.0 | 361.0 | 2494.5 | 385.5 |
| GR | 2494.0 | 410.0 | 2493.7 | 439.0 | 2493.3 | 468.0 | 2493.0 | 497.0 | 2492.7 | 521.3 |
| GR | 2492.3 | 545.7 | 2492.0 | 570.0 | 2491.5 | 595.0 | 2491.0 | 620.0 | 2490.5 | 645.0 |
| GR | 2490.0 | 670.0 | 2489.5 | 692.0 | 2489.0 | 714.0 | 2488.5 | 736.0 | 2488.0 | 758.0 |
| GR | 2487.3 | 780.3 | 2486.7 | 802.7 | 2486.0 | 825.0 | 2485.0 | 855.5 | 2484.0 | 886.0 |
| GR | 2483.5 | 910.5 | 2483.0 | 935.0 | 2483.0 | 958.0 | 2483.0 | 981.0 | 2482.5 | 990.5 |
| GR | 2482.0 | 1000.0 | 2482.5 | 1011.0 | 2483.0 | 1022.0 | 2484.0 | 1041.0 | 2488.0 | 1070.0 |
| GR | 2492.0 | 1102.0 | 2496.0 | 1121.0 | 2500.0 | 1140.0 | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 950 | 1040 |
| X1 | 1.767 | 46 | 990.0 | 1009.0 | 540 | 560 | 560 | | | |
| GR | 2500.0 | 50.0 | 2499.0 | 80.5 | 2498.0 | 111.0 | 2497.6 | 134.8 | 2497.2 | 158.6 |
| GR | 2496.8 | 182.4 | 2496.4 | 206.2 | 2496.0 | 230.0 | 2496.5 | 252.5 | 2497.0 | 275.0 |
| GR | 2496.0 | 309.0 | 2495.5 | 329.5 | 2495.0 | 350.0 | 2495.0 | 370.0 | 2495.5 | 399.5 |
| GR | 2496.0 | 429.0 | 2496.5 | 454.5 | 2497.0 | 480.0 | 2496.5 | 505.0 | 2496.0 | 530.0 |
| GR | 2495.7 | 551.7 | 2495.3 | 573.3 | 2495.0 | 595.0 | 2494.7 | 616.7 | 2494.3 | 638.3 |
| GR | 2494.0 | 660.0 | 2494.0 | 684.5 | 2494.0 | 709.0 | 2493.8 | 736.8 | 2493.5 | 764.5 |
| GR | 2493.3 | 792.3 | 2493.0 | 820.0 | 2492.5 | 850.5 | 2492.0 | 881.0 | 2493.0 | 918.0 |
| GR | 2492.0 | 950.0 | 2491.0 | 984.0 | 2490.6 | 990.0 | 2490.0 | 1000.0 | 2490.5 | 1009.0 |
| GR | 2491.0 | 1018.0 | 2491.5 | 1040.0 | 2492.0 | 1062.0 | 2496.0 | 1090.0 | 2496.5 | 1116.5 |
| GR | 2500.7 | 1125.8 | | | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 960 | 1115 |
| X1 | 1.873 | 42 | 1000.0 | 1024.5 | 500 | 585 | 560 | | | |
| GR | 2508.0 | 360.0 | 2507.0 | 390.0 | 2506.0 | 420.0 | 2505.5 | 449.5 | 2505.0 | 479.0 |
| GR | 2504.7 | 504.3 | 2504.3 | 529.7 | 2504.0 | 555.0 | 2503.0 | 583.3 | 2502.0 | 611.7 |
| GR | 2501.0 | 640.0 | 2500.5 | 670.0 | 2500.0 | 700.0 | 2500.0 | 724.5 | 2500.0 | 749.0 |
| GR | 2500.5 | 774.5 | 2501.0 | 800.0 | 2500.0 | 830.0 | 2499.7 | 853.0 | 2499.3 | 876.0 |
| GR | 2499.0 | 899.0 | 2498.5 | 929.5 | 2498.0 | 960.0 | 2497.5 | 980.0 | 2497.0 | 1000.0 |
| GR | 2497.0 | 1024.5 | 2497.0 | 1049.0 | 2497.3 | 1071.0 | 2497.7 | 1093.0 | 2498.0 | 1115.0 |
| GR | 2498.3 | 1137.0 | 2498.7 | 1159.0 | 2499.0 | 1181.0 | 2499.5 | 1206.5 | 2500.0 | 1232.0 |
| GR | 2500.8 | 1256.0 | 2501.5 | 1280.0 | 2502.3 | 1304.0 | 2503.0 | 1328.0 | 2504.0 | 1360.0 |
| GR | 2506.0 | 1385.0 | 2508.0 | 1410.0 | | | | | | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= .100 CEHV= .300
*SECNO 2.435
WATER EL=X5 CARD= 2309.800
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 952.0 1228.0 TYPE= 1 TARGET= 276.000
CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.435 | 6.37 | 2309.87 | 2309.87 | .00 | 2311.91 | 2.03 | .00 | .00 | 2304.00 |
| 6943.0 | 829.2 | 3269.5 | 2844.4 | 123.2 | 219.6 | 397.0 | .0 | .0 | 2304.00 |
| .00 | 6.73 | 14.89 | 7.16 | .050 | .030 | .050 | .000 | 2303.50 | 957.69 |
| .008113 | 500. | 490. | 455. | 0 | 5 | 3 | .00 | 180.52 | 1138.21 |

FLOW DISTRIBUTION FOR SECNO= 2.43 CWSEL= 2309.87

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 958. | 976. | 991. | 1027. | 1037. | 1047. | 1057. | 1067. | 1077. | 1092. | 1102. | 1138. |
| Q= | 3.9 | 8.1 | 47.1 | 7.1 | 6.5 | 5.9 | 5.3 | 4.8 | 6.1 | 3.1 | 2.3 |
| AREA= | 50.1 | 73.1 | 219.6 | 57.2 | 54.2 | 51.2 | 48.2 | 45.2 | 61.9 | 34.7 | 44.2 |
| VEL= | 5.4 | 7.7 | 14.9 | 8.6 | 8.3 | 8.0 | 7.6 | 7.3 | 6.9 | 6.1 | 3.6 |
| DEPTH= | 2.7 | 4.9 | 6.1 | 5.7 | 5.4 | 5.1 | 4.8 | 4.5 | 4.1 | 3.5 | 1.2 |

1490 NH CARD USED
*SECNO 2.539

3265 DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 465.3 1100.0 TYPE= 1 TARGET= 634.700
ELENCL= 2317.30 ELENCR= 2317.00
AT HIGH FLOW, BOTH YUCCA FLAT WASH AND FLYING E WASH CHANNELS
ARE USED. SECTION REPEATED FOR BOTH MODELS. NH CARD DEFINES CHANNELS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.539 | 6.51 | 2315.51 | 2315.51 | .00 | 2316.75 | 1.23 | 4.16 | .08 | 2313.50 |
| 6943.0 | 374.5 | 1748.2 | 4820.2 | 127.7 | 185.8 | 533.5 | 9.4 | 3.5 | 2313.20 |
| .02 | 2.93 | 9.41 | 9.03 | .050 | .030 | .038 | .000 | 2309.00 | 509.79 |
| .007925 | 570. | 550. | 490. | 0 | 5 | 0 | .00 | 395.38 | 1059.11 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 2.54 CWSEL= 2315.51

| STA= | 510. | 593. | 822. | 881. | 907. | 962. | 980. | 1000. | 1012. | 1027. | 1035. | 1059. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 1.5 | 25.2 | 3.4 | 3.2 | 3.9 | 27.0 | 16.2 | 10.6 | 3.3 | 1.8 | |
| AREA= | 86.8 | 40.9 | 185.8 | 53.8 | 70.4 | 52.0 | 125.3 | 75.2 | 86.5 | 34.1 | 36.3 | |
| VEL= | 3.2 | 2.5 | 9.4 | 4.3 | 3.1 | 5.3 | 15.0 | 15.0 | 8.5 | 6.7 | 3.5 | |
| DEPTH= | 1.0 | .2 | 3.1 | 2.1 | 1.3 | 2.9 | 6.3 | 6.3 | 5.8 | 4.3 | 1.5 | |

*SECNO 2.630

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .51

UPPER FLYING E WASH FULLY DEFINED CHANNEL

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.630 | 4.19 | 2319.19 | 2317.86 | .00 | 2319.65 | .46 | 2.83 | .08 | 2315.40 |
| 2152.0 | 959.7 | 1080.5 | 111.9 | 257.2 | 159.5 | 34.6 | 16.5 | 6.4 | 2315.40 |
| .04 | 3.73 | 6.77 | 3.23 | .050 | .030 | .050 | .000 | 2315.00 | 892.64 |
| .002956 | 480. | 480. | 460. | 2 | 14 | 0 | .00 | 138.04 | 1030.68 |

FLOW DISTRIBUTION FOR SECNO= 2.63 CWSEL= 2319.19

| STA= | 893. | 968. | 976. | 1016. | 1024. | 1031. |
|---|---|---|---|---|---|---|
| PER Q= | 39.1 | 5.5 | 50.2 | 4.4 | .8 | |
| AREA= | 227.1 | 30.1 | 159.5 | 26.2 | 8.5 | |
| VEL= | 3.7 | 3.9 | 6.8 | 3.6 | 2.0 | |
| DEPTH= | 3.0 | 3.8 | 4.0 | 3.4 | 1.2 | |

*SECNO 2.725

3265 DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.725 | 3.77 | 2325.77 | 2325.77 | .00 | 2326.90 | 1.14 | 2.70 | .20 | 2323.50 |
| 2152.0 | 100.4 | 1011.6 | 1039.9 | 29.3 | 97.7 | 153.3 | 20.7 | 8.0 | 2323.50 |
| .06 | 3.43 | 10.35 | 6.78 | .050 | .030 | .050 | .000 | 2322.00 | 907.30 |
| .012847 | 515. | 500. | 485. | 0 | 11 | 0 | .00 | 147.44 | 1151.54 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 2.72 CWSEL= 2325.77

| STA= | 907. | 981. | 1020. | 1121. | 1138. | 1148. | 1152. |
|---|---|---|---|---|---|---|---|
| PER Q= | 4.7 | 47.0 | 15.2 | 24.3 | 8.4 | .4 | |
| AREA= | 29.3 | 97.7 | 58.5 | 64.1 | 27.7 | 3.1 | |
| VEL= | 3.4 | 10.4 | 5.6 | 8.2 | 6.6 | 2.9 | |
| DEPTH= | .4 | 2.5 | .6 | 3.8 | 2.8 | .9 | |

*SECNO 2.812

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 895.0 1425.0 TYPE= 1 TARGET= 530.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.812 | 3.56 | 2331.06 | 2331.06 | .00 | 2331.66 | .60 | 3.79 | .05 | 2327.80 |
| 2152.0 | 298.0 | 1039.8 | 814.2 | 72.1 | 124.2 | 320.7 | 25.0 | 11.2 | 2327.80 |
| .08 | 4.13 | 8.37 | 2.54 | .050 | .030 | .050 | .000 | 2327.50 | 942.05 |
| .005596 | 440. | 460. | 480. | 0 | 12 | 0 | .00 | 433.86 | 1375.90 |

FLOW DISTRIBUTION FOR SECNO= 2.81 CWSEL= 2331.06

| STA= | 942. | 965. | 977. | 1013. | 1020. | 1026. | 1038. | 1062. | 1186. | 1237. | 1289. | 1328. | 1353. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.6 | 8.2 | 48.3 | 4.7 | 3.6 | 4.8 | 3.6 | 3.5 | 4.0 | 3.3 | 4.0 | 4.7 | |
| AREA= | 35.1 | 37.0 | 124.2 | 21.2 | 17.2 | 27.1 | 29.9 | 52.6 | 42.8 | 38.7 | 38.5 | 36.4 | |
| VEL= | 3.4 | 4.8 | 8.4 | 4.8 | 4.5 | 3.8 | 2.6 | 1.4 | 2.0 | 1.8 | 2.3 | 2.8 | |
| DEPTH= | 1.5 | 3.2 | 3.4 | 3.2 | 2.9 | 2.3 | 1.2 | .4 | .8 | .7 | 1.0 | 1.4 | |

| STA= | 1353. | 1376. |
|---|---|---|
| PER Q= | 1.6 | |
| AREA= | 16.2 | |
| VEL= | 2.1 | |
| DEPTH= | .7 | |

*SECNO 2.922

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.922 | 3.68 | 2337.68 | 2337.68 | .00 | 2338.44 | .76 | 3.80 | .05 | 2335.00 |
| 2152.0 | 932.7 | 950.2 | 269.1 | 268.4 | 98.4 | 58.1 | 31.0 | 15.6 | 2335.00 |
| .11 | 3.48 | 9.65 | 4.63 | .050 | .030 | .050 | .000 | 2334.00 | 695.41 |
| .008161 | 585. | 580. | 525. | 0 | 8 | 0 | .00 | 270.11 | 1047.64 |

FLOW DISTRIBUTION FOR SECNO= 2.92 CWSEL= 2337.68

| STA= | 695. | 737. | 759. | 790. | 814. | 838. | 855. | 985. | 989. | 1020. | 1027. | 1034. | 1041. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.6 | 3.6 | 6.8 | 8.9 | 8.9 | 3.4 | 4.6 | 2.4 | 44.2 | 4.2 | 3.8 | 3.4 | |
| AREA= | 37.4 | 25.9 | 43.4 | 46.2 | 46.2 | 22.9 | 35.5 | 10.9 | 98.4 | 18.0 | 16.8 | 15.9 | |
| VEL= | 2.6 | 3.0 | 3.4 | 4.2 | 4.2 | 3.2 | 2.8 | 4.8 | 9.7 | 5.0 | 4.8 | 4.6 | |
| DEPTH= | .9 | 1.2 | 1.4 | 1.9 | 1.9 | 1.3 | .3 | 2.4 | 3.2 | 2.6 | 2.4 | 2.3 | |

| STA= | 1041. | 1048. |
|---|---|---|
| PER Q= | 1.1 | |
| AREA= | 7.4 | |
| VEL= | 3.2 | |
| DEPTH= | 1.1 | |

SECNO 3.005

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.005 | 3.62 | 2344.12 | 2344.12 | .00 | 2344.78 | .66 | 3.08 | .01 | 2340.90 |
| 2152.0 | 264.7 | 1107.5 | 779.8 | 72.6 | 128.6 | 297.7 | 35.8 | 19.1 | 2340.90 |
| .13 | 3.65 | 8.61 | 2.62 | .050 | .030 | .050 | .000 | 2340.50 | 936.55 |
| .005885 | 425. | 440. | 490. | 0 | 5 | 0 | .00 | 390.48 | 1416.51 |

FLOW DISTRIBUTION FOR SECNO= 3.01 CWSEL= 2344.12

```
   ECNO     DEPTH    CWSEL    CRIWS    WSELK    EG       HV       HL       OLOSS    L-BANK ELEV
   Q        QLOB     QCH      QROB     ALOB     ACH      AROB     VOL      TWA      R-BANK ELEV
  TIME      VLOB     VCH      VROB     XNL      XNCH     XNR      WTN      ELMIN    SSTA
  SLOPE     XLOBL    XLCH     XLOBR    ITRIAL   IDC      ICONT    CORAR    TOPWID   ENDST


STA=     937.     967.     977.     983.    1021.    1028.    1035.    1110.    1160.    1190.    1313.    1330.    1367.
  PER Q=     3.5      4.2      4.5     51.5      5.1      4.3      3.7      4.2      3.8      4.7      4.0      3.0
   AREA=    29.4     22.9     20.3    128.6     22.4     20.4     30.7     43.5     33.6     51.3     27.6     31.3
    VEL=     2.6      4.0      4.8      8.6      4.9      4.5      2.6      2.1      2.5      2.0      3.1      2.1
  DEPTH=     1.0      2.3      3.1      3.4      3.2      2.8       .4       .9      1.1       .4      1.6       .8

STA=    1367.    1415.
  PER Q=     3.3
   AREA=    36.8
    VEL=     1.9
  DEPTH=      .8

*SECNO 3.047
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
    3.047     4.40  2347.40  2347.40      .00  2348.28      .88     1.56      .07  2344.00
   2152.0     40.7    914.3   1197.1     10.6     86.4    298.6     38.4     20.9  2344.00
      .14     3.84    10.58     4.01     .050     .030     .050     .000  2343.00   980.77
  .007194     205.     220.     265.        0       11        0      .00   227.57  1208.34


FLOW DISTRIBUTION FOR SECNO=      3.05          CWSEL=   2347.40

STA=     981.     987.    1009.    1013.    1019.    1026.    1044.    1058.    1079.    1099.    1120.    1170.    1208.
  PER Q=     1.9     42.5      3.4      4.0      3.7      9.3      8.3     12.5      6.8      3.1      3.9       .8
   AREA=    10.6     86.4     13.8     17.3     16.6     43.9     37.1     55.6     37.9     24.1     38.6     13.6
    VEL=     3.8     10.6      5.2      4.9      4.8      4.5      4.8      4.8      3.9      2.8      2.2      1.3
  DEPTH=     1.7      4.0      3.0      2.7      2.6      2.4      2.6      2.6      1.9      1.1       .8       .4

*SECNO 3.113

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      950.0    1100.0  TYPE=      1  TARGET=      150.000
          FLYING E TANK - NO DESIGN OR CONSTRUCTION INFORMATION AVAILABLE FOR
          LOW DAM FORMING TANK:  NOT DEPENDABLE FOR FLOOD RISK PLANNING.
          SECTION 3.200 IS CONTROL SECTION FOR PONDING IN TANK.
          MAP PROVIDES TWO WATER SURFACE ELEVATIONS.  TANK WSEL IS THE
```

EG ELEVATION AT THE CONTROL SECTION (2359.00 FT). CHANNEL WSELs
FROM NORMAL ANALYSIS WITH ENCROACHMENT AT 950 (THIS SECTION) TO
OMIT TANK FROM FLOW AREA.
ENTIRE INUNDATED AREA AND DAM INCLUDED IN AE ZONE.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.113 | 5.11 | 2352.61 | 2352.61 | .00 | 2354.39 | 1.78 | 2.41 | .27 | 2347.50 |
| 2152.0 | 623.3 | 1308.9 | 219.8 | 94.5 | 102.2 | 47.9 | 40.7 | 21.9 | 2347.50 |
| .15 | 6.59 | 12.80 | 4.59 | .050 | .030 | .050 | .000 | 2347.50 | 973.52 |
| .007588 | 370. | 350. | 270. | 0 | 8 | 0 | .00 | 72.76 | 1046.28 |

FLOW DISTRIBUTION FOR SECNO= 3.11 CWSEL= 2352.61

| STA= | 974. | 983. | 986. | 989. | 993. | 996. | 1000. | 1020. | 1023. | 1028. | 1042. | 1046. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.5 | 3.0 | 4.0 | 5.9 | 6.0 | 6.5 | 60.8 | 3.4 | 3.7 | 3.1 | .1 | |
| AREA= | 17.4 | 10.8 | 12.8 | 17.4 | 17.5 | 18.5 | 102.2 | 11.2 | 16.2 | 19.2 | 1.3 | |
| VEL= | 4.3 | 6.0 | 6.7 | 7.3 | 7.4 | 7.6 | 12.8 | 6.5 | 4.9 | 3.4 | 1.3 | |
| DEPTH= | 1.8 | 3.6 | 4.3 | 4.7 | 4.9 | 5.0 | 5.1 | 4.5 | 2.8 | 1.4 | .3 | |

*SECNO 3.200

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
FLYING E TANK OVERFLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.200 | 3.16 | 2358.16 | 2358.16 | .00 | 2359.00 | .84 | 3.84 | .09 | 2355.00 |
| 2152.0 | 443.1 | 948.6 | 760.3 | 104.4 | 94.9 | 181.5 | 44.1 | 23.7 | 2355.00 |
| .17 | 4.25 | 9.99 | 4.19 | .050 | .030 | .050 | .000 | 2355.00 | 924.58 |
| .008755 | 390. | 460. | 590. | 0 | 14 | 0 | .00 | 240.55 | 1165.13 |

FLOW DISTRIBUTION FOR SECNO= 3.20 CWSEL= 2358.16

| STA= | 925. | 975. | 1000. | 1030. | 1040. | 1060. | 1085. | 1100. | 1141. | 1165. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.5 | 15.1 | 44.1 | 7.7 | 11.2 | 9.5 | 3.5 | 3.1 | .3 | |
| AREA= | 41.5 | 62.9 | 94.9 | 29.1 | 48.3 | 47.9 | 21.2 | 29.1 | 5.8 | |
| VEL= | 2.8 | 5.2 | 10.0 | 5.7 | 5.0 | 4.3 | 3.5 | 2.3 | 1.1 | |
| DEPTH= | .8 | 2.5 | 3.2 | 2.9 | 2.4 | 1.9 | 1.4 | .7 | .2 | |

*SECNO 3.261

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.58

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.261 | 3.85 | 2360.35 | 2359.61 | .00 | 2360.68 | .33 | 1.63 | .05 | 2358.00 |
| 2152.0 | 1250.0 | 721.5 | 180.5 | 390.4 | 109.0 | 81.9 | 47.5 | 25.5 | 2358.00 |
| .19 | 3.20 | 6.62 | 2.20 | .050 | .030 | .050 | .000 | 2356.50 | 815.50 |
| .003524 | 330. | 320. | 250. | 2 | 5 | 0 | .00 | 274.33 | 1089.83 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 3.26 CWSEL= 2360.35

| STA= | 816. | 851. | 860. | 875. | 890. | 903. | 918. | 932. | 958. | 980. | 990. | 1022. | 1037. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 8.1 | 5.5 | 7.0 | 7.0 | 8.0 | 7.0 | 3.9 | 4.7 | 3.9 | 2.8 | 33.5 | 3.6 | |
| AREA= | 61.4 | 30.1 | 42.7 | 42.7 | 43.5 | 42.7 | 29.4 | 41.6 | 35.2 | 21.0 | 109.0 | 28.3 | |
| VEL= | 2.8 | 3.9 | 3.5 | 3.5 | 3.9 | 3.5 | 2.9 | 2.4 | 2.4 | 2.9 | 6.6 | 2.7 | |
| DEPTH= | 1.7 | 3.3 | 2.8 | 2.8 | 3.3 | 2.8 | 2.1 | 1.6 | 1.6 | 2.1 | 3.4 | 1.9 | |

| STA= | 1037. | 1071. | 1090. |
|---|---|---|---|
| PER Q= | 4.2 | .6 | |
| AREA= | 43.2 | 10.5 | |
| VEL= | 2.1 | 1.2 | |
| DEPTH= | 1.3 | .6 | |

*SECNO 3.308
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.308 | 3.14 | 2362.14 | 2362.14 | .00 | 2362.83 | .69 | 1.33 | .11 | 2359.30 |
| 2152.0 | 1230.7 | 795.8 | 125.5 | 327.3 | 81.9 | 26.6 | 50.4 | 27.2 | 2359.30 |
| .20 | 3.76 | 9.71 | 4.71 | .050 | .030 | .050 | .000 | 2359.00 | 720.37 |
| 08882 | 250. | 250. | 250. | 0 | 15 | 0 | .00 | 302.21 | 1022.58 |

FLOW DISTRIBUTION FOR SECNO= 3.31 CWSEL= 2362.14

| STA= | 720. | 762. | 783. | 830. | 890. | 916. | 929. | 939. | 950. | 957. | 963. | 970. | 977. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 9.6 | 4.7 | 4.5 | 3.7 | 3.3 | 3.2 | 3.5 | 4.6 | 3.8 | 4.4 | 4.6 | 4.9 | |
| AREA= | 56.2 | 29.2 | 38.8 | 38.4 | 25.2 | 18.9 | 18.3 | 21.5 | 16.6 | 17.8 | 18.2 | 18.9 | |
| VEL= | 3.7 | 3.5 | 2.5 | 2.1 | 2.8 | 3.6 | 4.1 | 4.6 | 5.0 | 5.3 | 5.4 | 5.6 | |
| DEPTH= | 1.4 | 1.4 | .8 | .6 | 1.0 | 1.5 | 1.8 | 2.1 | 2.4 | 2.6 | 2.7 | 2.8 | |

| STA= | 977. | 980. | 1007. | 1015. | 1023. |
|---|---|---|---|---|---|
| PER Q= | 2.4 | 37.0 | 4.8 | 1.0 | |
| AREA= | 9.4 | 81.9 | 19.7 | 6.9 | |
| VEL= | 5.6 | 9.7 | 5.2 | 3.2 | |
| DEPTH= | 2.8 | 3.0 | 2.6 | .9 | |

*SECNO 3.355

3265 DIVIDED FLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
CONFLUENCE OF UPPER FLYING E WASH AND HOLLY WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.355 | 3.20 | 2365.70 | 2365.70 | .00 | 2366.26 | .56 | 2.09 | .01 | 2362.80 |
| 2152.0 | 1147.2 | 666.7 | 338.1 | 351.2 | 70.7 | 80.0 | 53.1 | 29.1 | 2362.80 |
| .21 | 3.27 | 9.43 | 4.23 | .050 | .030 | .050 | .000 | 2362.50 | 648.69 |
| .008263 | 240. | 250. | 245. | 0 | 5 | 0 | .00 | 392.98 | 1062.19 |

FLOW DISTRIBUTION FOR SECNO= 3.36 CWSEL= 2365.70

| STA= | 649. | 690. | 710. | 728. | 738. | 747. | 760. | 800. | 835. | 890. | 970. | 980. | 987. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 8.2 | 4.7 | 4.2 | 3.8 | 3.4 | 3.0 | 3.7 | 4.1 | 3.9 | 3.1 | 4.0 | 4.7 | |
| AREA= | 52.3 | 29.1 | 26.2 | 19.5 | 17.6 | 18.9 | 33.2 | 33.4 | 38.8 | 33.8 | 20.1 | 18.8 | |
| VEL= | 3.4 | 3.5 | 3.5 | 4.2 | 4.2 | 3.5 | 2.4 | 2.6 | 2.1 | 2.0 | 4.3 | 5.4 | |
| DEPTH= | 1.3 | 1.5 | 1.5 | 2.0 | 2.0 | 1.5 | .8 | 1.0 | .7 | .4 | 2.0 | 2.8 | |

| STA= | 987. | 990. | 1013. | 1020. | 1026. | 1036. | 1050. | 1062. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 2.4 | 31.0 | 4.7 | 3.5 | 3.0 | 3.6 | .9 | |
| AREA= | 9.6 | 70.7 | 18.8 | 15.2 | 16.4 | 21.5 | 8.1 | |
| VEL= | 5.5 | 9.4 | 5.4 | 5.0 | 4.0 | 3.6 | 2.4 | |
| DEPTH= | 2.9 | 3.0 | 2.8 | 2.5 | 1.7 | 1.5 | .7 | |

*SECNO 3.454

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
UPPER FLYING E WASH/HOLLY WASH CONFLUENCE
HYDRAULIC CONTROL LINE IS AT STATION 1000.0

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.454 | 3.28 | 2371.78 | 2371.78 | .00 | 2372.24 | .46 | 5.74 | .01 | 2370.50 |
| 2152.0 | 1325.9 | 173.7 | 652.4 | 304.0 | 21.8 | 99.9 | 58.1 | 33.5 | 2370.50 |
| .24 | 4.36 | 7.97 | 6.53 | .050 | .030 | .050 | .000 | 2368.50 | 626.23 |
| .018591 | 450. | 520. | 530. | 0 | 5 | 0 | .00 | 430.55 | 1222.47 |

FLOW DISTRIBUTION FOR SECNO= 3.45 CWSEL= 2371.78

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 626. | 660. | 680. | 691. | 704. | 730. | 788. | 823. | 840. | 856. | 896. | 979. | 996. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.3 | 7.7 | 6.7 | 8.0 | 7.4 | 3.4 | 4.9 | 4.1 | 3.7 | 4.5 | 3.2 | 3.8 | |
| AREA= | 21.0 | 30.6 | 22.4 | 26.4 | 33.3 | 25.9 | 29.1 | 19.8 | 18.1 | 29.0 | 24.8 | 19.2 | |
| VEL= | 3.4 | 5.4 | 6.5 | 6.5 | 4.8 | 2.8 | 3.6 | 4.4 | 4.4 | 3.3 | 2.8 | 4.3 | |
| DEPTH= | .6 | 1.5 | 2.0 | 2.0 | 1.3 | .5 | .8 | 1.1 | 1.1 | .7 | .3 | 1.1 | |

| STA= | 996. | 1000. | 1017. | 1191. | 1198. | 1201. | 1204. | 1207. | 1210. | 1215. | 1222. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 1.0 | 8.1 | 3.5 | 5.0 | 3.3 | 3.6 | 3.9 | 3.1 | 5.4 | 2.6 | |
| AREA= | 4.4 | 21.8 | 24.2 | 15.7 | 8.6 | 9.1 | 9.5 | 7.8 | 14.8 | 10.1 | |
| VEL= | 4.7 | 8.0 | 3.1 | 6.8 | 8.2 | 8.5 | 8.8 | 8.6 | 7.8 | 5.5 | |
| DEPTH= | 1.2 | 1.3 | .1 | 2.2 | 2.9 | 3.0 | 3.2 | 3.1 | 2.7 | 1.4 | |

*SECNO 3.549

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .55

UPPER FLYING E WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.549 | 2.04 | 2380.04 | 2379.87 | .00 | 2380.26 | .22 | 7.99 | .02 | 2378.80 |
| 896.0 | 389.7 | 140.5 | 365.8 | 125.6 | 21.8 | 127.1 | 62.2 | 38.1 | 2378.80 |
| .28 | 3.10 | 6.44 | 2.88 | .050 | .030 | .050 | .000 | 2378.00 | 804.32 |
| 10750 | 525. | 500. | 500. | 4 | 14 | 0 | .00 | 350.86 | 1155.18 |

FLOW DISTRIBUTION FOR SECNO= 3.55 CWSEL= 2380.04

| STA= | 804. | 826. | 831. | 836. | 840. | 845. | 875. | 900. | 925. | 980. | 990. | 1006. | 1017. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 6.2 | 4.9 | 5.1 | 5.1 | 4.1 | 3.5 | 3.1 | 3.1 | 4.1 | 4.3 | 15.7 | 3.9 | |
| AREA= | 17.5 | 9.6 | 9.2 | 9.2 | 8.5 | 14.2 | 13.5 | 13.5 | 19.0 | 11.4 | 21.8 | 11.2 | |
| VEL= | 3.2 | 4.6 | 5.0 | 5.0 | 4.3 | 2.2 | 2.0 | 2.0 | 1.9 | 3.4 | 6.4 | 3.1 | |
| DEPTH= | .8 | 1.8 | 2.0 | 2.0 | 1.7 | .5 | .5 | .5 | .3 | 1.1 | 1.4 | 1.0 | |

| STA= | 1017. | 1043. | 1059. | 1077. | 1095. | 1113. | 1130. | 1155. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.6 | 4.1 | 6.6 | 6.6 | 6.4 | 6.4 | 3.1 | |
| AREA= | 15.3 | 13.2 | 18.7 | 18.7 | 18.2 | 18.2 | 13.5 | |
| VEL= | 2.1 | 2.8 | 3.2 | 3.2 | 3.2 | 3.2 | 2.0 | |
| DEPTH= | .6 | .8 | 1.0 | 1.0 | 1.0 | 1.0 | .5 | |

*SECNO 3.643

3265 DIVIDED FLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.643 | 2.54 | 2387.54 | 2387.54 | .00 | 2388.00 | .46 | 4.50 | .07 | 2385.50 |
| 896.0 | 426.1 | 375.7 | 94.3 | 157.5 | 48.3 | 32.6 | 65.2 | 41.7 | 2385.50 |
| .30 | 2.71 | 7.77 | 2.89 | .050 | .030 | .050 | .000 | 2385.00 | 719.31 |
| .007619 | 505. | 500. | 495. | 0 | 11 | 0 | .00 | 263.89 | 1051.29 |

FLOW DISTRIBUTION FOR SECNO= 3.64 CWSEL= 2387.54

| STA= | 719. | 795. | 800. | 805. | 810. | 816. | 828. | 895. | 912. | 924. | 935. | 945. | 995. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.2 | 3.3 | 4.2 | 3.8 | 3.0 | 3.2 | 4.1 | 3.1 | 4.0 | 5.9 | 3.2 | 5.6 | |
| AREA= | 17.9 | 8.2 | 9.5 | 9.0 | 8.3 | 11.3 | 24.8 | 12.7 | 12.8 | 16.1 | 10.4 | 16.4 | |
| VEL= | 2.1 | 3.6 | 4.0 | 3.8 | 3.2 | 2.5 | 1.5 | 2.2 | 2.8 | 3.3 | 2.7 | 3.1 | |
| DEPTH= | .2 | 1.6 | 1.9 | 1.8 | 1.4 | .9 | .4 | .7 | 1.1 | 1.4 | 1.0 | .3 | |

| STA= | 995. | 1015. | 1020. | 1031. | 1051. |
|---|---|---|---|---|---|
| PER Q= | 41.9 | 3.8 | 4.8 | 1.9 | |
| AREA= | 48.3 | 9.0 | 14.2 | 9.5 | |
| VEL= | 7.8 | 3.8 | 3.0 | 1.8 | |
| DEPTH= | 2.4 | 1.8 | 1.2 | .5 | |

*SECNO 3.740

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.740 | 2.56 | 2395.56 | 2395.56 | .00 | 2395.98 | .42 | 3.91 | .00 | 2393.50 |
| 896.0 | 461.4 | 350.2 | 84.4 | 185.7 | 46.0 | 23.6 | 68.0 | 44.7 | 2393.50 |
| .34 | 2.48 | 7.61 | 3.58 | .050 | .030 | .050 | .000 | 2393.00 | 746.92 |
| .007781 | 505. | 510. | 510. | 0 | 5 | 0 | .00 | 258.55 | 1027.08 |

FLOW DISTRIBUTION FOR SECNO= 3.74 CWSEL= 2395.56

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 747. | 794. | 818. | 841. | 861. | 880. | 900. | 918. | 937. | 983. | 990. | 1010. | 1015. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.4 | 4.9 | 6.4 | 6.4 | 6.4 | 6.4 | 5.0 | 3.8 | 3.1 | 4.8 | 39.1 | 4.4 | |
| AREA= | 22.7 | 19.0 | 22.5 | 21.0 | 20.8 | 21.0 | 17.6 | 15.0 | 14.4 | 11.7 | 46.0 | 9.7 | |
| VEL= | 1.7 | 2.3 | 2.6 | 2.7 | 2.7 | 2.7 | 2.6 | 2.3 | 1.9 | 3.6 | 7.6 | 4.1 | |
| DEPTH= | .5 | .8 | 1.0 | 1.1 | 1.1 | 1.1 | 1.0 | .8 | .3 | 1.6 | 2.3 | 1.9 | |

| STA= | 1015. | 1020. | 1027. |
|---|---|---|---|
| PER Q= | 3.4 | 1.6 | |
| AREA= | 8.3 | 5.5 | |
| VEL= | 3.7 | 2.6 | |
| DEPTH= | 1.7 | .8 | |

*SECNO 3.838

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.838 | 2.24 | 2404.74 | 2404.74 | .00 | 2405.08 | .34 | 4.29 | .01 | 2403.00 |
| 896.0 | 575.8 | 290.3 | 29.9 | 222.4 | 39.8 | 10.1 | 71.2 | 48.4 | 2403.00 |
| .37 | 2.59 | 7.29 | 2.97 | .050 | .030 | .050 | .000 | 2402.50 | 638.53 |
| .008676 | 525. | 520. | 515. | 0 | 10 | 0 | .00 | 352.43 | 1021.60 |

FLOW DISTRIBUTION FOR SECNO= 3.84 CWSEL= 2404.74

| STA= | 639. | 660. | 687. | 702. | 718. | 734. | 750. | 773. | 810. | 904. | 940. | 988. | 990. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.1 | 16.2 | 4.6 | 3.7 | 4.9 | 6.1 | 7.0 | 3.3 | 3.1 | 5.8 | 3.1 | 1.5 | |
| AREA= | 16.6 | 40.2 | 14.8 | 13.4 | 15.8 | 18.2 | 22.8 | 17.2 | 24.2 | 24.2 | 11.2 | 3.5 | |
| VEL= | 2.7 | 3.6 | 2.7 | 2.5 | 2.7 | 3.0 | 2.7 | 1.7 | 1.1 | 2.1 | 2.5 | 3.7 | |
| DEPTH= | .8 | 1.5 | 1.0 | .8 | 1.0 | 1.1 | 1.0 | .5 | .3 | .7 | .2 | 1.6 | |

| STA= | 990. | 1010. | 1018. | 1022. |
|---|---|---|---|---|
| PER Q= | 32.4 | 3.2 | .1 | |
| AREA= | 39.8 | 9.1 | 1.0 | |
| VEL= | 7.3 | 3.1 | 1.3 | |
| DEPTH= | 2.0 | 1.1 | .3 | |

*SECNO 3.950

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.950 | 3.58 | 2415.08 | 2415.08 | .00 | 2415.94 | .86 | 5.01 | .16 | 2412.00 |
| 896.0 | 33.3 | 428.1 | 434.5 | 8.9 | 43.2 | 107.2 | 74.2 | 51.4 | 2412.00 |
| .39 | 3.75 | 9.92 | 4.05 | .050 | .030 | .050 | .000 | 2411.50 | 989.23 |
| .008139 | 600. | 590. | 600. | 0 | 14 | 0 | .00 | 92.23 | 1081.46 |

FLOW DISTRIBUTION FOR SECNO= 3.95 CWSEL= 2415.08

| STA= | 989. | 995. | 1008. | 1011. | 1014. | 1017. | 1021. | 1024. | 1027. | 1030. | 1037. | 1046. | 1057. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 47.8 | 5.9 | 5.6 | 4.9 | 4.6 | 4.1 | 3.8 | 3.3 | 5.1 | 3.4 | 3.9 | |
| AREA= | 8.9 | 43.2 | 9.4 | 9.2 | 8.5 | 8.3 | 7.5 | 7.3 | 6.6 | 11.7 | 10.3 | 12.4 | |
| VEL= | 3.8 | 9.9 | 5.6 | 5.4 | 5.2 | 5.0 | 4.8 | 4.6 | 4.4 | 3.9 | 2.9 | 2.8 | |
| DEPTH= | 1.5 | 3.3 | 3.0 | 2.9 | 2.7 | 2.6 | 2.4 | 2.3 | 2.1 | 1.8 | 1.1 | 1.1 | |

| STA= | 1057. | 1080. | 1081. |
|---|---|---|---|
| PER Q= | 4.0 | .0 | |
| AREA= | 16.0 | .1 | |
| VEL= | 2.2 | .0 | |
| DEPTH= | .7 | .0 | |

*SECNO 3.980
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.980 | 4.17 | 2417.67 | 2417.67 | .00 | 2418.65 | .97 | 1.15 | .03 | 2415.00 |
| 896.0 | 39.1 | 654.1 | 202.8 | 11.7 | 72.2 | 63.7 | 74.7 | 51.7 | 2415.00 |
| .40 | 3.34 | 9.06 | 3.18 | .050 | .030 | .050 | .000 | 2413.50 | 983.07 |
| .006653 | 160. | 160. | 150. | 0 | 11 | 0 | .00 | 82.72 | 1065.80 |

FLOW DISTRIBUTION FOR SECNO= 3.98 CWSEL= 2417.67

| STA= | 983. | 992. | 1013. | 1016. | 1021. | 1027. | 1033. | 1043. | 1058. | 1066. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.4 | 73.0 | 3.5 | 5.3 | 3.8 | 3.2 | 3.5 | 3.1 | .2 | |
| AREA= | 11.7 | 72.2 | 7.1 | 11.8 | 9.8 | 9.1 | 11.4 | 12.7 | 1.8 | |
| VEL= | 3.3 | 9.1 | 4.5 | 4.0 | 3.4 | 3.1 | 2.8 | 2.2 | 1.1 | |
| DEPTH= | 1.3 | 3.4 | 2.5 | 2.1 | 1.7 | 1.5 | 1.2 | .8 | .2 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 4.032
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.032 | 3.59 | 2422.59 | 2422.59 | .00 | 2423.51 | .91 | 1.87 | .01 | 2419.50 |
| 896.0 | 196.0 | 509.1 | 190.8 | 55.3 | 53.4 | 42.0 | 75.6 | 52.3 | 2419.50 |
| .41 | 3.55 | 9.54 | 4.55 | .050 | .030 | .050 | .000 | 2419.00 | 934.21 |
| .007464 | 290. | 270. | 235. | 0 | 15 | 0 | .00 | 97.30 | 1031.51 |

FLOW DISTRIBUTION FOR SECNO= 4.03 CWSEL= 2422.59

| STA= | 934. | 979. | 986. | 990. | 993. | 995. | 1011. | 1014. | 1017. | 1020. | 1023. | 1032. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 5.5 | 4.4 | 3.7 | 4.3 | 56.8 | 5.3 | 4.9 | 4.5 | 3.6 | 3.0 | |
| AREA= | 19.7 | 12.9 | 8.6 | 6.7 | 7.4 | 53.4 | 9.0 | 8.5 | 8.1 | 7.4 | 9.0 | |
| VEL= | 1.8 | 3.8 | 4.6 | 5.0 | 5.2 | 9.5 | 5.3 | 5.2 | 5.0 | 4.3 | 3.0 | |
| DEPTH= | .4 | 1.8 | 2.4 | 2.7 | 2.9 | 3.3 | 3.0 | 2.8 | 2.7 | 2.2 | 1.1 | |

*SECNO 4.103
7185 MINIMUM SPECIFIC ENERGY
[illegible] CRITICAL DEPTH ASSUMED
DOWNSTREAM OF GEORGE'S TANK DAM EMBANKMENT

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.103 | 2.37 | 2428.37 | 2428.37 | .00 | 2428.94 | .57 | 3.25 | .03 | 2426.30 |
| 896.0 | 270.5 | 375.6 | 249.9 | 79.8 | 44.4 | 73.9 | 77.1 | 53.3 | 2426.30 |
| .43 | 3.39 | 8.46 | 3.38 | .050 | .030 | .050 | .000 | 2426.00 | 922.23 |
| .010078 | 355. | 375. | 405. | 0 | 14 | 0 | .00 | 151.47 | 1073.70 |

FLOW DISTRIBUTION FOR SECNO= 4.10 CWSEL= 2428.37

| STA= | 922. | 925. | 990. | 1010. | 1070. | 1074. |
|---|---|---|---|---|---|---|
| PER Q= | .1 | 30.1 | 41.9 | 27.8 | .1 | |
| AREA= | .5 | 79.3 | 44.4 | 73.2 | .7 | |
| VEL= | 1.0 | 3.4 | 8.5 | 3.4 | 1.0 | |
| DEPTH= | .2 | 1.2 | 2.2 | 1.2 | .2 | |

*SECNO 4.168
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
UPSTREAM OF GEORGE'S TANK DAM EMBANKMENT
GEORGE'S TANK - NO DESIGN OR CONSTRUCTION DATA AVAILABLE FOR
DAM FORMING TANK: NOT DEPENDABLE FOR FLOOD RISK PLANNING.

EXCESS FLOWS BREAK INTO SMALL CHANNEL ALONG WEST EDGE OF TANK OVER
A WIDE, FLAT SADDLE. SMALL CHANNEL ANALYZED AND SUBMITTED SEPARATELY
AS A ZONE A UNDER THE TITLE "GEORGE'S TANK BREAKOUT".

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.168 | 1.94 | 2434.34 | 2434.34 | .00 | 2434.82 | .48 | 3.85 | .01 | 2432.50 |
| 896.0 | 421.2 | 305.0 | 169.8 | 120.6 | 36.8 | 51.9 | 78.7 | 54.7 | 2432.70 |
| .45 | 3.49 | 8.29 | 3.27 | .050 | .030 | .050 | .000 | 2432.40 | 875.75 |
| .012421 | 345. | 345. | 345. | 0 | 15 | 0 | .00 | 188.97 | 1064.72 |

FLOW DISTRIBUTION FOR SECNO= 4.17 CWSEL= 2434.34

| STA= | 876. | 880. | 990. | 1010. | 1062. | 1065. |
|---|---|---|---|---|---|---|
| PER Q= | .1 | 46.9 | 34.0 | 18.9 | .1 | |
| AREA= | .7 | 119.9 | 36.8 | 51.5 | .5 | |
| VEL= | 1.0 | 3.5 | 8.3 | 3.3 | 1.0 | |
| DEPTH= | .2 | 1.1 | 1.8 | 1.0 | .2 | |

*SECNO 4.213

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.53

LOWER PORTION OF GEORGE'S TANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.213 | 4.11 | 2435.61 | 2434.73 | .00 | 2435.82 | .20 | .97 | .03 | 2432.00 |
| 896.0 | 371.5 | 311.1 | 213.4 | 180.2 | 58.0 | 91.5 | 80.3 | 55.7 | 2432.00 |
| .47 | 2.06 | 5.37 | 2.33 | .050 | .030 | .050 | .000 | 2431.50 | 888.16 |
| .001942 | 270. | 235. | 195. | 4 | 14 | 0 | .00 | 167.98 | 1056.14 |

FLOW DISTRIBUTION FOR SECNO= 4.21 CWSEL= 2435.61

| STA= | 888. | 894. | 907. | 920. | 935. | 955. | 970. | 983. | 995. | 1010. | 1025. | 1040. | 1056. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .0 | .8 | 2.8 | 6.2 | 8.3 | 4.9 | 6.4 | 12.1 | 34.7 | 14.5 | 7.6 | 1.6 | |
| AREA= | .9 | 8.0 | 16.4 | 28.0 | 37.3 | 24.2 | 26.4 | 38.9 | 58.0 | 46.7 | 31.7 | 13.0 | |
| VEL= | .4 | .9 | 1.5 | 2.0 | 2.0 | 1.8 | 2.2 | 2.8 | 5.4 | 2.8 | 2.2 | 1.1 | |
| DEPTH= | .2 | .6 | 1.3 | 1.9 | 1.9 | 1.6 | 2.1 | 3.1 | 3.9 | 3.1 | 2.1 | .8 | |

*SECNO 4.301
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

UPPER PORTION OF GEORGE'S TANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.301 | 1.87 | 2442.87 | 2442.87 | .00 | 2443.41 | .54 | 1.91 | .10 | 2441.20 |
| 896.0 | 357.2 | 302.0 | 236.8 | 90.8 | 35.4 | 61.6 | 83.0 | 57.5 | 2441.20 |
| .49 | 3.93 | 8.53 | 3.84 | .050 | .030 | .050 | .000 | 2441.00 | 900.30 |
| .013832 | 465. | 465. | 465. | 0 | 14 | 0 | .00 | 171.03 | 1071.34 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 4.30 CWSEL= 2442.87

| STA= | 900. | 906. | 926. | 945. | 963. | 982. | 989. | 1009. | 1025. | 1050. | 1071. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .0 | 2.6 | 6.9 | 10.1 | 13.7 | 6.5 | 33.7 | 12.6 | 11.8 | 2.1 | |
| AREA= | .5 | 10.4 | 18.0 | 22.6 | 27.2 | 12.2 | 35.4 | 24.3 | 28.0 | 9.3 | |
| VEL= | .7 | 2.3 | 3.4 | 4.0 | 4.5 | 4.8 | 8.5 | 4.6 | 3.8 | 2.0 | |
| DEPTH= | .1 | .5 | 1.0 | 1.2 | 1.5 | 1.6 | 1.8 | 1.5 | 1.1 | .4 | |

*SECNO 4.384
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.384 | 2.49 | 2449.49 | 2449.49 | .00 | 2450.24 | .75 | 5.20 | .06 | 2447.30 |
| 896.0 | 279.6 | 426.6 | 189.8 | 68.3 | 46.8 | 45.6 | 84.7 | 58.8 | 2447.30 |
| .51 | 4.10 | 9.11 | 4.17 | .050 | .030 | .050 | .000 | 2447.00 | 935.37 |
| .010886 | 405. | 440. | 430. | 0 | 11 | 0 | .00 | 105.80 | 1041.17 |

FLOW DISTRIBUTION FOR SECNO= 4.38 CWSEL= 2449.49

| STA= | 935. | 942. | 963. | 982. | 988. | 1008. | 1027. | 1041. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | .2 | 7.2 | 16.1 | 7.7 | 47.6 | 18.2 | 3.0 | |
| AREA= | 1.6 | 20.8 | 32.2 | 13.6 | 46.8 | 35.0 | 10.6 | |
| VEL= | 1.2 | 3.1 | 4.5 | 5.1 | 9.1 | 4.7 | 2.5 | |
| DEPTH= | .2 | 1.0 | 1.7 | 2.1 | 2.3 | 1.8 | .7 | |

*SECNO 4.493
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.493 | 1.64 | 2458.64 | 2458.64 | .00 | 2459.00 | .35 | 6.99 | .04 | 2457.40 |
| 896.0 | 81.3 | 230.1 | 584.6 | 27.5 | 29.8 | 185.0 | 87.3 | 61.6 | 2457.10 |
| .55 | 2.96 | 7.72 | 3.16 | .050 | .030 | .050 | .000 | 2457.00 | 941.83 |
| .014251 | 465. | 575. | 600. | 0 | 23 | 0 | .00 | 324.01 | 1265.84 |

FLOW DISTRIBUTION FOR SECNO= 4.49 CWSEL= 2458.64

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 942. | 977. | 986. | 1006. | 1022. | 1045. | 1067. | 1089. | 1109. | 1129. | 1150. | 1170. | 1190. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.7 | 4.4 | 25.7 | 11.8 | 12.7 | 8.7 | 5.4 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | |
| AREA= | 17.1 | 10.4 | 29.8 | 23.3 | 27.6 | 22.2 | 16.5 | 13.0 | 13.0 | 13.0 | 13.0 | 13.0 | |
| VEL= | 2.5 | 3.8 | 7.7 | 4.5 | 4.1 | 3.5 | 2.9 | 2.6 | 2.6 | 2.6 | 2.6 | 2.6 | |
| DEPTH= | .5 | 1.1 | 1.5 | 1.4 | 1.2 | 1.0 | .7 | .6 | .6 | .6 | .6 | .6 | |

| STA= | 1190. | 1210. | 1255. | 1266. |
|---|---|---|---|---|
| PER Q= | 3.8 | 3.6 | .1 | |
| AREA= | 13.0 | 16.6 | .8 | |
| VEL= | 2.6 | 1.9 | .6 | |
| DEPTH= | .6 | .4 | .1 | |

*SECNO 4.594

3265 DIVIDED FLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.594 | 1.37 | 2467.37 | 2467.34 | .00 | 2467.71 | .34 | 8.71 | .00 | 2466.50 |
| 896.0 | 352.1 | 167.4 | 376.6 | 93.4 | 22.7 | 99.9 | 90.1 | 65.4 | 2466.50 |
| .58 | 3.77 | 7.37 | 3.77 | .050 | .030 | .050 | .000 | 2466.00 | 796.57 |
| .019356 | 520. | 530. | 530. | 3 | 15 | 0 | .00 | 300.11 | 1337.12 |

FLOW DISTRIBUTION FOR SECNO= 4.59 CWSEL= 2467.37

| STA= | 797. | 836. | 860. | 885. | 910. | 992. | 1013. | 1038. | 1190. | 1211. | 1228. | 1320. | 1337. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.2 | 9.0 | 15.9 | 9.0 | 1.2 | 18.7 | 3.3 | 6.8 | 16.4 | 6.2 | 5.2 | 4.2 | |
| AREA= | 15.5 | 21.4 | 30.1 | 21.3 | 5.1 | 22.7 | 11.3 | 18.1 | 28.8 | 14.8 | 15.2 | 11.7 | |
| VEL= | 2.4 | 3.8 | 4.7 | 3.8 | 2.2 | 7.4 | 2.6 | 3.3 | 5.1 | 3.8 | 3.1 | 3.2 | |
| DEPTH= | .4 | .9 | 1.2 | .9 | .1 | 1.1 | .4 | .1 | 1.4 | .9 | .2 | .7 | |

*SECNO 4.688
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.688 | 2.61 | 2475.61 | 2475.61 | .00 | 2476.06 | .45 | 6.70 | .03 | 2473.90 |
| 896.0 | 576.4 | 299.3 | 20.3 | 181.1 | 36.7 | 7.4 | 92.5 | 68.2 | 2473.90 |
| .61 | 3.18 | 8.15 | 2.73 | .050 | .030 | .050 | .000 | 2473.00 | 791.75 |
| .010707 | 440. | 500. | 530. | 0 | 17 | 0 | .00 | 221.26 | 1013.00 |

FLOW DISTRIBUTION FOR SECNO= 4.69 CWSEL= 2475.61

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 792. | 810. | 833. | 855. | 879. | 902. | 926. | 949. | 979. | 986. | 1004. | 1013. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .9 | 6.0 | 12.9 | 13.4 | 6.3 | 3.5 | 3.5 | 12.2 | 5.7 | 33.4 | 2.3 | |
| AREA= | 5.6 | 19.3 | 30.6 | 31.9 | 20.2 | 14.3 | 14.3 | 33.3 | 11.8 | 36.7 | 7.4 | |
| VEL= | 1.4 | 2.8 | 3.8 | 3.8 | 2.8 | 2.2 | 2.2 | 3.3 | 4.3 | 8.1 | 2.7 | |
| DEPTH= | .3 | .9 | 1.4 | 1.4 | .9 | .6 | .6 | 1.1 | 1.7 | 2.0 | .9 | |

*SECNO 4.787

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.787 | 2.24 | 2484.24 | 2484.24 | .00 | 2484.60 | .36 | 5.59 | .01 | 2482.70 |
| 896.0 | 545.9 | 293.2 | 56.8 | 199.7 | 39.6 | 19.6 | 95.6 | 71.7 | 2482.70 |
| .64 | 2.73 | 7.41 | 2.90 | .050 | .030 | .050 | .000 | 2482.00 | 637.90 |
| .009465 | 580. | 520. | 470. | 0 | 10 | 0 | .00 | 310.84 | 1035.56 |

FLOW DISTRIBUTION FOR SECNO= 4.79 CWSEL= 2484.24

| | 638. | 700. | 725. | 750. | 778. | 890. | 915. | 985. | 990. | 1011. | 1021. | 1036. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 10.4 | 11.5 | 11.5 | 8.7 | 7.9 | 4.9 | 3.3 | 2.8 | 32.7 | 4.9 | 1.4 | |
| AREA= | 38.3 | 30.9 | 30.9 | 27.2 | 34.2 | 18.4 | 12.8 | 6.9 | 39.6 | 13.1 | 6.5 | |
| VEL= | 2.4 | 3.3 | 3.3 | 2.9 | 2.1 | 2.4 | 2.3 | 3.6 | 7.4 | 3.4 | 2.0 | |
| DEPTH= | .6 | 1.2 | 1.2 | 1.0 | .3 | .7 | .2 | 1.4 | 1.9 | 1.2 | .5 | |

*SECNO 4.881

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.881 | 2.54 | 2489.54 | 2489.54 | .00 | 2490.12 | .58 | 4.86 | .07 | 2487.70 |
| 896.0 | 65.9 | 372.7 | 457.4 | 17.9 | 43.5 | 134.2 | 98.1 | 74.3 | 2487.70 |
| .67 | 3.69 | 8.57 | 3.41 | .050 | .030 | .050 | .000 | 2487.00 | 971.98 |
| .010462 | 470. | 500. | 495. | 0 | 8 | 0 | .00 | 160.79 | 1346.20 |

FLOW DISTRIBUTION FOR SECNO= 4.88 CWSEL= 2489.54

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 972. | 988. | 1008. | 1017. | 1100. | 1120. | 1135. | 1300. | 1325. | 1346. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.4 | 41.6 | 4.4 | 3.4 | 14.0 | 3.4 | 3.8 | 17.4 | 4.7 | |
| AREA= | 17.9 | 43.5 | 11.2 | 12.0 | 30.8 | 11.9 | 13.4 | 38.5 | 16.3 | |
| VEL= | 3.7 | 8.6 | 3.5 | 2.5 | 4.1 | 2.5 | 2.5 | 4.1 | 2.6 | |
| DEPTH= | 1.1 | 2.2 | 1.2 | .1 | 1.5 | .8 | .1 | 1.5 | .8 | |

*SECNO 5.014
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.014 | 3.01 | 2500.01 | 2500.01 | .00 | 2500.71 | .70 | 6.72 | .04 | 2497.50 |
| 896.0 | 165.3 | 463.7 | 267.1 | 42.4 | 53.3 | 83.1 | 101.4 | 76.9 | 2497.50 |
| .70 | 3.90 | 8.71 | 3.21 | .050 | .030 | .050 | .000 | 2497.00 | 959.98 |
| .008108 | 485. | 700. | 850. | 0 | 11 | 0 | .00 | 130.11 | 1090.09 |

FLOW DISTRIBUTION FOR SECNO= 5.01 CWSEL= 2500.01

| STA= | 960. | 975. | 980. | 985. | 990. | 1010. | 1014. | 1019. | 1025. | 1035. | 1045. | 1055. | 1070. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.3 | 3.8 | 5.2 | 6.2 | 51.7 | 6.0 | 4.9 | 4.2 | 3.9 | 3.0 | 3.0 | 3.7 | |
| AREA= | 11.3 | 8.8 | 10.5 | 11.8 | 53.3 | 11.3 | 9.9 | 9.7 | 11.9 | 10.1 | 10.1 | 13.3 | |
| VEL= | 2.6 | 3.9 | 4.4 | 4.7 | 8.7 | 4.7 | 4.4 | 3.9 | 2.9 | 2.7 | 2.7 | 2.5 | |
| DEPTH= | .8 | 1.8 | 2.1 | 2.4 | 2.7 | 2.4 | 2.1 | 1.8 | 1.1 | 1.0 | 1.0 | .9 | |

| STA= | 1070. | 1090. |
|---|---|---|
| PER Q= | 1.2 | |
| AREA= | 6.9 | |
| VEL= | 1.5 | |
| DEPTH= | .3 | |

*SECNO 5.082
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.082 | 2.55 | 2506.55 | 2506.55 | .00 | 2506.97 | .42 | 2.86 | .03 | 2504.50 |
| 896.0 | 394.3 | 368.9 | 132.8 | 165.6 | 49.3 | 41.2 | 103.2 | 78.7 | 2504.50 |
| .72 | 2.38 | 7.49 | 3.22 | .050 | .030 | .050 | .000 | 2504.00 | 766.84 |
| .007575 | 410. | 360. | 310. | 0 | 9 | 0 | .00 | 281.88 | 1048.72 |

FLOW DISTRIBUTION FOR SECNO= 5.08 CWSEL= 2506.55

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 767. | 785. | 790. | 801. | 817. | 846. | 876. | 905. | 935. | 965. | 980. | 985. | 990. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 3.0 | 4.6 | 3.9 | 3.3 | 3.2 | 3.2 | 3.2 | 3.2 | 4.9 | 3.3 | 4.2 | |
| AREA= | 13.9 | 8.0 | 13.5 | 14.3 | 16.7 | 16.3 | 16.2 | 16.5 | 16.6 | 15.8 | 8.3 | 9.5 | |
| VEL= | 2.6 | 3.4 | 3.1 | 2.4 | 1.8 | 1.7 | 1.7 | 1.7 | 1.7 | 2.8 | 3.6 | 4.0 | |
| DEPTH= | .8 | 1.5 | 1.3 | .9 | .6 | .6 | .6 | .6 | .6 | 1.1 | 1.7 | 1.9 | |

| STA= | 990. | 1012. | 1018. | 1023. | 1034. | 1049. |
|---|---|---|---|---|---|---|
| PER Q= | 41.2 | 5.8 | 3.1 | 4.6 | 1.3 | |
| AREA= | 49.3 | 13.1 | 7.6 | 13.9 | 6.6 | |
| VEL= | 7.5 | 4.0 | 3.6 | 3.0 | 1.7 | |
| DEPTH= | 2.3 | 1.9 | 1.7 | 1.2 | .5 | |

*SECNO 5.175

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.175 | 3.51 | 2514.51 | 2514.51 | .00 | 2515.17 | .66 | 3.35 | .07 | 2511.50 |
| 896.0 | 276.8 | 478.1 | 141.1 | 100.5 | 57.0 | 36.4 | 105.8 | 81.4 | 2511.50 |
| .75 | 2.76 | 8.39 | 3.88 | .050 | .030 | .050 | .000 | 2511.00 | 732.82 |
| .005969 | 530. | 490. | 460. | 0 | 11 | 0 | .00 | 183.79 | 1027.56 |

FLOW DISTRIBUTION FOR SECNO= 5.18 CWSEL= 2514.51

| STA= | 733. | 923. | 960. | 975. | 980. | 985. | 990. | 1008. | 1010. | 1015. | 1020. | 1028. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 3.1 | 6.0 | 5.0 | 6.3 | 7.4 | 53.4 | 3.8 | 6.5 | 4.1 | 1.4 | |
| AREA= | 24.1 | 18.8 | 18.9 | 11.3 | 13.1 | 14.3 | 57.0 | 7.3 | 13.3 | 10.1 | 5.7 | |
| VEL= | 1.2 | 1.5 | 2.8 | 3.9 | 4.4 | 4.6 | 8.4 | 4.7 | 4.4 | 3.6 | 2.1 | |
| DEPTH= | .1 | .5 | 1.3 | 2.3 | 2.6 | 2.9 | 3.3 | 2.9 | 2.7 | 2.0 | .8 | |

*SECNO 5.279
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.279 | 4.29 | 2522.29 | 2522.29 | .00 | 2523.02 | .73 | 2.85 | .02 | 2519.00 |
| 896.0 | 62.7 | 615.1 | 218.2 | 20.1 | 75.8 | 96.3 | 108.2 | 83.7 | 2519.00 |
| .77 | 3.13 | 8.12 | 2.27 | .050 | .030 | .050 | .000 | 2518.00 | 976.29 |
| .004580 | 540. | 550. | 550. | 0 | 11 | 0 | .00 | 172.69 | 1148.98 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 5.28 CWSEL= 2522.29

| STA= | 976. | 990. | 1010. | 1015. | 1020. | 1030. | 1045. | 1070. | 1149. |
|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.0 | 68.6 | 6.7 | 4.4 | 4.1 | 3.6 | 3.2 | 2.3 | |
| AREA= | 20.1 | 75.8 | 14.7 | 11.4 | 14.4 | 15.6 | 17.7 | 22.5 | |
| VEL= | 3.1 | 8.1 | 4.1 | 3.5 | 2.6 | 2.1 | 1.6 | .9 | |
| DEPTH= | 1.5 | 3.8 | 2.9 | 2.3 | 1.4 | 1.0 | .7 | .3 | |

*SECNO -3.454
START TRIB COMP
-3.454 3.454 2371.782

3265 DIVIDED FLOW

HOLLY WASH/FLYING E WASH CONFLUENCE
HYDRAULIC CONTROL LINE IS AT STATION 1207.0

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| -3.454 | 3.28 | 2371.78 | .00 | .00 | 2372.67 | .89 | 5.14 | -2.26 | 2369.00 |
| 2152.0 | 1495.0 | 553.1 | 103.9 | 365.7 | 42.3 | 17.7 | 111.7 | 87.0 | 2369.00 |
| .79 | 4.09 | 13.07 | 5.87 | .050 | .030 | .050 | .000 | 2368.50 | 626.23 |
| 015985 | 450. | 545. | 530. | 0 | 0 | 0 | .00 | 430.55 | 1222.47 |

FLOW DISTRIBUTION FOR SECNO= -3.45 CWSEL= 2371.78

| STA= | 626. | 660. | 680. | 691. | 704. | 730. | 788. | 823. | 840. | 856. | 896. | 982. | 1000. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 7.1 | 6.3 | 7.4 | 6.9 | 3.2 | 4.5 | 3.8 | 3.4 | 4.2 | 3.6 | 3.8 | |
| AREA= | 21.0 | 30.6 | 22.4 | 26.4 | 33.3 | 25.9 | 29.1 | 19.8 | 18.1 | 29.0 | 28.2 | 20.1 | |
| VEL= | 3.1 | 5.0 | 6.0 | 6.0 | 4.4 | 2.6 | 3.3 | 4.1 | 4.1 | 3.1 | 2.7 | 4.1 | |
| DEPTH= | .6 | 1.5 | 2.0 | 2.0 | 1.3 | .5 | .8 | 1.1 | 1.1 | .7 | .3 | 1.1 | |

| STA= | 1000. | 1014. | 1187. | 1198. | 1212. | 1218. | 1222. |
|---|---|---|---|---|---|---|---|
| PER Q= | 3.6 | 3.2 | 5.6 | 25.7 | 4.1 | .7 | |
| AREA= | 17.4 | 23.9 | 20.3 | 42.3 | 13.7 | 4.0 | |
| VEL= | 4.4 | 2.9 | 5.9 | 13.1 | 6.5 | 3.7 | |
| DEPTH= | 1.3 | .1 | 1.9 | 3.0 | 2.3 | .9 | |

*SECNO .198
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
HOLLY WASH
HOLLY WASH RIVER MILES MEASURED FROM CONFLUENCE AT SECTION 3.355

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| .198 | 4.47 | 2377.47 | 2377.47 | .00 | 2378.51 | 1.04 | 5.54 | .05 | 2374.30 |
| 1361.0 | 495.6 | 806.5 | 58.9 | 134.9 | 79.0 | 18.1 | 115.4 | 90.1 | 2374.30 |
| .81 | 3.67 | 10.21 | 3.26 | .050 | .030 | .050 | .000 | 2373.00 | 906.98 |
| .006918 | 500. | 500. | 510. | 0 | 11 | 0 | .00 | 116.51 | 1023.48 |

FLOW DISTRIBUTION FOR SECNO= .20 CWSEL= 2377.47

| STA= | 907. | 972. | 976. | 980. | 983. | 987. | 1007. | 1013. | 1023. |
|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 21.6 | 3.4 | 3.4 | 3.7 | 4.4 | 59.3 | 3.4 | .9 | |
| AREA= | 93.3 | 9.9 | 9.8 | 10.4 | 11.5 | 79.0 | 12.0 | 6.1 | |
| VEL= | 3.1 | 4.6 | 4.7 | 4.9 | 5.2 | 10.2 | 3.9 | 2.1 | |
| DEPTH= | 1.4 | 2.6 | 2.6 | 2.8 | 3.0 | 3.9 | 2.0 | .6 | |

*SECNO .291
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .291 | 3.92 | 2382.42 | 2382.42 | .00 | 2383.56 | 1.15 | 3.81 | .03 | 2379.00 |
| 1361.0 | 583.0 | 687.9 | 90.2 | 115.9 | 62.2 | 20.1 | 117.9 | 91.3 | 2379.00 |
| .83 | 5.03 | 11.06 | 4.49 | .050 | .030 | .050 | .000 | 2378.50 | 935.66 |
| .008861 | 485. | 490. | 490. | 0 | 15 | 0 | .00 | 89.07 | 1024.74 |

FLOW DISTRIBUTION FOR SECNO= .29 CWSEL= 2382.42

| STA= | 936. | 956. | 962. | 966. | 970. | 974. | 978. | 981. | 985. | 989. | 993. | 1010. | 1014. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 4.8 | 4.1 | 4.6 | 4.4 | 4.0 | 3.8 | 3.5 | 4.1 | 5.5 | 50.5 | 4.5 | |
| AREA= | 17.7 | 13.5 | 10.5 | 11.3 | 10.8 | 10.0 | 9.8 | 9.2 | 10.6 | 12.6 | 62.2 | 11.3 | |
| VEL= | 3.1 | 4.8 | 5.3 | 5.6 | 5.6 | 5.4 | 5.3 | 5.1 | 5.3 | 6.0 | 11.1 | 5.5 | |
| DEPTH= | .9 | 2.2 | 2.6 | 2.8 | 2.8 | 2.7 | 2.6 | 2.5 | 2.6 | 3.1 | 3.7 | 2.8 | |

| STA= | 1014. | 1025. |
|---|---|---|
| PER Q= | 2.1 | |
| AREA= | 8.8 | |
| VEL= | 3.3 | |
| DEPTH= | .8 | |

*SECNO .387

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .387 | 4.71 | 2387.71 | 2387.71 | .00 | 2389.38 | 1.67 | 4.32 | .16 | 2383.30 |
| 1361.0 | 277.8 | 873.3 | 209.9 | 45.5 | 71.4 | 40.6 | 119.9 | 92.1 | 2383.30 |
| .84 | 6.10 | 12.23 | 5.18 | .050 | .030 | .050 | .000 | 2383.00 | 975.64 |
| .008105 | 510. | 510. | 510. | 0 | 11 | 0 | .00 | 53.02 | 1028.66 |

FLOW DISTRIBUTION FOR SECNO= .39 CWSEL= 2387.71

| STA= | 976. | 985. | 988. | 991. | 1007. | 1010. | 1013. | 1018. | 1029. |
|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.0 | 6.6 | 6.9 | 64.2 | 7.4 | 3.8 | 3.1 | 1.2 | |
| AREA= | 19.7 | 12.8 | 13.1 | 71.4 | 14.2 | 8.9 | 10.6 | 6.8 | |
| VEL= | 4.8 | 7.0 | 7.1 | 12.2 | 7.1 | 5.8 | 4.0 | 2.4 | |
| DEPTH= | 2.1 | 4.3 | 4.4 | 4.5 | 4.3 | 3.6 | 1.9 | .7 | |

*SECNO .482

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .482 | 5.00 | 2392.00 | 2391.79 | .00 | 2393.01 | 1.01 | 3.56 | .07 | 2390.00 |
| 1361.0 | 498.9 | 846.2 | 15.9 | 113.5 | 87.6 | 5.9 | 122.0 | 92.9 | 2390.00 |
| .86 | 4.40 | 9.66 | 2.70 | .050 | .030 | .050 | .000 | 2387.00 | 932.01 |
| .006449 | 485. | 500. | 485. | 2 | 5 | 0 | .00 | 84.89 | 1016.89 |

FLOW DISTRIBUTION FOR SECNO= .48 CWSEL= 2392.00

| STA= | 932. | 943. | 945. | 948. | 950. | 954. | 957. | 963. | 981. | 989. | 1011. | 1017. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.1 | 3.2 | 4.4 | 4.4 | 5.6 | 3.9 | 3.5 | 3.2 | 3.3 | 62.2 | 1.2 | |
| AREA= | 18.0 | 8.0 | 10.0 | 10.0 | 13.6 | 10.8 | 11.9 | 17.6 | 13.6 | 87.6 | 5.9 | |
| VEL= | 3.8 | 5.5 | 6.0 | 6.0 | 5.6 | 4.9 | 4.0 | 2.5 | 3.3 | 9.7 | 2.7 | |
| DEPTH= | 1.7 | 3.6 | 4.0 | 4.0 | 3.7 | 3.0 | 2.2 | 1.0 | 1.6 | 4.0 | 1.0 | |

*SECNO .559

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

```
   ECNO     DEPTH    CWSEL    CRIWS    WSELK    EG       HV       HL       OLOSS    L-BANK ELEV
   Q        QLOB     QCH      QROB     ALOB     ACH      AROB     VOL      TWA      R-BANK ELEV
   TIME     VLOB     VCH      VROB     XNL      XNCH     XNR      WTN      ELMIN    SSTA
   SLOPE    XLOBL    XLCH     XLOBR    ITRIAL   IDC      ICONT    CORAR    TOPWID   ENDST


3470 ENCROACHMENT STATIONS=      978.0    1022.0  TYPE=      1  TARGET=      44.000
      .559      4.71   2400.71   2400.71       .00   2402.28      1.58      3.20       .17   2400.00
    1361.0        .0    1361.0        .0        .0     135.0        .0     123.6      93.5 100000.00
       .87       .00     10.08       .00      .000      .030      .000      .000   2396.00    978.00
   .009920      405.      405.      405.         0        11         0       .00     44.00   1022.00


FLOW DISTRIBUTION FOR SECNO=       .56          CWSEL=   2400.71

STA=     978.    1022.
  PER Q=    100.0
   AREA=    135.0
    VEL=     10.1
  DEPTH=      3.1

*SECNO  .607
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
      .607      4.46   2403.46   2403.46       .00   2405.01      1.55      2.36       .00   2399.60
    1361.0     243.9     879.0     238.1      44.4      74.9      43.2     124.5      93.8   2399.60
       .88      5.49     11.74      5.51      .050      .030      .050      .000   2399.00    972.02
   .008410      290.      255.      265.         0        11         0       .00     55.20   1027.22


FLOW DISTRIBUTION FOR SECNO=       .61          CWSEL=   2403.46

STA=     972.     982.     985.     988.     991.    1009.    1012.    1015.    1018.    1025.    1027.
  PER Q=      3.7      3.8      5.0      5.5     64.6      5.5      5.0      3.9      3.0       .1
   AREA=     13.3      9.2     10.7     11.3     74.9     11.3     10.7      9.6     10.6      1.0
    VEL=      3.8      5.6      6.3      6.6     11.7      6.6      6.3      5.5      3.9      1.4
  DEPTH=      1.3      3.1      3.6      3.8      4.2      3.8      3.6      3.0      1.7       .4

*SECNO  .681
      .681      3.91   2406.91   2406.88       .00   2408.11      1.20      3.06       .03   2403.30
    1361.0     126.6     951.4     283.0      34.0      93.5      67.7     126.1      94.4   2403.50
       .89      3.73     10.18      4.18      .050      .030      .050      .000   2403.00    966.81
   .007351      390.      390.      390.         1        15         0       .00     83.38   1050.19
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .68 CWSEL= 2406.91

| STA= | 967. | 985. | 987. | 1013. | 1015. | 1037. | 1048. | 1050. |
|---|---|---|---|---|---|---|---|---|
| PER Q= | 6.3 | 3.0 | 69.9 | 3.1 | 15.8 | 1.8 | .0 | |
| AREA= | 26.5 | 7.5 | 93.5 | 7.9 | 49.0 | 10.6 | .2 | |
| VEL= | 3.2 | 5.4 | 10.2 | 5.4 | 4.4 | 2.4 | .6 | |
| DEPTH= | 1.5 | 3.3 | 3.7 | 3.2 | 2.3 | .9 | .1 | |

*SECNO .747

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .747 | 6.12 | 2411.12 | 2411.12 | .00 | 2412.87 | 1.75 | 2.44 | .17 | 2407.40 |
| 1361.0 | 124.6 | 1131.0 | 105.4 | 28.5 | 98.4 | 25.1 | 127.5 | 94.9 | 2407.40 |
| .90 | 4.37 | 11.49 | 4.20 | .050 | .030 | .050 | .000 | 2405.00 | 973.30 |
| .006686 | 370. | 350. | 320. | 0 | 14 | 0 | .00 | 48.41 | 1021.70 |

DISTRIBUTION FOR SECNO= .75 CWSEL= 2411.12

| STA= | 973. | 976. | 979. | 982. | 985. | 988. | 1008. | 1010. | 1013. | 1016. | 1019. | 1022. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .1 | .6 | 1.6 | 2.8 | 4.1 | 83.1 | 2.7 | 2.8 | 1.6 | .6 | .1 | |
| AREA= | 1.0 | 3.4 | 5.8 | 8.2 | 10.3 | 98.4 | 6.8 | 8.2 | 5.8 | 3.4 | 1.0 | |
| VEL= | 1.2 | 2.6 | 3.7 | 4.6 | 5.4 | 11.5 | 5.4 | 4.6 | 3.7 | 2.6 | 1.2 | |
| DEPTH= | .4 | 1.1 | 1.9 | 2.7 | 3.4 | 4.9 | 3.4 | 2.7 | 1.9 | 1.1 | .4 | |

*SECNO .853

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .853 | 3.77 | 2420.77 | 2420.77 | .00 | 2421.78 | 1.01 | 4.34 | .07 | 2417.50 |
| 1361.0 | 531.5 | 563.8 | 265.7 | 113.4 | 50.7 | 49.8 | 129.7 | 95.8 | 2417.50 |
| .92 | 4.69 | 11.12 | 5.33 | .050 | .030 | .050 | .000 | 2417.00 | 929.63 |
| .009520 | 510. | 560. | 560. | 0 | 14 | 0 | .00 | 102.73 | 1032.36 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .85 CWSEL= 2420.77

| STA= | 930. | 955. | 965. | 970. | 976. | 981. | 986. | 991. | 996. | 1010. | 1015. | 1020. | 1026. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.6 | 5.6 | 3.5 | 4.0 | 4.6 | 5.1 | 5.7 | 6.0 | 41.4 | 7.1 | 6.2 | 4.5 | |
| AREA= | 21.2 | 18.1 | 10.3 | 11.3 | 12.3 | 12.8 | 13.9 | 13.6 | 50.7 | 15.6 | 14.3 | 12.5 | |
| VEL= | 2.9 | 4.2 | 4.6 | 4.9 | 5.1 | 5.4 | 5.6 | 6.0 | 11.1 | 6.2 | 5.8 | 4.9 | |
| DEPTH= | .8 | 1.7 | 2.0 | 2.2 | 2.4 | 2.5 | 2.7 | 3.0 | 3.5 | 3.1 | 2.9 | 2.3 | |

| STA= | 1026. | 1032. |
|---|---|---|
| PER Q= | 1.8 | |
| AREA= | 7.5 | |
| VEL= | 3.2 | |
| DEPTH= | 1.1 | |

*SECNO .954
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .954 | 4.00 | 2433.00 | 2433.00 | .00 | 2434.16 | 1.16 | 4.59 | .04 | 2429.80 |
| 1361.0 | 233.4 | 815.7 | 311.9 | 49.6 | 77.5 | 70.4 | 132.2 | 96.9 | 2429.80 |
| .94 | 4.70 | 10.53 | 4.43 | .050 | .030 | .050 | .000 | 2429.00 | 961.86 |
| 08202 | 440. | 530. | 605. | 0 | 8 | 0 | .00 | 86.64 | 1048.50 |

FLOW DISTRIBUTION FOR SECNO= .95 CWSEL= 2433.00

| STA= | 962. | 976. | 982. | 987. | 1008. | 1015. | 1020. | 1025. | 1035. | 1049. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.6 | 5.7 | 5.9 | 59.9 | 8.3 | 4.6 | 3.5 | 4.7 | 1.8 | |
| AREA= | 20.5 | 15.1 | 14.0 | 77.5 | 20.5 | 12.5 | 10.8 | 16.8 | 9.9 | |
| VEL= | 3.7 | 5.1 | 5.7 | 10.5 | 5.5 | 5.0 | 4.5 | 3.8 | 2.5 | |
| DEPTH= | 1.4 | 2.7 | 3.1 | 3.6 | 2.9 | 2.5 | 2.2 | 1.7 | .7 | |

*SECNO 1.005

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.30

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.005 | 4.87 | 2434.87 | 2433.43 | .00 | 2435.07 | .20 | .81 | .10 | 2430.50 |
| 1361.0 | 685.8 | 422.1 | 253.1 | 296.9 | 78.4 | 99.5 | 134.3 | 97.8 | 2430.50 |
| .96 | 2.31 | 5.39 | 2.54 | .050 | .030 | .050 | .000 | 2430.00 | 854.70 |
| .001545 | 280. | 270. | 255. | 2 | 15 | 0 | .00 | 189.40 | 1044.10 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.00 CWSEL= 2434.87

| STA= | 855. | 921. | 941. | 951. | 961. | 966. | 971. | 976. | 981. | 986. | 991. | 1008. | 1015. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.9 | 8.1 | 5.3 | 6.1 | 3.3 | 3.5 | 3.7 | 4.0 | 4.1 | 4.4 | 31.0 | 6.8 | |
| AREA= | 73.0 | 50.8 | 29.7 | 32.4 | 17.1 | 17.6 | 18.3 | 19.1 | 19.0 | 19.8 | 78.4 | 30.8 | |
| VEL= | 1.5 | 2.2 | 2.4 | 2.6 | 2.6 | 2.7 | 2.8 | 2.9 | 2.9 | 3.0 | 5.4 | 3.0 | |
| DEPTH= | 1.1 | 2.5 | 3.0 | 3.2 | 3.4 | 3.5 | 3.7 | 3.8 | 4.0 | 4.2 | 4.6 | 4.1 | |

| STA= | 1015. | 1020. | 1029. | 1044. |
|---|---|---|---|---|
| PER Q= | 3.6 | 5.5 | 2.7 | |
| AREA= | 17.5 | 29.7 | 21.6 | |
| VEL= | 2.8 | 2.5 | 1.7 | |
| DEPTH= | 3.7 | 3.2 | 1.4 | |

*SECNO 1.101

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.101 | 3.65 | 2438.65 | 2438.65 | .00 | 2439.75 | 1.10 | 1.57 | .27 | 2435.70 |
| 1361.0 | 168.7 | 709.3 | 483.1 | 36.0 | 66.5 | 96.9 | 138.1 | 99.4 | 2435.70 |
| .98 | 4.69 | 10.66 | 4.99 | .050 | .030 | .050 | .000 | 2435.00 | 968.43 |
| .009369 | 485. | 510. | 515. | 0 | 19 | 0 | .00 | 92.09 | 1060.52 |

FLOW DISTRIBUTION FOR SECNO= 1.10 CWSEL= 2438.65

| STA= | 968. | 985. | 990. | 1010. | 1015. | 1021. | 1026. | 1032. | 1037. | 1043. | 1059. | 1061. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 6.5 | 5.9 | 52.1 | 5.9 | 6.1 | 6.0 | 6.1 | 4.9 | 3.3 | 3.2 | .0 | |
| AREA= | 22.0 | 14.0 | 66.5 | 14.0 | 15.1 | 14.8 | 15.1 | 13.0 | 10.3 | 14.4 | .1 | |
| VEL= | 4.0 | 5.7 | 10.7 | 5.7 | 5.5 | 5.5 | 5.5 | 5.1 | 4.4 | 3.0 | .5 | |
| DEPTH= | 1.3 | 2.8 | 3.3 | 2.8 | 2.7 | 2.7 | 2.7 | 2.4 | 1.9 | .9 | .1 | |

*SECNO 1.202
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.202 | 3.65 | 2449.65 | 2449.65 | .00 | 2450.59 | .95 | 4.71 | .02 | 2446.80 |
| 1361.0 | 421.0 | 722.6 | 217.4 | 102.0 | 72.4 | 50.8 | 140.7 | 100.6 | 2446.80 |
| 1.00 | 4.13 | 9.98 | 4.28 | .050 | .030 | .050 | .000 | 2446.00 | 933.76 |
| .008481 | 510. | 530. | 540. | 0 | 5 | 0 | .00 | 113.55 | 1047.32 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.20 CWSEL= 2449.65

| STA= | 934. | 945. | 956. | 966. | 976. | 985. | 990. | 992. | 1014. | 1019. | 1025. | 1030. | 1047. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.4 | 4.8 | 4.8 | 4.8 | 6.7 | 4.3 | 2.2 | 53.1 | 5.1 | 4.7 | 3.2 | 3.0 | |
| AREA= | 13.8 | 17.0 | 17.0 | 16.9 | 20.2 | 11.7 | 5.5 | 72.4 | 12.9 | 13.2 | 10.4 | 14.3 | |
| VEL= | 3.4 | 3.8 | 3.8 | 3.9 | 4.5 | 5.0 | 5.3 | 10.0 | 5.4 | 4.9 | 4.2 | 2.8 | |
| DEPTH= | 1.2 | 1.6 | 1.6 | 1.7 | 2.1 | 2.5 | 2.7 | 3.2 | 2.7 | 2.4 | 1.9 | .8 | |

*SECNO 1.295
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.295 | 3.57 | 2455.57 | 2455.57 | .00 | 2456.42 | .86 | 4.09 | .01 | 2452.70 |
| 1361.0 | 226.8 | 687.5 | 446.7 | 56.0 | 70.9 | 115.3 | 143.3 | 102.1 | 2452.80 |
| 1.02 | 4.05 | 9.70 | 3.88 | .050 | .030 | .050 | .000 | 2452.00 | 951.71 |
| .008172 | 490. | 490. | 495. | 0 | 5 | 0 | .00 | 149.49 | 1101.20 |

FLOW DISTRIBUTION FOR SECNO= 1.29 CWSEL= 2455.57

| | 952. | 977. | 982. | 987. | 991. | 1014. | 1018. | 1023. | 1028. | 1033. | 1038. | 1048. | 1058. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| Q= | 4.9 | 3.1 | 4.2 | 4.5 | 50.5 | 4.5 | 4.4 | 4.0 | 3.6 | 3.0 | 5.0 | 3.7 | |
| AREA= | 22.2 | 10.0 | 12.1 | 11.7 | 70.9 | 12.0 | 12.3 | 11.6 | 10.8 | 9.8 | 17.4 | 14.8 | |
| VEL= | 3.0 | 4.2 | 4.8 | 5.2 | 9.7 | 5.2 | 4.9 | 4.7 | 4.5 | 4.2 | 3.9 | 3.4 | |
| DEPTH= | .9 | 2.0 | 2.4 | 2.7 | 3.2 | 2.7 | 2.5 | 2.3 | 2.2 | 2.0 | 1.7 | 1.4 | |

| STA= | 1058. | 1074. | 1101. |
|---|---|---|---|
| PER Q= | 3.2 | 1.3 | |
| AREA= | 15.7 | 10.7 | |
| VEL= | 2.7 | 1.7 | |
| DEPTH= | 1.0 | .4 | |

*SECNO 1.399
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.399 | 2.96 | 2463.96 | 2463.96 | .00 | 2464.67 | .70 | 4.73 | .02 | 2461.50 |
| 1361.0 | 518.6 | 610.4 | 232.0 | 138.7 | 66.7 | 60.7 | 146.6 | 104.3 | 2461.50 |
| 1.04 | 3.74 | 9.15 | 3.82 | .050 | .030 | .050 | .000 | 2461.00 | 871.81 |
| .008972 | 580. | 550. | 530. | 0 | 15 | 0 | .00 | 187.47 | 1059.28 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.40 CWSEL= 2463.96

| STA= | 872. | 919. | 936. | 945. | 954. | 962. | 971. | 981. | 986. | 1010. | 1020. | 1030. | 1050. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.4 | 5.2 | 3.4 | 4.0 | 4.6 | 5.3 | 7.0 | 4.2 | 44.9 | 7.8 | 5.1 | 4.0 | |
| AREA= | 26.4 | 21.6 | 12.9 | 14.0 | 15.3 | 16.7 | 20.5 | 11.3 | 66.7 | 22.1 | 17.1 | 19.3 | |
| VEL= | 2.3 | 3.3 | 3.6 | 3.9 | 4.1 | 4.3 | 4.6 | 5.0 | 9.1 | 4.8 | 4.0 | 2.8 | |
| DEPTH= | .6 | 1.2 | 1.5 | 1.6 | 1.8 | 1.9 | 2.1 | 2.4 | 2.7 | 2.2 | 1.7 | 1.0 | |

| STA= | 1050. | 1059. |
|---|---|---|
| PER Q= | .2 | |
| AREA= | 2.2 | |
| VEL= | 1.1 | |
| DEPTH= | .2 | |

*SECNO 1.473
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.473 | 3.53 | 2469.53 | 2469.53 | .00 | 2470.36 | .82 | 3.33 | .04 | 2466.50 |
| 1361.0 | 259.9 | 680.3 | 420.9 | 82.1 | 71.6 | 95.4 | 148.9 | 105.9 | 2466.50 |
| 1.06 | 3.16 | 9.51 | 4.41 | .050 | .030 | .050 | .000 | 2466.00 | 898.38 |
| 07898 | 420. | 395. | 370. | 0 | 11 | 0 | .00 | 160.24 | 1058.62 |

FLOW DISTRIBUTION FOR SECNO= 1.47 CWSEL= 2469.53

| STA= | 898. | 957. | 975. | 983. | 988. | 1010. | 1020. | 1030. | 1040. | 1050. | 1059. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.8 | 5.7 | 4.6 | 4.0 | 50.0 | 10.7 | 8.2 | 6.3 | 4.6 | 1.1 | |
| AREA= | 31.5 | 24.0 | 15.6 | 11.1 | 71.6 | 27.8 | 23.8 | 20.3 | 16.8 | 6.6 | |
| VEL= | 2.1 | 3.2 | 4.0 | 5.0 | 9.5 | 5.2 | 4.7 | 4.2 | 3.7 | 2.2 | |
| DEPTH= | .5 | 1.3 | 1.9 | 2.6 | 3.2 | 2.8 | 2.4 | 2.0 | 1.7 | .8 | |

*SECNO 1.576
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.576 | 2.01 | 2476.01 | 2476.01 | .00 | 2476.74 | .73 | 5.85 | .01 | 2474.00 |
| 1361.0 | 134.2 | 380.0 | 846.7 | 30.4 | 38.2 | 160.9 | 151.9 | 107.8 | 2474.00 |
| 1.08 | 4.42 | 9.94 | 5.26 | .050 | .030 | .050 | .000 | 2474.00 | 969.86 |
| .015834 | 520. | 540. | 545. | 0 | 11 | 0 | .00 | 155.23 | 1125.08 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.58 CWSEL= 2476.01

| STA= | 970. | 993. | 1000. | 1019. | 1029. | 1040. | 1050. | 1070. | 1090. | 1110. | 1125. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.6 | 5.3 | 27.9 | 9.1 | 9.2 | 9.1 | 15.5 | 11.0 | 7.1 | 1.4 | |
| AREA= | 17.2 | 13.2 | 38.2 | 20.7 | 20.9 | 20.7 | 37.3 | 30.3 | 23.3 | 7.7 | |
| VEL= | 3.6 | 5.4 | 9.9 | 6.0 | 6.0 | 6.0 | 5.7 | 4.9 | 4.1 | 2.4 | |
| DEPTH= | .8 | 1.8 | 2.0 | 2.0 | 2.0 | 2.0 | 1.9 | 1.5 | 1.2 | .5 | |

*SECNO 1.615
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
SECTION TAKEN FROM TOPOGRAPHIC MAP

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.615 | 2.86 | 2481.86 | 2481.86 | .00 | 2482.69 | .82 | 2.55 | .03 | 2479.00 |
| 1361.0 | 398.4 | 572.4 | 390.2 | 79.6 | 57.3 | 107.2 | 153.0 | 108.5 | 2479.00 |
| 1.09 | 5.00 | 9.99 | 3.64 | .050 | .030 | .050 | .000 | 2479.00 | 950.68 |
| .010002 | 205. | 205. | 205. | 0 | 11 | 0 | .00 | 151.23 | 1101.91 |

FLOW DISTRIBUTION FOR SECNO= 1.62 CWSEL= 2481.86

| | 951. | 960. | 990. | 1010. | 1025. | 1102. |
|---|---|---|---|---|---|---|
| PER Q= | 1.8 | 27.5 | 42.1 | 13.7 | 14.9 | |
| AREA= | 8.7 | 70.9 | 57.3 | 35.5 | 71.7 | |
| VEL= | 2.8 | 5.3 | 10.0 | 5.3 | 2.8 | |
| DEPTH= | .9 | 2.4 | 2.9 | 2.4 | .9 | |

*SECNO 1.661
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.661 | 2.71 | 2484.71 | 2484.71 | .00 | 2485.40 | .69 | 2.59 | .01 | 2482.50 |
| 1361.0 | 681.5 | 486.4 | 193.1 | 164.3 | 50.4 | 46.4 | 154.4 | 109.5 | 2482.50 |
| 1.10 | 4.15 | 9.64 | 4.16 | .050 | .030 | .050 | .000 | 2482.00 | 864.32 |
| .011424 | 255. | 245. | 215. | 0 | 11 | 0 | .00 | 181.83 | 1046.15 |

FLOW DISTRIBUTION FOR SECNO= 1.66 CWSEL= 2484.71

| STA= | 864. | 886. | 911. | 935. | 958. | 981. | 991. | 1011. | 1022. | 1041. | 1046. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .9 | 5.3 | 10.8 | 13.1 | 13.1 | 6.8 | 35.7 | 7.9 | 6.1 | .2 | |
| AREA= | 7.7 | 23.5 | 35.8 | 39.3 | 39.3 | 18.6 | 50.4 | 21.6 | 23.0 | 1.8 | |
| VEL= | 1.6 | 3.1 | 4.1 | 4.5 | 4.5 | 5.0 | 9.6 | 5.0 | 3.6 | 1.6 | |
| DEPTH= | .4 | 1.0 | 1.5 | 1.7 | 1.7 | 2.0 | 2.5 | 2.0 | 1.2 | .4 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.767
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.767 | 3.17 | 2493.17 | 2493.17 | .00 | 2493.75 | .58 | 5.28 | .01 | 2490.60 |
| 1361.0 | 467.7 | 498.5 | 394.8 | 159.3 | 55.0 | 100.0 | 158.0 | 112.3 | 2490.50 |
| 1.13 | 2.94 | 9.07 | 3.95 | .050 | .030 | .050 | .000 | 2490.00 | 804.38 |
| .008151 | 540. | 560. | 560. | 0 | 11 | 0 | .00 | 265.80 | 1070.18 |

FLOW DISTRIBUTION FOR SECNO= 1.77 CWSEL= 2493.17

| STA= | 804. | 820. | 851. | 881. | 918. | 950. | 984. | 990. | 1009. | 1018. | 1040. | 1062. | 1070. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .1 | 1.4 | 5.2 | 3.7 | 3.2 | 15.7 | 5.0 | 36.6 | 7.7 | 12.9 | 7.8 | .7 | |
| AREA= | 1.3 | 12.8 | 28.0 | 24.8 | 21.4 | 56.8 | 14.2 | 55.0 | 21.8 | 42.2 | 31.2 | 4.8 | |
| VEL= | .5 | 1.5 | 2.5 | 2.1 | 2.1 | 3.8 | 4.8 | 9.1 | 4.8 | 4.1 | 3.4 | 1.9 | |
| DEPTH= | .1 | .4 | .9 | .7 | .7 | 1.7 | 2.4 | 2.9 | 2.4 | 1.9 | 1.4 | .6 | |

*SECNO 1.873

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.873 | 1.87 | 2498.87 | 2498.85 | .00 | 2499.38 | .51 | 5.62 | .01 | 2497.00 |
| 1361.0 | 285.2 | 393.4 | 682.3 | 78.0 | 45.9 | 161.5 | 161.8 | 115.5 | 2497.00 |
| 1.16 | 3.66 | 8.58 | 4.22 | .050 | .030 | .050 | .000 | 2497.00 | 906.83 |
| 013009 | 500. | 560. | 585. | 0 | 11 | 0 | .00 | 264.75 | 1171.58 |

FLOW DISTRIBUTION FOR SECNO= 1.87 CWSEL= 2498.87

| STA= | 907. | 930. | 960. | 980. | 1000. | 1025. | 1049. | 1071. | 1093. | 1115. | 1137. | 1159. | 1172. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .3 | 3.4 | 6.0 | 11.1 | 28.9 | 17.3 | 13.5 | 9.3 | 5.7 | 3.2 | 1.1 | .1 | |
| AREA= | 4.2 | 19.0 | 22.4 | 32.4 | 45.9 | 45.9 | 37.9 | 30.2 | 22.5 | 15.9 | 8.2 | 1.1 | |
| VEL= | 1.1 | 2.5 | 3.7 | 4.7 | 8.6 | 5.1 | 4.9 | 4.2 | 3.4 | 2.7 | 1.8 | .7 | |
| DEPTH= | .2 | .6 | 1.1 | 1.6 | 1.9 | 1.9 | 1.7 | 1.4 | 1.0 | .7 | .4 | .1 | |

T1 FLOODWAY RUN
T2 FLOODWAY ESTABLISHED IN UPPER HOLLY WASH
T3 AB: UPPER FLYING E WASH

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| J1 | ICHECK | INQ | NINV | IDIR | STRT | METRIC | HVINS | Q | WSEL | FQ |
| | 0 | 3 | 0 | 0 | .008304 | 0 | 0 | 0 | 2309.8 | 0 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| J2 | NPROF | IPLOT | PRFVS | XSECV | XSECH | FN | ALLDC | IBW | CHNIM | ITRACE |
| | 15 | | -1 | | | | -1 | | | |

```
ECNO     DEPTH    CWSEL    CRIWS    WSELK    EG       HV       HL       OLOSS    L-BANK ELEV
Q        QLOB     QCH      QROB     ALOB     ACH      AROB     VOL      TWA      R-BANK ELEV
TIME     VLOB     VCH      VROB     XNL      XNCH     XNR      WTN      ELMIN    SSTA
SLOPE    XLOBL    XLCH     XLOBR    ITRIAL   IDC      ICONT    CORAR    TOPWID   ENDST


*PROF 2

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV=     .100 CEHV=     .300
*SECNO 2.435
 WATER EL=X5 CARD=   2309.800

3470 ENCROACHMENT STATIONS=      957.7    1102.0  TYPE=      1  TARGET=      144.310
          CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH
    2.435      6.41   2309.91   2309.80   2309.87   2312.10      2.18       .00       .00   2304.00
   6943.0     856.4    3357.8    2728.8     124.5     221.0     355.8        .0        .0   2304.00
      .00      6.88     15.19      7.67      .050      .030      .050      .000   2303.50    957.69
  .008374      500.      490.      455.         0         5         3       .00    144.31   1102.00


1490 NH CARD USED
*SECNO 2.539

DIVIDED FLOW


3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      465.3    1100.0  TYPE=      1  TARGET=      634.700
 ELENCL=   2317.30  ELENCR=   2317.00
          AT HIGH FLOW, BOTH YUCCA FLAT WASH AND FLYING E WASH CHANNELS
          ARE USED.  SECTION REPEATED FOR BOTH MODELS. NH CARD DEFINES CHANNELS
    2.539      6.51   2315.51   2315.51   2315.51   2316.75      1.24      4.25       .09   2313.50
   6943.0     371.4    1747.4    4824.2     126.3     185.3     532.0       9.2       3.3   2313.20
      .02      2.94      9.43      9.07      .050      .030      .038      .000   2309.00    509.92
  .007990      570.      550.      490.         0         5         0       .00    394.83   1059.04


*SECNO 2.630

3301 HV CHANGED MORE THAN HVINS
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .51

3470 ENCROACHMENT STATIONS= 893.3 1030.5 TYPE= 1 TARGET= 137.150
UPPER FLYING E WASH FULLY DEFINED CHANNEL

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.630 | 4.20 | 2319.20 | 2317.86 | 2319.19 | 2319.66 | .46 | 2.83 | .08 | 2315.40 |
| 2152.0 | 959.9 | 1080.0 | 112.1 | 258.1 | 160.0 | 34.8 | 16.2 | 6.2 | 2315.40 |
| .04 | 3.72 | 6.75 | 3.22 | .050 | .030 | .050 | .000 | 2315.00 | 893.34 |
| .002928 | 480. | 480. | 460. | 2 | 14 | 0 | .00 | 137.15 | 1030.49 |

*SECNO 2.725

3265 DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 907.3 1151.5 TYPE= 1 TARGET= 244.240

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.725 | 3.77 | 2325.77 | 2325.77 | 2325.77 | 2326.90 | 1.13 | 2.67 | .20 | 2323.50 |
| 2152.0 | 101.1 | 1011.6 | 1039.3 | 29.6 | 97.9 | 153.7 | 20.4 | 7.8 | 2323.50 |
| .06 | 3.42 | 10.33 | 6.76 | .050 | .030 | .050 | .000 | 2322.00 | 907.30 |
| .012747 | 515. | 500. | 485. | 0 | 11 | 0 | .00 | 147.64 | 1151.54 |

*SECNO 2.812

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 942.0 1375.9 TYPE= 1 TARGET= 433.850

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.812 | 3.56 | 2331.06 | 2331.06 | 2331.06 | 2331.66 | .60 | 3.78 | .05 | 2327.80 |
| 2152.0 | 298.0 | 1039.6 | 814.4 | 72.1 | 124.3 | 320.8 | 24.7 | 11.0 | 2327.80 |
| .08 | 4.13 | 8.37 | 2.54 | .050 | .030 | .050 | .000 | 2327.50 | 942.05 |
| .005591 | 440. | 460. | 480. | 0 | 12 | 0 | .00 | 433.85 | 1375.90 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.922

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 695.4 1047.6 TYPE= 1 TARGET= 352.230

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.922 | 3.68 | 2337.68 | 2337.68 | 2337.68 | 2338.44 | .76 | 3.78 | .05 | 2335.00 |
| 2152.0 | 934.6 | 948.4 | 269.0 | 269.7 | 98.6 | 58.3 | 30.8 | 15.4 | 2335.00 |
| .11 | 3.47 | 9.62 | 4.61 | .050 | .030 | .050 | .000 | 2334.00 | 695.41 |
| .008080 | 585. | 580. | 525. | 0 | 8 | 0 | .00 | 270.33 | 1047.64 |

*SECNO 3.005

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
[illegible] CRITICAL DEPTH ASSUMED

[illegible] ENCROACHMENT STATIONS= 936.5 1416.5 TYPE= 1 TARGET= 479.960

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.005 | 3.62 | 2344.12 | 2344.12 | 2344.12 | 2344.78 | .66 | 3.08 | .01 | 2340.90 |
| 2152.0 | 264.8 | 1109.3 | 777.9 | 72.4 | 128.5 | 296.4 | 35.6 | 18.9 | 2340.90 |
| .13 | 3.66 | 8.64 | 2.62 | .050 | .030 | .050 | .000 | 2340.50 | 936.60 |
| .005930 | 425. | 440. | 490. | 0 | 5 | 0 | .00 | 390.12 | 1416.45 |

*SECNO 3.047
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 980.8 1208.3 TYPE= 1 TARGET= 227.570

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.047 | 4.40 | 2347.40 | 2347.40 | 2347.40 | 2348.28 | .88 | 1.56 | .07 | 2344.00 |
| 2152.0 | 40.7 | 914.1 | 1197.2 | 10.6 | 86.4 | 298.7 | 38.2 | 20.7 | 2344.00 |
| .14 | 3.84 | 10.58 | 4.01 | .050 | .030 | .050 | .000 | 2343.00 | 980.77 |
| .007187 | 205. | 220. | 265. | 0 | 11 | 0 | .00 | 227.57 | 1208.34 |

*SECNO 3.113

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 973.5 1046.3 TYPE= 1 TARGET= 72.760
FLYING E TANK - NO DESIGN OR CONSTRUCTION INFORMATION AVAILABLE FOR
LOW DAM FORMING TANK: NOT DEPENDABLE FOR FLOOD RISK PLANNING.
SECTION 3.200 IS CONTROL SECTION FOR PONDING IN TANK.
MAP PROVIDES TWO WATER SURFACE ELEVATIONS. TANK WSEL IS THE
EG ELEVATION AT THE CONTROL SECTION (2359.00 FT). CHANNEL WSELs
FROM NORMAL ANALYSIS WITH ENCROACHMENT AT 950 (THIS SECTION) TO
OMIT TANK FROM FLOW AREA.
ENTIRE INUNDATED AREA AND DAM INCLUDED IN AE ZONE.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.113 | 5.11 | 2352.61 | 2352.61 | 2352.61 | 2354.39 | 1.77 | 2.41 | .27 | 2347.50 |
| 2152.0 | 623.3 | 1308.7 | 220.0 | 94.6 | 102.3 | 47.9 | 40.4 | 21.7 | 2347.50 |
| .15 | 6.59 | 12.80 | 4.59 | .050 | .030 | .050 | .000 | 2347.50 | 973.52 |
| .007573 | 370. | 350. | 270. | 0 | 8 | 0 | .00 | 72.76 | 1046.28 |

*SECNO 3.200

HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 924.9 1164.9 TYPE= 1 TARGET= 239.950
FLYING E TANK OVERFLOW

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.200 | 3.18 | 2358.18 | 2358.18 | 2358.16 | 2359.00 | .83 | 3.81 | .09 | 2355.00 |
| 2152.0 | 444.0 | 946.3 | 761.8 | 105.1 | 95.3 | 182.9 | 43.9 | 23.5 | 2355.00 |
| .17 | 4.22 | 9.93 | 4.17 | .050 | .030 | .050 | .000 | 2355.00 | 924.94 |
| .008617 | 390. | 460. | 590. | 0 | 14 | 0 | .00 | 239.95 | 1164.89 |

*SECNO 3.261

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 1.56

3470 ENCROACHMENT STATIONS= 815.5 1089.9 TYPE= 1 TARGET= 274.400

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.261 | 3.85 | 2360.35 | 2359.60 | 2360.35 | 2360.68 | .33 | 1.63 | .05 | 2358.00 |
| 2152.0 | 1249.8 | 722.2 | 180.0 | 389.4 | 108.8 | 81.6 | 47.3 | 25.3 | 2358.00 |
| .19 | 3.21 | 6.64 | 2.21 | .050 | .030 | .050 | .000 | 2356.50 | 815.54 |
| .003549 | 330. | 320. | 250. | 2 | 5 | 0 | .00 | 274.26 | 1089.80 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 3.308
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 720.4 1022.6 TYPE= 1 TARGET= 302.190

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.308 | 3.14 | 2362.14 | 2362.14 | 2362.14 | 2362.83 | .69 | 1.33 | .11 | 2359.30 |
| 2152.0 | 1230.1 | 796.3 | 125.6 | 326.7 | 81.9 | 26.6 | 50.2 | 26.9 | 2359.30 |
| .20 | 3.77 | 9.73 | 4.72 | .050 | .030 | .050 | .000 | 2359.00 | 720.38 |
| .008917 | 250. | 250. | 250. | 0 | 15 | 0 | .00 | 302.17 | 1022.56 |

*SECNO 3.355

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 648.7 1062.2 TYPE= 1 TARGET= 413.490
CONFLUENCE OF UPPER FLYING E WASH AND HOLLY WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.355 | 3.21 | 2365.71 | 2365.71 | 2365.70 | 2366.26 | .56 | 2.09 | .01 | 2362.80 |
| 2152.0 | 1148.0 | 666.0 | 338.0 | 351.9 | 70.7 | 80.1 | 52.8 | 28.9 | 2362.80 |
| .21 | 3.26 | 9.42 | 4.22 | .050 | .030 | .050 | .000 | 2362.50 | 648.70 |
| .008227 | 240. | 250. | 245. | 0 | 5 | 0 | .00 | 393.05 | 1062.19 |

*SECNO 3.454

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 626.2 1222.5 TYPE= 1 TARGET= 596.230
UPPER FLYING E WASH/HOLLY WASH CONFLUENCE
HYDRAULIC CONTROL LINE IS AT STATION 1000.0

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.454 | 3.28 | 2371.78 | 2371.78 | 2371.78 | 2372.24 | .46 | 5.72 | .01 | 2370.50 |
| 2152.0 | 1325.8 | 173.7 | 652.5 | 303.8 | 21.8 | 99.9 | 57.9 | 33.3 | 2370.50 |
| .24 | 4.36 | 7.97 | 6.53 | .050 | .030 | .050 | .000 | 2368.50 | 626.24 |
| .018614 | 450. | 520. | 530. | 0 | 5 | 0 | .00 | 430.48 | 1222.47 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 3.549

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = .55

3470 ENCROACHMENT STATIONS= 804.3 1155.2 TYPE= 1 TARGET= 350.860

UPPER FLYING E WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.549 | 2.04 | 2380.04 | 2379.87 | 2380.04 | 2380.26 | .22 | 7.99 | .02 | 2378.80 |
| 896.0 | 389.7 | 140.5 | 365.8 | 125.7 | 21.8 | 127.2 | 62.0 | 37.9 | 2378.80 |
| .28 | 3.10 | 6.44 | 2.88 | .050 | .030 | .050 | .000 | 2378.00 | 804.32 |
| .010732 | 525. | 500. | 500. | 4 | 14 | 0 | .00 | 350.86 | 1155.18 |

*SECNO 3.643

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 719.3 1051.3 TYPE= 1 TARGET= 331.980

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.643 | 2.54 | 2387.54 | 2387.54 | 2387.54 | 2388.00 | .46 | 4.50 | .07 | 2385.50 |
| 896.0 | 425.9 | 375.8 | 94.3 | 157.3 | 48.3 | 32.6 | 65.0 | 41.4 | 2385.50 |
| .30 | 2.71 | 7.78 | 2.89 | .050 | .030 | .050 | .000 | 2385.00 | 719.32 |
| .007633 | 505. | 500. | 495. | 0 | 11 | 0 | .00 | 263.83 | 1051.28 |

*SECNO 3.740

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 746.9 1027.1 TYPE= 1 TARGET= 280.160

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.740 | 2.56 | 2395.56 | 2395.56 | 2395.56 | 2395.98 | .42 | 3.91 | .00 | 2393.50 |
| 896.0 | 461.6 | 350.1 | 84.3 | 185.8 | 46.0 | 23.6 | 67.8 | 44.5 | 2393.50 |
| .34 | 2.48 | 7.61 | 3.58 | .050 | .030 | .050 | .000 | 2393.00 | 746.92 |
| .007771 | 505. | 510. | 510. | 0 | 5 | 0 | .00 | 258.55 | 1027.08 |

*SECNO 3.838

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 638.5 1021.6 TYPE= 1 TARGET= 383.070

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.838 | 2.21 | 2404.71 | 2404.71 | 2404.74 | 2405.08 | .37 | 4.45 | .01 | 2403.00 |
| 896.0 | 570.4 | 295.7 | 30.0 | 214.2 | 39.3 | 9.8 | 71.0 | 48.1 | 2403.00 |
| .37 | 2.66 | 7.52 | 3.06 | .050 | .030 | .050 | .000 | 2402.50 | 638.92 |
| .009394 | 525. | 520. | 515. | 0 | 9 | 0 | .00 | 351.51 | 1021.43 |

*SECNO 3.950
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 989.2 1081.5 TYPE= 1 TARGET= 92.230

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.950 | 3.58 | 2415.08 | 2415.08 | 2415.08 | 2415.94 | .86 | 5.19 | .15 | 2412.00 |
| 896.0 | 33.4 | 427.8 | 434.8 | 8.9 | 43.2 | 107.5 | 73.9 | 51.2 | 2412.00 |
| .39 | 3.75 | 9.91 | 4.05 | .050 | .030 | .050 | .000 | 2411.50 | 989.23 |
| .008101 | 600. | 590. | 600. | 0 | 14 | 0 | .00 | 92.23 | 1081.46 |

*SECNO 3.980
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 983.1 1065.8 TYPE= 1 TARGET= 82.730

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 3.980 | 4.18 | 2417.68 | 2417.68 | 2417.67 | 2418.65 | .97 | 1.14 | .03 | 2415.00 |
| 896.0 | 39.1 | 653.9 | 203.0 | 11.7 | 72.2 | 63.9 | 74.4 | 51.5 | 2415.00 |
| .40 | 3.34 | 9.05 | 3.18 | .050 | .030 | .050 | .000 | 2413.50 | 983.07 |
| .006633 | 160. | 160. | 150. | 0 | 11 | 0 | .00 | 82.73 | 1065.80 |

*SECNO 4.032
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 934.2 1031.5 TYPE= 1 TARGET= 97.300

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.032 | 3.60 | 2422.60 | 2422.60 | 2422.59 | 2423.51 | .91 | 1.86 | .01 | 2419.50 |
| 896.0 | 196.2 | 508.9 | 190.9 | 55.4 | 53.4 | 42.0 | 75.3 | 52.0 | 2419.50 |
| .41 | 3.54 | 9.53 | 4.54 | .050 | .030 | .050 | .000 | 2419.00 | 934.21 |
| .007444 | 290. | 270. | 235. | 0 | 15 | 0 | .00 | 97.30 | 1031.51 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 4.103
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 922.2 1073.7 TYPE= 1 TARGET= 151.470
DOWNSTREAM OF GEORGE'S TANK DAM EMBANKMENT

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.103 | 2.37 | 2428.37 | 2428.37 | 2428.37 | 2428.94 | .57 | 3.24 | .03 | 2426.30 |
| 896.0 | 270.6 | 375.4 | 250.0 | 79.9 | 44.4 | 73.9 | 76.8 | 53.1 | 2426.30 |
| .43 | 3.39 | 8.45 | 3.38 | .050 | .030 | .050 | .000 | 2426.00 | 922.23 |
| .010056 | 355. | 375. | 405. | 0 | 14 | 0 | .00 | 151.47 | 1073.70 |

*SECNO 4.168
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 875.8 1064.7 TYPE= 1 TARGET= 188.970
UPSTREAM OF GEORGE'S TANK DAM EMBANKMENT
GEORGE'S TANK - NO DESIGN OR CONSTRUCTION DATA AVAILABLE FOR
DAM FORMING TANK: NOT DEPENDABLE FOR FLOOD RISK PLANNING.
EXCESS FLOWS BREAK INTO SMALL CHANNEL ALONG WEST EDGE OF TANK OVER
A WIDE, FLAT SADDLE. SMALL CHANNEL ANALYZED AND SUBMITTED SEPARATELY
AS A ZONE A UNDER THE TITLE "GEORGE'S TANK BREAKOUT".

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.168 | 1.94 | 2434.34 | 2434.34 | 2434.34 | 2434.82 | .48 | 3.85 | .01 | 2432.50 |
| 896.0 | 421.2 | 305.1 | 169.7 | 120.5 | 36.8 | 51.9 | 78.4 | 54.5 | 2432.70 |
| .45 | 3.50 | 8.30 | 3.27 | .050 | .030 | .050 | .000 | 2432.40 | 875.77 |
| .012454 | 345. | 345. | 345. | 0 | 15 | 0 | .00 | 188.94 | 1064.71 |

*SECNO 4.213

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.53

3470 ENCROACHMENT STATIONS= 888.2 1056.1 TYPE= 1 TARGET= 167.980
LOWER PORTION OF GEORGE'S TANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.213 | 4.11 | 2435.61 | 2434.73 | 2435.61 | 2435.82 | .20 | .97 | .03 | 2432.00 |
| 896.0 | 371.6 | 311.1 | 213.4 | 180.2 | 58.0 | 91.5 | 79.9 | 55.5 | 2432.00 |
| .47 | 2.06 | 5.37 | 2.33 | .050 | .030 | .050 | .000 | 2431.50 | 888.16 |
| .001941 | 270. | 235. | 195. | 4 | 14 | 0 | .00 | 167.98 | 1056.14 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 4.301
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 900.3 1071.3 TYPE= 1 TARGET= 171.040
UPPER PORTION OF GEORGE'S TANK

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.301 | 1.88 | 2442.88 | 2442.88 | 2442.87 | 2443.41 | .53 | 1.90 | .10 | 2441.20 |
| 896.0 | 357.6 | 301.3 | 237.1 | 91.4 | 35.6 | 62.1 | 82.7 | 57.3 | 2441.20 |
| .49 | 3.91 | 8.47 | 3.82 | .050 | .030 | .050 | .000 | 2441.00 | 900.30 |
| .013585 | 465. | 465. | 465. | 0 | 14 | 0 | .00 | 171.04 | 1071.34 |

*SECNO 4.384
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 935.4 1041.2 TYPE= 1 TARGET= 105.800

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.384 | 2.50 | 2449.50 | 2449.50 | 2449.49 | 2450.24 | .74 | 5.10 | .06 | 2447.30 |
| 896.0 | 280.2 | 425.7 | 190.1 | 68.8 | 47.0 | 45.9 | 84.4 | 58.6 | 2447.30 |
| .51 | 4.07 | 9.05 | 4.14 | .050 | .030 | .050 | .000 | 2447.00 | 935.37 |
| .010683 | 405. | 440. | 430. | 0 | 11 | 0 | .00 | 105.80 | 1041.17 |

*SECNO 4.493
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 941.8 1265.8 TYPE= 1 TARGET= 324.010

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.493 | 1.68 | 2458.68 | 2458.68 | 2458.64 | 2459.00 | .32 | 6.51 | .04 | 2457.40 |
| 896.0 | 82.5 | 224.5 | 589.0 | 29.0 | 30.5 | 194.2 | 87.1 | 61.4 | 2457.10 |
| .55 | 2.84 | 7.35 | 3.03 | .050 | .030 | .050 | .000 | 2457.00 | 941.83 |
| .012539 | 465. | 575. | 600. | 0 | 18 | 0 | .00 | 324.01 | 1265.84 |

*SECNO 4.594

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 795.8 1337.4 TYPE= 1 TARGET= 541.530

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.594 | 1.34 | 2467.34 | 2467.34 | 2467.37 | 2467.71 | .37 | 8.55 | .02 | 2466.50 |
| 896.0 | 350.8 | 169.1 | 376.1 | 89.3 | 22.1 | 95.3 | 89.9 | 65.1 | 2466.50 |
| .58 | 3.93 | 7.67 | 3.95 | .050 | .030 | .050 | .000 | 2466.00 | 797.80 |
| .021751 | 520. | 530. | 530. | 0 | 15 | 0 | .00 | 293.74 | 1336.73 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 4.688
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 791.7 1013.0 TYPE= 1 TARGET= 221.340

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.688 | 2.62 | 2475.62 | 2475.62 | 2475.61 | 2476.06 | .44 | 6.93 | .02 | 2473.90 |
| 896.0 | 577.8 | 297.8 | 20.4 | 183.0 | 36.9 | 7.5 | 92.2 | 67.9 | 2473.90 |
| .61 | 3.16 | 8.07 | 2.72 | .050 | .030 | .050 | .000 | 2473.00 | 791.68 |
| .010442 | 440. | 500. | 530. | 0 | 17 | 0 | .00 | 221.34 | 1013.02 |

*SECNO 4.787

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 637.9 1035.6 TYPE= 1 TARGET= 397.650

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.787 | 2.21 | 2484.21 | 2484.21 | 2484.24 | 2484.60 | .38 | 5.72 | .01 | 2482.70 |
| 896.0 | 541.6 | 297.8 | 56.6 | 193.5 | 39.1 | 19.0 | 95.3 | 71.4 | 2482.70 |
| .64 | 2.80 | 7.62 | 2.98 | .050 | .030 | .050 | .000 | 2482.00 | 639.09 |
| .010170 | 580. | 520. | 470. | 0 | 9 | 0 | .00 | 306.86 | 1035.21 |

*SECNO 4.881

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 972.0 1346.2 TYPE= 1 TARGET= 374.220

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 4.881 | 2.55 | 2489.55 | 2489.55 | 2489.54 | 2490.12 | .57 | 4.99 | .06 | 2487.70 |
| 896.0 | 66.0 | 371.6 | 458.3 | 18.0 | 43.6 | 135.2 | 97.8 | 74.0 | 2487.70 |
| .67 | 3.67 | 8.52 | 3.39 | .050 | .030 | .050 | .000 | 2487.00 | 971.98 |
| .010275 | 470. | 500. | 495. | 0 | 8 | 0 | .00 | 161.09 | 1346.20 |

*SECNO 5.014
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3470 ENCROACHMENT STATIONS= 960.0 1090.1 TYPE= 1 TARGET= 130.120

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.014 | 3.01 | 2500.01 | 2500.01 | 2500.01 | 2500.71 | .70 | 6.66 | .04 | 2497.50 |
| 896.0 | 165.3 | 463.5 | 267.3 | 42.5 | 53.3 | 83.2 | 101.1 | 76.5 | 2497.50 |
| .70 | 3.89 | 8.70 | 3.21 | .050 | .030 | .050 | .000 | 2497.00 | 959.98 |
| .008083 | 485. | 700. | 850. | 0 | 11 | 0 | .00 | 130.12 | 1090.10 |

*SECNO 5.082
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 766.8 1048.8 TYPE= 1 TARGET= 281.950

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.082 | 2.55 | 2506.55 | 2506.55 | 2506.55 | 2506.97 | .42 | 2.84 | .03 | 2504.50 |
| 896.0 | 394.8 | 368.4 | 132.8 | 166.0 | 49.3 | 41.3 | 102.9 | 78.3 | 2504.50 |
| .72 | 2.38 | 7.47 | 3.22 | .050 | .030 | .050 | .000 | 2504.00 | 766.81 |
| .007536 | 410. | 360. | 310. | 0 | 9 | 0 | .00 | 281.93 | 1048.74 |

*SECNO 5.175

3685 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 732.8 1027.6 TYPE= 1 TARGET= 294.760

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.175 | 3.51 | 2514.51 | 2514.51 | 2514.51 | 2515.17 | .66 | 3.34 | .07 | 2511.50 |
| 896.0 | 277.2 | 477.8 | 141.1 | 100.8 | 57.0 | 36.4 | 105.5 | 81.1 | 2511.50 |
| .75 | 2.75 | 8.38 | 3.88 | .050 | .030 | .050 | .000 | 2511.00 | 732.80 |
| .005949 | 530. | 490. | 460. | 0 | 11 | 0 | .00 | 183.99 | 1027.56 |

*SECNO 5.279
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 976.3 1149.0 TYPE= 1 TARGET= 172.660

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 5.279 | 4.29 | 2522.29 | 2522.29 | 2522.29 | 2523.02 | .73 | 2.85 | .02 | 2519.00 |
| 896.0 | 62.7 | 615.3 | 218.0 | 20.0 | 75.7 | 96.1 | 108.0 | 83.3 | 2519.00 |
| .77 | 3.13 | 8.12 | 2.27 | .050 | .030 | .050 | .000 | 2518.00 | 976.31 |
| .004589 | 540. | 550. | 550. | 0 | 11 | 0 | .00 | 172.65 | 1148.95 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

```
*SECNO -3.454
START TRIB COMP
    -3.454     3.454  2371.781

3265 DIVIDED FLOW


3470 ENCROACHMENT STATIONS=      626.2    1222.5  TYPE=      1  TARGET=      596.230
          HOLLY WASH/FLYING E WASH CONFLUENCE
          HYDRAULIC CONTROL LINE IS AT STATION 1207.0
   -3.454      3.28   2371.78       .00   2371.78   2372.67       .89      5.15     -2.27   2369.00
   2152.0    1494.8     553.3     103.9     365.5      42.3      17.7     111.4      86.6   2369.00
      .79      4.09     13.07      5.87      .050      .030      .050      .000   2368.50    626.24
  .016004      450.      545.      530.         0         0         0       .00    430.48   1222.47


*SECNO  .198
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

ENCROACHMENT STATIONS=      906.8    1012.8  TYPE=      1  TARGET=      106.030
          HOLLY WASH
          HOLLY WASH RIVER MILES MEASURED FROM CONFLUENCE AT SECTION 3.355
     .198      4.53   2377.53   2377.53   2377.47   2378.55      1.02      5.42       .04   2374.30
   1361.0     509.8     807.1      44.1     139.5      80.2      12.0     115.2      89.7   2374.30
      .81      3.65     10.07      3.68      .050      .030      .050      .000   2373.00    906.79
  .006601      500.      500.      510.         0        14         0       .00    106.03   1012.82


*SECNO  .291
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      935.7    1024.7  TYPE=      1  TARGET=       89.080
     .291      3.92   2382.42   2382.42   2382.42   2383.56      1.14      3.70       .04   2379.00
   1361.0     583.3     687.5      90.2     116.2      62.3      20.2     117.6      90.8   2379.00
      .83      5.02     11.04      4.48      .050      .030      .050      .000   2378.50    935.66
  .008815      485.      490.      490.         0        15         0       .00     89.08   1024.74


*SECNO  .387
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 975.6 1028.7 TYPE= 1 TARGET= 53.020

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .387 | 4.73 | 2387.73 | 2387.73 | 2387.71 | 2389.38 | 1.65 | 4.26 | .15 | 2383.30 |
| 1361.0 | 278.1 | 871.9 | 211.0 | 45.9 | 71.8 | 41.1 | 119.7 | 91.6 | 2383.30 |
| .84 | 6.06 | 12.15 | 5.14 | .050 | .030 | .050 | .000 | 2383.00 | 975.64 |
| .007938 | 510. | 510. | 510. | 0 | 11 | 0 | .00 | 53.02 | 1028.66 |

*SECNO .482

3301 HV CHANGED MORE THAN HVINS

3470 ENCROACHMENT STATIONS= 932.0 1016.9 TYPE= 1 TARGET= 84.880

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .482 | 4.98 | 2391.98 | 2391.78 | 2392.00 | 2393.01 | 1.03 | 3.56 | .06 | 2390.00 |
| 1361.0 | 497.5 | 847.8 | 15.7 | 112.5 | 87.2 | 5.8 | 121.7 | 92.4 | 2390.00 |
| .86 | 4.42 | 9.72 | 2.70 | .050 | .030 | .050 | .000 | 2387.00 | 932.06 |
| .006575 | 485. | 500. | 485. | 2 | 5 | 0 | .00 | 84.78 | 1016.84 |

*SECNO .559

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 978.0 1022.0 TYPE= 1 TARGET= 44.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .559 | 4.71 | 2400.71 | 2400.71 | 2400.71 | 2402.28 | 1.58 | 3.23 | .16 | 2400.00 |
| 1361.0 | .0 | 1361.0 | .0 | .0 | 135.1 | .0 | 123.3 | 93.0 | 100000.00 |
| .87 | .00 | 10.07 | .00 | .000 | .030 | .000 | .000 | 2396.00 | 978.00 |
| .009902 | 405. | 405. | 405. | 0 | 11 | 0 | .00 | 44.00 | 1022.00 |

*SECNO .607
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

```
SECNO     DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
Q         QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


3470 ENCROACHMENT STATIONS=      972.0    1027.2  TYPE=      1  TARGET=      55.220
      .607      4.46   2403.46   2403.46   2403.46   2405.01      1.55      2.36       .00   2399.60
    1361.0     243.9     879.0     238.1      44.4      74.9      43.2     124.2      93.3   2399.60
       .88      5.49     11.74      5.51      .050      .030      .050      .000   2399.00    972.02
   .008412      290.      255.      265.         0        11         0       .00     55.20   1027.22


*SECNO  .681
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      966.8    1050.2  TYPE=      1  TARGET=      83.340
      .681      3.92   2406.92   2406.92   2406.91   2408.11      1.19      3.05       .04   2403.30
    1361.0     127.0     950.4     283.5      34.1      93.7      68.0     125.8      93.9   2403.50
       .89      3.72     10.14      4.17      .050      .030      .050      .000   2403.00    966.83
   .007282      390.      390.      390.         0        15         0       .00     83.34   1050.17


*SECNO  .747

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      973.3    1021.7  TYPE=      1  TARGET=      48.400
      .747      6.12   2411.12   2411.12   2411.12   2412.87      1.75      2.43       .17   2407.40
    1361.0     124.6    1131.0     105.4      28.5      98.4      25.1     127.2      94.4   2407.40
       .90      4.37     11.50      4.20      .050      .030      .050      .000   2405.00    973.30
   .006692      370.      350.      320.         0        14         0       .00     48.40   1021.70


*SECNO  .853

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      929.6    1032.4  TYPE=      1  TARGET=     102.730
      .853      3.77   2420.77   2420.77   2420.77   2421.78      1.01      4.34       .07   2417.50
    1361.0     531.6     563.7     265.7     113.5      50.7      49.9     129.4      95.3   2417.50
       .92      4.69     11.11      5.33      .050      .030      .050      .000   2417.00    929.63
   .009508      510.      560.      560.         0        14         0       .00    102.73   1032.36
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .954
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 962.0 1035.0 TYPE= 1 TARGET= 73.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .954 | 3.98 | 2432.98 | 2432.98 | 2433.00 | 2434.24 | 1.26 | 4.75 | .07 | 2429.80 |
| 1361.0 | 237.5 | 835.1 | 288.4 | 49.0 | 77.0 | 59.9 | 131.8 | 96.4 | 2429.80 |
| .94 | 4.84 | 10.85 | 4.81 | .050 | .030 | .050 | .000 | 2429.00 | 962.00 |
| .008786 | 440. | 530. | 605. | 0 | 8 | 0 | .00 | 73.00 | 1035.00 |

*SECNO 1.005

3301 HV CHANGED MORE THAN HVINS

3302 WARNING: CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE, KRATIO = 2.03

3470 ENCROACHMENT STATIONS= 941.0 1029.0 TYPE= 1 TARGET= 88.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.005 | 5.02 | 2435.02 | 2433.42 | 2434.87 | 2435.37 | .35 | 1.03 | .09 | 2430.50 |
| 1361.0 | 578.6 | 523.4 | 259.0 | 180.4 | 80.9 | 81.1 | 133.4 | 96.9 | 2430.50 |
| .95 | 3.21 | 6.47 | 3.19 | .050 | .030 | .050 | .000 | 2430.00 | 941.00 |
| .002136 | 280. | 270. | 255. | 2 | 15 | 0 | .00 | 88.00 | 1029.00 |

*SECNO 1.101

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 968.0 1043.0 TYPE= 1 TARGET= 75.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.101 | 3.64 | 2438.64 | 2438.64 | 2438.65 | 2439.87 | 1.22 | 2.02 | .26 | 2435.70 |
| 1361.0 | 173.9 | 732.7 | 454.4 | 35.8 | 66.4 | 82.4 | 136.5 | 97.8 | 2435.70 |
| .97 | 4.86 | 11.04 | 5.52 | .050 | .030 | .050 | .000 | 2435.00 | 968.48 |
| .010066 | 485. | 510. | 515. | 0 | 19 | 0 | .00 | 74.52 | 1043.00 |

*SECNO 1.202
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

```
ECNO      DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
Q         QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


3470 ENCROACHMENT STATIONS=      934.0    1030.0  TYPE=      1  TARGET=      96.000
     1.202      3.66   2449.66   2449.66   2449.65   2450.70      1.03      4.99       .02   2446.80
    1361.0     437.9     746.7     176.4     102.9      72.8      36.8     138.9      98.8   2446.80
       .99      4.25     10.26      4.80      .050      .030      .050      .000   2446.00    934.00
   .008907      510.      530.      540.         0         5         0       .00     96.00   1030.00


*SECNO 1.295
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      952.0    1058.0  TYPE=      1  TARGET=     106.000
     1.295      3.58   2455.58   2455.58   2455.57   2456.56       .98      4.36       .01   2452.70
    1361.0     239.2     720.8     401.1      56.6      71.2      89.0     141.3     100.0   2452.80
      1.01      4.23     10.12      4.50      .050      .030      .050      .000   2452.00    952.00
   .008851      490.      490.      495.         0         8         0       .00    106.00   1058.00


NO 1.399
MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      919.0    1030.0  TYPE=      1  TARGET=     111.000
     1.399      2.97   2463.97   2463.97   2463.96   2464.91       .94      5.40       .00   2461.50
    1361.0     502.5     672.3     186.2     112.6      66.9      39.4     144.1     101.4   2461.50
      1.03      4.46     10.04      4.72      .050      .030      .050      .000   2461.00    919.00
   .010773      580.      550.      530.         0        15         0       .00    111.00   1030.00


*SECNO 1.473
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      957.0    1050.0  TYPE=      1  TARGET=      93.000
     1.473      3.48   2469.48   2469.48   2469.53   2470.54      1.07      4.05       .04   2466.50
    1361.0     201.9     732.5     426.5      48.9      70.3      86.5     146.0     102.3   2466.50
      1.04      4.13     10.42      4.93      .050      .030      .050      .000   2466.00    957.00
   .009728      420.      395.      370.         0        11         0       .00     93.00   1050.00


*SECNO 1.576
7185 MINIMUM SPECIFIC ENERGY
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 970.0 1070.0 TYPE= 1 TARGET= 100.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.576 | 2.28 | 2476.28 | 2476.28 | 2476.01 | 2477.27 | .98 | 6.59 | .01 | 2474.00 |
| 1361.0 | 187.2 | 468.0 | 705.9 | 38.5 | 43.4 | 113.4 | 148.5 | 103.5 | 2474.00 |
| 1.06 | 4.87 | 10.79 | 6.23 | .050 | .030 | .050 | .000 | 2474.00 | 970.00 |
| .015808 | 520. | 540. | 545. | 0 | 14 | 0 | .00 | 100.00 | 1070.00 |

*SECNO 1.615
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 960.0 1025.0 TYPE= 1 TARGET= 65.000
SECTION TAKEN FROM TOPOGRAPHIC MAP

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.615 | 3.02 | 2482.02 | 2482.02 | 2481.86 | 2483.35 | 1.33 | 2.88 | .10 | 2479.00 |
| 1361.0 | 446.3 | 700.6 | 214.0 | 75.6 | 60.4 | 37.8 | 149.4 | 103.9 | 2479.00 |
| 1.07 | 5.91 | 11.60 | 5.66 | .050 | .030 | .050 | .000 | 2479.00 | 960.00 |
| .012575 | 205. | 205. | 205. | 0 | 11 | 0 | .00 | 65.00 | 1025.00 |

*SECNO 1.661

3301 HV CHANGED MORE THAN HVINS

3470 ENCROACHMENT STATIONS= 910.0 1041.0 TYPE= 1 TARGET= 131.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.661 | 3.11 | 2485.11 | 2484.74 | 2484.71 | 2485.65 | .53 | 2.21 | .08 | 2482.50 |
| 1361.0 | 662.9 | 484.8 | 213.2 | 166.2 | 58.7 | 56.7 | 150.6 | 104.4 | 2482.50 |
| 1.08 | 3.99 | 8.26 | 3.76 | .050 | .030 | .050 | .000 | 2482.00 | 910.00 |
| .006838 | 255. | 245. | 215. | 2 | 15 | 0 | .00 | 131.00 | 1041.00 |

*SECNO 1.767

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 950.0 1040.0 TYPE= 1 TARGET= 90.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.767 | 3.33 | 2493.33 | 2493.33 | 2493.17 | 2494.40 | 1.07 | 4.72 | .16 | 2490.60 |
| 1361.0 | 370.6 | 633.9 | 356.5 | 77.4 | 58.0 | 69.0 | 153.7 | 105.8 | 2490.50 |
| 1.10 | 4.79 | 10.92 | 5.17 | .050 | .030 | .050 | .000 | 2490.00 | 950.00 |
| .010999 | 540. | 560. | 560. | 0 | 8 | 0 | .00 | 90.00 | 1040.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.873

3301 HV CHANGED MORE THAN HVINS

3470 ENCROACHMENT STATIONS= 960.0 1115.0 TYPE= 1 TARGET= 155.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.873 | 2.22 | 2499.22 | 2498.84 | 2498.87 | 2499.66 | .44 | 5.20 | .06 | 2497.00 |
| 1361.0 | 263.0 | 412.1 | 685.9 | 68.9 | 54.4 | 168.1 | 156.9 | 107.4 | 2497.00 |
| 1.13 | 3.82 | 7.57 | 4.08 | .050 | .030 | .050 | .000 | 2497.00 | 960.00 |
| .008058 | 500. | 560. | 585. | 3 | 11 | 0 | .00 | 155.00 | 1115.00 |

THIS RUN EXECUTED 05AUG92 11:43:47

**********
HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991
**********

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

AB: UPPER FLYING E WASH

SUMMARY PRINTOUT TABLE 150

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 2.435 | .00 | .00 | .00 | 2303.50 | 6943.00 | 2309.87 | 2309.87 | 2311.91 | 81.13 | 14.89 | 739.77 | 770.81 |
| * | 2.435 | .00 | .00 | .00 | 2303.50 | 6943.00 | 2309.91 | 2309.80 | 2312.10 | 83.74 | 15.19 | 701.30 | 758.71 |
| * | 2.539 | 550.00 | .00 | .00 | 2309.00 | 6943.00 | 2315.51 | 2315.51 | 2316.75 | 79.25 | 9.41 | 847.02 | 779.93 |
| * | 2.539 | 550.00 | .00 | .00 | 2309.00 | 6943.00 | 2315.51 | 2315.51 | 2316.75 | 79.90 | 9.43 | 843.65 | 776.75 |
| | 2.630 | 480.00 | .00 | .00 | 2315.00 | 2152.00 | 2319.19 | 2317.86 | 2319.65 | 29.56 | 6.77 | 451.44 | 395.85 |
| * | 2.630 | 480.00 | .00 | .00 | 2315.00 | 2152.00 | 2319.20 | 2317.86 | 2319.66 | 29.28 | 6.75 | 452.81 | 397.70 |
| * | 2.725 | 500.00 | .00 | .00 | 2322.00 | 2152.00 | 2325.77 | 2325.77 | 2326.90 | 128.47 | 10.35 | 280.34 | 189.86 |
| * | 2.725 | 500.00 | .00 | .00 | 2322.00 | 2152.00 | 2325.77 | 2325.77 | 2326.90 | 127.47 | 10.33 | 281.20 | 190.61 |
| * | 2.812 | 460.00 | .00 | .00 | 2327.50 | 2152.00 | 2331.06 | 2331.06 | 2331.66 | 55.96 | 8.37 | 517.00 | 287.68 |
| * | 2.812 | 460.00 | .00 | .00 | 2327.50 | 2152.00 | 2331.06 | 2331.06 | 2331.66 | 55.91 | 8.37 | 517.21 | 287.80 |
| * | 2.922 | 580.00 | .00 | .00 | 2334.00 | 2152.00 | 2337.68 | 2337.68 | 2338.44 | 81.61 | 9.65 | 424.94 | 238.21 |
| * | 2.922 | 580.00 | .00 | .00 | 2334.00 | 2152.00 | 2337.68 | 2337.68 | 2338.44 | 80.80 | 9.62 | 426.59 | 239.41 |
| * | 3.005 | 440.00 | .00 | .00 | 2340.50 | 2152.00 | 2344.12 | 2344.12 | 2344.78 | 58.85 | 8.61 | 499.00 | 280.53 |
| * | 3.005 | 440.00 | .00 | .00 | 2340.50 | 2152.00 | 2344.12 | 2344.12 | 2344.78 | 59.30 | 8.64 | 497.28 | 279.46 |
| * | 3.047 | 220.00 | .00 | .00 | 2343.00 | 2152.00 | 2347.40 | 2347.40 | 2348.28 | 71.94 | 10.58 | 395.59 | 253.72 |
| * | 3.047 | 220.00 | .00 | .00 | 2343.00 | 2152.00 | 2347.40 | 2347.40 | 2348.28 | 71.87 | 10.58 | 395.76 | 253.84 |
| * | 3.113 | 350.00 | .00 | .00 | 2347.50 | 2152.00 | 2352.61 | 2352.61 | 2354.39 | 75.88 | 12.80 | 244.65 | 247.05 |
| * | 3.113 | 350.00 | .00 | .00 | 2347.50 | 2152.00 | 2352.61 | 2352.61 | 2354.39 | 75.73 | 12.80 | 244.82 | 247.28 |
| * | 3.200 | 460.00 | .00 | .00 | 2355.00 | 2152.00 | 2358.16 | 2358.16 | 2359.00 | 87.55 | 9.99 | 380.77 | 230.00 |
| * | 3.200 | 460.00 | .00 | .00 | 2355.00 | 2152.00 | 2358.18 | 2358.18 | 2359.00 | 86.17 | 9.93 | 383.28 | 231.83 |
| * | 3.261 | 320.00 | .00 | .00 | 2356.50 | 2152.00 | 2360.35 | 2359.61 | 2360.68 | 35.24 | 6.62 | 581.30 | 362.52 |
| | 3.261 | 320.00 | .00 | .00 | 2356.50 | 2152.00 | 2360.35 | 2359.60 | 2360.68 | 35.49 | 6.64 | 579.83 | 361.23 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 3.308 | 250.00 | .00 | .00 | 2359.00 | 2152.00 | 2362.14 | 2362.14 | 2362.83 | 88.82 | 9.71 | 435.86 | 228.34 |
| * | 3.308 | 250.00 | .00 | .00 | 2359.00 | 2152.00 | 2362.14 | 2362.14 | 2362.83 | 89.17 | 9.73 | 435.19 | 227.90 |
| * | 3.355 | 250.00 | .00 | .00 | 2362.50 | 2152.00 | 2365.70 | 2365.70 | 2366.26 | 82.63 | 9.43 | 501.84 | 236.74 |
| * | 3.355 | 250.00 | .00 | .00 | 2362.50 | 2152.00 | 2365.71 | 2365.71 | 2366.26 | 82.27 | 9.42 | 502.70 | 237.26 |
| * | 3.454 | 520.00 | .00 | .00 | 2368.50 | 2152.00 | 2371.78 | 2371.78 | 2372.24 | 185.91 | 7.97 | 425.70 | 157.83 |
| * | 3.454 | 520.00 | .00 | .00 | 2368.50 | 2152.00 | 2371.78 | 2371.78 | 2372.24 | 186.14 | 7.97 | 425.49 | 157.73 |
| * | 3.549 | 500.00 | .00 | .00 | 2378.00 | 896.00 | 2380.04 | 2379.87 | 2380.26 | 107.50 | 6.44 | 274.49 | 86.42 |
| * | 3.549 | 500.00 | .00 | .00 | 2378.00 | 896.00 | 2380.04 | 2379.87 | 2380.26 | 107.32 | 6.44 | 274.66 | 86.49 |
| * | 3.643 | 500.00 | .00 | .00 | 2385.00 | 896.00 | 2387.54 | 2387.54 | 2388.00 | 76.19 | 7.77 | 238.42 | 102.65 |
| * | 3.643 | 500.00 | .00 | .00 | 2385.00 | 896.00 | 2387.54 | 2387.54 | 2388.00 | 76.33 | 7.78 | 238.22 | 102.56 |
| * | 3.740 | 510.00 | .00 | .00 | 2393.00 | 896.00 | 2395.56 | 2395.56 | 2395.98 | 77.81 | 7.61 | 255.30 | 101.58 |
| * | 3.740 | 510.00 | .00 | .00 | 2393.00 | 896.00 | 2395.56 | 2395.56 | 2395.98 | 77.71 | 7.61 | 255.43 | 101.64 |
| * | 3.838 | 520.00 | .00 | .00 | 2402.50 | 896.00 | 2404.74 | 2404.74 | 2405.08 | 86.76 | 7.29 | 272.25 | 96.19 |
| * | 3.838 | 520.00 | .00 | .00 | 2402.50 | 896.00 | 2404.71 | 2404.71 | 2405.08 | 93.94 | 7.52 | 263.31 | 92.44 |
| * | 3.950 | 590.00 | .00 | .00 | 2411.50 | 896.00 | 2415.08 | 2415.08 | 2415.94 | 81.39 | 9.92 | 159.27 | 99.32 |
| * | 3.950 | 590.00 | .00 | .00 | 2411.50 | 896.00 | 2415.08 | 2415.08 | 2415.94 | 81.01 | 9.91 | 159.56 | 99.55 |
| | 3.980 | 160.00 | .00 | .00 | 2413.50 | 896.00 | 2417.67 | 2417.67 | 2418.65 | 66.53 | 9.06 | 147.60 | 109.85 |
| | 3.980 | 160.00 | .00 | .00 | 2413.50 | 896.00 | 2417.68 | 2417.68 | 2418.65 | 66.33 | 9.05 | 147.78 | 110.01 |
| * | 4.032 | 270.00 | .00 | .00 | 2419.00 | 896.00 | 2422.59 | 2422.59 | 2423.51 | 74.64 | 9.54 | 150.63 | 103.71 |
| * | 4.032 | 270.00 | .00 | .00 | 2419.00 | 896.00 | 2422.60 | 2422.60 | 2423.51 | 74.44 | 9.53 | 150.82 | 103.85 |
| * | 4.103 | 375.00 | .00 | .00 | 2426.00 | 896.00 | 2428.37 | 2428.37 | 2428.94 | 100.78 | 8.46 | 198.08 | 89.25 |
| * | 4.103 | 375.00 | .00 | .00 | 2426.00 | 896.00 | 2428.37 | 2428.37 | 2428.94 | 100.56 | 8.45 | 198.22 | 89.35 |
| * | 4.168 | 345.00 | .00 | .00 | 2432.40 | 896.00 | 2434.34 | 2434.34 | 2434.82 | 124.21 | 8.29 | 209.34 | 80.39 |
| * | 4.168 | 345.00 | .00 | .00 | 2432.40 | 896.00 | 2434.34 | 2434.34 | 2434.82 | 124.54 | 8.30 | 209.15 | 80.29 |
| * | 4.213 | 235.00 | .00 | .00 | 2431.50 | 896.00 | 2435.61 | 2434.73 | 2435.82 | 19.42 | 5.37 | 329.58 | 203.30 |
| * | 4.213 | 235.00 | .00 | .00 | 2431.50 | 896.00 | 2435.61 | 2434.73 | 2435.82 | 19.41 | 5.37 | 329.66 | 203.37 |
| * | 4.301 | 465.00 | .00 | .00 | 2441.00 | 896.00 | 2442.87 | 2442.87 | 2443.41 | 138.32 | 8.53 | 187.88 | 76.18 |
| * | 4.301 | 465.00 | .00 | .00 | 2441.00 | 896.00 | 2442.88 | 2442.88 | 2443.41 | 135.85 | 8.47 | 189.09 | 76.88 |
| * | 4.384 | 440.00 | .00 | .00 | 2447.00 | 896.00 | 2449.49 | 2449.49 | 2450.24 | 108.86 | 9.11 | 160.64 | 85.88 |
| * | 4.384 | 440.00 | .00 | .00 | 2447.00 | 896.00 | 2449.50 | 2449.50 | 2450.24 | 106.83 | 9.05 | 161.73 | 86.69 |
| * | 4.493 | 575.00 | .00 | .00 | 2457.00 | 896.00 | 2458.64 | 2458.64 | 2459.00 | 142.51 | 7.72 | 242.27 | 75.06 |
| * | 4.493 | 575.00 | .00 | .00 | 2457.00 | 896.00 | 2458.68 | 2458.68 | 2459.00 | 125.39 | 7.35 | 253.82 | 80.02 |
| | 4.594 | 530.00 | .00 | .00 | 2466.00 | 896.00 | 2467.37 | 2467.34 | 2467.71 | 193.56 | 7.37 | 216.03 | 64.40 |
| | 4.594 | 530.00 | .00 | .00 | 2466.00 | 896.00 | 2467.34 | 2467.34 | 2467.71 | 217.51 | 7.67 | 206.68 | 60.75 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 4.688 | 500.00 | .00 | .00 | 2473.00 | 896.00 | 2475.61 | 2475.61 | 2476.06 | 107.07 | 8.15 | 225.33 | 86.59 |
| * | 4.688 | 500.00 | .00 | .00 | 2473.00 | 896.00 | 2475.62 | 2475.62 | 2476.06 | 104.42 | 8.07 | 227.38 | 87.68 |
| * | 4.787 | 520.00 | .00 | .00 | 2482.00 | 896.00 | 2484.24 | 2484.24 | 2484.60 | 94.65 | 7.41 | 258.85 | 92.10 |
| * | 4.787 | 520.00 | .00 | .00 | 2482.00 | 896.00 | 2484.21 | 2484.21 | 2484.60 | 101.70 | 7.62 | 251.61 | 88.85 |
| * | 4.881 | 500.00 | .00 | .00 | 2487.00 | 896.00 | 2489.54 | 2489.54 | 2490.12 | 104.62 | 8.57 | 195.51 | 87.60 |
| * | 4.881 | 500.00 | .00 | .00 | 2487.00 | 896.00 | 2489.55 | 2489.55 | 2490.12 | 102.75 | 8.52 | 196.85 | 88.39 |
| * | 5.014 | 700.00 | .00 | .00 | 2497.00 | 896.00 | 2500.01 | 2500.01 | 2500.71 | 81.08 | 8.71 | 178.75 | 99.51 |
| * | 5.014 | 700.00 | .00 | .00 | 2497.00 | 896.00 | 2500.01 | 2500.01 | 2500.71 | 80.83 | 8.70 | 178.97 | 99.66 |
| * | 5.082 | 360.00 | .00 | .00 | 2504.00 | 896.00 | 2506.55 | 2506.55 | 2506.97 | 75.75 | 7.49 | 256.02 | 102.95 |
| * | 5.082 | 360.00 | .00 | .00 | 2504.00 | 896.00 | 2506.55 | 2506.55 | 2506.97 | 75.36 | 7.47 | 256.57 | 103.22 |
| * | 5.175 | 490.00 | .00 | .00 | 2511.00 | 896.00 | 2514.51 | 2514.51 | 2515.17 | 59.69 | 8.39 | 193.78 | 115.98 |
| * | 5.175 | 490.00 | .00 | .00 | 2511.00 | 896.00 | 2514.51 | 2514.51 | 2515.17 | 59.49 | 8.38 | 194.13 | 116.17 |
| * | 5.279 | 550.00 | .00 | .00 | 2518.00 | 896.00 | 2522.29 | 2522.29 | 2523.02 | 45.80 | 8.12 | 192.12 | 132.39 |
| * | 5.279 | 550.00 | .00 | .00 | 2518.00 | 896.00 | 2522.29 | 2522.29 | 2523.02 | 45.89 | 8.12 | 191.90 | 132.27 |
| | -3.454 | 545.00 | .00 | .00 | 2368.50 | 2152.00 | 2371.78 | .00 | 2372.67 | 159.85 | 13.07 | 425.70 | 170.21 |
| | -3.454 | 545.00 | .00 | .00 | 2368.50 | 2152.00 | 2371.78 | .00 | 2372.67 | 160.04 | 13.07 | 425.49 | 170.11 |
| | .198 | 500.00 | .00 | .00 | 2373.00 | 1361.00 | 2377.47 | 2377.47 | 2378.51 | 69.18 | 10.21 | 231.93 | 163.63 |
| | .198 | 500.00 | .00 | .00 | 2373.00 | 1361.00 | 2377.53 | 2377.53 | 2378.55 | 66.01 | 10.07 | 231.61 | 167.51 |
| * | .291 | 490.00 | .00 | .00 | 2378.50 | 1361.00 | 2382.42 | 2382.42 | 2383.56 | 88.61 | 11.06 | 198.25 | 144.59 |
| * | .291 | 490.00 | .00 | .00 | 2378.50 | 1361.00 | 2382.42 | 2382.42 | 2383.56 | 88.15 | 11.04 | 198.64 | 144.96 |
| * | .387 | 510.00 | .00 | .00 | 2383.00 | 1361.00 | 2387.71 | 2387.71 | 2389.38 | 81.05 | 12.23 | 157.46 | 151.18 |
| * | .387 | 510.00 | .00 | .00 | 2383.00 | 1361.00 | 2387.73 | 2387.73 | 2389.38 | 79.38 | 12.15 | 158.74 | 152.75 |
| | .482 | 500.00 | .00 | .00 | 2387.00 | 1361.00 | 2392.00 | 2391.79 | 2393.01 | 64.49 | 9.66 | 206.98 | 169.48 |
| | .482 | 500.00 | .00 | .00 | 2387.00 | 1361.00 | 2391.98 | 2391.78 | 2393.01 | 65.75 | 9.72 | 205.43 | 167.85 |
| * | .559 | 405.00 | .00 | .00 | 2396.00 | 1361.00 | 2400.71 | 2400.71 | 2402.28 | 99.20 | 10.08 | 135.02 | 136.65 |
| * | .559 | 405.00 | .00 | .00 | 2396.00 | 1361.00 | 2400.71 | 2400.71 | 2402.28 | 99.02 | 10.07 | 135.10 | 136.77 |
| * | .607 | 255.00 | .00 | .00 | 2399.00 | 1361.00 | 2403.46 | 2403.46 | 2405.01 | 84.10 | 11.74 | 162.56 | 148.41 |
| * | .607 | 255.00 | .00 | .00 | 2399.00 | 1361.00 | 2403.46 | 2403.46 | 2405.01 | 84.12 | 11.74 | 162.55 | 148.39 |
| | .681 | 390.00 | .00 | .00 | 2403.00 | 1361.00 | 2406.91 | 2406.88 | 2408.11 | 73.51 | 10.18 | 195.15 | 158.74 |
| * | .681 | 390.00 | .00 | .00 | 2403.00 | 1361.00 | 2406.92 | 2406.92 | 2408.11 | 72.82 | 10.14 | 195.84 | 159.49 |
| * | .747 | 350.00 | .00 | .00 | 2405.00 | 1361.00 | 2411.12 | 2411.12 | 2412.87 | 66.86 | 11.49 | 152.04 | 166.44 |
| * | .747 | 350.00 | .00 | .00 | 2405.00 | 1361.00 | 2411.12 | 2411.12 | 2412.87 | 66.92 | 11.50 | 151.99 | 166.38 |
| * | .853 | 560.00 | .00 | .00 | 2417.00 | 1361.00 | 2420.77 | 2420.77 | 2421.78 | 95.20 | 11.12 | 213.95 | 139.49 |
| | .853 | 560.00 | .00 | .00 | 2417.00 | 1361.00 | 2420.77 | 2420.77 | 2421.78 | 95.08 | 11.11 | 214.05 | 139.58 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | .954 | 530.00 | .00 | .00 | 2429.00 | 1361.00 | 2433.00 | 2433.00 | 2434.16 | 82.02 | 10.53 | 197.53 | 150.28 |
| * | .954 | 530.00 | .00 | .00 | 2429.00 | 1361.00 | 2432.98 | 2432.98 | 2434.24 | 87.86 | 10.85 | 185.97 | 145.20 |
| * | 1.005 | 270.00 | .00 | .00 | 2430.00 | 1361.00 | 2434.87 | 2433.43 | 2435.07 | 15.45 | 5.39 | 474.84 | 346.26 |
| * | 1.005 | 270.00 | .00 | .00 | 2430.00 | 1361.00 | 2435.02 | 2433.42 | 2435.37 | 21.36 | 6.47 | 342.44 | 294.49 |
| * | 1.101 | 510.00 | .00 | .00 | 2435.00 | 1361.00 | 2438.65 | 2438.65 | 2439.75 | 93.69 | 10.66 | 199.31 | 140.61 |
| * | 1.101 | 510.00 | .00 | .00 | 2435.00 | 1361.00 | 2438.64 | 2438.64 | 2439.87 | 100.66 | 11.04 | 184.58 | 135.66 |
| * | 1.202 | 530.00 | .00 | .00 | 2446.00 | 1361.00 | 2449.65 | 2449.65 | 2450.59 | 84.81 | 9.98 | 225.15 | 147.79 |
| * | 1.202 | 530.00 | .00 | .00 | 2446.00 | 1361.00 | 2449.66 | 2449.66 | 2450.70 | 89.07 | 10.26 | 212.44 | 144.21 |
| * | 1.295 | 490.00 | .00 | .00 | 2452.00 | 1361.00 | 2455.57 | 2455.57 | 2456.42 | 81.72 | 9.70 | 242.16 | 150.55 |
| * | 1.295 | 490.00 | .00 | .00 | 2452.00 | 1361.00 | 2455.58 | 2455.58 | 2456.56 | 88.51 | 10.12 | 216.81 | 144.66 |
| * | 1.399 | 550.00 | .00 | .00 | 2461.00 | 1361.00 | 2463.96 | 2463.96 | 2464.67 | 89.72 | 9.15 | 266.18 | 143.68 |
| * | 1.399 | 550.00 | .00 | .00 | 2461.00 | 1361.00 | 2463.97 | 2463.97 | 2464.91 | 107.73 | 10.04 | 218.94 | 131.13 |
| * | 1.473 | 395.00 | .00 | .00 | 2466.00 | 1361.00 | 2469.53 | 2469.53 | 2470.36 | 78.98 | 9.51 | 249.10 | 153.15 |
| * | 1.473 | 395.00 | .00 | .00 | 2466.00 | 1361.00 | 2469.48 | 2469.48 | 2470.54 | 97.28 | 10.42 | 205.71 | 137.99 |
| * | 1.576 | 540.00 | .00 | .00 | 2474.00 | 1361.00 | 2476.01 | 2476.01 | 2476.74 | 158.34 | 9.94 | 229.51 | 108.16 |
| * | 1.576 | 540.00 | .00 | .00 | 2474.00 | 1361.00 | 2476.28 | 2476.28 | 2477.27 | 158.08 | 10.79 | 195.17 | 108.25 |
| | 1.615 | 205.00 | .00 | .00 | 2479.00 | 1361.00 | 2481.86 | 2481.86 | 2482.69 | 100.02 | 9.99 | 244.08 | 136.09 |
| | 1.615 | 205.00 | .00 | .00 | 2479.00 | 1361.00 | 2482.02 | 2482.02 | 2483.35 | 125.75 | 11.60 | 173.74 | 121.37 |
| * | 1.661 | 245.00 | .00 | .00 | 2482.00 | 1361.00 | 2484.71 | 2484.71 | 2485.40 | 114.24 | 9.64 | 261.19 | 127.34 |
| | 1.661 | 245.00 | .00 | .00 | 2482.00 | 1361.00 | 2485.11 | 2484.74 | 2485.65 | 68.38 | 8.26 | 281.65 | 164.58 |
| * | 1.767 | 560.00 | .00 | .00 | 2490.00 | 1361.00 | 2493.17 | 2493.17 | 2493.75 | 81.51 | 9.07 | 314.25 | 150.75 |
| * | 1.767 | 560.00 | .00 | .00 | 2490.00 | 1361.00 | 2493.33 | 2493.33 | 2494.40 | 109.99 | 10.92 | 204.45 | 129.77 |
| | 1.873 | 560.00 | .00 | .00 | 2497.00 | 1361.00 | 2498.87 | 2498.85 | 2499.38 | 130.09 | 8.58 | 285.39 | 119.32 |
| | 1.873 | 560.00 | .00 | .00 | 2497.00 | 1361.00 | 2499.22 | 2498.84 | 2499.66 | 80.58 | 7.57 | 291.36 | 151.61 |

UPPER FLYING E WASH

SUMMARY PRINTOUT TABLE 150

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 2.435 | 6943.00 | 2309.87 | .00 | .00 | .00 | 180.52 | .00 |
| * | 2.435 | 6943.00 | 2309.91 | .04 | .00 | .04 | 144.31 | .00 |
| * | 2.539 | 6943.00 | 2315.51 | .00 | 5.64 | .00 | 395.38 | 550.00 |
| * | 2.539 | 6943.00 | 2315.51 | -.01 | 5.59 | -.01 | 394.83 | 550.00 |
| * | 2.630 | 2152.00 | 2319.19 | .00 | 3.68 | .00 | 138.04 | 480.00 |
| * | 2.630 | 2152.00 | 2319.20 | .01 | 3.69 | .01 | 137.15 | 480.00 |
| * | 2.725 | 2152.00 | 2325.77 | .00 | 6.58 | .00 | 147.44 | 500.00 |
| * | 2.725 | 2152.00 | 2325.77 | .01 | 6.57 | .01 | 147.64 | 500.00 |
| * | 2.812 | 2152.00 | 2331.06 | .00 | 5.29 | .00 | 433.86 | 460.00 |
| * | 2.812 | 2152.00 | 2331.06 | .00 | 5.29 | .00 | 433.85 | 460.00 |
| * | 2.922 | 2152.00 | 2337.68 | .00 | 6.61 | .00 | 270.11 | 580.00 |
| * | 2.922 | 2152.00 | 2337.68 | .01 | 6.62 | .01 | 270.33 | 580.00 |
| * | 3.005 | 2152.00 | 2344.12 | .00 | 6.45 | .00 | 390.48 | 440.00 |
| * | 3.005 | 2152.00 | 2344.12 | .00 | 6.44 | .00 | 390.12 | 440.00 |
| * | 3.047 | 2152.00 | 2347.40 | .00 | 3.28 | .00 | 227.57 | 220.00 |
| * | 3.047 | 2152.00 | 2347.40 | .00 | 3.28 | .00 | 227.57 | 220.00 |
| * | 3.113 | 2152.00 | 2352.61 | .00 | 5.21 | .00 | 72.76 | 350.00 |
| * | 3.113 | 2152.00 | 2352.61 | .00 | 5.22 | .00 | 72.76 | 350.00 |
| * | 3.200 | 2152.00 | 2358.16 | .00 | 5.55 | .00 | 240.55 | 460.00 |
| * | 3.200 | 2152.00 | 2358.18 | .01 | 5.56 | .01 | 239.95 | 460.00 |
| * | 3.261 | 2152.00 | 2360.35 | .00 | 2.19 | .00 | 274.33 | 320.00 |
| * | 3.261 | 2152.00 | 2360.35 | -.01 | 2.17 | -.01 | 274.26 | 320.00 |
| * | 3.308 | 2152.00 | 2362.14 | .00 | 1.79 | .00 | 302.21 | 250.00 |
| * | 3.308 | 2152.00 | 2362.14 | .00 | 1.79 | .00 | 302.17 | 250.00 |
| * | 3.355 | 2152.00 | 2365.70 | .00 | 3.56 | .00 | 392.98 | 250.00 |
| * | 3.355 | 2152.00 | 2365.71 | .00 | 3.57 | .00 | 393.05 | 250.00 |
| * | 3.454 | 2152.00 | 2371.78 | .00 | 6.08 | .00 | 430.55 | 520.00 |
| * | 3.454 | 2152.00 | 2371.78 | .00 | 6.07 | .00 | 430.48 | 520.00 |
| * | 3.549 | 896.00 | 2380.04 | .00 | 8.26 | .00 | 350.86 | 500.00 |
| * | 3.549 | 896.00 | 2380.04 | .00 | 8.26 | .00 | 350.86 | 500.00 |
| * | 3.643 | 896.00 | 2387.54 | .00 | 7.50 | .00 | 263.89 | 500.00 |
| * | 3.643 | 896.00 | 2387.54 | .00 | 7.50 | .00 | 263.83 | 500.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
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| * | 3.740 | 896.00 | 2395.56 | .00 | 8.02 | .00 | 258.55 | 510.00 |
| * | 3.740 | 896.00 | 2395.56 | .00 | 8.02 | .00 | 258.55 | 510.00 |
| * | 3.838 | 896.00 | 2404.74 | .00 | 9.18 | .00 | 352.43 | 520.00 |
| * | 3.838 | 896.00 | 2404.71 | -.03 | 9.15 | -.03 | 351.51 | 520.00 |
| * | 3.950 | 896.00 | 2415.08 | .00 | 10.34 | .00 | 92.23 | 590.00 |
| * | 3.950 | 896.00 | 2415.08 | .00 | 10.37 | .00 | 92.23 | 590.00 |
| * | 3.980 | 896.00 | 2417.67 | .00 | 2.60 | .00 | 82.72 | 160.00 |
| * | 3.980 | 896.00 | 2417.68 | .00 | 2.59 | .00 | 82.73 | 160.00 |
| * | 4.032 | 896.00 | 2422.59 | .00 | 4.92 | .00 | 97.30 | 270.00 |
| * | 4.032 | 896.00 | 2422.60 | .00 | 4.92 | .00 | 97.30 | 270.00 |
| * | 4.103 | 896.00 | 2428.37 | .00 | 5.78 | .00 | 151.47 | 375.00 |
| * | 4.103 | 896.00 | 2428.37 | .00 | 5.78 | .00 | 151.47 | 375.00 |
| * | 4.168 | 896.00 | 2434.34 | .00 | 5.97 | .00 | 188.97 | 345.00 |
| * | 4.168 | 896.00 | 2434.34 | .00 | 5.97 | .00 | 188.94 | 345.00 |
| * | 4.213 | 896.00 | 2435.61 | .00 | 1.27 | .00 | 167.98 | 235.00 |
| * | 4.213 | 896.00 | 2435.61 | .00 | 1.28 | .00 | 167.98 | 235.00 |
| | 4.301 | 896.00 | 2442.87 | .00 | 7.26 | .00 | 171.03 | 465.00 |
| | 4.301 | 896.00 | 2442.88 | .01 | 7.26 | .01 | 171.04 | 465.00 |
| * | 4.384 | 896.00 | 2449.49 | .00 | 6.62 | .00 | 105.80 | 440.00 |
| * | 4.384 | 896.00 | 2449.50 | .01 | 6.62 | .01 | 105.80 | 440.00 |
| * | 4.493 | 896.00 | 2458.64 | .00 | 9.15 | .00 | 324.01 | 575.00 |
| * | 4.493 | 896.00 | 2458.68 | .04 | 9.18 | .04 | 324.01 | 575.00 |
| | 4.594 | 896.00 | 2467.37 | .00 | 8.73 | .00 | 300.11 | 530.00 |
| * | 4.594 | 896.00 | 2467.34 | -.03 | 8.66 | -.03 | 293.74 | 530.00 |
| * | 4.688 | 896.00 | 2475.61 | .00 | 8.24 | .00 | 221.26 | 500.00 |
| * | 4.688 | 896.00 | 2475.62 | .01 | 8.28 | .01 | 221.34 | 500.00 |
| * | 4.787 | 896.00 | 2484.24 | .00 | 8.63 | .00 | 310.84 | 520.00 |
| * | 4.787 | 896.00 | 2484.21 | -.02 | 8.60 | -.02 | 306.86 | 520.00 |
| * | 4.881 | 896.00 | 2489.54 | .00 | 5.30 | .00 | 160.79 | 500.00 |
| * | 4.881 | 896.00 | 2489.55 | .01 | 5.34 | .01 | 161.09 | 500.00 |
| * | 5.014 | 896.00 | 2500.01 | .00 | 10.46 | .00 | 130.11 | 700.00 |
| * | 5.014 | 896.00 | 2500.01 | .00 | 10.46 | .00 | 130.12 | 700.00 |
| * | 5.082 | 896.00 | 2506.55 | .00 | 6.55 | .00 | 281.88 | 360.00 |
| | 5.082 | 896.00 | 2506.55 | .00 | 6.55 | .00 | 281.93 | 360.00 |

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| * | 5.175 | 896.00 | 2514.51 | .00 | 7.96 | .00 | 183.79 | 490.00 |
| * | 5.175 | 896.00 | 2514.51 | .00 | 7.96 | .00 | 183.99 | 490.00 |
| * | 5.279 | 896.00 | 2522.29 | .00 | 7.78 | .00 | 172.69 | 550.00 |
| * | 5.279 | 896.00 | 2522.29 | .00 | 7.77 | .00 | 172.65 | 550.00 |
| | -3.454 | 2152.00 | 2371.78 | .00 | -150.51 | .00 | 430.55 | 545.00 |
| | -3.454 | 2152.00 | 2371.78 | .00 | -150.51 | .00 | 430.48 | 545.00 |
| * | .198 | 1361.00 | 2377.47 | .00 | 5.69 | .00 | 116.51 | 500.00 |
| * | .198 | 1361.00 | 2377.53 | .06 | 5.75 | .06 | 106.03 | 500.00 |
| * | .291 | 1361.00 | 2382.42 | .00 | 4.94 | .00 | 89.07 | 490.00 |
| * | .291 | 1361.00 | 2382.42 | .00 | 4.89 | .00 | 89.08 | 490.00 |
| * | .387 | 1361.00 | 2387.71 | .00 | 5.29 | .00 | 53.02 | 510.00 |
| * | .387 | 1361.00 | 2387.73 | .02 | 5.31 | .02 | 53.02 | 510.00 |
| | .482 | 1361.00 | 2392.00 | .00 | 4.29 | .00 | 84.89 | 500.00 |
| | .482 | 1361.00 | 2391.98 | -.02 | 4.25 | -.02 | 84.78 | 500.00 |
| * | .559 | 1361.00 | 2400.71 | .00 | 8.71 | .00 | 44.00 | 405.00 |
| * | .559 | 1361.00 | 2400.71 | .00 | 8.73 | .00 | 44.00 | 405.00 |
| | .607 | 1361.00 | 2403.46 | .00 | 2.76 | .00 | 55.20 | 255.00 |
| | .607 | 1361.00 | 2403.46 | .00 | 2.75 | .00 | 55.20 | 255.00 |
| | .681 | 1361.00 | 2406.91 | .00 | 3.44 | .00 | 83.38 | 390.00 |
| * | .681 | 1361.00 | 2406.92 | .01 | 3.46 | .01 | 83.34 | 390.00 |
| * | .747 | 1361.00 | 2411.12 | .00 | 4.22 | .00 | 48.41 | 350.00 |
| * | .747 | 1361.00 | 2411.12 | .00 | 4.20 | .00 | 48.40 | 350.00 |
| * | .853 | 1361.00 | 2420.77 | .00 | 9.64 | .00 | 102.73 | 560.00 |
| * | .853 | 1361.00 | 2420.77 | .00 | 9.65 | .00 | 102.73 | 560.00 |
| * | .954 | 1361.00 | 2433.00 | .00 | 12.24 | .00 | 86.64 | 530.00 |
| * | .954 | 1361.00 | 2432.98 | -.02 | 12.21 | -.02 | 73.00 | 530.00 |
| * | 1.005 | 1361.00 | 2434.87 | .00 | 1.87 | .00 | 189.40 | 270.00 |
| * | 1.005 | 1361.00 | 2435.02 | .15 | 2.04 | .15 | 88.00 | 270.00 |
| * | 1.101 | 1361.00 | 2438.65 | .00 | 3.78 | .00 | 92.09 | 510.00 |
| * | 1.101 | 1361.00 | 2438.64 | -.01 | 3.62 | -.01 | 74.52 | 510.00 |
| * | 1.202 | 1361.00 | 2449.65 | .00 | 11.00 | .00 | 113.55 | 530.00 |
| * | 1.202 | 1361.00 | 2449.66 | .02 | 11.02 | .02 | 96.00 | 530.00 |
| * | 1.295 | 1361.00 | 2455.57 | .00 | 5.92 | .00 | 149.49 | 490.00 |
| | 1.295 | 1361.00 | 2455.58 | .01 | 5.92 | .01 | 106.00 | 490.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 1.399 | 1361.00 | 2463.96 | .00 | 8.40 | .00 | 187.47 | 550.00 |
| * | 1.399 | 1361.00 | 2463.97 | .01 | 8.39 | .01 | 111.00 | 550.00 |
| * | 1.473 | 1361.00 | 2469.53 | .00 | 5.57 | .00 | 160.24 | 395.00 |
| * | 1.473 | 1361.00 | 2469.48 | -.06 | 5.50 | -.06 | 93.00 | 395.00 |
| * | 1.576 | 1361.00 | 2476.01 | .00 | 6.48 | .00 | 155.23 | 540.00 |
| * | 1.576 | 1361.00 | 2476.28 | .27 | 6.81 | .27 | 100.00 | 540.00 |
| * | 1.615 | 1361.00 | 2481.86 | .00 | 5.85 | .00 | 151.23 | 205.00 |
| * | 1.615 | 1361.00 | 2482.02 | .15 | 5.74 | .15 | 65.00 | 205.00 |
| * | 1.661 | 1361.00 | 2484.71 | .00 | 2.85 | .00 | 181.83 | 245.00 |
| | 1.661 | 1361.00 | 2485.11 | .40 | 3.09 | .40 | 131.00 | 245.00 |
| * | 1.767 | 1361.00 | 2493.17 | .00 | 8.46 | .00 | 265.80 | 560.00 |
| * | 1.767 | 1361.00 | 2493.33 | .16 | 8.22 | .16 | 90.00 | 560.00 |
| | 1.873 | 1361.00 | 2498.87 | .00 | 5.70 | .00 | 264.75 | 560.00 |
| | 1.873 | 1361.00 | 2499.22 | .35 | 5.89 | .35 | 155.00 | 560.00 |

SUMMARY OF ERRORS AND SPECIAL NOTES

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CAUTION SECNO=     2.435  PROFILE=  1  CRITICAL DEPTH ASSUMED
NOTE    SECNO=     2.435  PROFILE=  1  WSEL BASED ON X5 CARD
NOTE    SECNO=     2.435  PROFILE=  2  WSEL BASED ON X5 CARD

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CAUTION SECNO=     2.539  PROFILE=  2  MINIMUM SPECIFIC ENERGY

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WARNING SECNO=     2.630  PROFILE=  2  CONVEYANCE CHANGE OUTSIDE ACCEPTABLE RANGE

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CAUTION SECNO=      1.576  PROFILE=  1  CRITICAL DEPTH ASSUMED
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CAUTION SECNO=      1.767  PROFILE=  1  MINIMUM SPECIFIC ENERGY
CAUTION SECNO=      1.767  PROFILE=  2  CRITICAL DEPTH ASSUMED
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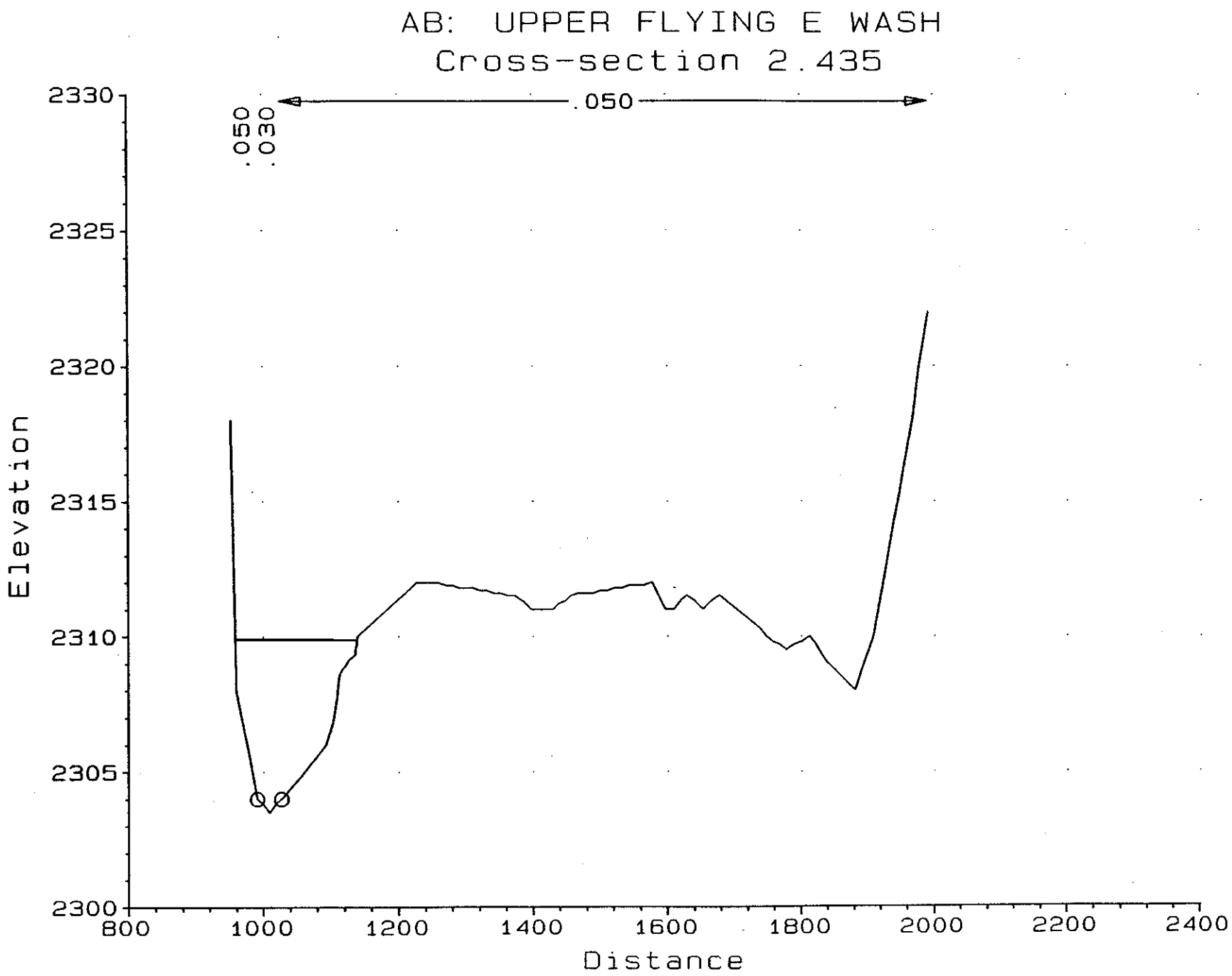
FLOODWAY DATA, AB: UPPER FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| 2.435 | 144. | 701. | 9.9 | 2309.9 | 2309.9 | .0 |
| 2.539 | 549. | 844. | 8.2 | 2315.5 | 2315.5 | .0 |
| 2.630 | 137. | 453. | 4.8 | 2319.2 | 2319.2 | .0 |
| 2.725 | 244. | 281. | 7.7 | 2325.8 | 2325.8 | .0 |
| 2.812 | 434. | 517. | 4.2 | 2331.1 | 2331.1 | .0 |
| 2.922 | 352. | 427. | 5.0 | 2337.7 | 2337.7 | .0 |
| 3.005 | 480. | 497. | 4.3 | 2344.1 | 2344.1 | .0 |
| 3.047 | 228. | 396. | 5.4 | 2347.4 | 2347.4 | .0 |
| 3.113 | 73. | 245. | 8.8 | 2352.6 | 2352.6 | .0 |
| 3.200 | 240. | 383. | 5.6 | 2358.2 | 2358.2 | .0 |
| 3.261 | 274. | 580. | 3.7 | 2360.4 | 2360.4 | .0 |
| 3.308 | 302. | 435. | 4.9 | 2362.1 | 2362.1 | .0 |
| 3.355 | 413. | 503. | 4.3 | 2365.7 | 2365.7 | .0 |
| 3.454 | 596. | 425. | 5.1 | 2371.8 | 2371.8 | .0 |
| 3.549 | 351. | 275. | 3.3 | 2380.0 | 2380.0 | .0 |
| 3.643 | 332. | 238. | 3.8 | 2387.5 | 2387.5 | .0 |
| 3.740 | 280. | 255. | 3.5 | 2395.6 | 2395.6 | .0 |
| 3.838 | 383. | 263. | 3.4 | 2404.7 | 2404.7 | .0 |
| 3.950 | 92. | 160. | 5.6 | 2415.1 | 2415.1 | .0 |
| 3.980 | 83. | 148. | 6.1 | 2417.7 | 2417.7 | .0 |
| 4.032 | 97. | 151. | 5.9 | 2422.6 | 2422.6 | .0 |
| 4.103 | 151. | 198. | 4.5 | 2428.4 | 2428.4 | .0 |
| 4.168 | 189. | 209. | 4.3 | 2434.3 | 2434.3 | .0 |
| 4.213 | 168. | 330. | 2.7 | 2435.6 | 2435.6 | .0 |
| 4.301 | 171. | 189. | 4.7 | 2442.9 | 2442.9 | .0 |
| 4.384 | 106. | 162. | 5.5 | 2449.5 | 2449.5 | .0 |
| 4.493 | 324. | 254. | 3.5 | 2458.6 | 2458.6 | .0 |
| 4.594 | 539. | 207. | 4.3 | 2467.4 | 2467.4 | .0 |
| 4.688 | 221. | 227. | 3.9 | 2475.6 | 2475.6 | .0 |
| 4.787 | 396. | 252. | 3.6 | 2484.2 | 2484.2 | .0 |
| 4.881 | 374. | 197. | 4.6 | 2489.5 | 2489.5 | .0 |
| 5.014 | 130. | 179. | 5.0 | 2500.0 | 2500.0 | .0 |
| 5.082 | 282. | 257. | 3.5 | 2506.6 | 2506.6 | .0 |
| 5.175 | 295. | 194. | 4.6 | 2514.5 | 2514.5 | .0 |
| 5.279 | 173. | 192. | 4.7 | 2522.3 | 2522.3 | .0 |
| -3.454 | 596. | 425. | 5.1 | 2371.8 | 2371.8 | .0 |
| .198 | 106. | 232. | 5.9 | 2377.6 | 2377.5 | .1 |
| .291 | 89. | 199. | 6.9 | 2382.4 | 2382.4 | .0 |
| .387 | 53. | 159. | 8.6 | 2387.7 | 2387.7 | .0 |
| .482 | 85. | 205. | 6.6 | 2392.0 | 2392.0 | .0 |
| .559 | 44. | 135. | 10.1 | 2400.7 | 2400.7 | .0 |
| .607 | 55. | 163. | 8.4 | 2403.5 | 2403.5 | .0 |

FLOODWAY DATA, AB: UPPER FLYING E WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| .681 | 83. | 196. | 6.9 | 2406.9 | 2406.9 | .0 |
| .747 | 48. | 152. | 9.0 | 2411.1 | 2411.1 | .0 |
| .853 | 103. | 214. | 6.4 | 2420.8 | 2420.8 | .0 |
| .954 | 73. | 186. | 7.3 | 2433.0 | 2433.0 | .0 |
| 1.005 | 88. | 342. | 4.0 | 2435.0 | 2434.9 | .1 |
| 1.101 | 75. | 185. | 7.4 | 2438.7 | 2438.7 | .0 |
| 1.202 | 96. | 212. | 6.4 | 2449.6 | 2449.6 | .0 |
| 1.295 | 106. | 217. | 6.3 | 2455.6 | 2455.6 | .0 |
| 1.399 | 111. | 219. | 6.2 | 2464.0 | 2464.0 | .0 |
| 1.473 | 93. | 206. | 6.6 | 2469.4 | 2469.5 | -.1 |
| 1.576 | 100. | 195. | 7.0 | 2476.3 | 2476.0 | .3 |
| 1.615 | 65. | 174. | 7.8 | 2482.1 | 2481.9 | .2 |
| 1.661 | 131. | 282. | 4.8 | 2485.1 | 2484.7 | .4 |
| 1.767 | 90. | 204. | 6.7 | 2493.4 | 2493.2 | .2 |
| 1.873 | 155. | 291. | 4.7 | 2499.2 | 2498.9 | .3 |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.050
.030
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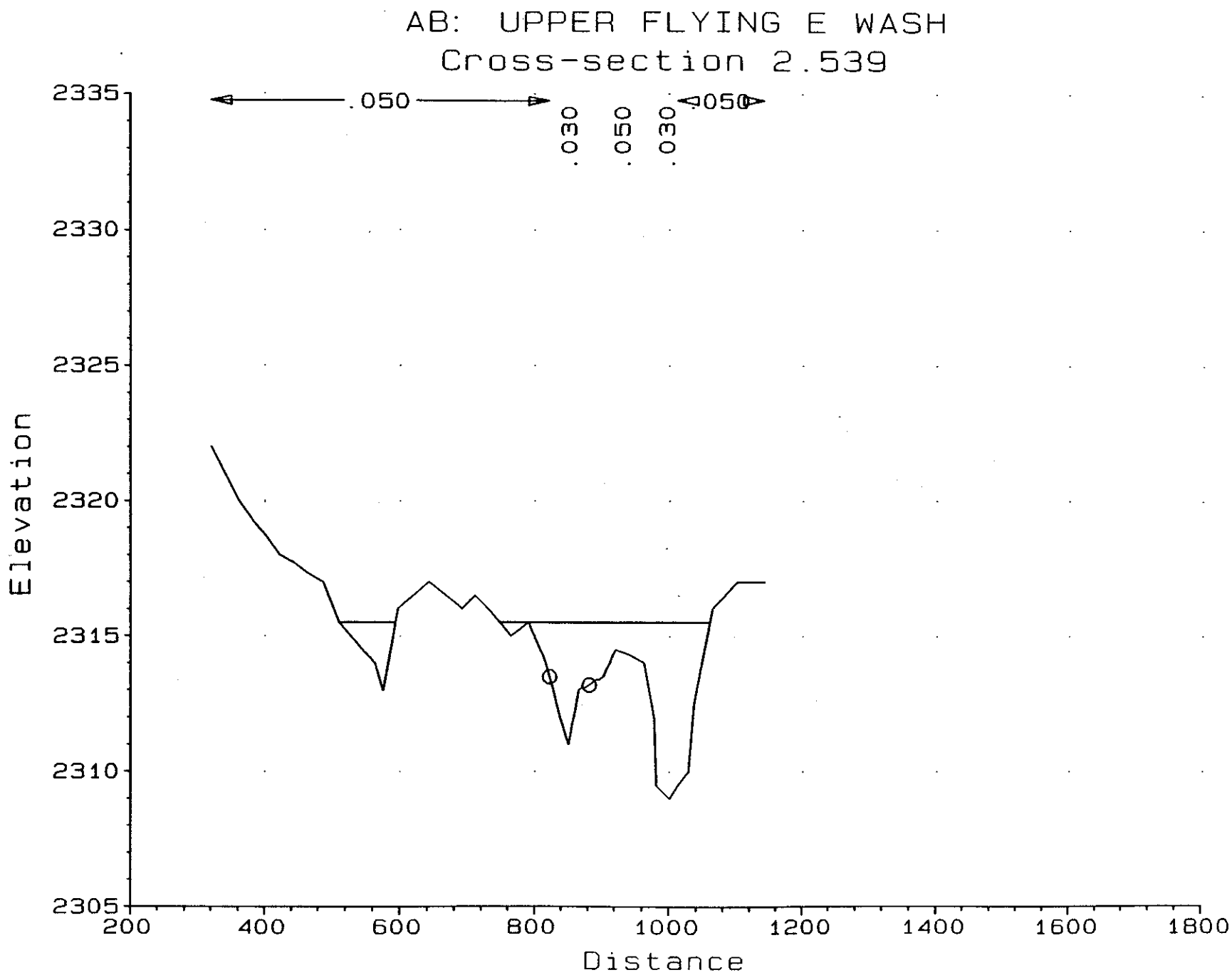
2325
2320
2315
2310
2305
2300
Elevation
800
1000
1200
1400
1600
1800
2000
2200
2400
Distance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.050
.030
.050
.030
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2310
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Elevation
200
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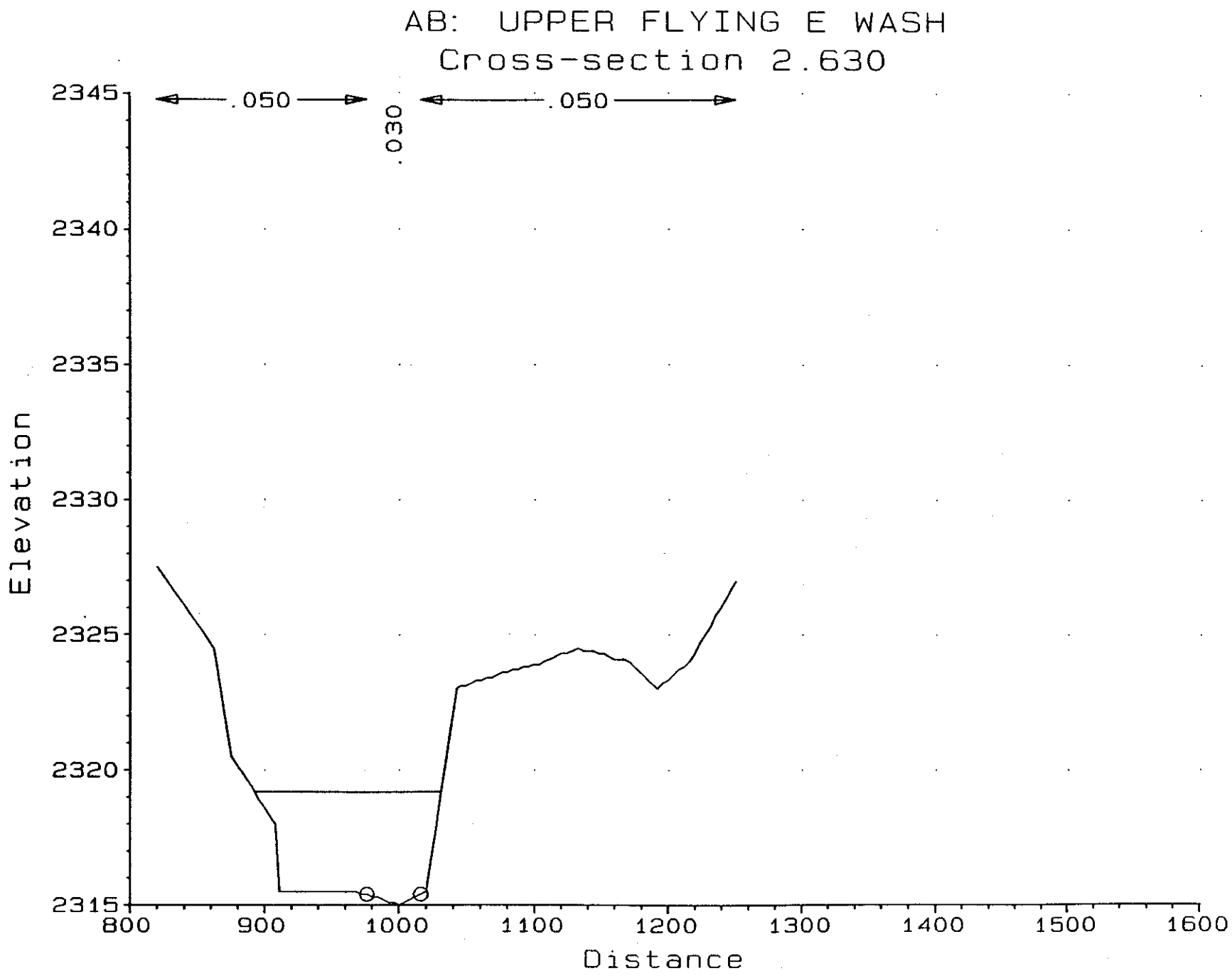
600
800
1000
1200
1400
1600
1800
Distance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Cross-section 2.630
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.050
2345
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2320
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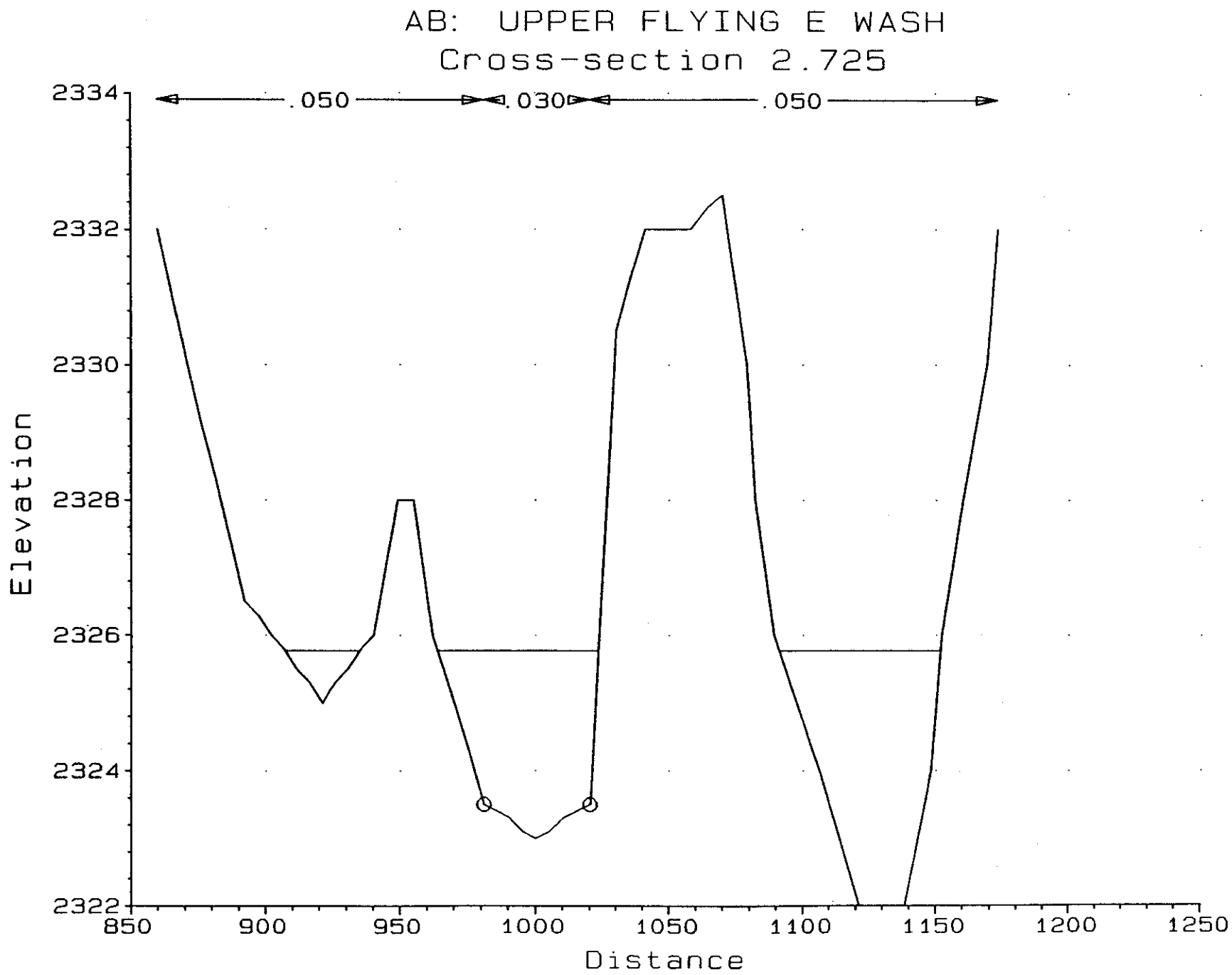
Elevation
800
900
1000
1100
1200
1300
1400
1500
1600
Distance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Cross-section 2.725
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.050
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2332
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2324
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Elevation
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900
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1000
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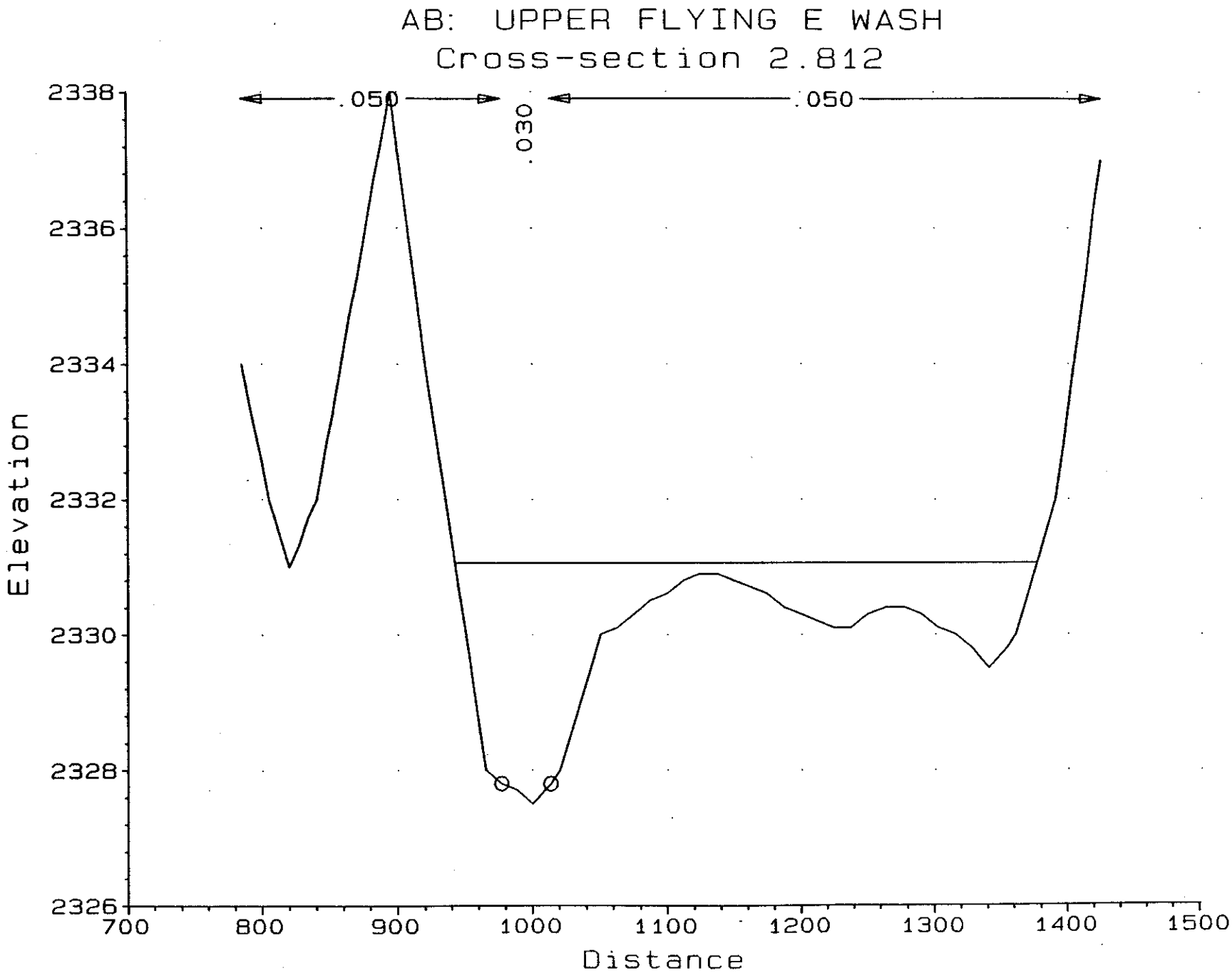
1100
1150
1200
1250
Distance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Cross-section 2.812
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.050
2338
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2328
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Elevation
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900
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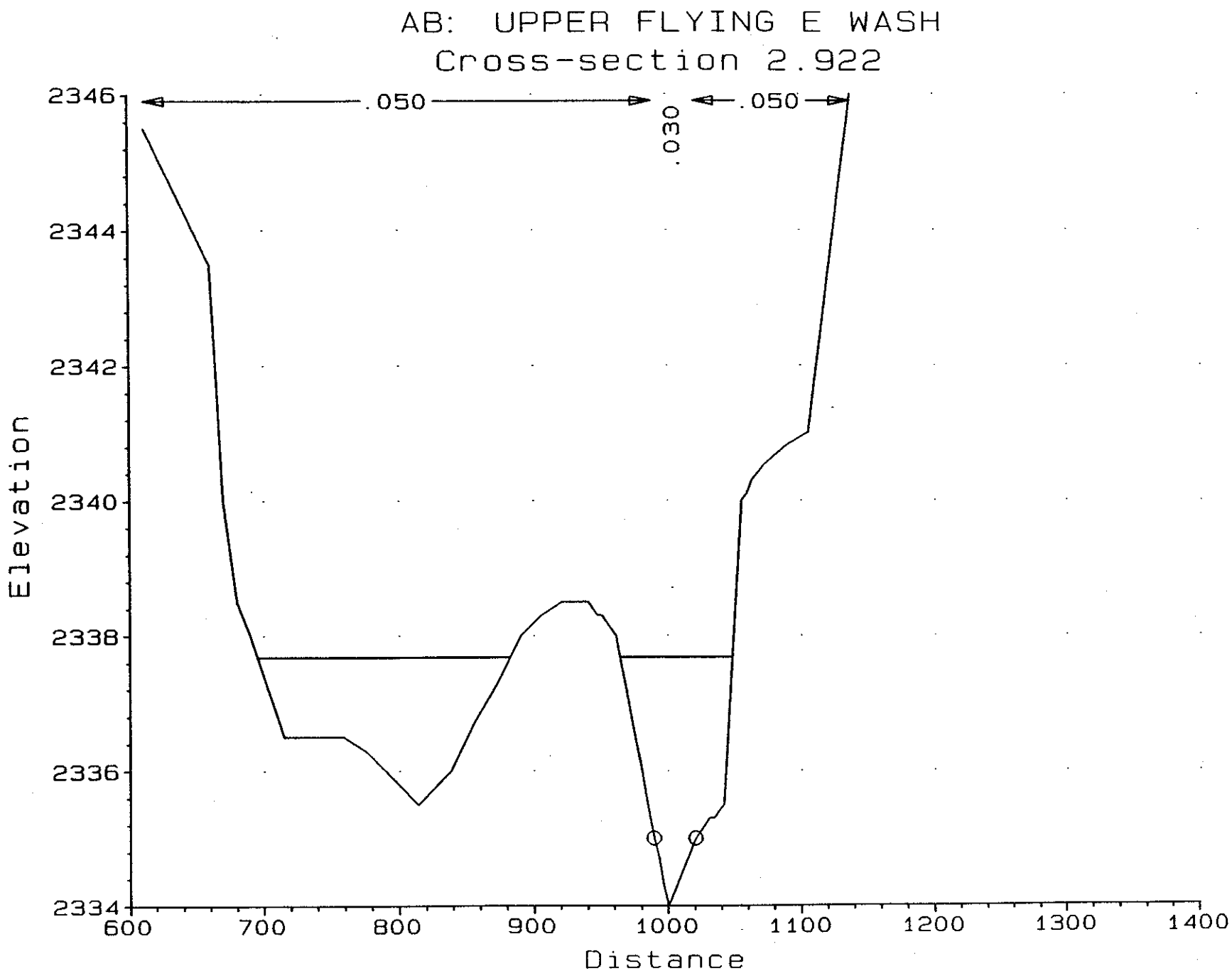
1400
1500
Distance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2336
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Elevation
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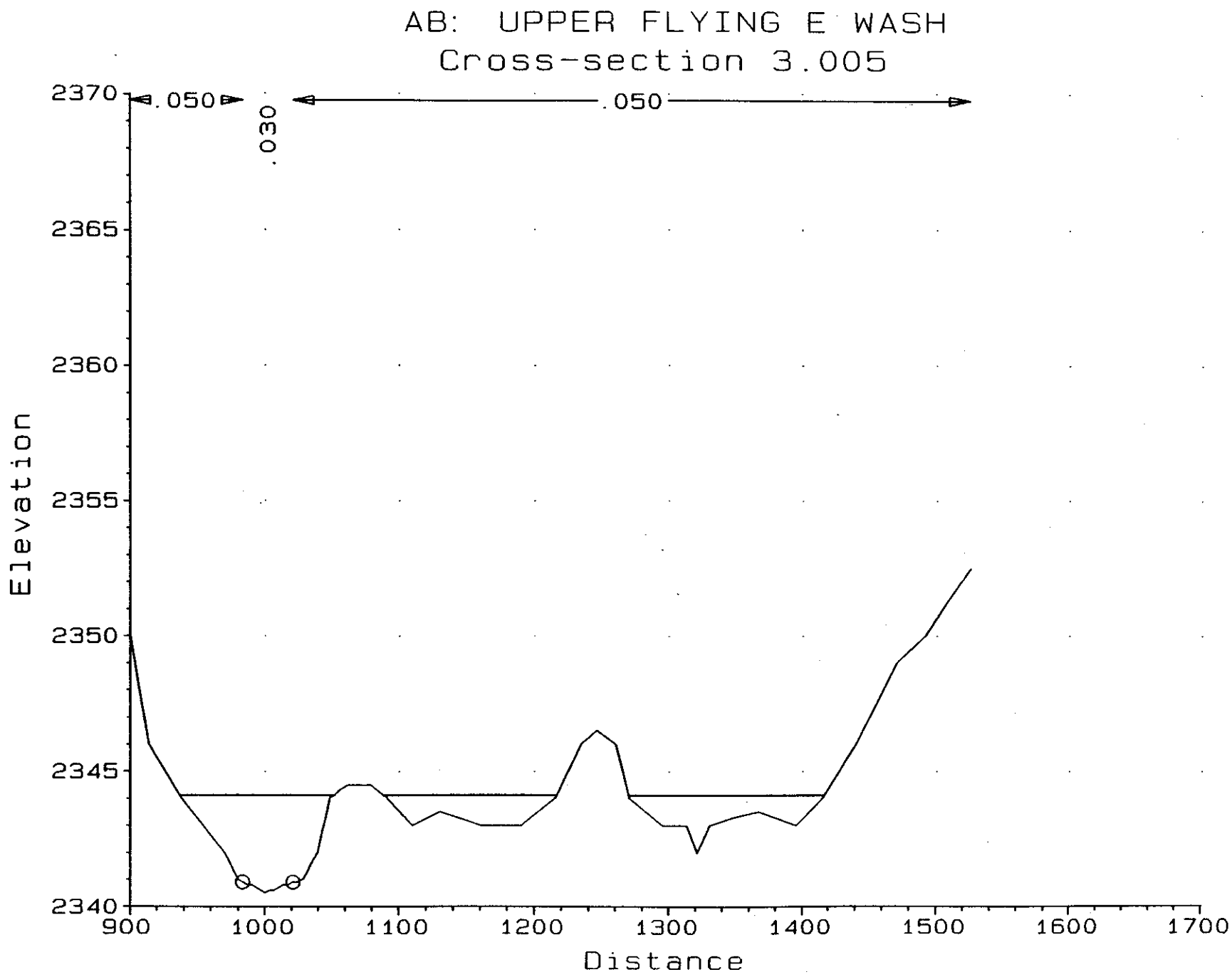
1300
1400
Distance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Cross-section 3.005
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Elevation
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1000
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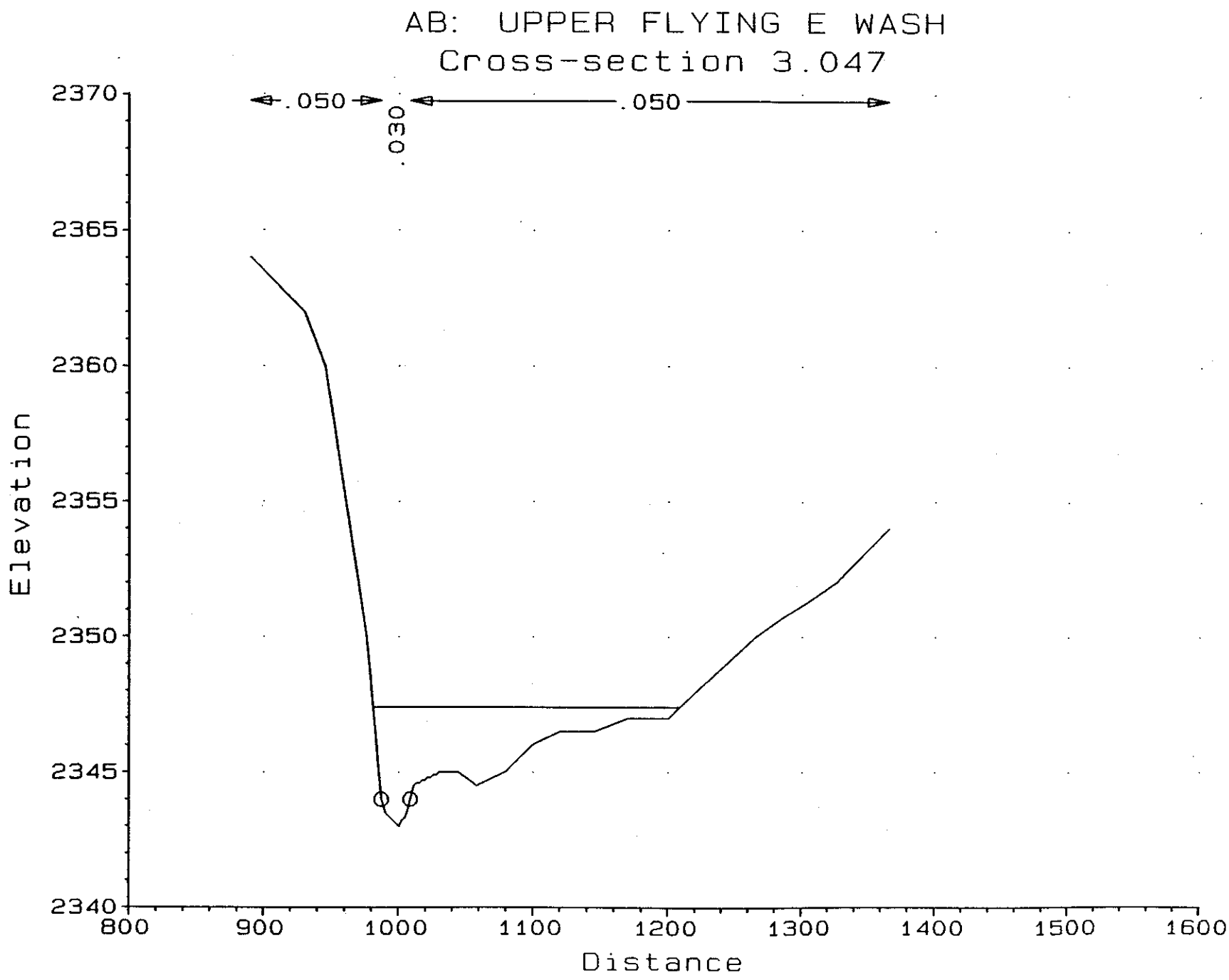
1200
1300
1400
1500
1600
1700
Distance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Cross-section 3.047
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.050
Elevation
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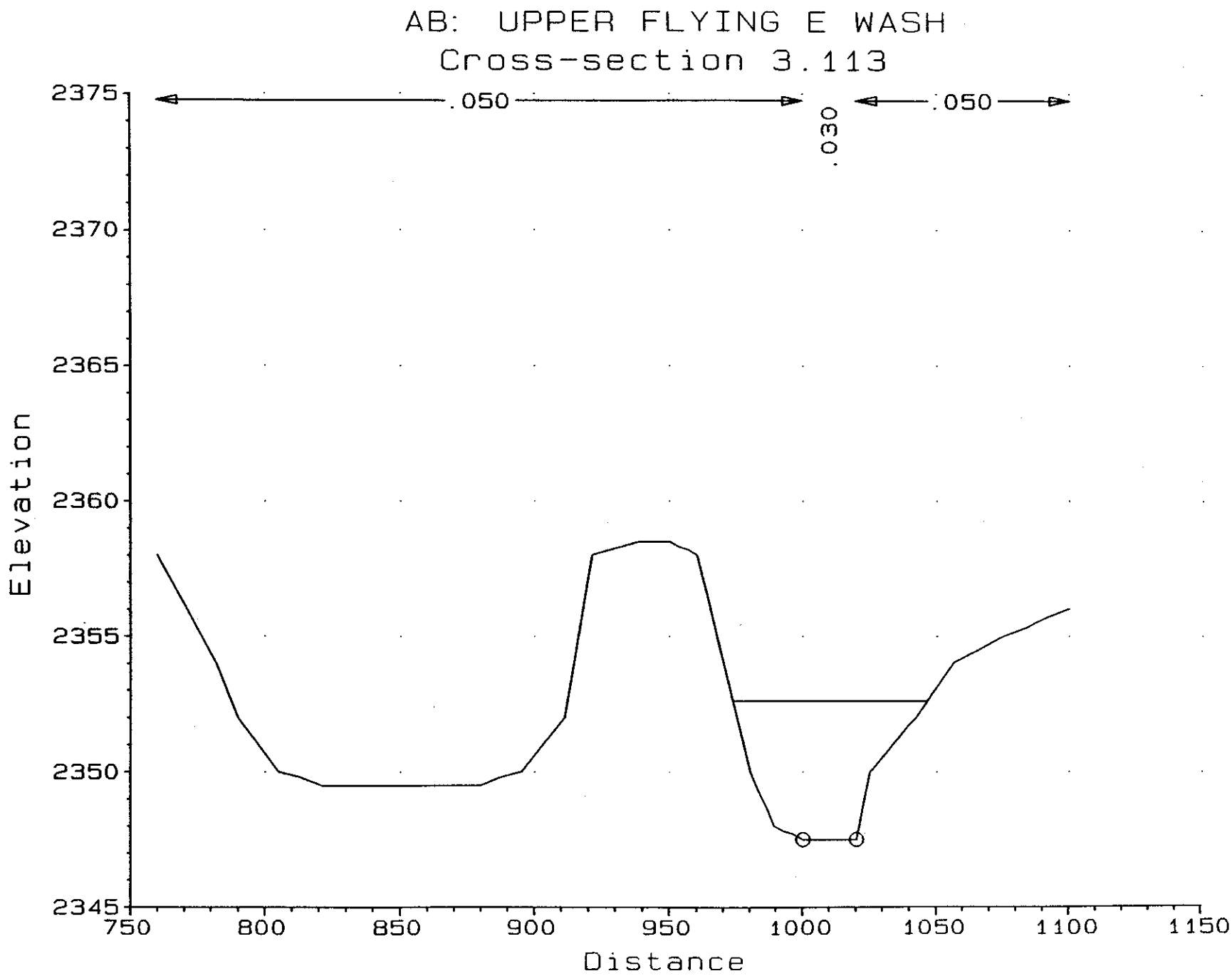
1100
1200
1300
1400
1500
1600
Distance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Cross-section 3.113
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.030
.050
2375
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Elevation
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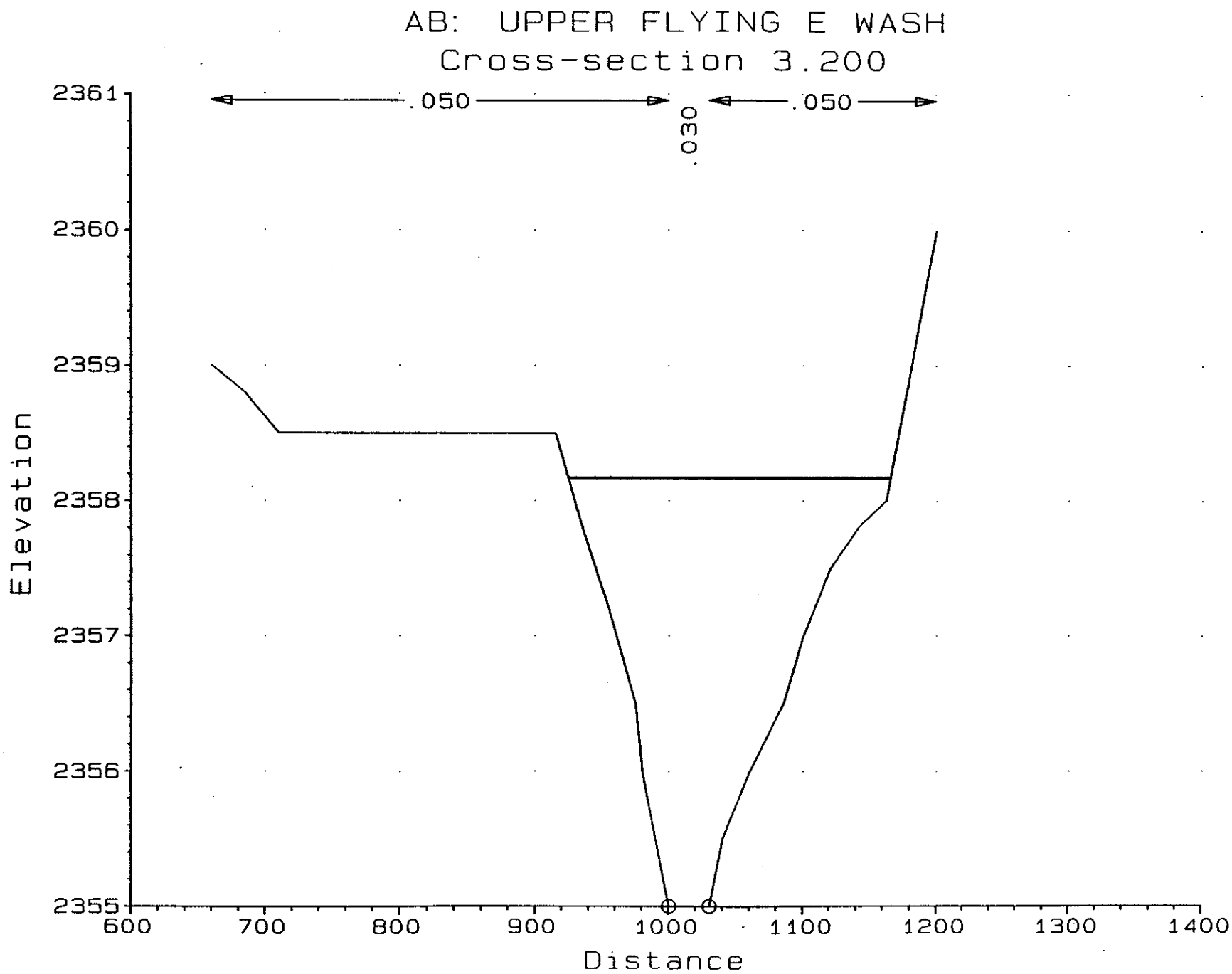
850
900
950
1000
1050
1100
1150
Distance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Cross-section 3.200
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.030
.050
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2360
2359
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2357
2356
2355
Elevation
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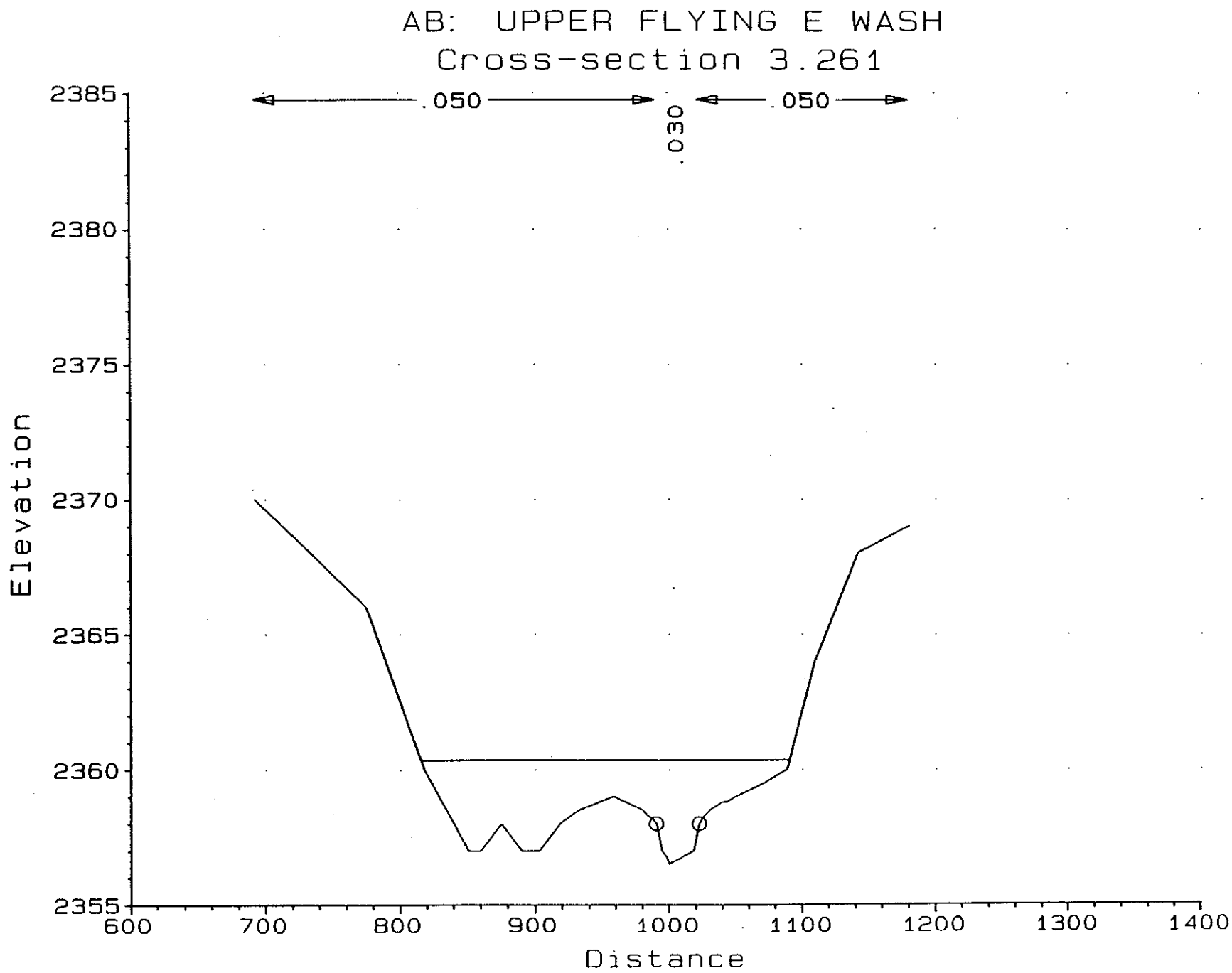
1300
1400
Distance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Cross-section 3.261
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.030
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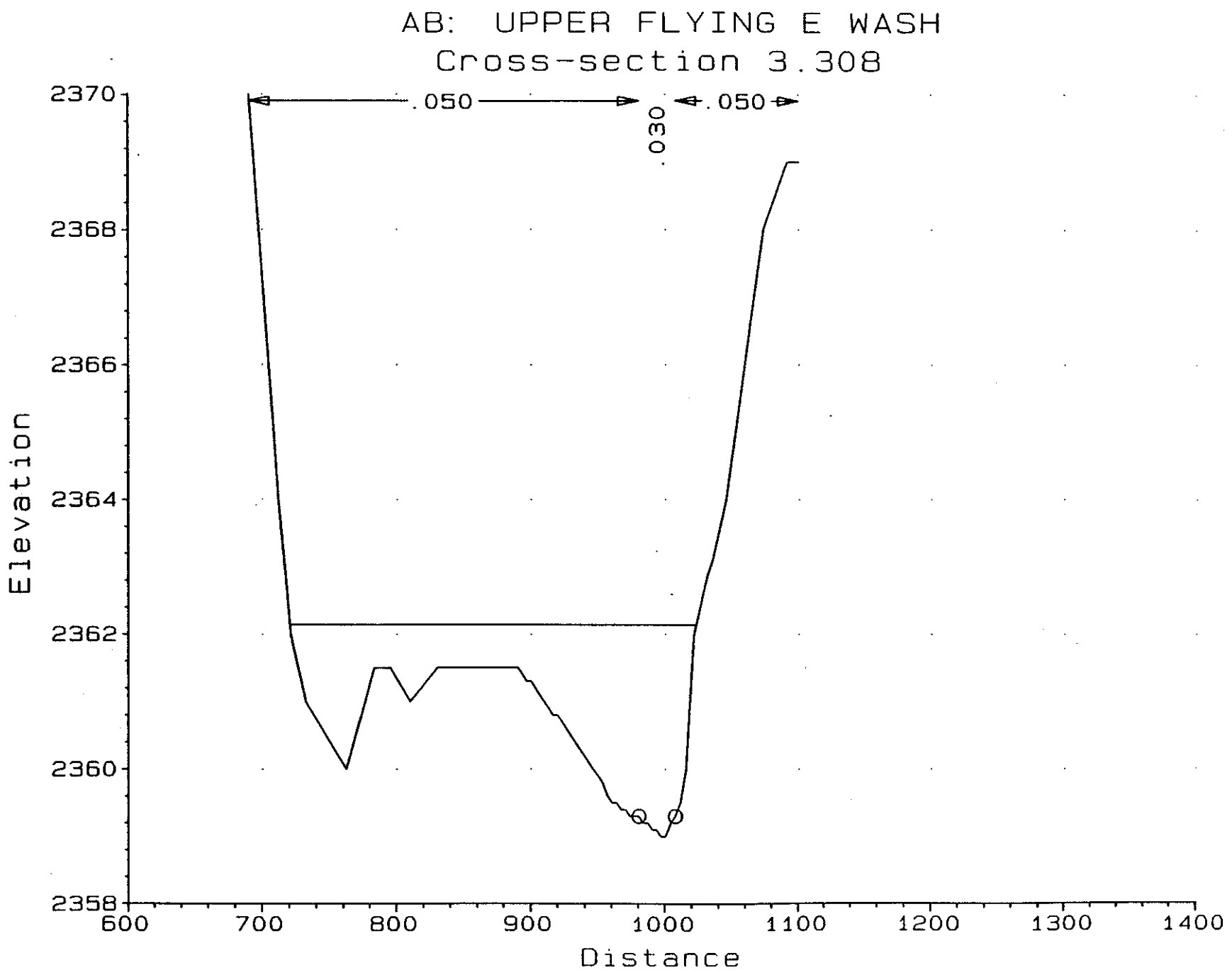
Distance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Cross-section 3.308
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.050
.030
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2366
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2362
2360
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Elevation
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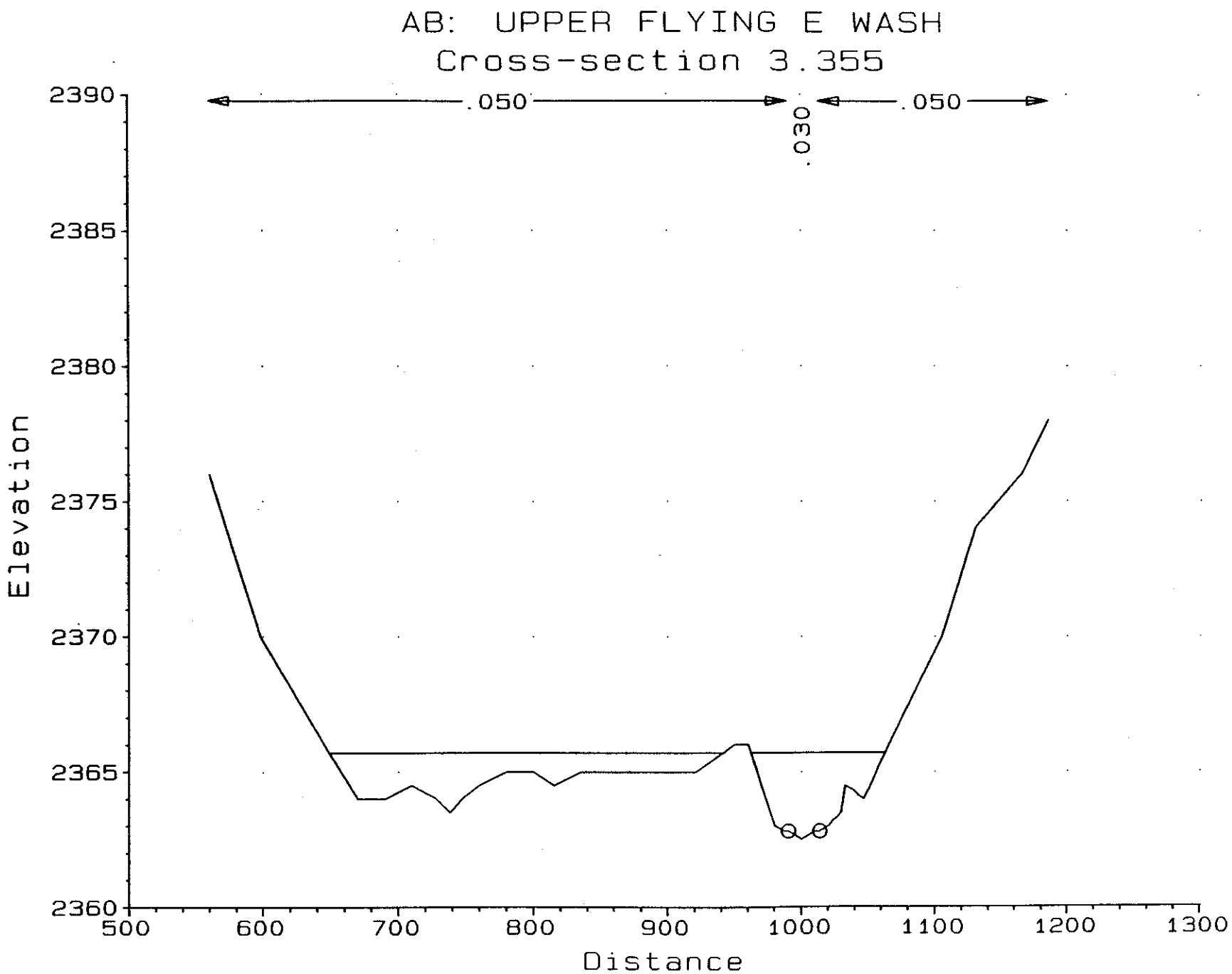
1300
1400
Distance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Cross-section 3.355
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.030
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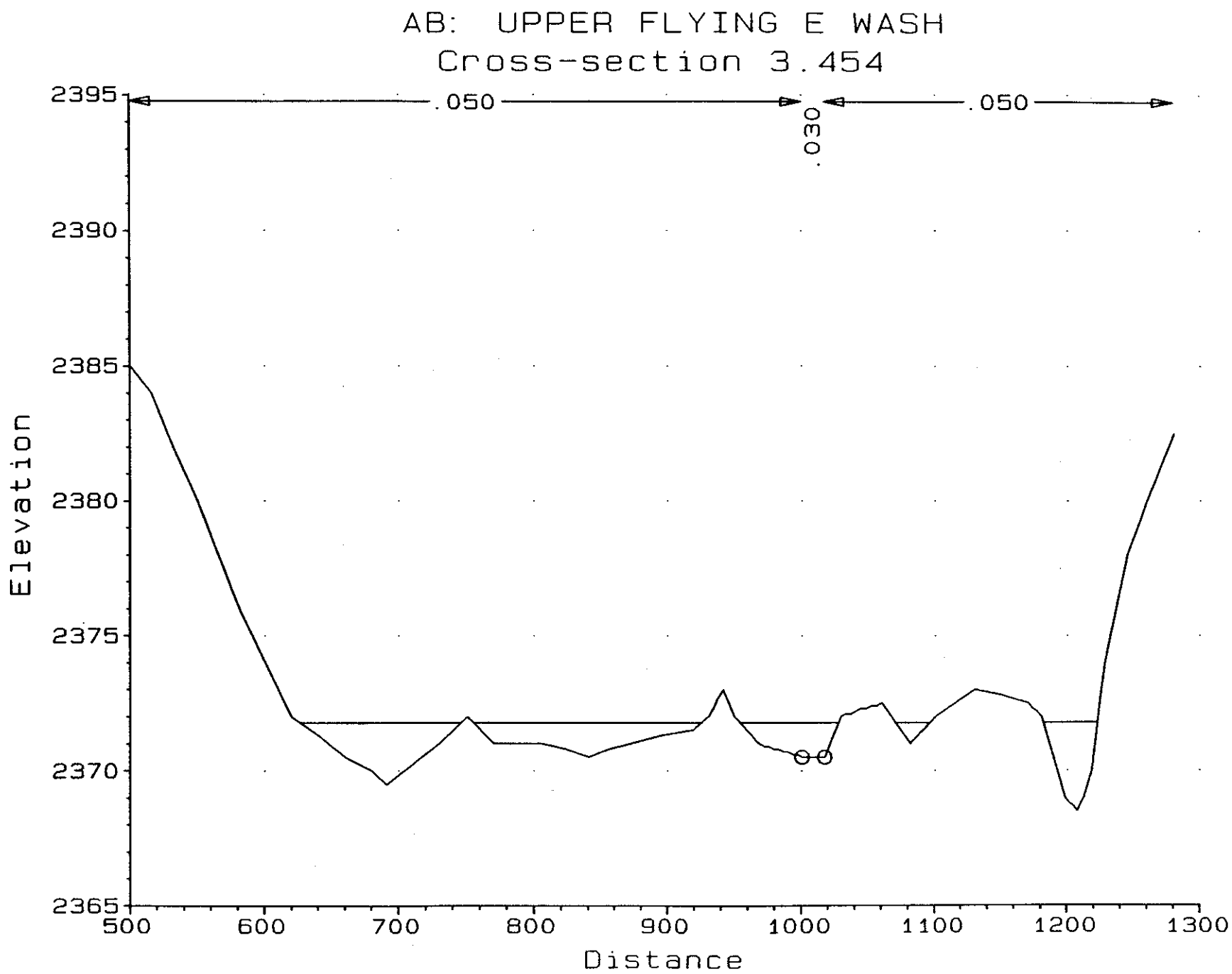
Distance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Cross-section 3.454
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.050
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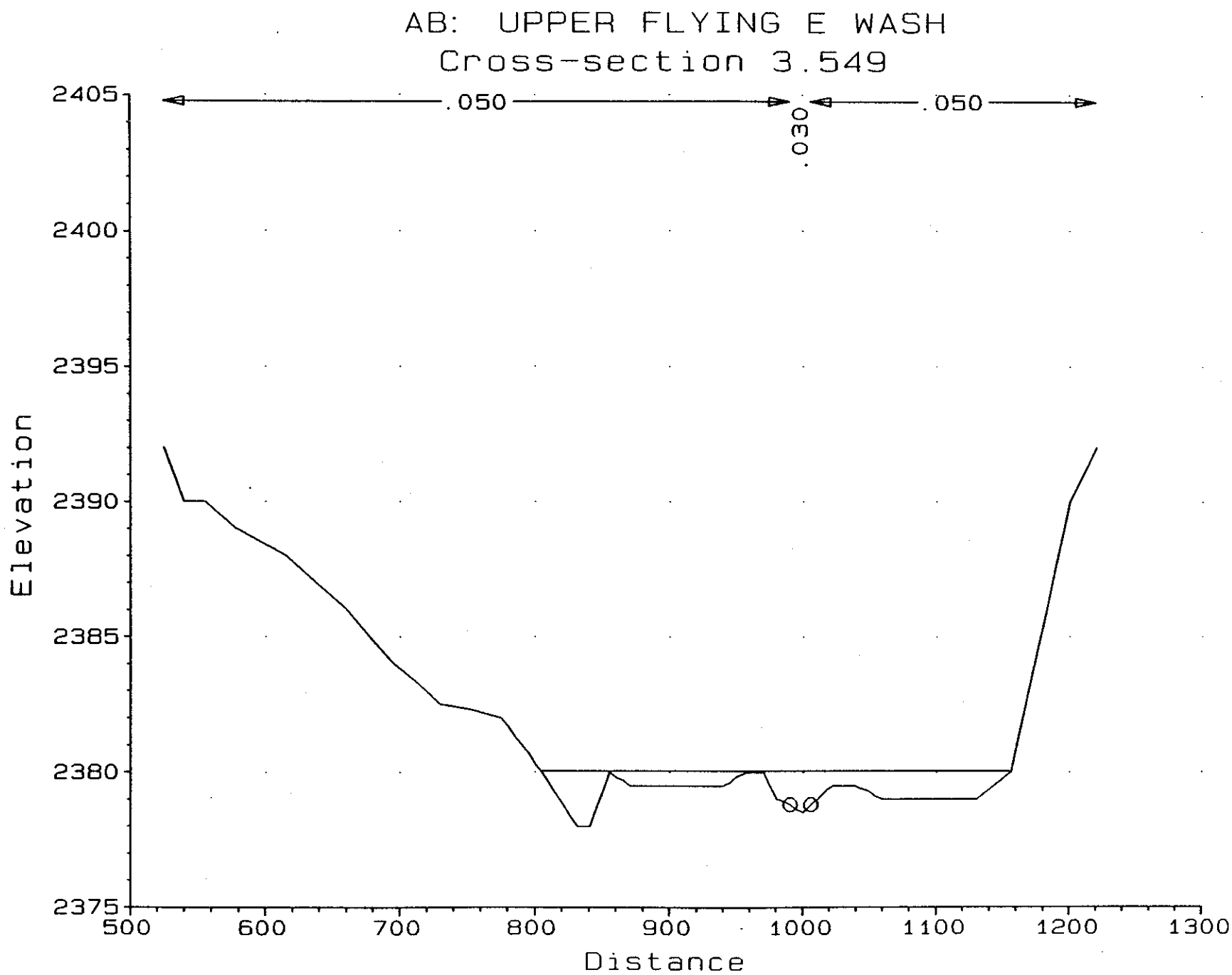
1200
1300
Distance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Cross-section 3.549
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.030
.050
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2380
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Elevation
500
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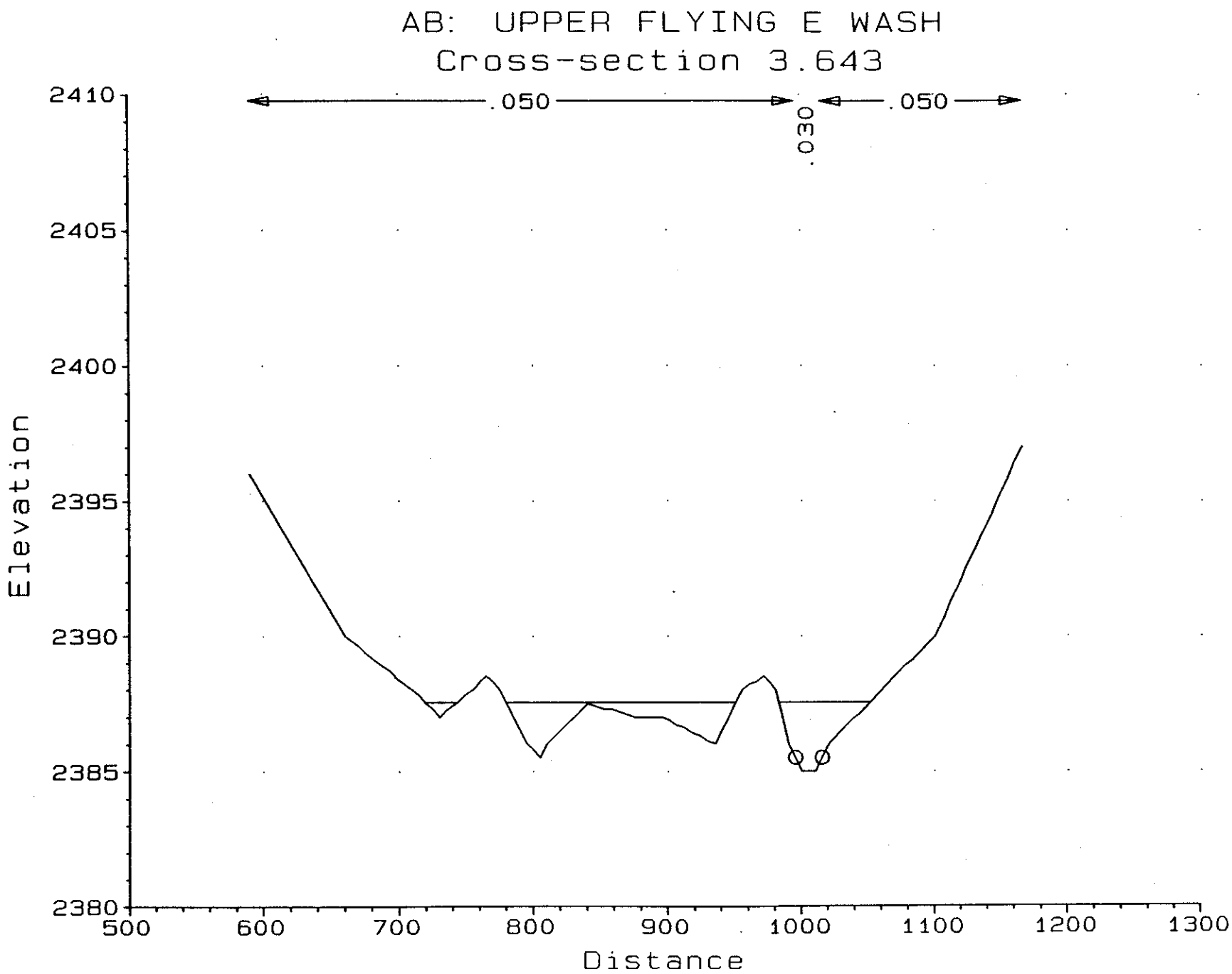
1100
1200
1300
Distance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Cross-section 3.643
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Elevation
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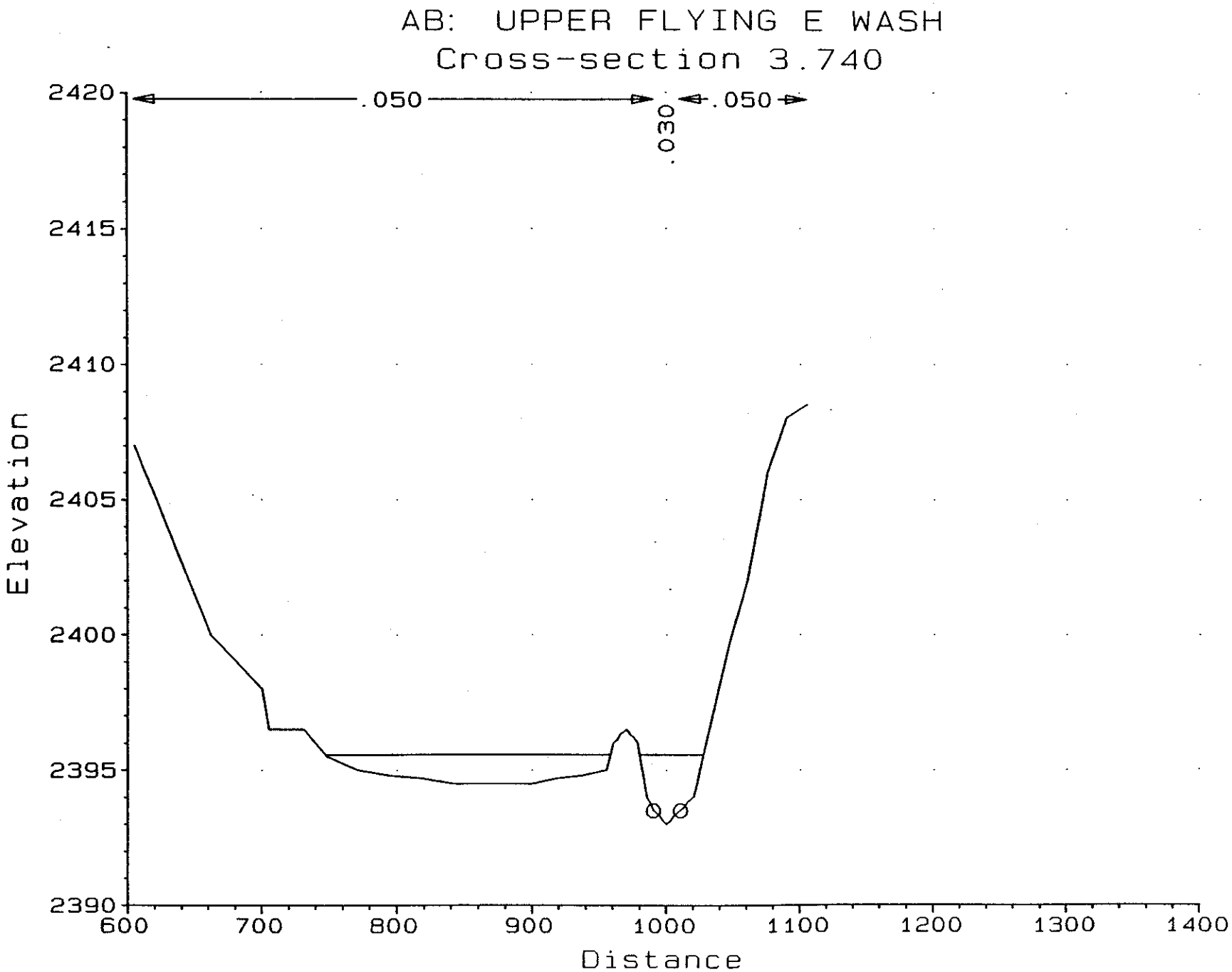
1100
1200
1300
Distance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Cross-section 3.740
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.050
.030
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2400
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Elevation
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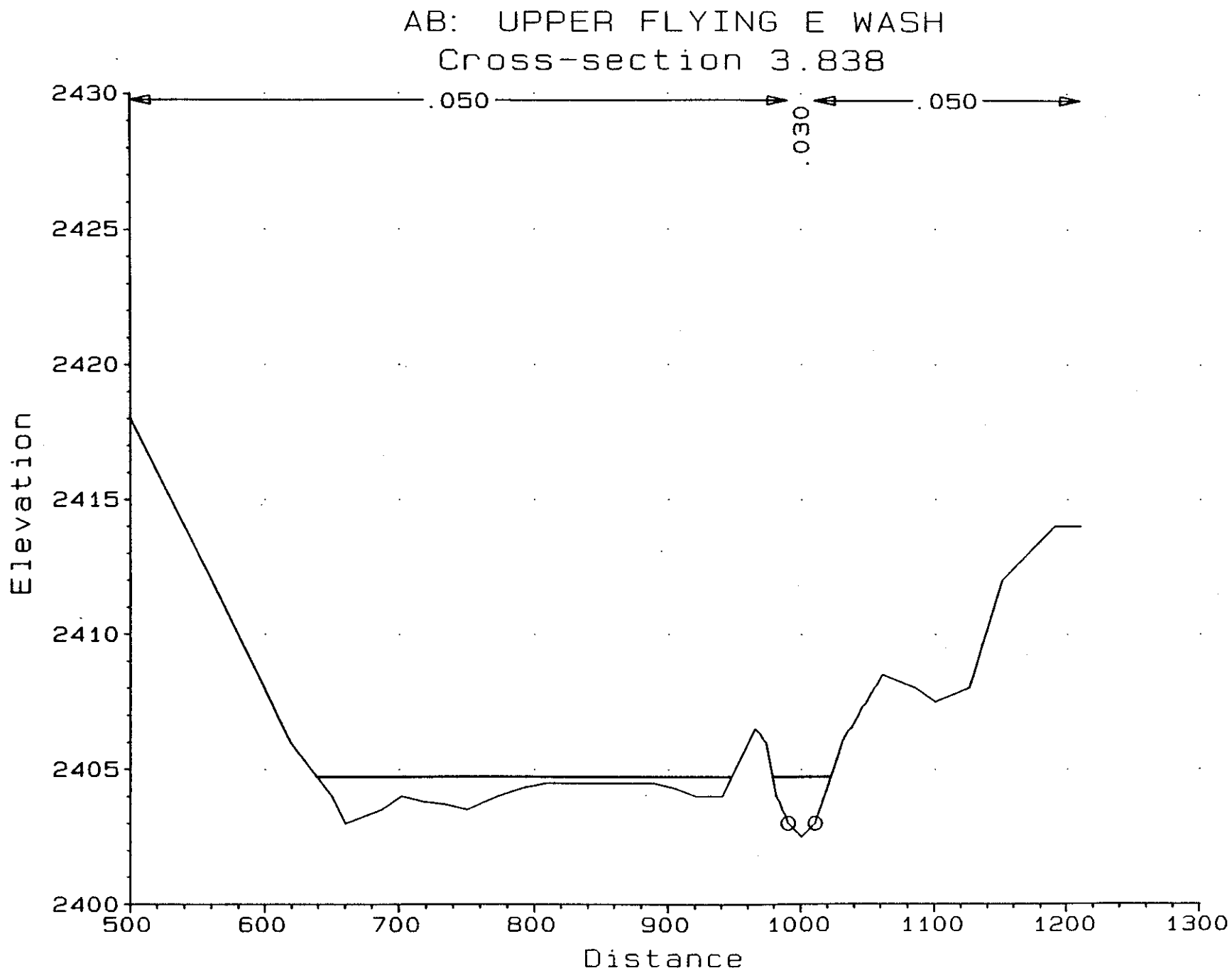
1000
1100
1200
1300
1400
Distance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Cross-section 3.838
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.030
.050
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2405
2400
Elevation
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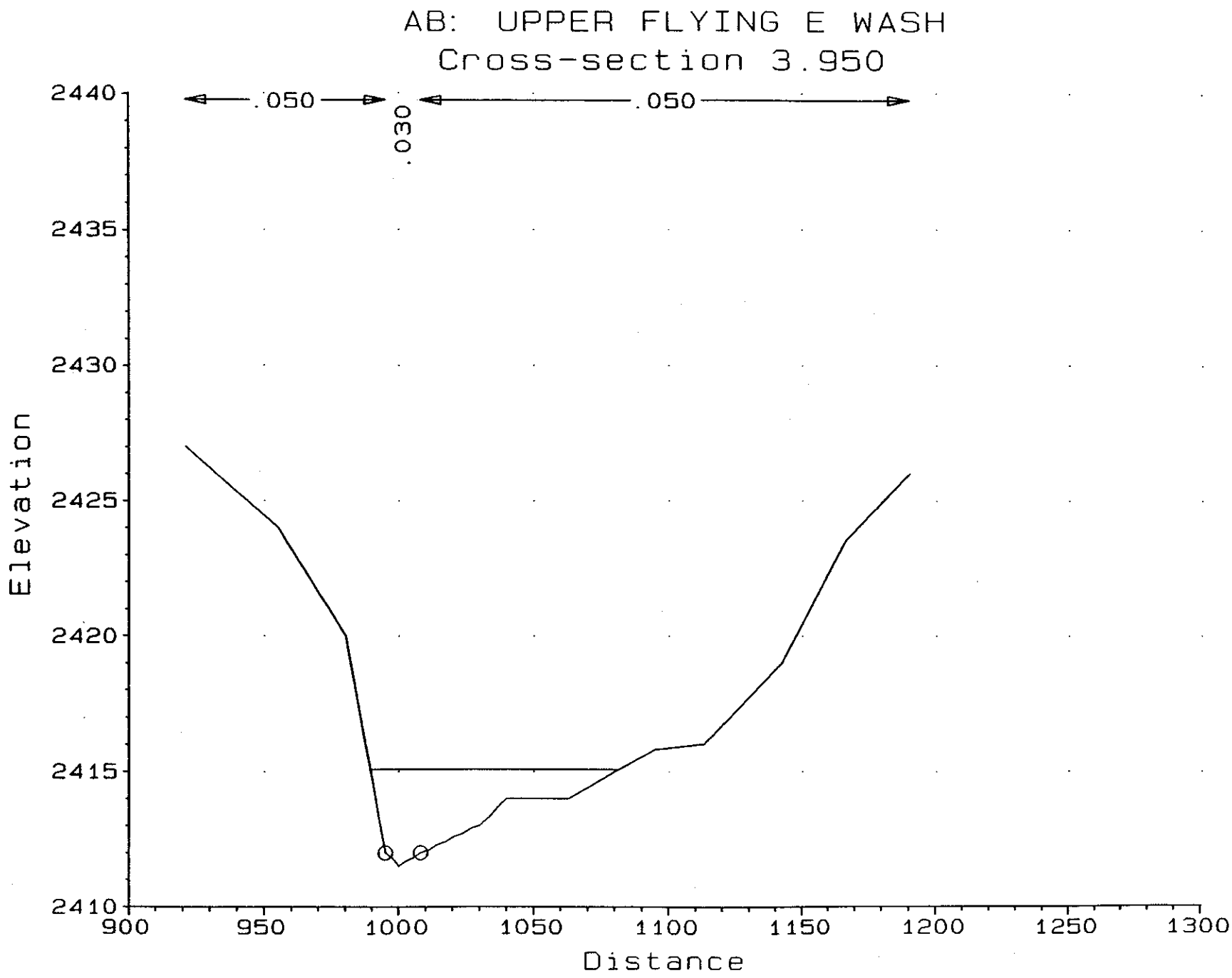
1100
1200
1300
Distance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Cross-section 3.950
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Elevation
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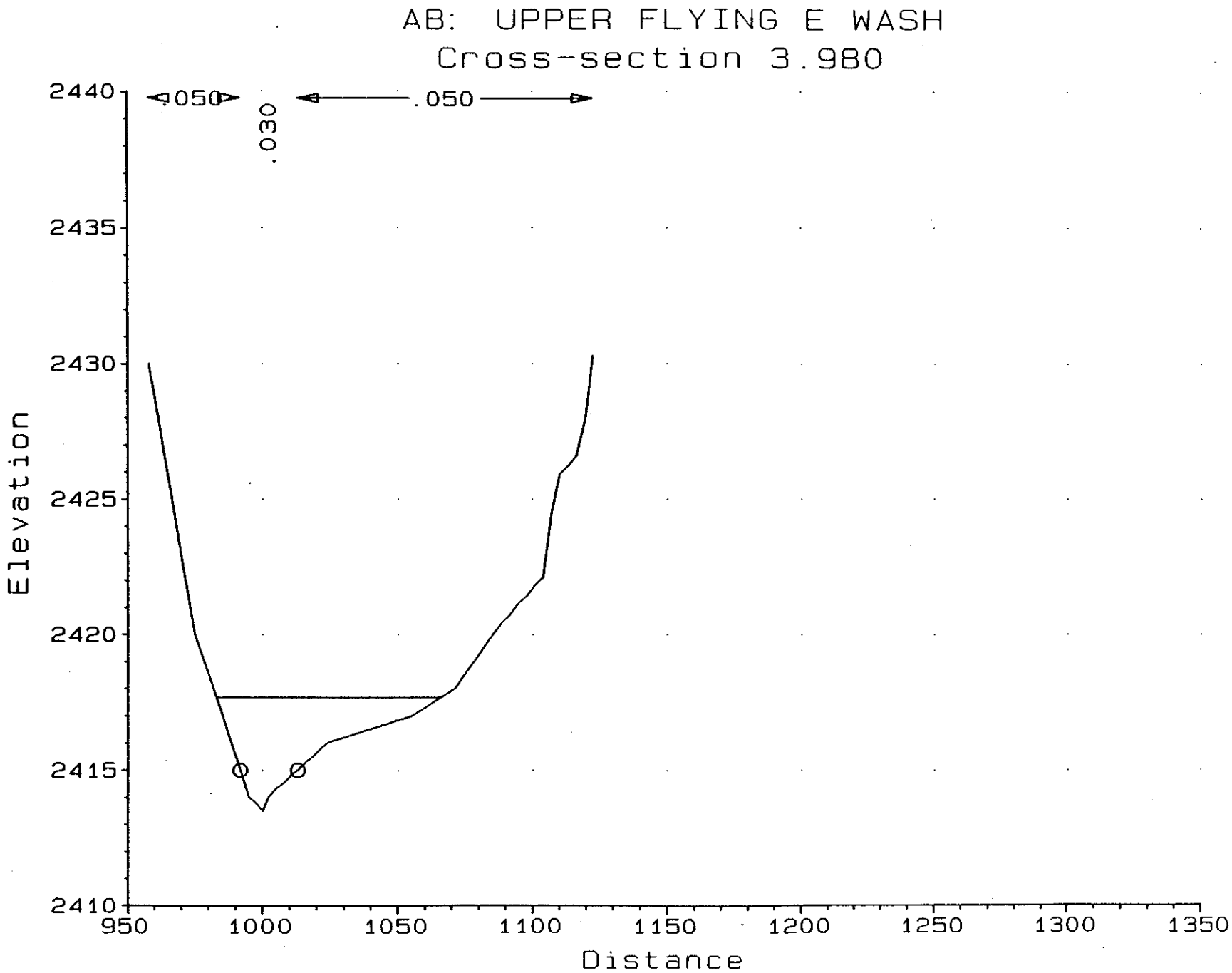
1250
1300
Distance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Cross-section 3.980
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.050
2440
2435
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Elevation
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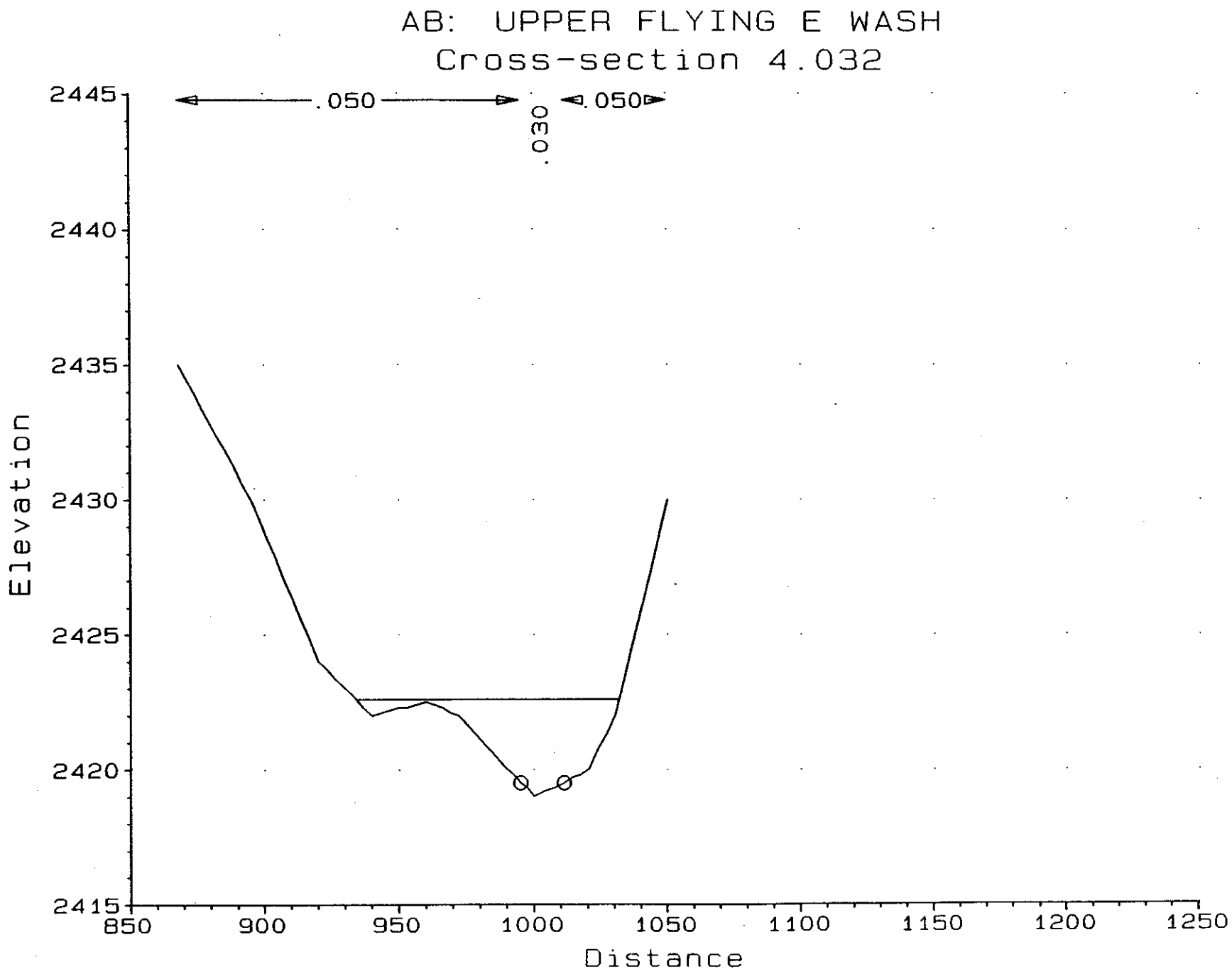
1300
1350
Distance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Cross-section 4.032
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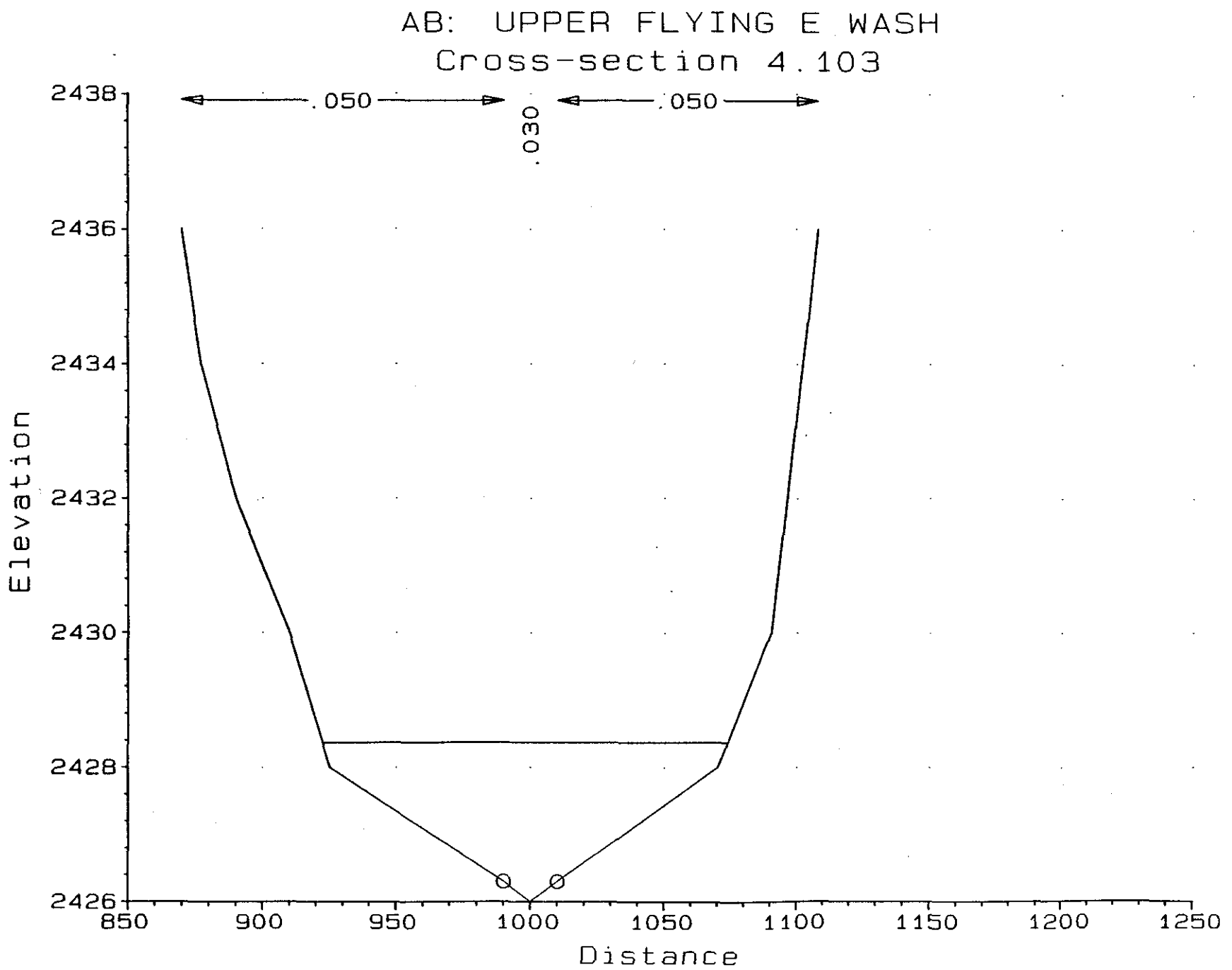
1100
1150
1200
1250
Distance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Cross-section 4.103
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.030
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Elevation
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1100
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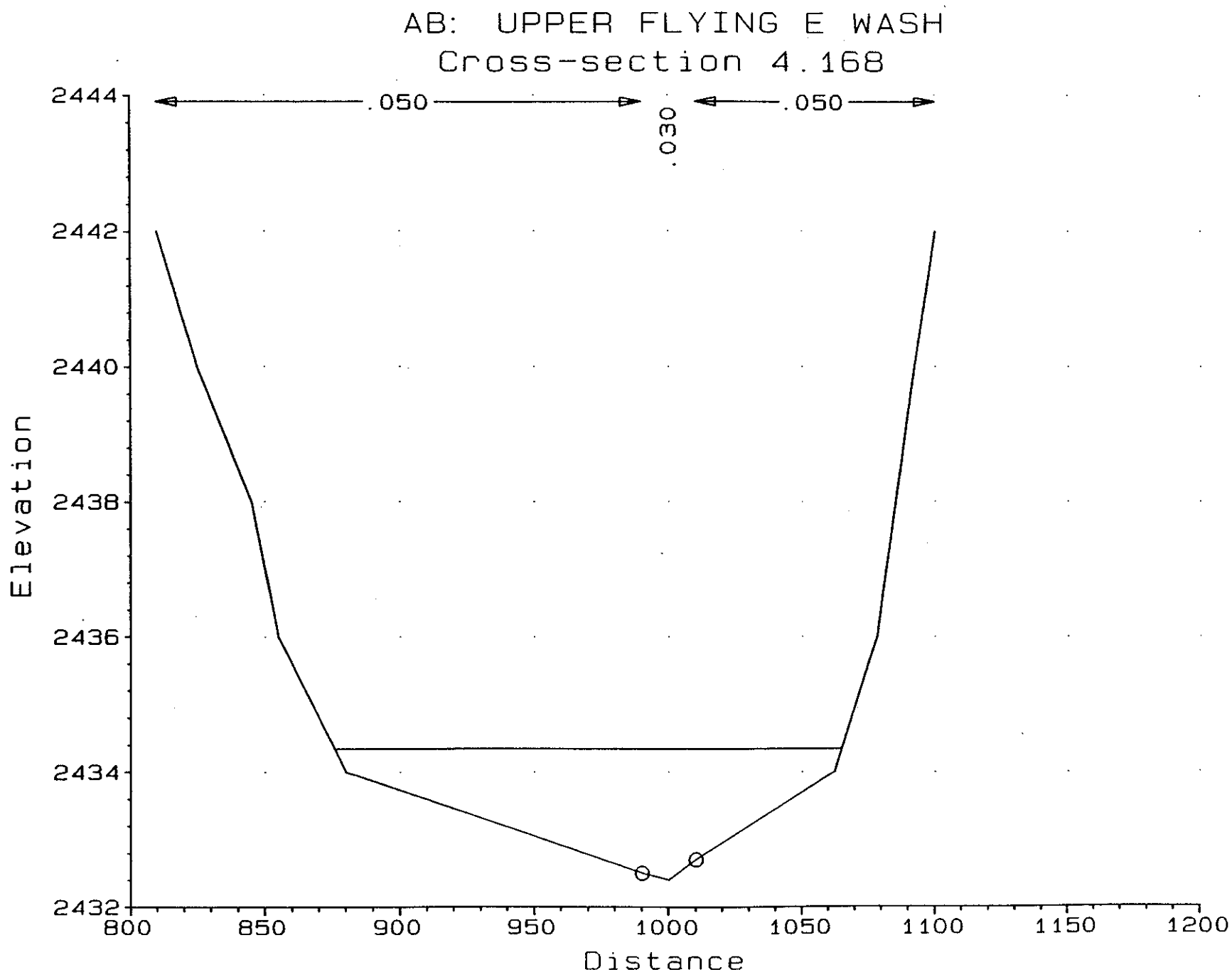
1200
1250
Distance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Cross-section 4.168
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.050
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2436
2434
2432
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900
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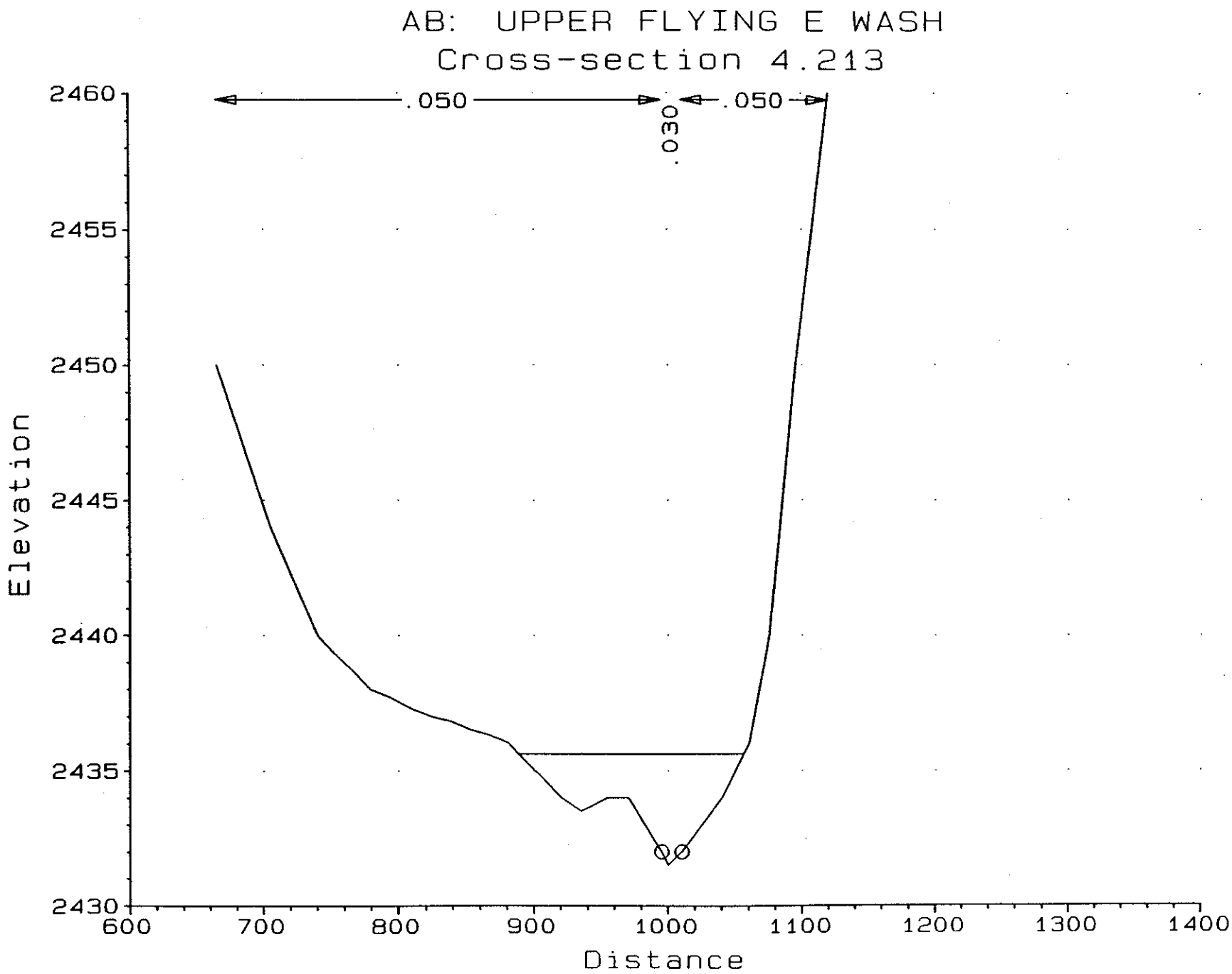
1050
1100
1150
1200
Distance


AB: UPPER FLYING E WASH
Cross-section 4.213
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.050
.030
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2435
2430
Elevation
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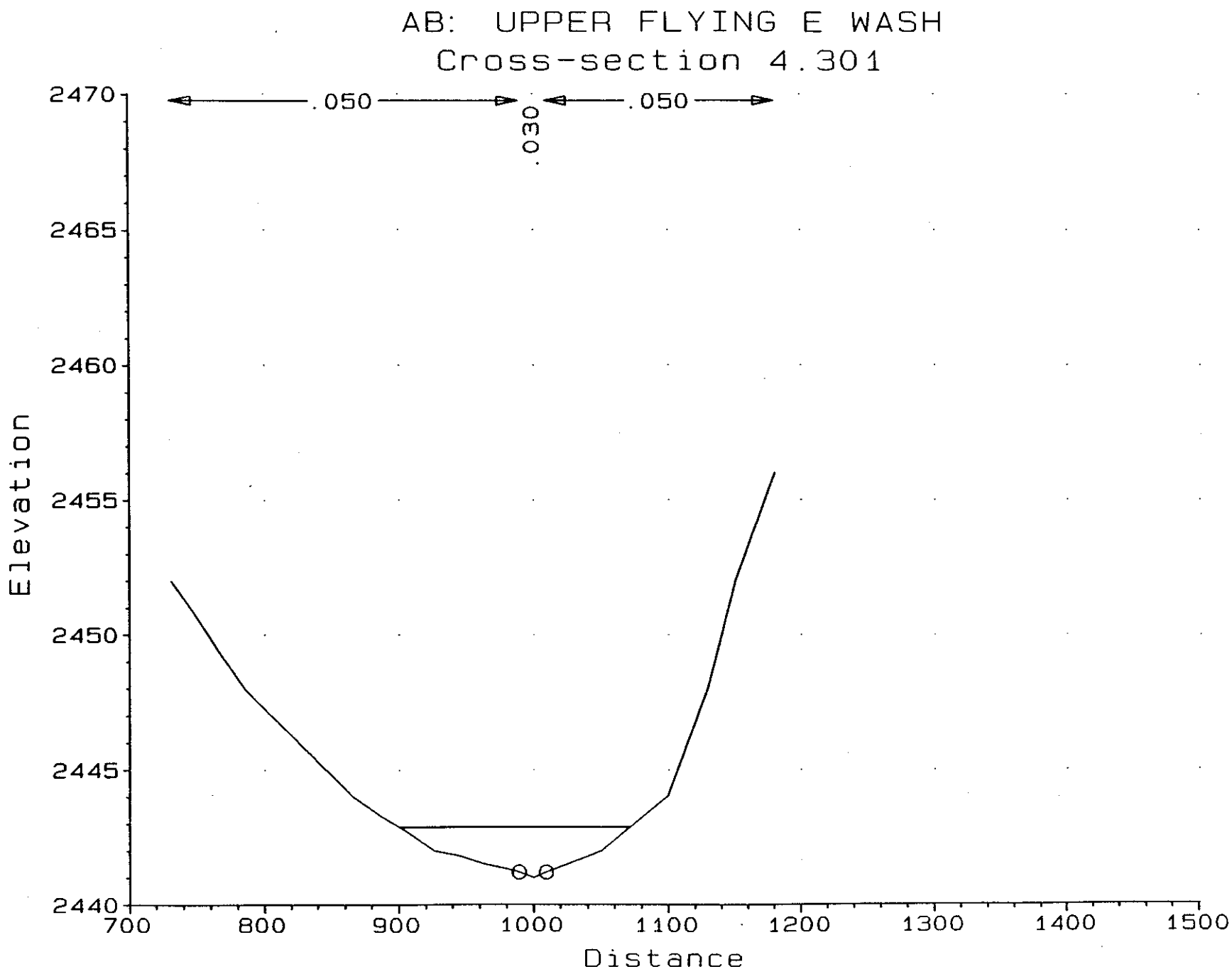
1300
1400
Distance


AB: UPPER FLYING E WASH
Cross-section 4.301
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Elevation
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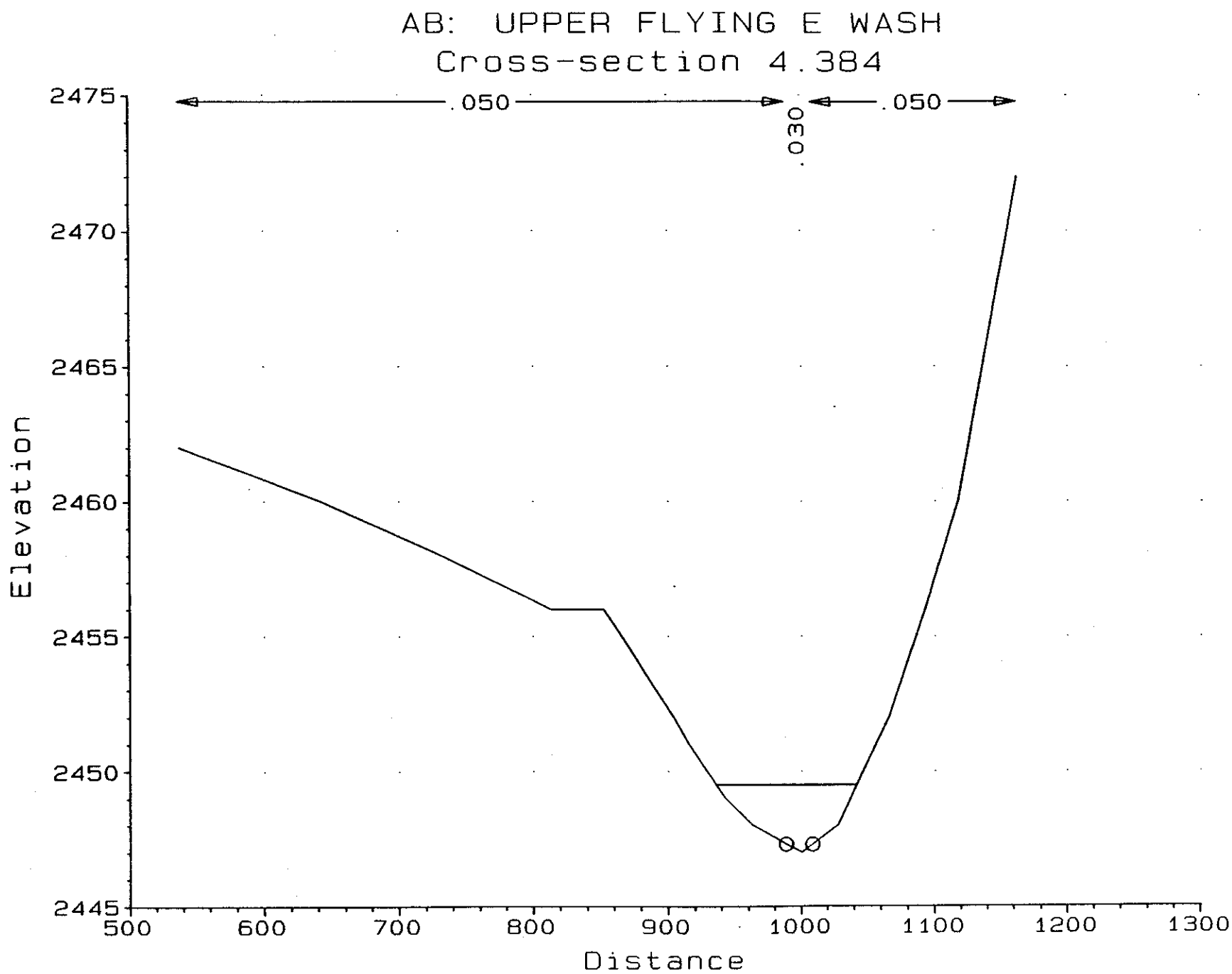
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Elevation
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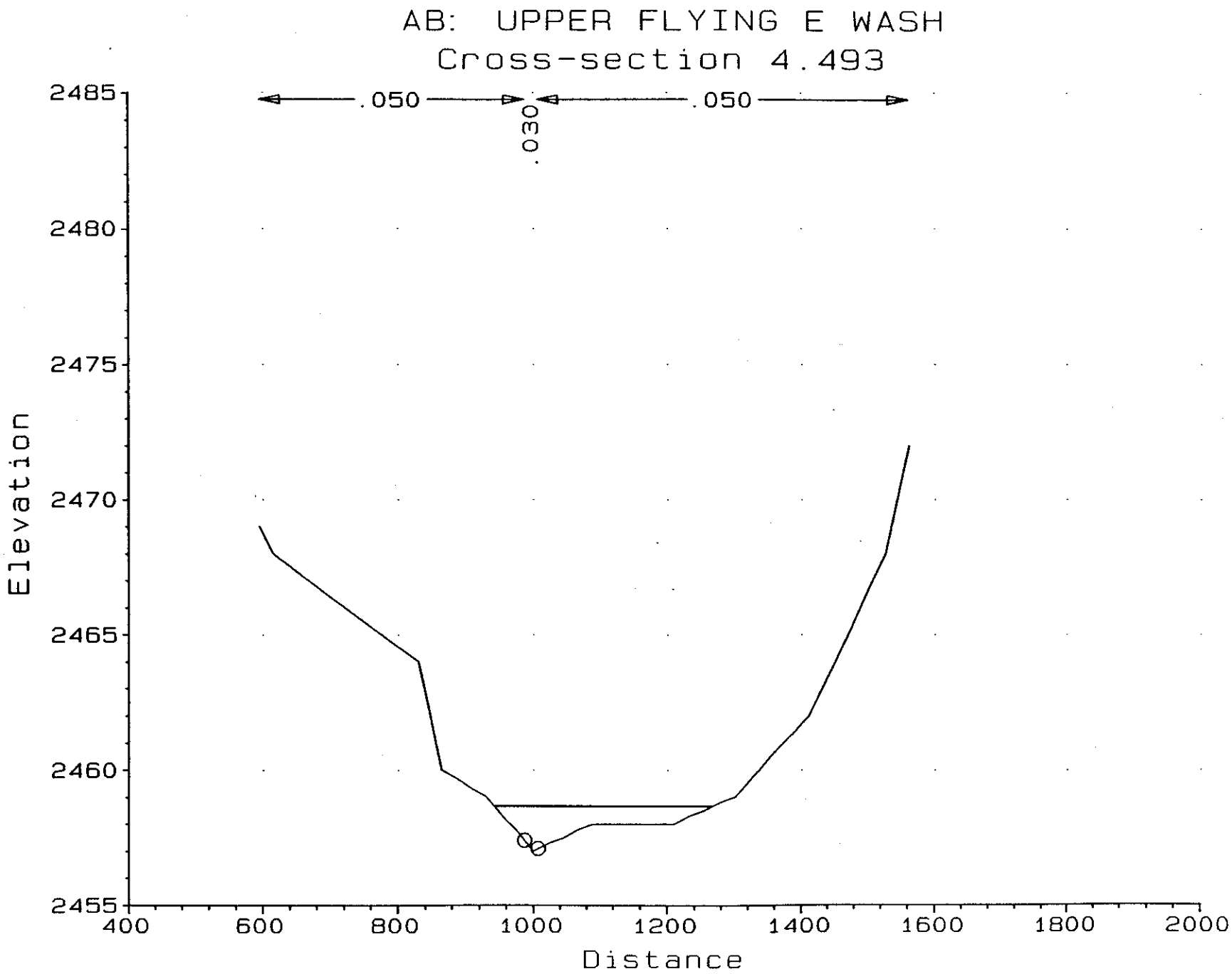
Distance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Cross-section 4.493
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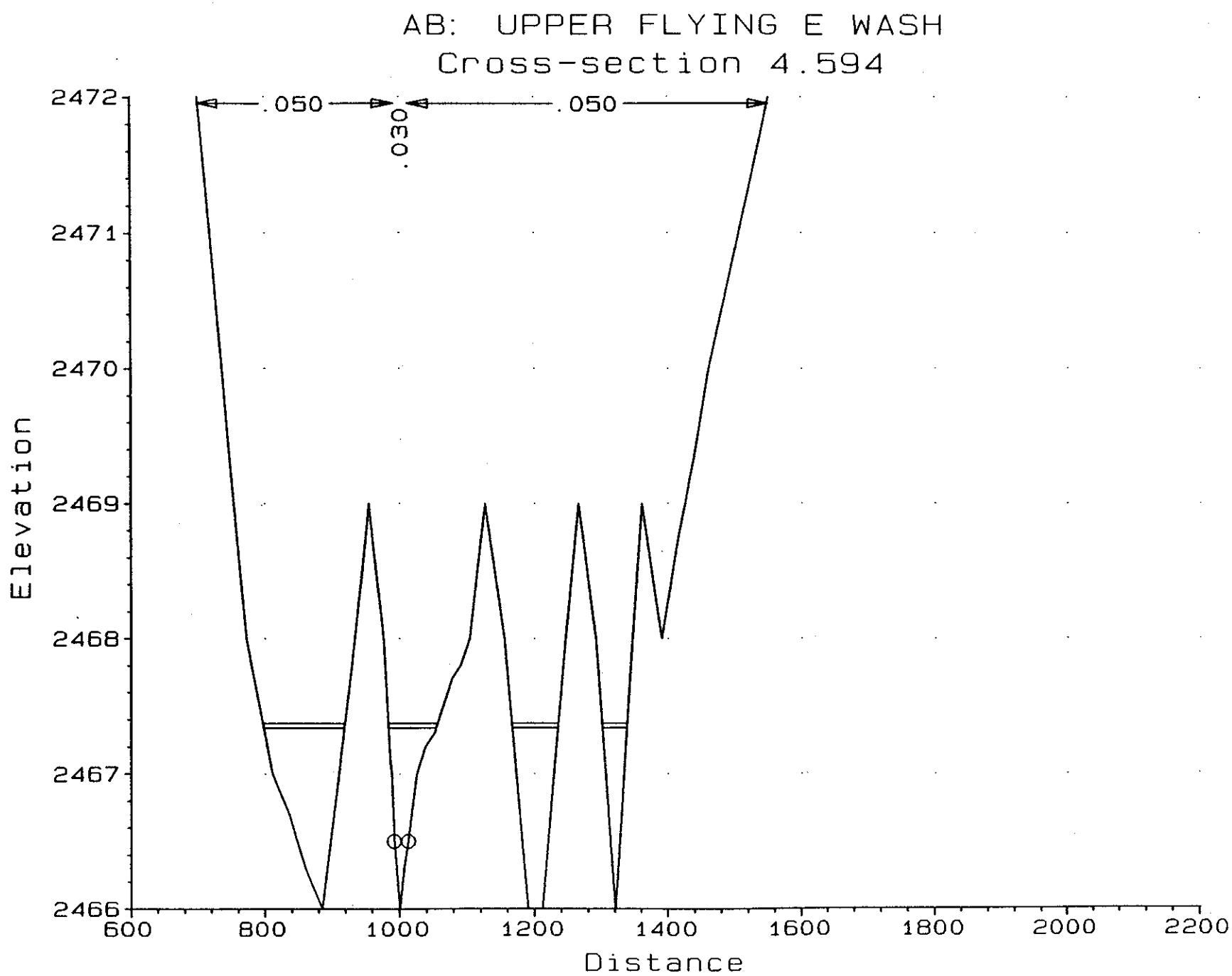
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Elevation
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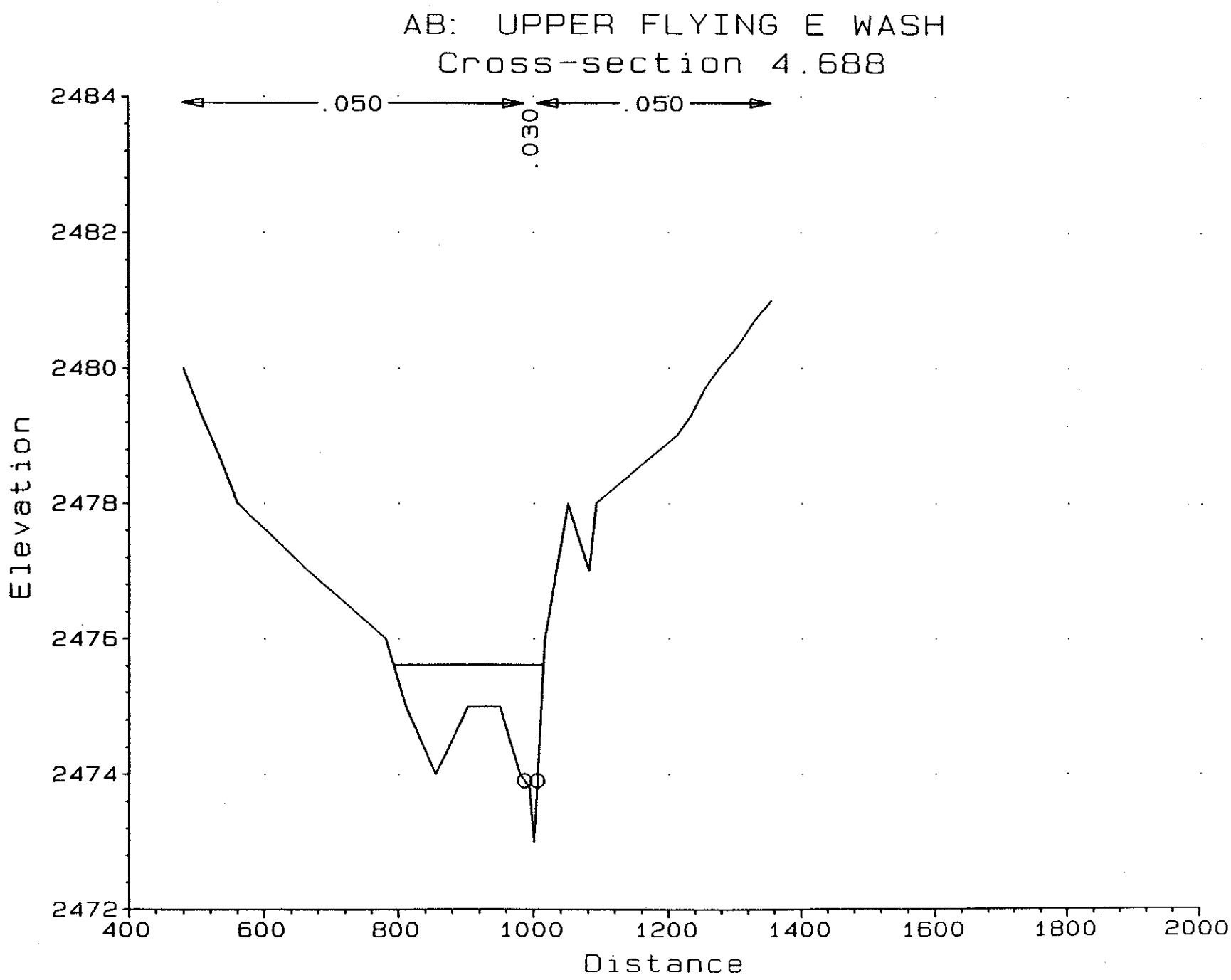
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Cross-section 4.688
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Elevation
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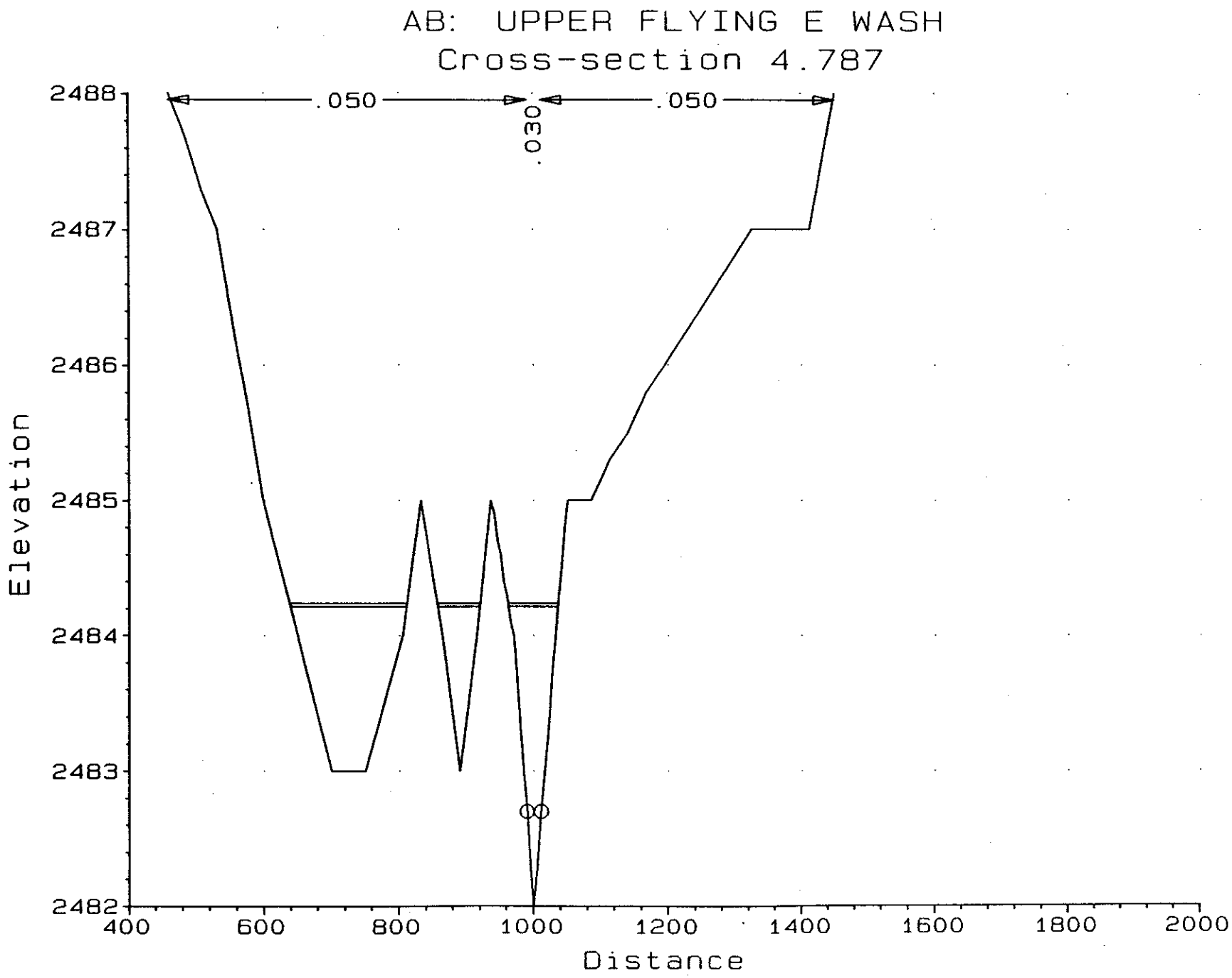
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Cross-section 4.787
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.050
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2484
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Elevation
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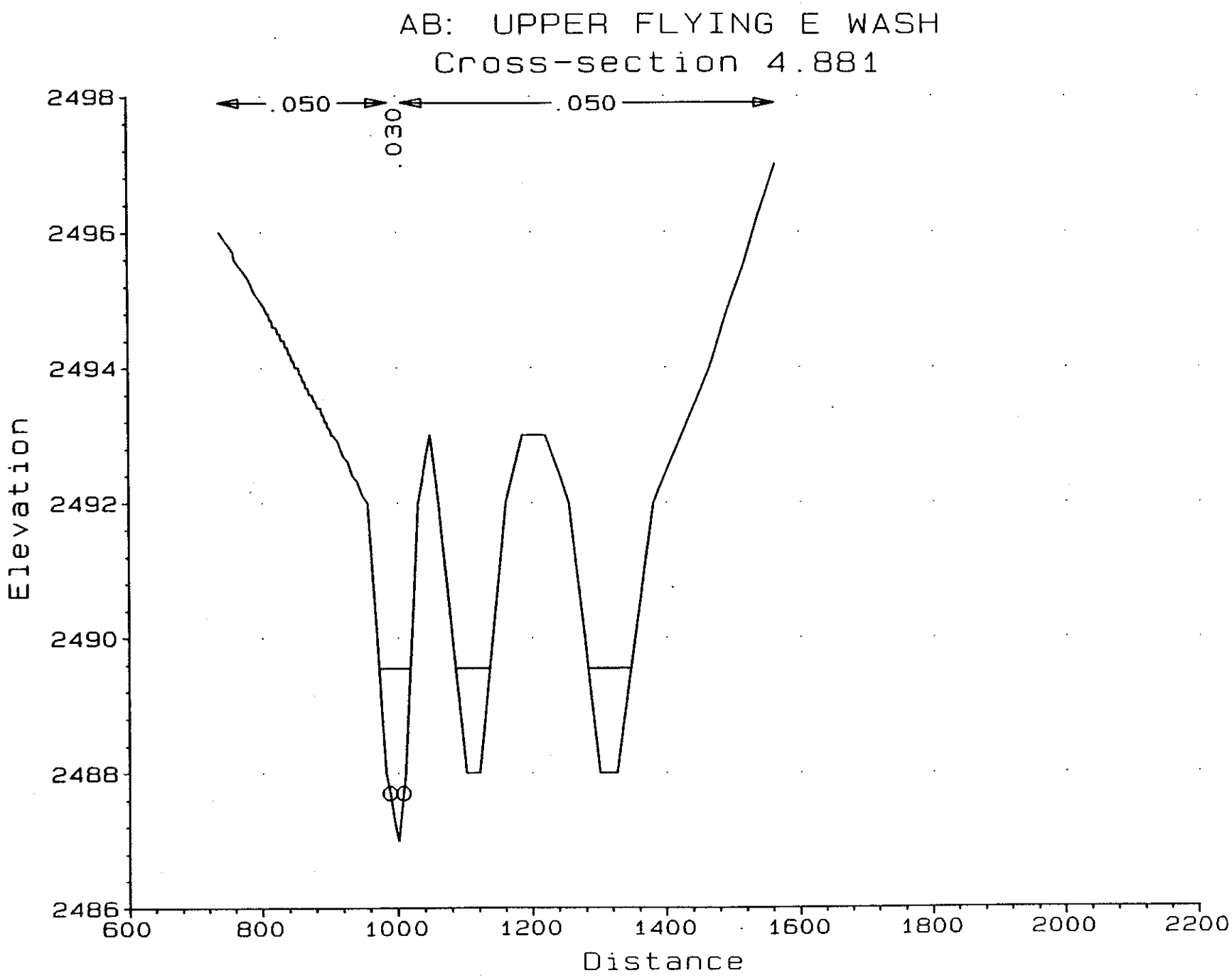
Distance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Elevation
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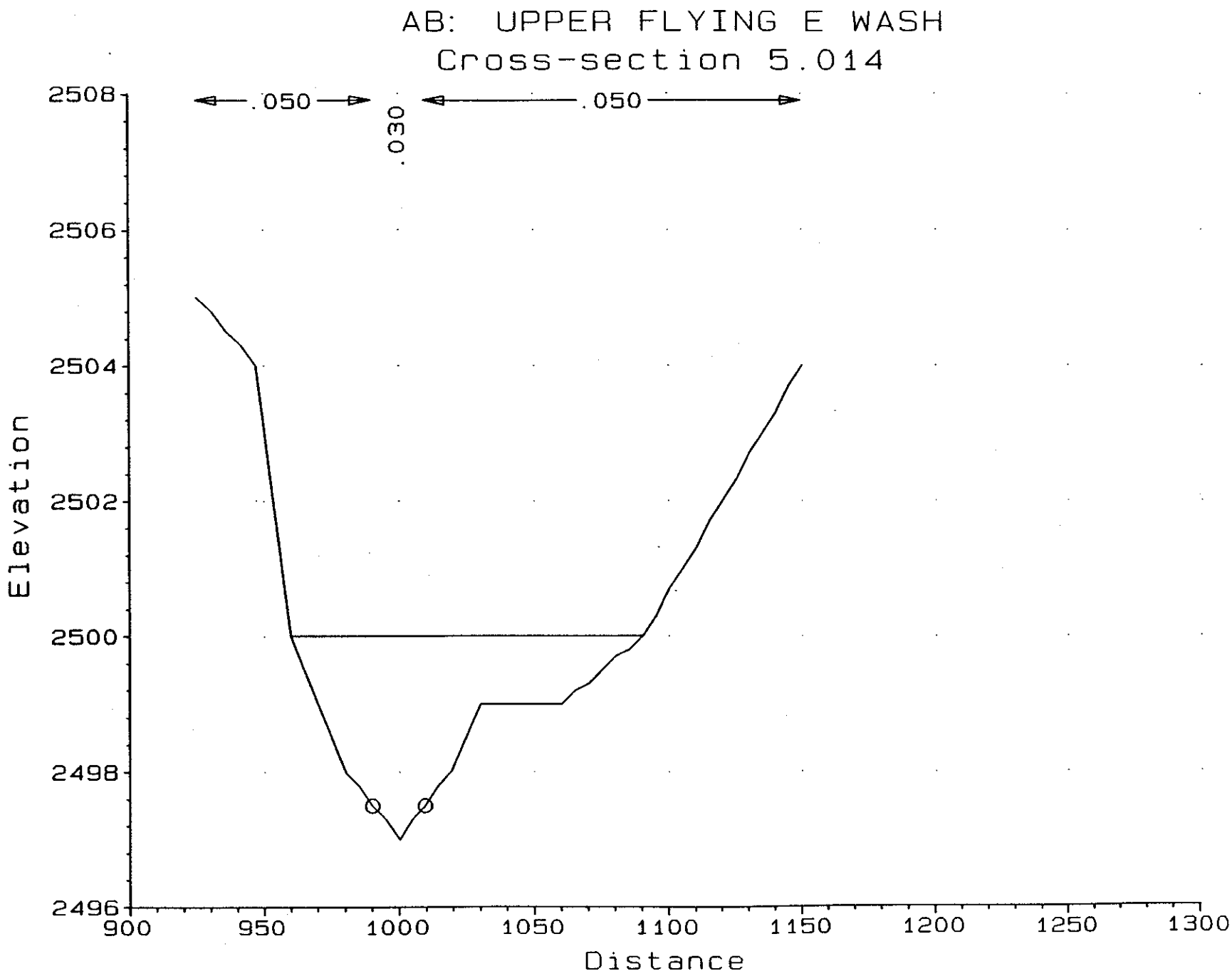
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Cross-section 5.014
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Elevation
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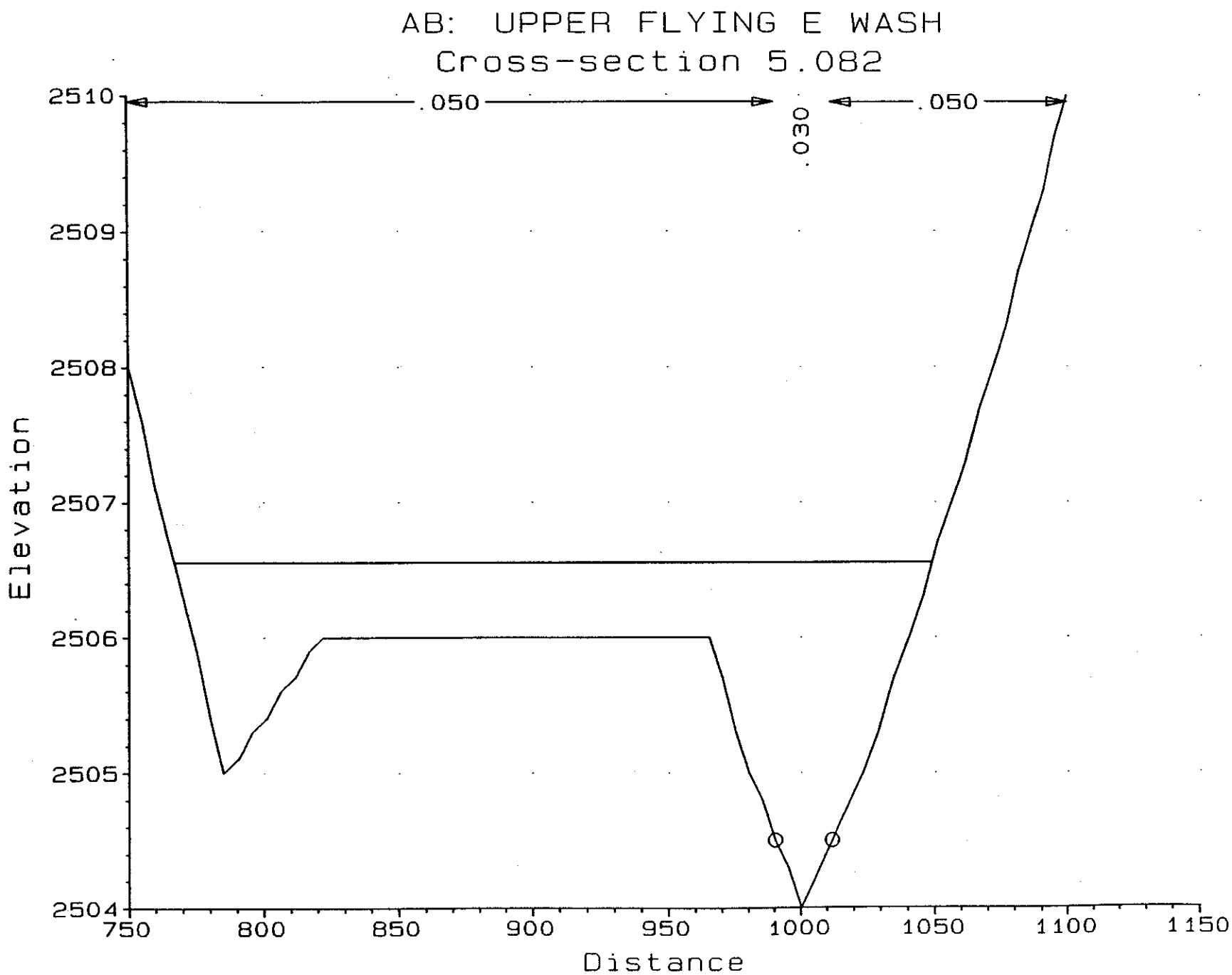
AB: UPPER FLYING E WASH
Cross-section 5.082
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Elevation
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1150
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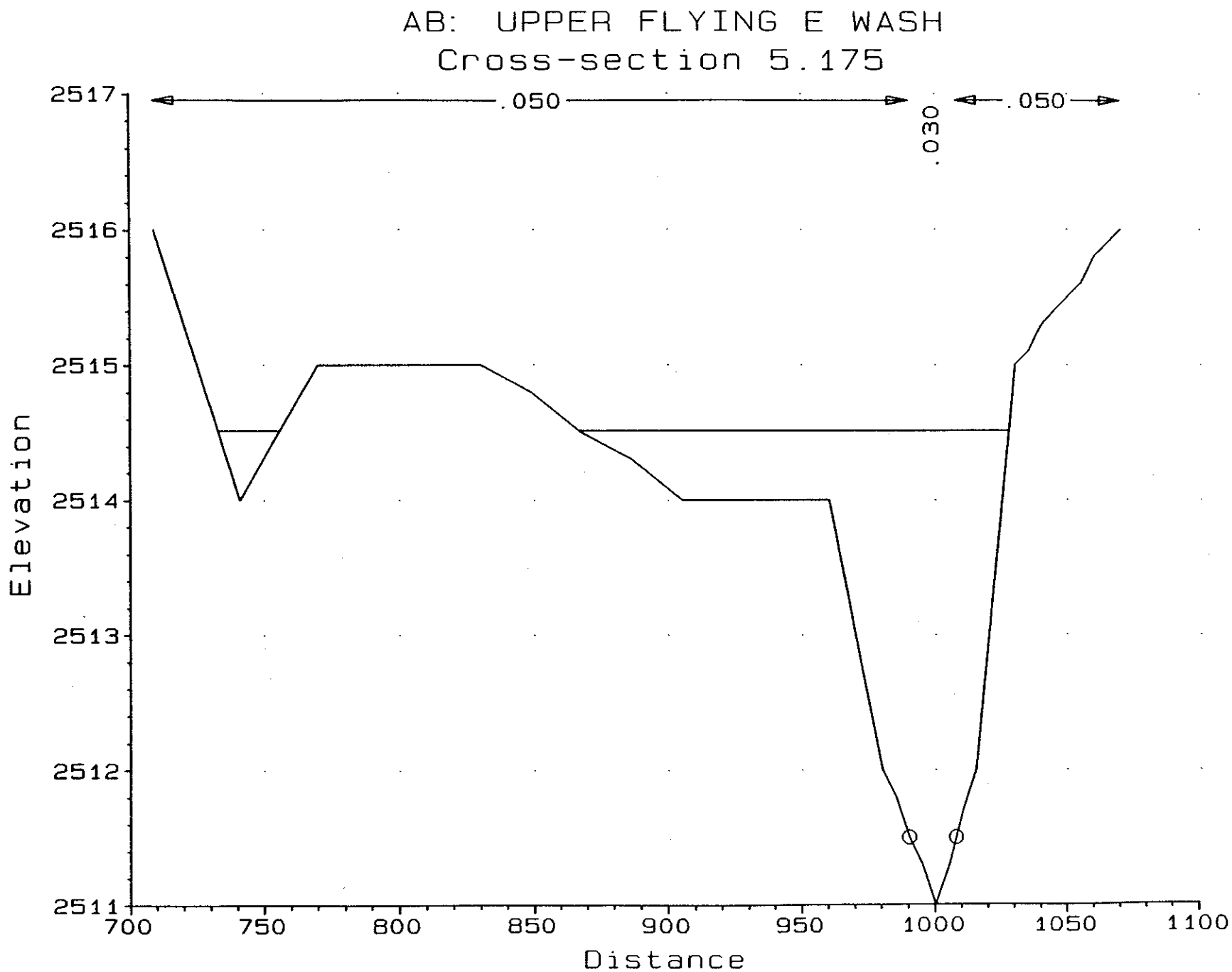
AB: UPPER FLYING E WASH
Cross-section 5.175
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Elevation
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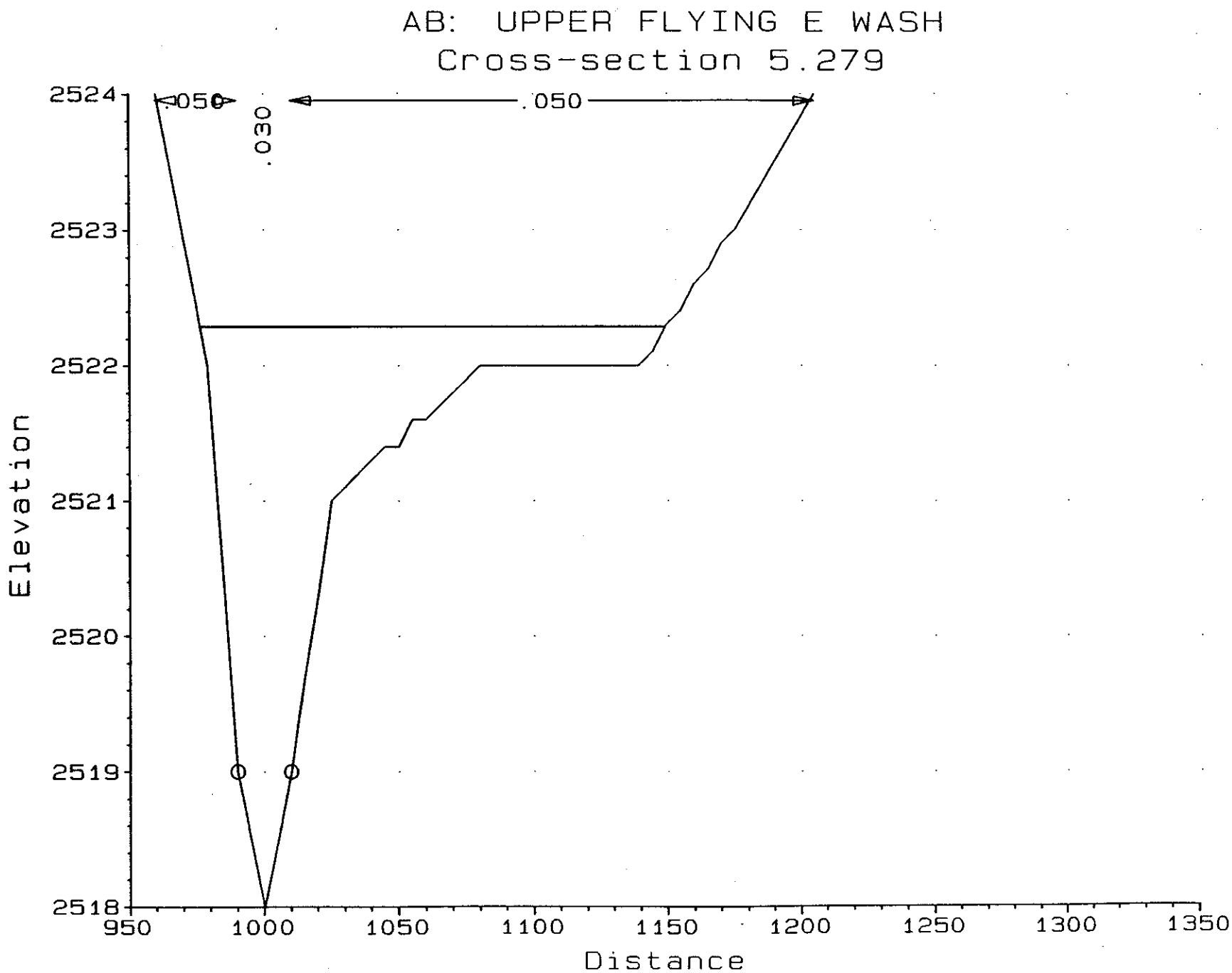
Distance


AB: UPPER FLYING E WASH
Cross-section 5.279
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.050
.030
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2523
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2521
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Elevation
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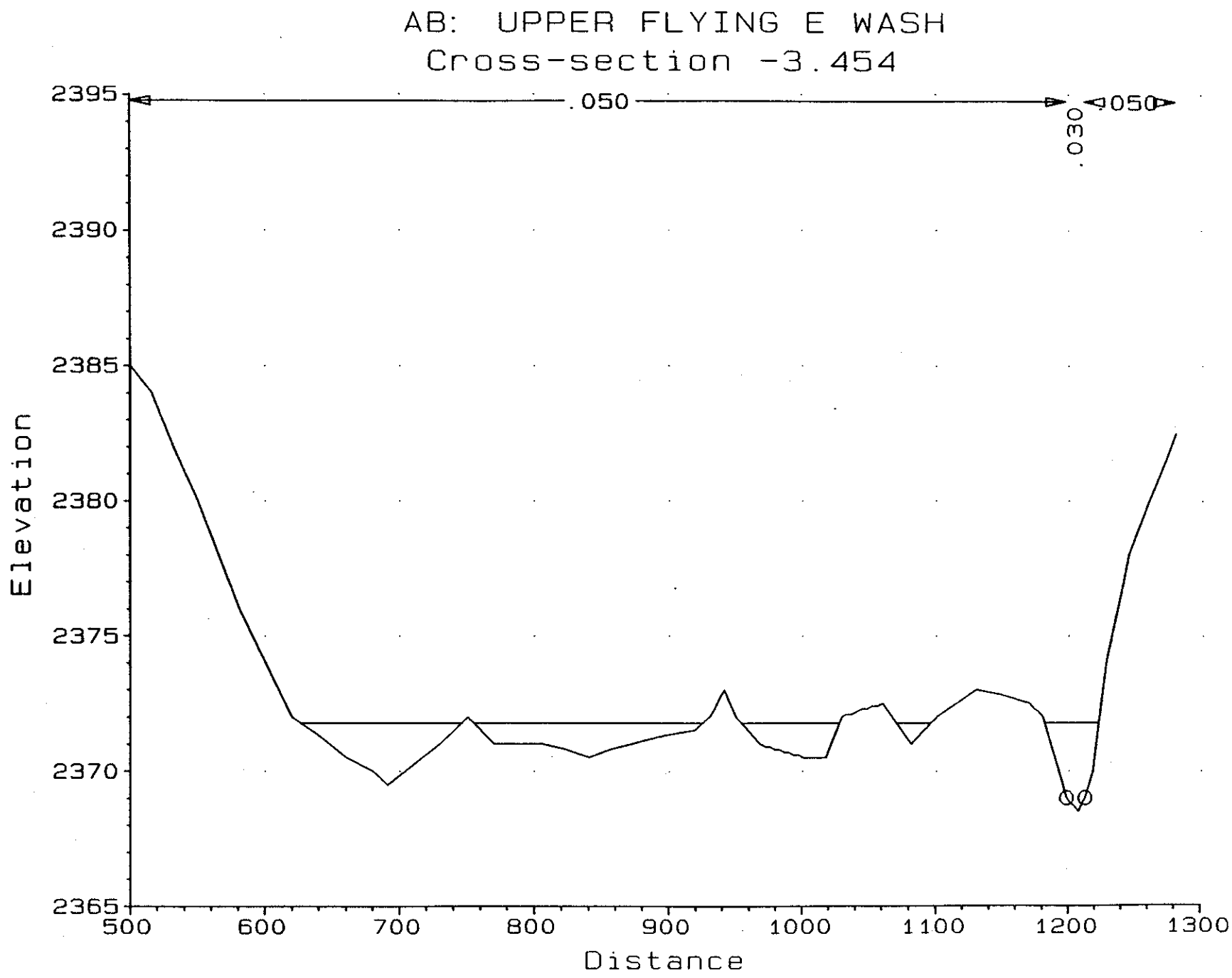
1350
Distance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Cross-section -3.454
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.050
.030
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Elevation
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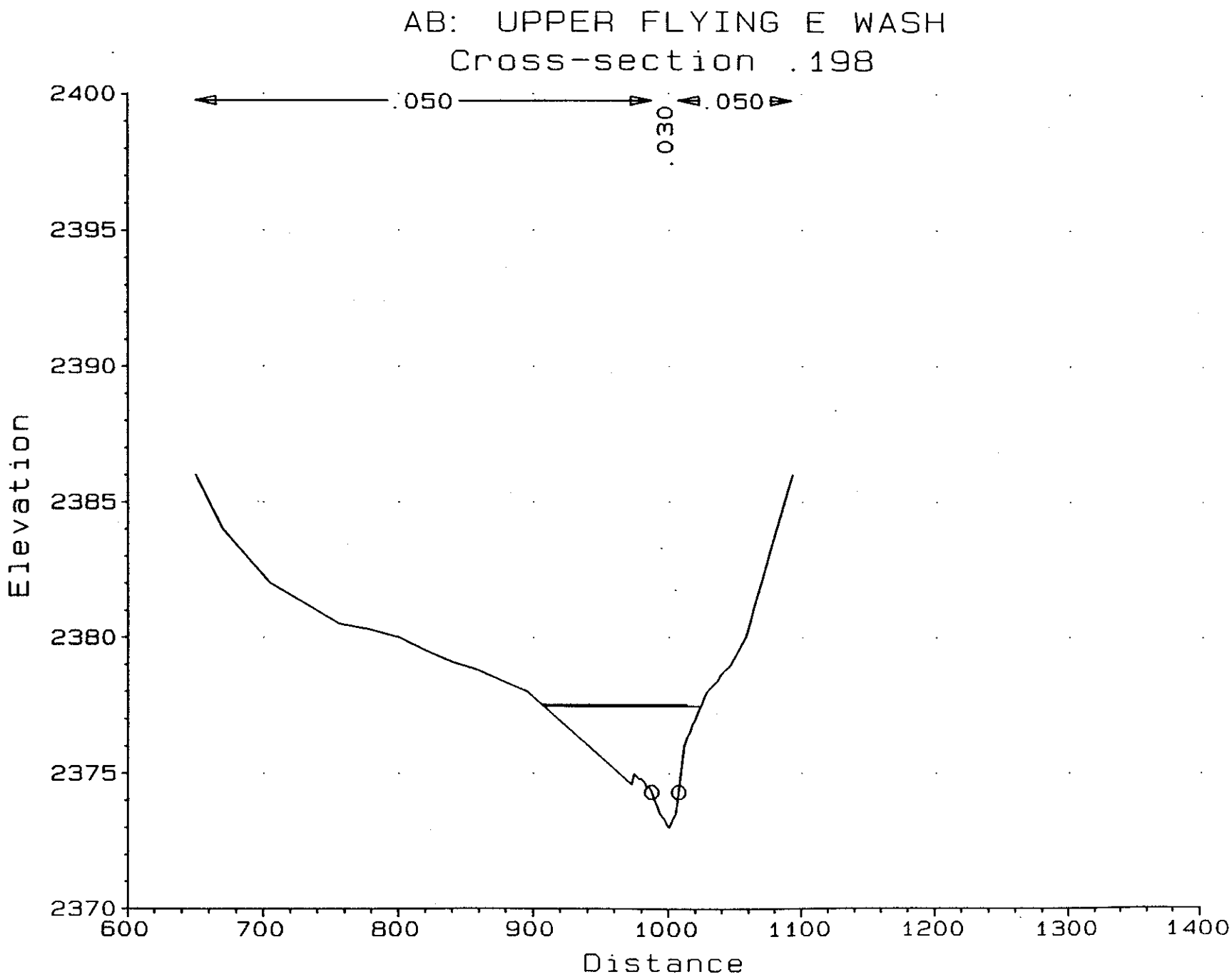
Distance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Cross-section .198
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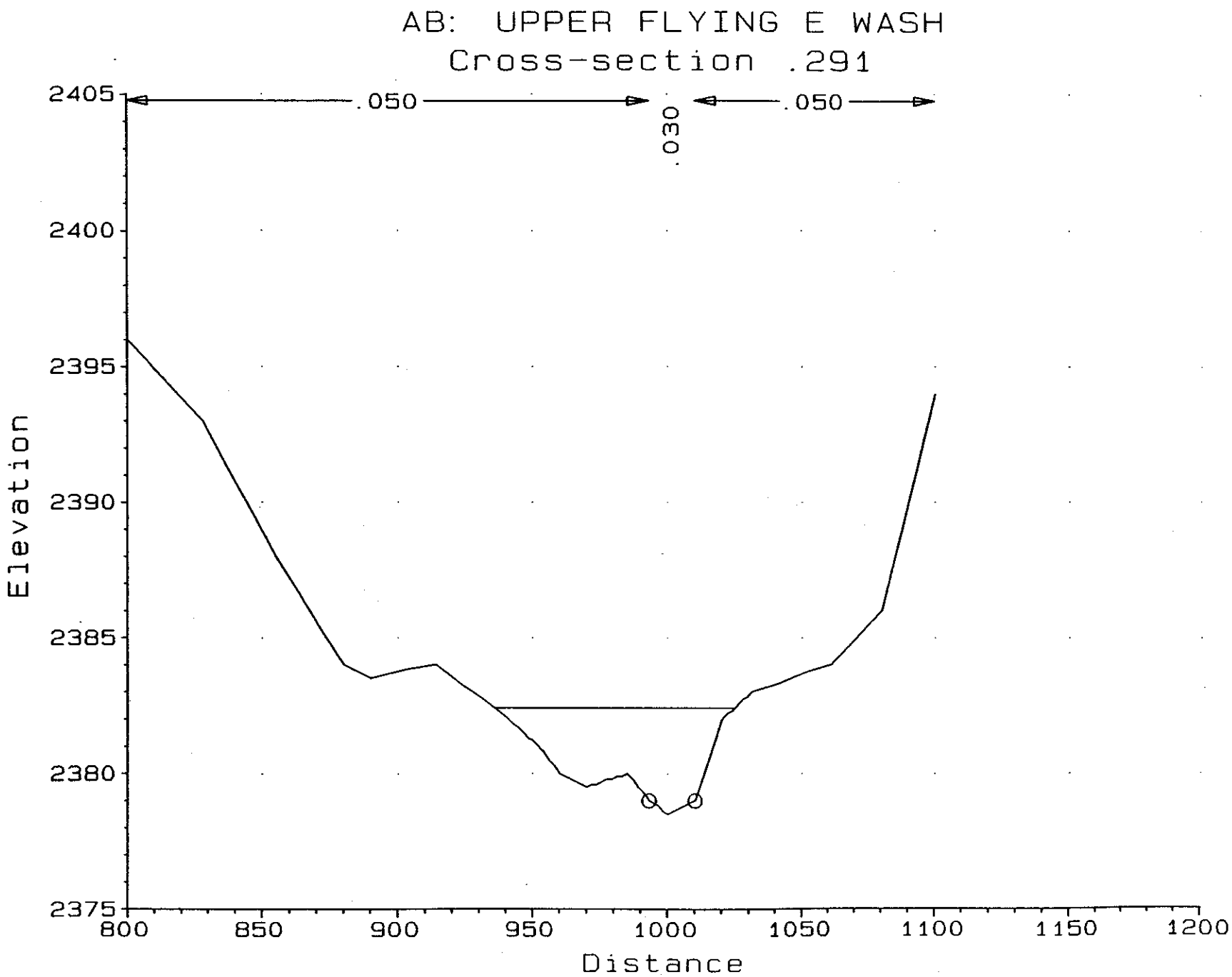
Distance


AB: UPPER FLYING E WASH
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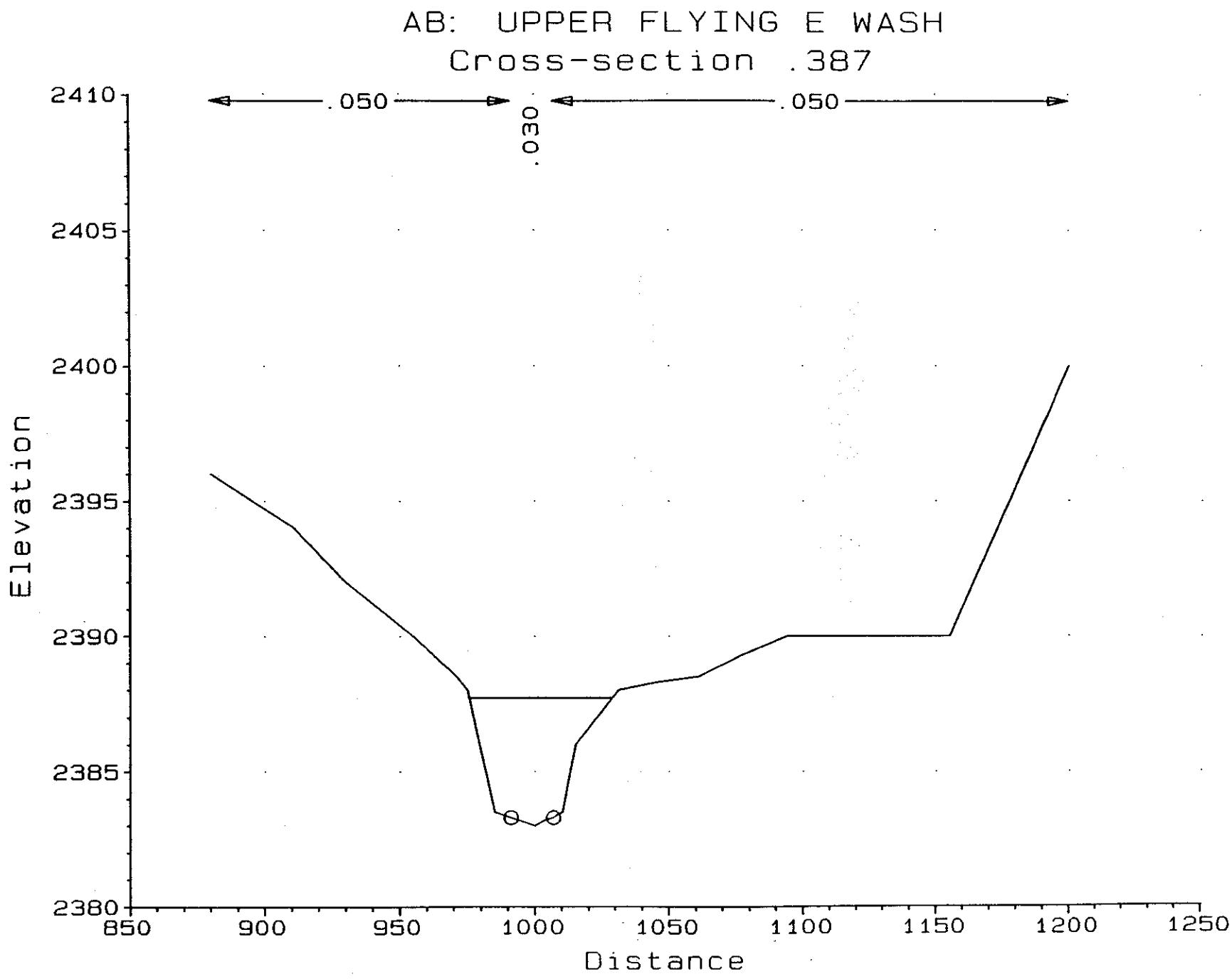
1100
1150
1200
Distance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Cross-section .387
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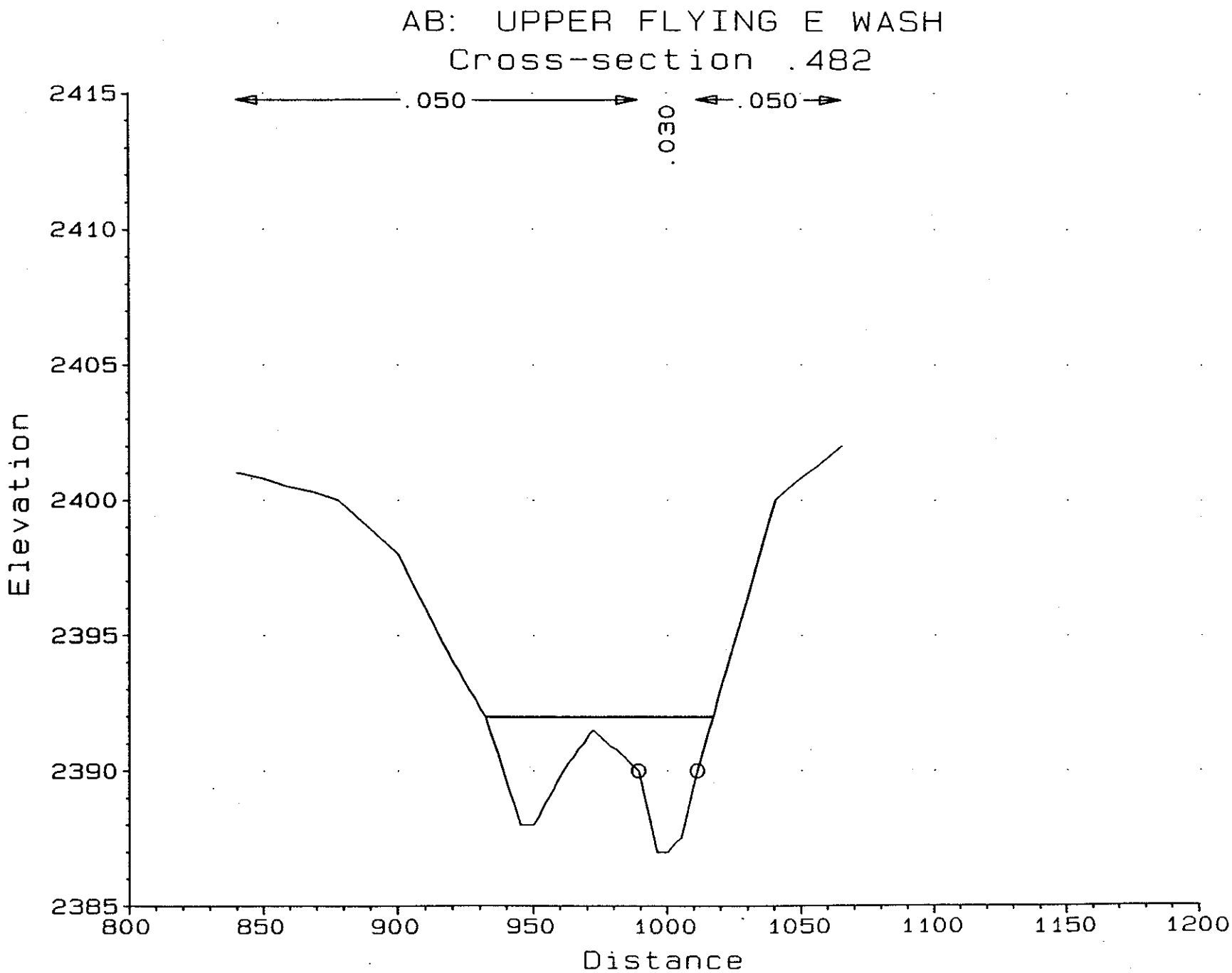
1200
1250
Distance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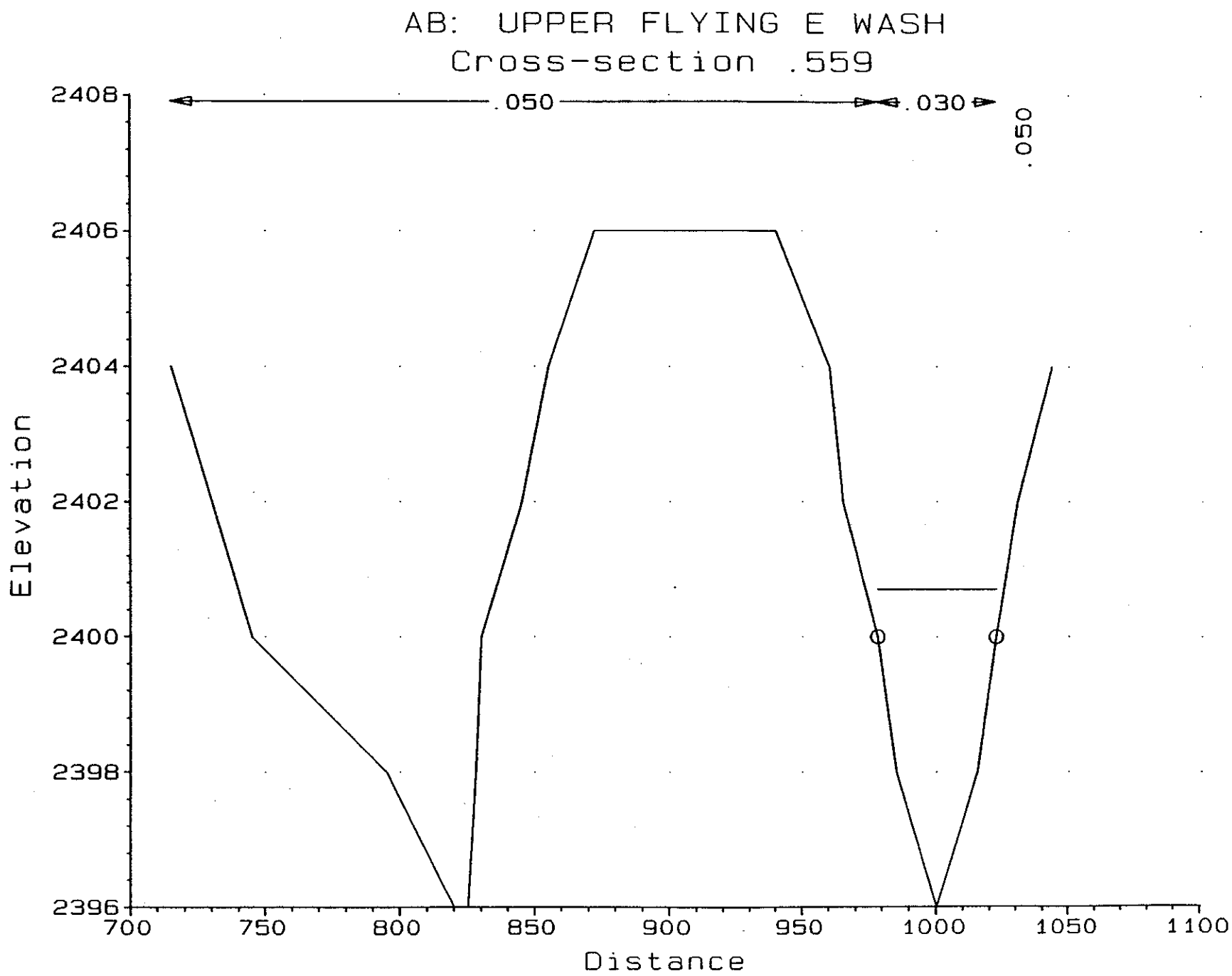
Distance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Cross-section .559
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Elevation
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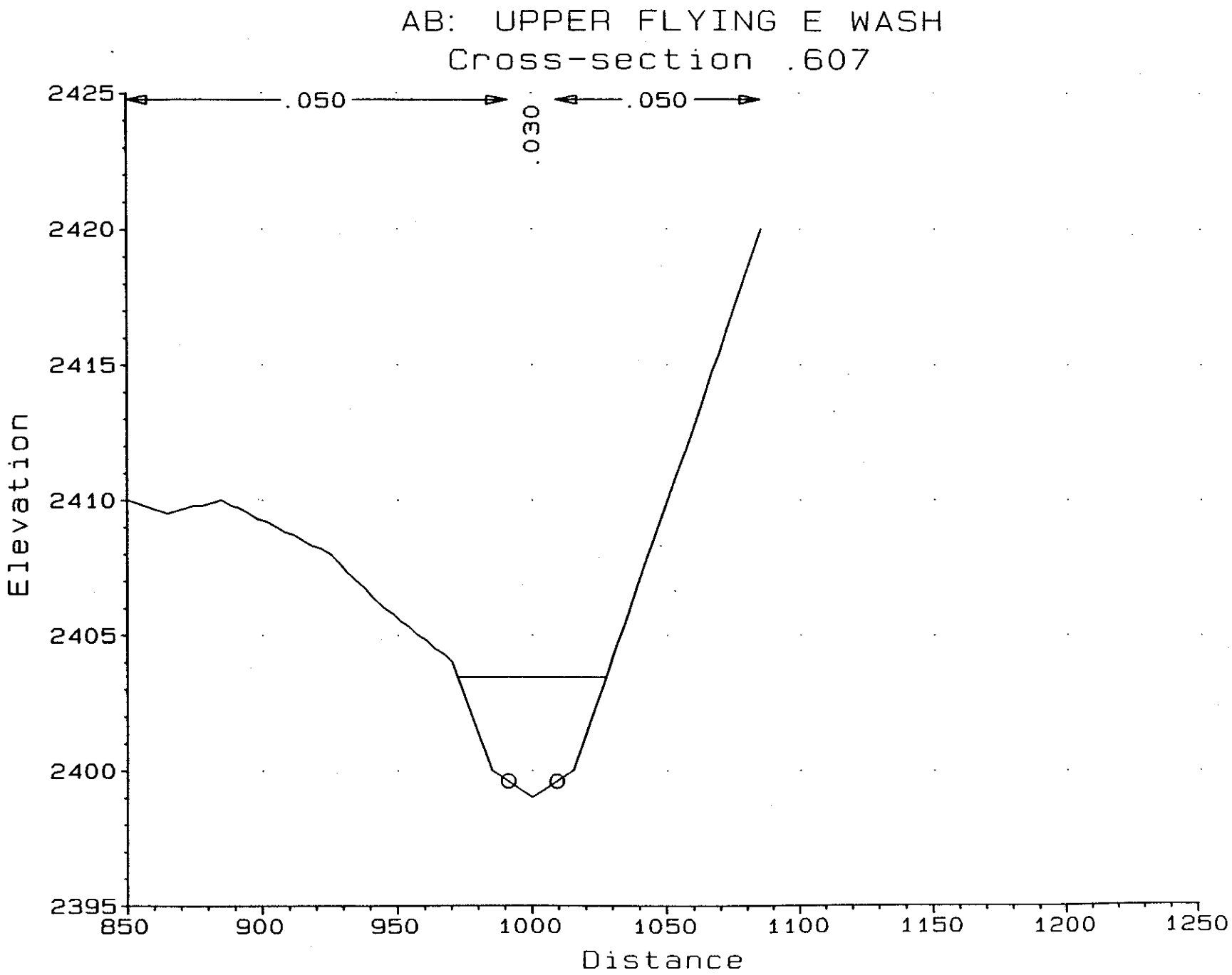
Distance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Elevation
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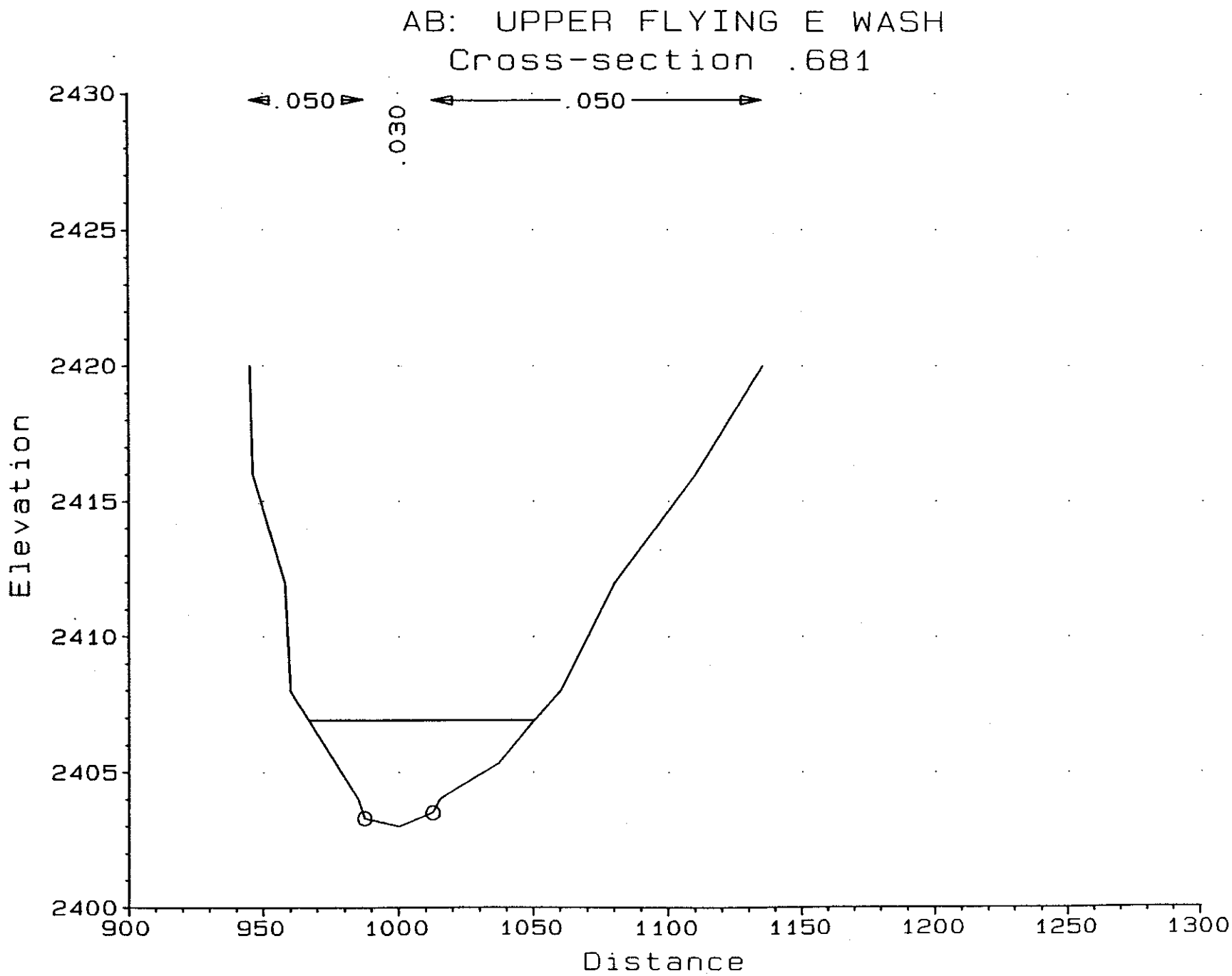
Distance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Cross-section .681
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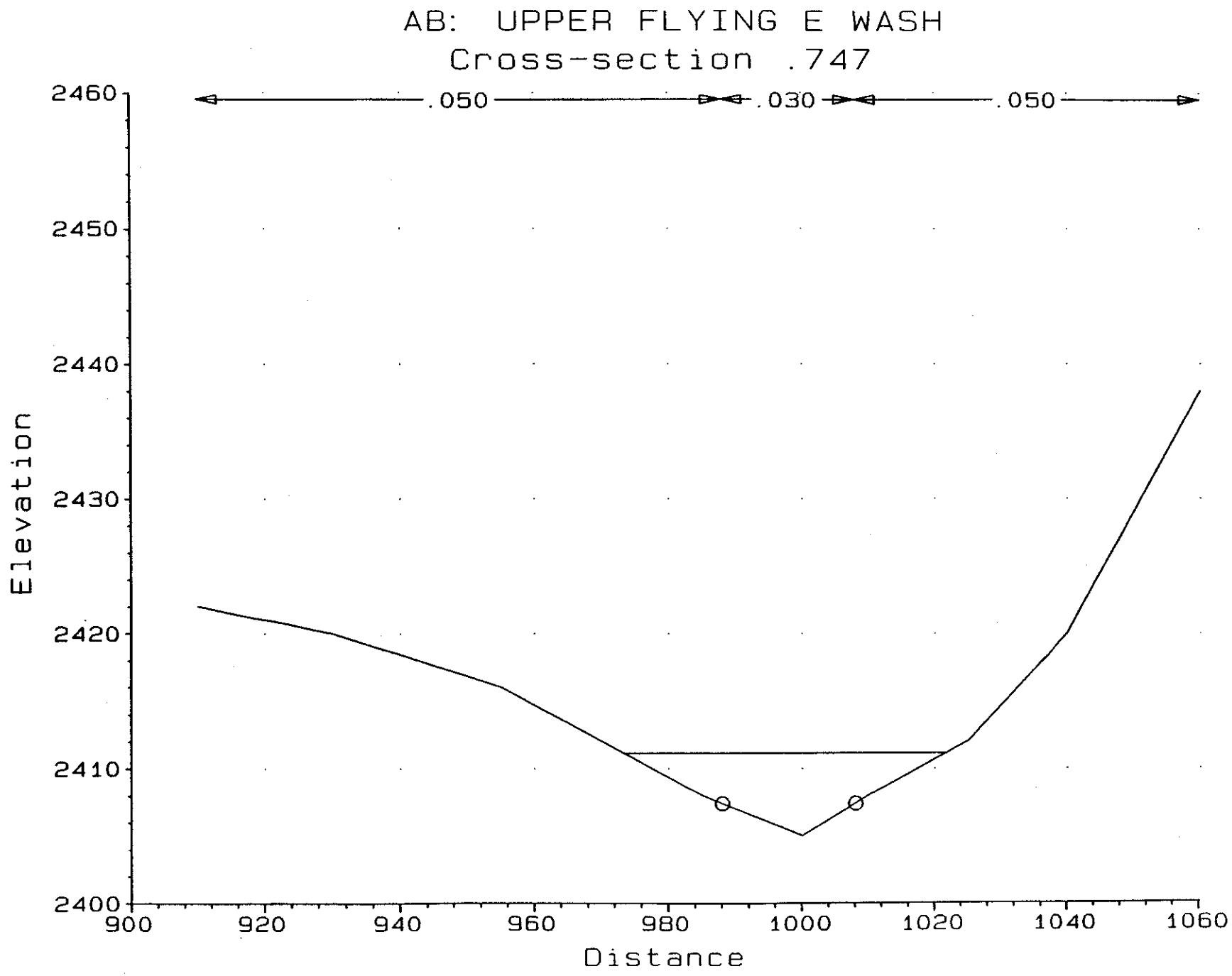
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1040
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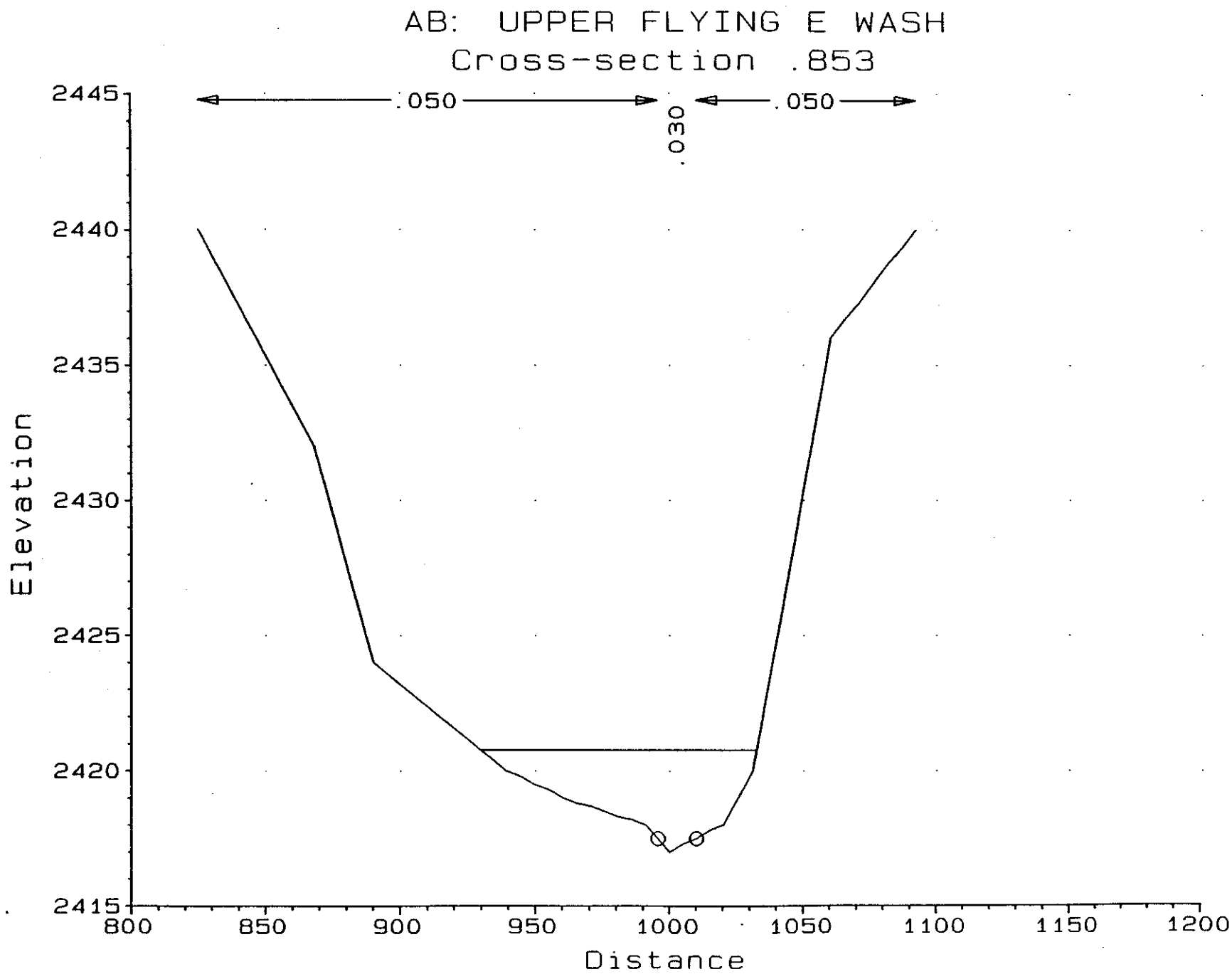
Distance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Cross-section .853
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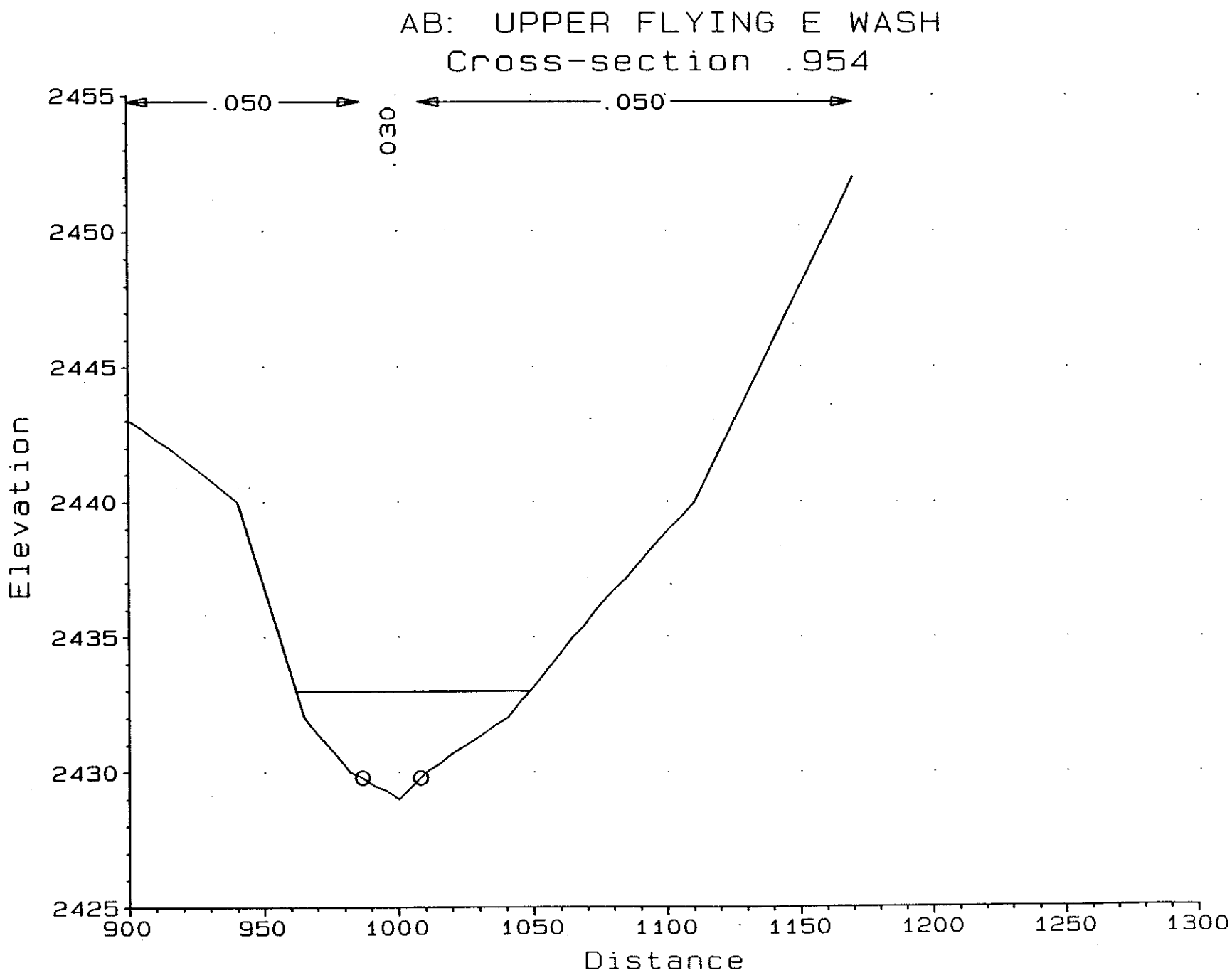
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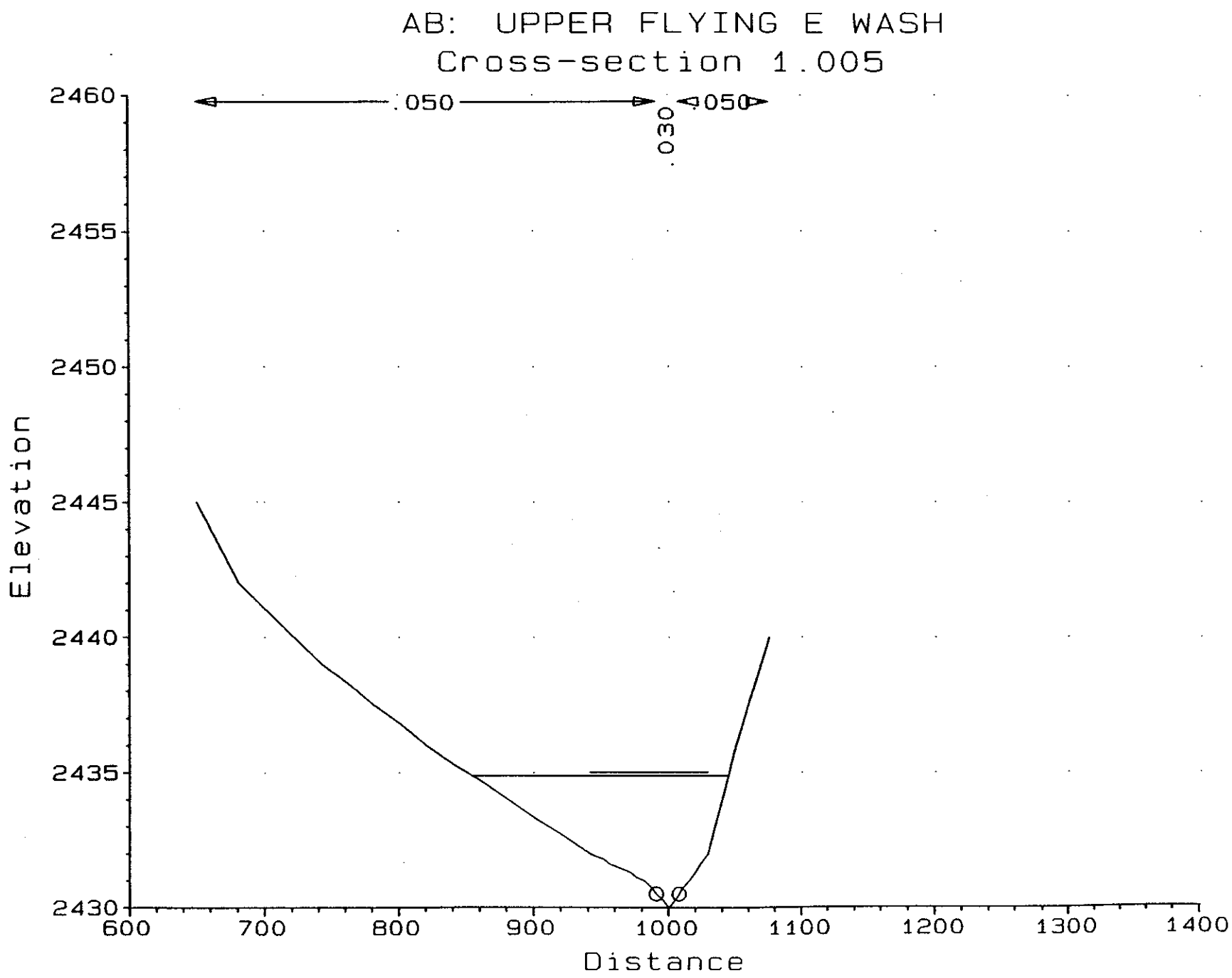
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Cross-section 1.005
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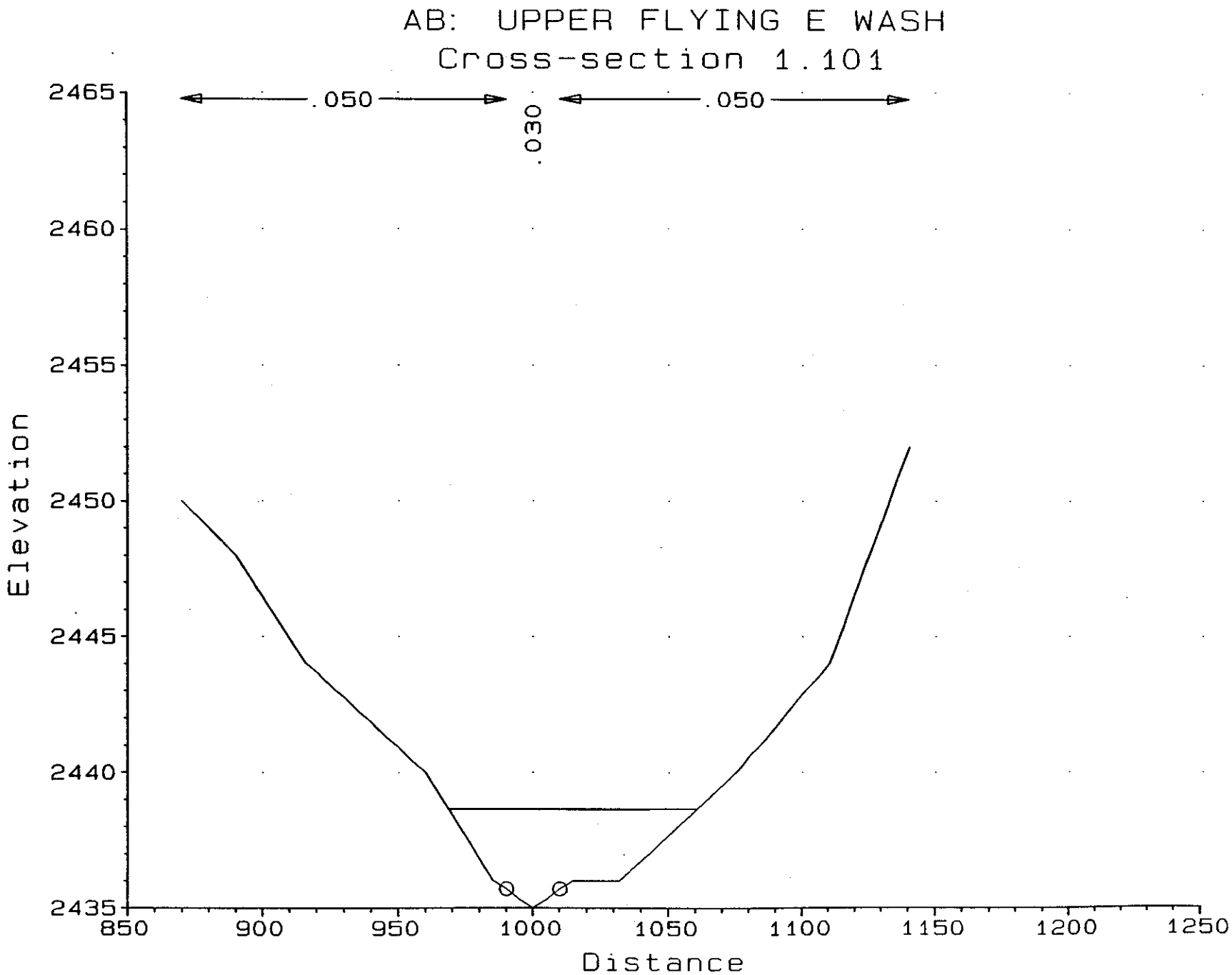
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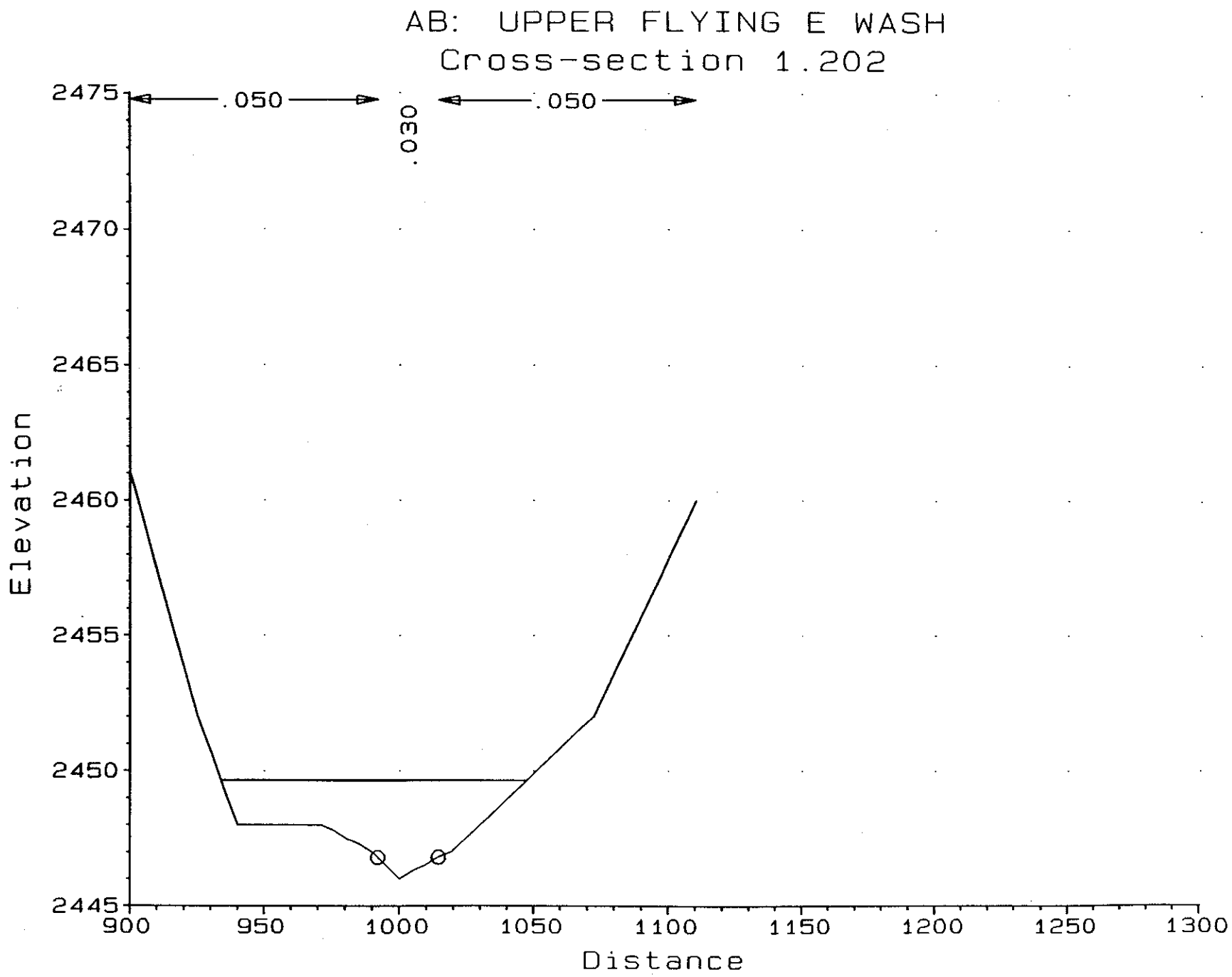
AB: UPPER FLYING E WASH
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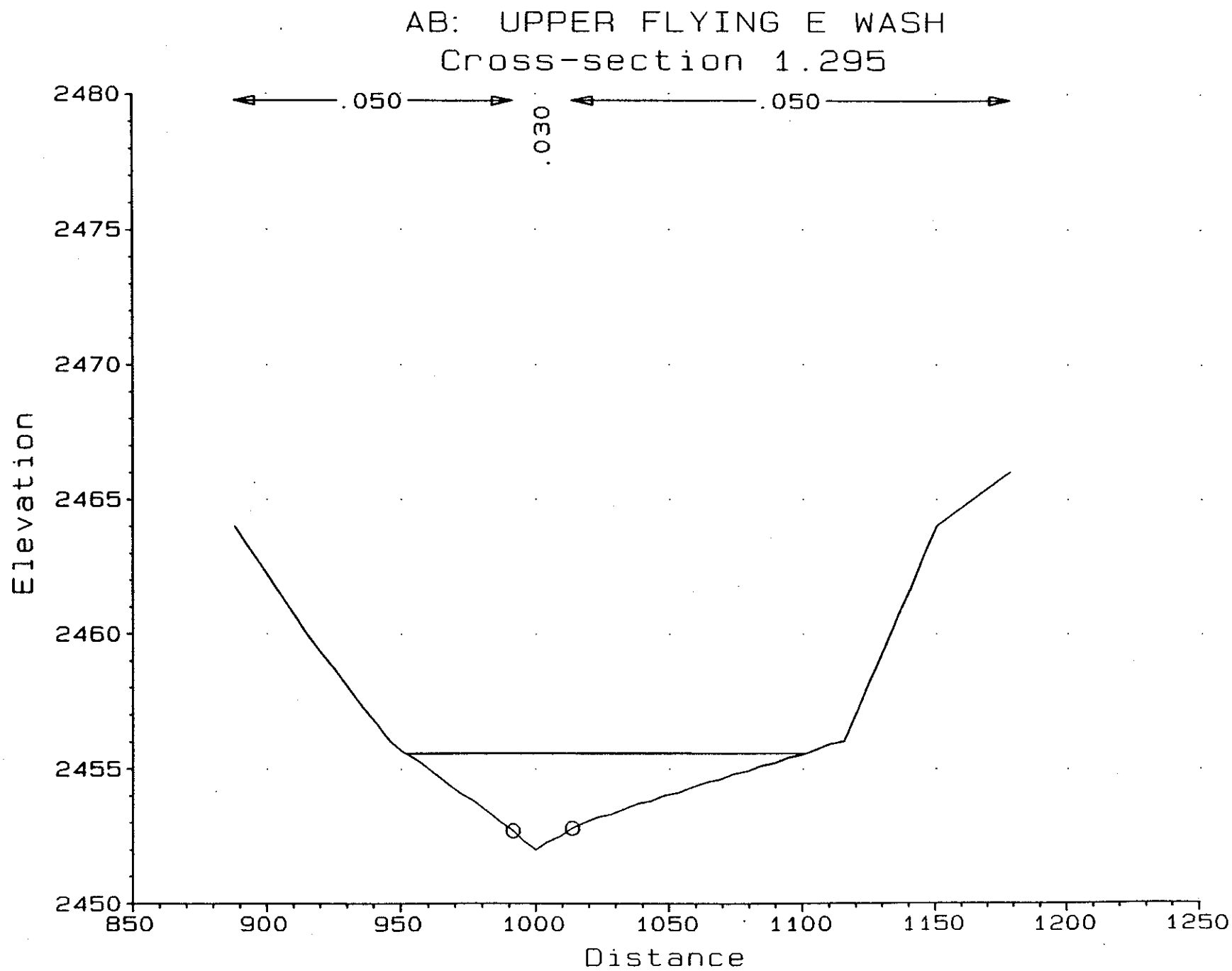
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Cross-section 1.295
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Elevation
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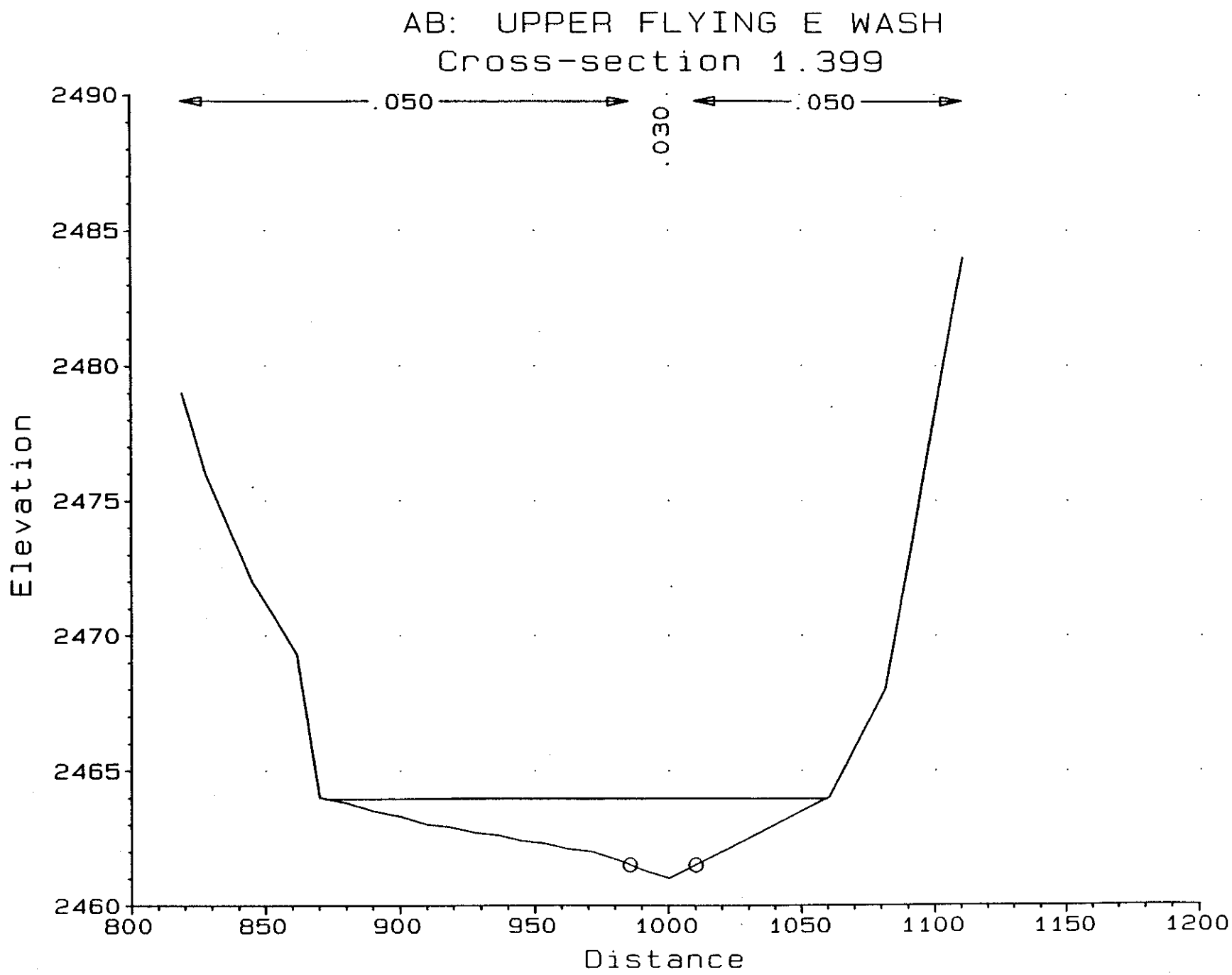
Distance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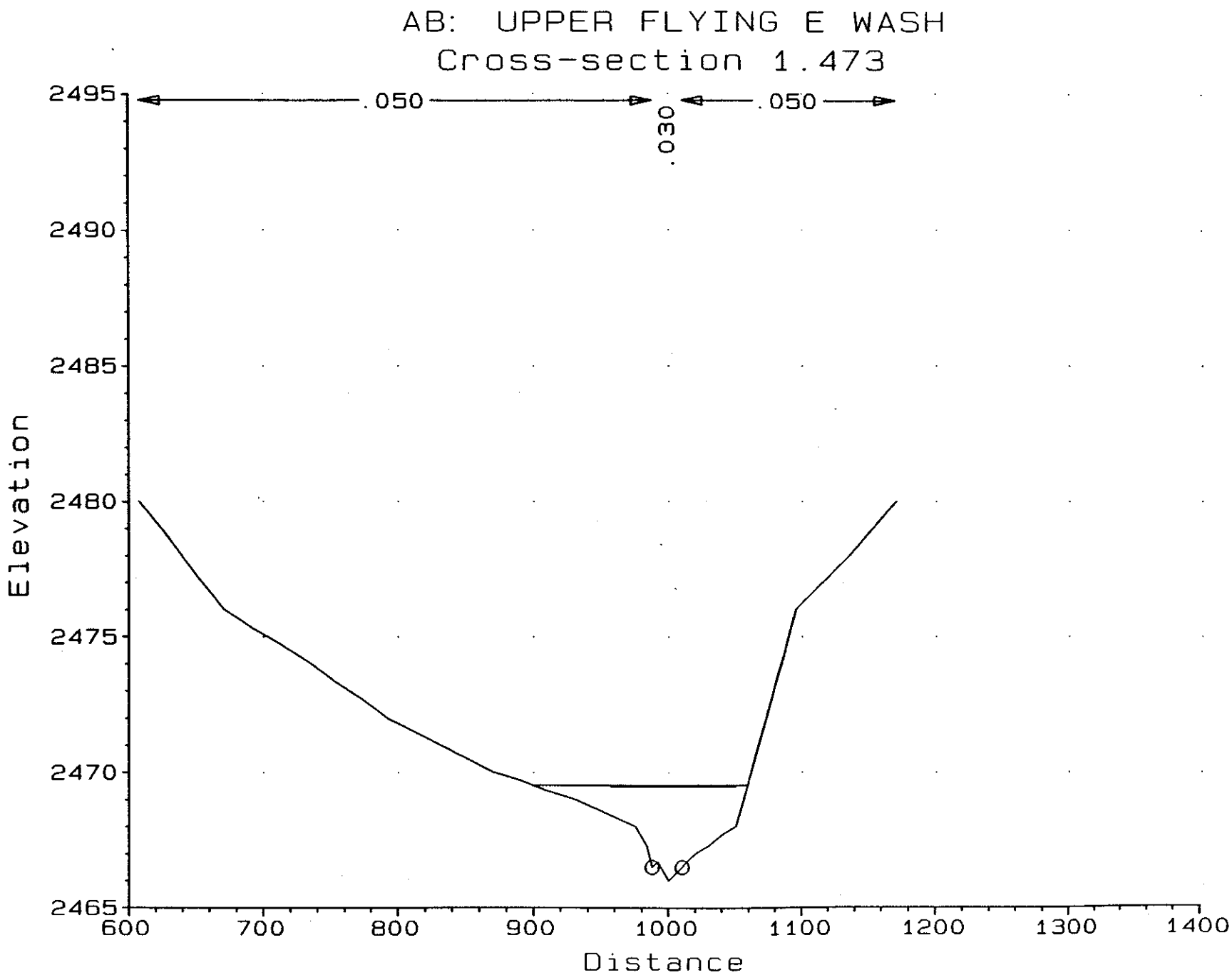
Distance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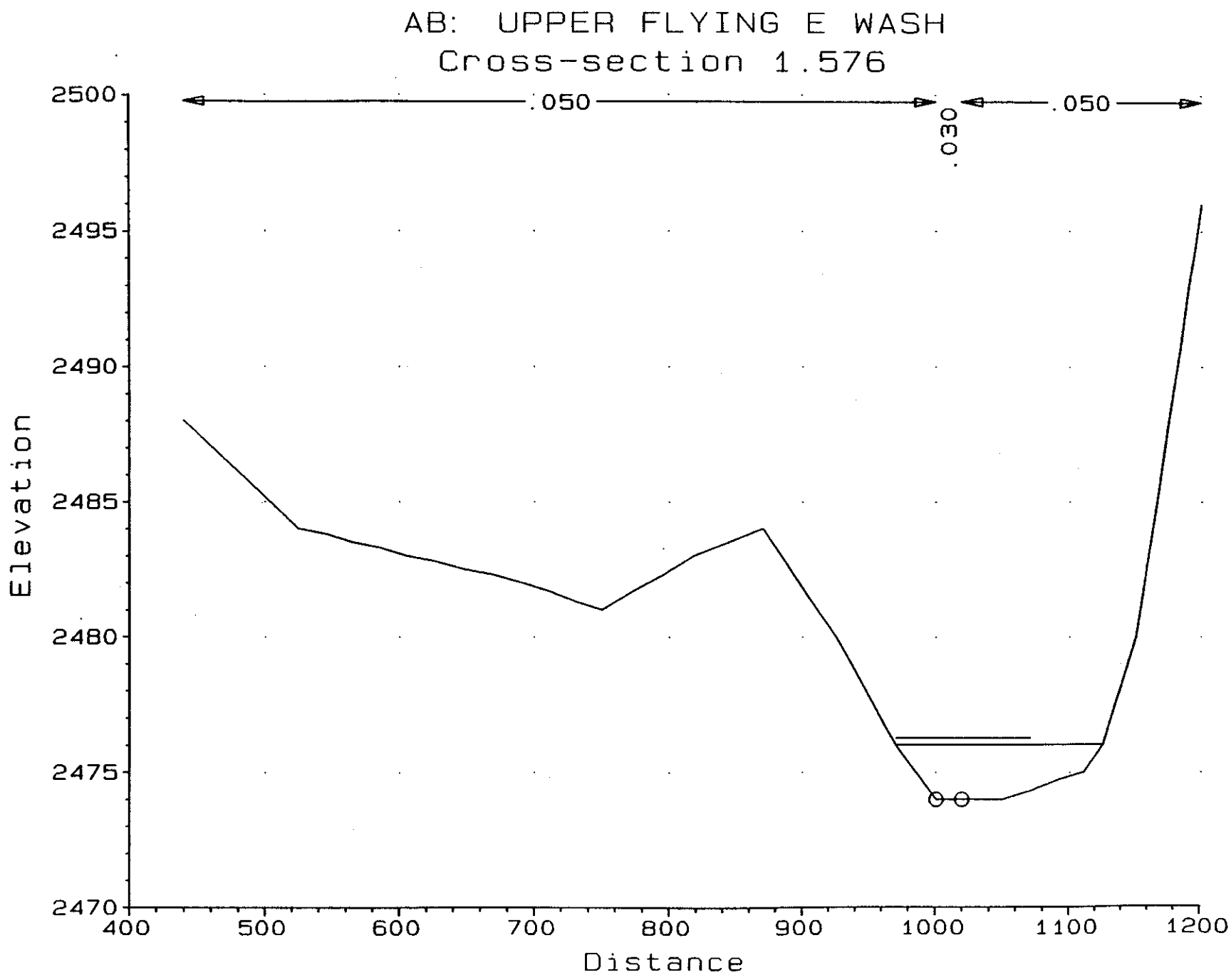
Distance


AB: UPPER FLYING E WASH
Cross-section 1.576
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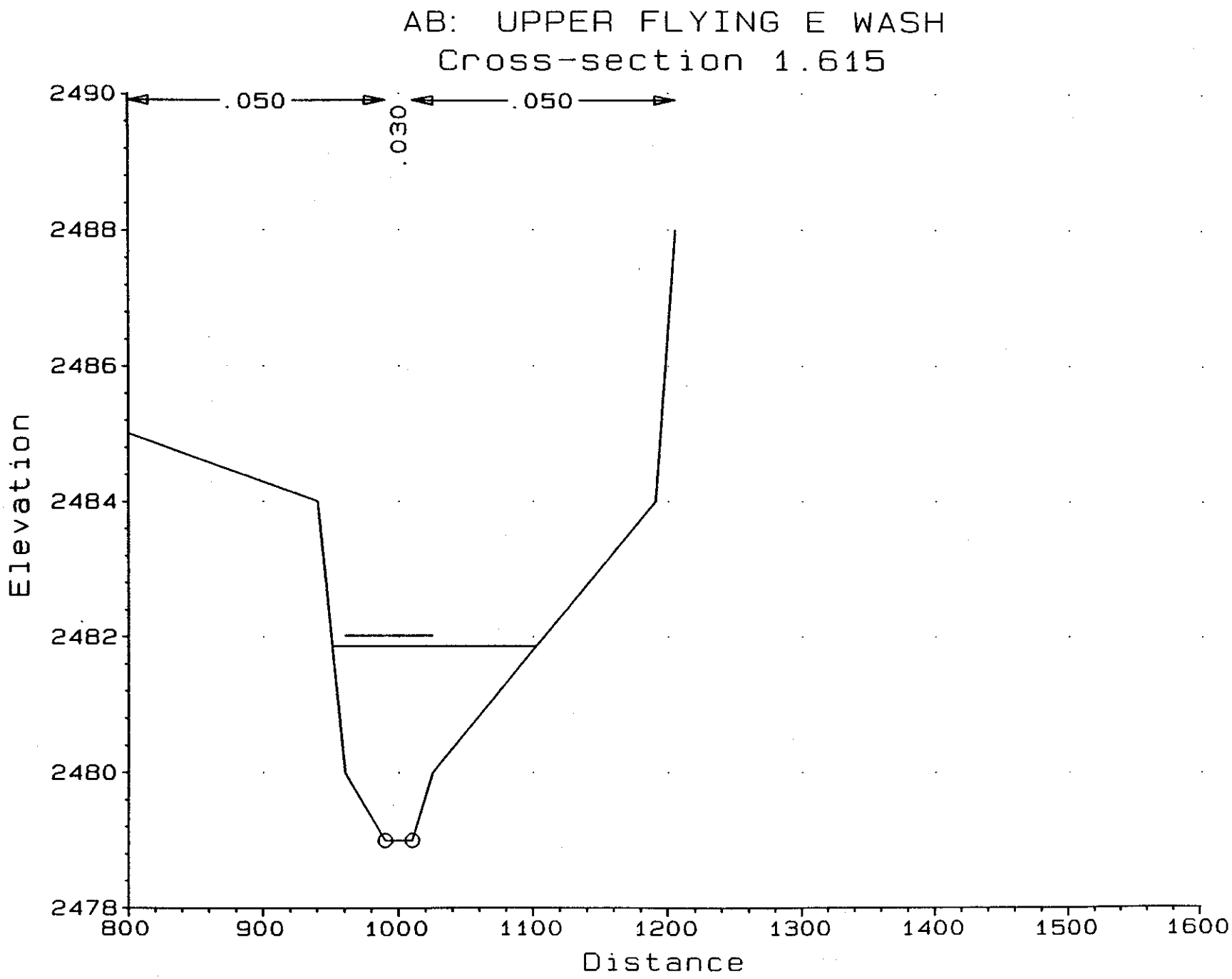
Distance


AB: UPPER FLYING E WASH
Cross-section 1.615
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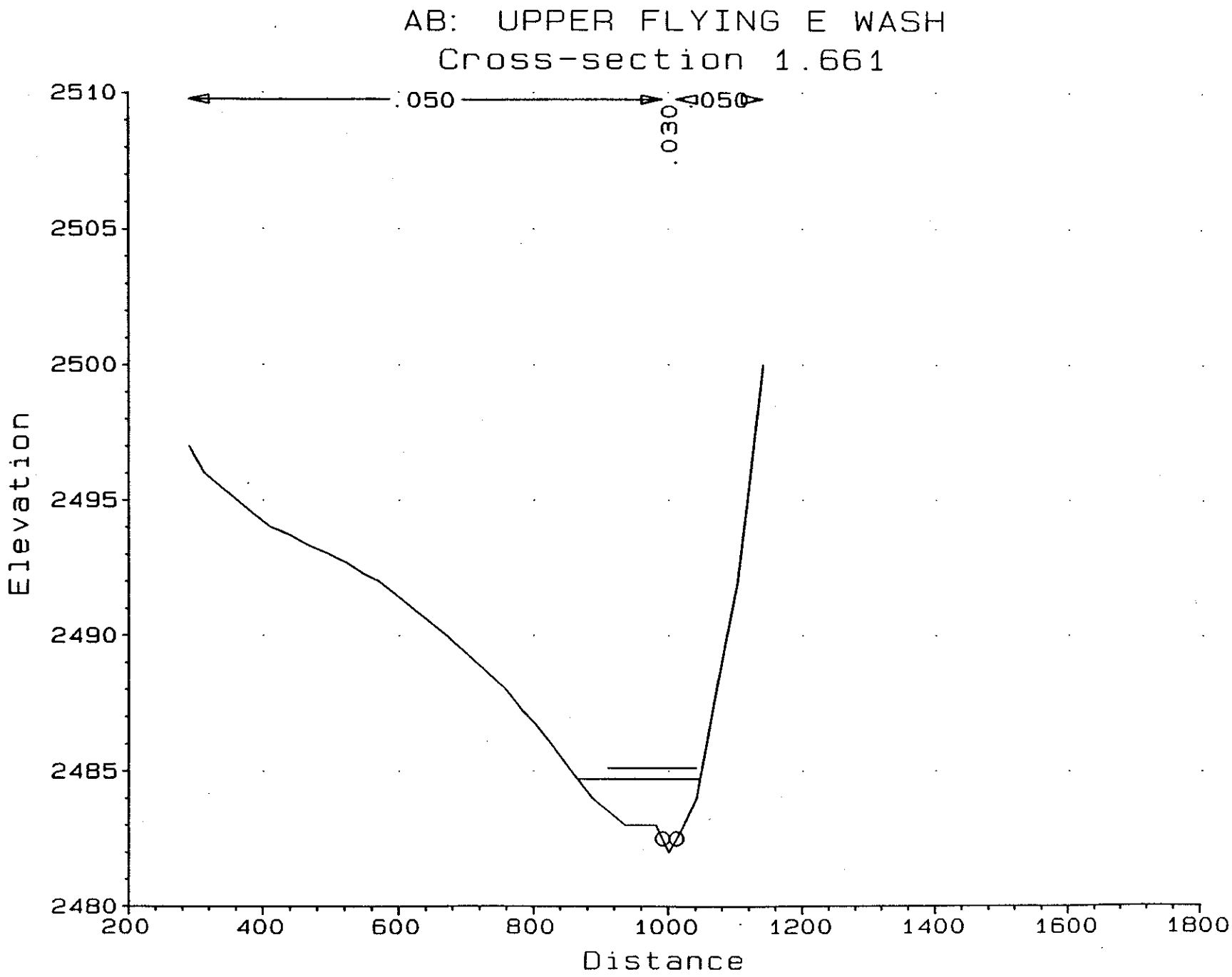
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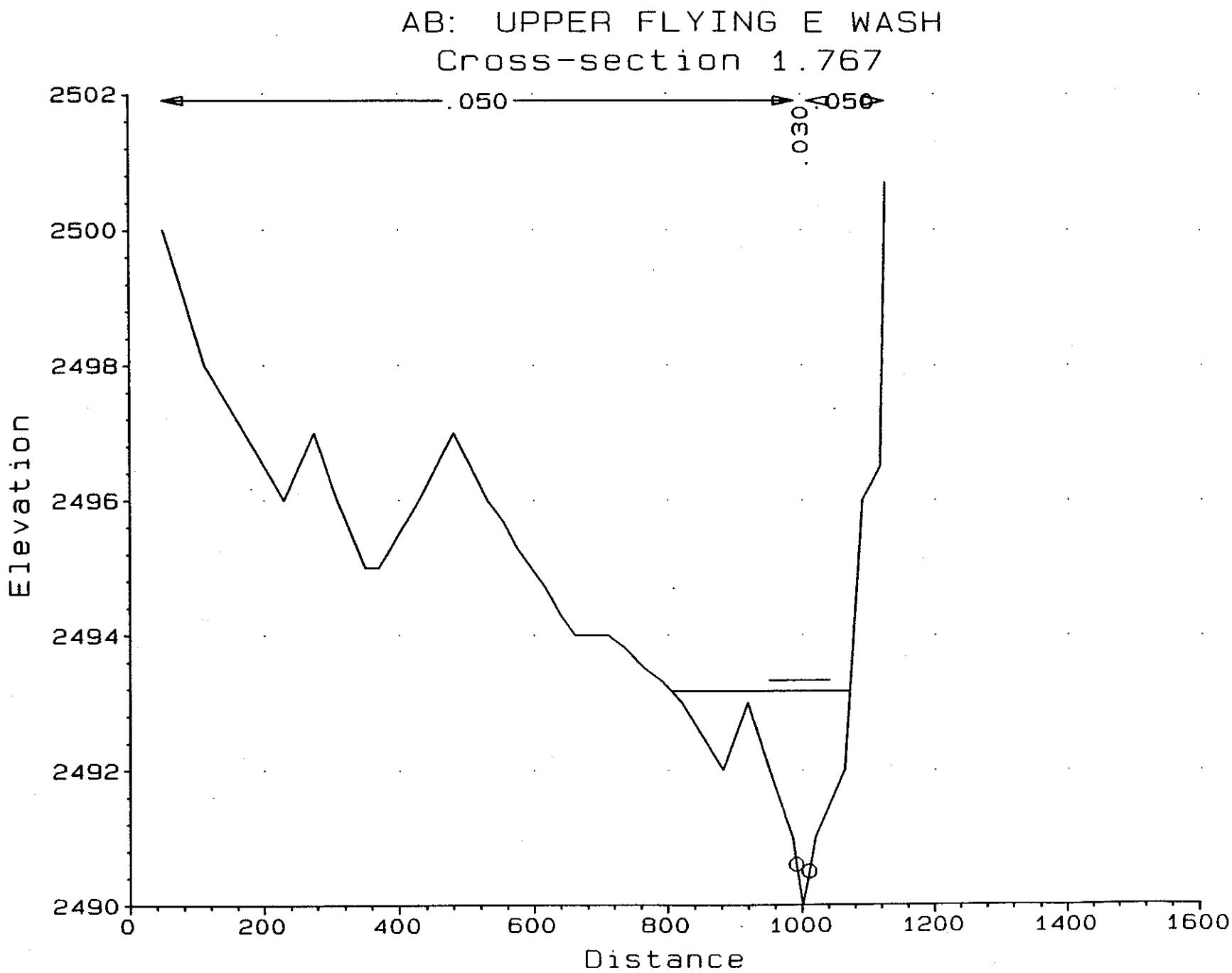
Distance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Elevation
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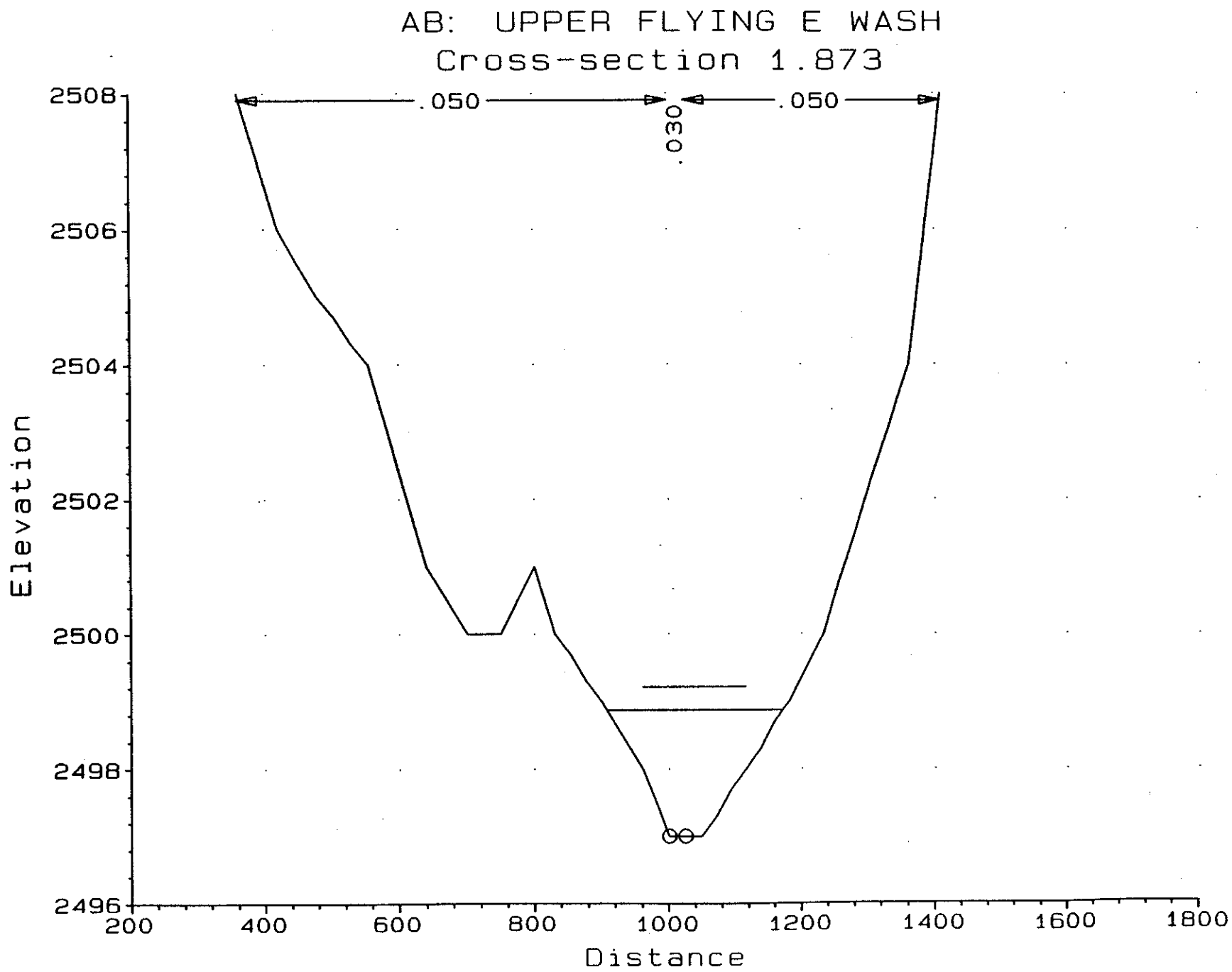
Distance


AB: UPPER FLYING E WASH
Cross-section 1.873
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Elevation
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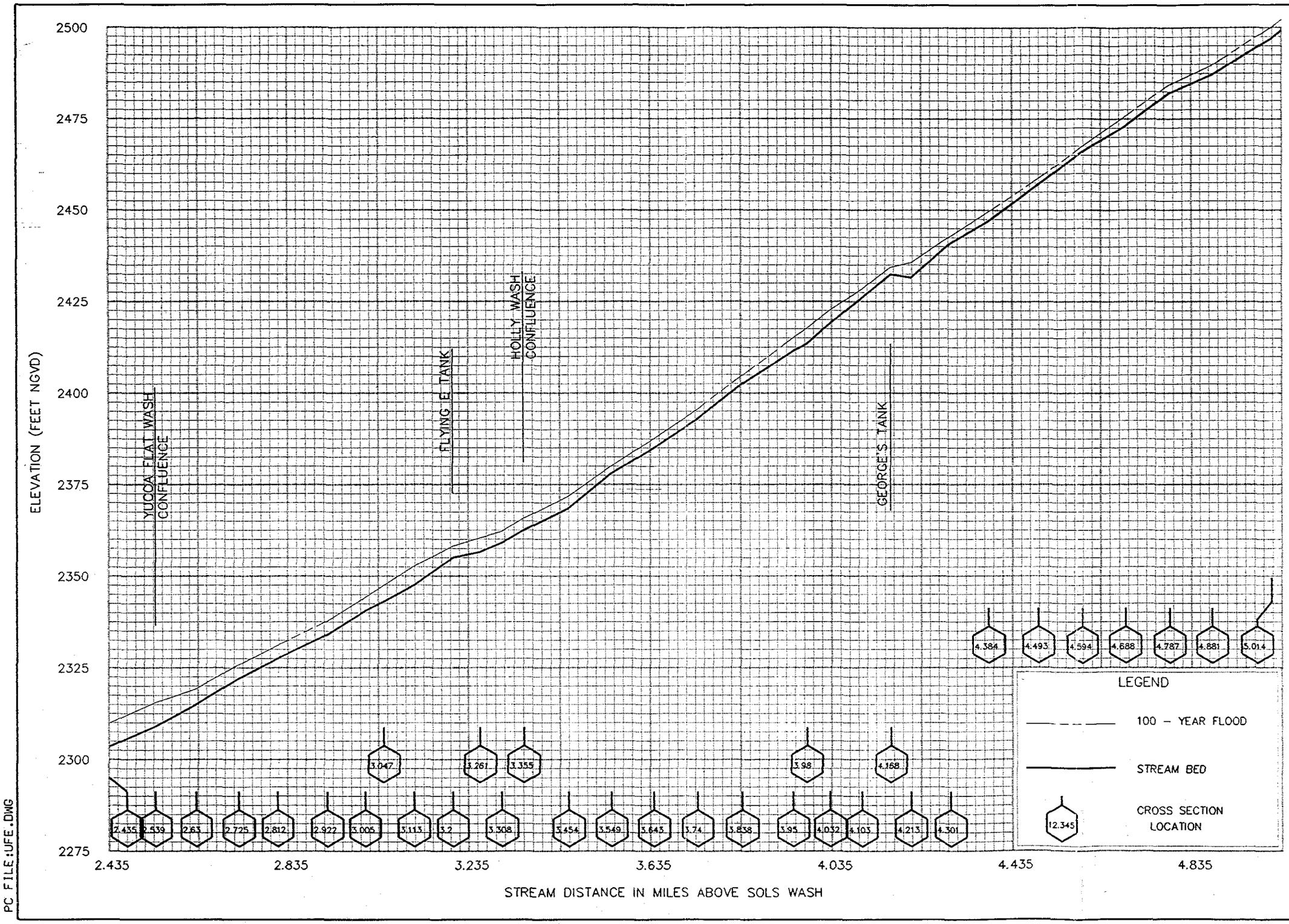
Distance



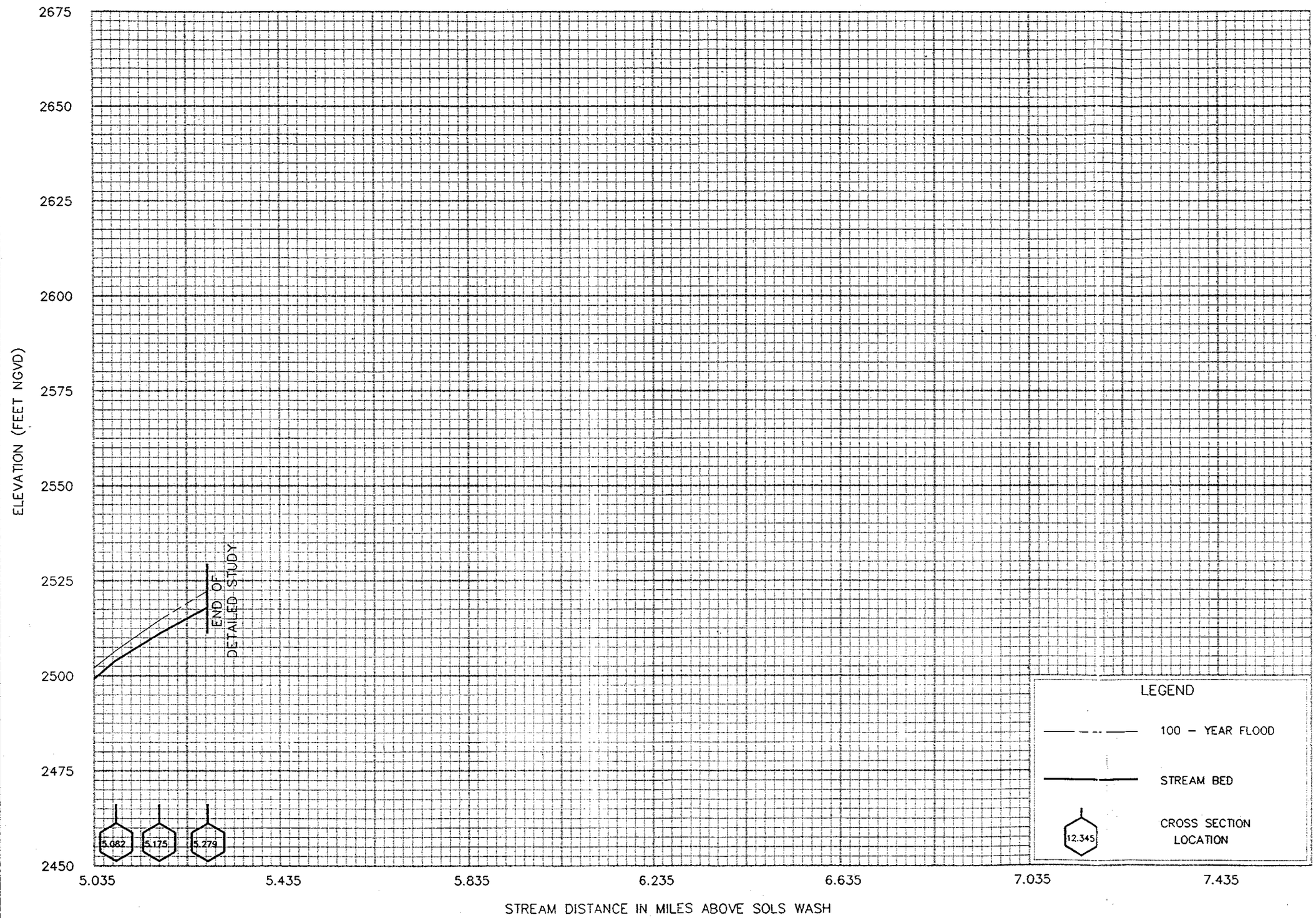

FLOOD PROFILES

FLYING E WASH (UPPER)

FEDERAL EMERGENCY MANAGEMENT AGENCY

MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

PC FILE:UFE.DWG



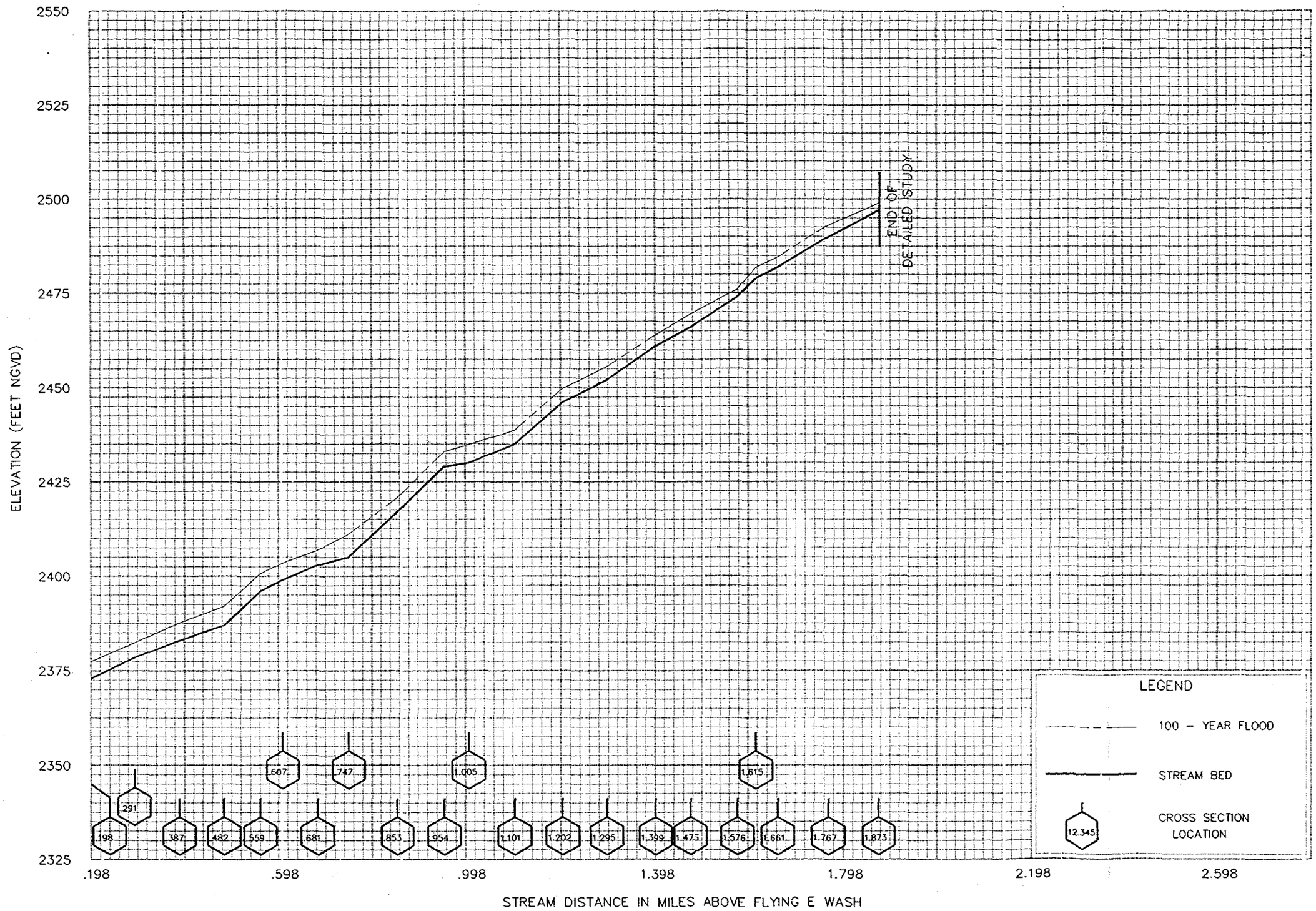

FLOOD PROFILES

FLYING E WASH (UPPER)

FEDERAL EMERGENCY MANAGEMENT AGENCY
MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

02/21/94 13:28:26 ACD-12-

PC FILE:UFE.DWG




FLOOD PROFILES

HOLLY WASH

FEDERAL EMERGENCY MANAGEMENT AGENCY

MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

02/17/94 15:25:54 ACD-12_

PC FILE:HOLLY.DWG

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*  HEC-2 WATER SURFACE PROFILES             *
*                                           *
*  Version   4.6.2;  May 1991               *
*                                           *
*  RUN DATE    28OCT92    TIME   16:42:52   *
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*  U.S. ARMY CORPS OF ENGINEERS        *
*  HYDROLOGIC ENGINEERING CENTER       *
*  609 SECOND STREET, SUITE D          *
*  DAVIS, CALIFORNIA 95616-4687        *
*          (916) 756-1104              *
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X     X  XXXXXXX   XXXXX              XXXXX
X     X  X        X     X            X     X
X     X  X        X                        X
XXXXXXX  XXXX     X         XXXXX    XXXXX
X     X  X        X                  X
X     X  X        X     X            X
X     X  XXXXXXX   XXXXX             XXXXXXX
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THIS RUN EXECUTED 28OCT92 16:42:52

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************************************
 HEC-2 WATER SURFACE PROFILES

 Version   4.6.2;  May 1991
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T1      WICKENBURG ADMS: CONTRACT FCD 89-79
T2      BLACK & VEATCH PN 17676; COE & VAN LOO JN 1197-02
T2      YUCCA FLAT WASH AND TWIN PEAKS WASH TRIBUTARIES TO FLYING E WASH
T3      AB: YUCCA FLAT WASH        (FILE YUCCA.DAT)

J1  ICHECK    INQ       NINV      IDIR      STRT      METRIC    HVINS     Q         WSEL      FQ

      0         2         0         0   .008304         0         0         0    2309.8         0

J2  NPROF     IPLOT     PRFVS     XSECV     XSECH     FN        ALLDC     IBW       CHNIM     ITRACE

      1         0        -1         0         0         0        -1         0         0        15


J3  VARIABLE CODES FOR SUMMARY PRINTOUT

    50        200

NC    0.050     0.050     0.030       0.1       0.3
QT        2    6943.0    6943.0
ET                7.1       9.1                                          952.     1228.0     957.69       1102
          STARTING WSEL FROM UPPER FLYING E WASH ANALYSIS.
          CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH.

X1    2.435        93     991.0    1027.0       500       455       490
X5        2    2309.8    2309.8
GR   2318.0     952.0    2308.0     959.0    2307.0     967.5    2306.0     976.0    2304.0     991.0
GR   2303.8    1000.0    2303.5    1009.0    2303.8    1018.0    2304.0    1027.0    2304.3    1037.0
GR   2304.6    1047.0    2304.9    1057.0    2305.2    1067.0    2305.5    1077.0    2306.0    1092.0
GR   2306.8    1102.0    2307.7    1108.0    2308.5    1112.0    2308.6    1112.7    2308.8    1117.4
GR   2308.9    1120.1    2309.1    1124.8    2309.3    1135.5    2309.4    1136.2    2309.6    1136.9
GR   2309.7    1137.6    2309.9    1138.3    2310.0    1139.0    2311.0    1183.5    2312.0    1228.0
GR   2312.0    1258.3    2311.9    1268.7    2311.9    1279.0    2311.8    1289.3    2311.8    1310.0
GR   2311.7    1320.3    2311.7    1330.7    2311.6    1341.0    2311.6    1351.3    2311.5    1361.7
GR   2311.5    1372.0    2311.3    1384.5    2311.0    1397.0    2311.0    1429.0    2311.2    1438.0
GR   2311.3    1447.0    2311.5    1456.0    2311.6    1466.9    2311.6    1488.7    2311.7    1499.6
GR   2311.7    1510.6    2311.8    1521.4    2311.8    1532.4    2311.9    1543.3    2311.9    1565.1
GR   2312.0    1576.0    2311.5    1586.0    2311.0    1596.0    2311.0    1609.0    2311.3    1618.5
GR   2311.5    1628.0    2311.3    1640.0    2311.0    1652.0    2311.3    1664.5    2311.5    1677.0
GR   2311.3    1687.0    2311.1    1697.0    2310.9    1707.0    2310.7    1717.0    2310.5    1727.0
GR   2310.3    1737.0    2310.0    1747.0    2309.8    1757.0    2309.7    1767.0    2309.5    1777.0
GR   2309.7    1788.7    2309.8    1800.3    2310.0    1812.0    2309.7    1821.0    2309.3    1830.0
GR   2309.0    1839.0    2308.0    1880.0    2308.7    1889.0    2309.3    1898.0    2310.0    1907.0
GR   2311.3    1917.0    2312.7    1927.0    2314.0    1937.0    2315.3    1947.0    2316.7    1957.0
GR   2318.0    1967.0    2320.0    1977.0    2322.0    1991.0
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         2      6943      6943

Cross section 2.539 repeated from Flying E Wash with Hydraulic Control
    Line at Station 850.  Several tributaries join at this section.
    Encroachment placed at station 920 to limit flow to Yucca Flat Wash
    channel.

NH       5       .05     821.5       .03     880.9       .05       980       .03      1012       .05
NH    1142
         AT HIGH FLOW, BOTH YUCCA FLAT WASH AND FLYING E WASH CHANNELS
         ARE USED.  SECTION REPEATED FOR BOTH MODELS. NH CARD DEFINES CHANNELS
         HYDRAULIC CONTROL LINE IS AT STATION 850.0

X1    2.539      63     821.5     880.9       570       490       550
X3                              465.3    2317.3    1100.    2317.0
GR     2322     320      2321     340.5      2320       361    2319.3     381.3    2318.7     401.7
GR     2318     422    2317.7     443.7    2317.3     465.3      2317       487    2315.5       510
GR     2315   527.7    2314.5     545.3      2314       563      2313       575      2316       596
GR   2316.5     619      2317       642    2316.5     666.5      2316       691    2316.5       710
GR     2316     730    2315.5       747      2315       764    2315.5       790    2315.2     795.2
GR   2314.9   800.4    2314.6     805.6    2314.3     810.8      2314       816    2313.5     821.5
GR     2313     827    2312.5       832      2312       837    2311.7     841.3    2311.3     845.7
GR     2311     850    2311.7       855    2312.3       860      2313       865    2313.1     870.3
GR   2313.1   875.6    2313.2     880.9    2313.3     886.1    2313.4     891.4    2313.4     896.7
GR   2313.5     902    2313.8     906.5      2314       911    2314.3     915.5    2314.5       920
GR   2314.3     941      2314       962      2312       977    2309.5       980      2309      1000
GR   2309.5    1012      2310      1027    2312.5      1035      2316      1063    2316.5    1081.5
GR     2317    1100      2317      1121      2317      1142

New N values due to heavy braiding
  and some growth in main channel.

QT       2    5152      5152
NC   0.060   0.060     0.040
ET                       9.1                                                      560      1093
X1   0.191      97       960      1020       410       500       490
GR  2330.0   379.0    2329.8     386.0    2329.7     393.0    2329.5     400.0    2329.5     430.0
GR  2329.6   437.8    2329.7     445.6    2329.8     453.4    2329.9     461.2    2330.0     469.0
GR  2329.5   477.3    2329.0     485.5    2328.5     493.8    2328.0     502.0    2326.7     508.7
GR  2325.3   515.3    2324.0     522.0    2323.7     529.3    2323.4     536.5    2323.1     543.8
GR  2322.8   551.0    2322.4     558.3    2322.1     565.5    2321.8     572.8    2321.5     580.0
GR  2321.3   588.0    2321.0     596.0    2320.8     604.0    2320.5     612.0    2320.2     618.7
GR  2319.8   625.3    2319.5     632.0    2320.3     639.3    2321.2     646.7    2322.0     654.0
GR  2321.5   663.0    2321.0     672.0    2321.4     679.0    2321.8     686.0    2322.1     693.0
GR  2322.5   700.0    2322.4     707.5    2322.3     715.0    2322.1     722.5    2322.0     730.0
GR  2321.6   737.5    2321.3     745.0    2320.9     752.5    2320.5     760.0    2320.0     767.5
GR  2319.5   775.0    2320.0     782.3    2320.5     789.7    2321.0     797.0    2320.9     803.8
GR  2320.8   810.6    2320.7     817.4    2320.6     824.2    2320.5     831.0    2320.6     838.5
GR  2320.8   846.0    2320.9     853.5    2321.0     861.0    2320.8     868.3    2320.5     875.5
GR  2320.3   882.8    2320.0     890.0    2318.8     898.0    2317.5     906.0    2318.8     913.0
GR  2320.0   920.0    2320.2     926.7    2320.3     933.3    2320.5     940.0    2320.3     946.7
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| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2320.2 | 953.3 | 2320.0 | 960.0 | 2319.8 | 967.5 | 2319.5 | 975.0 | 2318.0 | 985.0 |
| | 2317.8 | 992.5 | 2317.5 | 1000.0 | 2318.0 | 1011.0 | 2320.0 | 1020.0 | 2322.0 | 1029.0 |
| GR | 2322.2 | 1037.7 | 2322.3 | 1046.3 | 2322.5 | 1055.0 | 2322.4 | 1062.5 | 2322.3 | 1070.0 |
| GR | 2322.1 | 1077.5 | 2322.0 | 1085.0 | 2322.3 | 1092.0 | 2322.5 | 1099.0 | 2325.0 | 1106.3 |
| GR | 2327.5 | 1113.7 | 2330.0 | 1121.0 | | | | | | |
| NC | .050 | .050 | .030 | | | | | | | |
| ET | | | 9.1 | | | | | | 774 | 1163 |
| X1 | 0.290 | 73 | 976.6 | 1028.7 | 420 | 520 | 520 | | | |
| GR | 2338 | 613 | 2336.4 | 625.8 | 2334.8 | 638.6 | 2334 | 645 | 2333.2 | 645.7 |
| GR | 2332.3 | 658.3 | 2331.5 | 665 | 2331.3 | 671.9 | 2331.2 | 678.8 | 2330.8 | 692.6 |
| GR | 2330.7 | 699.4 | 2330.3 | 713.2 | 2330.2 | 720.1 | 2329.8 | 734 | 2329.4 | 748 |
| GR | 2329.3 | 755 | 2328.9 | 769 | 2328.7 | 776 | 2328.6 | 783 | 2328.2 | 797 |
| GR | 2328 | 804 | 2327 | 819.5 | 2326 | 835 | 2325.8 | 842.5 | 2325.5 | 850 |
| GR | 2325.8 | 856.7 | 2326.2 | 863.3 | 2326.5 | 870 | 2327.5 | 886 | 2328 | 894 |
| GR | 2328.2 | 901.7 | 2328.3 | 909.3 | 2328.5 | 917 | 2328.3 | 932 | 2328.1 | 939.5 |
| GR | 2328 | 947 | 2327.2 | 961.8 | 2326.4 | 976.6 | 2326 | 984 | 2325 | 1000 |
| GR | 2326 | 1016 | 2326.2 | 1022.3 | 2326.3 | 1028.7 | 2326.5 | 1035 | 2326.3 | 1041.7 |
| GR | 2326.2 | 1048.3 | 2326 | 1055 | 2325.7 | 1061.7 | 2325.3 | 1068.3 | 2325 | 1075 |
| GR | 2325 | 1095 | 2326 | 1107 | 2327 | 1121 | 2328 | 1135 | 2328 | 1161.4 |
| GR | 2330 | 1165 | 2330.9 | 1174.8 | 2330.8 | 1181.5 | 2331.6 | 1188.3 | 2331.5 | 1195 |
| GR | 2332 | 1202.3 | 2332.2 | 1209.7 | 2332.8 | 1223.5 | 2334 | 1230 | 2334.3 | 1236.5 |
| GR | 2335.5 | 1243 | 2336 | 1246.3 | 2338.5 | 1257.7 | 2339.5 | 1272 | 2339 | 1279 |
| GR | 2339.5 | 1286 | 2339.8 | 1293.5 | 2340 | 1301 | | | | |
| | | | 9.1 | | | | | | 922 | 1301 |
| | 0.390 | 69 | 982 | 1016 | 530 | 490 | 530 | | | |
| GR | 2348 | 598 | 2347.3 | 608.7 | 2346.7 | 619.3 | 2346 | 630 | 2345.3 | 640.3 |
| GR | 2344.7 | 650.7 | 2344 | 661 | 2342.9 | 681 | 2341.7 | 701 | 2340.6 | 721 |
| GR | 2340 | 731 | 2338.8 | 742 | 2337.5 | 753 | 2336.9 | 772.5 | 2336.3 | 792 |
| GR | 2335.6 | 811.5 | 2335 | 831 | 2335.3 | 843 | 2335.5 | 855 | 2335.5 | 883 |
| GR | 2335.2 | 902.3 | 2334.8 | 921.7 | 2334.5 | 941 | 2334.8 | 951.5 | 2335 | 962 |
| GR | 2334 | 982 | 2332 | 1000 | 2334 | 1016 | 2334.5 | 1028 | 2335 | 1040 |
| GR | 2334.7 | 1057.3 | 2334.5 | 1066 | 2335.5 | 1081 | 2335.3 | 1093.5 | 2335 | 1106 |
| GR | 2335 | 1132 | 2334.5 | 1151 | 2335 | 1169 | 2335.1 | 1179.8 | 2335.3 | 1190.5 |
| GR | 2335.4 | 1201.3 | 2335.5 | 1212 | 2335.3 | 1223 | 2335 | 1234 | 2334.3 | 1252.7 |
| GR | 2334 | 1262 | 2334.2 | 1281.7 | 2334.3 | 1301.3 | 2334.5 | 1321 | 2334 | 1338.5 |
| GR | 2333.5 | 1356 | 2334 | 1367.3 | 2334.5 | 1378.7 | 2335 | 1390 | 2334.8 | 1400.5 |
| GR | 2334.5 | 1411 | 2335.2 | 1421.7 | 2335.8 | 1432.3 | 2336.5 | 1443 | 2336 | 1460.3 |
| GR | 2335.8 | 1469 | 2335.5 | 1483 | 2338.5 | 1501 | 2340 | 1510 | 2341 | 1520.5 |
| GR | 2342 | 1531 | 2343 | 1550 | 2344 | 1569 | 2346 | 1581 | | |
| ET | | | 9.1 | | | | | | 939 | 1329 |
| X1 | 0.477 | 50 | 965 | 1007.2 | 450 | 440 | 460 | | | |
| GR | 2354 | 755 | 2353.7 | 769.7 | 2353.3 | 784.3 | 2353 | 799 | 2352.6 | 813.4 |
| GR | 2352.2 | 827.8 | 2351.6 | 842.6 | 2350.8 | 857.8 | 2350 | 873 | 2346 | 884 |
| GR | 2344.4 | 900.4 | 2342.8 | 916.8 | 2342 | 925 | 2341.3 | 939 | 2341 | 946 |
| GR | 2341.3 | 958.7 | 2341.5 | 965 | 2341.5 | 1000 | 2341.4 | 1007.2 | 2341.3 | 1021.5 |
| GR | 2341.1 | 1035.8 | 2341.3 | 1050.5 | 2341.8 | 1065.5 | 2342.1 | 1080.3 | 2342.2 | 1095 |
| GR | 2342.3 | 1109.7 | 2342.4 | 1124.3 | 2342.4 | 1154.8 | 2342.3 | 1170.6 | 2342.2 | 1186.3 |
| | 2342.1 | 1202.1 | 2341.9 | 1217.6 | 2341.7 | 1232.8 | 2341.5 | 1248 | 2341.3 | 1262.8 |
| | 2341.1 | 1277.6 | 2341 | 1285 | 2341 | 1315 | 2341.5 | 1329 | 2342 | 1343 |
| GR | 2342.3 | 1357.7 | 2342.4 | 1372.3 | 2342.1 | 1386.8 | 2341.9 | 1401.5 | 2341.6 | 1416.5 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2341.7 | 1431.7 | 2342 | 1447 | 2344.8 | 1461.4 | 2347.6 | 1475.8 | 2349 | 1483 |
| ET | | 7.1 | 9.1 | | | | 790 | 1450 | 971 | 1312 |

ENCROACHED TO 1450 DUE TO SMALL RIGHT BANK TRIBUTARY. FLOODPLAIN MAPPED TO WSEL.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 0.578 | 91 | 980 | 1020 | 530 | 510 | 530 | | | |
| GR | 2364.0 | 790.0 | 2361.0 | 799.5 | 2360.0 | 809.0 | 2358.0 | 820.0 | 2357.0 | 831.0 |
| GR | 2355.3 | 841.3 | 2354.7 | 851.7 | 2353.0 | 862.0 | 2352.8 | 873.5 | 2352.5 | 885.0 |
| GR | 2352.7 | 893.7 | 2352.8 | 902.3 | 2353.0 | 911.0 | 2353.3 | 921.0 | 2353.5 | 931.0 |
| GR | 2353.3 | 940.7 | 2353.2 | 950.3 | 2352.5 | 960.0 | 2352.0 | 970.0 | 2350.0 | 980.0 |
| GR | 2345.5 | 992.0 | 2345.5 | 1000.0 | 2348.5 | 1010.0 | 2348.8 | 1020.0 | 2349.2 | 1030.0 |
| GR | 2349.5 | 1040.0 | 2349.6 | 1050.0 | 2349.8 | 1060.0 | 2349.9 | 1070.0 | 2350.0 | 1080.0 |
| GR | 2349.8 | 1091.5 | 2349.5 | 1103.0 | 2349.8 | 1111.5 | 2350.0 | 1120.0 | 2349.8 | 1129.5 |
| GR | 2349.5 | 1139.0 | 2350.0 | 1149.5 | 2350.5 | 1160.0 | 2350.2 | 1169.0 | 2349.8 | 1178.0 |
| GR | 2349.5 | 1187.0 | 2350.0 | 1200.0 | 2349.8 | 1209.5 | 2349.5 | 1219.0 | 2350.0 | 1229.5 |
| GR | 2350.5 | 1240.0 | 2350.5 | 1251.0 | 2350.5 | 1262.0 | 2349.9 | 1271.5 | 2349.3 | 1281.0 |
| GR | 2349.0 | 1285 | 2348.6 | 1290.5 | 2348 | 1300 | 2349 | 1306 | 2350 | 1312 |
| GR | 2351 | 1332 | 2351 | 1375 | 2350.8 | 1386.5 | 2350.5 | 1398 | 2350 | 1409.5 |
| GR | 2349.5 | 1421 | 2349.8 | 1430.5 | 2350 | 1440 | 2350.3 | 1450 | 2350.5 | 1460 |
| GR | 2350.5 | 1490 | 2350.3 | 1508.5 | 2350.1 | 1517.8 | 2350.0 | 1527.0 | 2349.8 | 1536.0 |
| GR | 2349.7 | 1545.0 | 2349.5 | 1554.0 | 2349.3 | 1563.0 | 2349.2 | 1572.0 | 2349.0 | 1581.0 |
| GR | 2348.8 | 1591.2 | 2348.6 | 1601.4 | 2348.4 | 1611.6 | 2348.2 | 1621.8 | 2348.0 | 1632.0 |
| GR | 2347.9 | 1640.6 | 2347.8 | 1649.2 | 2347.7 | 1657.8 | 2347.6 | 1666.4 | 2347.5 | 1675.0 |
| GR | 2348.2 | 1683.0 | 2348.8 | 1691.0 | 2349.5 | 1699.0 | 2353.0 | 1710.0 | 2356.5 | 1721.0 |
| GR | 2360.0 | 1732.0 | | | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 830 | 1043 |
| X1 | 0.697 | 95 | 973.4 | 1017 | 610 | 590 | 630 | | | |
| GR | 2362.5 | 595.0 | 2362.3 | 607.0 | 2362.0 | 619.0 | 2360.8 | 629.5 | 2359.5 | 640.0 |
| GR | 2359.0 | 652.0 | 2358.8 | 663.0 | 2358.5 | 674.0 | 2358.3 | 685.0 | 2358.0 | 696.0 |
| GR | 2357.9 | 707.2 | 2357.8 | 718.4 | 2357.7 | 729.6 | 2357.6 | 740.8 | 2357.5 | 752.0 |
| GR | 2358.0 | 763.0 | 2358.5 | 774.0 | 2358.3 | 782.7 | 2358.2 | 791.3 | 2358.0 | 800.0 |
| GR | 2357.8 | 810.0 | 2357.5 | 820.0 | 2357.3 | 830.0 | 2357.0 | 840.0 | 2356.7 | 851.7 |
| GR | 2356.3 | 863.3 | 2356.0 | 875.0 | 2355.8 | 886.7 | 2355.7 | 898.3 | 2355.5 | 910.0 |
| GR | 2356.0 | 922.0 | 2356.3 | 933.5 | 2356.5 | 945.0 | 2356.5 | 950.0 | 2356.4 | 952.1 |
| GR | 2356.4 | 954.2 | 2356.3 | 956.3 | 2356.3 | 958.4 | 2356.2 | 960.6 | 2356.2 | 962.7 |
| GR | 2356.1 | 964.8 | 2356.1 | 966.9 | 2356.0 | 969.0 | 2355.8 | 971.2 | 2355.6 | 973.4 |
| GR | 2355.4 | 975.6 | 2355.2 | 977.8 | 2355.0 | 980.0 | 2354.8 | 982.0 | 2354.6 | 984.0 |
| GR | 2354.4 | 986.0 | 2354.2 | 988.0 | 2354.0 | 990.0 | 2353.9 | 992.0 | 2353.8 | 994.0 |
| GR | 2353.7 | 996.0 | 2353.6 | 998.0 | 2353.5 | 1000.0 | 2353.5 | 1002.2 | 2353.5 | 1004.4 |
| GR | 2353.5 | 1006.6 | 2353.5 | 1008.8 | 2353.5 | 1011.0 | 2354.1 | 1013.0 | 2354.7 | 1015.0 |
| GR | 2355.3 | 1017.0 | 2355.9 | 1019.0 | 2356.5 | 1021.0 | 2356.6 | 1023.0 | 2356.7 | 1025.0 |
| GR | 2356.8 | 1027.0 | 2356.8 | 1029.0 | 2356.9 | 1031.0 | 2357.0 | 1033.0 | 2357.0 | 1042.6 |
| GR | 2357.0 | 1052.1 | 2357.0 | 1061.7 | 2357.0 | 1071.3 | 2357.0 | 1080.9 | 2357.0 | 1090.4 |
| GR | 2357.0 | 1100.0 | 2357.1 | 1110.2 | 2357.2 | 1120.3 | 2357.3 | 1130.5 | 2357.3 | 1140.7 |
| GR | 2357.4 | 1150.8 | 2357.5 | 1161.0 | 2358.0 | 1170.0 | 2358.8 | 1180.0 | 2359.6 | 1190.0 |
| GR | 2360.4 | 1200.0 | 2361.2 | 1210.0 | 2362.0 | 1220.0 | 2362.3 | 1232.5 | 2362.5 | 1245.0 |

Flying E Ranch access road lies between sections 0.771 and 0.866

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 850 | 1024 |
| X1 | 0.788 | 65 | 974.3 | 1017.3 | 470 | 455 | 480 | | | |
| GR | 2369.0 | 400.0 | 2368.8 | 422.5 | 2368.5 | 445.0 | 2368.3 | 467.5 | 2368.0 | 490.0 |
| GR | 2367.8 | 510.0 | 2367.5 | 530.0 | 2367.3 | 550.0 | 2367.0 | 570.0 | 2367.0 | 590.0 |
| GR | 2366.8 | 607.5 | 2366.5 | 625.0 | 2366.4 | 643.6 | 2366.3 | 662.2 | 2366.2 | 680.8 |
| GR | 2366.1 | 699.4 | 2366.0 | 718.0 | 2365.0 | 739.0 | 2364.0 | 760.0 | 2363.5 | 782.0 |
| GR | 2363.0 | 810.0 | 2363.3 | 832.5 | 2363.5 | 855.0 | 2362.8 | 877.5 | 2362.0 | 900.0 |
| GR | 2361.0 | 925.0 | 2361.5 | 950.0 | 2361.4 | 952.2 | 2361.4 | 954.4 | 2361.3 | 956.7 |
| GR | 2361.3 | 958.9 | 2361.2 | 961.1 | 2361.2 | 963.3 | 2361.1 | 965.6 | 2361.1 | 967.8 |
| GR | 2361.0 | 970.0 | 2360.8 | 972.1 | 2360.6 | 974.3 | 2360.4 | 976.4 | 2360.1 | 978.6 |
| GR | 2359.9 | 980.7 | 2359.7 | 982.9 | 2359.5 | 985.0 | 2359.4 | 987.1 | 2359.4 | 989.3 |
| GR | 2359.3 | 991.4 | 2359.2 | 993.6 | 2359.1 | 995.7 | 2359.1 | 997.9 | 2359.0 | 1000.0 |
| GR | 2359.1 | 1002.1 | 2359.1 | 1004.3 | 2359.2 | 1006.4 | 2359.3 | 1008.6 | 2359.4 | 1010.7 |
| GR | 2359.4 | 1012.9 | 2359.5 | 1015.0 | 2360.8 | 1017.3 | 2362.1 | 1019.5 | 2363.4 | 1021.8 |
| GR | 2364.8 | 1024.0 | 2366.1 | 1026.3 | 2367.4 | 1028.5 | 2368.7 | 1030.8 | 2370.0 | 1033.0 |
| ET | | | 9.1 | | | | | | 949 | 1043 |
| X1 | 0.883 | 44 | 981.7 | 1020 | 470 | 500 | 500 | | | |
| GR | 2378.0 | 725.0 | 2376.0 | 746.0 | 2374.0 | 770.0 | 2373.0 | 795.0 | 2372.0 | 820.0 |
| GR | 2371.5 | 835.0 | 2370.5 | 852.0 | 2371.0 | 880.0 | 2371.0 | 896.0 | 2370.0 | 920.0 |
| GR | 2366.0 | 949.0 | 2365.9 | 954.6 | 2365.8 | 960.2 | 2365.7 | 965.8 | 2365.6 | 971.4 |
| GR | 2365.5 | 977.0 | 2365.3 | 981.7 | 2365.2 | 986.3 | 2365.0 | 991.0 | 2364.8 | 995.5 |
| GR | 2364.5 | 1000.0 | 2364.6 | 1005.0 | 2364.8 | 1010.0 | 2364.9 | 1015.0 | 2365.0 | 1020.0 |
| GR | 2365.5 | 1026.0 | 2366.0 | 1032.0 | 2367.0 | 1037.3 | 2368.0 | 1042.7 | 2369.0 | 1048.0 |
| [illegible] | 2369.4 | 1053.5 | 2369.8 | 1059.0 | 2370.1 | 1064.5 | 2370.5 | 1070.0 | 2371.0 | 1100.0 |
| [illegible] | 2370.8 | 1117.5 | 2370.5 | 1135.0 | 2370.5 | 1157.0 | 2370.8 | 1178.5 | 2371.0 | 1200.0 |
| [illegible] | 2371.5 | 1216.5 | 2372.0 | 1233.0 | 2373.0 | 1249.0 | 2374.0 | 1265.0 | | |
| ET | | | 9.1 | | | | | | 959 | 1117 |
| X1 | 0.972 | 50 | 988.3 | 1027.2 | 470 | 470 | 470 | | | |
| GR | 2385.5 | 910.0 | 2380.0 | 930.0 | 2379.5 | 940.0 | 2378.8 | 943.4 | 2378.1 | 946.8 |
| GR | 2377.4 | 950.3 | 2376.7 | 953.7 | 2376.0 | 957.1 | 2375.3 | 960.5 | 2374.5 | 963.9 |
| GR | 2373.8 | 967.3 | 2373.1 | 970.8 | 2372.4 | 974.2 | 2371.7 | 977.6 | 2371.0 | 981.0 |
| GR | 2370.7 | 984.7 | 2370.3 | 988.3 | 2370.0 | 992.0 | 2369.8 | 996.0 | 2369.5 | 1000.0 |
| GR | 2369.5 | 1003.7 | 2369.5 | 1007.3 | 2369.5 | 1011.0 | 2369.6 | 1014.3 | 2369.8 | 1017.5 |
| GR | 2369.9 | 1020.8 | 2370.0 | 1024.0 | 2370.3 | 1027.2 | 2370.6 | 1030.4 | 2370.9 | 1033.6 |
| GR | 2371.2 | 1036.8 | 2371.5 | 1040.0 | 2371.0 | 1059.0 | 2372.0 | 1071.0 | 2374.0 | 1100.0 |
| GR | 2376.0 | 1122.0 | 2377.5 | 1151.0 | 2377.5 | 1170.0 | 2377.0 | 1200.0 | 2378.0 | 1228.0 |
| GR | 2378.3 | 1244.0 | 2378.5 | 1260.0 | 2379.0 | 1280.0 | 2379.5 | 1300.0 | 2379.3 | 1320.0 |
| GR | 2379.0 | 1340.0 | 2379.3 | 1355.5 | 2379.5 | 1371.0 | 2379.5 | 1398.0 | 2382.0 | 1416.0 |
| ET | | | 9.1 | | | | | | 985 | 1075 |
| X1 | 1.070 | 49 | 990 | 1036.3 | 540 | 460 | 520 | | | |
| GR | 2388.0 | 780.0 | 2387.6 | 789.8 | 2387.2 | 799.6 | 2386.8 | 809.4 | 2386.4 | 819.2 |
| GR | 2386.0 | 829.0 | 2385.5 | 839.3 | 2385.0 | 849.5 | 2384.5 | 859.8 | 2384.0 | 870.0 |
| GR | 2382.0 | 885.0 | 2381.0 | 896.0 | 2382.0 | 910.0 | 2382.8 | 920.0 | 2383.5 | 930.0 |
| GR | 2383.5 | 942.0 | 2383.1 | 946.8 | 2382.8 | 951.5 | 2382.4 | 956.3 | 2382.0 | 961.0 |
| GR | 2381.2 | 965.8 | 2380.4 | 970.6 | 2379.6 | 975.4 | 2378.8 | 980.2 | 2378.0 | 985.0 |
| GR | 2376.8 | 990.0 | 2375.5 | 995.0 | 2375.0 | 1000.0 | 2375.3 | 1005.0 | 2375.5 | 1010.0 |
| GR | 2375.5 | 1012.0 | 2376.0 | 1016.5 | 2376.5 | 1021.0 | 2376.3 | 1026.5 | 2376.0 | 1032.0 |
| [illegible] | 2376.2 | 1036.3 | 2376.3 | 1040.7 | 2376.5 | 1045.0 | 2376.0 | 1050.0 | 2377.0 | 1054.5 |
| [illegible] | 2378.0 | 1059.0 | 2379.3 | 1064.3 | 2380.7 | 1069.7 | 2382.0 | 1075.0 | 2385.0 | 1130.0 |
| GR | 2385.6 | 1140.0 | 2386.3 | 1150.0 | 2386.9 | 1160.0 | 2387.5 | 1170.0 | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 895 | 1025 |
| X1 | 1.163 | 75 | 975 | 1015 | 445 | 490 | 490 | | | |
| GR | 2392.0 | 540.0 | 2391.8 | 551.0 | 2391.6 | 562.0 | 2391.4 | 573.0 | 2391.2 | 584.0 |
| GR | 2391.0 | 595.0 | 2390.8 | 606.3 | 2390.5 | 617.5 | 2390.3 | 628.8 | 2390.0 | 640.0 |
| GR | 2389.5 | 651.3 | 2389.0 | 662.5 | 2388.5 | 673.8 | 2388.0 | 685.0 | 2387.5 | 693.5 |
| GR | 2387.0 | 702.0 | 2387.0 | 710.0 | 2388.0 | 721.0 | 2389.0 | 730.5 | 2390.0 | 740.0 |
| GR | 2389.8 | 752.5 | 2389.5 | 765.0 | 2389.0 | 776.0 | 2388.5 | 787.0 | 2388.0 | 798.0 |
| GR | 2387.0 | 808.0 | 2386.0 | 818.0 | 2385.0 | 830.0 | 2385.5 | 845.0 | 2385.5 | 860.0 |
| GR | 2384.0 | 870.0 | 2383.0 | 882.5 | 2382.0 | 895.0 | 2381.5 | 902.0 | 2381.3 | 911.3 |
| GR | 2381.2 | 920.7 | 2381.0 | 930.0 | 2381.2 | 940.0 | 2381.3 | 950.0 | 2381.5 | 960.0 |
| GR | 2381.5 | 962.5 | 2381.5 | 965.0 | 2381.5 | 967.5 | 2381.5 | 970.0 | 2380.8 | 972.5 |
| GR | 2380.0 | 975.0 | 2380.0 | 977.3 | 2380.0 | 979.5 | 2380.0 | 981.8 | 2380.0 | 984.1 |
| GR | 2380.0 | 986.4 | 2380.0 | 988.6 | 2380.0 | 990.9 | 2380.0 | 993.2 | 2380.0 | 995.5 |
| GR | 2380.0 | 997.7 | 2380.0 | 1000.0 | 2380.0 | 1002.1 | 2380.0 | 1004.3 | 2380.0 | 1006.4 |
| GR | 2380.0 | 1008.6 | 2380.0 | 1010.7 | 2380.0 | 1012.9 | 2380.0 | 1015.0 | 2381.4 | 1017.3 |
| GR | 2382.7 | 1019.5 | 2384.1 | 1021.8 | 2385.4 | 1024.1 | 2386.8 | 1026.4 | 2388.2 | 1028.6 |
| GR | 2389.6 | 1030.9 | 2390.9 | 1033.2 | 2392.3 | 1035.4 | 2393.6 | 1037.7 | 2395.0 | 1040.0 |
| ET | | | 9.1 | | | | | | 905 | 1034 |
| X1 | 1.239 | 39 | 975 | 1012 | 370 | 410 | 400 | | | |
| GR | 2395.5 | 510.0 | 2394.0 | 525.0 | 2393.5 | 550.0 | 2393.3 | 566.7 | 2393.2 | 583.3 |
| GR | 2393.0 | 600.0 | 2392.8 | 620.0 | 2392.5 | 640.0 | 2392.5 | 656.7 | 2392.5 | 673.3 |
| GR | 2392.5 | 690.0 | 2392.8 | 711.0 | 2393.0 | 732.0 | 2392.8 | 756.0 | 2392.5 | 780.0 |
| GR | 2392.5 | 795.0 | 2392.5 | 810.0 | 2392.3 | 827.5 | 2392.0 | 845.0 | 2391.0 | 862.5 |
| GR | 2390.0 | 880.0 | 2389.0 | 905.0 | 2388.5 | 922.5 | 2388.0 | 930.0 | 2386.0 | 950.0 |
| | 2385.5 | 965.0 | 2385.0 | 970.0 | 2384.5 | 975.0 | 2384.0 | 980.0 | 2383.1 | 980.4 |
| | 2383.1 | 985.3 | 2383.1 | 990.2 | 2383.0 | 995.1 | 2383.0 | 1000.0 | 2383.5 | 1010.0 |
| GR | 2384.0 | 1012.0 | 2386.7 | 1020.0 | 2389.3 | 1030.0 | 2392.0 | 1040.0 | | |
| ET | | | 9.1 | | | | | | 845 | 1166 |
| X1 | 1.367 | 58 | 978 | 1022 | 390 | 630 | 680 | | | |
| GR | 2402.0 | 510.0 | 2401.0 | 530.5 | 2400.0 | 551.0 | 2399.0 | 566.5 | 2398.0 | 582.0 |
| GR | 2396.0 | 595.0 | 2395.5 | 604.0 | 2395.3 | 622.0 | 2395.0 | 640.0 | 2395.5 | 670.0 |
| GR | 2395.5 | 689.0 | 2395.5 | 708.0 | 2394.8 | 724.0 | 2394.0 | 740.0 | 2393.7 | 760.0 |
| GR | 2393.3 | 780.0 | 2393.0 | 800.0 | 2393.5 | 830.0 | 2392.5 | 845.0 | 2392.0 | 872.0 |
| GR | 2394.5 | 891.0 | 2394.5 | 920.0 | 2394.5 | 949.0 | 2394.0 | 954.3 | 2393.5 | 959.7 |
| GR | 2393.0 | 965.0 | 2392.3 | 969.3 | 2391.7 | 973.7 | 2391.0 | 978.0 | 2390.0 | 984.0 |
| GR | 2389.0 | 990.0 | 2388.8 | 995.0 | 2388.5 | 1000.0 | 2388.8 | 1006.0 | 2389.0 | 1012.0 |
| GR | 2390.0 | 1017.0 | 2391.0 | 1022.0 | 2391.5 | 1026.5 | 2392.0 | 1031.0 | 2392.2 | 1036.3 |
| GR | 2392.3 | 1041.7 | 2392.5 | 1047.0 | 2392.0 | 1062.0 | 2391.5 | 1075.0 | 2392.0 | 1090.0 |
| GR | 2392.5 | 1112.0 | 2392.5 | 1142.0 | 2393.3 | 1166.0 | 2394.0 | 1190.0 | 2394.5 | 1212.5 |
| GR | 2395.0 | 1235.0 | 2396.0 | 1253.0 | 2397.3 | 1273.7 | 2398.7 | 1294.3 | 2400.0 | 1315.0 |
| GR | 2400.7 | 1336.7 | 2401.3 | 1358.3 | 2402.0 | 1380.0 | | | | |
| ET | | | 9.1 | | | | | | 981 | 1168 |
| X1 | 1.462 | 79 | 992.9 | 1032.8 | 445 | 440 | 500 | | | |
| GR | 2408.0 | 535.0 | 2407.5 | 552.0 | 2407.0 | 569.0 | 2406.5 | 589.5 | 2406.0 | 610.0 |
| GR | 2405.0 | 630.0 | 2405.5 | 640.0 | 2406.0 | 655.0 | 2406.5 | 665.0 | 2406.5 | 780.0 |
| GR | 2406.0 | 802.0 | 2405.3 | 820.0 | 2404.7 | 838.0 | 2404.0 | 856.0 | 2403.5 | 875.0 |
| GR | 2403.3 | 895.0 | 2403.0 | 915.0 | 2402.5 | 941.0 | 2402.5 | 975.0 | 2402.3 | 977.5 |
| | 2402.0 | 980.0 | 2401.1 | 982.1 | 2400.3 | 984.3 | 2399.4 | 986.4 | 2398.6 | 988.6 |
| | 2397.7 | 990.7 | 2396.9 | 992.9 | 2396.0 | 995.0 | 2395.8 | 997.5 | 2395.5 | 1000.0 |
| GR | 2395.6 | 1002.2 | 2395.7 | 1004.3 | 2395.8 | 1006.5 | 2395.8 | 1008.7 | 2395.9 | 1010.8 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2396.0 | 1013.0 | 2396.1 | 1015.3 | 2396.3 | 1017.5 | 2396.4 | 1019.8 | 2396.5 | 1022.0 |
| | 2396.6 | 1024.2 | 2396.7 | 1026.3 | 2396.8 | 1028.5 | 2396.8 | 1030.7 | 2396.9 | 1032.8 |
| GR | 2397.0 | 1035.0 | 2396.9 | 1037.1 | 2396.9 | 1039.3 | 2396.8 | 1041.4 | 2396.7 | 1043.6 |
| GR | 2396.6 | 1045.7 | 2396.6 | 1047.9 | 2396.5 | 1050.0 | 2396.7 | 1052.2 | 2396.8 | 1054.4 |
| GR | 2397.0 | 1056.7 | 2397.2 | 1058.9 | 2397.3 | 1061.1 | 2397.5 | 1063.3 | 2397.7 | 1065.6 |
| GR | 2397.8 | 1067.8 | 2398.0 | 1070.0 | 2399.0 | 1100.0 | 2398.5 | 1120.0 | 2399.0 | 1139.0 |
| GR | 2400.0 | 1168.0 | 2400.5 | 1189.0 | 2401.0 | 1210.0 | 2401.8 | 1230.0 | 2402.5 | 1250.0 |
| GR | 2403.5 | 1270.0 | 2404.5 | 1290.0 | 2404.8 | 1314.0 | 2405.0 | 1338.0 | 2405.5 | 1358.7 |
| GR | 2406.0 | 1379.3 | 2406.5 | 1400.0 | 2406.8 | 1420.0 | 2407.0 | 1440.0 | | |
| ET | | | 9.1 | | | | | | 956 | 1100 |
| X1 | 1.551 | 42 | 988 | 1029.4 | 470 | 380 | 470 | | | |
| GR | 2420.0 | 930.0 | 2408.0 | 950.0 | 2407.0 | 955.5 | 2406.0 | 961.0 | 2405.0 | 966.5 |
| GR | 2404.0 | 972.0 | 2403.7 | 977.3 | 2403.3 | 982.7 | 2403.0 | 988.0 | 2402.5 | 994.0 |
| GR | 2402.0 | 1000.0 | 2402.3 | 1004.8 | 2402.5 | 1009.5 | 2402.8 | 1014.3 | 2403.0 | 1019.0 |
| GR | 2403.0 | 1024.2 | 2403.0 | 1029.4 | 2403.0 | 1034.6 | 2403.0 | 1039.7 | 2403.0 | 1044.9 |
| GR | 2403.0 | 1050.1 | 2403.0 | 1055.3 | 2403.0 | 1060.4 | 2403.0 | 1065.6 | 2403.0 | 1070.8 |
| GR | 2403.0 | 1076.0 | 2404.0 | 1100.0 | 2405.0 | 1130.0 | 2405.8 | 1155.3 | 2406.5 | 1180.5 |
| GR | 2407.3 | 1205.8 | 2408.0 | 1231.0 | 2408.4 | 1256.8 | 2408.8 | 1282.6 | 2409.2 | 1308.4 |
| GR | 2409.6 | 1334.2 | 2410.0 | 1360.0 | 2410.4 | 1384.0 | 2410.8 | 1408.0 | 2411.2 | 1432.0 |
| GR | 2411.6 | 1456.0 | 2412.0 | 1480.0 | | | | | | |

Confluence of Twin Peaks Wash with Yucca Flats Wash

Floodplain = Floodway from Section 1.646 through 1.905

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 908 | 1071 |
| X1 | 1.646 | 56 | 980 | 1025 | 525 | 460 | 500 | | | |
| GR | 2420.0 | 740.0 | 2416.0 | 752.0 | 2415.4 | 773.1 | 2414.9 | 794.3 | 2414.3 | 815.4 |
| GR | 2413.7 | 836.6 | 2413.1 | 857.7 | 2412.6 | 878.9 | 2412.0 | 900.0 | 2411.0 | 926.0 |
| GR | 2410.0 | 952.0 | 2409.6 | 956.6 | 2409.2 | 961.2 | 2408.8 | 965.8 | 2408.4 | 970.4 |
| GR | 2408.0 | 975.0 | 2407.3 | 980.0 | 2406.7 | 985.0 | 2406.0 | 990.0 | 2405.5 | 995.0 |
| GR | 2405.0 | 1000.0 | 2405.3 | 1005.0 | 2405.7 | 1010.0 | 2406.0 | 1015.0 | 2406.7 | 1020.0 |
| GR | 2407.3 | 1025.0 | 2408.0 | 1030.0 | 2408.4 | 1035.0 | 2408.9 | 1040.0 | 2409.3 | 1045.0 |
| GR | 2409.8 | 1050.0 | 2410.2 | 1055.0 | 2410.7 | 1060.0 | 2411.1 | 1065.0 | 2411.6 | 1070.0 |
| GR | 2412.0 | 1075.0 | 2412.5 | 1100.0 | 2413.0 | 1125.0 | 2413.5 | 1144.3 | 2414.0 | 1163.7 |
| GR | 2414.5 | 1183.0 | 2415.0 | 1202.3 | 2415.5 | 1221.7 | 2416.0 | 1241.0 | 2416.4 | 1262.8 |
| GR | 2416.8 | 1284.6 | 2417.2 | 1306.4 | 2417.6 | 1328.2 | 2418.0 | 1350.0 | 2418.3 | 1370.0 |
| GR | 2418.6 | 1390.0 | 2418.9 | 1410.0 | 2419.1 | 1430.0 | 2419.4 | 1450.0 | 2419.7 | 1470.0 |
| GR | 2420.0 | 1490.0 | | | | | | | | |

Sections 1.718, 1.808 at confluence of Yucca Flat Wash and Twin Peaks Wash

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 820 | 1080 |

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH (DOWNSTREAM)

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 1.718 | 58 | 990 | 1014 | 380 | 380 | 380 | | | |
| GR | 2424.0 | 560.0 | 2422.7 | 583.7 | 2421.3 | 607.3 | 2420.0 | 631.0 | 2419.4 | 655.1 |
| | 2418.9 | 679.3 | 2418.3 | 703.4 | 2417.7 | 727.6 | 2417.1 | 751.7 | 2416.6 | 775.9 |
| | 2416.0 | 800.0 | 2414.0 | 827.5 | 2412.0 | 855.0 | 2410.0 | 872.0 | 2410.5 | 892.5 |
| GR | 2411.0 | 913.0 | 2410.0 | 930.0 | 2410.3 | 935.0 | 2410.5 | 940.0 | 2410.8 | 945.0 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2411.0 | 950.0 | 2411.0 | 954.8 | 2411.0 | 959.7 | 2411.0 | 964.5 | 2411.0 | 969.3 |
| | 2411.0 | 974.2 | 2411.0 | 979.0 | 2410.5 | 984.5 | 2410.0 | 990.0 | 2409.5 | 995.0 |
| GR | 2409.0 | 1000.0 | 2409.3 | 1004.7 | 2409.7 | 1009.3 | 2410.0 | 1014.0 | 2410.3 | 1018.5 |
| GR | 2410.5 | 1023.0 | 2410.8 | 1027.5 | 2411.0 | 1032.0 | 2411.2 | 1036.7 | 2411.3 | 1041.3 |
| GR | 2411.5 | 1046.0 | 2411.7 | 1050.7 | 2411.8 | 1055.3 | 2412.0 | 1060.0 | 2414.0 | 1075.0 |
| GR | 2417.0 | 1100.0 | 2417.5 | 1125.0 | 2418.0 | 1150.0 | 2419.0 | 1176.7 | 2420.0 | 1203.3 |
| GR | 2421.0 | 1230.0 | 2421.4 | 1254.3 | 2421.9 | 1278.6 | 2422.3 | 1302.9 | 2422.7 | 1327.1 |
| GR | 2423.1 | 1351.4 | 2423.6 | 1375.7 | 2424.0 | 1400.0 | | | | |
| QT | 2 | 2085 | 2085 | | | | | | | |
| ET | | 7.1 | 9.1 | | | | 780 | 1200 | 780.0 | 1114.0 |

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH (UPSTREAM)

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 1.808 | 60 | 990 | 1015 | 490 | 465 | 475 | | | |
| GR | 2432 | 420 | 2428 | 455 | 2424 | 490 | 2422 | 640 | 2420 | 790 |
| GR | 2420.0 | 820.0 | 2419.8 | 825.0 | 2419.6 | 830.0 | 2419.4 | 835.0 | 2419.2 | 840.0 |
| GR | 2419.0 | 845.0 | 2418.8 | 850.0 | 2418.6 | 855.0 | 2418.4 | 860.0 | 2418.2 | 865.0 |
| GR | 2418.0 | 870.0 | 2418.2 | 875.0 | 2418.4 | 880.0 | 2418.7 | 885.0 | 2418.9 | 890.0 |
| GR | 2419.1 | 895.0 | 2419.3 | 900.0 | 2419.6 | 905.0 | 2419.8 | 910.0 | 2420.0 | 915.0 |
| GR | 2420.0 | 935.0 | 2419.9 | 940.0 | 2419.7 | 945.0 | 2419.6 | 950.0 | 2419.4 | 955.0 |
| GR | 2419.3 | 960.0 | 2419.1 | 965.0 | 2419.0 | 970.0 | 2418.8 | 975.0 | 2418.5 | 980.0 |
| GR | 2418.3 | 985.0 | 2418.0 | 990.0 | 2417.5 | 995.0 | 2417.0 | 1000.0 | 2417.3 | 1005.0 |
| GR | 2417.7 | 1010.0 | 2418.0 | 1015.0 | 2418.2 | 1020.0 | 2418.4 | 1025.0 | 2418.6 | 1030.0 |
| GR | 2418.8 | 1035.0 | 2419.0 | 1040.0 | 2418.8 | 1045.2 | 2418.7 | 1050.3 | 2418.5 | 1055.5 |
| GR | 2418.3 | 1060.7 | 2418.2 | 1065.8 | 2418.0 | 1071.0 | 2419.0 | 1088.0 | 2420.0 | 1105.0 |
| | 2422.0 | 1125.0 | 2424.0 | 1145.0 | 2425.3 | 1168.3 | 2426.7 | 1191.7 | 2428.0 | 1215.0 |

Yucca Flat Wash flowrate above Twin Peaks confluence calculated adding routed
Yucca Tank inflow (RAH192) and the flow attributable to the intervening area

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 949 | 1198 |

YUCCA FLATS WASH

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 1.905 | 55 | 990 | 1015 | 510 | 500 | 510 | | | |
| GR | 2436.0 | 680.0 | 2434.7 | 699.3 | 2433.3 | 718.7 | 2432.0 | 738.0 | 2431.0 | 764.0 |
| GR | 2430.0 | 790.0 | 2429.5 | 815.0 | 2429.0 | 840.0 | 2428.5 | 865.0 | 2428.0 | 890.0 |
| GR | 2427.3 | 910.0 | 2426.7 | 930.0 | 2426.0 | 950.0 | 2425.6 | 955.0 | 2425.2 | 960.0 |
| GR | 2424.8 | 965.0 | 2424.4 | 970.0 | 2424.0 | 975.0 | 2423.7 | 980.0 | 2423.3 | 985.0 |
| GR | 2423.0 | 990.0 | 2422.5 | 995.0 | 2422.0 | 1000.0 | 2422.3 | 1005.0 | 2422.7 | 1010.0 |
| GR | 2423.0 | 1015.0 | 2423.7 | 1019.7 | 2424.3 | 1024.3 | 2425.0 | 1029.0 | 2425.0 | 1034.1 |
| GR | 2425.0 | 1039.3 | 2425.0 | 1044.4 | 2425.0 | 1049.6 | 2425.0 | 1054.7 | 2425.0 | 1059.9 |
| GR | 2425.0 | 1065.0 | 2424.7 | 1070.0 | 2424.3 | 1075.0 | 2424.0 | 1080.0 | 2423.8 | 1084.6 |
| GR | 2423.6 | 1089.2 | 2423.4 | 1093.8 | 2423.2 | 1098.4 | 2423.0 | 1103.0 | 2424.0 | 1120.0 |
| GR | 2424.5 | 1137.5 | 2425.0 | 1155.0 | 2424.5 | 1172.5 | 2424.0 | 1190.0 | 2432.0 | 1221.0 |
| GR | 2433.0 | 1245.5 | 2434.0 | 1270.0 | 2434.0 | 1300.0 | 2433.0 | 1326.0 | 2432.0 | 1352.0 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 768 | 1039 |
| X1 | 2.003 | 76 | 981 | 1010 | 530 | 450 | 520 | | | |
| GR | 2438.0 | 460.0 | 2438.0 | 490.0 | 2437.5 | 507.5 | 2437.0 | 525.0 | 2436.5 | 543.0 |
| GR | 2436.0 | 561.0 | 2435.3 | 584.7 | 2434.7 | 608.3 | 2434.0 | 632.0 | 2433.6 | 654.6 |
| GR | 2433.2 | 677.2 | 2432.8 | 699.8 | 2432.4 | 722.4 | 2432.0 | 745.0 | 2431.5 | 767.5 |
| GR | 2431.0 | 790.0 | 2431.0 | 812.5 | 2431.0 | 835.0 | 2431.5 | 853.0 | 2432.0 | 871.0 |
| GR | 2432.0 | 887.5 | 2432.0 | 904.0 | 2431.9 | 908.8 | 2431.8 | 913.7 | 2431.8 | 918.5 |
| GR | 2431.7 | 923.3 | 2431.6 | 928.2 | 2431.5 | 933.0 | 2431.4 | 937.8 | 2431.3 | 942.7 |
| GR | 2431.3 | 947.5 | 2431.2 | 952.3 | 2431.1 | 957.2 | 2431.0 | 962.0 | 2430.8 | 966.8 |
| GR | 2430.5 | 971.5 | 2430.3 | 976.3 | 2430.0 | 981.0 | 2429.8 | 985.8 | 2429.5 | 990.5 |
| GR | 2429.3 | 995.3 | 2429.0 | 1000.0 | 2429.5 | 1005.0 | 2430.0 | 1010.0 | 2430.7 | 1015.0 |
| GR | 2431.3 | 1020.0 | 2432.0 | 1025.0 | 2432.3 | 1030.0 | 2432.7 | 1035.0 | 2433.0 | 1040.0 |
| GR | 2433.3 | 1045.0 | 2433.7 | 1050.0 | 2434.0 | 1055.0 | 2434.3 | 1060.0 | 2434.7 | 1065.0 |
| GR | 2435.0 | 1070.0 | 2434.9 | 1075.2 | 2434.8 | 1080.4 | 2434.7 | 1085.6 | 2434.6 | 1090.8 |
| GR | 2434.5 | 1096.0 | 2434.4 | 1101.2 | 2434.3 | 1106.4 | 2434.2 | 1111.6 | 2434.1 | 1116.8 |
| GR | 2434.0 | 1122.0 | 2433.5 | 1146.0 | 2433.0 | 1170.0 | 2434.5 | 1196.0 | 2436.0 | 1222.0 |
| GR | 2436.7 | 1243.3 | 2437.3 | 1264.7 | 2438.0 | 1286.0 | 2438.7 | 1307.3 | 2439.3 | 1328.7 |
| GR | 2440.0 | 1350.0 | | | | | | | | |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 800 | 1015 |
| X1 | 2.091 | 55 | 970 | 1000 | 300 | 460 | 460 | | | |
| GR | 2440.0 | 640.0 | 2438.0 | 659.5 | 2436.0 | 679.0 | 2434.0 | 710.0 | 2436.0 | 741.0 |
| GR | 2436.3 | 760.7 | 2436.7 | 780.3 | 2437.0 | 800.0 | 2436.7 | 818.3 | 2436.3 | 836.7 |
| GR | 2436.0 | 855.0 | 2435.0 | 880.0 | 2436.0 | 900.0 | 2437.0 | 921.0 | 2436.8 | 926.2 |
| GR | 2436.7 | 931.3 | 2436.5 | 936.5 | 2436.3 | 941.7 | 2436.2 | 946.8 | 2436.0 | 952.0 |
| GR | 2435.5 | 956.5 | 2435.0 | 961.0 | 2434.5 | 965.5 | 2434.0 | 970.0 | 2434.0 | 975.0 |
| GR | 2434.0 | 980.0 | 2434.0 | 985.0 | 2434.0 | 990.0 | 2434.0 | 995.0 | 2434.0 | 1000.0 |
| GR | 2434.5 | 1005.0 | 2435.0 | 1010.0 | 2435.5 | 1015.0 | 2436.0 | 1020.0 | 2437.0 | 1026.0 |
| GR | 2438.0 | 1032.0 | 2438.2 | 1037.2 | 2438.3 | 1042.3 | 2438.5 | 1047.5 | 2438.7 | 1052.7 |
| GR | 2438.8 | 1057.8 | 2439.0 | 1063.0 | 2439.1 | 1068.2 | 2439.2 | 1073.4 | 2439.3 | 1078.6 |
| GR | 2439.4 | 1083.8 | 2439.5 | 1089.0 | 2439.6 | 1094.2 | 2439.7 | 1099.4 | 2439.8 | 1104.6 |
| GR | 2439.9 | 1109.8 | 2440.0 | 1115.0 | 2442.7 | 1137.0 | 2445.3 | 1159.0 | 2448.0 | 1181.0 |

Hydraulic Base Line for 2.189 used to be at station 1060. Modified 6/17/92.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 821 | 1040 |
| X1 | 2.172 | 20 | 990 | 1010 | 370 | 440 | 430 | | | |
| GR | 2446.0 | 640.0 | 2445.0 | 665.0 | 2444.0 | 690.0 | 2442.7 | 724.0 | 2441.3 | 758.0 |
| GR | 2440.0 | 792.0 | 2440.0 | 806.3 | 2440.0 | 820.7 | 2440.0 | 835.0 | 2440.7 | 848.3 |
| GR | 2441.3 | 861.7 | 2442 | 920 | 2440 | 970 | 2439 | 990 | 2438 | 1000 |
| GR | 2439 | 1010 | 2440 | 1030 | 2444 | 1070 | 2448 | 1090 | 2452 | 1120 |

Floodplain and FW for section 2.284 shifted 20 ft right to fit topography.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | 7.1 | 9.1 | | | | 723.7 | 1208 | 951 | 1148 |

ENCROACHED TO 1208 DUE TO SMALL RIGHT BANK TRIBUTARY. FLOODPLAIN
MAPPED TO WSEL.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| X1 | 2.284 | 46 | 977.5 | 1005 | 530 | 540 | 590 | | | |
| GR | 2461.3 | 723.7 | 2462.0 | 750.0 | 2462.0 | 775.0 | 2462.0 | 800.0 | 2461.0 | 823.0 |
| GR | 2460.0 | 846.0 | 2458.0 | 872.0 | 2456.0 | 898.0 | 2452.0 | 942.0 | 2450.0 | 956.0 |
| GR | 2448 | 970 | 2447.5 | 977.5 | 2447 | 985 | 2447 | 1000 | 2447.5 | 1005 |
| GR | 2447.6 | 1006 | 2447.7 | 1007 | 2447.8 | 1008 | 2448.0 | 1010 | 2449.0 | 1026 |
| GR | 2449.0 | 1040.0 | 2448.0 | 1060.0 | 2448.5 | 1072.5 | 2449.0 | 1085.0 | 2449.3 | 1116.7 |
| GR | 2449.7 | 1148.3 | 2450.0 | 1180.0 | 2450.3 | 1208.3 | 2450.7 | 1236.7 | 2451.0 | 1265.0 |
| GR | 2451.0 | 1296.7 | 2451.0 | 1328.3 | 2451.0 | 1360.0 | 2450.5 | 1384.5 | 2450.0 | 1409.0 |
| GR | 2452.0 | 1450.0 | 2452.5 | 1477.5 | 2453.0 | 1505.0 | 2453.5 | 1532.5 | 2454.0 | 1560.0 |
| GR | 2454.7 | 1594.7 | 2455.3 | 1629.3 | 2456.0 | 1664.0 | 2457.3 | 1697.7 | 2458.7 | 1731.3 |
| GR | 2460.0 | 1765.0 | | | | | | | | |

Sections 2.384 through end of Yucca Flat Wash in the shadow of Yucca Tank.
Floodplain = Floodway.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 894 | 1095 |
| X1 | 2.384 | 30 | 990 | 1009 | 490 | 520 | 530 | | | |
| GR | 2461.3 | 704.0 | 2461.7 | 727.0 | 2462.0 | 750.0 | 2461.5 | 780.0 | 2461.0 | 810.0 |
| GR | 2460.0 | 834.0 | 2456.0 | 865.0 | 2455.5 | 893.5 | 2455.0 | 922.0 | 2455.0 | 943.5 |
| GR | 2455.0 | 965.0 | 2454.0 | 980.0 | 2453.0 | 990.0 | 2453.0 | 1000.0 | 2453.0 | 1009.0 |
| GR | 2454.0 | 1020.0 | 2455.0 | 1041.0 | 2455.5 | 1060.5 | 2456.0 | 1080.0 | 2457.0 | 1100.0 |
| GR | 2458.0 | 1120.0 | 2459.0 | 1151.0 | 2460.0 | 1182.0 | 2461.3 | 1206.3 | 2462.7 | 1230.7 |
| GR | 2464.0 | 1255.0 | 2465.0 | 1281.3 | 2466.0 | 1307.5 | 2467.0 | 1333.8 | 2468.0 | 1360.0 |
| | | | 9.1 | | | | | | 935 | 1334 |
| X1 | 2.477 | 71 | 991 | 1015 | 510 | 420 | 490 | | | |
| GR | 2472.0 | 762.0 | 2471.5 | 781.0 | 2471.0 | 800.0 | 2470.0 | 830.0 | 2469.0 | 849.5 |
| GR | 2468.0 | 869.0 | 2466.0 | 890.5 | 2464.0 | 912.0 | 2463.7 | 916.9 | 2463.3 | 921.8 |
| GR | 2463.0 | 926.7 | 2462.7 | 931.6 | 2462.3 | 936.4 | 2462.0 | 941.3 | 2461.7 | 946.2 |
| GR | 2461.3 | 951.1 | 2461.0 | 956.0 | 2460.7 | 960.7 | 2460.3 | 965.3 | 2460.0 | 970.0 |
| GR | 2459.5 | 975.3 | 2459.0 | 980.5 | 2458.5 | 985.8 | 2458.0 | 991.0 | 2457.5 | 995.5 |
| GR | 2457.0 | 1000.0 | 2457.3 | 1005.0 | 2457.7 | 1010.0 | 2458.0 | 1015.0 | 2458.7 | 1020.0 |
| GR | 2459.3 | 1025.0 | 2460.0 | 1030.0 | 2460.3 | 1035.0 | 2460.5 | 1040.0 | 2460.8 | 1045.0 |
| GR | 2461.0 | 1050.0 | 2461.1 | 1055.1 | 2461.1 | 1060.3 | 2461.2 | 1065.4 | 2461.3 | 1070.6 |
| GR | 2461.4 | 1075.7 | 2461.4 | 1080.9 | 2461.5 | 1086.0 | 2461.6 | 1091.1 | 2461.6 | 1096.3 |
| GR | 2461.7 | 1101.4 | 2461.8 | 1106.6 | 2461.9 | 1111.7 | 2461.9 | 1116.9 | 2462.0 | 1122.0 |
| GR | 2462.3 | 1144.3 | 2462.7 | 1166.7 | 2463.0 | 1189.0 | 2462.5 | 1209.5 | 2462.0 | 1230.0 |
| GR | 2461.7 | 1253.3 | 2461.3 | 1276.7 | 2461.0 | 1300.0 | 2462.0 | 1330.0 | 2464.0 | 1348.0 |
| GR | 2466.0 | 1365.0 | 2466.3 | 1386.0 | 2466.7 | 1407.0 | 2467.0 | 1428.0 | 2467.3 | 1452.0 |
| GR | 2467.7 | 1476.0 | 2468.0 | 1500.0 | 2469.0 | 1520.0 | 2470.0 | 1540.0 | 2471.0 | 1560.0 |
| GR | 2472.0 | 1580.0 | | | | | | | | |
| ET | | | 9.1 | | | | | | 912 | 1193 |
| X1 | 2.562 | 77 | 987.5 | 1012.5 | 420 | 475 | 450 | | | |
| GR | 2480.0 | 680.0 | 2478.7 | 690.0 | 2477.3 | 700.0 | 2476.0 | 710.0 | 2474.0 | 722.5 |
| GR | 2472.0 | 735.0 | 2472.0 | 748.3 | 2472.0 | 761.7 | 2472.0 | 775.0 | 2472.3 | 787.3 |
| GR | 2472.5 | 799.5 | 2472.8 | 811.8 | 2473.0 | 824.0 | 2472.7 | 837.7 | 2472.3 | 851.3 |
| GR | 2472.0 | 865.0 | 2470.7 | 878.3 | 2469.3 | 891.7 | 2468.0 | 905.0 | 2467.0 | 917.5 |
| GR | 2466.0 | 930.0 | 2465.8 | 941.3 | 2465.5 | 952.5 | 2465.3 | 963.8 | 2465.0 | 975.0 |
| GR | 2465.0 | 987.5 | 2465.0 | 1000.0 | 2465.0 | 1012.5 | 2465.0 | 1025.0 | 2465.3 | 1035.0 |
| GR | 2465.7 | 1045.0 | 2466.0 | 1055.0 | 2466.7 | 1065.3 | 2467.3 | 1075.7 | 2468.0 | 1086.0 |

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2468.0 | 1090.9 | 2468.0 | 1095.7 | 2468.0 | 1100.6 | 2468.0 | 1105.4 | 2468.0 | 1110.3 |
| | 2468.0 | 1115.1 | 2468.0 | 1120.0 | 2467.3 | 1125.0 | 2466.7 | 1130.0 | 2466.0 | 1135.0 |
| GR | 2465.5 | 1140.0 | 2465.0 | 1145.0 | 2465.5 | 1150.0 | 2466.0 | 1155.0 | 2466.3 | 1160.5 |
| GR | 2466.5 | 1166.0 | 2466.8 | 1171.5 | 2467.0 | 1177.0 | 2467.1 | 1181.9 | 2467.3 | 1186.8 |
| GR | 2467.4 | 1191.6 | 2467.5 | 1196.5 | 2467.6 | 1201.4 | 2467.8 | 1206.3 | 2467.9 | 1211.1 |
| GR | 2468.0 | 1216.0 | 2469.0 | 1228.0 | 2470.0 | 1240.0 | 2471.0 | 1252.0 | 2472.0 | 1264.0 |
| GR | 2472.0 | 1277.0 | 2472.0 | 1290.0 | 2471.7 | 1300.3 | 2471.3 | 1310.7 | 2471.0 | 1321.0 |
| GR | 2471.5 | 1333.0 | 2472.0 | 1345.0 | 2474.0 | 1359.0 | 2476.0 | 1373.0 | 2477.3 | 1384.3 |
| GR | 2478.7 | 1395.7 | 2480.0 | 1407.0 | | | | | | |
| ET | | | 9.1 | | | | | | 821 | 1044 |
| X1 | 2.672 | 44 | 986 | 1011 | 610 | 525 | 580 | | | |
| GR | 2484.0 | 671.0 | 2483.0 | 682.0 | 2482.0 | 693.0 | 2481.0 | 704.0 | 2480.0 | 715.0 |
| GR | 2478.7 | 726.7 | 2477.3 | 738.3 | 2476.0 | 750.0 | 2476.0 | 760.5 | 2476.0 | 771.0 |
| GR | 2476.0 | 781.5 | 2476.0 | 792.0 | 2475.8 | 802.9 | 2475.6 | 813.8 | 2475.3 | 824.7 |
| GR | 2475.1 | 835.6 | 2474.9 | 846.4 | 2474.7 | 857.3 | 2474.4 | 868.2 | 2474.2 | 879.1 |
| GR | 2474.0 | 890.0 | 2473.5 | 900.0 | 2473.0 | 910.0 | 2472.0 | 922.0 | 2472.5 | 930.5 |
| GR | 2473.0 | 939.0 | 2474.0 | 952.0 | 2474.0 | 961.0 | 2474.0 | 970.0 | 2473.0 | 986.0 |
| GR | 2472.0 | 1000.0 | 2473.0 | 1011.0 | 2473.5 | 1021.0 | 2474.0 | 1031.0 | 2475.0 | 1040.5 |
| GR | 2476.0 | 1050.0 | 2477.3 | 1062.3 | 2478.7 | 1074.7 | 2480.0 | 1087.0 | 2480.8 | 1097.6 |
| GR | 2481.6 | 1108.2 | 2482.4 | 1118.8 | 2483.2 | 1129.4 | 2484.0 | 1140.0 | | |
| ET | | | 9.1 | | | | | | 797 | 1081 |
| X1 | 2.761 | 93 | 974.3 | 1006.5 | 385 | 460 | 470 | | | |
| GR | 2492.5 | 575.0 | 2492.0 | 582.5 | 2491.5 | 590.0 | 2491.3 | 596.4 | 2491.1 | 602.8 |
| | 2490.9 | 609.1 | 2490.8 | 615.5 | 2490.6 | 621.9 | 2490.4 | 628.3 | 2490.2 | 634.6 |
| | 2490.0 | 641.0 | 2489.9 | 647.4 | 2489.8 | 653.8 | 2489.6 | 660.3 | 2489.5 | 666.7 |
| | 2489.4 | 673.1 | 2489.3 | 679.5 | 2489.1 | 685.9 | 2489.0 | 692.3 | 2488.9 | 698.8 |
| GR | 2488.8 | 705.2 | 2488.6 | 711.6 | 2488.5 | 718.0 | 2488.4 | 723.8 | 2488.3 | 729.5 |
| GR | 2488.1 | 735.3 | 2488.0 | 741.0 | 2487.3 | 747.3 | 2486.7 | 753.7 | 2486.0 | 760.0 |
| GR | 2485.0 | 767.5 | 2484.0 | 775.0 | 2483.0 | 781.3 | 2482.0 | 787.5 | 2481.0 | 793.8 |
| GR | 2480.0 | 800.0 | 2479.9 | 806.5 | 2479.8 | 812.9 | 2479.7 | 819.4 | 2479.6 | 825.9 |
| GR | 2479.6 | 832.3 | 2479.5 | 838.8 | 2479.4 | 845.3 | 2479.3 | 851.8 | 2479.2 | 858.2 |
| GR | 2479.1 | 864.7 | 2479.0 | 871.2 | 2478.9 | 877.7 | 2478.9 | 884.1 | 2478.8 | 890.6 |
| GR | 2478.7 | 897.1 | 2478.6 | 903.5 | 2478.5 | 910.0 | 2478.5 | 916.4 | 2478.4 | 922.9 |
| GR | 2478.4 | 935.7 | 2478.3 | 942.1 | 2478.3 | 955.0 | 2478.2 | 961.4 | 2478.2 | 967.9 |
| GR | 2478.1 | 974.3 | 2478.1 | 987.1 | 2478.0 | 993.6 | 2478.0 | 1000.0 | 2478.2 | 1006.5 |
| GR | 2478.4 | 1013.1 | 2478.6 | 1019.6 | 2478.7 | 1026.2 | 2478.9 | 1032.7 | 2479.1 | 1039.3 |
| GR | 2479.3 | 1045.8 | 2479.4 | 1052.4 | 2479.6 | 1058.9 | 2479.8 | 1065.4 | 2480.0 | 1072.0 |
| GR | 2480.4 | 1078.6 | 2480.7 | 1085.1 | 2481.1 | 1091.6 | 2481.4 | 1098.2 | 2481.8 | 1104.7 |
| GR | 2482.2 | 1111.3 | 2482.6 | 1117.8 | 2482.9 | 1124.4 | 2483.3 | 1130.9 | 2483.6 | 1137.4 |
| GR | 2484.0 | 1144.0 | 2484.6 | 1150.4 | 2485.1 | 1156.9 | 2485.7 | 1163.3 | 2486.3 | 1169.7 |
| GR | 2486.9 | 1176.1 | 2487.4 | 1182.6 | 2488.0 | 1189.0 | | | | |

Sections 2.840 and 2.948 from topographic maps.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 957 | 1314 |
| X1 | 2.857 | 11 | 985 | 1015 | 480 | 485 | 510 | | | |
| GR | 2500 | 860 | 2496 | 880 | 2492 | 920 | 2488 | 960 | 2486 | 985 |
| GR | 2486 | 1000 | 2486 | 1015 | 2488 | 1310 | 2492 | 1370 | 2496 | 1385 |
| | 2500 | 1400 | | | | | | | | |

```
                                9.1                                                                922       1254
X1     2.965        9       985      1015       570       350       570
GR      2504      880      2500       890      2496       930      2495       985      2495      1000
GR      2495     1015      2496      1250      2500      1270      2504      1280


QT         2     5152      5152
ET                          9.1                                                                820       1080

          CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH
X1    -1.718       58       990      1014       380       380       380
GR    2424.0    560.0    2422.7     583.7    2421.3     607.3    2420.0     631.0    2419.4     655.1
GR    2418.9    679.3    2418.3     703.4    2417.7     727.6    2417.1     751.7    2416.6     775.9
GR    2416.0    800.0    2414.0     827.5    2412.0     855.0    2410.0     872.0    2410.5     892.5
GR    2411.0    913.0    2410.0     930.0    2410.3     935.0    2410.5     940.0    2410.8     945.0
GR    2411.0    950.0    2411.0     954.8    2411.0     959.7    2411.0     964.5    2411.0     969.3
GR    2411.0    974.2    2411.0     979.0    2410.5     984.5    2410.0     990.0    2409.5     995.0
GR    2409.0   1000.0    2409.3    1004.7    2409.7    1009.3    2410.0    1014.0    2410.3    1018.5
GR    2410.5   1023.0    2410.8    1027.5    2411.0    1032.0    2411.2    1036.7    2411.3    1041.3
GR    2411.5   1046.0    2411.7    1050.7    2411.8    1055.3    2412.0    1060.0    2414.0    1075.0
GR    2417.0   1100.0    2417.5    1125.0    2418.0    1150.0    2419.0    1176.7    2420.0    1203.3
GR    2421.0   1230.0    2421.4    1254.3    2421.9    1278.6    2422.3    1302.9    2422.7    1327.1
GR    2423.1   1351.4    2423.6    1375.7    2424.0    1400.0

 Begin Twin Peaks Wash.


QT         2     2099      2099
ET                          9.1                                                                911       1145
X1     0.098       29      977.0     1016.0       410       565       520
GR    2426.0    736.0    2425.0     760.0    2424.0     784.0    2423.0     804.5    2422.0     825.0
GR    2421.0    845.5    2420.0     866.0    2419.4     888.2    2418.8     910.4    2418.2     932.6
GR    2417.6    954.8    2417.0     977.0    2416.0    1000.0    2415.0    1016.0    2416.0    1037.0
GR    2417.0   1056.5    2418.0    1076.0    2417.0    1091.0    2418.0    1107.0    2418.4    1127.4
GR    2418.8   1145.8    2419.2    1165.2    2419.6    1184.6    2420.0    1204.0    2420.3    1224.5
GR      2420     1226      2424      1491      2428      1561      2432      1596
  Q from HEC-1 model operation CAB 186.
    Section .190 renumbered to avoid duplication of section from Yucca Flat Wash
       Formerly .191

ET                          9.1                                                                955       1036
X1     0.190       44       985    1007.5       510       420       490
GR      2428      780      2426       800      2424       820      2423     845.5      2422       871
GR      2423      890      2423     910.5      2423       931    2422.9     935.9    2422.7     940.7
GR    2422.6    945.6    2422.4     950.4    2422.3     955.3    2422.1     960.1      2422       965
GR    2421.3      970    2420.7       975      2420       980    2419.5       985    2418.5       995
GR      2418     1000      2419      1005    2419.5    1007.5      2420      1010      2421    1015.5
GR      2422     1021    2422.1    1026.1    2422.2    1031.2    2422.3    1036.3    2422.4    1041.4
GR    2422.5   1046.5    2422.6    1051.6    2422.7    1056.7    2422.8    1061.8    2422.9    1066.9
GR      2423     1072    2423.3    1076.5    2423.5      1081    2423.8    1085.5      2424      1090
        2425     1095      2426      1100      2428      1105      2428      1110
```

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | | 7.1 | 9.1 | | | | 850 | 1425 | 937 | 1055 |
| X1 | 0.301 | 82 | 987 | 1009 | 450 | 610 | 580 | | | |
| GR | 2440.0 | 440.0 | 2436.0 | 470.0 | 2434.0 | 487.5 | 2432.0 | 505.0 | 2431.0 | 522.5 |
| GR | 2430.0 | 540.0 | 2429.7 | 561.7 | 2429.3 | 583.3 | 2429.0 | 605.0 | 2429.0 | 612.0 |
| GR | 2429.7 | 636.3 | 2430.3 | 660.7 | 2431.0 | 685.0 | 2430.7 | 706.7 | 2430.3 | 728.3 |
| GR | 2430.0 | 750.0 | 2430.0 | 776.7 | 2430.0 | 803.3 | 2430.0 | 830.0 | 2430.5 | 855.5 |
| GR | 2431.0 | 881.0 | 2430.9 | 886.1 | 2430.8 | 891.2 | 2430.7 | 896.3 | 2430.6 | 901.4 |
| GR | 2430.5 | 906.5 | 2430.4 | 911.6 | 2430.3 | 916.7 | 2430.2 | 921.8 | 2430.1 | 926.9 |
| GR | 2430.0 | 932.0 | 2429.9 | 936.8 | 2429.8 | 941.6 | 2429.7 | 946.3 | 2429.6 | 951.1 |
| GR | 2429.4 | 955.9 | 2429.3 | 960.7 | 2429.2 | 965.4 | 2429.1 | 970.2 | 2429.0 | 975.0 |
| GR | 2428.5 | 981.0 | 2428.0 | 987.0 | 2427.7 | 991.3 | 2427.3 | 995.7 | 2427.0 | 1000.0 |
| GR | 2427.5 | 1004.5 | 2428.0 | 1009.0 | 2428.5 | 1015.0 | 2429.0 | 1021.0 | 2429.1 | 1025.9 |
| GR | 2429.2 | 1030.8 | 2429.3 | 1035.7 | 2429.4 | 1040.6 | 2429.6 | 1045.4 | 2429.7 | 1050.3 |
| GR | 2429.8 | 1055.2 | 2429.9 | 1060.1 | 2430.0 | 1065.0 | 2430.0 | 1070.0 | 2430.0 | 1075.0 |
| GR | 2430.0 | 1080.0 | 2430.0 | 1085.0 | 2430.0 | 1090.0 | 2430.0 | 1095.0 | 2430.0 | 1100.0 |
| GR | 2430.0 | 1105.0 | 2430.0 | 1110.0 | 2430.0 | 1115.0 | 2430.0 | 1120.0 | 2430.0 | 1125.0 |
| GR | 2430.0 | 1130.0 | 2430.0 | 1135.0 | 2430.7 | 1140.0 | 2431.3 | 1145.0 | 2432.0 | 1150.0 |
| GR | 2433.0 | 1155.0 | 2434.0 | 1160.0 | 2435.0 | 1165.0 | 2436.0 | 1170.0 | 2438.0 | 1189.0 |
| GR | 2439.0 | 1217.0 | 2440.0 | 1245.0 | | | | | | |
| ET | | | 9.1 | | | | | | 948 | 1041 |
| X1 | 0.384 | 72 | 990 | 1011 | 440 | 440 | 440 | | | |
| GR | 2448.0 | 670.0 | 2446.0 | 695.0 | 2444.0 | 720.0 | 2442.7 | 743.3 | 2441.3 | 766.7 |
| GR | 2440.0 | 790.0 | 2439.0 | 813.3 | 2438.0 | 836.7 | 2437.0 | 860.0 | 2436.7 | 883.3 |
| GR | 2436.3 | 906.7 | 2436.0 | 930.0 | 2435.4 | 935.0 | 2434.9 | 940.0 | 2434.3 | 945.0 |
| | 2433.7 | 950.0 | 2433.1 | 955.0 | 2432.6 | 960.0 | 2432.0 | 965.0 | 2431.6 | 970.0 |
| | 2431.2 | 975.0 | 2430.8 | 980.0 | 2430.4 | 985.0 | 2430.0 | 990.0 | 2429.5 | 995.0 |
| GR | 2429.0 | 1000.0 | 2429.5 | 1005.5 | 2430.0 | 1011.0 | 2430.3 | 1016.0 | 2430.7 | 1021.0 |
| GR | 2431.0 | 1026.0 | 2431.3 | 1031.0 | 2431.7 | 1036.0 | 2432.0 | 1041.0 | 2432.4 | 1045.9 |
| GR | 2432.9 | 1050.7 | 2433.3 | 1055.6 | 2433.7 | 1060.4 | 2434.1 | 1065.3 | 2434.6 | 1070.1 |
| GR | 2435.0 | 1075.0 | 2435.2 | 1079.8 | 2435.4 | 1084.6 | 2435.6 | 1089.4 | 2435.8 | 1094.2 |
| GR | 2436.0 | 1099.0 | 2435.0 | 1120.0 | 2436.0 | 1155.0 | 2436.5 | 1185.0 | 2437.0 | 1215.0 |
| GR | 2436.0 | 1240.0 | 2440.0 | 1275.0 | 2441.0 | 1315.0 | 2442.0 | 1350.0 | 2441.0 | 1380.0 |
| GR | 2439.0 | 1410.0 | 2437.0 | 1437.0 | 2438.0 | 1458.0 | 2438.5 | 1489.0 | 2439.0 | 1520.0 |
| GR | 2440.0 | 1541.0 | 2441.0 | 1562.0 | 2442.0 | 1600.0 | 2442.7 | 1630.0 | 2443.3 | 1660.0 |
| GR | 2444.0 | 1690.0 | 2444.7 | 1720.3 | 2445.3 | 1750.7 | 2446.0 | 1781.0 | 2446.7 | 1812.3 |
| GR | 2447.3 | 1843.7 | 2448.0 | 1875.0 | | | | | | |
| ET | | | 9.1 | | | | | | 930 | 1032 |
| X1 | 0.473 | 64 | 985 | 1012 | 550 | 420 | 470 | | | |
| GR | 2456 | 500 | 2452 | 600 | 2448 | 640 | 2446 | 665 | 2444 | 690 |
| GR | 2441.0 | 791.0 | 2440.0 | 812.0 | 2440.0 | 839.0 | 2440.0 | 866.0 | 2439.5 | 888.0 |
| GR | 2439.0 | 910.0 | 2438.9 | 915.1 | 2438.8 | 920.2 | 2438.7 | 925.3 | 2438.6 | 930.4 |
| GR | 2438.5 | 935.5 | 2438.4 | 940.6 | 2438.3 | 945.7 | 2438.2 | 950.8 | 2438.1 | 955.9 |
| GR | 2438.0 | 961.0 | 2438.0 | 965.8 | 2438.0 | 970.6 | 2438.0 | 975.4 | 2438.0 | 980.2 |
| GR | 2438.0 | 985.0 | 2437.7 | 990.0 | 2437.3 | 995.0 | 2437.0 | 1000.0 | 2437.5 | 1006.0 |
| GR | 2438.0 | 1012.0 | 2438.5 | 1016.5 | 2439.0 | 1021.0 | 2439.5 | 1025.5 | 2440.0 | 1030.0 |
| GR | 2442.0 | 1035.0 | 2444.0 | 1040.0 | 2444.5 | 1045.0 | 2445.0 | 1050.0 | 2445.0 | 1054.8 |
| GR | 2445.0 | 1059.7 | 2445.0 | 1064.5 | 2445.0 | 1069.3 | 2445.0 | 1074.2 | 2445.0 | 1079.0 |
| GR | 2445.0 | 1083.8 | 2445.0 | 1088.7 | 2445.0 | 1093.5 | 2445.0 | 1098.3 | 2445.0 | 1103.2 |
| | 2445.0 | 1108.0 | 2445.3 | 1133.3 | 2445.7 | 1158.7 | 2446.0 | 1184.0 | 2446.0 | 1208.0 |
| | 2446.0 | 1232.0 | 2446.0 | 1256.0 | 2446.0 | 1280.0 | 2446.0 | 1304.0 | 2446.4 | 1324.8 |
| GR | 2446.8 | 1345.6 | 2447.2 | 1366.4 | 2447.6 | 1387.2 | 2448.0 | 1408.0 | | |

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|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 961 | 1073 |
| X1 | 0.581 | 33 | 990 | 1010 | 270 | 570 | 570 | | | |
| GR | 2456 | 641 | 2452 | 776 | 2448 | 871 | 2447.0 | 961.0 | 2446.8 | 965.8 |
| GR | 2446.5 | 970.5 | 2446.3 | 975.3 | 2446.0 | 980.0 | 2445.0 | 985.0 | 2444.0 | 990.0 |
| GR | 2443.5 | 995.0 | 2443.0 | 1000.0 | 2443.5 | 1005.0 | 2444.0 | 1010.0 | 2445.0 | 1015.5 |
| GR | 2446.0 | 1021.0 | 2446.2 | 1025.7 | 2446.3 | 1030.3 | 2446.5 | 1035.0 | 2446.7 | 1039.7 |
| GR | 2446.8 | 1044.3 | 2447.0 | 1049.0 | 2447.0 | 1073.0 | 2447.0 | 1097.0 | 2447.0 | 1121.0 |
| GR | 2447.0 | 1145.0 | 2447.5 | 1175.0 | 2448.0 | 1205.0 | 2449.3 | 1231.3 | 2450.7 | 1257.7 |
| GR | 2452.0 | 1284.0 | 2454.0 | 1311.5 | 2456.0 | 1339.0 | | | | |

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|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 911 | 1040 |
| X1 | 0.669 | 61 | 990 | 1010 | 420 | 390 | 460 | | | |
| GR | 2464.0 | 770.0 | 2460.0 | 799.0 | 2456.0 | 811.0 | 2453.0 | 840.5 | 2450.0 | 870.0 |
| GR | 2450.0 | 899.0 | 2451.0 | 911.0 | 2451.0 | 915.9 | 2451.0 | 920.8 | 2451.0 | 925.7 |
| GR | 2451.0 | 930.6 | 2451.0 | 935.5 | 2451.0 | 940.4 | 2451.0 | 945.3 | 2451.0 | 950.2 |
| GR | 2451.0 | 955.1 | 2451.0 | 960.0 | 2450.8 | 964.8 | 2450.5 | 969.5 | 2450.3 | 974.3 |
| GR | 2450.0 | 979.0 | 2449.5 | 984.5 | 2449.0 | 990.0 | 2448.5 | 995.0 | 2448.0 | 1000.0 |
| GR | 2448.5 | 1005.0 | 2449.0 | 1010.0 | 2449.3 | 1014.8 | 2449.5 | 1019.5 | 2449.8 | 1024.3 |
| GR | 2450.0 | 1029.0 | 2450.3 | 1034.3 | 2450.7 | 1039.7 | 2451.0 | 1045.0 | 2451.0 | 1050.0 |
| GR | 2451.0 | 1055.0 | 2451.0 | 1060.0 | 2451.0 | 1065.0 | 2451.0 | 1070.0 | 2451.0 | 1075.0 |
| GR | 2451.0 | 1080.0 | 2451.0 | 1085.0 | 2451.0 | 1090.0 | 2451.0 | 1095.0 | 2451.0 | 1100.0 |
| GR | 2451.0 | 1105.0 | 2452.0 | 1140.0 | 2452.5 | 1165.0 | 2453.0 | 1190.0 | 2454.0 | 1216.7 |
| GR | 2455.0 | 1243.3 | 2456.0 | 1270.0 | 2457.0 | 1295.0 | 2458.0 | 1320.0 | 2459.0 | 1345.0 |
| GR | 2460.0 | 1370.0 | 2460.8 | 1396.0 | 2461.6 | 1422.0 | 2462.4 | 1448.0 | 2463.2 | 1474.0 |
| GR | 2464.0 | 1500.0 | | | | | | | | |

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|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 965 | 1032 |
| X1 | 0.765 | 56 | 990 | 1005 | 470 | 490 | 510 | | | |
| GR | 2472.0 | 675.0 | 2470.0 | 688.5 | 2468.0 | 702.0 | 2466.0 | 715.5 | 2464.0 | 729.0 |
| GR | 2460.0 | 748.0 | 2457.0 | 770.0 | 2457.3 | 785.0 | 2457.5 | 800.0 | 2457.8 | 815.0 |
| GR | 2458.0 | 830.0 | 2457.3 | 847.0 | 2456.7 | 864.0 | 2456.0 | 881.0 | 2457.0 | 899.0 |
| GR | 2458.0 | 917.0 | 2458.0 | 921.7 | 2458.0 | 926.4 | 2458.0 | 931.1 | 2458.0 | 935.9 |
| GR | 2458.0 | 940.6 | 2458.0 | 945.3 | 2458.0 | 950.0 | 2457.7 | 955.0 | 2457.3 | 960.0 |
| GR | 2457.0 | 965.0 | 2456.0 | 970.0 | 2455.0 | 975.0 | 2454.0 | 980.0 | 2453.8 | 985.0 |
| GR | 2453.5 | 990.0 | 2453.3 | 995.0 | 2453.0 | 1000.0 | 2453.5 | 1005.0 | 2454.0 | 1010.0 |
| GR | 2455.0 | 1015.0 | 2456.0 | 1020.0 | 2457.0 | 1025.0 | 2458.0 | 1030.0 | 2459.0 | 1035.0 |
| GR | 2460.0 | 1040.0 | 2460.5 | 1044.9 | 2461.0 | 1049.8 | 2461.5 | 1054.6 | 2462.0 | 1059.5 |
| GR | 2462.5 | 1064.4 | 2463.0 | 1069.3 | 2463.5 | 1074.1 | 2464.0 | 1079.0 | 2464.3 | 1093.7 |
| GR | 2464.6 | 1108.4 | 2464.9 | 1123.1 | 2465.1 | 1137.9 | 2465.4 | 1152.6 | 2465.7 | 1167.3 |
| GR | 2466.0 | 1182.0 | | | | | | | | |

Section 0.866 through end of Twin Peaks Wash Floodplain = Floodway.

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| ET | | | 9.1 | | | | | | 907 | 1030 |
| X1 | 0.866 | 45 | 992 | 1010 | 510 | 530 | 530 | | | |
| GR | 2470.0 | 785.0 | 2469.0 | 801.0 | 2468.0 | 817.0 | 2467.2 | 833.4 | 2466.4 | 849.8 |
| GR | 2465.6 | 866.2 | 2464.8 | 882.6 | 2464.0 | 899.0 | 2462.0 | 914.5 | 2460.0 | 930.0 |
| GR | 2460.0 | 950.0 | 2460.5 | 955.0 | 2461.0 | 960.0 | 2461.5 | 965.0 | 2462.0 | 970.0 |
| GR | 2461.5 | 975.5 | 2461.0 | 981.0 | 2460.0 | 986.5 | 2459.0 | 992.0 | 2458.5 | 996.0 |
| GR | 2458.0 | 1000.0 | 2458.5 | 1005.0 | 2459.0 | 1010.0 | 2459.5 | 1015.0 | 2460.0 | 1020.0 |
| GR | 2461.5 | 1025.0 | 2463.0 | 1030.0 | 2463.1 | 1035.0 | 2463.3 | 1040.0 | 2463.4 | 1045.0 |
| GR | 2463.5 | 1050.0 | 2463.6 | 1055.0 | 2463.8 | 1060.0 | 2463.9 | 1065.0 | 2464.0 | 1070.0 |

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|---|---|---|---|---|---|---|---|---|---|---|
| | 2464.4 | 1085.6 | 2464.8 | 1101.2 | 2465.2 | 1116.8 | 2465.6 | 1132.4 | 2466.0 | 1148.0 |
| | 2467.0 | 1164.0 | 2468.0 | 1180.0 | 2469.0 | 1193.3 | 2470.0 | 1206.7 | 2471.0 | 1220.0 |
| ET | | | 9.1 | | | | | | 965 | 1039 |
| X1 | 0.949 | 22 | 990 | 1010 | 440 | 440 | 440 | | | |
| GR | 2476.0 | 810.0 | 2474.7 | 823.3 | 2473.3 | 836.7 | 2472.0 | 850.0 | 2471.8 | 864.0 |
| GR | 2471.6 | 878.0 | 2471.4 | 892.0 | 2471.2 | 906.0 | 2471.0 | 920.0 | 2470.7 | 933.3 |
| GR | 2470.3 | 946.7 | 2470.0 | 960.0 | 2468.0 | 979.0 | 2464.0 | 990.0 | 2463.0 | 1000.0 |
| GR | 2464.0 | 1010.0 | 2466.0 | 1020.0 | 2468.0 | 1030.0 | 2470.0 | 1042.0 | 2472.0 | 1054.0 |
| GR | 2473.5 | 1067.0 | 2475.0 | 1080.0 | | | | | | |
| ET | | | 9.1 | | | | | | 904 | 1074 |
| X1 | 1.045 | 52 | 990 | 1010 | 510 | 535 | 510 | | | |
| GR | 2484.0 | 807.0 | 2483.0 | 820.3 | 2482.0 | 833.5 | 2481.0 | 846.8 | 2480.0 | 860.0 |
| GR | 2476.0 | 881.0 | 2475.0 | 896.0 | 2474.0 | 911.0 | 2473.5 | 925.5 | 2473.0 | 940.0 |
| GR | 2473.0 | 945.4 | 2473.0 | 950.8 | 2473.0 | 956.2 | 2473.0 | 961.6 | 2473.0 | 967.0 |
| GR | 2472.7 | 971.3 | 2472.3 | 975.7 | 2472.0 | 980.0 | 2471.0 | 985.0 | 2470.0 | 990.0 |
| GR | 2469.5 | 995.0 | 2469.0 | 1000.0 | 2469.5 | 1005.0 | 2470.0 | 1010.0 | 2470.5 | 1015.5 |
| GR | 2471.0 | 1021.0 | 2471.4 | 1025.8 | 2471.8 | 1030.6 | 2472.2 | 1035.4 | 2472.6 | 1040.2 |
| GR | 2473.0 | 1045.0 | 2473.3 | 1049.8 | 2473.5 | 1054.7 | 2473.8 | 1059.5 | 2474.0 | 1064.3 |
| GR | 2474.3 | 1069.2 | 2474.5 | 1074.0 | 2474.8 | 1078.8 | 2475.0 | 1083.7 | 2475.3 | 1088.5 |
| GR | 2475.5 | 1093.3 | 2475.8 | 1098.2 | 2476.0 | 1103.0 | 2476.3 | 1117.5 | 2476.7 | 1132.0 |
| GR | 2477.0 | 1146.5 | 2477.3 | 1161.0 | 2477.7 | 1175.5 | 2478.0 | 1190.0 | 2480.0 | 1212.0 |
| GR | 2482.0 | 1227.5 | 2484.0 | 1243.0 | | | | | | |
| ET | | | 9.1 | | | | | | 958 | 1035 |
| | 1.148 | 44 | 989 | 1010 | 525 | 540 | 540 | | | |
| | 2488.0 | 850.0 | 2487.5 | 864.8 | 2487.0 | 879.5 | 2486.5 | 894.3 | 2486.0 | 909.0 |
| GR | 2485.8 | 913.9 | 2485.5 | 918.8 | 2485.3 | 923.6 | 2485.0 | 928.5 | 2484.8 | 933.4 |
| GR | 2484.5 | 938.3 | 2484.3 | 943.1 | 2484.0 | 948.0 | 2482.7 | 952.3 | 2481.3 | 956.7 |
| GR | 2480.0 | 961.0 | 2479.0 | 966.5 | 2478.0 | 972.0 | 2477.3 | 977.7 | 2476.7 | 983.3 |
| GR | 2476.0 | 989.0 | 2475.5 | 994.5 | 2475.0 | 1000.0 | 2475.5 | 1005.0 | 2476.0 | 1010.0 |
| GR | 2478.0 | 1015.0 | 2480.0 | 1020.0 | 2480.3 | 1025.0 | 2480.7 | 1030.0 | 2481.0 | 1035.0 |
| GR | 2481.2 | 1040.0 | 2481.4 | 1045.0 | 2481.6 | 1050.0 | 2481.8 | 1055.0 | 2482.0 | 1060.0 |
| GR | 2482.3 | 1075.3 | 2482.7 | 1090.7 | 2483.0 | 1106.0 | 2483.3 | 1121.3 | 2483.7 | 1136.7 |
| GR | 2484.0 | 1152.0 | 2485.0 | 1165.3 | 2486.0 | 1178.7 | 2487.0 | 1192.0 | | |
| ET | | | 9.1 | | | | | | 947 | 1061 |
| X1 | 1.242 | 41 | 990 | 1010 | 500 | 485 | 500 | | | |
| GR | 2492.0 | 883.0 | 2488.0 | 900.0 | 2488.0 | 916.0 | 2488.0 | 932.0 | 2487.7 | 936.7 |
| GR | 2487.4 | 941.4 | 2487.1 | 946.1 | 2486.9 | 950.9 | 2486.6 | 955.6 | 2486.3 | 960.3 |
| GR | 2486.0 | 965.0 | 2485.3 | 970.0 | 2484.7 | 975.0 | 2484.0 | 980.0 | 2483.0 | 985.0 |
| GR | 2482.0 | 990.0 | 2481.5 | 995.0 | 2481.0 | 1000.0 | 2481.5 | 1005.0 | 2482.0 | 1010.0 |
| GR | 2483.0 | 1015.0 | 2484.0 | 1020.0 | 2484.4 | 1025.0 | 2484.8 | 1030.0 | 2485.2 | 1035.0 |
| GR | 2485.6 | 1040.0 | 2486.0 | 1045.0 | 2486.3 | 1050.0 | 2486.7 | 1055.0 | 2487.0 | 1060.0 |
| GR | 2487.3 | 1065.0 | 2487.7 | 1070.0 | 2488.0 | 1075.0 | 2488.1 | 1089.3 | 2488.3 | 1103.6 |
| GR | 2488.4 | 1117.9 | 2488.6 | 1132.1 | 2488.7 | 1146.4 | 2488.9 | 1160.7 | 2489.0 | 1175.0 |
| GR | 2492.0 | 1192.0 | | | | | | | | |

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|---|---|---|---|---|---|---|---|---|---|---|
| | | | 9.1 | | | | | | 972 | 1043 |
| X1 | 1.343 | 29 | 985 | 1012 | 530 | 510 | 530 | | | |
| GR | 2504.0 | 950.0 | 2502.7 | 955.0 | 2501.3 | 960.0 | 2500.0 | 965.0 | 2496.0 | 972.0 |
| GR | 2494.7 | 976.3 | 2493.3 | 980.7 | 2492.0 | 985.0 | 2491.3 | 989.7 | 2490.7 | 994.3 |
| GR | 2490.0 | 999.0 | 2489.0 | 1000.0 | 2490.0 | 1005.0 | 2492.0 | 1012.0 | 2492.6 | 1017.4 |
| GR | 2493.2 | 1022.8 | 2493.8 | 1028.2 | 2494.4 | 1033.6 | 2495.0 | 1039.0 | 2496.3 | 1043.8 |
| GR | 2497.5 | 1048.5 | 2498.8 | 1053.3 | 2500.0 | 1058.0 | 2501.3 | 1063.3 | 2502.7 | 1068.7 |
| GR | 2504.0 | 1074.0 | 2505.3 | 1079.3 | 2506.7 | 1084.7 | 2508.0 | 1090.0 | | |
| ET | | | 9.1 | | | | | | 971 | 1062 |
| X1 | 1.428 | 54 | 990 | 1010 | 435 | 435 | 450 | | | |
| GR | 2510.0 | 870.0 | 2509.5 | 875.8 | 2509.0 | 881.5 | 2508.5 | 887.3 | 2508.0 | 893.0 |
| GR | 2507.2 | 898.4 | 2506.4 | 903.8 | 2505.6 | 909.2 | 2504.8 | 914.6 | 2504.0 | 920.0 |
| GR | 2503.9 | 925.0 | 2503.7 | 930.0 | 2503.6 | 935.0 | 2503.4 | 940.0 | 2503.3 | 945.0 |
| GR | 2503.1 | 950.0 | 2503.0 | 955.0 | 2502.3 | 960.0 | 2501.5 | 965.0 | 2500.8 | 970.0 |
| GR | 2500.0 | 975.0 | 2498.7 | 980.0 | 2497.3 | 985.0 | 2496.0 | 990.0 | 2495.5 | 995.0 |
| GR | 2495.0 | 1000.0 | 2495.5 | 1005.0 | 2496.0 | 1010.0 | 2496.5 | 1015.0 | 2497.0 | 1020.0 |
| GR | 2497.5 | 1025.0 | 2498.0 | 1030.0 | 2498.4 | 1035.6 | 2498.8 | 1041.2 | 2499.2 | 1046.8 |
| GR | 2499.6 | 1052.4 | 2500.0 | 1058.0 | 2501.0 | 1063.2 | 2502.0 | 1068.3 | 2503.0 | 1073.5 |
| GR | 2504.0 | 1078.7 | 2505.0 | 1083.8 | 2506.0 | 1089.0 | 2507.0 | 1094.3 | 2508.0 | 1099.7 |
| GR | 2509.0 | 1105.0 | 2510.0 | 1110.3 | 2511.0 | 1115.7 | 2512.0 | 1121.0 | 2512.8 | 1126.8 |
| GR | 2513.6 | 1132.6 | 2514.4 | 1138.4 | 2515.2 | 1144.2 | 2516.0 | 1150.0 | | |
| ET | | | 9.1 | | | | | | 934 | 1031 |
| X1 | 1.525 | 50 | 990 | 1010 | 500 | 460 | 510 | | | |
| [illegible] | 2516.0 | 830.0 | 2515.7 | 835.0 | 2515.4 | 840.0 | 2515.1 | 845.0 | 2514.9 | 850.0 |
| [illegible] | 2514.6 | 855.0 | 2514.3 | 860.0 | 2514.0 | 865.0 | 2513.8 | 870.0 | 2513.6 | 875.0 |
| GR | 2513.3 | 880.0 | 2513.1 | 885.0 | 2512.9 | 890.0 | 2512.7 | 895.0 | 2512.4 | 900.0 |
| GR | 2512.2 | 905.0 | 2512.0 | 910.0 | 2510.0 | 915.5 | 2508.0 | 921.0 | 2507.3 | 925.8 |
| GR | 2506.7 | 930.7 | 2506.0 | 935.5 | 2505.3 | 940.3 | 2504.7 | 945.2 | 2504.0 | 950.0 |
| GR | 2503.8 | 955.0 | 2503.7 | 960.0 | 2503.5 | 965.0 | 2503.3 | 970.0 | 2503.2 | 975.0 |
| GR | 2503.0 | 980.0 | 2502.5 | 985.0 | 2502.0 | 990.0 | 2501.5 | 995.0 | 2501.0 | 1000.0 |
| GR | 2501.5 | 1005.0 | 2502.0 | 1010.0 | 2503.0 | 1015.0 | 2504.0 | 1020.0 | 2505.0 | 1025.0 |
| GR | 2506.0 | 1030.0 | 2507.0 | 1035.0 | 2508.0 | 1040.0 | 2509.7 | 1045.0 | 2511.4 | 1050.0 |
| GR | 2513.1 | 1055.0 | 2514.9 | 1060.0 | 2516.6 | 1065.0 | 2518.3 | 1070.0 | 2520.0 | 1075.0 |
| ET | | | 9.1 | | | | | | 968 | 1061 |
| X1 | 1.619 | 94 | 992.5 | 1012.5 | 460 | 525 | 500 | | | |
| GR | 2524.0 | 885.0 | 2523.6 | 890.0 | 2523.3 | 892.5 | 2523.1 | 895.0 | 2522.9 | 897.5 |
| GR | 2522.7 | 900.0 | 2522.4 | 902.5 | 2522.2 | 905.0 | 2522.0 | 907.5 | 2521.8 | 910.0 |
| GR | 2521.6 | 912.5 | 2521.3 | 915.0 | 2521.1 | 917.5 | 2520.9 | 920.0 | 2520.7 | 922.5 |
| GR | 2520.4 | 925.0 | 2520.2 | 927.5 | 2520.0 | 930.0 | 2519.7 | 932.5 | 2519.4 | 935.0 |
| GR | 2519.1 | 937.5 | 2518.9 | 940.0 | 2518.6 | 942.5 | 2518.3 | 945.0 | 2518.0 | 947.5 |
| GR | 2517.7 | 950.0 | 2517.4 | 952.5 | 2517.1 | 955.0 | 2516.9 | 957.5 | 2516.6 | 960.0 |
| GR | 2516.3 | 962.5 | 2516.0 | 965.0 | 2515.3 | 967.5 | 2514.7 | 970.0 | 2514.0 | 972.5 |
| GR | 2513.3 | 975.0 | 2512.7 | 977.5 | 2512.0 | 980.0 | 2511.8 | 982.5 | 2511.5 | 985.0 |
| GR | 2511.3 | 987.5 | 2511.0 | 990.0 | 2510.8 | 992.5 | 2510.5 | 995.0 | 2510.3 | 997.5 |
| GR | 2510.0 | 1000.0 | 2510.2 | 1002.5 | 2510.3 | 1005.0 | 2510.5 | 1007.5 | 2510.7 | 1010.0 |
| GR | 2510.8 | 1012.5 | 2511.0 | 1015.0 | 2511.2 | 1017.5 | 2511.3 | 1020.0 | 2511.5 | 1022.5 |
| GR | 2511.7 | 1025.0 | 2511.8 | 1027.5 | 2512.0 | 1030.0 | 2512.3 | 1032.5 | 2512.5 | 1035.0 |
| [illegible] | 2512.8 | 1037.5 | 2513.0 | 1040.0 | 2513.3 | 1042.5 | 2513.5 | 1045.0 | 2513.8 | 1047.5 |
| [illegible] | 2514.0 | 1050.0 | 2514.3 | 1052.5 | 2514.5 | 1055.0 | 2514.8 | 1057.5 | 2515.0 | 1060.0 |
| GR | 2515.3 | 1062.5 | 2515.5 | 1065.0 | 2515.8 | 1067.5 | 2516.0 | 1070.0 | 2516.3 | 1072.5 |

```
     2516.5    1075.0    2516.8    1077.5    2517.0    1080.0    2518.3    1082.5    2519.5    1085.0
     2519.8    1087.5    2520.0    1090.0    2521.3    1092.5    2522.5    1095.0    2523.8    1097.5
GR   2524.0    1100.0    2524.3    1102.5    2525.5    1105.0    2525.8    1107.5    2526.0    1110.0
GR   2526.3    1112.5    2527.6    1115.0    2527.9    1117.5    2528.0    1120.0

ET                       9.1                                                          967       1069
X1    1.719       37     990       1011      515       490       525
GR   2540.0     930.0    2538.0    935.0     2536.0    940.0     2534.0    945.0     2532.0    950.0
GR   2528.0     956.0    2524.0    962.0     2522.7    967.7     2521.3    973.3     2520.0    979.0
GR   2519.5     984.5    2519.0    990.0     2518.5    995.0     2518.0    1000.0    2518.5    1005.5
GR   2519.0    1011.0    2519.2    1015.8    2519.4    1020.6    2519.6    1025.4    2519.8    1030.2
GR   2520.0    1035.0    2520.4    1040.0    2520.9    1045.0    2521.3    1050.0    2521.7    1055.0
GR   2522.1    1060.0    2522.6    1065.0    2523.0    1070.0    2523.8    1075.3    2524.5    1080.5
GR   2525.3    1085.8    2526.0    1091.0    2527.2    1096.8    2528.4    1102.6    2529.6    1108.4
GR   2530.8    1114.2    2532.0    1120.0

ET                       9.1                                                          947       1015
X1    1.802       37     989       1010      440       350       440
GR   2534.0     870.0    2533.8    875.0     2533.6    880.0     2533.3    885.0     2533.1    890.0
GR   2532.9     895.0    2532.7    900.0     2532.4    905.0     2532.2    910.0     2532.0    915.0
GR   2531.6     920.0    2531.3    925.0     2530.9    930.0     2530.6    935.0     2530.2    940.0
GR   2529.8     945.0    2529.4    950.0     2529.1    955.0     2528.7    960.0     2528.4    965.0
GR   2528.0     970.0    2527.0    974.8     2526.0    979.5     2525.0    984.3     2524.0    989.0
GR   2523.5     994.5    2523.0    1000.0    2523.5    1005.0    2524.0    1010.0    2529.3    1015.0
GR   2534.7    1020.0    2540.0    1025.0    2541.6    1030.0    2543.2    1035.0    2544.8    1040.0
     2546.4    1045.0    2548.0    1050.0
```

for upper Twin Peaks Wash calculated by adding HEC-1 model operation RAB182 and portion of SAB185 attributable to intervening area. Small tributary enters from left in this vicinity.

```
QT       2       1650      1650
ET                         9.1                                                          952       1045
X1    1.897       50       985.8     1008.0    480       545       500
GR   2544.0     920.0      2543.3    923.3     2542.7    926.7     2542.0    930.0     2541.3    933.3
GR   2540.7     936.7      2540.0    940.0     2539.7    943.5     2539.3    947.0     2539.0    950.5
GR   2538.7     954.0      2538.3    957.5     2538.0    961.0     2537.6    964.0     2537.2    967.0
GR   2536.8     970.0      2536.4    973.0     2536.0    976.0     2535.8    979.3     2535.5    982.5
GR   2535.3     985.8      2535.0    989.0     2534.7    992.7     2534.3    996.3     2534.0    1000.0
GR   2534.5    1002.5      2535.0    1005.0    2535.3    1008.0    2535.5    1011.0    2535.8    1014.0
GR   2536.0    1017.0      2536.3    1020.5    2536.7    1024.0    2537.0    1027.5    2537.3    1031.0
GR   2537.7    1034.5      2538.0    1038.0    2538.4    1041.4    2538.8    1044.8    2539.2    1048.2
GR   2539.6    1051.6      2540.0    1055.0    2540.6    1058.3    2541.3    1061.5    2541.9    1064.8
GR   2542.5    1068.0      2543.1    1071.3    2543.8    1074.5    2544.4    1077.8    2545.0    1081.0

ET                         9.1                                                          911       1034
X1    1.993       58       990       1010      535       430       510
GR   2552.0     770.0      2551.0    775.3     2550.0    780.5     2549.0    785.8     2548.0    791.0
GR   2547.3     797.3      2546.7    803.7     2546.0    810.0     2545.7    815.1     2545.4    820.3
GR   2545.1     825.4      2544.9    830.6     2544.6    835.7     2544.3    840.9     2544.0    846.0
     2543.9     851.3      2543.9    856.6     2543.8    861.9     2543.7    867.2     2543.6    872.5
     2543.5     877.8      2543.5    883.2     2543.4    888.5     2543.3    893.8     2543.2    899.1
GR   2543.1     904.4      2543.1    909.7     2543.0    915.0     2542.9    920.6     2542.8    926.1
```

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 2542.7 | 931.7 | 2542.6 | 937.2 | 2542.4 | 942.8 | 2542.3 | 948.3 | 2542.2 | 953.9 |
| | 2542.1 | 959.4 | 2542.0 | 965.0 | 2541.0 | 971.5 | 2540.0 | 978.0 | 2539.5 | 984.0 |
| GR | 2539.0 | 990.0 | 2538.5 | 995.0 | 2538.0 | 1000.0 | 2538.5 | 1005.0 | 2539.0 | 1010.0 |
| GR | 2539.5 | 1015.0 | 2540.0 | 1020.0 | 2541.3 | 1026.3 | 2542.7 | 1032.7 | 2544.0 | 1039.0 |
| GR | 2544.5 | 1044.8 | 2545.0 | 1050.5 | 2545.5 | 1056.3 | 2546.0 | 1062.0 | 2546.5 | 1067.8 |
| GR | 2547.0 | 1073.5 | 2547.5 | 1079.3 | 2548.0 | 1085.0 | | | | |
| ET | | | 9.1 | | | | | | 976 | 1063 |
| X1 | 2.094 | 41 | 990 | 1011 | 495 | 530 | 530 | | | |
| GR | 2552.0 | 940.0 | 2552.3 | 945.0 | 2552.7 | 950.0 | 2553.0 | 955.0 | 2552.7 | 959.7 |
| GR | 2552.3 | 964.3 | 2552.0 | 969.0 | 2550.0 | 974.5 | 2548.0 | 980.0 | 2546.5 | 985.0 |
| GR | 2545.0 | 990.0 | 2544.5 | 995.0 | 2544.0 | 1000.0 | 2544.5 | 1005.5 | 2545.0 | 1011.0 |
| GR | 2545.7 | 1015.7 | 2546.3 | 1020.3 | 2547.0 | 1025.0 | 2547.3 | 1030.0 | 2547.5 | 1035.0 |
| GR | 2547.8 | 1040.0 | 2548.0 | 1045.0 | 2548.4 | 1050.5 | 2548.8 | 1056.0 | 2549.2 | 1061.5 |
| GR | 2549.6 | 1067.0 | 2550.0 | 1072.5 | 2550.4 | 1078.0 | 2550.8 | 1083.5 | 2551.2 | 1089.0 |
| GR | 2551.6 | 1094.5 | 2552.0 | 1100.0 | 2552.4 | 1105.6 | 2552.9 | 1111.1 | 2553.3 | 1116.7 |
| GR | 2553.8 | 1122.2 | 2554.2 | 1127.8 | 2554.7 | 1133.3 | 2555.1 | 1138.9 | 2555.6 | 1144.4 |
| GR | 2556.0 | 1150.0 | | | | | | | | |
| ET | | | 9.1 | | | | | | 966 | 1027 |
| X1 | 2.183 | 69 | 990 | 1009 | 470 | 410 | 470 | | | |
| GR | 2562.0 | 710.0 | 2561.6 | 715.0 | 2561.2 | 720.0 | 2560.8 | 725.0 | 2560.4 | 730.0 |
| GR | 2560.0 | 735.0 | 2559.5 | 740.3 | 2559.0 | 745.5 | 2558.5 | 750.8 | 2558.0 | 756.0 |
| GR | 2557.5 | 761.3 | 2557.0 | 766.5 | 2556.5 | 771.8 | 2556.0 | 777.0 | 2555.7 | 781.9 |
| GR | 2555.4 | 786.7 | 2555.1 | 791.6 | 2554.9 | 796.4 | 2554.6 | 801.3 | 2554.3 | 806.1 |
| | 2554.0 | 811.0 | 2554.1 | 815.9 | 2554.2 | 820.8 | 2554.3 | 825.7 | 2554.4 | 830.6 |
| | 2554.4 | 835.5 | 2554.6 | 840.5 | 2554.6 | 845.4 | 2554.7 | 850.3 | 2554.8 | 855.2 |
| GR | 2554.9 | 860.1 | 2555.0 | 865.0 | 2555.3 | 870.3 | 2555.5 | 875.5 | 2555.8 | 880.8 |
| GR | 2556.0 | 886.0 | 2555.8 | 890.8 | 2555.6 | 895.6 | 2555.4 | 900.4 | 2555.2 | 905.2 |
| GR | 2555.0 | 910.0 | 2554.9 | 915.0 | 2554.8 | 920.0 | 2554.7 | 925.0 | 2554.6 | 930.0 |
| GR | 2554.5 | 935.0 | 2554.4 | 940.0 | 2554.3 | 945.0 | 2554.2 | 950.0 | 2554.1 | 955.0 |
| GR | 2554.0 | 960.0 | 2553.0 | 965.0 | 2552.0 | 970.0 | 2551.0 | 975.0 | 2550.0 | 980.0 |
| GR | 2549.0 | 985.0 | 2548.7 | 990.0 | 2548.3 | 995.0 | 2548.0 | 1000.0 | 2548.3 | 1004.5 |
| GR | 2548.5 | 1009.0 | 2548.8 | 1013.5 | 2549.0 | 1018.0 | 2552.0 | 1025.0 | 2553.6 | 1030.0 |
| GR | 2555.2 | 1035.0 | 2556.8 | 1040.0 | 2558.4 | 1045.0 | 2560.0 | 1050.0 | | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

```
*PROF 1

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV=     .100 CEHV=     .300
*SECNO 2.435
 WATER EL=X5 CARD=   2309.800
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      952.0    1228.0  TYPE=      1  TARGET=      276.000
         STARTING WSEL FROM UPPER FLYING E WASH ANALYSIS.
         CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH.

    2.435      6.37   2309.87   2309.87       .00   2311.91      2.03       .00       .00   2304.00
   6943.0     829.2    3269.5    2844.4     123.2     219.6     397.0        .0        .0   2304.00
      .00      6.73     14.89      7.16      .050      .030      .050      .000   2303.50    957.69
  .008113      500.      490.      455.         0         5         3       .00    180.52   1138.21


FLOW DISTRIBUTION FOR SECNO=      2.43         CWSEL=   2309.87

        958.     976.     991.    1027.    1037.    1047.    1057.    1067.    1077.    1092.    1102.    1138.
  PER Q=      3.9      8.1     47.1      7.1      6.5      5.9      5.3      4.8      6.1      3.1      2.3
   AREA=     50.1     73.1    219.6     57.2     54.2     51.2     48.2     45.2     61.9     34.7     44.2
    VEL=      5.4      7.7     14.9      8.6      8.3      8.0      7.6      7.3      6.9      6.1      3.6
  DEPTH=      2.7      4.9      6.1      5.7      5.4      5.1      4.8      4.5      4.1      3.5      1.2

1490 NH CARD USED
*SECNO 2.539

3265 DIVIDED FLOW


3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      465.3    1100.0  TYPE=      1  TARGET=      634.700
 ELENCL=   2317.30  ELENCR=   2317.00
         AT HIGH FLOW, BOTH YUCCA FLAT WASH AND FLYING E WASH CHANNELS
         ARE USED.  SECTION REPEATED FOR BOTH MODELS. NH CARD DEFINES CHANNELS
```

HYDRAULIC CONTROL LINE IS AT STATION 850.0

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.539 | 6.51 | 2315.51 | 2315.51 | .00 | 2316.75 | 1.23 | 4.16 | .08 | 2313.50 |
| 6943.0 | 374.5 | 1748.2 | 4820.2 | 127.7 | 185.8 | 533.5 | 9.4 | 3.5 | 2313.20 |
| .02 | 2.93 | 9.41 | 9.03 | .050 | .030 | .038 | .000 | 2309.00 | 509.79 |
| .007925 | 570. | 550. | 490. | 0 | 5 | 0 | .00 | 395.38 | 1059.11 |

FLOW DISTRIBUTION FOR SECNO= 2.54 CWSEL= 2315.51

| STA= | 510. | 593. | 822. | 881. | 907. | 962. | 980. | 1000. | 1012. | 1027. | 1035. | 1059. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 1.5 | 25.2 | 3.4 | 3.2 | 3.9 | 27.0 | 16.2 | 10.6 | 3.3 | 1.8 | |
| AREA= | 86.8 | 40.9 | 185.8 | 53.8 | 70.4 | 52.0 | 125.3 | 75.2 | 86.5 | 34.1 | 36.3 | |
| VEL= | 3.2 | 2.5 | 9.4 | 4.3 | 3.1 | 5.3 | 15.0 | 15.0 | 8.5 | 6.7 | 3.5 | |
| DEPTH= | 1.0 | .2 | 3.1 | 2.1 | 1.3 | 2.9 | 6.3 | 6.3 | 5.8 | 4.3 | 1.5 | |

*SECNO .191

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .191 | 4.85 | 2322.35 | 2322.35 | .00 | 2323.22 | .87 | 4.50 | .04 | 2320.00 |
| 5152.0 | 2842.6 | 2260.4 | 49.0 | 629.0 | 224.0 | 20.2 | 18.5 | 8.1 | 2320.00 |
| .04 | 4.52 | 10.09 | 2.43 | .060 | .040 | .060 | .000 | 2317.50 | 559.50 |
| .012840 | 410. | 490. | 500. | 0 | 16 | 0 | .00 | 502.63 | 1093.75 |

FLOW DISTRIBUTION FOR SECNO= .19 CWSEL= 2322.35

| STA= | 559. | 612. | 632. | 663. | 760. | 775. | 790. | 817. | 846. | 876. | 898. | 906. | 913. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 4.6 | 3.1 | 3.5 | 3.4 | 3.3 | 3.1 | 3.9 | 3.2 | 5.3 | 4.7 | 4.1 | |
| AREA= | 51.1 | 47.0 | 40.6 | 62.6 | 35.3 | 34.5 | 42.3 | 49.7 | 44.6 | 53.7 | 33.6 | 29.4 | |
| VEL= | 3.2 | 5.0 | 3.9 | 2.9 | 5.0 | 5.0 | 3.7 | 4.1 | 3.7 | 5.1 | 7.2 | 7.2 | |
| DEPTH= | 1.0 | 2.4 | 1.3 | .6 | 2.4 | 2.3 | 1.5 | 1.7 | 1.5 | 2.4 | 4.2 | 4.2 | |

| STA= | 913. | 927. | 947. | 960. | 1020. | 1094. |
|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 3.5 | 2.6 | 43.9 | 1.0 | |
| AREA= | 35.7 | 40.0 | 28.9 | 224.0 | 20.2 | |
| VEL= | 5.3 | 4.5 | 4.7 | 10.1 | 2.4 | |
| DEPTH= | 2.6 | 2.0 | 2.2 | 3.7 | .3 | |

*SECNO .290
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .290 | 3.76 | 2328.76 | 2328.76 | .00 | 2329.79 | 1.02 | 5.93 | .05 | 2326.40 |
| 5152.0 | 1373.4 | 1755.2 | 2023.4 | 274.5 | 156.2 | 314.7 | 27.1 | 12.7 | 2326.30 |
| .05 | 5.00 | 11.24 | 6.43 | .050 | .030 | .050 | .000 | 2325.00 | 773.82 |
| .011927 | 420. | 520. | 520. | 0 | 15 | 0 | .00 | 388.95 | 1162.77 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .29 CWSEL= 2328.76

| STA= | 774. | 835. | 850. | 863. | 886. | 977. | 1029. | 1042. | 1055. | 1068. | 1075. | 1095. | 1107. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.6 | 5.9 | 5.1 | 4.4 | 5.7 | 34.1 | 3.4 | 4.1 | 5.5 | 3.6 | 11.5 | 5.4 | |
| AREA= | 65.1 | 44.8 | 39.1 | 44.4 | 81.1 | 156.2 | 30.7 | 34.4 | 41.0 | 24.2 | 75.2 | 39.1 | |
| VEL= | 4.5 | 6.7 | 6.7 | 5.1 | 3.6 | 11.2 | 5.8 | 6.1 | 6.9 | 7.6 | 7.9 | 7.1 | |
| DEPTH= | 1.1 | 3.0 | 2.9 | 2.0 | .9 | 3.0 | 2.4 | 2.6 | 3.1 | 3.6 | 3.8 | 3.3 | |

| STA= | 1107. | 1121. | 1163. |
|---|---|---|---|
| PER Q= | 3.4 | 2.4 | |
| AREA= | 31.7 | 38.3 | |
| VEL= | 5.6 | 3.2 | |
| DEPTH= | 2.3 | .9 | |

*SECNO .390

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
[illegible] CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .390 | 4.34 | 2336.34 | 2336.34 | .00 | 2337.04 | .70 | 5.72 | .03 | 2334.00 |
| 5152.0 | 818.9 | 1283.4 | 3049.8 | 223.9 | 113.5 | 699.8 | 37.5 | 19.0 | 2334.00 |
| .08 | 3.66 | 11.31 | 4.36 | .050 | .030 | .050 | .000 | 2332.00 | 790.79 |
| .010549 | 530. | 530. | 490. | 0 | 11 | 0 | .00 | 689.13 | 1488.02 |

FLOW DISTRIBUTION FOR SECNO= .39 CWSEL= 2336.34

| STA= | 791. | 855. | 922. | 952. | 982. | 1016. | 1040. | 1066. | 1106. | 1151. | 1180. | 1234. | 1262. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 4.2 | 4.2 | 4.4 | 24.9 | 4.0 | 3.3 | 3.1 | 4.9 | 3.3 | 3.4 | 4.7 | |
| AREA= | 53.3 | 68.5 | 50.3 | 51.8 | 113.5 | 44.1 | 40.8 | 46.6 | 64.9 | 42.5 | 55.7 | 51.9 | |
| VEL= | 2.9 | 3.2 | 4.3 | 4.4 | 11.3 | 4.6 | 4.1 | 3.4 | 3.9 | 4.0 | 3.1 | 4.6 | |
| DEPTH= | .8 | 1.0 | 1.7 | 1.7 | 3.3 | 1.8 | 1.6 | 1.2 | 1.4 | 1.5 | 1.0 | 1.9 | |

| STA= | 1262. | 1282. | 1301. | 1321. | 1339. | 1356. | 1367. | 1390. | 1422. | 1488. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.5 | 4.0 | 3.5 | 3.5 | 5.1 | 3.3 | 3.7 | 3.9 | 1.2 | |
| AREA= | 44.1 | 40.9 | 38.2 | 36.5 | 45.3 | 29.2 | 41.7 | 48.7 | 28.6 | |
| VEL= | 5.2 | 5.0 | 4.7 | 5.0 | 5.8 | 5.7 | 4.6 | 4.1 | 2.2 | |
| DEPTH= | 2.2 | 2.1 | 1.9 | 2.1 | 2.6 | 2.6 | 1.8 | 1.5 | .4 | |

```
 SECNO     DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
 Q         QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
 TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
 SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


*SECNO  .477
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED
     .477      2.25   2343.25   2343.25       .00   2344.00       .75      6.56       .01   2341.50
   5152.0     542.6     797.4    3812.0      83.7      74.4     642.2      46.8      25.2   2341.40
     .09      6.48     10.72      5.94      .050      .030      .050      .000   2341.00    912.14
  .021967     450.      460.      440.         0        11         0       .00    541.32   1453.45


FLOW DISTRIBUTION FOR SECNO=       .48          CWSEL=   2343.25

STA=     912.     939.     959.     965.    1007.    1022.    1036.    1051.    1066.    1095.    1155.    1202.    1233.
  PER Q=      3.2      5.8      1.5     15.5      3.6      4.1      4.2      3.1      3.5      4.3      4.1      4.4
   AREA=     30.5     41.5     11.7     74.4     27.2     29.4     30.2     25.6     35.6     54.1     47.5     41.6
    VEL=      5.4      7.2      6.6     10.7      6.8      7.1      7.1      6.3      5.0      4.1      4.4      5.4
  DEPTH=      1.1      2.1      1.9      1.8      1.9      2.1      2.1      1.7      1.2       .9      1.0      1.4

STA=    1233.    1248.    1263.    1278.    1315.    1329.    1358.    1402.    1432.    1453.
  PER Q=      3.0      3.5      4.2     12.3      3.8      3.8      4.1      5.4      2.6
   AREA=     25.2     27.5     30.4     84.0     28.1     37.3     46.2     47.0     25.5
    VEL=      6.2      6.6      7.1      7.6      7.0      5.3      4.6      5.9      5.2
  DEPTH=      1.7      1.9      2.1      2.2      2.0      1.3      1.1      1.6      1.2

*SECNO  .578
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      790.0    1450.0  TYPE=      1  TARGET=      660.000
          ENCROACHED TO 1450 DUE TO SMALL RIGHT BANK TRIBUTARY.  FLOODPLAIN
          MAPPED TO WSEL.
     .578      6.29   2351.79   2351.79       .00   2352.72       .93      6.14       .05   2350.00
   5152.0      18.7    2013.5    3119.7       8.0     178.0     776.3      57.2      31.3   2348.80
     .12      2.35     11.31      4.02      .050      .030      .050      .000   2345.50    971.06
  .007428     530.      530.      510.         0        20         0       .00    478.93   1450.00


FLOW DISTRIBUTION FOR SECNO=       .58          CWSEL=   2351.79
```

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 971. | 980. | 1020. | 1040. | 1060. | 1092. | 1112. | 1139. | 1169. | 1200. | 1219. | 1251. | 1281. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .4 | 39.1 | 4.9 | 3.6 | 4.5 | 3.5 | 4.3 | 3.6 | 4.9 | 3.0 | 3.6 | 3.6 | |
| AREA= | 8.0 | 178.0 | 52.2 | 43.2 | 59.4 | 42.7 | 54.3 | 50.5 | 61.8 | 38.2 | 51.7 | 50.0 | |
| VEL= | 2.3 | 11.3 | 4.9 | 4.3 | 3.9 | 4.2 | 4.0 | 3.7 | 4.1 | 4.1 | 3.6 | 3.7 | |
| DEPTH= | .9 | 4.4 | 2.6 | 2.2 | 1.9 | 2.1 | 2.0 | 1.7 | 2.0 | 2.0 | 1.6 | 1.7 | |

| STA= | 1281. | 1300. | 1312. | 1387. | 1421. | 1440. | 1450. |
|---|---|---|---|---|---|---|---|
| PER Q= | 6.5 | 3.3 | 3.4 | 3.7 | 3.0 | 1.0 | |
| AREA= | 60.1 | 33.4 | 69.8 | 54.2 | 38.2 | 16.4 | |
| VEL= | 5.5 | 5.1 | 2.5 | 3.6 | 4.1 | 3.2 | |
| DEPTH= | 3.2 | 2.8 | .9 | 1.6 | 2.0 | 1.6 | |

*SECNO .697
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .697 | 5.34 | 2358.84 | 2358.84 | .00 | 2359.74 | .89 | 4.11 | .00 | 2355.60 |
| 5152.0 | 2041.3 | 2189.9 | 920.8 | 523.5 | 203.2 | 271.3 | 70.8 | 38.1 | 2355.30 |
| .14 | 3.90 | 10.78 | 3.39 | .050 | .030 | .050 | .000 | 2353.50 | 660.61 |
| .006146 | 610. | 630. | 590. | 0 | 9 | 0 | .00 | 519.93 | 1180.54 |

FLOW DISTRIBUTION FOR SECNO= .70 CWSEL= 2358.84

| STA= | 661. | 752. | 830. | 863. | 887. | 898. | 910. | 922. | 945. | 961. | 973. | 1017. | 1043. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.4 | 3.1 | 4.9 | 6.0 | 3.4 | 3.8 | 3.6 | 5.0 | 3.1 | 3.3 | 42.5 | 4.1 | |
| AREA= | 75.9 | 69.8 | 67.4 | 66.0 | 35.9 | 37.9 | 37.1 | 59.1 | 38.2 | 36.2 | 203.2 | 54.5 | |
| VEL= | 2.3 | 2.3 | 3.8 | 4.7 | 4.9 | 5.1 | 4.9 | 4.4 | 4.2 | 4.7 | 10.8 | 3.9 | |
| DEPTH= | .8 | .9 | 2.0 | 2.8 | 3.1 | 3.2 | 3.1 | 2.6 | 2.4 | 2.8 | 4.7 | 2.1 | |

| STA= | 1043. | 1071. | 1100. | 1131. | 1170. | 1181. |
|---|---|---|---|---|---|---|
| PER Q= | 3.6 | 3.6 | 3.3 | 3.1 | .1 | |
| AREA= | 52.9 | 52.9 | 51.7 | 54.9 | 4.4 | |
| VEL= | 3.5 | 3.5 | 3.3 | 2.9 | 1.3 | |
| DEPTH= | 1.8 | 1.8 | 1.7 | 1.4 | .4 | |

*SECNO .788
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .788 | 5.94 | 2364.94 | 2364.94 | .00 | 2366.24 | 1.30 | 2.88 | .12 | 2360.60 |
| 5152.0 | 2328.7 | 2765.2 | 58.0 | 524.8 | 234.2 | 14.6 | 80.4 | 42.4 | 2360.80 |
| .16 | 4.44 | 11.81 | 3.98 | .050 | .030 | .050 | .000 | 2359.00 | 740.28 |
| .006005 | 470. | 480. | 455. | 0 | 8 | 0 | .00 | 283.97 | 1024.25 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .79 CWSEL= 2364.94

| STA= | 740. | 810. | 855. | 900. | 925. | 950. | 959. | 968. | 974. | 1017. | 1024. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.6 | 4.7 | 7.4 | 8.8 | 9.8 | 3.3 | 3.6 | 3.0 | 53.7 | 1.1 | |
| AREA= | 82.7 | 74.9 | 97.4 | 86.0 | 92.2 | 31.7 | 33.5 | 26.4 | 234.2 | 14.6 | |
| VEL= | 2.8 | 3.2 | 3.9 | 5.2 | 5.5 | 5.4 | 5.6 | 5.8 | 11.8 | 4.0 | |
| DEPTH= | 1.2 | 1.7 | 2.2 | 3.4 | 3.7 | 3.6 | 3.8 | 4.1 | 5.4 | 2.1 | |

*SECNO .883

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .883 | 6.16 | 2370.66 | 2370.66 | .00 | 2372.36 | 1.70 | 3.07 | .12 | 2365.30 |
| 5152.0 | 1502.4 | 2880.3 | 769.3 | 245.8 | 222.1 | 138.6 | 88.0 | 45.3 | 2365.00 |
| .17 | 6.11 | 12.97 | 5.55 | .050 | .030 | .050 | .000 | 2364.50 | 849.22 |
| .006587 | 470. | 500. | 500. | 0 | 8 | 0 | .00 | 231.01 | 1168.74 |

DISTRIBUTION FOR SECNO= .88 CWSEL= 2370.66

| STA= | 849. | 949. | 955. | 960. | 966. | 971. | 977. | 982. | 1020. | 1026. | 1032. | 1043. | 1169. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.0 | 3.5 | 3.6 | 3.7 | 3.9 | 4.0 | 3.5 | 55.9 | 4.7 | 4.0 | 4.3 | 1.9 | |
| AREA= | 83.5 | 26.4 | 27.0 | 27.5 | 28.1 | 28.6 | 24.7 | 222.1 | 32.5 | 29.5 | 39.2 | 37.5 | |
| VEL= | 4.3 | 6.8 | 6.9 | 7.0 | 7.1 | 7.2 | 7.3 | 13.0 | 7.4 | 7.0 | 5.7 | 2.6 | |
| DEPTH= | .8 | 4.7 | 4.8 | 4.9 | 5.0 | 5.1 | 5.3 | 5.8 | 5.4 | 4.9 | 3.7 | .3 | |

*SECNO .972
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .972 | 6.04 | 2375.54 | 2375.54 | .00 | 2377.40 | 1.86 | 3.21 | .05 | 2370.30 |
| 5152.0 | 507.2 | 3017.1 | 1627.7 | 85.4 | 224.8 | 275.9 | 94.5 | 47.4 | 2370.30 |
| .18 | 5.94 | 13.42 | 5.90 | .050 | .030 | .050 | .000 | 2369.50 | 959.34 |
| .007093 | 470. | 470. | 470. | 0 | 8 | 0 | .00 | 157.57 | 1116.92 |

FLOW DISTRIBUTION FOR SECNO= .97 CWSEL= 2375.54

| STA= | 959. | 978. | 985. | 988. | 1027. | 1034. | 1040. | 1059. | 1071. | 1100. | 1117. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 4.1 | 2.6 | 58.6 | 4.4 | 3.6 | 10.4 | 6.0 | 6.6 | .5 | |
| AREA= | 35.7 | 31.6 | 18.1 | 224.8 | 31.6 | 27.8 | 81.5 | 48.5 | 73.6 | 13.0 | |
| VEL= | 4.5 | 6.7 | 7.3 | 13.4 | 7.2 | 6.6 | 6.6 | 6.3 | 4.6 | 2.1 | |
| DEPTH= | 2.0 | 4.4 | 5.0 | 5.8 | 4.9 | 4.3 | 4.3 | 4.0 | 2.5 | .8 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.070

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.070 | 6.89 | 2381.89 | 2381.89 | .00 | 2384.10 | 2.21 | 3.49 | .10 | 2376.80 |
| 5152.0 | 362.0 | 3765.9 | 1024.1 | 77.9 | 280.6 | 151.0 | 100.7 | 49.1 | 2376.20 |
| .19 | 4.65 | 13.42 | 6.78 | .050 | .030 | .050 | .000 | 2375.00 | 886.18 |
| .006694 | 540. | 520. | 460. | 0 | 8 | 0 | .00 | 135.24 | 1074.56 |

FLOW DISTRIBUTION FOR SECNO= 1.07 CWSEL= 2381.89

| STA= | 886. | 985. | 990. | 1036. | 1041. | 1045. | 1050. | 1055. | 1064. | 1075. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.2 | 2.8 | 73.1 | 3.7 | 3.5 | 4.2 | 3.5 | 4.2 | .8 | |
| AREA= | 55.4 | 22.5 | 280.6 | 24.8 | 23.6 | 28.2 | 24.3 | 37.0 | 13.1 | |
| VEL= | 3.9 | 6.5 | 13.4 | 7.7 | 7.6 | 7.7 | 7.4 | 5.9 | 3.2 | |
| DEPTH= | .6 | 4.5 | 6.1 | 5.6 | 5.5 | 5.6 | 5.4 | 3.8 | 1.3 | |

O 1.163

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.163 | 5.75 | 2385.75 | 2385.11 | .00 | 2386.99 | 1.25 | 2.80 | .10 | 2380.00 |
| 5152.0 | 2395.1 | 2630.3 | 126.6 | 450.8 | 230.3 | 27.6 | 107.3 | 50.9 | 2380.00 |
| .21 | 5.31 | 11.42 | 4.58 | .050 | .030 | .050 | .000 | 2380.00 | 820.92 |
| .005154 | 445. | 490. | 490. | 2 | 15 | 0 | .00 | 203.77 | 1024.69 |

FLOW DISTRIBUTION FOR SECNO= 1.16 CWSEL= 2385.75

| STA= | 821. | 895. | 911. | 921. | 930. | 940. | 950. | 960. | 968. | 975. | 1015. | 1025. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 6.5 | 7.4 | 4.8 | 5.0 | 5.4 | 5.1 | 4.8 | 3.5 | 4.1 | 51.1 | 2.5 | |
| AREA= | 93.9 | 68.6 | 42.4 | 43.3 | 46.6 | 45.1 | 43.6 | 31.9 | 35.5 | 230.3 | 27.6 | |
| VEL= | 3.5 | 5.6 | 5.8 | 5.9 | 5.9 | 5.8 | 5.7 | 5.6 | 5.9 | 11.4 | 4.6 | |
| DEPTH= | 1.3 | 4.2 | 4.5 | 4.7 | 4.7 | 4.5 | 4.4 | 4.3 | 4.7 | 5.8 | 2.9 | |

*SECNO 1.239

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.239 | 7.38 | 2390.38 | 2390.38 | .00 | 2392.39 | 2.01 | 2.08 | .23 | 2384.50 |
| 5152.0 | 1313.4 | 3492.9 | 345.7 | 258.5 | 261.3 | 66.2 | 113.0 | 52.5 | 2384.00 |
| .22 | 5.08 | 13.37 | 5.23 | .050 | .030 | .050 | .000 | 2383.00 | 873.38 |
| .005507 | 370. | 400. | 410. | 0 | 11 | 0 | .00 | 160.62 | 1033.99 |

FLOW DISTRIBUTION FOR SECNO= 1.24 CWSEL= 2390.38

| STA= | 873. | 880. | 905. | 923. | 930. | 950. | 965. | 970. | 975. | 1012. | 1020. | 1030. | 1034. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .0 | .9 | 1.7 | 1.1 | 6.5 | 8.3 | 3.3 | 3.8 | 67.8 | 4.9 | 1.8 | .1 | |
| AREA= | 1.3 | 22.0 | 28.5 | 16.0 | 67.6 | 69.4 | 25.6 | 28.1 | 261.3 | 40.2 | 23.8 | 2.2 | |
| VEL= | .7 | 2.0 | 3.1 | 3.6 | 4.9 | 6.1 | 6.5 | 7.0 | 13.4 | 6.2 | 3.8 | 1.4 | |
| DEPTH= | .2 | .9 | 1.6 | 2.1 | 3.4 | 4.6 | 5.1 | 5.6 | 7.1 | 5.0 | 2.4 | .5 | |

*SECNO 1.367

HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.367 | 6.42 | 2394.92 | 2394.92 | .00 | 2395.82 | .90 | 3.00 | .11 | 2391.00 |
| 5152.0 | 1054.4 | 2518.5 | 1579.1 | 357.9 | 243.5 | 432.0 | 123.3 | 56.4 | 2391.00 |
| .25 | 2.95 | 10.34 | 3.66 | .050 | .030 | .050 | .000 | 2388.50 | 721.22 |
| .004506 | 390. | 680. | 630. | 0 | 10 | 0 | .00 | 510.25 | 1231.47 |

FLOW DISTRIBUTION FOR SECNO= 1.37 CWSEL= 2394.92

| STA= | 721. | 800. | 845. | 872. | 965. | 978. | 1022. | 1036. | 1062. | 1075. | 1090. | 1112. | 1142. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.5 | 4.5 | 5.4 | 3.1 | 3.0 | 48.9 | 3.9 | 5.0 | 3.4 | 4.0 | 4.4 | 5.1 | |
| AREA= | 93.8 | 79.0 | 72.1 | 75.0 | 38.0 | 243.5 | 45.7 | 67.9 | 41.2 | 47.6 | 58.8 | 72.6 | |
| VEL= | 2.5 | 2.9 | 3.8 | 2.1 | 4.1 | 10.3 | 4.3 | 3.8 | 4.3 | 4.3 | 3.8 | 3.6 | |
| DEPTH= | 1.2 | 1.8 | 2.7 | .8 | 2.9 | 5.5 | 3.2 | 2.6 | 3.2 | 3.2 | 2.7 | 2.4 | |

| STA= | 1142. | 1166. | 1231. |
|---|---|---|---|
| PER Q= | 3.0 | 1.9 | |
| AREA= | 48.5 | 49.6 | |
| VEL= | 3.2 | 2.0 | |
| DEPTH= | 2.0 | .8 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.462

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.462 | 5.93 | 2401.43 | 2401.43 | .00 | 2402.90 | 1.47 | 2.63 | .17 | 2396.90 |
| 5152.0 | 129.6 | 2641.8 | 2380.7 | 26.4 | 210.0 | 453.9 | 132.4 | 60.2 | 2396.90 |
| .26 | 4.91 | 12.58 | 5.24 | .050 | .030 | .050 | .000 | 2395.50 | 981.32 |
| .007107 | 445. | 500. | 440. | 0 | 11 | 0 | .00 | 239.49 | 1220.81 |

FLOW DISTRIBUTION FOR SECNO= 1.46 CWSEL= 2401.43

| STA= | 981. | 993. | 1033. | 1039. | 1046. | 1052. | 1059. | 1066. | 1100. | 1120. | 1139. | 1168. | 1221. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 2.5 | 51.3 | 3.9 | 4.1 | 4.4 | 4.0 | 3.3 | 10.6 | 5.0 | 4.8 | 4.2 | 1.9 | |
| AREA= | 26.4 | 210.0 | 29.2 | 30.0 | 31.5 | 30.3 | 26.9 | 103.9 | 53.7 | 51.0 | 56.0 | 41.5 | |
| VEL= | 4.9 | 12.6 | 6.8 | 7.0 | 7.2 | 6.8 | 6.3 | 5.2 | 4.8 | 4.8 | 3.9 | 2.4 | |
| DEPTH= | 2.3 | 5.3 | 4.5 | 4.7 | 4.8 | 4.5 | 4.0 | 3.0 | 2.7 | 2.7 | 1.9 | .8 | |

O 1.551
MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.551 | 4.92 | 2406.92 | 2406.92 | .00 | 2408.34 | 1.42 | 3.49 | .00 | 2403.00 |
| 5152.0 | 462.2 | 2256.2 | 2433.5 | 78.3 | 177.5 | 398.7 | 138.7 | 62.4 | 2403.00 |
| .27 | 5.90 | 12.71 | 6.10 | .050 | .030 | .050 | .000 | 2402.00 | 955.92 |
| .009472 | 470. | 470. | 380. | 0 | 15 | 0 | .00 | 238.00 | 1193.92 |

FLOW DISTRIBUTION FOR SECNO= 1.55 CWSEL= 2406.92

| STA= | 956. | 977. | 988. | 1029. | 1040. | 1050. | 1060. | 1071. | 1100. | 1130. | 1181. | 1194. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 5.1 | 43.8 | 5.6 | 5.7 | 5.6 | 5.7 | 13.3 | 7.4 | 3.8 | .1 | |
| AREA= | 39.8 | 38.5 | 177.5 | 40.4 | 40.8 | 40.4 | 40.8 | 102.6 | 72.7 | 58.1 | 2.8 | |
| VEL= | 5.0 | 6.8 | 12.7 | 7.2 | 7.2 | 7.2 | 7.2 | 6.7 | 5.2 | 3.4 | 1.0 | |
| DEPTH= | 1.9 | 3.6 | 4.3 | 3.9 | 3.9 | 3.9 | 3.9 | 3.5 | 2.4 | 1.2 | .2 | |

*SECNO 1.646
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.646 | 7.64 | 2412.64 | 2412.64 | .00 | 2414.35 | 1.71 | 3.26 | .09 | 2407.30 |
| 5152.0 | 835.3 | 3631.7 | 685.0 | 201.2 | 297.8 | 154.0 | 146.1 | 65.0 | 2407.30 |
| .29 | 4.15 | 12.19 | 4.45 | .050 | .030 | .050 | .000 | 2405.00 | 877.19 |
| .004914 | 525. | 500. | 460. | 0 | 14 | 0 | .00 | 229.83 | 1107.02 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.65 CWSEL= 2412.64

| STA= | 877. | 952. | 966. | 975. | 980. | 1025. | 1035. | 1045. | 1060. | 1107. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.2 | 4.0 | 4.1 | 2.9 | 70.5 | 5.3 | 3.7 | 3.1 | 1.2 | |
| AREA= | 92.5 | 44.7 | 39.0 | 25.0 | 297.8 | 47.2 | 37.7 | 39.6 | 29.6 | |
| VEL= | 2.9 | 4.6 | 5.5 | 6.0 | 12.2 | 5.8 | 5.0 | 4.0 | 2.1 | |
| DEPTH= | 1.2 | 3.2 | 4.2 | 5.0 | 6.6 | 4.7 | 3.8 | 2.6 | .6 | |

*SECNO 1.718

3301 HV CHANGED MORE THAN HVINS

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH (DOWNSTREAM)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.718 | 6.39 | 2415.39 | 2413.76 | .00 | 2415.86 | .47 | 1.38 | .12 | 2410.00 |
| 5152.0 | 3017.5 | 1204.7 | 929.8 | 715.6 | 141.4 | 240.4 | 153.7 | 67.3 | 2410.00 |
| .31 | 4.22 | 8.52 | 3.87 | .050 | .030 | .050 | .000 | 2409.00 | 808.39 |
| .002796 | 380. | 380. | 380. | 2 | 14 | 0 | .00 | 278.19 | 1086.58 |

FLOW DISTRIBUTION FOR SECNO= 1.72 CWSEL= 2415.39

| STA= | 808. | 855. | 872. | 893. | 913. | 930. | 940. | 950. | 960. | 969. | 979. | 990. | 1014. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 6.1 | 9.6 | 8.1 | 7.3 | 4.6 | 3.9 | 3.5 | 3.4 | 3.5 | 4.7 | 23.4 | |
| AREA= | 79.0 | 74.6 | 105.4 | 95.1 | 83.1 | 51.1 | 46.1 | 42.6 | 42.1 | 42.6 | 53.8 | 141.4 | |
| VEL= | 2.5 | 4.2 | 4.7 | 4.4 | 4.5 | 4.7 | 4.4 | 4.2 | 4.2 | 4.2 | 4.5 | 8.5 | |
| DEPTH= | 1.7 | 4.4 | 5.1 | 4.6 | 4.9 | 5.1 | 4.6 | 4.4 | 4.4 | 4.4 | 4.9 | 5.9 | |

| STA= | 1014. | 1023. | 1032. | 1041. | 1055. | 1075. | 1087. |
|---|---|---|---|---|---|---|---|
| PER Q= | 4.2 | 3.5 | 3.1 | 4.0 | 3.1 | .2 | |
| AREA= | 46.0 | 41.5 | 39.2 | 53.3 | 52.2 | 8.0 | |
| VEL= | 4.7 | 4.4 | 4.1 | 3.8 | 3.1 | 1.2 | |
| DEPTH= | 5.1 | 4.6 | 4.2 | 3.8 | 2.7 | .7 | |

*SECNO 1.808
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 780.0 1200.0 TYPE= 1 TARGET= 420.000

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH (UPSTREAM)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.808 | 3.33 | 2420.33 | 2420.33 | .00 | 2420.98 | .65 | 1.79 | .05 | 2418.00 |
| 2085.0 | 764.2 | 690.8 | 630.0 | 211.5 | 70.8 | 148.6 | 162.2 | 70.6 | 2418.00 |
| .33 | 3.61 | 9.75 | 4.24 | .050 | .030 | .050 | .000 | 2417.00 | 780.00 |
| .009703 | 490. | 475. | 465. | 0 | 11 | 0 | .00 | 328.34 | 1108.34 |

FLOW DISTRIBUTION FOR SECNO= 1.81 CWSEL= 2420.33

| STA= | 780. | 845. | 860. | 870. | 880. | 890. | 915. | 965. | 980. | 990. | 1015. | 1025. | 1035. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.6 | 4.8 | 5.0 | 5.0 | 3.3 | 3.1 | 3.3 | 4.0 | 4.7 | 33.1 | 5.0 | 3.5 | |
| AREA= | 33.5 | 24.5 | 21.3 | 21.3 | 16.6 | 22.1 | 29.4 | 22.0 | 20.6 | 70.8 | 21.3 | 17.3 | |
| VEL= | 2.2 | 4.1 | 4.9 | 4.9 | 4.1 | 2.9 | 2.3 | 3.8 | 4.7 | 9.7 | 4.9 | 4.2 | |
| DEPTH= | .5 | 1.6 | 2.1 | 2.1 | 1.7 | .9 | .6 | 1.5 | 2.1 | 2.8 | 2.1 | 1.7 | |

| STA= | 1035. | 1050. | 1061. | 1071. | 1088. | 1108. |
|---|---|---|---|---|---|---|
| PER Q= | 4.2 | 4.0 | 5.2 | 6.6 | 1.8 | |
| AREA= | 22.7 | 19.1 | 22.2 | 31.2 | 14.7 | |
| VEL= | 3.8 | 4.4 | 4.9 | 4.4 | 2.5 | |
| DEPTH= | 1.5 | 1.8 | 2.2 | 1.8 | .7 | |

*SECNO 1.905
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

YUCCA FLATS WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.905 | 3.82 | 2425.82 | 2425.82 | .00 | 2426.60 | .77 | 4.56 | .04 | 2423.00 |
| 2085.0 | 230.3 | 838.0 | 1016.8 | 55.6 | 83.1 | 266.8 | 167.0 | 73.9 | 2423.00 |
| .35 | 4.14 | 10.09 | 3.81 | .050 | .030 | .050 | .000 | 2422.00 | 952.23 |
| .008407 | 510. | 510. | 500. | 0 | 11 | 0 | .00 | 244.84 | 1197.06 |

FLOW DISTRIBUTION FOR SECNO= 1.90 CWSEL= 2425.82

| STA= | 952. | 975. | 985. | 990. | 1015. | 1024. | 1055. | 1080. | 1089. | 1098. | 1103. | 1120. | 1138. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.0 | 4.7 | 3.4 | 40.2 | 4.4 | 3.2 | 4.2 | 3.9 | 5.3 | 3.2 | 9.0 | 4.9 | |
| AREA= | 20.7 | 21.5 | 13.4 | 83.1 | 20.0 | 26.6 | 28.3 | 18.6 | 22.3 | 12.5 | 39.5 | 27.5 | |
| VEL= | 3.0 | 4.5 | 5.2 | 10.1 | 4.6 | 2.5 | 3.1 | 4.4 | 4.9 | 5.3 | 4.8 | 3.7 | |
| DEPTH= | .9 | 2.1 | 2.7 | 3.3 | 2.2 | .9 | 1.1 | 2.0 | 2.4 | 2.7 | 2.3 | 1.6 | |

| STA= | 1138. | 1173. | 1190. | 1197. |
|---|---|---|---|---|
| PER Q= | 5.1 | 4.9 | .8 | |
| AREA= | 37.5 | 27.5 | 6.4 | |
| VEL= | 2.9 | 3.7 | 2.5 | |
| DEPTH= | 1.1 | 1.6 | .9 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.003
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.003 | 3.76 | 2432.76 | 2432.76 | .00 | 2433.43 | .67 | 3.98 | .01 | 2430.00 |
| 2085.0 | 1096.8 | 878.2 | 110.1 | 338.2 | 94.1 | 30.8 | 172.0 | 77.3 | 2430.00 |
| .38 | 3.24 | 9.33 | 3.57 | .050 | .030 | .050 | .000 | 2429.00 | 701.95 |
| .007416 | 530. | 520. | 450. | 0 | 5 | 0 | .00 | 334.08 | 1036.03 |

FLOW DISTRIBUTION FOR SECNO= 2.00 CWSEL= 2432.76

| STA= | 702. | 768. | 790. | 813. | 835. | 853. | 888. | 923. | 943. | 957. | 967. | 976. | 981. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.0 | 5.5 | 7.1 | 7.1 | 4.4 | 3.5 | 3.4 | 3.5 | 3.6 | 3.1 | 4.5 | 2.9 | |
| AREA= | 39.2 | 34.0 | 39.6 | 39.6 | 27.2 | 30.8 | 30.4 | 24.5 | 22.2 | 17.2 | 21.3 | 12.3 | |
| VEL= | 2.1 | 3.4 | 3.7 | 3.7 | 3.4 | 2.4 | 2.3 | 3.0 | 3.4 | 3.8 | 4.4 | 4.8 | |
| DEPTH= | .6 | 1.5 | 1.8 | 1.8 | 1.5 | .9 | .8 | 1.3 | 1.5 | 1.8 | 2.2 | 2.6 | |

| STA= | 981. | 1010. | 1020. | 1036. |
|---|---|---|---|---|
| PER Q= | 42.1 | 4.2 | 1.1 | |
| AREA= | 94.1 | 20.9 | 10.0 | |
| VEL= | 9.3 | 4.2 | 2.2 | |
| DEPTH= | 3.2 | 2.1 | .6 | |

*SECNO 2.091

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.091 | 3.00 | 2437.00 | 2437.00 | .00 | 2437.64 | .64 | 2.90 | .00 | 2434.00 |
| 2085.0 | 1078.6 | 826.6 | 179.7 | 314.3 | 89.9 | 42.9 | 175.6 | 79.8 | 2434.00 |
| .39 | 3.43 | 9.20 | 4.19 | .050 | .030 | .050 | .000 | 2434.00 | 669.29 |
| .007978 | 300. | 460. | 460. | 0 | 15 | 0 | .00 | 356.06 | 1025.98 |

FLOW DISTRIBUTION FOR SECNO= 2.09 CWSEL= 2437.00

| STA= | 669. | 710. | 741. | 837. | 880. | 900. | 957. | 966. | 970. | 1000. | 1005. | 1015. | 1026. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 12.9 | 12.5 | 3.6 | 8.0 | 5.0 | 3.1 | 3.6 | 3.1 | 39.6 | 3.4 | 4.1 | 1.2 | |
| AREA= | 66.7 | 61.9 | 41.1 | 52.9 | 29.9 | 31.4 | 18.0 | 12.4 | 89.9 | 13.7 | 20.0 | 9.2 | |
| VEL= | 4.0 | 4.2 | 1.8 | 3.2 | 3.5 | 2.1 | 4.2 | 5.2 | 9.2 | 5.2 | 4.2 | 2.6 | |
| DEPTH= | 1.6 | 2.0 | .4 | 1.2 | 1.5 | .6 | 2.0 | 2.7 | 3.0 | 2.7 | 2.0 | .8 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.172
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.172 | 4.03 | 2442.03 | 2442.03 | .00 | 2442.72 | .69 | 3.17 | .02 | 2439.00 |
| 2085.0 | 1066.6 | 716.5 | 301.9 | 300.8 | 70.6 | 71.2 | 179.6 | 82.8 | 2439.00 |
| .41 | 3.55 | 10.15 | 4.24 | .050 | .030 | .050 | .000 | 2438.00 | 740.29 |
| .007869 | 370. | 430. | 440. | 0 | 14 | 0 | .00 | 310.00 | 1050.29 |

FLOW DISTRIBUTION FOR SECNO= 2.17 CWSEL= 2442.03

| STA= | 740. | 792. | 806. | 821. | 835. | 848. | 920. | 970. | 990. | 1010. | 1030. | 1050. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.8 | 5.9 | 5.9 | 5.9 | 4.0 | 3.2 | 6.6 | 11.9 | 34.4 | 11.9 | 2.6 | |
| AREA= | 53.3 | 29.0 | 29.2 | 29.0 | 22.3 | 35.9 | 51.5 | 50.6 | 70.6 | 50.6 | 20.6 | |
| VEL= | 3.0 | 4.2 | 4.2 | 4.2 | 3.7 | 1.9 | 2.7 | 4.9 | 10.2 | 4.9 | 2.7 | |
| DEPTH= | 1.0 | 2.0 | 2.0 | 2.0 | 1.7 | .5 | 1.0 | 2.5 | 3.5 | 2.5 | 1.0 | |

*SECNO 2.284
7185 MINIMUM SPECIFIC ENERGY
[illegible] CRITICAL DEPTH ASSUMED

[illegible] ENCROACHMENT STATIONS= 723.7 1208.0 TYPE= 1 TARGET= 484.300
ENCROACHED TO 1208 DUE TO SMALL RIGHT BANK TRIBUTARY. FLOODPLAIN
MAPPED TO WSEL.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.284 | 3.57 | 2450.57 | 2450.57 | .00 | 2451.34 | .77 | 4.25 | .02 | 2447.50 |
| 2085.0 | 184.7 | 926.3 | 974.1 | 44.3 | 95.0 | 275.7 | 185.0 | 86.3 | 2447.50 |
| .44 | 4.17 | 9.75 | 3.53 | .050 | .030 | .050 | .000 | 2447.00 | 952.01 |
| .007424 | 530. | 590. | 540. | 0 | 15 | 0 | .00 | 255.99 | 1208.00 |

FLOW DISTRIBUTION FOR SECNO= 2.28 CWSEL= 2450.57

| STA= | 952. | 970. | 978. | 1005. | 1010. | 1026. | 1040. | 1060. | 1073. | 1085. | 1117. | 1148. | 1208. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 5.2 | 44.4 | 3.4 | 6.6 | 3.6 | 8.2 | 6.2 | 4.2 | 7.0 | 4.3 | 3.1 | |
| AREA= | 23.1 | 21.1 | 95.0 | 14.1 | 33.1 | 22.0 | 41.4 | 29.0 | 22.7 | 45.0 | 33.8 | 34.6 | |
| VEL= | 3.3 | 5.1 | 9.7 | 5.1 | 4.2 | 3.5 | 4.2 | 4.5 | 3.8 | 3.2 | 2.7 | 1.8 | |
| DEPTH= | 1.3 | 2.8 | 3.5 | 2.8 | 2.1 | 1.6 | 2.1 | 2.3 | 1.8 | 1.4 | 1.1 | .6 | |

*SECNO 2.384
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
|---|---|---|---|---|---|---|---|---|---|
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| 2.384 | 3.65 | 2456.65 | 2456.65 | .00 | 2457.45 | .80 | 4.05 | .01 | 2453.00 |
| 2085.0 | 797.6 | 741.1 | 546.3 | 202.0 | 69.4 | 128.9 | 189.8 | 89.1 | 2453.00 |
| .46 | 3.95 | 10.69 | 4.24 | .050 | .030 | .050 | .000 | 2453.00 | 859.96 |
| .008277 | 490. | 530. | 520. | 0 | 8 | 0 | .00 | 233.06 | 1093.01 |

FLOW DISTRIBUTION FOR SECNO= 2.38 CWSEL= 2456.65

| STA= | 860. | 894. | 922. | 944. | 965. | 980. | 990. | 1009. | 1020. | 1041. | 1061. | 1093. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 6.5 | 6.4 | 6.4 | 7.0 | 8.8 | 35.5 | 9.6 | 9.8 | 4.4 | 2.4 | |
| AREA= | 27.3 | 39.9 | 35.5 | 35.5 | 32.3 | 31.5 | 69.4 | 34.7 | 45.2 | 27.3 | 21.8 | |
| VEL= | 2.4 | 3.4 | 3.8 | 3.8 | 4.5 | 5.8 | 10.7 | 5.8 | 4.5 | 3.4 | 2.3 | |
| DEPTH= | .8 | 1.4 | 1.7 | 1.7 | 2.2 | 3.2 | 3.7 | 3.2 | 2.2 | 1.4 | .7 | |

*SECNO 2.477

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.477 | 5.33 | 2462.33 | 2462.33 | .00 | 2463.10 | .78 | 2.80 | .00 | 2458.00 |
| 2085.0 | 409.4 | 1082.8 | 592.7 | 108.6 | 115.9 | 235.4 | 194.4 | 92.1 | 2458.00 |
| .48 | 3.77 | 9.34 | 2.52 | .050 | .030 | .050 | .000 | 2457.00 | 936.05 |
| .004379 | 510. | 490. | 420. | 0 | 11 | 0 | .00 | 326.36 | 1332.96 |

FLOW DISTRIBUTION FOR SECNO= 2.48 CWSEL= 2462.33

| STA= | 936. | 965. | 975. | 981. | 986. | 991. | 1015. | 1020. | 1025. | 1035. | 1050. | 1076. | 1253. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 4.0 | 3.2 | 4.2 | 5.1 | 51.9 | 4.7 | 3.5 | 4.1 | 3.4 | 3.1 | 3.1 | |
| AREA= | 28.4 | 23.9 | 16.0 | 19.0 | 21.2 | 115.9 | 19.9 | 16.6 | 24.3 | 25.2 | 29.5 | 47.6 | |
| VEL= | 2.3 | 3.5 | 4.2 | 4.6 | 5.0 | 9.3 | 4.9 | 4.4 | 3.6 | 2.8 | 2.2 | 1.3 | |
| DEPTH= | 1.0 | 2.4 | 3.1 | 3.6 | 4.1 | 4.8 | 4.0 | 3.3 | 2.4 | 1.7 | 1.1 | .3 | |

| STA= | 1253. | 1300. | 1333. |
|---|---|---|---|
| PER Q= | 4.5 | 2.1 | |
| AREA= | 46.9 | 25.4 | |
| VEL= | 2.0 | 1.7 | |
| DEPTH= | 1.0 | .8 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.562

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.562 | 2.37 | 2467.37 | 2467.37 | .00 | 2468.14 | .77 | 3.22 | .00 | 2465.00 |
| 2085.0 | 659.7 | 611.4 | 813.9 | 124.7 | 59.4 | 166.2 | 198.6 | 95.0 | 2465.00 |
| .50 | 5.29 | 10.30 | 4.90 | .050 | .030 | .050 | .000 | 2465.00 | 912.82 |
| .013647 | 420. | 450. | 475. | 0 | 14 | 0 | .00 | 229.89 | 1190.38 |

FLOW DISTRIBUTION FOR SECNO= 2.56 CWSEL= 2467.37

| STA= | 913. | 941. | 953. | 964. | 975. | 988. | 1013. | 1025. | 1035. | 1045. | 1055. | 1135. | 1145. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.3 | 4.6 | 5.8 | 7.1 | 8.8 | 29.3 | 8.8 | 6.3 | 4.7 | 3.4 | 3.1 | 4.8 | |
| AREA= | 28.5 | 19.3 | 22.3 | 24.9 | 29.7 | 59.4 | 29.7 | 22.2 | 18.7 | 15.2 | 21.5 | 18.7 | |
| VEL= | 3.9 | 5.0 | 5.5 | 5.9 | 6.2 | 10.3 | 6.2 | 5.9 | 5.3 | 4.6 | 3.0 | 5.3 | |
| DEPTH= | 1.0 | 1.7 | 2.0 | 2.2 | 2.4 | 2.4 | 2.4 | 2.2 | 1.9 | 1.5 | .3 | 1.9 | |

| | 1145. | 1155. | 1182. | 1190. |
|---|---|---|---|---|
| Q= | 4.8 | 3.1 | .0 | |
| AREA= | 18.7 | 20.3 | 1.0 | |
| VEL= | 5.3 | 3.2 | 1.0 | |
| DEPTH= | 1.9 | .8 | .1 | |

*SECNO 2.672
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.672 | 3.33 | 2475.33 | 2475.33 | .00 | 2476.15 | .82 | 7.09 | .02 | 2473.00 |
| 2085.0 | 1152.6 | 736.7 | 195.6 | 240.4 | 70.9 | 45.2 | 203.3 | 98.0 | 2473.00 |
| .52 | 4.80 | 10.40 | 4.33 | .050 | .030 | .050 | .000 | 2472.00 | 823.44 |
| .011027 | 610. | 580. | 525. | 0 | 14 | 0 | .00 | 220.24 | 1043.68 |

FLOW DISTRIBUTION FOR SECNO= 2.67 CWSEL= 2475.33

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 823. | 879. | 900. | 910. | 922. | 931. | 939. | 952. | 970. | 986. | 1011. | 1021. | 1031. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.7 | 5.5 | 5.1 | 10.2 | 8.3 | 6.2 | 5.3 | 4.4 | 6.6 | 35.3 | 5.1 | 3.2 | |
| AREA= | 30.7 | 29.3 | 20.8 | 34.0 | 26.2 | 22.0 | 23.9 | 24.0 | 29.4 | 70.9 | 20.8 | 15.8 | |
| VEL= | 2.5 | 3.9 | 5.1 | 6.2 | 6.6 | 5.9 | 4.7 | 3.8 | 4.7 | 10.4 | 5.1 | 4.2 | |
| DEPTH= | .6 | 1.4 | 2.1 | 2.8 | 3.1 | 2.6 | 1.8 | 1.3 | 1.8 | 2.8 | 2.1 | 1.6 | |

| STA= | 1031. | 1044. |
|---|---|---|
| PER Q= | 1.1 | |
| AREA= | 8.5 | |
| VEL= | 2.6 | |
| DEPTH= | .7 | |

*SECNO 2.761

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.761 | 2.33 | 2480.33 | 2480.27 | .00 | 2480.94 | .61 | 4.77 | .02 | 2478.10 |
| 2085.0 | 1088.7 | 667.5 | 328.8 | 248.1 | 72.8 | 82.3 | 206.9 | 100.3 | 2478.20 |
| .54 | 4.39 | 9.16 | 3.99 | .050 | .030 | .050 | .000 | 2478.00 | 797.94 |
| .011526 | 385. | 470. | 460. | 2 | 19 | 0 | .00 | 279.54 | 1077.48 |

FLOW DISTRIBUTION FOR SECNO= 2.76 CWSEL= 2480.33

| STA= | 798. | 845. | 865. | 878. | 891. | 904. | 916. | 936. | 942. | 955. | 961. | 968. | 974. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.5 | 3.4 | 3.2 | 3.7 | 4.5 | 5.3 | 8.7 | 3.1 | 6.4 | 3.3 | 3.5 | 3.6 | |
| AREA= | 29.6 | 21.0 | 17.3 | 18.8 | 21.1 | 23.3 | 37.0 | 12.7 | 26.2 | 13.3 | 13.9 | 14.0 | |
| VEL= | 2.5 | 3.4 | 3.9 | 4.1 | 4.4 | 4.7 | 4.9 | 5.0 | 5.1 | 5.2 | 5.3 | 5.4 | |
| DEPTH= | .6 | 1.1 | 1.3 | 1.5 | 1.6 | 1.8 | 1.9 | 2.0 | 2.0 | 2.1 | 2.1 | 2.2 | |

| STA= | 974. | 1007. | 1013. | 1026. | 1039. | 1065. | 1077. |
|---|---|---|---|---|---|---|---|
| PER Q= | 32.0 | 3.3 | 5.1 | 3.7 | 3.4 | .3 | |
| AREA= | 72.8 | 13.4 | 23.0 | 18.8 | 23.4 | 3.8 | |
| VEL= | 9.2 | 5.1 | 4.6 | 4.1 | 3.0 | 1.6 | |
| DEPTH= | 2.3 | 2.0 | 1.8 | 1.4 | .9 | .3 | |

*SECNO 2.857
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.857 | 2.22 | 2488.22 | 2488.22 | .00 | 2488.77 | .55 | 5.83 | .01 | 2486.00 |
| 2085.0 | 114.3 | 620.5 | 1350.1 | 30.7 | 66.6 | 360.3 | 211.7 | 103.9 | 2486.00 |
| .57 | 3.72 | 9.32 | 3.75 | .050 | .030 | .050 | .000 | 2486.00 | 957.80 |
| .012218 | 480. | 510. | 485. | 0 | 11 | 0 | .00 | 355.50 | 1313.30 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 2.86 CWSEL= 2488.22

| STA= | 958. | 985. | 1015. | 1310. | 1313. |
|---|---|---|---|---|---|
| PER Q= | 5.5 | 29.8 | 64.7 | .0 | |
| AREA= | 30.7 | 66.6 | 359.9 | .4 | |
| VEL= | 3.7 | 9.3 | 3.8 | .8 | |
| DEPTH= | 1.1 | 2.2 | 1.2 | .1 | |

*SECNO 2.965
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.965 | 1.72 | 2496.72 | 2496.72 | .00 | 2497.28 | .56 | 6.28 | .00 | 2495.00 |
| 2085.0 | 306.7 | 486.8 | 1291.5 | 69.5 | 51.5 | 287.2 | 215.7 | 107.0 | 2495.00 |
| .59 | 4.41 | 9.45 | 4.50 | .050 | .030 | .050 | .000 | 2495.00 | 922.83 |
| .017720 | 570. | 570. | 350. | 0 | 15 | 0 | .00 | 330.75 | 1253.58 |

FLOW DISTRIBUTION FOR SECNO= 2.96 CWSEL= 2496.72

| STA= | 923. | 930. | 985. | 1015. | 1250. | 1254. |
|---|---|---|---|---|---|---|
| PER Q= | .2 | 14.5 | 23.3 | 61.8 | .1 | |
| AREA= | 2.6 | 66.9 | 51.5 | 285.9 | 1.3 | |
| VEL= | 2.0 | 4.5 | 9.5 | 4.5 | 2.0 | |
| DEPTH= | .4 | 1.2 | 1.7 | 1.2 | .4 | |

*SECNO -1.718
START TRIB COMP
-1.718 1.718 2415.390

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| -1.718 | 6.39 | 2415.39 | .00 | .00 | 2415.86 | .47 | 1.56 | 4.73 | 2410.00 |
| 5152.0 | 3017.5 | 1204.6 | 929.8 | 715.7 | 141.4 | 240.4 | 222.3 | 109.7 | 2410.00 |
| .61 | 4.22 | 8.52 | 3.87 | .050 | .030 | .050 | .000 | 2409.00 | 808.38 |
| .002795 | 380. | 380. | 380. | 0 | 0 | 0 | .00 | 278.20 | 1086.59 |

FLOW DISTRIBUTION FOR SECNO= -1.72 CWSEL= 2415.39

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 808. | 855. | 872. | 893. | 913. | 930. | 940. | 950. | 960. | 969. | 979. | 990. | 1014. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 6.1 | 9.6 | 8.1 | 7.3 | 4.6 | 3.9 | 3.5 | 3.4 | 3.5 | 4.7 | 23.4 | |
| AREA= | 79.0 | 74.6 | 105.4 | 95.1 | 83.1 | 51.2 | 46.2 | 42.6 | 42.1 | 42.6 | 53.8 | 141.4 | |
| VEL= | 2.5 | 4.2 | 4.7 | 4.4 | 4.5 | 4.7 | 4.4 | 4.2 | 4.2 | 4.2 | 4.5 | 8.5 | |
| DEPTH= | 1.7 | 4.4 | 5.1 | 4.6 | 4.9 | 5.1 | 4.6 | 4.4 | 4.4 | 4.4 | 4.9 | 5.9 | |

| STA= | 1014. | 1023. | 1032. | 1041. | 1055. | 1075. | 1087. |
|---|---|---|---|---|---|---|---|
| PER Q= | 4.2 | 3.5 | 3.1 | 4.0 | 3.1 | .2 | |
| AREA= | 46.0 | 41.5 | 39.2 | 53.3 | 52.3 | 8.1 | |
| VEL= | 4.7 | 4.4 | 4.1 | 3.8 | 3.1 | 1.2 | |
| DEPTH= | 5.1 | 4.6 | 4.2 | 3.8 | 2.7 | .7 | |

*SECNO .098
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .098 | 3.78 | 2418.78 | 2418.78 | .00 | 2419.60 | .83 | 1.85 | .11 | 2417.00 |
| 2099.0 | 185.4 | 991.7 | 921.9 | 58.4 | 104.8 | 192.8 | 230.2 | 112.5 | 2415.00 |
| .63 | 3.17 | 9.46 | 4.78 | .050 | .030 | .050 | .000 | 2415.00 | 911.24 |
| .009781 | 410. | 520. | 565. | 0 | 14 | 0 | .00 | 233.52 | 1144.76 |

FLOW DISTRIBUTION FOR SECNO= .10 CWSEL= 2418.78

| STA= | 911. | 933. | 955. | 977. | 1016. | 1037. | 1057. | 1076. | 1091. | 1107. | 1127. | 1145. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .4 | 2.5 | 6.0 | 47.2 | 21.2 | 10.8 | 4.1 | 3.2 | 3.4 | 1.1 | .2 | |
| AREA= | 6.2 | 19.5 | 32.8 | 104.8 | 68.8 | 44.4 | 24.9 | 19.2 | 20.4 | 11.8 | 3.3 | |
| VEL= | 1.3 | 2.7 | 3.8 | 9.5 | 6.5 | 5.1 | 3.5 | 3.5 | 3.5 | 2.0 | 1.0 | |
| DEPTH= | .3 | .9 | 1.5 | 2.7 | 3.3 | 2.3 | 1.3 | 1.3 | 1.3 | .6 | .2 | |

*SECNO .190
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .190 | 5.87 | 2423.87 | 2423.87 | .00 | 2424.71 | .84 | 2.98 | .00 | 2419.50 |
| 2099.0 | 619.2 | 1118.4 | 361.5 | 217.0 | 115.3 | 118.4 | 234.6 | 115.2 | 2419.50 |
| .65 | 2.85 | 9.70 | 3.05 | .050 | .030 | .050 | .000 | 2418.00 | 823.23 |
| .004401 | 510. | 490. | 420. | 0 | 11 | 0 | .00 | 263.92 | 1087.15 |

FLOW DISTRIBUTION FOR SECNO= .19 CWSEL= 2423.87

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

| STA= | 823. | 871. | 890. | 931. | 955. | 970. | 980. | 985. | 1008. | 1016. | 1026. | 1041. | 1067. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.6 | 3.0 | 3.1 | 3.2 | 4.1 | 6.5 | 5.0 | 53.3 | 6.3 | 3.5 | 3.2 | 3.4 | |
| AREA= | 44.7 | 26.1 | 35.8 | 29.7 | 28.1 | 32.0 | 20.6 | 115.3 | 28.9 | 22.4 | 24.8 | 31.2 | |
| VEL= | 2.2 | 2.4 | 1.8 | 2.3 | 3.1 | 4.3 | 5.1 | 9.7 | 4.6 | 3.3 | 2.7 | 2.3 | |
| DEPTH= | .9 | 1.4 | .9 | 1.2 | 1.9 | 3.2 | 4.1 | 5.1 | 3.6 | 2.1 | 1.6 | 1.2 | |

| STA= | 1067. | 1087. |
|---|---|---|
| PER Q= | .8 | |
| AREA= | 11.2 | |
| VEL= | 1.5 | |
| DEPTH= | .6 | |

*SECNO .301
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 850.0 1425.0 TYPE= 1 TARGET= 575.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .301 | 4.28 | 2431.28 | 2431.28 | .00 | 2431.98 | .70 | 2.98 | .01 | 2428.00 |
| 2099.0 | 559.8 | 821.5 | 717.7 | 167.3 | 83.1 | 206.8 | 240.2 | 118.5 | 2428.00 |
| .68 | 3.35 | 9.89 | 3.47 | .050 | .030 | .050 | .000 | 2427.00 | 850.00 |
| 06814 | 450. | 580. | 610. | 0 | 13 | 0 | .00 | 294.80 | 1144.80 |

FLOW DISTRIBUTION FOR SECNO= .30 CWSEL= 2431.28

| STA= | 850. | 917. | 937. | 951. | 961. | 970. | 981. | 987. | 1009. | 1015. | 1021. | 1031. | 1041. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.5 | 3.1 | 3.4 | 3.1 | 3.8 | 5.4 | 4.4 | 39.1 | 4.4 | 3.3 | 4.2 | 3.6 | |
| AREA= | 40.4 | 23.6 | 21.8 | 17.8 | 19.7 | 25.8 | 18.2 | 83.1 | 18.2 | 15.2 | 21.3 | 19.4 | |
| VEL= | 1.8 | 2.7 | 3.3 | 3.7 | 4.0 | 4.4 | 5.1 | 9.9 | 5.1 | 4.5 | 4.1 | 3.9 | |
| DEPTH= | .6 | 1.2 | 1.5 | 1.9 | 2.1 | 2.4 | 3.0 | 3.8 | 3.0 | 2.5 | 2.2 | 2.0 | |

| STA= | 1041. | 1055. | 1075. | 1095. | 1115. | 1135. | 1145. |
|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 3.7 | 3.5 | 3.5 | 3.5 | .6 | |
| AREA= | 24.0 | 26.3 | 25.5 | 25.5 | 25.5 | 6.0 | |
| VEL= | 3.4 | 3.0 | 2.9 | 2.9 | 2.9 | 2.0 | |
| DEPTH= | 1.6 | 1.3 | 1.3 | 1.3 | 1.3 | .6 | |

*SECNO .384

3301 HV CHANGED MORE THAN HVINS

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| .384 | 5.00 | 2434.00 | 2433.96 | .00 | 2435.25 | 1.25 | 3.11 | .16 | 2430.00 |
| 2099.0 | 456.5 | 1089.1 | 553.5 | 92.7 | 94.5 | 112.7 | 244.0 | 120.6 | 2430.00 |
| .69 | 4.92 | 11.52 | 4.91 | .050 | .030 | .050 | .000 | 2429.00 | 947.49 |
| .007321 | 440. | 440. | 440. | 2 | 11 | 0 | .00 | 116.60 | 1064.09 |

FLOW DISTRIBUTION FOR SECNO= .38 CWSEL= 2434.00

| STA= | 947. | 970. | 980. | 985. | 990. | 1011. | 1016. | 1021. | 1026. | 1031. | 1041. | 1056. | 1064. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.7 | 6.7 | 4.7 | 5.6 | 51.9 | 5.7 | 4.9 | 4.1 | 3.5 | 5.0 | 3.0 | .2 | |
| AREA= | 28.7 | 28.0 | 17.0 | 19.0 | 94.5 | 19.3 | 17.5 | 15.8 | 14.3 | 23.3 | 19.7 | 3.0 | |
| VEL= | 3.5 | 5.1 | 5.7 | 6.2 | 11.5 | 6.2 | 5.9 | 5.5 | 5.1 | 4.5 | 3.2 | 1.4 | |
| DEPTH= | 1.3 | 2.8 | 3.4 | 3.8 | 4.5 | 3.9 | 3.5 | 3.2 | 2.9 | 2.3 | 1.4 | .3 | |

*SECNO .473
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .473 | 3.65 | 2440.65 | 2440.65 | .00 | 2441.47 | .81 | 3.99 | .04 | 2438.00 |
| 2099.0 | 1111.8 | 861.7 | 125.5 | 264.1 | 85.2 | 30.3 | 247.9 | 122.7 | 2438.00 |
| .71 | 4.21 | 10.12 | 4.14 | .050 | .030 | .050 | .000 | 2437.00 | 798.27 |
| 09057 | 550. | 470. | 420. | 0 | 19 | 0 | .00 | 233.36 | 1031.63 |

FLOW DISTRIBUTION FOR SECNO= .47 CWSEL= 2440.65

| STA= | 798. | 866. | 910. | 920. | 930. | 941. | 951. | 956. | 961. | 966. | 971. | 975. | 980. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 7.7 | 3.5 | 4.2 | 4.9 | 5.7 | 3.2 | 3.4 | 3.3 | 3.3 | 3.3 | 3.3 | |
| AREA= | 39.8 | 50.8 | 17.9 | 19.9 | 22.0 | 24.0 | 12.8 | 13.3 | 12.7 | 12.7 | 12.7 | 12.7 | |
| VEL= | 2.0 | 3.2 | 4.1 | 4.4 | 4.7 | 5.0 | 5.2 | 5.4 | 5.4 | 5.4 | 5.4 | 5.4 | |
| DEPTH= | .6 | 1.2 | 1.8 | 2.0 | 2.2 | 2.4 | 2.5 | 2.6 | 2.7 | 2.7 | 2.7 | 2.7 | |

| STA= | 980. | 985. | 1012. | 1021. | 1032. |
|---|---|---|---|---|---|
| PER Q= | 3.3 | 41.1 | 4.4 | 1.6 | |
| AREA= | 12.7 | 85.2 | 19.4 | 10.9 | |
| VEL= | 5.4 | 10.1 | 4.7 | 3.1 | |
| DEPTH= | 2.7 | 3.2 | 2.2 | 1.0 | |

*SECNO .581
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .581 | 5.41 | 2448.41 | 2448.41 | .00 | 2449.07 | .66 | 2.79 | .01 | 2444.00 |
| 2099.0 | 410.2 | 921.8 | 767.0 | 153.6 | 98.2 | 282.3 | 252.4 | 125.4 | 2444.00 |
| .74 | 2.67 | 9.39 | 2.72 | .050 | .030 | .050 | .000 | 2443.00 | 861.30 |
| .004336 | 270. | 570. | 570. | 0 | 11 | 0 | .00 | 351.96 | 1213.26 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .58 CWSEL= 2448.41

| STA= | 861. | 961. | 975. | 985. | 990. | 1010. | 1016. | 1021. | 1030. | 1044. | 1073. | 1097. | 1121. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 7.2 | 3.4 | 4.4 | 4.5 | 43.9 | 4.9 | 3.0 | 3.3 | 3.6 | 4.8 | 4.0 | 4.0 | |
| AREA= | 83.7 | 25.1 | 25.2 | 19.5 | 98.2 | 21.5 | 16.0 | 20.8 | 25.6 | 40.9 | 33.8 | 33.8 | |
| VEL= | 1.8 | 2.9 | 3.7 | 4.8 | 9.4 | 4.8 | 3.9 | 3.3 | 2.9 | 2.5 | 2.5 | 2.5 | |
| DEPTH= | .8 | 1.8 | 2.6 | 3.9 | 4.9 | 3.9 | 2.9 | 2.2 | 1.8 | 1.4 | 1.4 | 1.4 | |

| STA= | 1121. | 1145. | 1175. | 1213. |
|---|---|---|---|---|
| PER Q= | 4.0 | 3.6 | 1.4 | |
| AREA= | 33.8 | 34.8 | 21.4 | |
| VEL= | 2.5 | 2.2 | 1.4 | |
| DEPTH= | 1.4 | 1.2 | .6 | |

*SECNO .669
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .669 | 4.18 | 2452.18 | 2452.18 | .00 | 2452.81 | .63 | 2.30 | .00 | 2449.00 |
| 2099.0 | 803.2 | 720.1 | 575.8 | 225.0 | 73.5 | 172.3 | 257.2 | 128.5 | 2449.00 |
| .76 | 3.57 | 9.79 | 3.34 | .050 | .030 | .050 | .000 | 2448.00 | 848.59 |
| 06931 | 420. | 460. | 390. | 0 | 14 | 0 | .00 | 300.26 | 1148.85 |

FLOW DISTRIBUTION FOR SECNO= .67 CWSEL= 2452.18

| STA= | 849. | 899. | 911. | 931. | 950. | 970. | 979. | 990. | 1010. | 1015. | 1020. | 1029. | 1040. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 15.4 | 3.3 | 3.0 | 3.0 | 3.5 | 3.3 | 6.7 | 34.3 | 3.6 | 3.0 | 4.8 | 3.5 | |
| AREA= | 86.4 | 20.1 | 23.1 | 23.1 | 24.8 | 18.1 | 29.4 | 73.5 | 14.5 | 13.1 | 22.8 | 19.8 | |
| VEL= | 3.7 | 3.5 | 2.8 | 2.8 | 2.9 | 3.8 | 4.8 | 9.8 | 5.2 | 4.9 | 4.4 | 3.7 | |
| DEPTH= | 1.7 | 1.7 | 1.2 | 1.2 | 1.3 | 1.9 | 2.7 | 3.7 | 3.0 | 2.8 | 2.4 | 1.9 | |

| STA= | 1040. | 1060. | 1080. | 1100. | 1149. |
|---|---|---|---|---|---|
| PER Q= | 3.3 | 3.1 | 3.1 | 2.9 | |
| AREA= | 24.7 | 23.5 | 23.5 | 30.4 | |
| VEL= | 2.8 | 2.8 | 2.8 | 2.0 | |
| DEPTH= | 1.2 | 1.2 | 1.2 | .6 | |

*SECNO .765
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .765 | 5.31 | 2458.31 | 2458.31 | .00 | 2459.17 | .85 | 3.03 | .07 | 2453.50 |
| 2099.0 | 939.3 | 820.8 | 338.9 | 277.9 | 75.7 | 69.3 | 262.2 | 131.6 | 2453.50 |
| .78 | 3.38 | 10.84 | 4.89 | .050 | .030 | .050 | .000 | 2453.00 | 760.37 |
| .005554 | 470. | 510. | 490. | 0 | 11 | 0 | .00 | 271.19 | 1031.56 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .76 CWSEL= 2458.31

| STA= | 760. | 800. | 864. | 881. | 899. | 965. | 975. | 980. | 985. | 990. | 1005. | 1010. | 1015. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.9 | 4.9 | 5.5 | 5.1 | 3.0 | 4.3 | 4.8 | 6.3 | 6.9 | 39.1 | 6.6 | 4.8 | |
| AREA= | 37.5 | 49.7 | 33.4 | 32.6 | 37.2 | 23.1 | 19.1 | 22.1 | 23.3 | 75.7 | 22.8 | 19.1 | |
| VEL= | 2.2 | 2.1 | 3.5 | 3.3 | 1.7 | 3.9 | 5.3 | 6.0 | 6.2 | 10.8 | 6.1 | 5.3 | |
| DEPTH= | .9 | .8 | 2.0 | 1.8 | .6 | 2.3 | 3.8 | 4.4 | 4.7 | 5.0 | 4.6 | 3.8 | |

| STA= | 1015. | 1025. | 1032. |
|---|---|---|---|
| PER Q= | 4.3 | .4 | |
| AREA= | 23.1 | 4.3 | |
| VEL= | 3.9 | 1.8 | |
| DEPTH= | 2.3 | .7 | |

*SECNO .866
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .866 | 4.98 | 2462.98 | 2462.98 | .00 | 2464.20 | 1.21 | 3.42 | .11 | 2459.00 |
| 2099.0 | 869.5 | 961.5 | 267.9 | 183.0 | 80.7 | 49.7 | 266.5 | 133.9 | 2459.00 |
| .79 | 4.75 | 11.91 | 5.39 | .050 | .030 | .050 | .000 | 2458.00 | 906.87 |
| 07885 | 510. | 530. | 530. | 0 | 11 | 0 | .00 | 123.08 | 1029.95 |

FLOW DISTRIBUTION FOR SECNO= .87 CWSEL= 2462.98

| STA= | 907. | 930. | 950. | 955. | 965. | 981. | 987. | 992. | 1010. | 1015. | 1020. | 1030. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 6.4 | 15.6 | 3.4 | 4.0 | 3.6 | 3.1 | 5.5 | 45.8 | 5.6 | 4.4 | 2.7 | |
| AREA= | 34.5 | 59.7 | 13.7 | 19.8 | 22.5 | 13.7 | 19.2 | 80.7 | 18.7 | 16.2 | 14.8 | |
| VEL= | 3.9 | 5.5 | 5.1 | 4.2 | 3.4 | 4.8 | 6.0 | 11.9 | 6.3 | 5.8 | 3.8 | |
| DEPTH= | 1.5 | 3.0 | 2.7 | 2.0 | 1.4 | 2.5 | 3.5 | 4.5 | 3.7 | 3.2 | 1.5 | |

*SECNO .949

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .949 | 6.43 | 2469.43 | 2469.43 | .00 | 2471.32 | 1.89 | 3.05 | .20 | 2464.00 |
| 2099.0 | 209.6 | 1502.7 | 386.7 | 47.4 | 118.6 | 74.7 | 269.3 | 134.9 | 2464.00 |
| .81 | 4.42 | 12.67 | 5.18 | .050 | .030 | .050 | .000 | 2463.00 | 965.43 |
| .006141 | 440. | 440. | 440. | 0 | 11 | 0 | .00 | 73.14 | 1038.57 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= .95 CWSEL= 2469.43

| STA= | 965. | 979. | 990. | 1010. | 1020. | 1030. | 1039. |
|---|---|---|---|---|---|---|---|
| PER Q= | .9 | 9.1 | 71.6 | 13.1 | 4.8 | .5 | |
| AREA= | 9.7 | 37.7 | 118.6 | 44.3 | 24.3 | 6.1 | |
| VEL= | 1.9 | 5.1 | 12.7 | 6.2 | 4.2 | 1.8 | |
| DEPTH= | .7 | 3.4 | 5.9 | 4.4 | 2.4 | .7 | |

*SECNO 1.045

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.045 | 5.48 | 2474.48 | 2474.48 | .00 | 2475.58 | 1.09 | 3.07 | .08 | 2470.00 |
| 2099.0 | 459.3 | 1092.4 | 547.3 | 131.0 | 99.7 | 124.0 | 272.9 | 136.4 | 2470.00 |
| .83 | 3.51 | 10.96 | 4.41 | .050 | .030 | .050 | .000 | 2469.00 | 903.73 |
| .005786 | 510. | 510. | 535. | 0 | 15 | 0 | .00 | 169.89 | 1073.62 |

DISTRIBUTION FOR SECNO= 1.04 CWSEL= 2474.48

| STA= | 904. | 940. | 956. | 971. | 980. | 985. | 990. | 1010. | 1016. | 1021. | 1026. | 1031. | 1040. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 3.4 | 3.3 | 3.4 | 3.3 | 5.3 | 52.0 | 6.5 | 5.3 | 3.7 | 3.0 | 4.1 | |
| AREA= | 30.3 | 24.0 | 23.1 | 18.8 | 14.9 | 19.9 | 99.7 | 23.3 | 20.5 | 15.8 | 13.8 | 21.9 | |
| VEL= | 2.2 | 2.9 | 3.0 | 3.8 | 4.6 | 5.6 | 11.0 | 5.9 | 5.4 | 5.0 | 4.6 | 3.9 | |
| DEPTH= | .8 | 1.5 | 1.5 | 2.2 | 3.0 | 4.0 | 5.0 | 4.2 | 3.7 | 3.3 | 2.9 | 2.3 | |

| STA= | 1040. | 1060. | 1074. |
|---|---|---|---|
| PER Q= | 3.1 | .3 | |
| AREA= | 23.8 | 4.9 | |
| VEL= | 2.7 | 1.3 | |
| DEPTH= | 1.2 | .3 | |

*SECNO 1.148

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.148 | 5.99 | 2480.99 | 2480.99 | .00 | 2482.77 | 1.78 | 3.30 | .21 | 2476.00 |
| 2099.0 | 500.4 | 1434.5 | 164.1 | 91.3 | 115.3 | 37.3 | 276.5 | 137.9 | 2476.00 |
| .84 | 5.48 | 12.44 | 4.40 | .050 | .030 | .050 | .000 | 2475.00 | 957.72 |
| .006553 | 525. | 540. | 540. | 0 | 8 | 0 | .00 | 77.11 | 1034.84 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.15 CWSEL= 2480.99

| STA= | 958. | 961. | 967. | 972. | 978. | 983. | 989. | 1010. | 1015. | 1020. | 1025. | 1030. | 1035. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .1 | 1.2 | 2.9 | 4.9 | 6.4 | 8.4 | 68.3 | 5.5 | 1.7 | .4 | .2 | .0 | |
| AREA= | 1.6 | 8.2 | 13.7 | 19.0 | 22.3 | 26.4 | 115.3 | 20.0 | 10.0 | 4.2 | 2.5 | .7 | |
| VEL= | 1.5 | 3.1 | 4.4 | 5.3 | 6.0 | 6.7 | 12.4 | 5.8 | 3.6 | 2.1 | 1.5 | .7 | |
| DEPTH= | .5 | 1.5 | 2.5 | 3.3 | 4.0 | 4.6 | 5.5 | 4.0 | 2.0 | .8 | .5 | .1 | |

*SECNO 1.242
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.242 | 6.07 | 2487.07 | 2487.07 | .00 | 2488.49 | 1.42 | 3.02 | .04 | 2482.00 |
| 2099.0 | 361.8 | 1297.0 | 440.2 | 80.8 | 111.4 | 101.0 | 279.6 | 139.0 | 2482.00 |
| .86 | 4.48 | 11.64 | 4.36 | .050 | .030 | .050 | .000 | 2481.00 | 946.82 |
| .005632 | 500. | 500. | 485. | 0 | 5 | 0 | .00 | 114.35 | 1061.17 |

FLOW DISTRIBUTION FOR SECNO= 1.24 CWSEL= 2487.07

| | 947. | 975. | 985. | 990. | 1010. | 1015. | 1020. | 1025. | 1035. | 1061. |
|---|---|---|---|---|---|---|---|---|---|---|
| Q= | 3.5 | 7.2 | 6.6 | 61.8 | 6.6 | 4.4 | 3.1 | 4.2 | 2.7 | |
| AREA= | 26.5 | 31.5 | 22.9 | 111.4 | 22.9 | 17.9 | 14.4 | 22.7 | 23.3 | |
| VEL= | 2.7 | 4.8 | 6.1 | 11.6 | 6.1 | 5.1 | 4.5 | 3.9 | 2.5 | |
| DEPTH= | .9 | 3.1 | 4.6 | 5.6 | 4.6 | 3.6 | 2.9 | 2.3 | .9 | |

*SECNO 1.343
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.343 | 6.96 | 2495.96 | 2495.96 | .00 | 2497.75 | 1.78 | 3.15 | .11 | 2492.00 |
| 2099.0 | 108.7 | 1681.8 | 308.5 | 25.5 | 143.0 | 68.2 | 282.8 | 140.1 | 2492.00 |
| .87 | 4.26 | 11.76 | 4.52 | .050 | .030 | .050 | .000 | 2489.00 | 972.12 |
| .006389 | 530. | 530. | 510. | 0 | 8 | 0 | .00 | 70.43 | 1042.56 |

FLOW DISTRIBUTION FOR SECNO= 1.34 CWSEL= 2495.96

| STA= | 972. | 976. | 981. | 985. | 1012. | 1017. | 1023. | 1028. | 1034. | 1039. | 1043. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .2 | 1.5 | 3.5 | 80.1 | 5.3 | 3.9 | 2.7 | 1.7 | .9 | .1 | |
| AREA= | 2.6 | 8.6 | 14.2 | 143.0 | 19.8 | 16.5 | 13.3 | 10.1 | 6.8 | 1.7 | |
| VEL= | 1.7 | 3.6 | 5.1 | 11.8 | 5.6 | 5.0 | 4.3 | 3.6 | 2.8 | 1.4 | |
| DEPTH= | .6 | 2.0 | 3.3 | 5.3 | 3.7 | 3.1 | 2.5 | 1.9 | 1.3 | .5 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.428
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.428 | 5.72 | 2500.72 | 2500.72 | .00 | 2502.27 | 1.55 | 2.92 | .02 | 2496.00 |
| 2099.0 | 208.7 | 1271.4 | 618.9 | 42.4 | 104.4 | 123.8 | 285.4 | 140.9 | 2496.00 |
| .88 | 4.92 | 12.18 | 5.00 | .050 | .030 | .050 | .000 | 2495.00 | 970.51 |
| .006724 | 435. | 450. | 435. | 0 | 15 | 0 | .00 | 91.23 | 1061.74 |

FLOW DISTRIBUTION FOR SECNO= 1.43 CWSEL= 2500.72

| STA= | 971. | 985. | 990. | 1010. | 1015. | 1020. | 1025. | 1030. | 1036. | 1047. | 1062. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 4.1 | 5.9 | 60.6 | 7.0 | 5.8 | 4.6 | 3.5 | 3.0 | 3.9 | 1.7 | |
| AREA= | 22.1 | 20.3 | 104.4 | 22.3 | 19.8 | 17.3 | 14.8 | 14.1 | 21.5 | 13.9 | |
| VEL= | 3.9 | 6.1 | 12.2 | 6.6 | 6.1 | 5.6 | 5.0 | 4.5 | 3.8 | 2.5 | |
| DEPTH= | 1.5 | 4.1 | 5.2 | 4.5 | 4.0 | 3.5 | 3.0 | 2.5 | 1.9 | .9 | |

*SECNO 1.525
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.525 | 5.27 | 2506.27 | 2506.27 | .00 | 2507.70 | 1.43 | 3.52 | .01 | 2502.00 |
| 2099.0 | 718.7 | 1153.9 | 226.3 | 139.5 | 95.4 | 45.6 | 288.5 | 141.9 | 2502.00 |
| .90 | 5.15 | 12.09 | 4.96 | .050 | .030 | .050 | .000 | 2501.00 | 933.64 |
| .007469 | 500. | 510. | 460. | 0 | 11 | 0 | .00 | 97.72 | 1031.36 |

FLOW DISTRIBUTION FOR SECNO= 1.52 CWSEL= 2506.27

| STA= | 934. | 955. | 965. | 970. | 975. | 980. | 985. | 990. | 1010. | 1015. | 1020. | 1031. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 5.5 | 6.0 | 3.5 | 3.9 | 4.2 | 5.0 | 6.2 | 55.0 | 5.5 | 3.3 | 2.0 | |
| AREA= | 30.5 | 26.0 | 14.4 | 15.1 | 15.9 | 17.6 | 20.1 | 95.4 | 18.9 | 13.9 | 12.9 | |
| VEL= | 3.8 | 4.9 | 5.2 | 5.4 | 5.5 | 5.9 | 6.5 | 12.1 | 6.1 | 5.0 | 3.2 | |
| DEPTH= | 1.4 | 2.6 | 2.9 | 3.0 | 3.2 | 3.5 | 4.0 | 4.8 | 3.8 | 2.8 | 1.1 | |

*SECNO 1.619
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.619 | 5.09 | 2515.09 | 2515.09 | .00 | 2516.56 | 1.47 | 3.77 | .01 | 2510.80 |
| 2099.0 | 361.5 | 1140.7 | 596.8 | 64.0 | 93.6 | 111.3 | 291.6 | 143.0 | 2510.80 |
| .91 | 5.65 | 12.19 | 5.36 | .050 | .030 | .050 | .000 | 2510.00 | 968.37 |
| .007782 | 460. | 500. | 525. | 0 | 8 | 0 | .00 | 92.38 | 1060.75 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.62 CWSEL= 2515.09

| STA= | 968. | 980. | 985. | 990. | 993. | 1013. | 1015. | 1018. | 1023. | 1028. | 1033. | 1040. | 1055. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.4 | 4.6 | 5.8 | 3.4 | 54.3 | 3.4 | 3.1 | 5.7 | 4.8 | 4.0 | 4.1 | 3.1 | |
| AREA= | 17.8 | 16.6 | 19.1 | 10.5 | 93.6 | 10.5 | 10.0 | 18.8 | 17.1 | 15.3 | 18.3 | 19.7 | |
| VEL= | 4.0 | 5.8 | 6.4 | 6.8 | 12.2 | 6.8 | 6.6 | 6.3 | 5.9 | 5.5 | 4.8 | 3.3 | |
| DEPTH= | 1.5 | 3.3 | 3.8 | 4.2 | 4.7 | 4.2 | 4.0 | 3.8 | 3.4 | 3.1 | 2.4 | 1.3 | |

| STA= | 1055. | 1061. |
|---|---|---|
| PER Q= | .1 | |
| AREA= | 1.6 | |
| VEL= | 1.3 | |
| DEPTH= | .3 | |

*SECNO 1.719
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.719 | 4.92 | 2522.92 | 2522.92 | .00 | 2524.28 | 1.36 | 4.04 | .01 | 2519.00 |
| 2099.0 | 298.0 | 1103.4 | 697.7 | 55.8 | 92.8 | 131.8 | 294.8 | 144.1 | 2519.00 |
| .93 | 5.34 | 11.89 | 5.29 | .050 | .030 | .050 | .000 | 2518.00 | 966.74 |
| 07991 | 515. | 525. | 490. | 0 | 8 | 0 | .00 | 102.26 | 1068.99 |

FLOW DISTRIBUTION FOR SECNO= 1.72 CWSEL= 2522.92

| STA= | 967. | 979. | 985. | 990. | 1011. | 1016. | 1021. | 1025. | 1030. | 1035. | 1040. | 1050. | 1069. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.4 | 4.7 | 6.1 | 52.6 | 5.7 | 5.2 | 4.7 | 4.3 | 3.8 | 3.3 | 4.2 | 2.1 | |
| AREA= | 18.2 | 17.4 | 20.2 | 92.8 | 18.3 | 17.4 | 16.4 | 15.5 | 14.5 | 13.6 | 20.4 | 15.7 | |
| VEL= | 3.9 | 5.7 | 6.3 | 11.9 | 6.5 | 6.3 | 6.0 | 5.8 | 5.5 | 5.2 | 4.3 | 2.8 | |
| DEPTH= | 1.5 | 3.2 | 3.7 | 4.4 | 3.8 | 3.6 | 3.4 | 3.2 | 3.0 | 2.7 | 2.0 | .8 | |

*SECNO 1.802

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.802 | 6.63 | 2529.63 | 2529.63 | .00 | 2531.61 | 1.98 | 2.87 | .19 | 2524.00 |
| 2099.0 | 424.0 | 1620.7 | 54.3 | 87.3 | 128.7 | 14.9 | 297.2 | 144.9 | 2524.00 |
| .94 | 4.86 | 12.59 | 3.63 | .050 | .030 | .050 | .000 | 2523.00 | 947.13 |
| .005794 | 440. | 440. | 350. | 0 | 11 | 0 | .00 | 68.18 | 1015.31 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

FLOW DISTRIBUTION FOR SECNO= 1.80 CWSEL= 2529.63

| STA= | 947. | 955. | 960. | 965. | 970. | 975. | 980. | 984. | 989. | 1010. | 1015. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .1 | .3 | .6 | 1.0 | 1.8 | 3.3 | 5.4 | 7.6 | 77.2 | 2.6 | |
| AREA= | 2.2 | 3.6 | 5.4 | 7.1 | 10.2 | 14.7 | 19.8 | 24.1 | 128.7 | 14.9 | |
| VEL= | 1.1 | 1.8 | 2.4 | 2.9 | 3.7 | 4.8 | 5.7 | 6.6 | 12.6 | 3.6 | |
| DEPTH= | .3 | .7 | 1.1 | 1.4 | 2.1 | 3.1 | 4.1 | 5.1 | 6.1 | 3.0 | |

*SECNO 1.897

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.897 | 4.88 | 2538.88 | 2538.88 | .00 | 2540.17 | 1.29 | 3.22 | .07 | 2535.30 |
| 1650.0 | 297.4 | 1024.8 | 327.8 | 63.8 | 93.1 | 71.7 | 299.9 | 145.9 | 2535.30 |
| .96 | 4.66 | 11.01 | 4.57 | .050 | .030 | .050 | .000 | 2534.00 | 951.95 |
| .007375 | 480. | 500. | 545. | 0 | 19 | 0 | .00 | 93.49 | 1045.44 |

DISTRIBUTION FOR SECNO= 1.90 CWSEL= 2538.88

| STA= | 952. | 970. | 976. | 979. | 983. | 986. | 1008. | 1011. | 1014. | 1021. | 1028. | 1041. | 1045. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.1 | 4.2 | 3.1 | 3.5 | 4.1 | 62.1 | 3.7 | 3.3 | 5.7 | 4.0 | 3.1 | .1 | |
| AREA= | 17.3 | 14.9 | 9.8 | 10.3 | 11.5 | 93.1 | 10.4 | 9.7 | 18.5 | 15.4 | 16.7 | 1.0 | |
| VEL= | 3.0 | 4.7 | 5.3 | 5.6 | 5.8 | 11.0 | 5.8 | 5.6 | 5.1 | 4.3 | 3.0 | 1.0 | |
| DEPTH= | 1.0 | 2.5 | 3.0 | 3.2 | 3.5 | 4.2 | 3.5 | 3.2 | 2.8 | 2.2 | 1.2 | .2 | |

*SECNO 1.993
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.993 | 5.07 | 2543.07 | 2543.07 | .00 | 2544.25 | 1.18 | 3.39 | .01 | 2539.00 |
| 1650.0 | 393.0 | 981.1 | 275.9 | 98.3 | 91.4 | 58.1 | 302.6 | 147.1 | 2539.00 |
| .97 | 4.00 | 10.74 | 4.75 | .050 | .030 | .050 | .000 | 2538.00 | 911.38 |
| .006241 | 535. | 510. | 430. | 0 | 8 | 0 | .00 | 123.10 | 1034.49 |

FLOW DISTRIBUTION FOR SECNO= 1.99 CWSEL= 2543.07

| STA= | 911. | 965. | 978. | 984. | 990. | 1010. | 1015. | 1020. | 1026. | 1034. |
|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 3.2 | 6.4 | 6.3 | 7.9 | 59.5 | 6.6 | 5.2 | 3.9 | 1.0 | |
| AREA= | 28.5 | 26.9 | 19.9 | 22.9 | 91.4 | 19.1 | 16.6 | 15.2 | 7.2 | |
| VEL= | 1.9 | 3.9 | 5.2 | 5.7 | 10.7 | 5.7 | 5.2 | 4.2 | 2.3 | |
| DEPTH= | .5 | 2.1 | 3.3 | 3.8 | 4.6 | 3.8 | 3.3 | 2.4 | .9 | |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.094
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.094 | 5.29 | 2549.29 | 2549.29 | .00 | 2550.70 | 1.41 | 3.30 | .07 | 2545.00 |
| 1650.0 | 136.1 | 1123.6 | 390.3 | 30.2 | 100.6 | 92.9 | 305.4 | 148.3 | 2545.00 |
| .99 | 4.51 | 11.17 | 4.20 | .050 | .030 | .050 | .000 | 2544.00 | 976.45 |
| .006328 | 495. | 530. | 530. | 0 | 8 | 0 | .00 | 86.31 | 1062.76 |

FLOW DISTRIBUTION FOR SECNO= 2.09 CWSEL= 2549.29

| STA= | 976. | 990. | 1011. | 1016. | 1020. | 1025. | 1035. | 1051. | 1063. |
|---|---|---|---|---|---|---|---|---|---|
| PER Q= | 8.3 | 68.1 | 6.6 | 4.8 | 3.4 | 4.6 | 3.8 | .5 | |
| AREA= | 30.2 | 100.6 | 18.5 | 15.1 | 12.4 | 20.2 | 21.2 | 5.5 | |
| VEL= | 4.5 | 11.2 | 5.9 | 5.2 | 4.5 | 3.8 | 3.0 | 1.6 | |
| DEPTH= | 2.2 | 4.8 | 3.9 | 3.3 | 2.6 | 2.0 | 1.4 | .4 | |

*SECNO 2.183
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.183 | 4.75 | 2552.75 | 2552.75 | .00 | 2554.40 | 1.65 | 3.31 | .07 | 2548.70 |
| 1650.0 | 300.4 | 1034.8 | 314.8 | 54.7 | 84.6 | 52.4 | 307.5 | 149.1 | 2548.50 |
| 1.00 | 5.49 | 12.24 | 6.00 | .050 | .030 | .050 | .000 | 2548.00 | 966.24 |
| .008358 | 470. | 470. | 410. | 0 | 11 | 0 | .00 | 61.11 | 1027.35 |

FLOW DISTRIBUTION FOR SECNO= 2.18 CWSEL= 2552.75

| STA= | 966. | 970. | 975. | 980. | 985. | 990. | 1009. | 1014. | 1018. | 1025. | 1027. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PER Q= | .1 | 1.2 | 3.1 | 5.8 | 8.0 | 62.7 | 7.8 | 7.0 | 4.2 | .1 | |
| AREA= | 1.4 | 6.3 | 11.3 | 16.3 | 19.5 | 84.6 | 18.5 | 17.3 | 15.8 | .9 | |
| VEL= | 1.4 | 3.1 | 4.6 | 5.9 | 6.7 | 12.2 | 7.0 | 6.7 | 4.4 | 1.4 | |
| DEPTH= | .4 | 1.3 | 2.3 | 3.3 | 3.9 | 4.5 | 4.1 | 3.9 | 2.3 | .4 | |

T1 FLOODWAY DETERMINATION
T2 YUCCA FLAT WASH AND TWIN PEAKS WASH TRIBUTARIES TO FLYING E WASH
T3 AB: YUCCA FLATS WASH (FILE YUCCA.DAT)

| J1 | ICHECK | INQ | NINV | IDIR | STRT | METRIC | HVINS | Q | WSEL | FQ |
|---|---|---|---|---|---|---|---|---|---|---|
| | 0 | 3 | 0 | 0 | .008304 | 0 | 0 | 0 | 2309.8 | 0 |

| J2 | NPROF | IPLOT | PRFVS | XSECV | XSECH | FN | ALLDC | IBW | CHNIM | ITRACE |
|---|---|---|---|---|---|---|---|---|---|---|
| | 15 | 0 | -1 | 0 | 0 | 0 | -1 | 0 | 0 | 0 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*PROF 2

CRITICAL DEPTH TO BE CALCULATED AT ALL CROSS SECTIONS

CCHV= .100 CEHV= .300
*SECNO 2.435
WATER EL=X5 CARD= 2309.800

3470 ENCROACHMENT STATIONS= 957.7 1102.0 TYPE= 1 TARGET= 144.310
STARTING WSEL FROM UPPER FLYING E WASH ANALYSIS.
CONFLUENCE OF UPPER FLYING E WASH AND YUCCA FLAT WASH.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.435 | 6.41 | 2309.91 | 2309.80 | 2309.87 | 2312.10 | 2.18 | .00 | .00 | 2304.00 |
| 6943.0 | 856.4 | 3357.8 | 2728.8 | 124.5 | 221.0 | 355.8 | .0 | .0 | 2304.00 |
| .00 | 6.88 | 15.19 | 7.67 | .050 | .030 | .050 | .000 | 2303.50 | 957.69 |
| .008374 | 500. | 490. | 455. | 0 | 5 | 3 | .00 | 144.31 | 1102.00 |

1490 NH CARD USED
*SECNO 2.539

DIVIDED FLOW

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 465.3 1100.0 TYPE= 1 TARGET= 634.700
ELENCL= 2317.30 ELENCR= 2317.00
AT HIGH FLOW, BOTH YUCCA FLAT WASH AND FLYING E WASH CHANNELS
ARE USED. SECTION REPEATED FOR BOTH MODELS. NH CARD DEFINES CHANNELS
HYDRAULIC CONTROL LINE IS AT STATION 850.0

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.539 | 6.51 | 2315.51 | 2315.51 | 2315.51 | 2316.75 | 1.24 | 4.25 | .09 | 2313.50 |
| 6943.0 | 371.4 | 1747.4 | 4824.2 | 126.3 | 185.3 | 532.0 | 9.2 | 3.3 | 2313.20 |
| .02 | 2.94 | 9.43 | 9.07 | .050 | .030 | .038 | .000 | 2309.00 | 509.92 |
| .007990 | 570. | 550. | 490. | 0 | 5 | 0 | .00 | 394.83 | 1059.04 |

*SECNO .191

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 560.0 1093.0 TYPE= 1 TARGET= 533.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .191 | 4.85 | 2322.35 | 2322.35 | 2322.35 | 2323.22 | .87 | 4.53 | .04 | 2320.00 |
| 5152.0 | 2842.4 | 2260.6 | 49.0 | 628.8 | 224.0 | 20.1 | 18.2 | 7.8 | 2320.00 |
| .04 | 4.52 | 10.09 | 2.43 | .060 | .040 | .060 | .000 | 2317.50 | 560.00 |
| .012848 | 410. | 490. | 500. | 0 | 16 | 0 | .00 | 501.27 | 1093.00 |

*SECNO .290
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 774.0 1163.0 TYPE= 1 TARGET= 389.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .290 | 3.76 | 2328.76 | 2328.76 | 2328.76 | 2329.79 | 1.02 | 5.93 | .05 | 2326.40 |
| 5152.0 | 1373.5 | 1755.2 | 2023.4 | 274.6 | 156.2 | 314.8 | 26.8 | 12.5 | 2326.30 |
| .05 | 5.00 | 11.24 | 6.43 | .050 | .030 | .050 | .000 | 2325.00 | 774.00 |
| .011923 | 420. | 520. | 520. | 0 | 15 | 0 | .00 | 388.77 | 1162.77 |

*SECNO .390
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 922.0 1301.0 TYPE= 1 TARGET= 379.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .390 | 4.87 | 2336.87 | 2336.87 | 2336.34 | 2337.87 | .99 | 5.63 | .00 | 2334.00 |
| 5152.0 | 672.2 | 1617.5 | 2862.3 | 133.8 | 131.7 | 583.5 | 36.1 | 17.0 | 2334.00 |
| .07 | 5.02 | 12.28 | 4.91 | .050 | .030 | .050 | .000 | 2332.00 | 922.00 |
| .010207 | 530. | 530. | 490. | 0 | 14 | 0 | .00 | 379.00 | 1301.00 |

*SECNO .477
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 939.0 1329.0 TYPE= 1 TARGET= 390.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .477 | 2.52 | 2343.52 | 2343.52 | 2343.25 | 2344.46 | .94 | 6.32 | .01 | 2341.50 |
| 5152.0 | 430.1 | 982.6 | 3739.2 | 60.0 | 85.5 | 570.9 | 44.1 | 20.9 | 2341.40 |
| .09 | 7.17 | 11.49 | 6.55 | .050 | .030 | .050 | .000 | 2341.00 | 939.00 |
| .020979 | 450. | 460. | 440. | 0 | 11 | 0 | .00 | 390.00 | 1329.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .578
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 971.0 1312.0 TYPE= 1 TARGET= 341.000
ENCROACHED TO 1450 DUE TO SMALL RIGHT BANK TRIBUTARY. FLOODPLAIN
MAPPED TO WSEL.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .578 | 6.46 | 2351.96 | 2351.96 | 2351.79 | 2353.06 | 1.10 | 6.18 | .05 | 2350.00 |
| 5152.0 | 25.3 | 2186.2 | 2940.5 | 9.6 | 185.0 | 648.6 | 53.3 | 25.2 | 2348.80 |
| .11 | 2.65 | 11.82 | 4.53 | .050 | .030 | .050 | .000 | 2345.50 | 971.00 |
| .007703 | 530. | 530. | 510. | 0 | 20 | 0 | .00 | 341.00 | 1312.00 |

*SECNO .697
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 830.0 1043.0 TYPE= 1 TARGET= 213.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .697 | 5.57 | 2359.07 | 2359.07 | 2358.84 | 2360.55 | 1.48 | 4.77 | .11 | 2355.60 |
| 5152.0 | 2192.9 | 2675.5 | 283.6 | 409.8 | 212.9 | 61.0 | 63.9 | 29.0 | 2355.30 |
| .13 | 5.35 | 12.56 | 4.65 | .050 | .030 | .050 | .000 | 2353.50 | 830.00 |
| .007849 | 610. | 630. | 590. | 0 | 15 | 0 | .00 | 213.00 | 1043.00 |

*SECNO .788
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 850.0 1024.0 TYPE= 1 TARGET= 174.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .788 | 5.95 | 2364.95 | 2364.95 | 2364.94 | 2366.67 | 1.72 | 3.57 | .07 | 2360.60 |
| 5152.0 | 2054.4 | 3034.0 | 63.7 | 375.5 | 234.6 | 14.6 | 71.0 | 31.1 | 2360.80 |
| .14 | 5.47 | 12.93 | 4.36 | .050 | .030 | .050 | .000 | 2359.00 | 850.00 |
| .007192 | 470. | 480. | 455. | 0 | 8 | 0 | .00 | 174.00 | 1024.00 |

*SECNO .883

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 949.0 1043.0 TYPE= 1 TARGET= 94.000

| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
|---|---|---|---|---|---|---|---|---|---|
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| .883 | 6.02 | 2370.52 | 2370.52 | 2370.66 | 2372.99 | 2.47 | 3.92 | .23 | 2365.30 |
| 5152.0 | 1198.4 | 3213.8 | 739.8 | 157.5 | 216.4 | 98.5 | 77.2 | 32.6 | 2365.00 |
| .15 | 7.61 | 14.85 | 7.51 | .050 | .030 | .050 | .000 | 2364.50 | 949.00 |
| .008936 | 470. | 500. | 500. | 0 | 5 | 0 | .00 | 94.00 | 1043.00 |

*SECNO .972

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 959.0 1117.0 TYPE= 1 TARGET= 158.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .972 | 6.03 | 2375.53 | 2375.53 | 2375.54 | 2377.40 | 1.87 | 3.74 | .06 | 2370.30 |
| 5152.0 | 507.0 | 3018.1 | 1626.9 | 85.3 | 224.6 | 275.5 | 82.9 | 33.9 | 2370.30 |
| .16 | 5.95 | 13.44 | 5.91 | .050 | .030 | .050 | .000 | 2369.50 | 959.37 |
| .007115 | 470. | 470. | 470. | 0 | 5 | 0 | .00 | 157.50 | 1116.87 |

NO 1.070

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 985.0 1075.0 TYPE= 1 TARGET= 90.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.070 | 6.83 | 2381.83 | 2381.83 | 2381.89 | 2384.46 | 2.62 | 3.74 | .23 | 2376.80 |
| 5152.0 | 105.6 | 3971.9 | 1074.5 | 22.2 | 277.8 | 148.7 | 88.8 | 35.3 | 2376.20 |
| .17 | 4.76 | 14.30 | 7.23 | .050 | .030 | .050 | .000 | 2375.00 | 985.00 |
| .007701 | 540. | 520. | 460. | 0 | 8 | 0 | .00 | 89.31 | 1074.31 |

*SECNO 1.163

3301 HV CHANGED MORE THAN HVINS

3470 ENCROACHMENT STATIONS= 895.0 1025.0 TYPE= 1 TARGET= 130.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.163 | 6.12 | 2386.12 | 2385.18 | 2385.75 | 2387.45 | 1.33 | 2.86 | .13 | 2380.00 |
| 5152.0 | 2211.6 | 2797.0 | 143.4 | 385.9 | 244.8 | 31.2 | 94.8 | 36.5 | 2380.00 |
| .19 | 5.73 | 11.43 | 4.59 | .050 | .030 | .050 | .000 | 2380.00 | 895.00 |
| .004754 | 445. | 490. | 490. | 2 | 15 | 0 | .00 | 130.00 | 1025.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.239

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 905.0 1034.0 TYPE= 1 TARGET= 129.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.239 | 7.27 | 2390.27 | 2390.27 | 2390.38 | 2392.46 | 2.19 | 2.08 | .26 | 2384.50 |
| 5152.0 | 1256.2 | 3552.4 | 343.4 | 227.6 | 257.2 | 63.8 | 100.2 | 37.7 | 2384.00 |
| .20 | 5.52 | 13.81 | 5.39 | .050 | .030 | .050 | .000 | 2383.00 | 905.00 |
| .006001 | 370. | 400. | 410. | 0 | 11 | 0 | .00 | 128.59 | 1033.59 |

*SECNO 1.367

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 845.0 1166.0 TYPE= 1 TARGET= 321.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.367 | 6.43 | 2394.93 | 2394.93 | 2394.92 | 2396.20 | 1.27 | 3.60 | .09 | 2391.00 |
| 5152.0 | 653.3 | 2835.2 | 1663.5 | 185.8 | 243.7 | 383.2 | 109.1 | 40.4 | 2391.00 |
| .22 | 3.52 | 11.63 | 4.34 | .050 | .030 | .050 | .000 | 2388.50 | 845.00 |
| .005691 | 390. | 680. | 630. | 0 | 15 | 0 | .00 | 321.00 | 1166.00 |

*SECNO 1.462
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 981.0 1168.0 TYPE= 1 TARGET= 187.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.462 | 5.87 | 2401.37 | 2401.37 | 2401.43 | 2403.01 | 1.64 | 3.13 | .11 | 2396.90 |
| 5152.0 | 130.7 | 2714.2 | 2307.1 | 25.7 | 207.4 | 403.7 | 116.8 | 43.0 | 2396.90 |
| .23 | 5.09 | 13.09 | 5.71 | .050 | .030 | .050 | .000 | 2395.50 | 981.47 |
| .007814 | 445. | 500. | 440. | 0 | 15 | 0 | .00 | 186.53 | 1168.00 |

*SECNO 1.551
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

```
ECNO      DEPTH     CWSEL     CRIWS     WSELK     EG        HV        HL        OLOSS     L-BANK ELEV
          QLOB      QCH       QROB      ALOB      ACH       AROB      VOL       TWA       R-BANK ELEV
TIME      VLOB      VCH       VROB      XNL       XNCH      XNR       WTN       ELMIN     SSTA
SLOPE     XLOBL     XLCH      XLOBR     ITRIAL    IDC       ICONT     CORAR     TOPWID    ENDST


3470 ENCROACHMENT STATIONS=      956.0    1100.0  TYPE=      1  TARGET=      144.000
   1.551      5.07   2407.07   2407.07   2406.92   2408.97      1.90      3.94       .08   2403.00
  5152.0     537.2    2549.3    2065.5      83.1     183.7     275.6     122.5      44.6   2403.00
     .25      6.46     13.88      7.49      .050      .030      .050      .000   2402.00    956.00
 .010785      470.      470.      380.         0        15         0       .00    144.00   1100.00


*SECNO 1.646
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      908.0    1071.0  TYPE=      1  TARGET=      163.000
   1.646      7.47   2412.47   2412.47   2412.64   2414.39      1.92      3.72       .01   2407.30
  5152.0     790.0    3708.0     654.0     175.6     290.3     132.9     128.9      46.3   2407.30
     .26      4.50     12.77      4.92      .050      .030      .050      .000   2405.00    908.00
 .005578      525.      500.      460.         0        14         0       .00    163.00   1071.00


*SECNO 1.718

HV CHANGED MORE THAN HVINS


3302 WARNING:  CONVEYANCE CHANGE OUTSIDE OF ACCEPTABLE RANGE,  KRATIO =  1.46


3470 ENCROACHMENT STATIONS=      820.0    1080.0  TYPE=      1  TARGET=      260.000

        CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH (DOWNSTREAM)

   1.718      6.49   2415.49   2413.77   2415.39   2415.94       .45      1.40       .15   2410.00
  5152.0    3020.9    1196.7     934.4     726.7     143.6     244.0     136.4      48.2   2410.00
     .28      4.16      8.33      3.83      .050      .030      .050      .000   2409.00    820.00
 .002618      380.      380.      380.         2        14         0       .00    260.00   1080.00


*SECNO 1.808
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS=      780.0    1114.0  TYPE=      1  TARGET=      334.000
```

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH (UPSTREAM)

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.808 | 3.33 | 2420.33 | 2420.33 | 2420.33 | 2420.98 | .65 | 1.69 | .06 | 2418.00 |
| 2085.0 | 763.9 | 691.1 | 630.0 | 211.2 | 70.8 | 148.5 | 144.9 | 51.4 | 2418.00 |
| .30 | 3.62 | 9.76 | 4.24 | .050 | .030 | .050 | .000 | 2417.00 | 780.00 |
| .009726 | 490. | 475. | 465. | 0 | 11 | 0 | .00 | 328.33 | 1108.33 |

*SECNO 1.905
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 949.0 1198.0 TYPE= 1 TARGET= 249.000

YUCCA FLATS WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.905 | 3.82 | 2425.82 | 2425.82 | 2425.82 | 2426.60 | .78 | 4.57 | .04 | 2423.00 |
| 2085.0 | 230.2 | 838.1 | 1016.7 | 55.6 | 83.0 | 266.7 | 149.7 | 54.8 | 2423.00 |
| .32 | 4.14 | 10.09 | 3.81 | .050 | .030 | .050 | .000 | 2422.00 | 952.23 |
| .008414 | 510. | 510. | 500. | 0 | 11 | 0 | .00 | 244.83 | 1197.06 |

*SECNO 2.003
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

ENCROACHMENT STATIONS= 768.0 1039.0 TYPE= 1 TARGET= 271.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.003 | 3.79 | 2432.79 | 2432.79 | 2432.76 | 2433.52 | .73 | 4.07 | .00 | 2430.00 |
| 2085.0 | 1059.4 | 909.9 | 115.7 | 304.0 | 94.9 | 31.5 | 154.5 | 57.7 | 2430.00 |
| .35 | 3.48 | 9.59 | 3.67 | .050 | .030 | .050 | .000 | 2429.00 | 768.00 |
| .007752 | 530. | 520. | 450. | 0 | 5 | 0 | .00 | 268.47 | 1036.47 |

*SECNO 2.091
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 800.0 1015.0 TYPE= 1 TARGET= 215.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.091 | 3.49 | 2437.49 | 2437.49 | 2437.00 | 2438.35 | .86 | 2.94 | .04 | 2434.00 |
| 2085.0 | 857.0 | 1029.6 | 198.4 | 239.8 | 104.6 | 41.1 | 157.8 | 59.5 | 2434.00 |
| .36 | 3.57 | 9.84 | 4.83 | .050 | .030 | .050 | .000 | 2434.00 | 800.00 |
| .007468 | 300. | 460. | 460. | 0 | 15 | 0 | .00 | 215.00 | 1015.00 |

*SECNO 2.172
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 821.0 1040.0 TYPE= 1 TARGET= 219.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| 2.172 | 4.34 | 2442.34 | 2442.34 | 2442.03 | 2443.20 | .85 | 3.09 | .00 | 2439.00 |
| 2085.0 | 899.1 | 820.8 | 365.2 | 241.5 | 76.8 | 75.3 | 161.4 | 61.4 | 2439.00 |
| .38 | 3.72 | 10.68 | 4.85 | .050 | .030 | .050 | .000 | 2438.00 | 821.00 |
| .007780 | 370. | 430. | 440. | 0 | 11 | 0 | .00 | 219.00 | 1040.00 |

*SECNO 2.284
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 951.0 1148.0 TYPE= 1 TARGET= 197.000
ENCROACHED TO 1208 DUE TO SMALL RIGHT BANK TRIBUTARY. FLOODPLAIN
MAPPED TO WSEL.

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.284 | 3.55 | 2450.55 | 2450.55 | 2450.57 | 2451.42 | .88 | 4.45 | .01 | 2447.50 |
| 2085.0 | 190.3 | 961.3 | 933.4 | 43.7 | 94.5 | 237.9 | 166.2 | 64.0 | 2447.50 |
| .40 | 4.35 | 10.18 | 3.92 | .050 | .030 | .050 | .000 | 2447.00 | 952.16 |
| .008160 | 530. | 590. | 540. | 0 | 15 | 0 | .00 | 195.84 | 1148.00 |

*SECNO 2.384
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 894.0 1095.0 TYPE= 1 TARGET= 201.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.384 | 3.67 | 2456.67 | 2456.67 | 2456.65 | 2457.54 | .87 | 4.35 | .00 | 2453.00 |
| 2085.0 | 753.4 | 764.3 | 567.3 | 175.7 | 69.7 | 130.3 | 170.6 | 66.3 | 2453.00 |
| .42 | 4.29 | 10.97 | 4.35 | .050 | .030 | .050 | .000 | 2453.00 | 894.00 |
| .008669 | 490. | 530. | 520. | 0 | 8 | 0 | .00 | 199.35 | 1093.35 |

*SECNO 2.477

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 935.0 1334.0 TYPE= 1 TARGET= 399.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.477 | 5.33 | 2462.33 | 2462.33 | 2462.33 | 2463.10 | .78 | 2.85 | .01 | 2458.00 |
| 2085.0 | 409.4 | 1082.8 | 592.8 | 108.6 | 115.9 | 235.5 | 175.1 | 69.1 | 2458.00 |
| .44 | 3.77 | 9.34 | 2.52 | .050 | .030 | .050 | .000 | 2457.00 | 936.05 |
| .004378 | 510. | 490. | 420. | 0 | 11 | 0 | .00 | 326.39 | 1332.97 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.562

3265 DIVIDED FLOW

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 912.0 1193.0 TYPE= 1 TARGET= 281.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.562 | 2.38 | 2467.38 | 2467.38 | 2467.37 | 2468.14 | .76 | 3.21 | .00 | 2465.00 |
| 2085.0 | 659.7 | 611.3 | 814.0 | 124.8 | 59.4 | 166.3 | 179.3 | 72.0 | 2465.00 |
| .46 | 5.29 | 10.29 | 4.89 | .050 | .030 | .050 | .000 | 2465.00 | 912.81 |
| .013623 | 420. | 450. | 475. | 0 | 14 | 0 | .00 | 229.97 | 1190.43 |

*SECNO 2.672
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 821.0 1044.0 TYPE= 1 TARGET= 223.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.672 | 3.34 | 2475.34 | 2475.34 | 2475.33 | 2476.15 | .81 | 7.07 | .02 | 2473.00 |
| 2085.0 | 1152.9 | 736.3 | 195.7 | 240.8 | 70.9 | 45.2 | 184.0 | 75.0 | 2473.00 |
| .49 | 4.79 | 10.38 | 4.33 | .050 | .030 | .050 | .000 | 2472.00 | 823.34 |
| .010979 | 610. | 580. | 525. | 0 | 14 | 0 | .00 | 220.36 | 1043.70 |

*SECNO 2.761

3470 ENCROACHMENT STATIONS= 797.0 1081.0 TYPE= 1 TARGET= 284.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.761 | 2.33 | 2480.33 | 2480.27 | 2480.33 | 2480.94 | .61 | 4.77 | .02 | 2478.10 |
| 2085.0 | 1088.5 | 667.9 | 328.6 | 247.7 | 72.8 | 82.1 | 187.6 | 77.3 | 2478.20 |
| .51 | 4.39 | 9.18 | 4.00 | .050 | .030 | .050 | .000 | 2478.00 | 797.96 |
| .011581 | 385. | 470. | 460. | 2 | 19 | 0 | .00 | 279.49 | 1077.44 |

*SECNO 2.857
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 957.0 1314.0 TYPE= 1 TARGET= 357.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.857 | 2.22 | 2488.22 | 2488.22 | 2488.22 | 2488.77 | .55 | 5.82 | .01 | 2486.00 |
| 2085.0 | 114.4 | 619.6 | 1351.0 | 30.8 | 66.7 | 361.3 | 192.5 | 80.9 | 2486.00 |
| .53 | 3.71 | 9.29 | 3.74 | .050 | .030 | .050 | .000 | 2486.00 | 957.76 |
| .012113 | 480. | 510. | 485. | 0 | 11 | 0 | .00 | 355.59 | 1313.35 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 2.965
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 922.0 1254.0 TYPE= 1 TARGET= 332.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.965 | 1.72 | 2496.72 | 2496.72 | 2496.72 | 2497.28 | .56 | 6.26 | .00 | 2495.00 |
| 2085.0 | 306.7 | 487.0 | 1291.3 | 69.4 | 51.5 | 286.8 | 196.5 | 84.0 | 2495.00 |
| .55 | 4.42 | 9.47 | 4.50 | .050 | .030 | .050 | .000 | 2495.00 | 922.85 |
| .017787 | 570. | 570. | 350. | 0 | 15 | 0 | .00 | 330.72 | 1253.57 |

*SECNO -1.718
START TRIB COMP
-1.718 1.718 2415.492

3470 ENCROACHMENT STATIONS= 820.0 1080.0 TYPE= 1 TARGET= 260.000

CONFLUENCE OF TWIN PEAKS WASH AND YUCCA FLATS WASH

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| -1.718 | 6.49 | 2415.49 | .00 | 2415.39 | 2415.94 | .45 | 1.46 | 4.80 | 2410.00 |
| 5152.0 | 3021.2 | 1196.0 | 934.9 | 728.0 | 143.8 | 244.5 | 203.1 | 86.6 | 2410.00 |
| .57 | 4.15 | 8.32 | 3.82 | .050 | .030 | .050 | .000 | 2409.00 | 820.00 |
| .002603 | 380. | 380. | 380. | 0 | 0 | 0 | .00 | 260.00 | 1080.00 |

*SECNO .098
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 911.0 1145.0 TYPE= 1 TARGET= 234.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .098 | 3.77 | 2418.77 | 2418.77 | 2418.78 | 2419.60 | .83 | 1.75 | .11 | 2417.00 |
| 2099.0 | 184.9 | 992.4 | 921.7 | 58.2 | 104.7 | 192.3 | 211.2 | 89.3 | 2415.00 |
| .59 | 3.18 | 9.48 | 4.79 | .050 | .030 | .050 | .000 | 2415.00 | 911.39 |
| .009842 | 410. | 520. | 565. | 0 | 14 | 0 | .00 | 233.18 | 1144.57 |

*SECNO .190

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 955.0 1036.0 TYPE= 1 TARGET= 81.000

| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
|---|---|---|---|---|---|---|---|---|---|
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |
| .190 | 5.86 | 2423.86 | 2423.86 | 2423.87 | 2425.48 | 1.62 | 3.84 | .24 | 2419.50 |
| 2099.0 | 404.7 | 1387.5 | 306.8 | 80.8 | 115.0 | 67.5 | 214.5 | 91.0 | 2419.50 |
| .61 | 5.01 | 12.06 | 4.55 | .050 | .030 | .050 | .000 | 2418.00 | 955.00 |
| .006822 | 510. | 490. | 420. | 0 | 14 | 0 | .00 | 81.00 | 1036.00 |

*SECNO .301
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 937.0 1055.0 TYPE= 1 TARGET= 118.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .301 | 4.48 | 2431.48 | 2431.48 | 2431.28 | 2432.69 | 1.21 | 4.28 | .04 | 2428.00 |
| 2099.0 | 552.3 | 1018.0 | 528.7 | 113.4 | 87.6 | 107.2 | 218.0 | 92.2 | 2428.00 |
| .63 | 4.87 | 11.62 | 4.93 | .050 | .030 | .050 | .000 | 2427.00 | 937.00 |
| .008759 | 450. | 580. | 610. | 0 | 19 | 0 | .00 | 118.00 | 1055.00 |

*SECNO .384

3470 ENCROACHMENT STATIONS= 948.0 1041.0 TYPE= 1 TARGET= 93.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .384 | 5.55 | 2434.55 | 2433.96 | 2434.00 | 2435.53 | .98 | 2.82 | .02 | 2430.00 |
| 2099.0 | 513.9 | 1076.9 | 508.2 | 115.7 | 106.0 | 106.5 | 221.2 | 93.3 | 2430.00 |
| .64 | 4.44 | 10.16 | 4.77 | .050 | .030 | .050 | .000 | 2429.00 | 948.00 |
| .004884 | 440. | 440. | 440. | 3 | 8 | 0 | .00 | 93.00 | 1041.00 |

*SECNO .473
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 930.0 1032.0 TYPE= 1 TARGET= 102.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .473 | 3.86 | 2440.86 | 2440.86 | 2440.65 | 2442.16 | 1.30 | 3.43 | .10 | 2438.00 |
| 2099.0 | 884.6 | 1049.0 | 165.4 | 147.6 | 90.6 | 34.3 | 224.6 | 94.4 | 2438.00 |
| .66 | 5.99 | 11.58 | 4.82 | .050 | .030 | .050 | .000 | 2437.00 | 930.00 |
| .010919 | 550. | 470. | 420. | 0 | 19 | 0 | .00 | 102.00 | 1032.00 |

*SECNO .581
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 961.0 1073.0 TYPE= 1 TARGET= 112.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .581 | 5.60 | 2448.60 | 2448.60 | 2448.41 | 2449.91 | 1.31 | 3.93 | .00 | 2444.00 |
| 2099.0 | 346.7 | 1184.9 | 567.4 | 75.3 | 101.9 | 136.6 | 227.7 | 95.5 | 2444.00 |
| .68 | 4.60 | 11.62 | 4.15 | .050 | .030 | .050 | .000 | 2443.00 | 961.00 |
| .006317 | 270. | 570. | 570. | 0 | 11 | 0 | .00 | 112.00 | 1073.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| ECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO .669
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 911.0 1040.0 TYPE= 1 TARGET= 129.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .669 | 4.68 | 2452.68 | 2452.68 | 2452.18 | 2453.79 | 1.11 | 3.06 | .02 | 2449.00 |
| 2099.0 | 684.1 | 953.8 | 461.2 | 158.0 | 83.5 | 85.7 | 230.8 | 96.7 | 2449.00 |
| .69 | 4.33 | 11.42 | 5.38 | .050 | .030 | .050 | .000 | 2448.00 | 911.00 |
| .007949 | 420. | 460. | 390. | 0 | 12 | 0 | .00 | 129.00 | 1040.00 |

*SECNO .765

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 965.0 1032.0 TYPE= 1 TARGET= 67.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .765 | 5.41 | 2458.41 | 2458.41 | 2458.31 | 2460.19 | 1.78 | 4.07 | .20 | 2453.50 |
| 099.0 | 601.7 | 1053.9 | 443.4 | 90.1 | 77.2 | 72.0 | 234.0 | 97.8 | 2453.50 |
| .70 | 6.68 | 13.65 | 6.16 | .050 | .030 | .050 | .000 | 2453.00 | 965.00 |
| .008578 | 470. | 510. | 490. | 0 | 8 | 0 | .00 | 67.00 | 1032.00 |

*SECNO .866

3301 HV CHANGED MORE THAN HVINS

3470 ENCROACHMENT STATIONS= 907.0 1030.0 TYPE= 1 TARGET= 123.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .866 | 5.14 | 2463.14 | 2462.98 | 2462.98 | 2464.20 | 1.06 | 3.94 | .07 | 2459.00 |
| 2099.0 | 891.5 | 937.9 | 269.5 | 196.5 | 83.6 | 52.9 | 237.4 | 98.9 | 2459.00 |
| .72 | 4.54 | 11.22 | 5.10 | .050 | .030 | .050 | .000 | 2458.00 | 907.00 |
| .006683 | 510. | 530. | 530. | 2 | 15 | 0 | .00 | 123.00 | 1030.00 |

*SECNO .949

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3470 ENCROACHMENT STATIONS= 965.0 1039.0 TYPE= 1 TARGET= 74.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| .949 | 6.48 | 2469.48 | 2469.48 | 2469.43 | 2471.32 | 1.84 | 2.76 | .23 | 2464.00 |
| 2099.0 | 212.4 | 1496.9 | 389.7 | 48.7 | 119.6 | 76.2 | 240.3 | 99.9 | 2464.00 |
| .74 | 4.36 | 12.51 | 5.11 | .050 | .030 | .050 | .000 | 2463.00 | 965.00 |
| .005916 | 440. | 440. | 440. | 0 | 11 | 0 | .00 | 73.89 | 1038.89 |

*SECNO 1.045

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 904.0 1074.0 TYPE= 1 TARGET= 170.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.045 | 5.52 | 2474.52 | 2474.52 | 2474.48 | 2475.57 | 1.06 | 2.96 | .08 | 2470.00 |
| 2099.0 | 465.0 | 1084.7 | 549.3 | 134.0 | 100.4 | 126.3 | 243.9 | 101.3 | 2470.00 |
| .75 | 3.47 | 10.81 | 4.35 | .050 | .030 | .050 | .000 | 2469.00 | 904.00 |
| .005573 | 510. | 510. | 535. | 0 | 12 | 0 | .00 | 170.00 | 1074.00 |

*SECNO 1.148

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 958.0 1035.0 TYPE= 1 TARGET= 77.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.148 | 5.99 | 2480.99 | 2480.99 | 2480.99 | 2482.77 | 1.78 | 3.23 | .22 | 2476.00 |
| 2099.0 | 500.6 | 1434.2 | 164.2 | 91.4 | 115.3 | 37.3 | 247.6 | 102.8 | 2476.00 |
| .77 | 5.48 | 12.44 | 4.40 | .050 | .030 | .050 | .000 | 2475.00 | 958.00 |
| .006543 | 525. | 540. | 540. | 0 | 8 | 0 | .00 | 76.87 | 1034.87 |

*SECNO 1.242
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 947.0 1061.0 TYPE= 1 TARGET= 114.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.242 | 6.07 | 2487.07 | 2487.07 | 2487.07 | 2488.49 | 1.42 | 3.02 | .04 | 2482.00 |
| 2099.0 | 361.7 | 1297.2 | 440.1 | 80.8 | 111.4 | 101.0 | 250.7 | 103.9 | 2482.00 |
| .78 | 4.48 | 11.65 | 4.36 | .050 | .030 | .050 | .000 | 2481.00 | 947.00 |
| .005638 | 500. | 500. | 485. | 0 | 5 | 0 | .00 | 114.00 | 1061.00 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.343
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 972.0 1043.0 TYPE= 1 TARGET= 71.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.343 | 6.96 | 2495.96 | 2495.96 | 2495.96 | 2497.75 | 1.78 | 3.15 | .11 | 2492.00 |
| 2099.0 | 108.7 | 1681.7 | 308.6 | 25.5 | 143.0 | 68.3 | 253.9 | 105.0 | 2492.00 |
| .80 | 4.26 | 11.76 | 4.52 | .050 | .030 | .050 | .000 | 2489.00 | 972.12 |
| .006382 | 530. | 530. | 510. | 0 | 8 | 0 | .00 | 70.44 | 1042.56 |

*SECNO 1.428
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 971.0 1062.0 TYPE= 1 TARGET= 91.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.428 | 5.72 | 2500.72 | 2500.72 | 2500.72 | 2502.27 | 1.54 | 2.91 | .02 | 2496.00 |
| 2099.0 | 208.9 | 1270.9 | 619.2 | 42.4 | 104.4 | 124.0 | 256.4 | 105.8 | 2496.00 |
| .81 | 4.92 | 12.17 | 4.99 | .050 | .030 | .050 | .000 | 2495.00 | 971.00 |
| .006704 | 435. | 450. | 435. | 0 | 15 | 0 | .00 | 90.75 | 1061.75 |

*SECNO 1.525
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 934.0 1031.0 TYPE= 1 TARGET= 97.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.525 | 5.27 | 2506.27 | 2506.27 | 2506.27 | 2507.70 | 1.43 | 3.52 | .01 | 2502.00 |
| 2099.0 | 718.4 | 1154.4 | 226.2 | 139.3 | 95.4 | 45.5 | 259.6 | 106.9 | 2502.00 |
| .83 | 5.16 | 12.11 | 4.97 | .050 | .030 | .050 | .000 | 2501.00 | 934.00 |
| .007492 | 500. | 510. | 460. | 0 | 11 | 0 | .00 | 97.00 | 1031.00 |

*SECNO 1.619
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 968.0 1061.0 TYPE= 1 TARGET= 93.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.619 | 5.09 | 2515.09 | 2515.09 | 2515.09 | 2516.56 | 1.47 | 3.77 | .01 | 2510.80 |
| 2099.0 | 361.5 | 1140.5 | 596.9 | 64.0 | 93.6 | 111.4 | 262.7 | 108.0 | 2510.80 |
| .84 | 5.65 | 12.19 | 5.36 | .050 | .030 | .050 | .000 | 2510.00 | 968.37 |
| .007772 | 460. | 500. | 525. | 0 | 8 | 0 | .00 | 92.39 | 1060.76 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

*SECNO 1.719
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 967.0 1069.0 TYPE= 1 TARGET= 102.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.719 | 4.92 | 2522.92 | 2522.92 | 2522.92 | 2524.28 | 1.36 | 4.04 | .01 | 2519.00 |
| 2099.0 | 297.9 | 1103.5 | 697.6 | 55.8 | 92.8 | 131.7 | 265.9 | 109.1 | 2519.00 |
| .86 | 5.34 | 11.89 | 5.30 | .050 | .030 | .050 | .000 | 2518.00 | 967.00 |
| .007999 | 515. | 525. | 490. | 0 | 8 | 0 | .00 | 101.98 | 1068.98 |

*SECNO 1.802

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 947.0 1015.0 TYPE= 1 TARGET= 68.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.802 | 6.61 | 2529.61 | 2529.61 | 2529.63 | 2531.61 | 2.00 | 2.88 | .19 | 2524.00 |
| 2099.0 | 422.9 | 1623.4 | 52.6 | 86.7 | 128.4 | 14.8 | 268.3 | 109.9 | 2524.00 |
| .87 | 4.88 | 12.64 | 3.55 | .050 | .030 | .050 | .000 | 2523.00 | 947.31 |
| .005860 | 440. | 440. | 350. | 0 | 11 | 0 | .00 | 67.69 | 1015.00 |

*SECNO 1.897

3301 HV CHANGED MORE THAN HVINS

7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 952.0 1045.0 TYPE= 1 TARGET= 93.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.897 | 4.87 | 2538.87 | 2538.87 | 2538.88 | 2540.17 | 1.30 | 3.24 | .07 | 2535.30 |
| 1650.0 | 297.3 | 1025.0 | 327.7 | 63.7 | 93.1 | 71.6 | 270.9 | 110.8 | 2535.30 |
| .89 | 4.67 | 11.01 | 4.58 | .050 | .030 | .050 | .000 | 2534.00 | 952.00 |
| .007390 | 480. | 500. | 545. | 0 | 19 | 0 | .00 | 93.00 | 1045.00 |

*SECNO 1.993
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| SECNO | DEPTH | CWSEL | CRIWS | WSELK | EG | HV | HL | OLOSS | L-BANK ELEV |
| Q | QLOB | QCH | QROB | ALOB | ACH | AROB | VOL | TWA | R-BANK ELEV |
| TIME | VLOB | VCH | VROB | XNL | XNCH | XNR | WTN | ELMIN | SSTA |
| SLOPE | XLOBL | XLCH | XLOBR | ITRIAL | IDC | ICONT | CORAR | TOPWID | ENDST |

3470 ENCROACHMENT STATIONS= 911.0 1034.0 TYPE= 1 TARGET= 123.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 1.993 | 5.05 | 2543.05 | 2543.05 | 2543.07 | 2544.25 | 1.20 | 3.42 | .01 | 2539.00 |
| 1650.0 | 391.3 | 983.2 | 275.6 | 97.1 | 91.1 | 57.7 | 273.6 | 112.0 | 2539.00 |
| .90 | 4.03 | 10.79 | 4.77 | .050 | .030 | .050 | .000 | 2538.00 | 912.13 |
| .006332 | 535. | 510. | 430. | 0 | 8 | 0 | .00 | 121.87 | 1034.00 |

*SECNO 2.094
7185 MINIMUM SPECIFIC ENERGY
3720 CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 976.0 1063.0 TYPE= 1 TARGET= 87.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.094 | 5.30 | 2549.30 | 2549.30 | 2549.29 | 2550.70 | 1.40 | 3.31 | .06 | 2545.00 |
| 1650.0 | 136.3 | 1122.8 | 390.9 | 30.3 | 100.7 | 93.2 | 276.4 | 113.3 | 2545.00 |
| .92 | 4.50 | 11.14 | 4.19 | .050 | .030 | .050 | .000 | 2544.00 | 976.43 |
| .006293 | 495. | 530. | 530. | 0 | 8 | 0 | .00 | 86.41 | 1062.84 |

*SECNO 2.183
[illegible] MINIMUM SPECIFIC ENERGY
[illegible] CRITICAL DEPTH ASSUMED

3470 ENCROACHMENT STATIONS= 966.0 1027.0 TYPE= 1 TARGET= 61.000

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.183 | 4.76 | 2552.76 | 2552.76 | 2552.75 | 2554.40 | 1.64 | 3.28 | .07 | 2548.70 |
| 1650.0 | 300.9 | 1034.1 | 315.1 | 55.0 | 84.8 | 52.6 | 278.6 | 114.0 | 2548.50 |
| .93 | 5.47 | 12.20 | 5.99 | .050 | .030 | .050 | .000 | 2548.00 | 966.18 |
| .008274 | 470. | 470. | 410. | 0 | 11 | 0 | .00 | 60.82 | 1027.00 |

THIS RUN EXECUTED 28OCT92 16:44:01

**********
HEC-2 WATER SURFACE PROFILES

Version 4.6.2; May 1991
**********

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

AB: YUCCA FLAT WASH

SUMMARY PRINTOUT TABLE 150

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 2.435 | .00 | .00 | .00 | 2303.50 | 6943.00 | 2309.87 | 2309.87 | 2311.91 | 81.13 | 14.89 | 739.77 | 770.81 |
| * | 2.435 | .00 | .00 | .00 | 2303.50 | 6943.00 | 2309.91 | 2309.80 | 2312.10 | 83.74 | 15.19 | 701.30 | 758.71 |
| * | 2.539 | 550.00 | .00 | .00 | 2309.00 | 6943.00 | 2315.51 | 2315.51 | 2316.75 | 79.25 | 9.41 | 847.02 | 779.93 |
| * | 2.539 | 550.00 | .00 | .00 | 2309.00 | 6943.00 | 2315.51 | 2315.51 | 2316.75 | 79.90 | 9.43 | 843.65 | 776.75 |
| | .191 | 490.00 | .00 | .00 | 2317.50 | 5152.00 | 2322.35 | 2322.35 | 2323.22 | 128.40 | 10.09 | 873.17 | 454.68 |
| | .191 | 490.00 | .00 | .00 | 2317.50 | 5152.00 | 2322.35 | 2322.35 | 2323.22 | 128.48 | 10.09 | 872.91 | 454.53 |
| * | .290 | 520.00 | .00 | .00 | 2325.00 | 5152.00 | 2328.76 | 2328.76 | 2329.79 | 119.27 | 11.24 | 745.50 | 471.75 |
| * | .290 | 520.00 | .00 | .00 | 2325.00 | 5152.00 | 2328.76 | 2328.76 | 2329.79 | 119.23 | 11.24 | 745.59 | 471.83 |
| * | .390 | 530.00 | .00 | .00 | 2332.00 | 5152.00 | 2336.34 | 2336.34 | 2337.04 | 105.49 | 11.31 | 1037.17 | 501.61 |
| * | .390 | 530.00 | .00 | .00 | 2332.00 | 5152.00 | 2336.87 | 2336.87 | 2337.87 | 102.07 | 12.28 | 848.91 | 509.95 |
| * | .477 | 460.00 | .00 | .00 | 2341.00 | 5152.00 | 2343.25 | 2343.25 | 2344.00 | 219.67 | 10.72 | 800.32 | 347.61 |
| * | .477 | 460.00 | .00 | .00 | 2341.00 | 5152.00 | 2343.52 | 2343.52 | 2344.46 | 209.79 | 11.49 | 716.37 | 355.70 |
| * | .578 | 530.00 | .00 | .00 | 2345.50 | 5152.00 | 2351.79 | 2351.79 | 2352.72 | 74.28 | 11.31 | 962.22 | 597.79 |
| * | .578 | 530.00 | .00 | .00 | 2345.50 | 5152.00 | 2351.96 | 2351.96 | 2353.06 | 77.03 | 11.82 | 843.09 | 586.99 |
| * | .697 | 630.00 | .00 | .00 | 2353.50 | 5152.00 | 2358.84 | 2358.84 | 2359.74 | 61.46 | 10.78 | 998.02 | 657.17 |
| * | .697 | 630.00 | .00 | .00 | 2353.50 | 5152.00 | 2359.07 | 2359.07 | 2360.55 | 78.49 | 12.56 | 683.82 | 581.54 |
| * | .788 | 480.00 | .00 | .00 | 2359.00 | 5152.00 | 2364.94 | 2364.94 | 2366.24 | 60.05 | 11.81 | 773.60 | 664.85 |
| * | .788 | 480.00 | .00 | .00 | 2359.00 | 5152.00 | 2364.95 | 2364.95 | 2366.67 | 71.92 | 12.93 | 624.72 | 607.51 |
| * | .883 | 500.00 | .00 | .00 | 2364.50 | 5152.00 | 2370.66 | 2370.66 | 2372.36 | 65.87 | 12.97 | 606.49 | 634.81 |
| * | .883 | 500.00 | .00 | .00 | 2364.50 | 5152.00 | 2370.52 | 2370.52 | 2372.99 | 89.36 | 14.85 | 472.45 | 545.02 |
| * | .972 | 470.00 | .00 | .00 | 2369.50 | 5152.00 | 2375.54 | 2375.54 | 2377.40 | 70.93 | 13.42 | 586.07 | 611.73 |
| | .972 | 470.00 | .00 | .00 | 2369.50 | 5152.00 | 2375.53 | 2375.53 | 2377.40 | 71.15 | 13.44 | 585.38 | 610.76 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 1.070 | 520.00 | .00 | .00 | 2375.00 | 5152.00 | 2381.89 | 2381.89 | 2384.10 | 66.94 | 13.42 | 509.53 | 629.72 |
| * | 1.070 | 520.00 | .00 | .00 | 2375.00 | 5152.00 | 2381.83 | 2381.83 | 2384.46 | 77.01 | 14.30 | 448.64 | 587.08 |
| | 1.163 | 490.00 | .00 | .00 | 2380.00 | 5152.00 | 2385.75 | 2385.11 | 2386.99 | 51.54 | 11.42 | 708.65 | 717.61 |
| | 1.163 | 490.00 | .00 | .00 | 2380.00 | 5152.00 | 2386.12 | 2385.18 | 2387.45 | 47.54 | 11.43 | 661.92 | 747.22 |
| * | 1.239 | 400.00 | .00 | .00 | 2383.00 | 5152.00 | 2390.38 | 2390.38 | 2392.39 | 55.07 | 13.37 | 585.92 | 694.26 |
| * | 1.239 | 400.00 | .00 | .00 | 2383.00 | 5152.00 | 2390.27 | 2390.27 | 2392.46 | 60.01 | 13.81 | 548.59 | 665.06 |
| * | 1.367 | 680.00 | .00 | .00 | 2388.50 | 5152.00 | 2394.92 | 2394.92 | 2395.82 | 45.06 | 10.34 | 1033.36 | 767.50 |
| * | 1.367 | 680.00 | .00 | .00 | 2388.50 | 5152.00 | 2394.93 | 2394.93 | 2396.20 | 56.91 | 11.63 | 812.74 | 682.93 |
| * | 1.462 | 500.00 | .00 | .00 | 2395.50 | 5152.00 | 2401.43 | 2401.43 | 2402.90 | 71.07 | 12.58 | 690.27 | 611.12 |
| * | 1.462 | 500.00 | .00 | .00 | 2395.50 | 5152.00 | 2401.37 | 2401.37 | 2403.01 | 78.14 | 13.09 | 636.82 | 582.83 |
| * | 1.551 | 470.00 | .00 | .00 | 2402.00 | 5152.00 | 2406.92 | 2406.92 | 2408.34 | 94.72 | 12.71 | 654.53 | 529.37 |
| * | 1.551 | 470.00 | .00 | .00 | 2402.00 | 5152.00 | 2407.07 | 2407.07 | 2408.97 | 107.85 | 13.88 | 542.43 | 496.09 |
| * | 1.646 | 500.00 | .00 | .00 | 2405.00 | 5152.00 | 2412.64 | 2412.64 | 2414.35 | 49.14 | 12.19 | 653.03 | 734.97 |
| * | 1.646 | 500.00 | .00 | .00 | 2405.00 | 5152.00 | 2412.47 | 2412.47 | 2414.39 | 55.78 | 12.77 | 598.79 | 689.84 |
| | 1.718 | 380.00 | .00 | .00 | 2409.00 | 5152.00 | 2415.39 | 2413.76 | 2415.86 | 27.96 | 8.52 | 1097.31 | 974.25 |
| * | 1.718 | 380.00 | .00 | .00 | 2409.00 | 5152.00 | 2415.49 | 2413.77 | 2415.94 | 26.18 | 8.33 | 1114.25 | 1006.98 |
| | 1.808 | 475.00 | .00 | .00 | 2417.00 | 2085.00 | 2420.33 | 2420.33 | 2420.98 | 97.03 | 9.75 | 430.94 | 211.67 |
| | 1.808 | 475.00 | .00 | .00 | 2417.00 | 2085.00 | 2420.33 | 2420.33 | 2420.98 | 97.26 | 9.76 | 430.53 | 211.42 |
| * | 1.905 | 510.00 | .00 | .00 | 2422.00 | 2085.00 | 2425.82 | 2425.82 | 2426.60 | 84.07 | 10.09 | 405.42 | 227.39 |
| * | 1.905 | 510.00 | .00 | .00 | 2422.00 | 2085.00 | 2425.82 | 2425.82 | 2426.60 | 84.14 | 10.09 | 405.30 | 227.30 |
| * | 2.003 | 520.00 | .00 | .00 | 2429.00 | 2085.00 | 2432.76 | 2432.76 | 2433.43 | 74.16 | 9.33 | 463.17 | 242.12 |
| * | 2.003 | 520.00 | .00 | .00 | 2429.00 | 2085.00 | 2432.79 | 2432.79 | 2433.52 | 77.52 | 9.59 | 430.38 | 236.81 |
| * | 2.091 | 460.00 | .00 | .00 | 2434.00 | 2085.00 | 2437.00 | 2437.00 | 2437.64 | 79.78 | 9.20 | 447.07 | 233.43 |
| * | 2.091 | 460.00 | .00 | .00 | 2434.00 | 2085.00 | 2437.49 | 2437.49 | 2438.35 | 74.68 | 9.84 | 385.41 | 241.28 |
| * | 2.172 | 430.00 | .00 | .00 | 2438.00 | 2085.00 | 2442.03 | 2442.03 | 2442.72 | 78.69 | 10.15 | 442.59 | 235.05 |
| * | 2.172 | 430.00 | .00 | .00 | 2438.00 | 2085.00 | 2442.34 | 2442.34 | 2443.20 | 77.80 | 10.68 | 393.60 | 236.39 |
| * | 2.284 | 590.00 | .00 | .00 | 2447.00 | 2085.00 | 2450.57 | 2450.57 | 2451.34 | 74.24 | 9.75 | 415.01 | 241.98 |
| * | 2.284 | 590.00 | .00 | .00 | 2447.00 | 2085.00 | 2450.55 | 2450.55 | 2451.42 | 81.60 | 10.18 | 376.04 | 230.81 |
| * | 2.384 | 530.00 | .00 | .00 | 2453.00 | 2085.00 | 2456.65 | 2456.65 | 2457.45 | 82.77 | 10.69 | 400.26 | 229.17 |
| * | 2.384 | 530.00 | .00 | .00 | 2453.00 | 2085.00 | 2456.67 | 2456.67 | 2457.54 | 86.69 | 10.97 | 375.73 | 223.94 |
| * | 2.477 | 490.00 | .00 | .00 | 2457.00 | 2085.00 | 2462.33 | 2462.33 | 2463.10 | 43.79 | 9.34 | 459.87 | 315.07 |
| * | 2.477 | 490.00 | .00 | .00 | 2457.00 | 2085.00 | 2462.33 | 2462.33 | 2463.10 | 43.78 | 9.34 | 459.95 | 315.12 |
| * | 2.562 | 450.00 | .00 | .00 | 2465.00 | 2085.00 | 2467.37 | 2467.37 | 2468.14 | 136.47 | 10.30 | 350.23 | 178.48 |
| | 2.562 | 450.00 | .00 | .00 | 2465.00 | 2085.00 | 2467.38 | 2467.38 | 2468.14 | 136.23 | 10.29 | 350.46 | 178.64 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 2.672 | 580.00 | .00 | .00 | 2472.00 | 2085.00 | 2475.33 | 2475.33 | 2476.15 | 110.27 | 10.40 | 356.38 | 198.56 |
| * | 2.672 | 580.00 | .00 | .00 | 2472.00 | 2085.00 | 2475.34 | 2475.34 | 2476.15 | 109.79 | 10.38 | 356.97 | 198.99 |
| | 2.761 | 470.00 | .00 | .00 | 2478.00 | 2085.00 | 2480.33 | 2480.27 | 2480.94 | 115.26 | 9.16 | 403.29 | 194.21 |
| | 2.761 | 470.00 | .00 | .00 | 2478.00 | 2085.00 | 2480.33 | 2480.27 | 2480.94 | 115.81 | 9.18 | 402.61 | 193.74 |
| * | 2.857 | 510.00 | .00 | .00 | 2486.00 | 2085.00 | 2488.22 | 2488.22 | 2488.77 | 122.18 | 9.32 | 457.59 | 188.63 |
| * | 2.857 | 510.00 | .00 | .00 | 2486.00 | 2085.00 | 2488.22 | 2488.22 | 2488.77 | 121.13 | 9.29 | 458.90 | 189.45 |
| * | 2.965 | 570.00 | .00 | .00 | 2495.00 | 2085.00 | 2496.72 | 2496.72 | 2497.28 | 177.20 | 9.45 | 408.15 | 156.63 |
| * | 2.965 | 570.00 | .00 | .00 | 2495.00 | 2085.00 | 2496.72 | 2496.72 | 2497.28 | 177.87 | 9.47 | 407.66 | 156.34 |
| | -1.718 | 380.00 | .00 | .00 | 2409.00 | 5152.00 | 2415.39 | .00 | 2415.86 | 27.95 | 8.52 | 1097.51 | 974.51 |
| | -1.718 | 380.00 | .00 | .00 | 2409.00 | 5152.00 | 2415.49 | .00 | 2415.94 | 26.03 | 8.32 | 1116.34 | 1009.88 |
| * | .098 | 520.00 | .00 | .00 | 2415.00 | 2099.00 | 2418.78 | 2418.78 | 2419.60 | 97.81 | 9.46 | 356.05 | 212.23 |
| * | .098 | 520.00 | .00 | .00 | 2415.00 | 2099.00 | 2418.77 | 2418.77 | 2419.60 | 98.42 | 9.48 | 355.13 | 211.57 |
| * | .190 | 490.00 | .00 | .00 | 2418.00 | 2099.00 | 2423.87 | 2423.87 | 2424.71 | 44.01 | 9.70 | 450.72 | 316.41 |
| * | .190 | 490.00 | .00 | .00 | 2418.00 | 2099.00 | 2423.86 | 2423.86 | 2425.48 | 68.22 | 12.06 | 263.34 | 254.13 |
| * | .301 | 580.00 | .00 | .00 | 2427.00 | 2099.00 | 2431.28 | 2431.28 | 2431.98 | 68.14 | 9.89 | 457.20 | 254.27 |
| * | .301 | 580.00 | .00 | .00 | 2427.00 | 2099.00 | 2431.48 | 2431.48 | 2432.69 | 87.59 | 11.62 | 308.26 | 224.28 |
| | .384 | 440.00 | .00 | .00 | 2429.00 | 2099.00 | 2434.00 | 2433.96 | 2435.25 | 73.21 | 11.52 | 299.96 | 245.31 |
| | .384 | 440.00 | .00 | .00 | 2429.00 | 2099.00 | 2434.55 | 2433.96 | 2435.53 | 48.84 | 10.16 | 328.15 | 300.36 |
| * | .473 | 470.00 | .00 | .00 | 2437.00 | 2099.00 | 2440.65 | 2440.65 | 2441.47 | 90.57 | 10.12 | 379.55 | 220.56 |
| * | .473 | 470.00 | .00 | .00 | 2437.00 | 2099.00 | 2440.86 | 2440.86 | 2442.16 | 109.19 | 11.58 | 272.51 | 200.87 |
| * | .581 | 570.00 | .00 | .00 | 2443.00 | 2099.00 | 2448.41 | 2448.41 | 2449.07 | 43.36 | 9.39 | 534.09 | 318.76 |
| * | .581 | 570.00 | .00 | .00 | 2443.00 | 2099.00 | 2448.60 | 2448.60 | 2449.91 | 63.17 | 11.62 | 313.91 | 264.09 |
| * | .669 | 460.00 | .00 | .00 | 2448.00 | 2099.00 | 2452.18 | 2452.18 | 2452.81 | 69.31 | 9.79 | 470.92 | 252.13 |
| * | .669 | 460.00 | .00 | .00 | 2448.00 | 2099.00 | 2452.68 | 2452.68 | 2453.79 | 79.49 | 11.42 | 327.17 | 235.43 |
| * | .765 | 510.00 | .00 | .00 | 2453.00 | 2099.00 | 2458.31 | 2458.31 | 2459.17 | 55.54 | 10.84 | 422.94 | 281.64 |
| * | .765 | 510.00 | .00 | .00 | 2453.00 | 2099.00 | 2458.41 | 2458.41 | 2460.19 | 85.78 | 13.65 | 239.28 | 226.63 |
| * | .866 | 530.00 | .00 | .00 | 2458.00 | 2099.00 | 2462.98 | 2462.98 | 2464.20 | 78.85 | 11.91 | 313.45 | 236.38 |
| | .866 | 530.00 | .00 | .00 | 2458.00 | 2099.00 | 2463.14 | 2462.98 | 2464.20 | 66.83 | 11.22 | 332.94 | 256.76 |
| * | .949 | 440.00 | .00 | .00 | 2463.00 | 2099.00 | 2469.43 | 2469.43 | 2471.32 | 61.41 | 12.67 | 240.67 | 267.85 |
| * | .949 | 440.00 | .00 | .00 | 2463.00 | 2099.00 | 2469.48 | 2469.48 | 2471.32 | 59.16 | 12.51 | 244.56 | 272.91 |
| * | 1.045 | 510.00 | .00 | .00 | 2469.00 | 2099.00 | 2474.48 | 2474.48 | 2475.58 | 57.86 | 10.96 | 354.74 | 275.95 |
| * | 1.045 | 510.00 | .00 | .00 | 2469.00 | 2099.00 | 2474.52 | 2474.52 | 2475.57 | 55.73 | 10.81 | 360.67 | 281.16 |
| * | 1.148 | 540.00 | .00 | .00 | 2475.00 | 2099.00 | 2480.99 | 2480.99 | 2482.77 | 65.53 | 12.44 | 243.90 | 259.30 |
| | 1.148 | 540.00 | .00 | .00 | 2475.00 | 2099.00 | 2480.99 | 2480.99 | 2482.77 | 65.43 | 12.44 | 244.04 | 259.50 |

| | SECNO | XLCH | ELTRD | ELLC | ELMIN | Q | CWSEL | CRIWS | EG | 10*KS | VCH | AREA | .01K |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| * | 1.242 | 500.00 | .00 | .00 | 2481.00 | 2099.00 | 2487.07 | 2487.07 | 2488.49 | 56.32 | 11.64 | 293.29 | 279.69 |
| * | 1.242 | 500.00 | .00 | .00 | 2481.00 | 2099.00 | 2487.07 | 2487.07 | 2488.49 | 56.38 | 11.65 | 293.15 | 279.55 |
| * | 1.343 | 530.00 | .00 | .00 | 2489.00 | 2099.00 | 2495.96 | 2495.96 | 2497.75 | 63.89 | 11.76 | 236.74 | 262.60 |
| * | 1.343 | 530.00 | .00 | .00 | 2489.00 | 2099.00 | 2495.96 | 2495.96 | 2497.75 | 63.82 | 11.76 | 236.85 | 262.75 |
| * | 1.428 | 450.00 | .00 | .00 | 2495.00 | 2099.00 | 2500.72 | 2500.72 | 2502.27 | 67.24 | 12.18 | 270.61 | 255.97 |
| * | 1.428 | 450.00 | .00 | .00 | 2495.00 | 2099.00 | 2500.72 | 2500.72 | 2502.27 | 67.04 | 12.17 | 270.90 | 256.35 |
| * | 1.525 | 510.00 | .00 | .00 | 2501.00 | 2099.00 | 2506.27 | 2506.27 | 2507.70 | 74.69 | 12.09 | 280.57 | 242.88 |
| * | 1.525 | 510.00 | .00 | .00 | 2501.00 | 2099.00 | 2506.27 | 2506.27 | 2507.70 | 74.92 | 12.11 | 280.21 | 242.50 |
| * | 1.619 | 500.00 | .00 | .00 | 2510.00 | 2099.00 | 2515.09 | 2515.09 | 2516.56 | 77.82 | 12.19 | 268.83 | 237.94 |
| * | 1.619 | 500.00 | .00 | .00 | 2510.00 | 2099.00 | 2515.09 | 2515.09 | 2516.56 | 77.72 | 12.19 | 268.97 | 238.10 |
| * | 1.719 | 525.00 | .00 | .00 | 2518.00 | 2099.00 | 2522.92 | 2522.92 | 2524.28 | 79.91 | 11.89 | 280.40 | 234.81 |
| * | 1.719 | 525.00 | .00 | .00 | 2518.00 | 2099.00 | 2522.92 | 2522.92 | 2524.28 | 79.99 | 11.89 | 280.29 | 234.70 |
| * | 1.802 | 440.00 | .00 | .00 | 2523.00 | 2099.00 | 2529.63 | 2529.63 | 2531.61 | 57.94 | 12.59 | 230.96 | 275.76 |
| * | 1.802 | 440.00 | .00 | .00 | 2523.00 | 2099.00 | 2529.61 | 2529.61 | 2531.61 | 58.60 | 12.64 | 229.91 | 274.20 |
| * | 1.897 | 500.00 | .00 | .00 | 2534.00 | 1650.00 | 2538.88 | 2538.88 | 2540.17 | 73.75 | 11.01 | 228.58 | 192.13 |
| * | 1.897 | 500.00 | .00 | .00 | 2534.00 | 1650.00 | 2538.87 | 2538.87 | 2540.17 | 73.90 | 11.01 | 228.38 | 191.94 |
| | 1.993 | 510.00 | .00 | .00 | 2538.00 | 1650.00 | 2543.07 | 2543.07 | 2544.25 | 62.41 | 10.74 | 247.70 | 208.86 |
| | 1.993 | 510.00 | .00 | .00 | 2538.00 | 1650.00 | 2543.05 | 2543.05 | 2544.25 | 63.32 | 10.79 | 245.95 | 207.36 |
| * | 2.094 | 530.00 | .00 | .00 | 2544.00 | 1650.00 | 2549.29 | 2549.29 | 2550.70 | 63.28 | 11.17 | 223.71 | 207.41 |
| * | 2.094 | 530.00 | .00 | .00 | 2544.00 | 1650.00 | 2549.30 | 2549.30 | 2550.70 | 62.93 | 11.14 | 224.24 | 208.00 |
| * | 2.183 | 470.00 | .00 | .00 | 2548.00 | 1650.00 | 2552.75 | 2552.75 | 2554.40 | 83.58 | 12.24 | 191.72 | 180.48 |
| * | 2.183 | 470.00 | .00 | .00 | 2548.00 | 1650.00 | 2552.76 | 2552.76 | 2554.40 | 82.74 | 12.20 | 192.40 | 181.39 |

UCCA FLAT WASH

SUMMARY PRINTOUT TABLE 150

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 2.435 | 6943.00 | 2309.87 | .00 | .00 | .00 | 180.52 | .00 |
| * | 2.435 | 6943.00 | 2309.91 | .04 | .00 | .04 | 144.31 | .00 |
| * | 2.539 | 6943.00 | 2315.51 | .00 | 5.64 | .00 | 395.38 | 550.00 |
| * | 2.539 | 6943.00 | 2315.51 | -.01 | 5.59 | -.01 | 394.83 | 550.00 |
| * | .191 | 5152.00 | 2322.35 | .00 | 6.84 | .00 | 502.63 | 490.00 |
| * | .191 | 5152.00 | 2322.35 | .00 | 6.84 | .00 | 501.27 | 490.00 |
| * | .290 | 5152.00 | 2328.76 | .00 | 6.41 | .00 | 388.95 | 520.00 |
| * | .290 | 5152.00 | 2328.76 | .00 | 6.41 | .00 | 388.77 | 520.00 |
| * | .390 | 5152.00 | 2336.34 | .00 | 7.58 | .00 | 689.13 | 530.00 |
| * | .390 | 5152.00 | 2336.87 | .54 | 8.11 | .54 | 379.00 | 530.00 |
| * | .477 | 5152.00 | 2343.25 | .00 | 6.92 | .00 | 541.32 | 460.00 |
| * | .477 | 5152.00 | 2343.52 | .26 | 6.65 | .26 | 390.00 | 460.00 |
| | .578 | 5152.00 | 2351.79 | .00 | 8.53 | .00 | 478.93 | 530.00 |
| | .578 | 5152.00 | 2351.96 | .17 | 8.44 | .17 | 341.00 | 530.00 |
| * | .697 | 5152.00 | 2358.84 | .00 | 7.06 | .00 | 519.93 | 630.00 |
| * | .697 | 5152.00 | 2359.07 | .22 | 7.11 | .22 | 213.00 | 630.00 |
| * | .788 | 5152.00 | 2364.94 | .00 | 6.10 | .00 | 283.97 | 480.00 |
| * | .788 | 5152.00 | 2364.95 | .01 | 5.88 | .01 | 174.00 | 480.00 |
| * | .883 | 5152.00 | 2370.66 | .00 | 5.72 | .00 | 231.01 | 500.00 |
| * | .883 | 5152.00 | 2370.52 | -.15 | 5.57 | -.15 | 94.00 | 500.00 |
| * | .972 | 5152.00 | 2375.54 | .00 | 4.87 | .00 | 157.57 | 470.00 |
| * | .972 | 5152.00 | 2375.53 | .00 | 5.02 | .00 | 157.50 | 470.00 |
| * | 1.070 | 5152.00 | 2381.89 | .00 | 6.35 | .00 | 135.24 | 520.00 |
| * | 1.070 | 5152.00 | 2381.83 | -.06 | 6.30 | -.06 | 89.31 | 520.00 |
| | 1.163 | 5152.00 | 2385.75 | .00 | 3.85 | .00 | 203.77 | 490.00 |
| | 1.163 | 5152.00 | 2386.12 | .37 | 4.29 | .37 | 130.00 | 490.00 |
| * | 1.239 | 5152.00 | 2390.38 | .00 | 4.63 | .00 | 160.62 | 400.00 |
| * | 1.239 | 5152.00 | 2390.27 | -.11 | 4.15 | -.11 | 128.59 | 400.00 |
| * | 1.367 | 5152.00 | 2394.92 | .00 | 4.54 | .00 | 510.25 | 680.00 |
| * | 1.367 | 5152.00 | 2394.93 | .01 | 4.66 | .01 | 321.00 | 680.00 |
| | 1.462 | 5152.00 | 2401.43 | .00 | 6.51 | .00 | 239.49 | 500.00 |
| * | 1.462 | 5152.00 | 2401.37 | -.06 | 6.44 | -.06 | 186.53 | 500.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 1.551 | 5152.00 | 2406.92 | .00 | 5.49 | .00 | 238.00 | 470.00 |
| * | 1.551 | 5152.00 | 2407.07 | .15 | 5.71 | .15 | 144.00 | 470.00 |
| * | 1.646 | 5152.00 | 2412.64 | .00 | 5.72 | .00 | 229.83 | 500.00 |
| * | 1.646 | 5152.00 | 2412.47 | -.17 | 5.40 | -.17 | 163.00 | 500.00 |
| | 1.718 | 5152.00 | 2415.39 | .00 | 2.75 | .00 | 278.19 | 380.00 |
| * | 1.718 | 5152.00 | 2415.49 | .10 | 3.02 | .10 | 260.00 | 380.00 |
| * | 1.808 | 2085.00 | 2420.33 | .00 | 4.94 | .00 | 328.34 | 475.00 |
| * | 1.808 | 2085.00 | 2420.33 | .00 | 4.84 | .00 | 328.33 | 475.00 |
| * | 1.905 | 2085.00 | 2425.82 | .00 | 5.49 | .00 | 244.84 | 510.00 |
| * | 1.905 | 2085.00 | 2425.82 | .00 | 5.49 | .00 | 244.83 | 510.00 |
| * | 2.003 | 2085.00 | 2432.76 | .00 | 6.94 | .00 | 334.08 | 520.00 |
| * | 2.003 | 2085.00 | 2432.79 | .03 | 6.97 | .03 | 268.47 | 520.00 |
| * | 2.091 | 2085.00 | 2437.00 | .00 | 4.23 | .00 | 356.06 | 460.00 |
| * | 2.091 | 2085.00 | 2437.49 | .49 | 4.70 | .49 | 215.00 | 460.00 |
| * | 2.172 | 2085.00 | 2442.03 | .00 | 5.03 | .00 | 310.00 | 430.00 |
| * | 2.172 | 2085.00 | 2442.34 | .31 | 4.85 | .31 | 219.00 | 430.00 |
| | 2.284 | 2085.00 | 2450.57 | .00 | 8.54 | .00 | 255.99 | 590.00 |
| | 2.284 | 2085.00 | 2450.55 | -.02 | 8.21 | -.02 | 195.84 | 590.00 |
| * | 2.384 | 2085.00 | 2456.65 | .00 | 6.08 | .00 | 233.06 | 530.00 |
| * | 2.384 | 2085.00 | 2456.67 | .02 | 6.12 | .02 | 199.35 | 530.00 |
| * | 2.477 | 2085.00 | 2462.33 | .00 | 5.68 | .00 | 326.36 | 490.00 |
| * | 2.477 | 2085.00 | 2462.33 | .00 | 5.66 | .00 | 326.39 | 490.00 |
| * | 2.562 | 2085.00 | 2467.37 | .00 | 5.05 | .00 | 229.89 | 450.00 |
| * | 2.562 | 2085.00 | 2467.38 | .00 | 5.05 | .00 | 229.97 | 450.00 |
| * | 2.672 | 2085.00 | 2475.33 | .00 | 7.96 | .00 | 220.24 | 580.00 |
| * | 2.672 | 2085.00 | 2475.34 | .00 | 7.96 | .00 | 220.36 | 580.00 |
| | 2.761 | 2085.00 | 2480.33 | .00 | 4.99 | .00 | 279.54 | 470.00 |
| | 2.761 | 2085.00 | 2480.33 | .00 | 4.99 | .00 | 279.49 | 470.00 |
| * | 2.857 | 2085.00 | 2488.22 | .00 | 7.89 | .00 | 355.50 | 510.00 |
| * | 2.857 | 2085.00 | 2488.22 | .00 | 7.90 | .00 | 355.59 | 510.00 |
| * | 2.965 | 2085.00 | 2496.72 | .00 | 8.50 | .00 | 330.75 | 570.00 |
| * | 2.965 | 2085.00 | 2496.72 | .00 | 8.49 | .00 | 330.72 | 570.00 |
| | -1.718 | 5152.00 | 2415.39 | .00 | -81.33 | .00 | 278.20 | 380.00 |
| | -1.718 | 5152.00 | 2415.49 | .10 | -81.22 | .10 | 260.00 | 380.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | .098 | 2099.00 | 2418.78 | .00 | 3.39 | .00 | 233.52 | 520.00 |
| * | .098 | 2099.00 | 2418.77 | .00 | 3.28 | .00 | 233.18 | 520.00 |
| * | .190 | 2099.00 | 2423.87 | .00 | 5.10 | .00 | 263.92 | 490.00 |
| * | .190 | 2099.00 | 2423.86 | -.01 | 5.09 | -.01 | 81.00 | 490.00 |
| * | .301 | 2099.00 | 2431.28 | .00 | 7.40 | .00 | 294.80 | 580.00 |
| * | .301 | 2099.00 | 2431.48 | .21 | 7.62 | .21 | 118.00 | 580.00 |
| | .384 | 2099.00 | 2434.00 | .00 | 2.73 | .00 | 116.60 | 440.00 |
| | .384 | 2099.00 | 2434.55 | .55 | 3.07 | .55 | 93.00 | 440.00 |
| * | .473 | 2099.00 | 2440.65 | .00 | 6.65 | .00 | 233.36 | 470.00 |
| * | .473 | 2099.00 | 2440.86 | .20 | 6.31 | .20 | 102.00 | 470.00 |
| * | .581 | 2099.00 | 2448.41 | .00 | 7.75 | .00 | 351.96 | 570.00 |
| * | .581 | 2099.00 | 2448.60 | .19 | 7.74 | .19 | 112.00 | 570.00 |
| * | .669 | 2099.00 | 2452.18 | .00 | 3.77 | .00 | 300.26 | 460.00 |
| * | .669 | 2099.00 | 2452.68 | .50 | 4.08 | .50 | 129.00 | 460.00 |
| * | .765 | 2099.00 | 2458.31 | .00 | 6.14 | .00 | 271.19 | 510.00 |
| * | .765 | 2099.00 | 2458.41 | .10 | 5.74 | .10 | 67.00 | 510.00 |
| | .866 | 2099.00 | 2462.98 | .00 | 4.67 | .00 | 123.08 | 530.00 |
| | .866 | 2099.00 | 2463.14 | .16 | 4.73 | .16 | 123.00 | 530.00 |
| * | .949 | 2099.00 | 2469.43 | .00 | 6.44 | .00 | 73.14 | 440.00 |
| * | .949 | 2099.00 | 2469.48 | .05 | 6.34 | .05 | 73.89 | 440.00 |
| * | 1.045 | 2099.00 | 2474.48 | .00 | 5.06 | .00 | 169.89 | 510.00 |
| * | 1.045 | 2099.00 | 2474.52 | .03 | 5.04 | .03 | 170.00 | 510.00 |
| * | 1.148 | 2099.00 | 2480.99 | .00 | 6.51 | .00 | 77.11 | 540.00 |
| * | 1.148 | 2099.00 | 2480.99 | .00 | 6.47 | .00 | 76.87 | 540.00 |
| * | 1.242 | 2099.00 | 2487.07 | .00 | 6.08 | .00 | 114.35 | 500.00 |
| * | 1.242 | 2099.00 | 2487.07 | .00 | 6.08 | .00 | 114.00 | 500.00 |
| * | 1.343 | 2099.00 | 2495.96 | .00 | 8.89 | .00 | 70.43 | 530.00 |
| * | 1.343 | 2099.00 | 2495.96 | .00 | 8.90 | .00 | 70.44 | 530.00 |
| * | 1.428 | 2099.00 | 2500.72 | .00 | 4.76 | .00 | 91.23 | 450.00 |
| * | 1.428 | 2099.00 | 2500.72 | .00 | 4.76 | .00 | 90.75 | 450.00 |
| * | 1.525 | 2099.00 | 2506.27 | .00 | 5.55 | .00 | 97.72 | 510.00 |
| * | 1.525 | 2099.00 | 2506.27 | .00 | 5.55 | .00 | 97.00 | 510.00 |
| * | 1.619 | 2099.00 | 2515.09 | .00 | 8.82 | .00 | 92.38 | 500.00 |
| | 1.619 | 2099.00 | 2515.09 | .00 | 8.82 | .00 | 92.39 | 500.00 |

| | SECNO | Q | CWSEL | DIFWSP | DIFWSX | DIFKWS | TOPWID | XLCH |
|---|---|---|---|---|---|---|---|---|
| * | 1.719 | 2099.00 | 2522.92 | .00 | 7.83 | .00 | 102.26 | 525.00 |
| * | 1.719 | 2099.00 | 2522.92 | .00 | 7.83 | .00 | 101.98 | 525.00 |
| * | 1.802 | 2099.00 | 2529.63 | .00 | 6.71 | .00 | 68.18 | 440.00 |
| * | 1.802 | 2099.00 | 2529.61 | -.01 | 6.70 | -.01 | 67.69 | 440.00 |
| * | 1.897 | 1650.00 | 2538.88 | .00 | 9.25 | .00 | 93.49 | 500.00 |
| * | 1.897 | 1650.00 | 2538.87 | .00 | 9.26 | .00 | 93.00 | 500.00 |
| * | 1.993 | 1650.00 | 2543.07 | .00 | 4.19 | .00 | 123.10 | 510.00 |
| * | 1.993 | 1650.00 | 2543.05 | -.01 | 4.18 | -.01 | 121.87 | 510.00 |
| * | 2.094 | 1650.00 | 2549.29 | .00 | 6.22 | .00 | 86.31 | 530.00 |
| * | 2.094 | 1650.00 | 2549.30 | .01 | 6.24 | .01 | 86.41 | 530.00 |
| * | 2.183 | 1650.00 | 2552.75 | .00 | 3.46 | .00 | 61.11 | 470.00 |
| * | 2.183 | 1650.00 | 2552.76 | .01 | 3.47 | .01 | 60.82 | 470.00 |

SUMMARY OF ERRORS AND SPECIAL NOTES

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CAUTION SECNO=     2.435  PROFILE=  1  CRITICAL DEPTH ASSUMED
NOTE    SECNO=     2.435  PROFILE=  1  WSEL BASED ON X5 CARD
NOTE    SECNO=     2.435  PROFILE=  2  WSEL BASED ON X5 CARD

CAUTION SECNO=     2.539  PROFILE=  1  CRITICAL DEPTH ASSUMED
CAUTION SECNO=     2.539  PROFILE=  1  MINIMUM SPECIFIC ENERGY
CAUTION SECNO=     2.539  PROFILE=  2  CRITICAL DEPTH ASSUMED
CAUTION SECNO=     2.539  PROFILE=  2  MINIMUM SPECIFIC ENERGY

CAUTION SECNO=      .191  PROFILE=  1  CRITICAL DEPTH ASSUMED
CAUTION SECNO=      .191  PROFILE=  1  MINIMUM SPECIFIC ENERGY
CAUTION SECNO=      .191  PROFILE=  2  CRITICAL DEPTH ASSUMED
CAUTION SECNO=      .191  PROFILE=  2  MINIMUM SPECIFIC ENERGY

CAUTION SECNO=      .290  PROFILE=  1  CRITICAL DEPTH ASSUMED
CAUTION SECNO=      .290  PROFILE=  1  MINIMUM SPECIFIC ENERGY
CAUTION SECNO=      .290  PROFILE=  2  CRITICAL DEPTH ASSUMED
CAUTION SECNO=      .290  PROFILE=  2  MINIMUM SPECIFIC ENERGY

CAUTION SECNO=      .390  PROFILE=  1  CRITICAL DEPTH ASSUMED
CAUTION SECNO=      .390  PROFILE=  1  MINIMUM SPECIFIC ENERGY
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CAUTION SECNO=      .477  PROFILE=  1  CRITICAL DEPTH ASSUMED
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CAUTION SECNO=      .972  PROFILE=  1  MINIMUM SPECIFIC ENERGY
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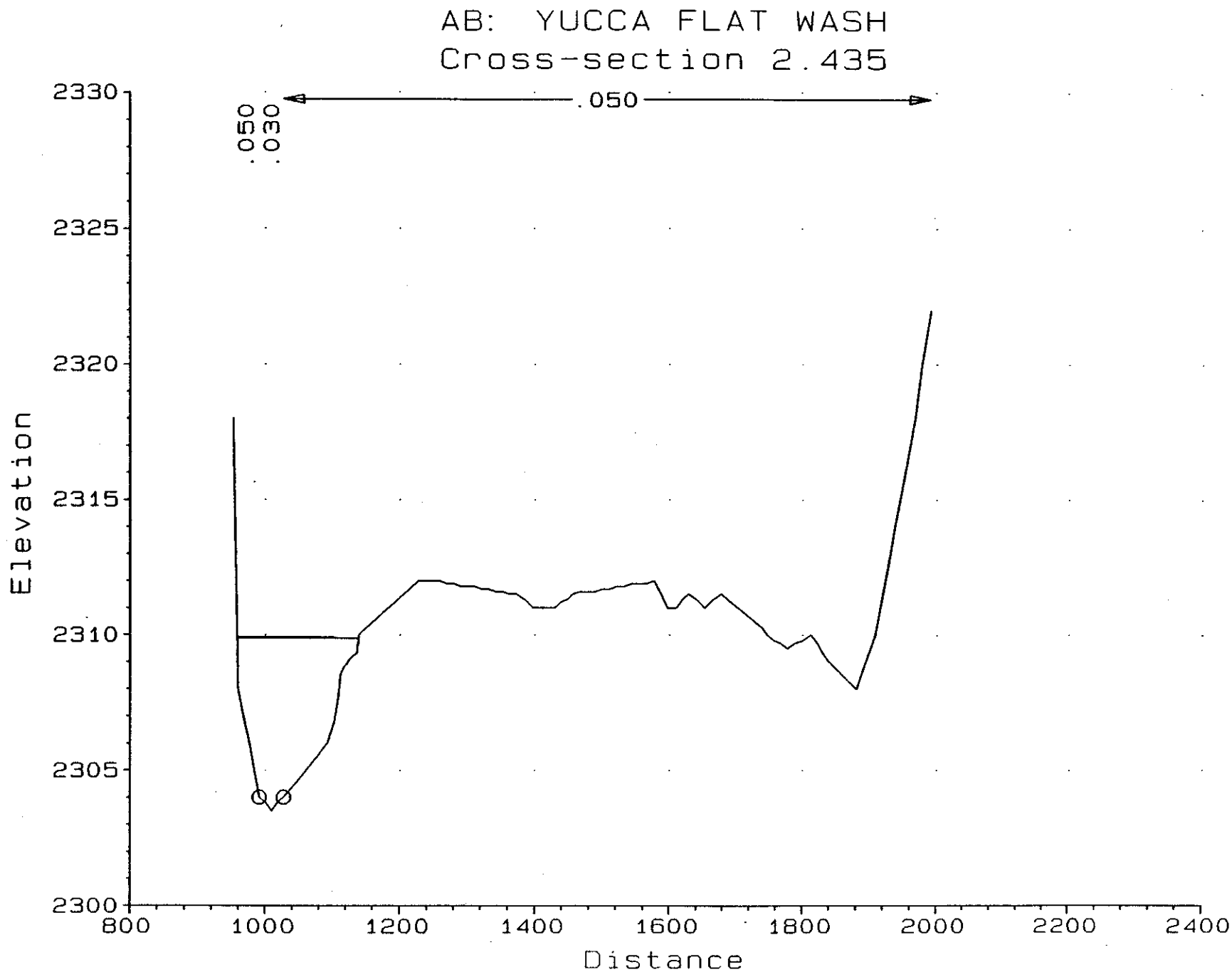
FLOODWAY DATA, AB: YUCCA FLAT WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| 2.435 | 144. | 701. | 9.9 | 2309.9 | 2309.9 | .0 |
| 2.539 | 549. | 844. | 8.2 | 2315.5 | 2315.5 | .0 |
| .191 | 533. | 873. | 5.9 | 2322.4 | 2322.4 | .0 |
| .290 | 389. | 746. | 6.9 | 2328.8 | 2328.8 | .0 |
| .390 | 379. | 849. | 6.1 | 2336.8 | 2336.3 | .5 |
| .477 | 390. | 716. | 7.2 | 2343.6 | 2343.3 | .3 |
| .578 | 341. | 843. | 6.1 | 2352.0 | 2351.8 | .2 |
| .697 | 213. | 684. | 7.5 | 2359.0 | 2358.8 | .2 |
| .788 | 174. | 625. | 8.2 | 2364.9 | 2364.9 | .0 |
| .883 | 94. | 472. | 10.9 | 2370.6 | 2370.7 | -.1 |
| .972 | 158. | 585. | 8.8 | 2375.5 | 2375.5 | .0 |
| 1.070 | 89. | 449. | 11.5 | 2381.8 | 2381.9 | -.1 |
| 1.163 | 130. | 662. | 7.8 | 2386.1 | 2385.7 | .4 |
| 1.239 | 129. | 549. | 9.4 | 2390.3 | 2390.4 | -.1 |
| 1.367 | 321. | 813. | 6.3 | 2394.9 | 2394.9 | .0 |
| 1.462 | 187. | 637. | 8.1 | 2401.3 | 2401.4 | -.1 |
| 1.551 | 144. | 542. | 9.5 | 2407.0 | 2406.9 | .1 |
| 1.646 | 163. | 599. | 8.6 | 2412.4 | 2412.6 | -.2 |
| 1.718 | 260. | 1114. | 4.6 | 2415.5 | 2415.4 | .1 |
| 1.808 | 328. | 431. | 4.8 | 2420.3 | 2420.3 | .0 |
| 1.905 | 245. | 405. | 5.1 | 2425.8 | 2425.8 | .0 |
| 2.003 | 268. | 430. | 4.8 | 2432.8 | 2432.8 | .0 |
| 2.091 | 215. | 385. | 5.4 | 2437.5 | 2437.0 | .5 |
| 2.172 | 219. | 394. | 5.3 | 2442.3 | 2442.0 | .3 |
| 2.284 | 196. | 376. | 5.5 | 2450.6 | 2450.6 | .0 |
| 2.384 | 199. | 376. | 5.5 | 2456.7 | 2456.7 | .0 |
| 2.477 | 397. | 460. | 4.5 | 2462.3 | 2462.3 | .0 |
| 2.562 | 278. | 350. | 5.9 | 2467.4 | 2467.4 | .0 |
| 2.672 | 220. | 357. | 5.8 | 2475.3 | 2475.3 | .0 |
| 2.761 | 279. | 403. | 5.2 | 2480.3 | 2480.3 | .0 |
| 2.857 | 356. | 459. | 4.5 | 2488.2 | 2488.2 | .0 |
| 2.965 | 331. | 408. | 5.1 | 2496.7 | 2496.7 | .0 |
| -1.718 | 260. | 1116. | 4.6 | 2415.5 | 2415.4 | .1 |
| .098 | 233. | 355. | 5.9 | 2418.8 | 2418.8 | .0 |
| .190 | 81. | 263. | 8.0 | 2423.9 | 2423.9 | .0 |
| .301 | 118. | 308. | 6.8 | 2431.5 | 2431.3 | .2 |
| .384 | 93. | 328. | 6.4 | 2434.5 | 2434.0 | .5 |
| .473 | 102. | 273. | 7.7 | 2440.9 | 2440.7 | .2 |
| .581 | 112. | 314. | 6.7 | 2448.6 | 2448.4 | .2 |
| .669 | 129. | 327. | 6.4 | 2452.7 | 2452.2 | .5 |
| .765 | 67. | 239. | 8.8 | 2458.4 | 2458.3 | .1 |
| .866 | 123. | 333. | 6.3 | 2463.2 | 2463.0 | .2 |

FLOODWAY DATA, AB: YUCCA FLAT WASH
PROFILE NO. 2

| STATION | FLOODWAY WIDTH | FLOODWAY SECTION AREA | FLOODWAY MEAN VELOCITY | WATER SURFACE ELEVATION WITH FLOODWAY | WATER SURFACE ELEVATION WITHOUT FLOODWAY | DIFFERENCE |
|---|---|---|---|---|---|---|
| .949 | 74. | 245. | 8.6 | 2469.5 | 2469.4 | .1 |
| 1.045 | 170. | 361. | 5.8 | 2474.5 | 2474.5 | .0 |
| 1.148 | 77. | 244. | 8.6 | 2481.0 | 2481.0 | .0 |
| 1.242 | 114. | 293. | 7.2 | 2487.1 | 2487.1 | .0 |
| 1.343 | 70. | 237. | 8.9 | 2496.0 | 2496.0 | .0 |
| 1.428 | 91. | 271. | 7.7 | 2500.7 | 2500.7 | .0 |
| 1.525 | 97. | 280. | 7.5 | 2506.3 | 2506.3 | .0 |
| 1.619 | 92. | 269. | 7.8 | 2515.1 | 2515.1 | .0 |
| 1.719 | 102. | 280. | 7.5 | 2522.9 | 2522.9 | .0 |
| 1.802 | 68. | 230. | 9.1 | 2529.6 | 2529.6 | .0 |
| 1.897 | 93. | 228. | 7.2 | 2538.9 | 2538.9 | .0 |
| 1.993 | 122. | 246. | 6.7 | 2543.1 | 2543.1 | .0 |
| 2.094 | 86. | 224. | 7.4 | 2549.3 | 2549.3 | .0 |
| 2.183 | 61. | 192. | 8.6 | 2552.8 | 2552.8 | .0 |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.050
.030
Elevation
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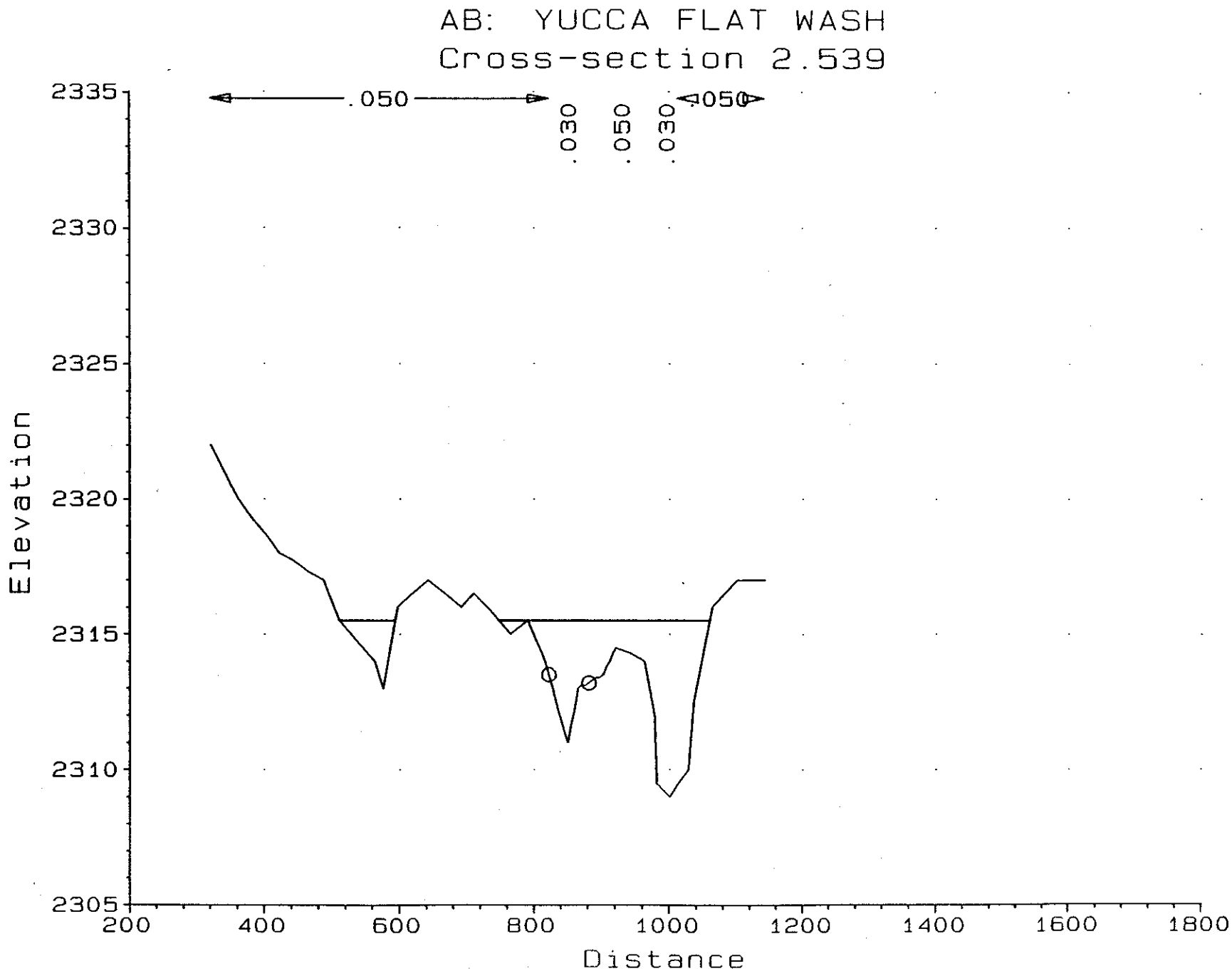
2310
2305
2300
800
1000
1200
1400
1600
1800
2000
2200
2400
Distance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Cross-section 2.539
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.050
.030
.050
.030
Elevation
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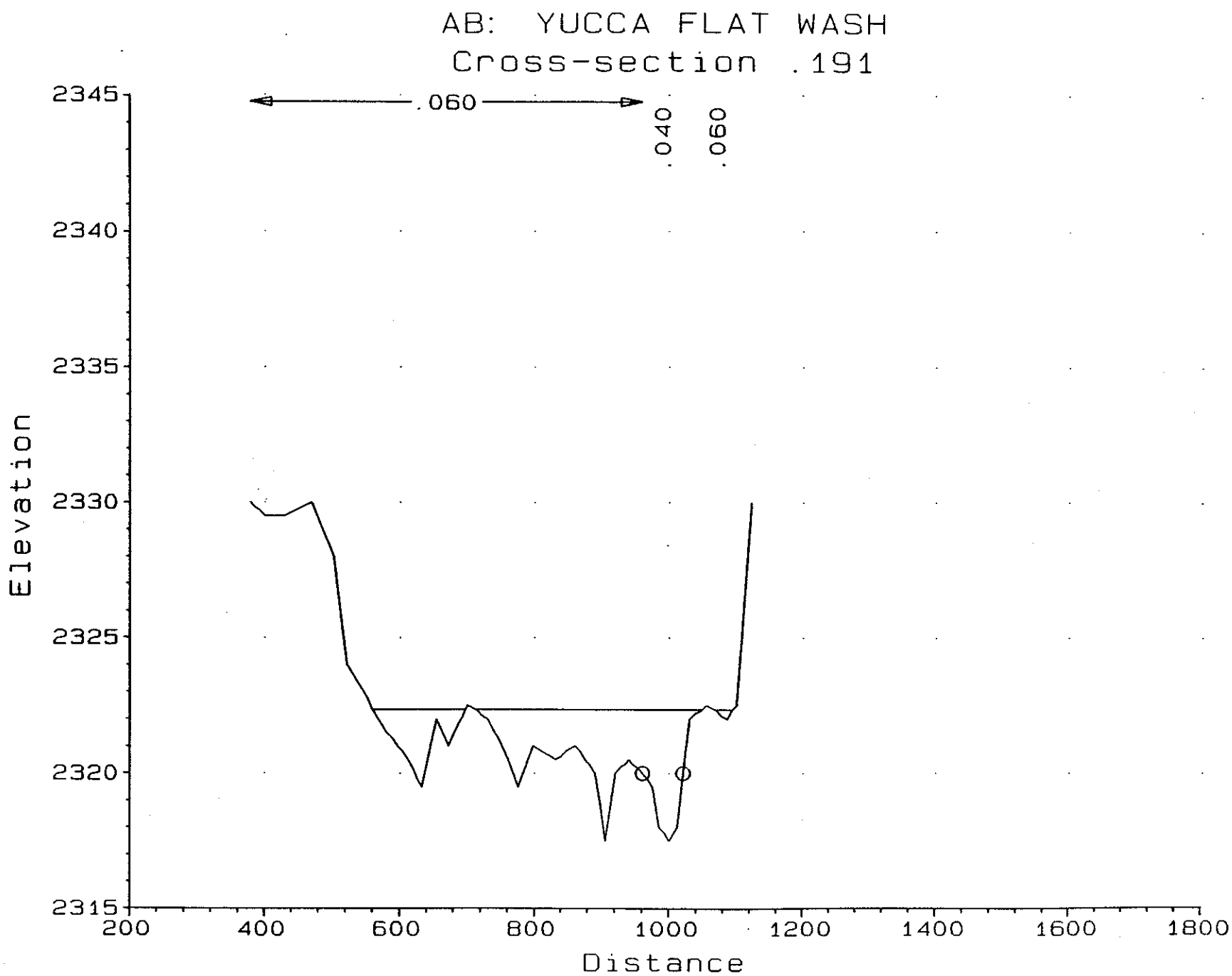
Distance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Cross-section .191
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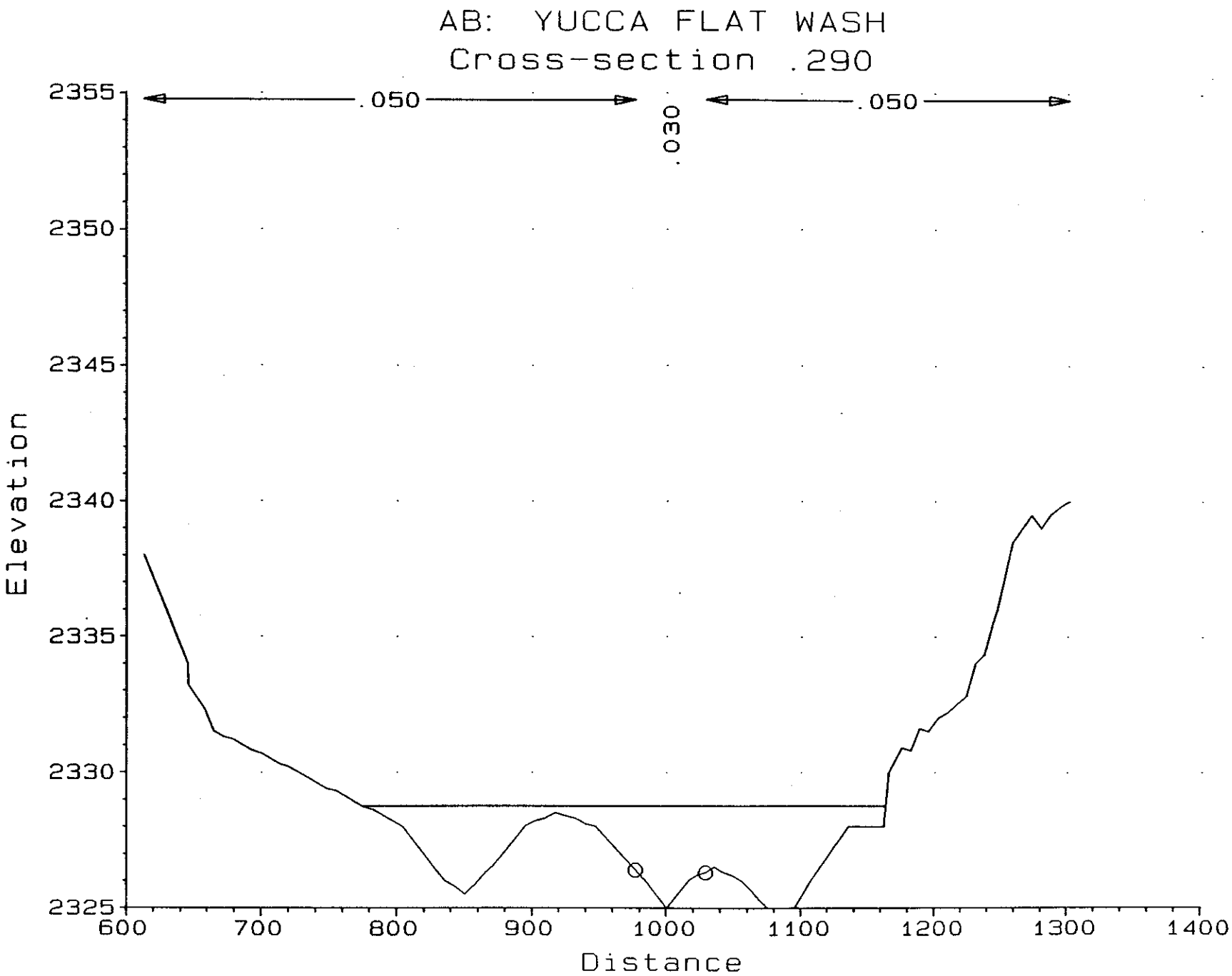
1800
Distance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.030
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Elevation
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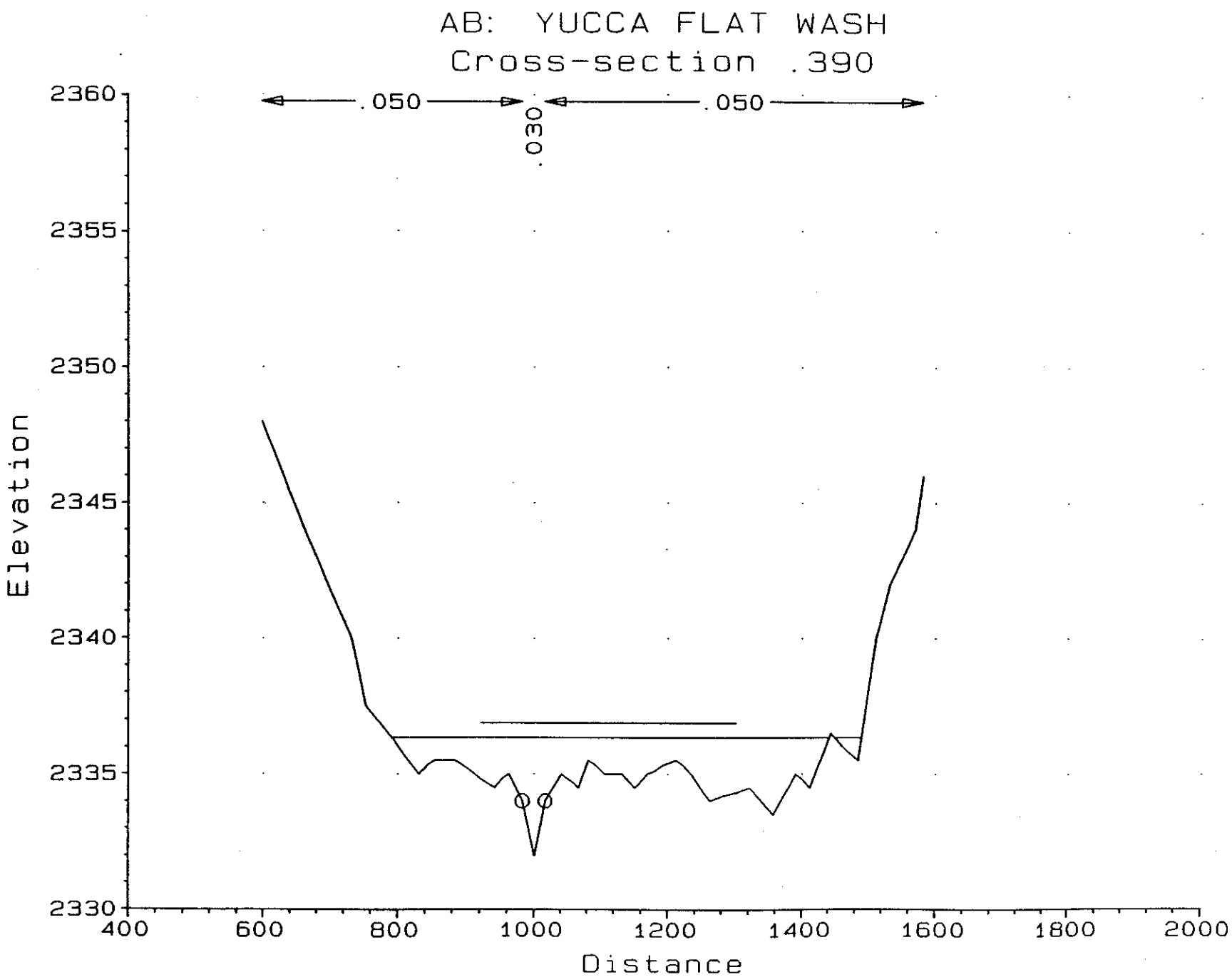
1000
1100
1200
1300
1400
Distance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.050
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1200
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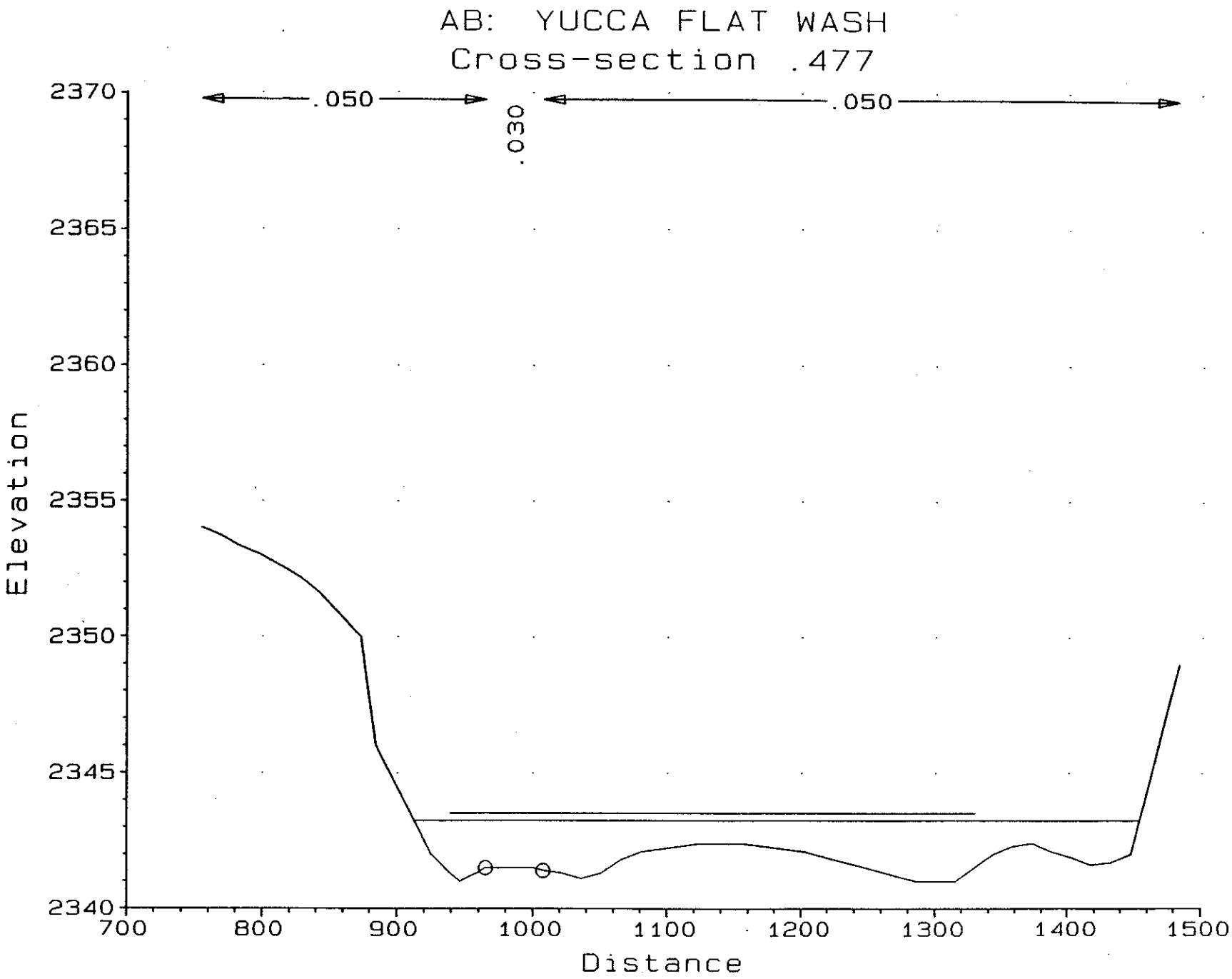
1600
1800
2000
Distance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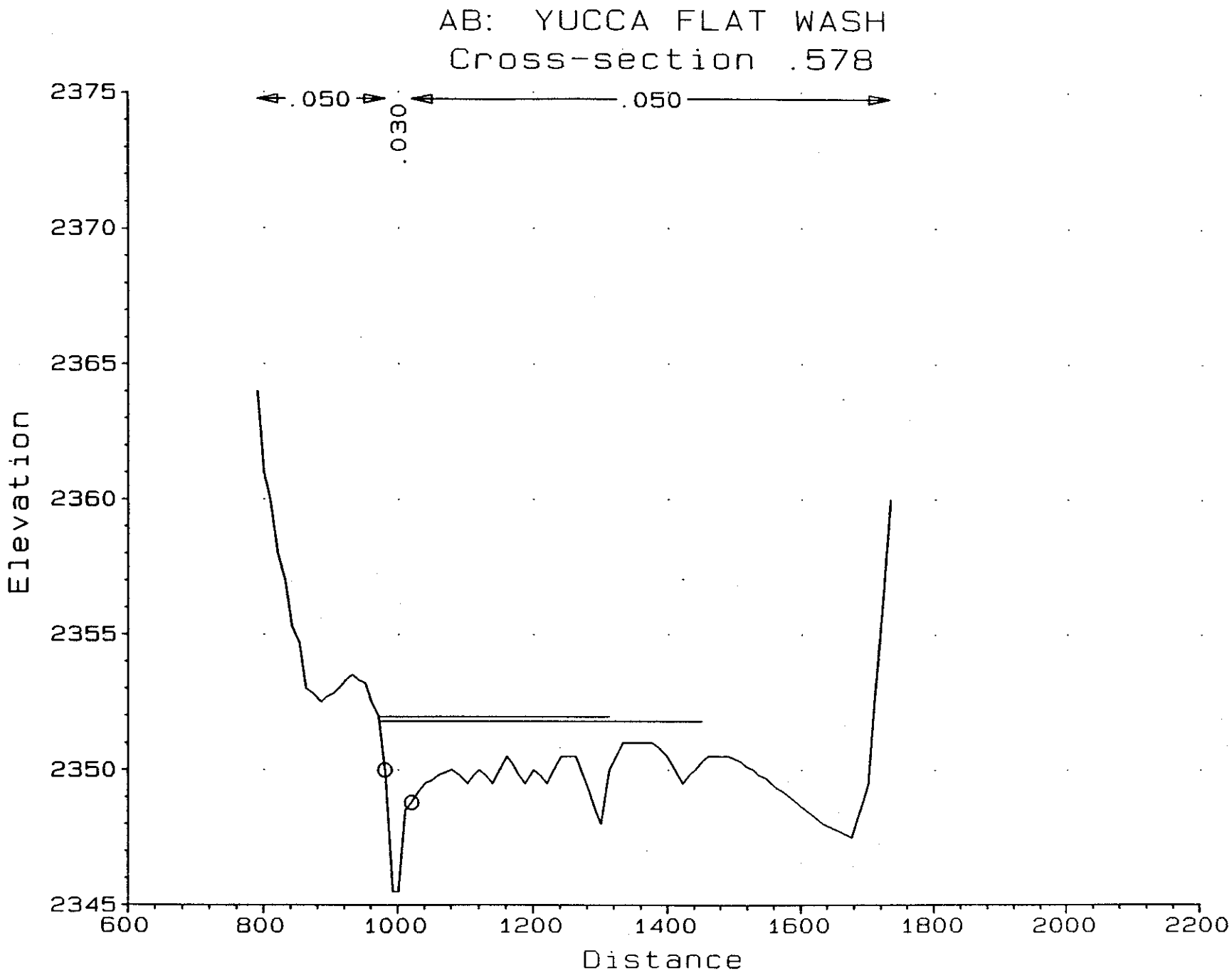
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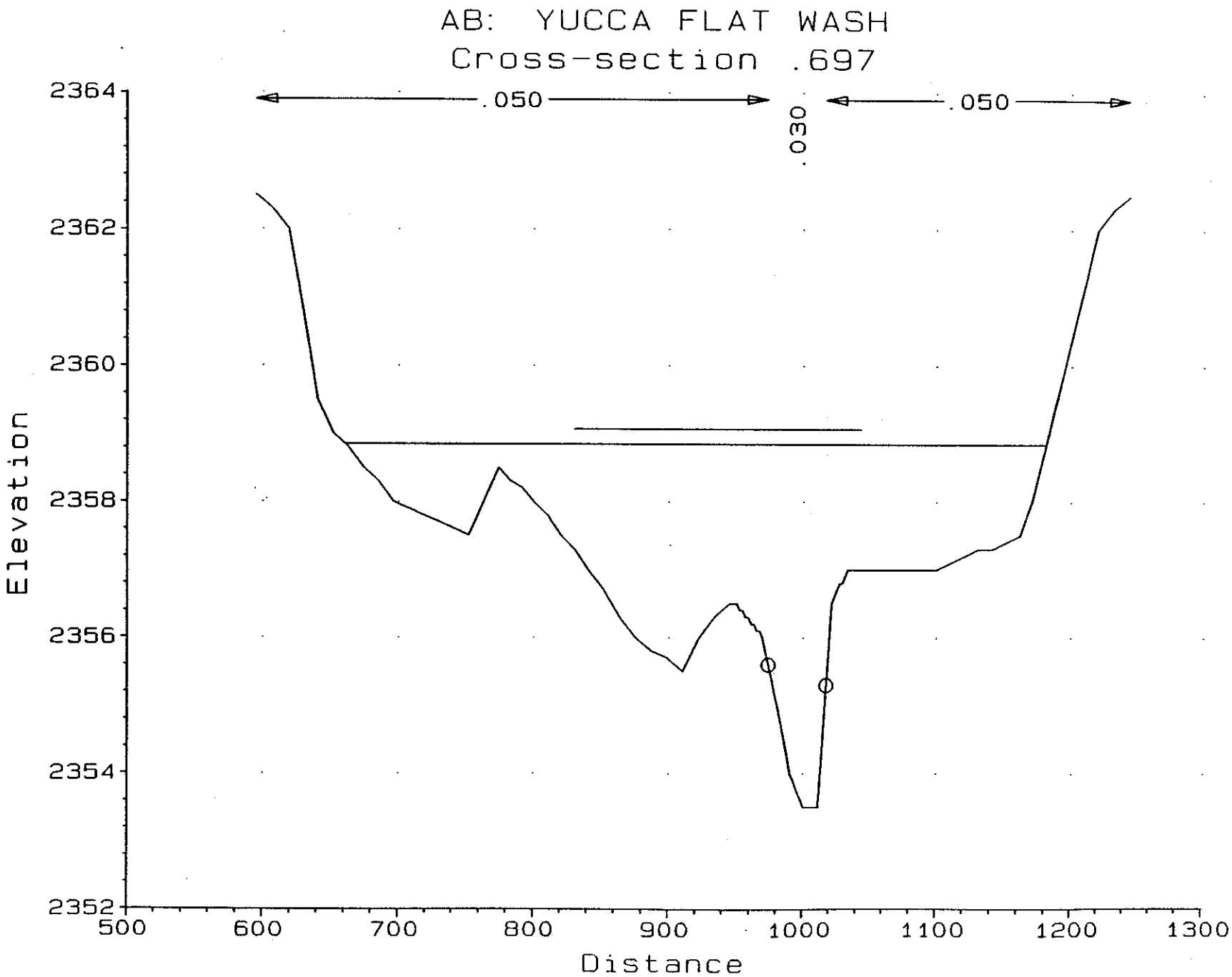
Distance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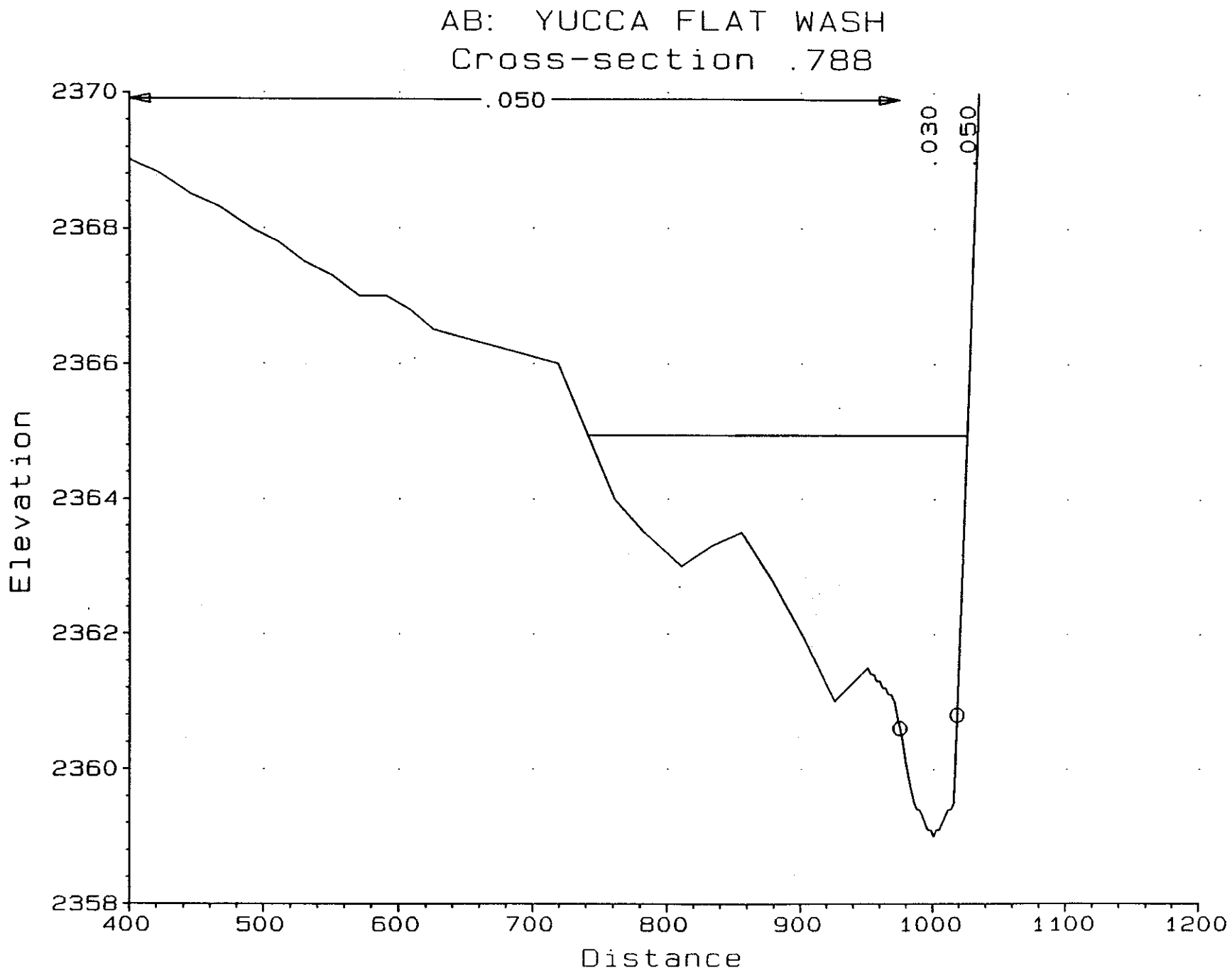
Distance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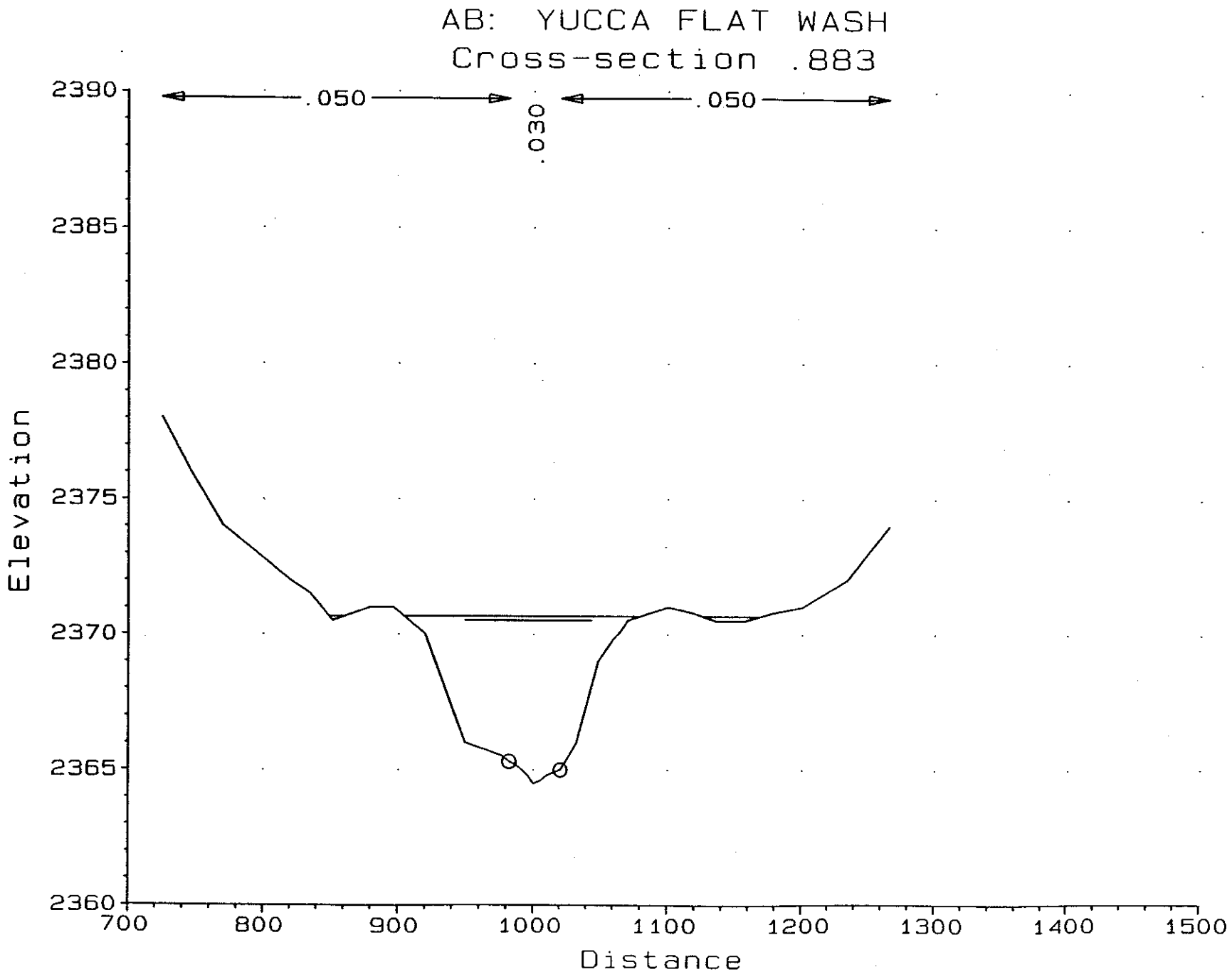
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Cross-section .883
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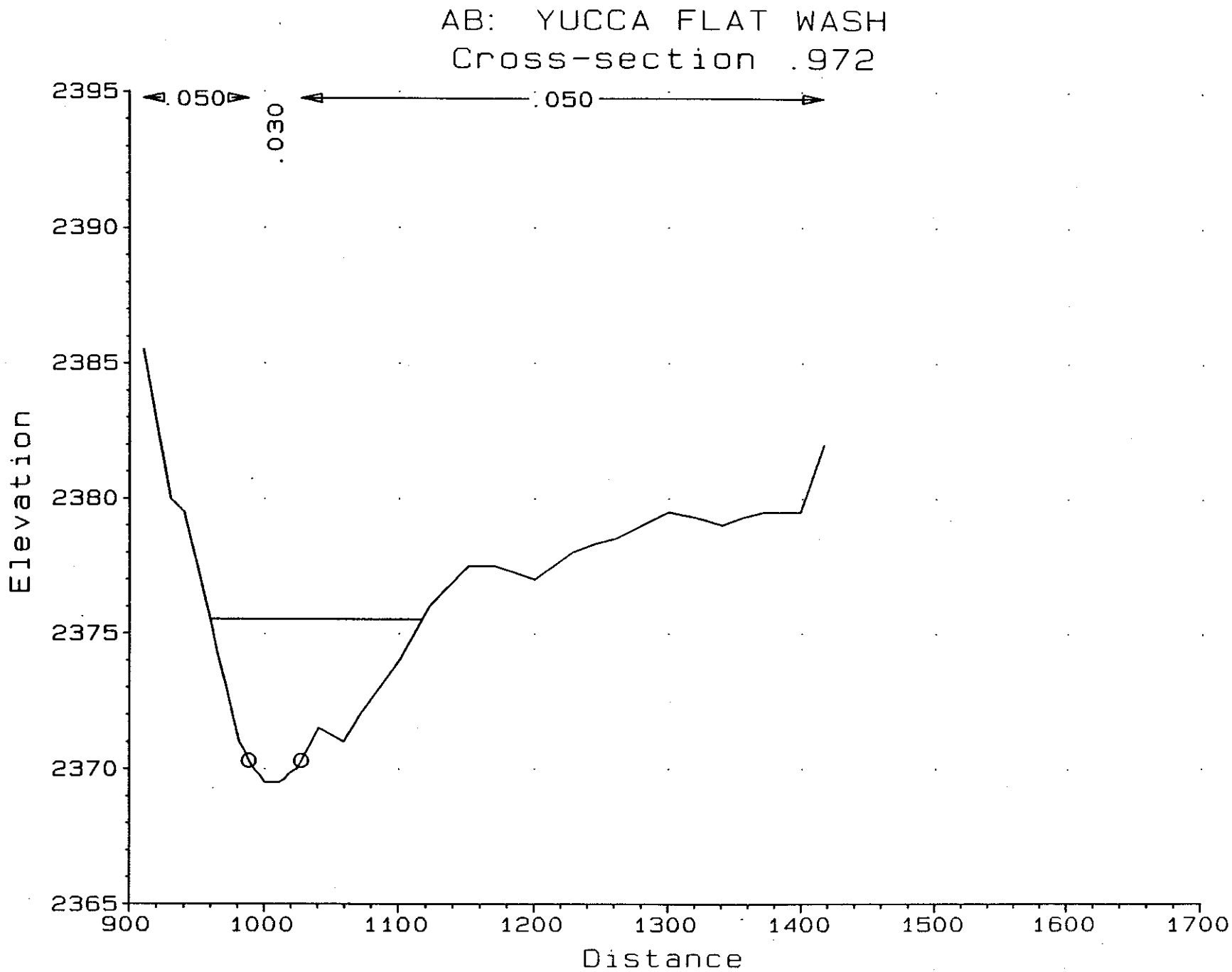
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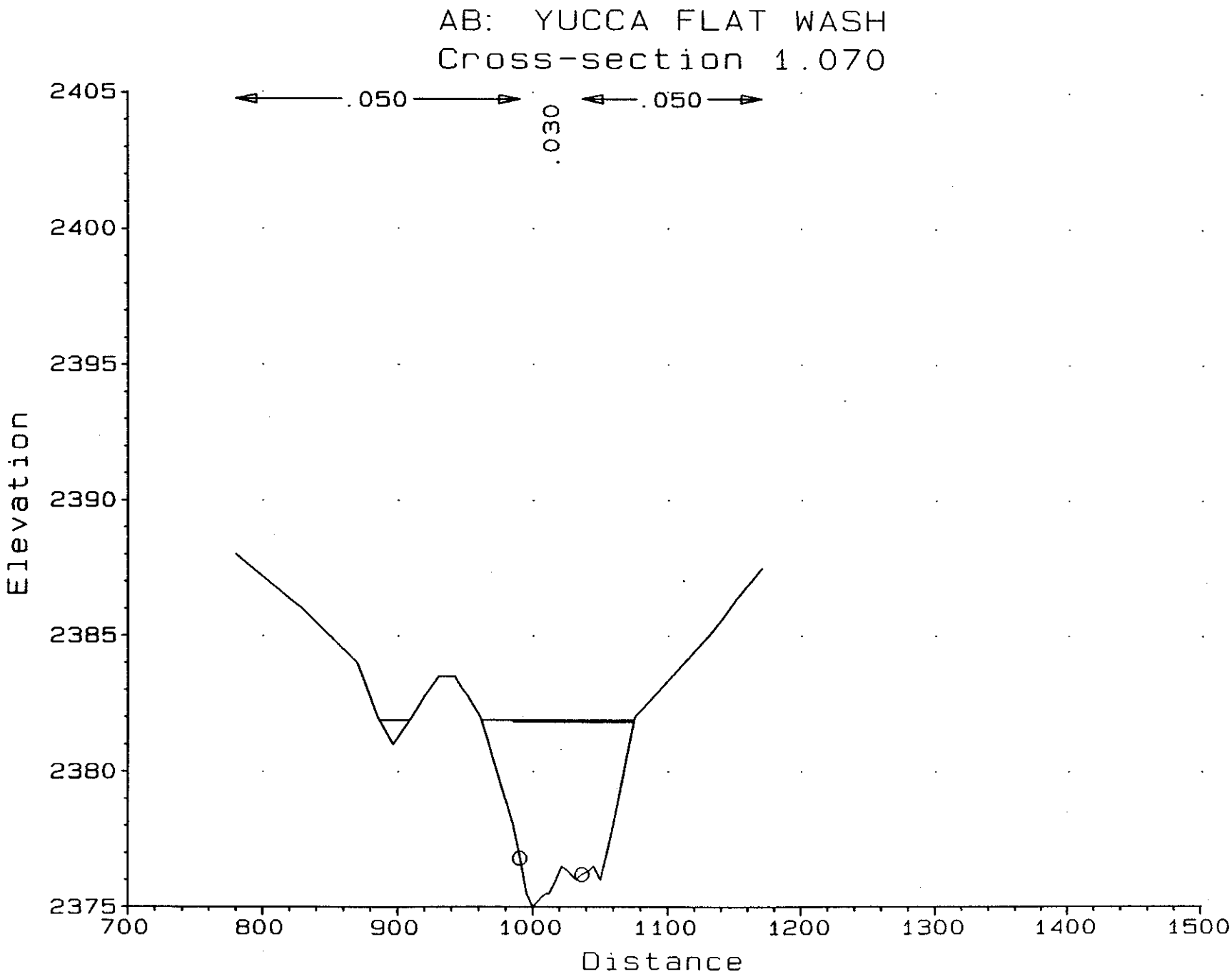
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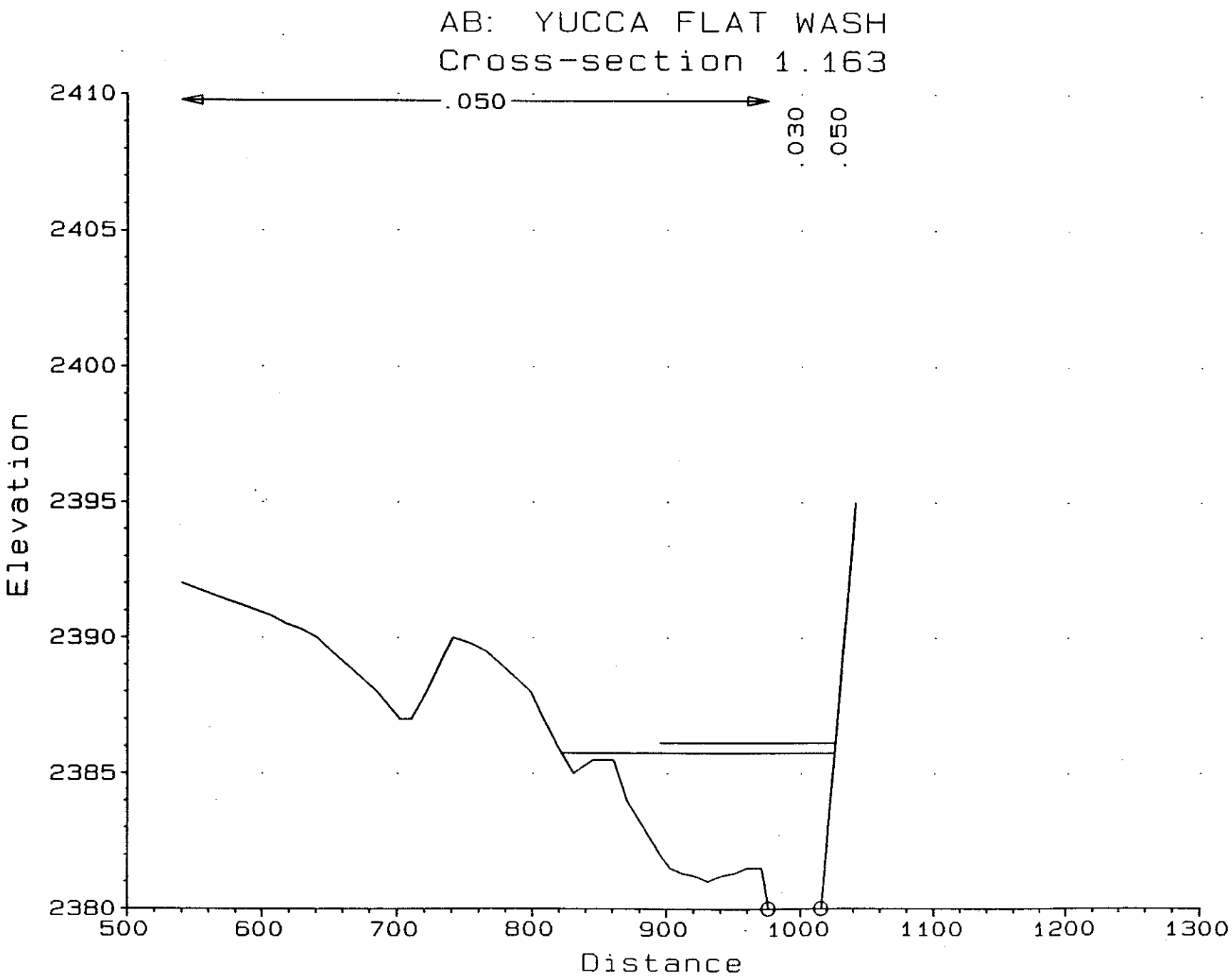
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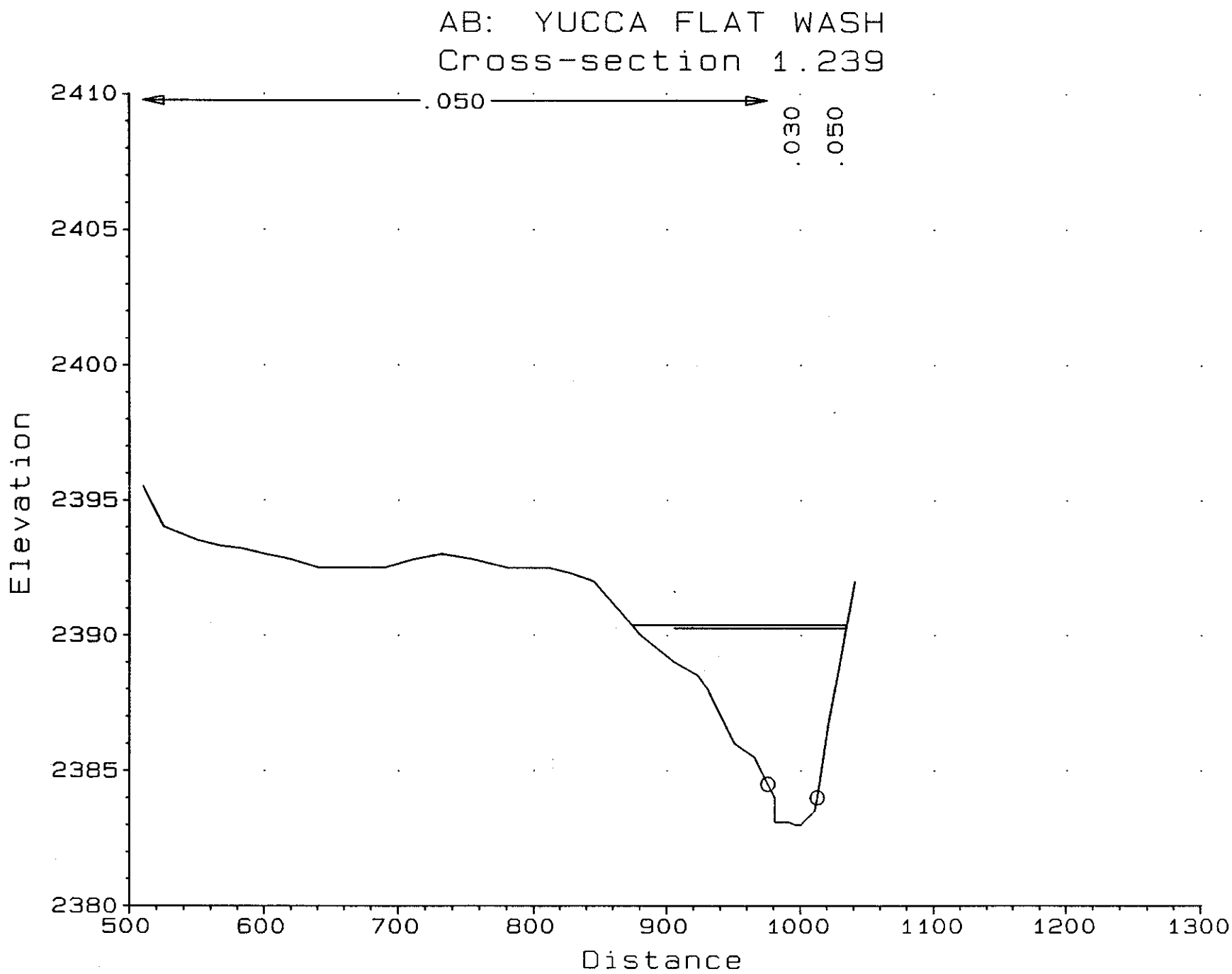
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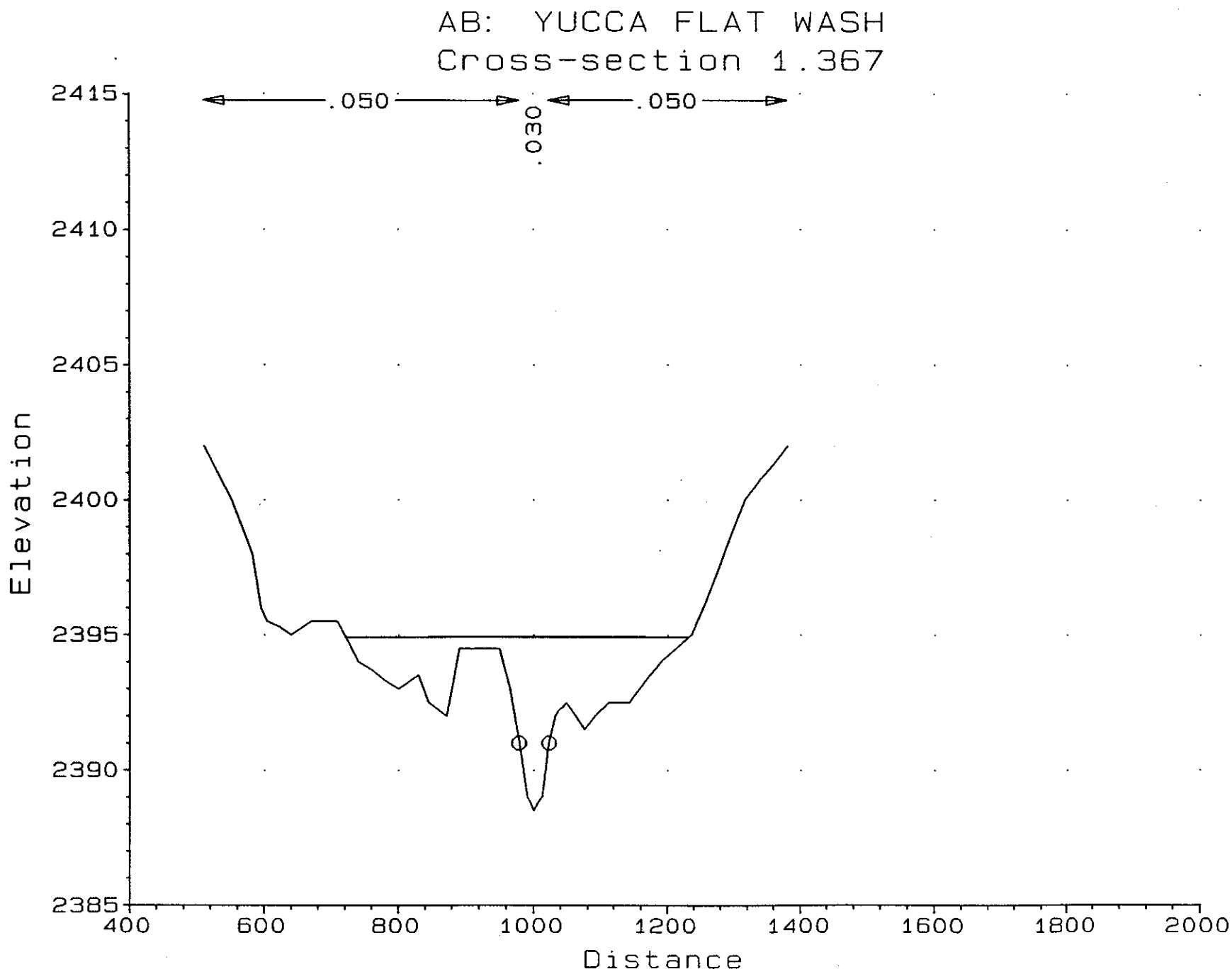
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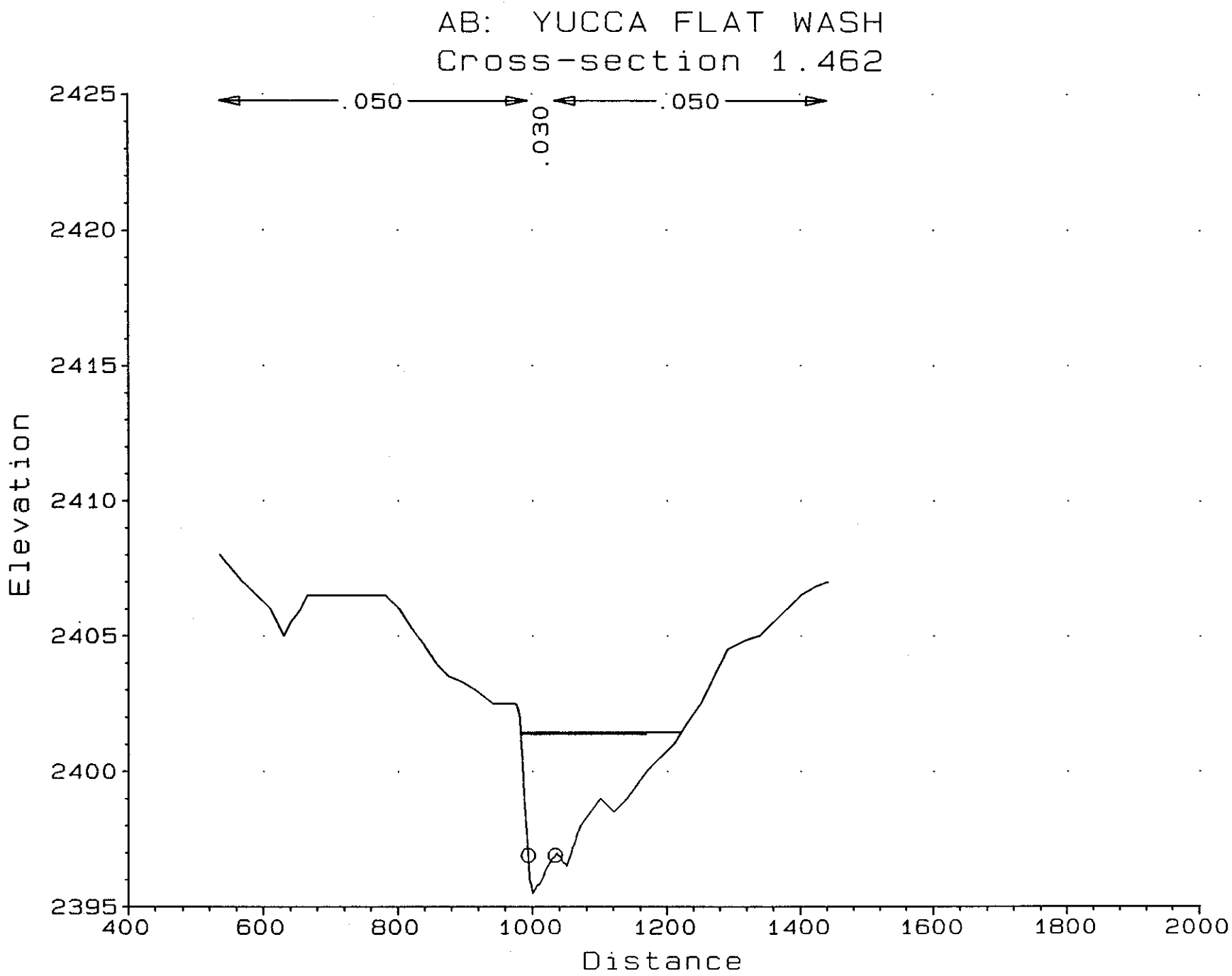
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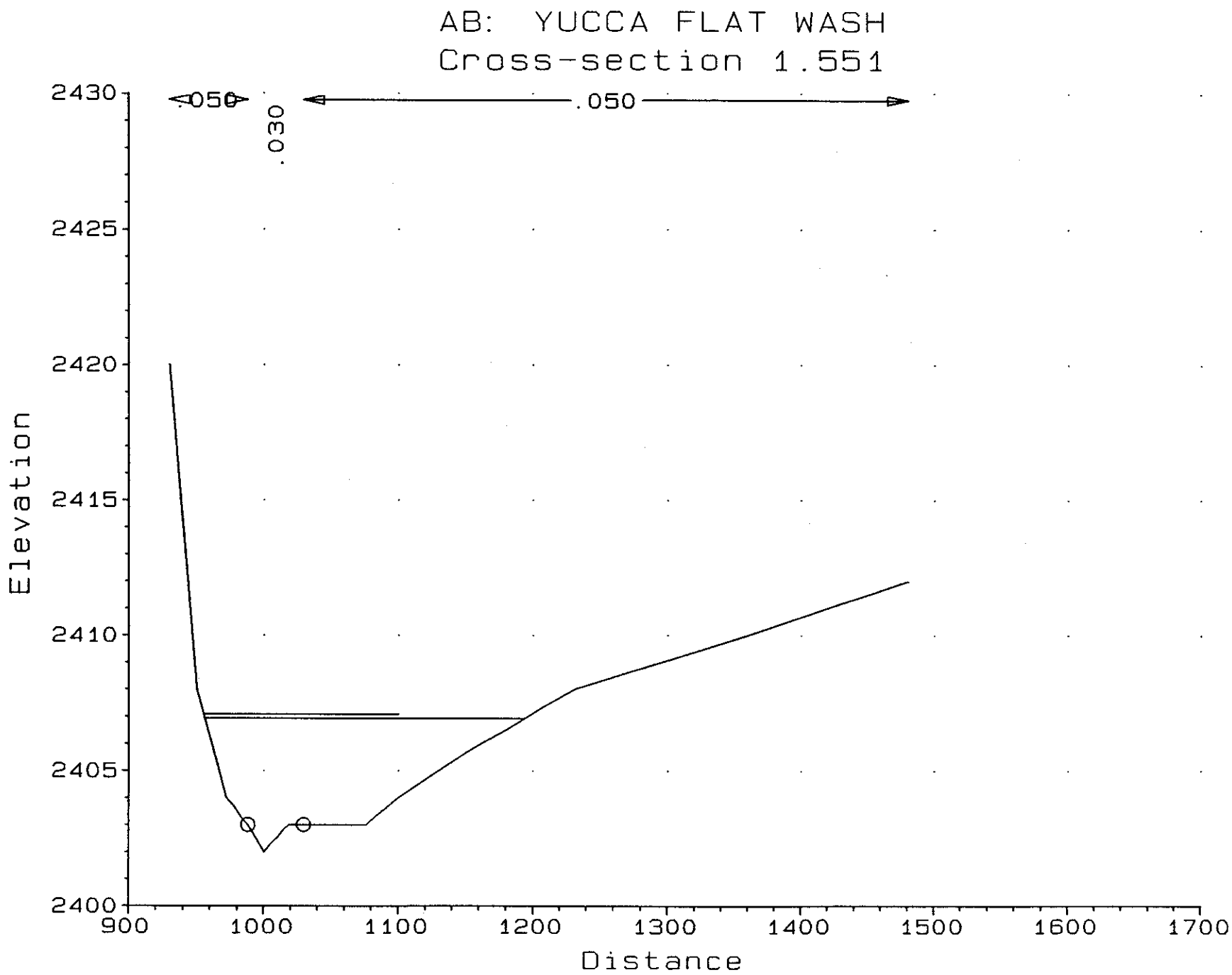
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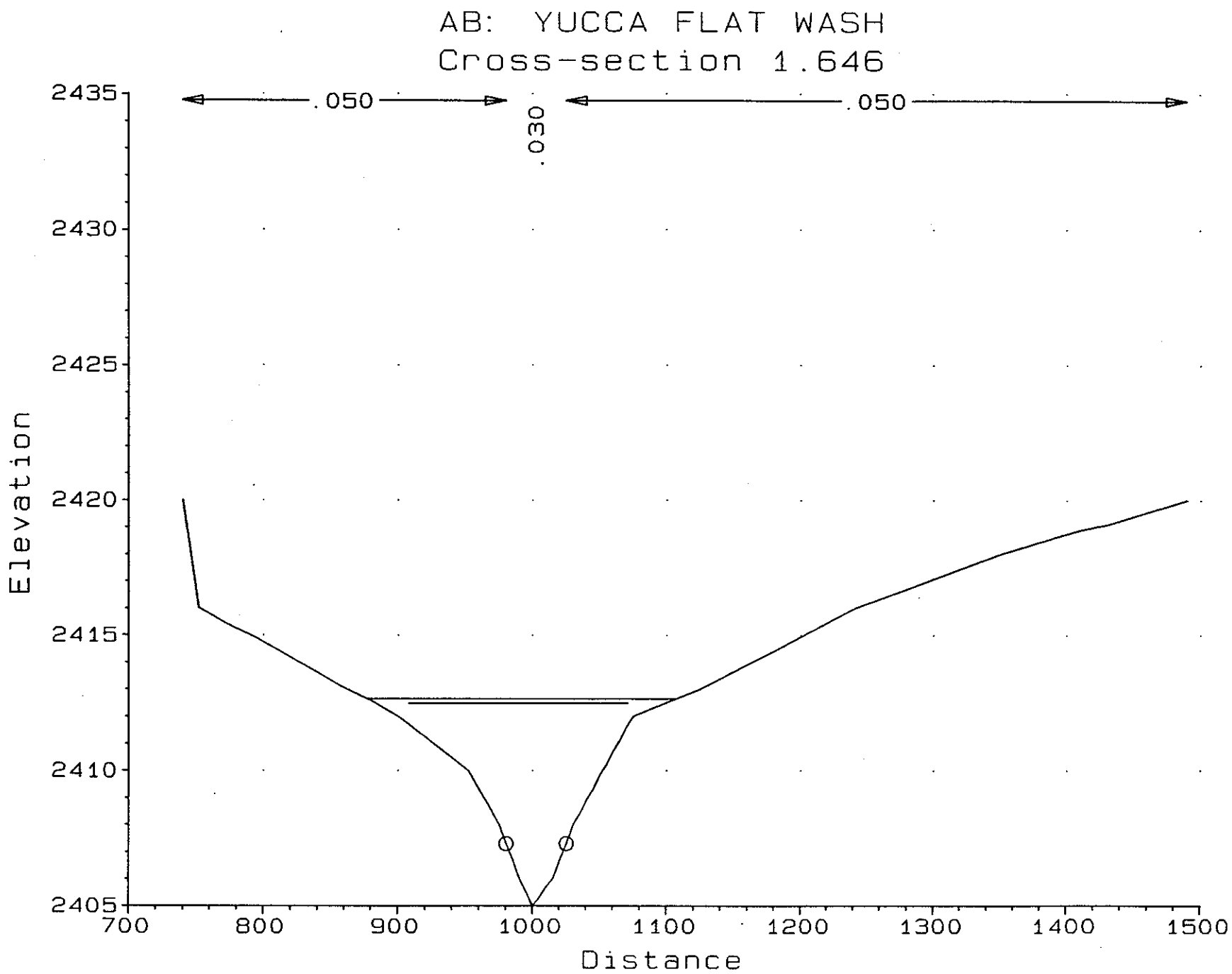
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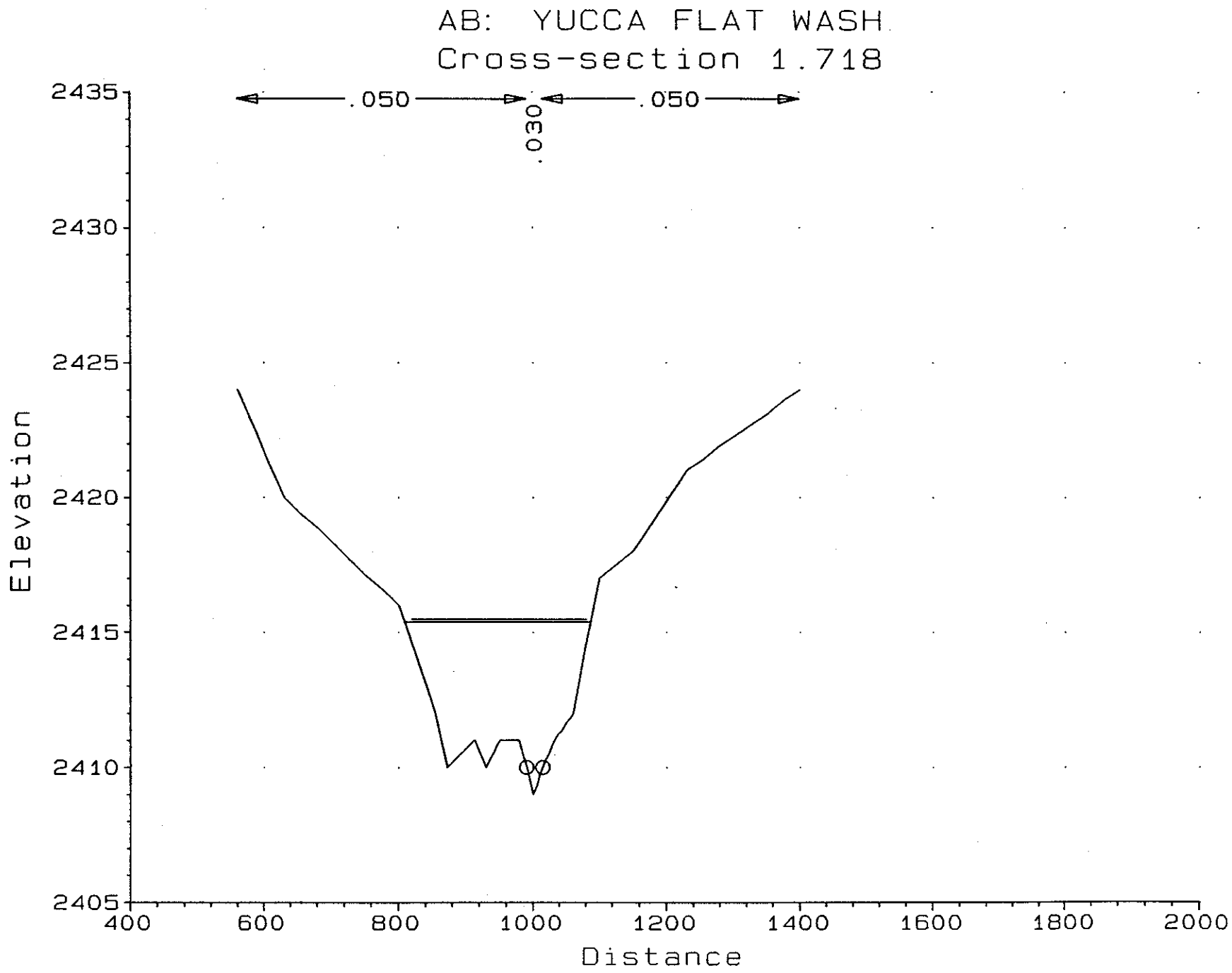
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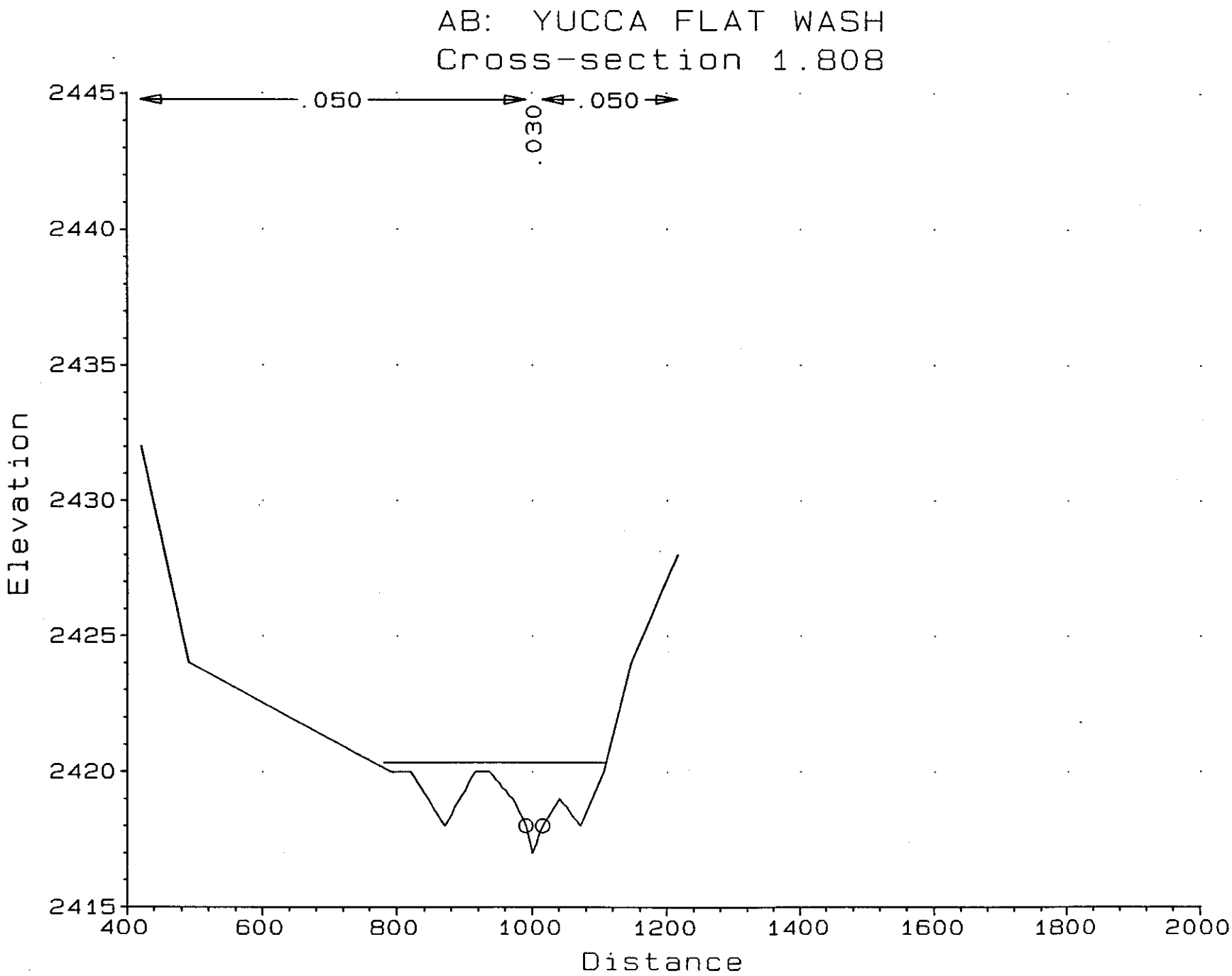
AB: YUCCA FLAT WASH
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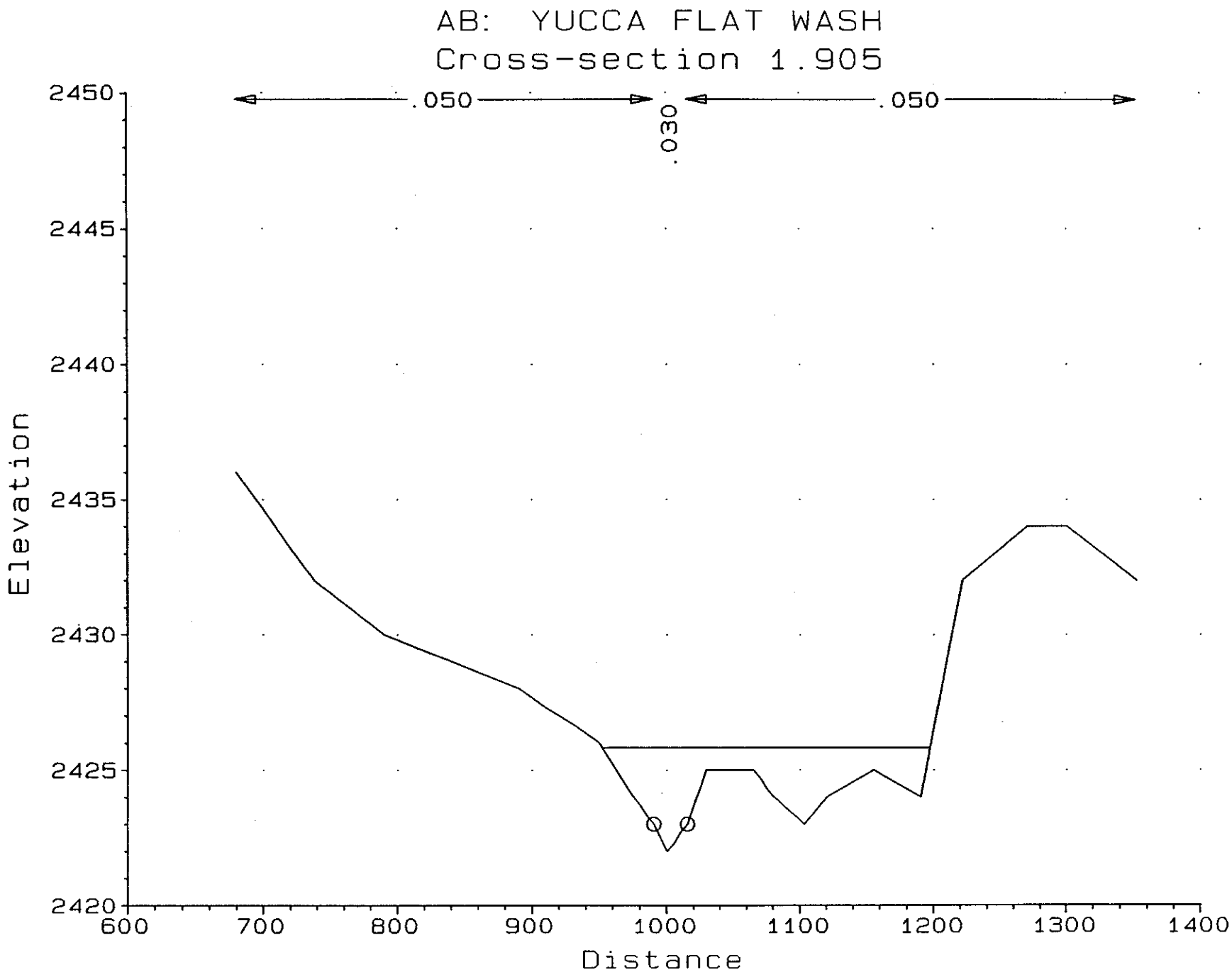
AB: YUCCA FLAT WASH
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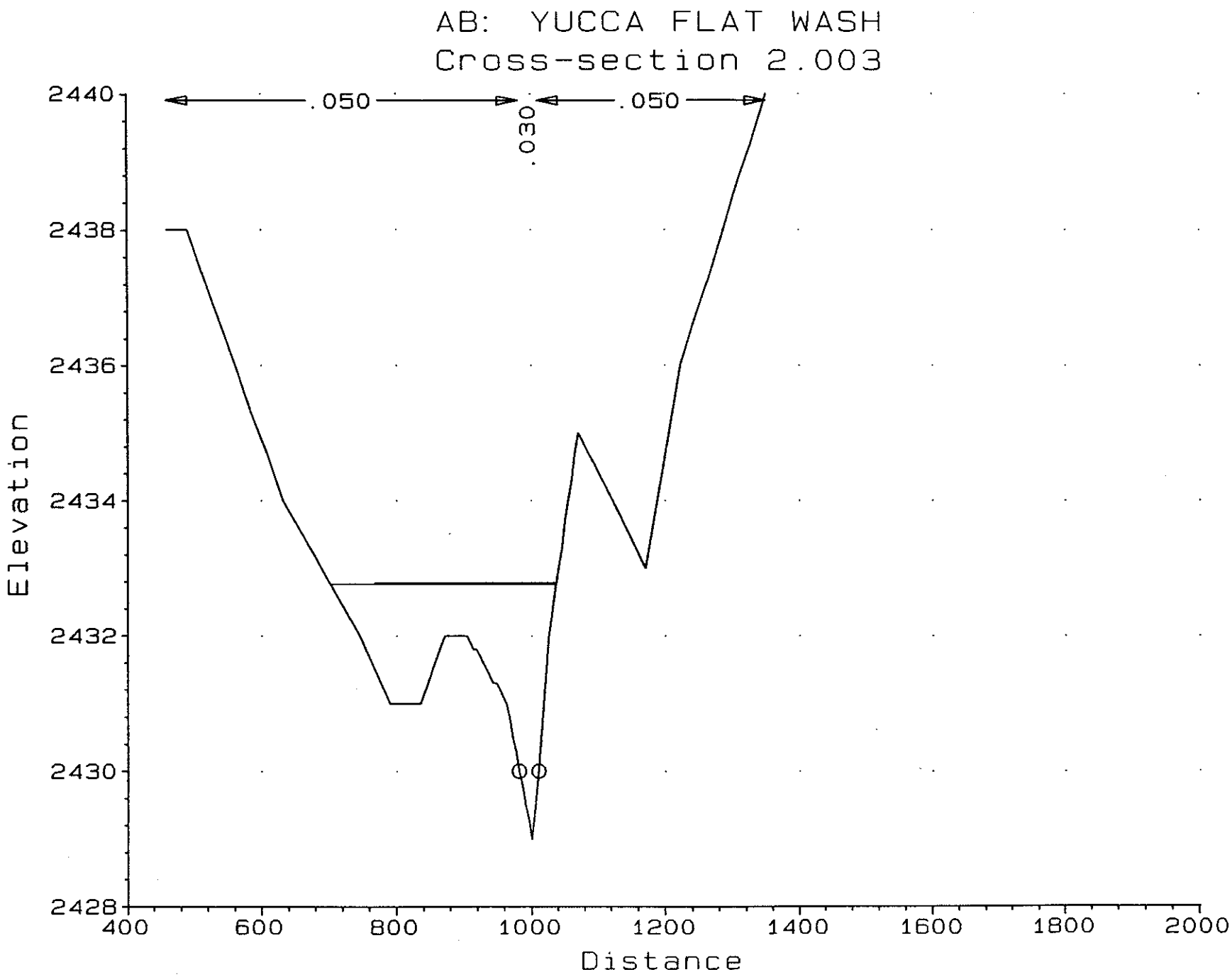
Distance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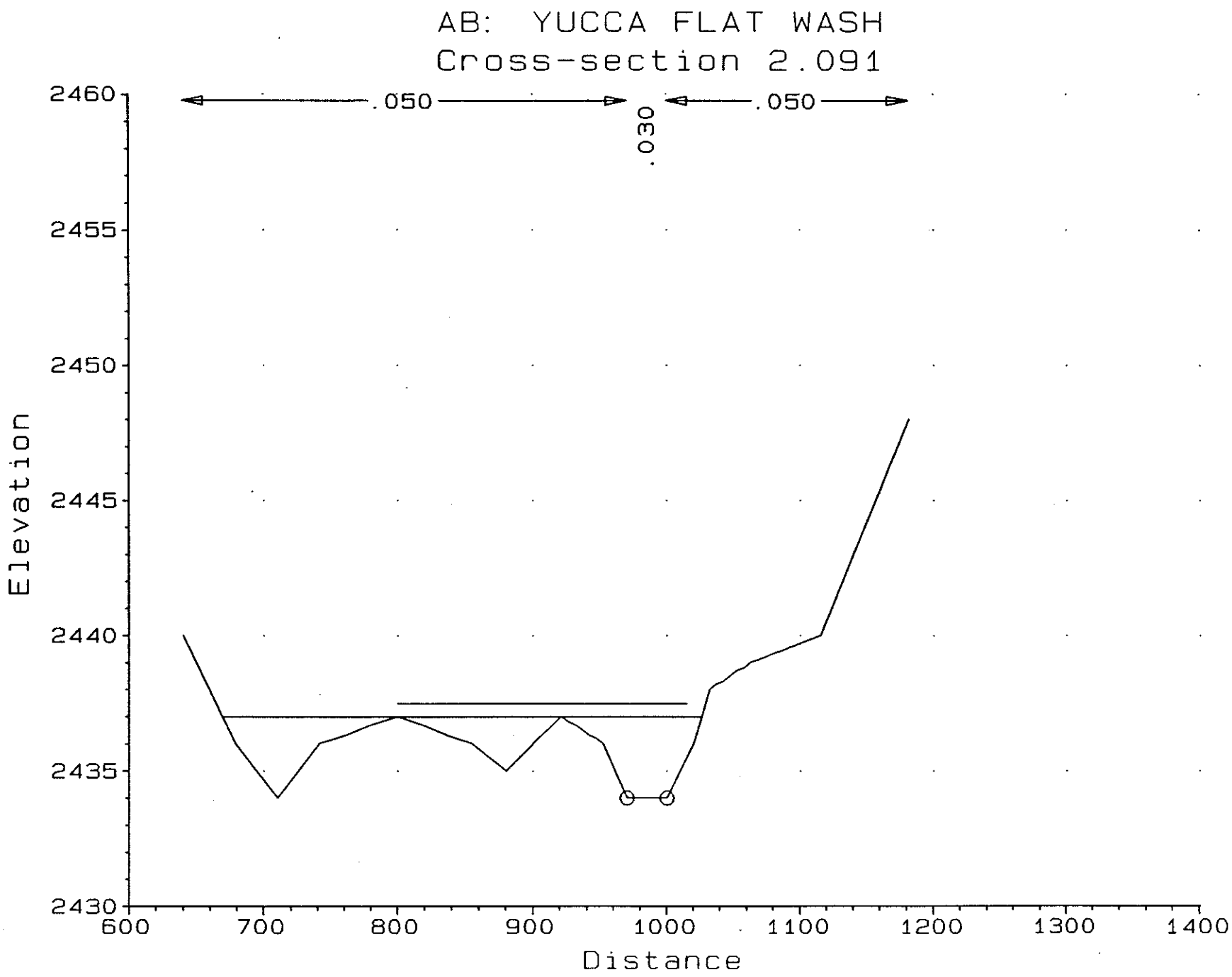
AB: YUCCA FLAT WASH
Cross-section 2.091
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Elevation
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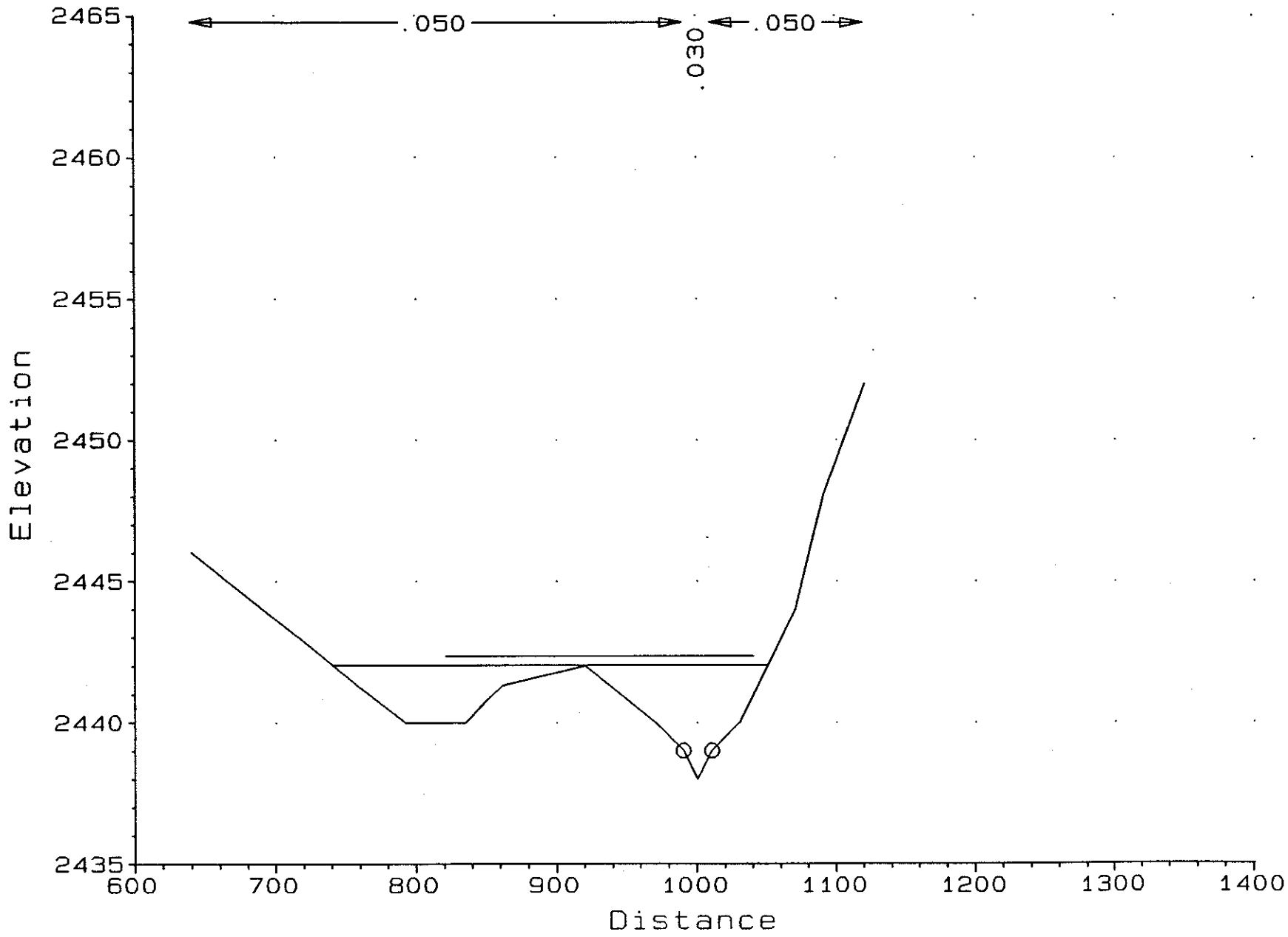
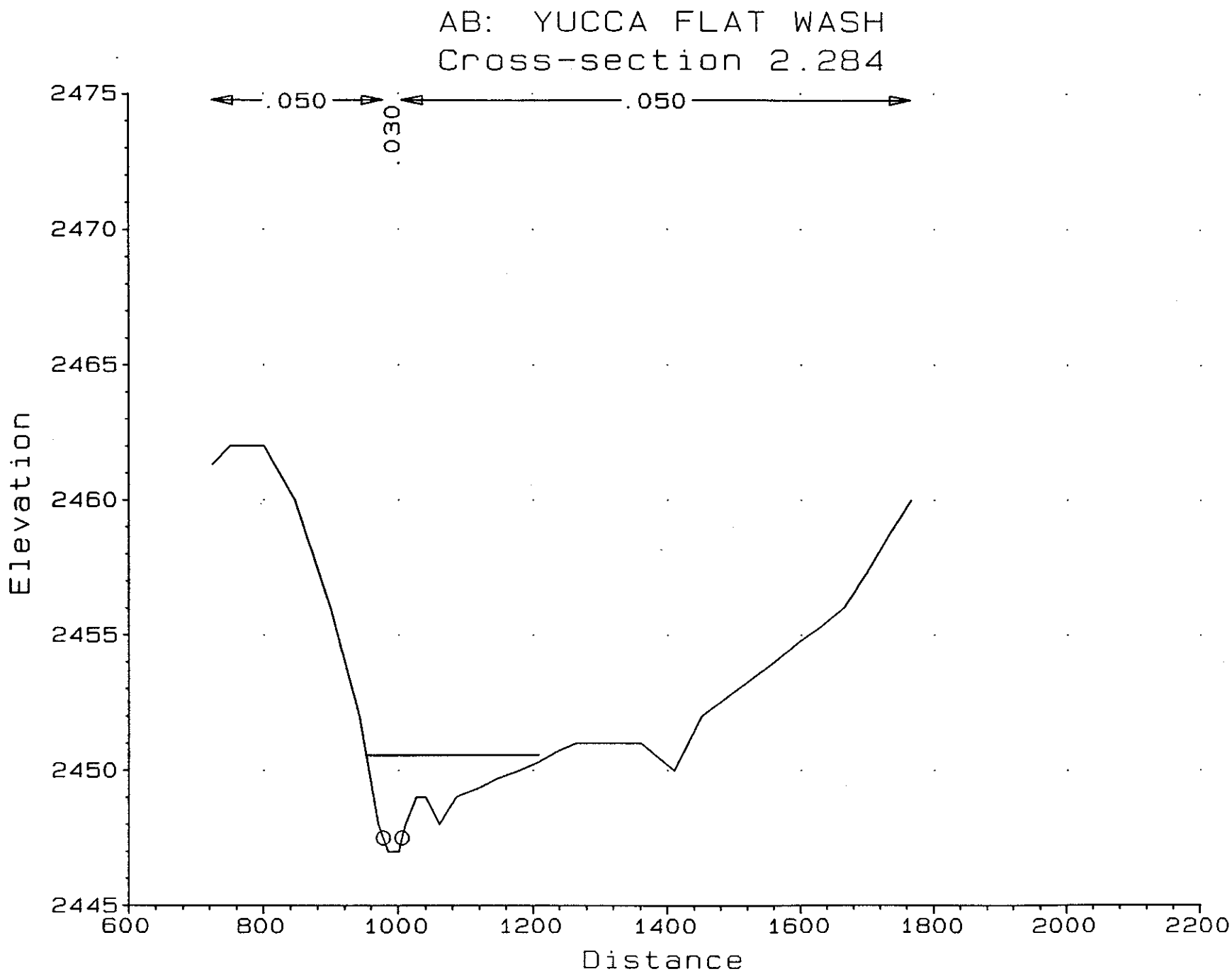
1000
1100
1200
1300
1400
Distance

AB: YUCCA FLAT WASH
Cross-section 2.172




AB: YUCCA FLAT WASH
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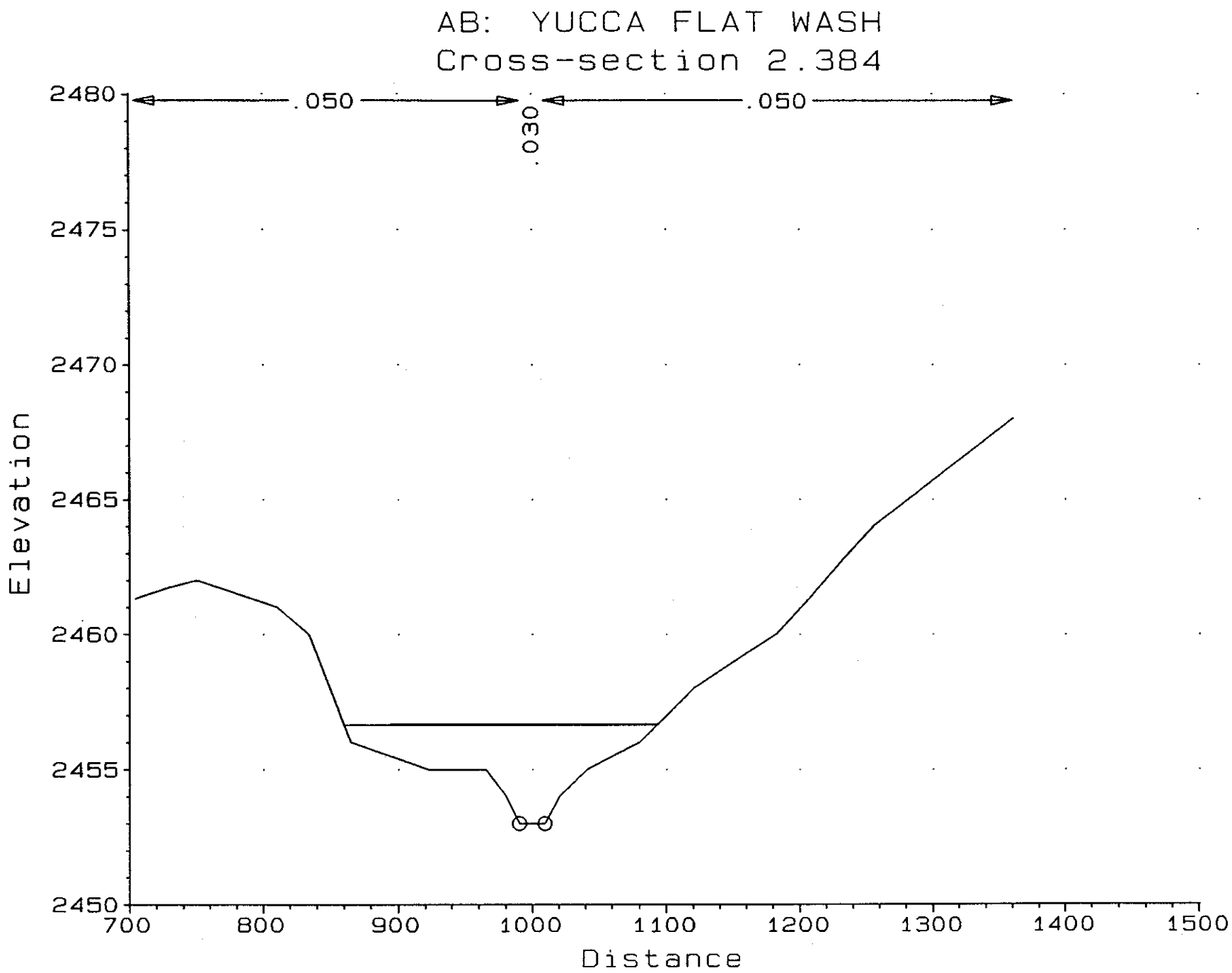
AB: YUCCA FLAT WASH
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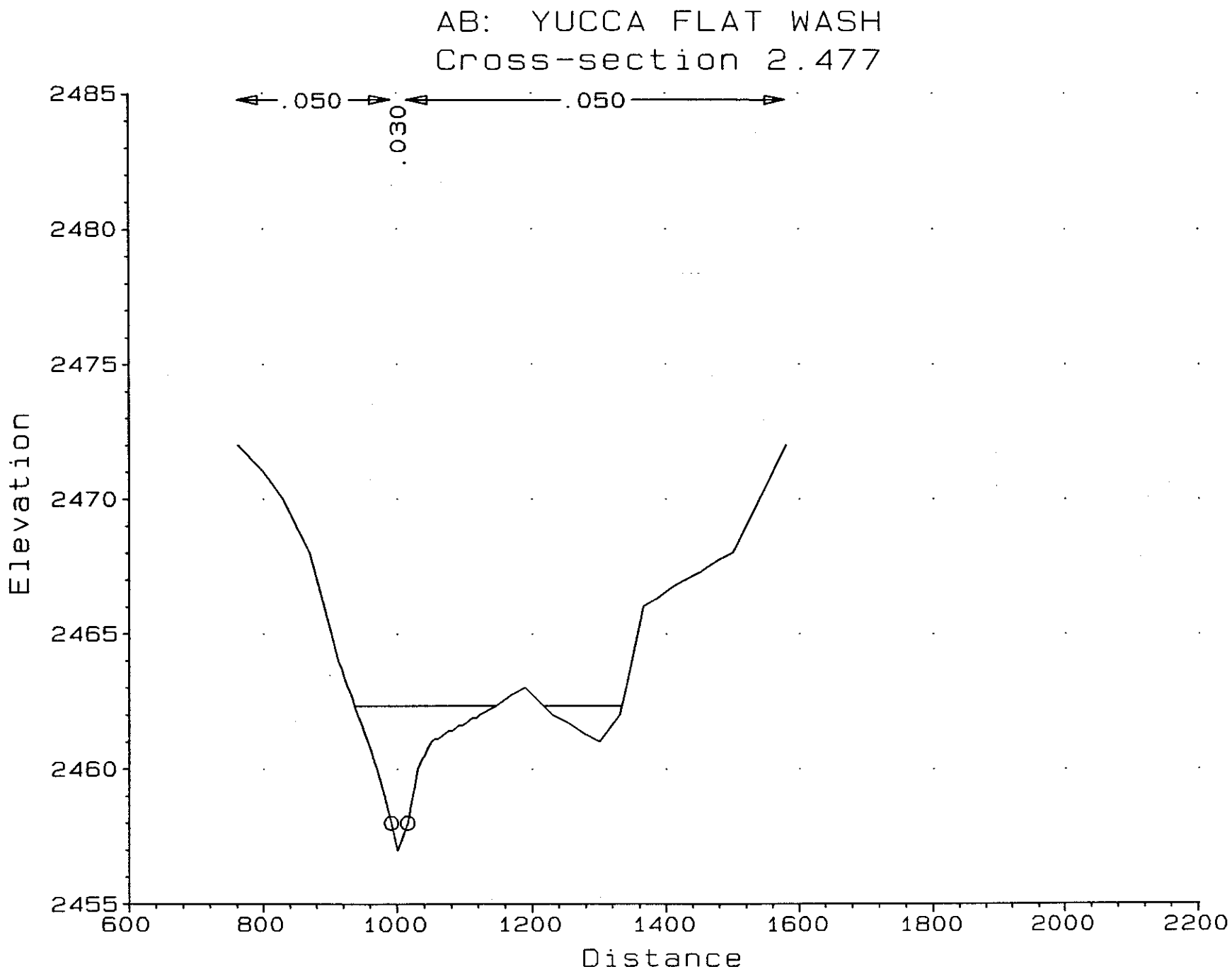
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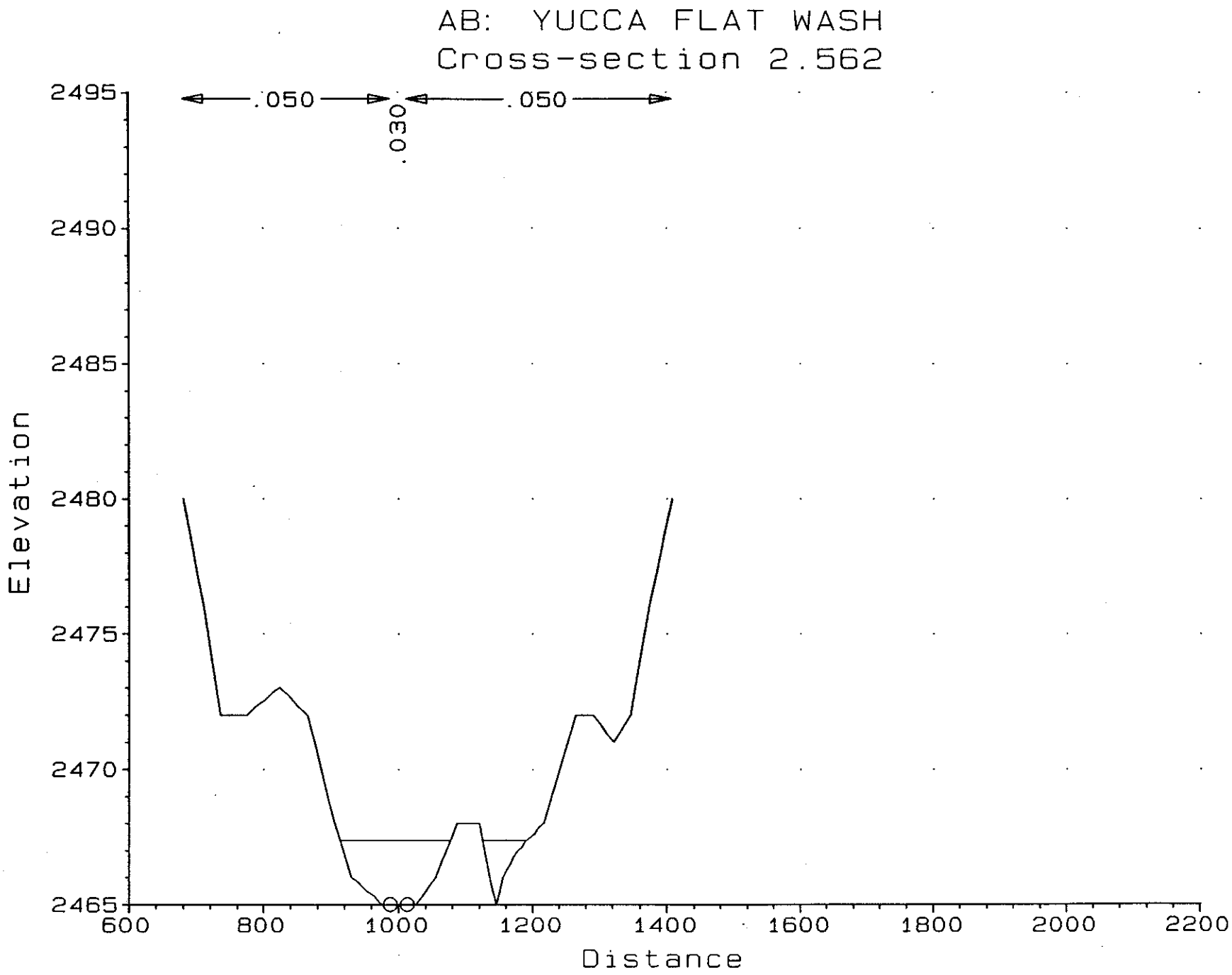
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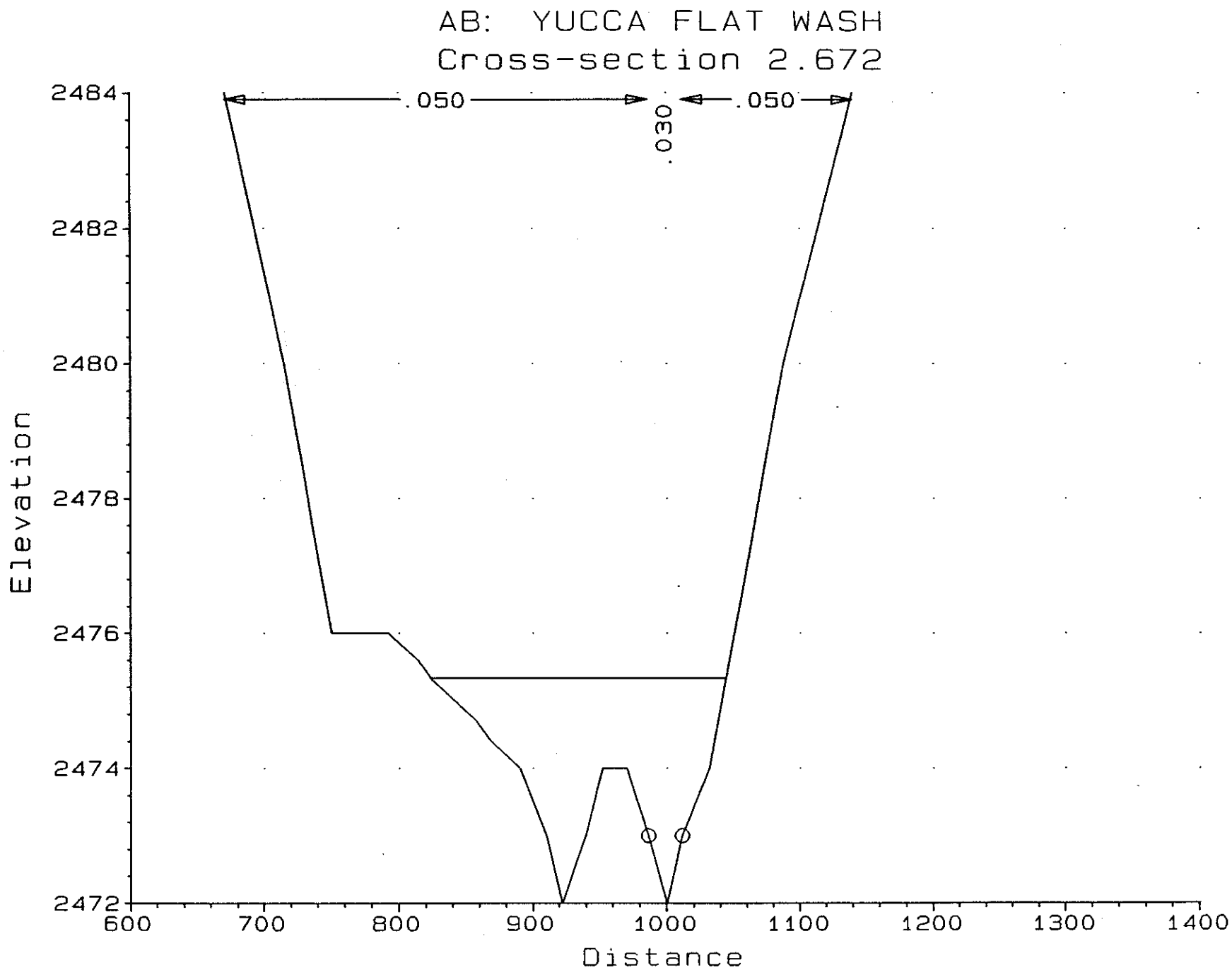
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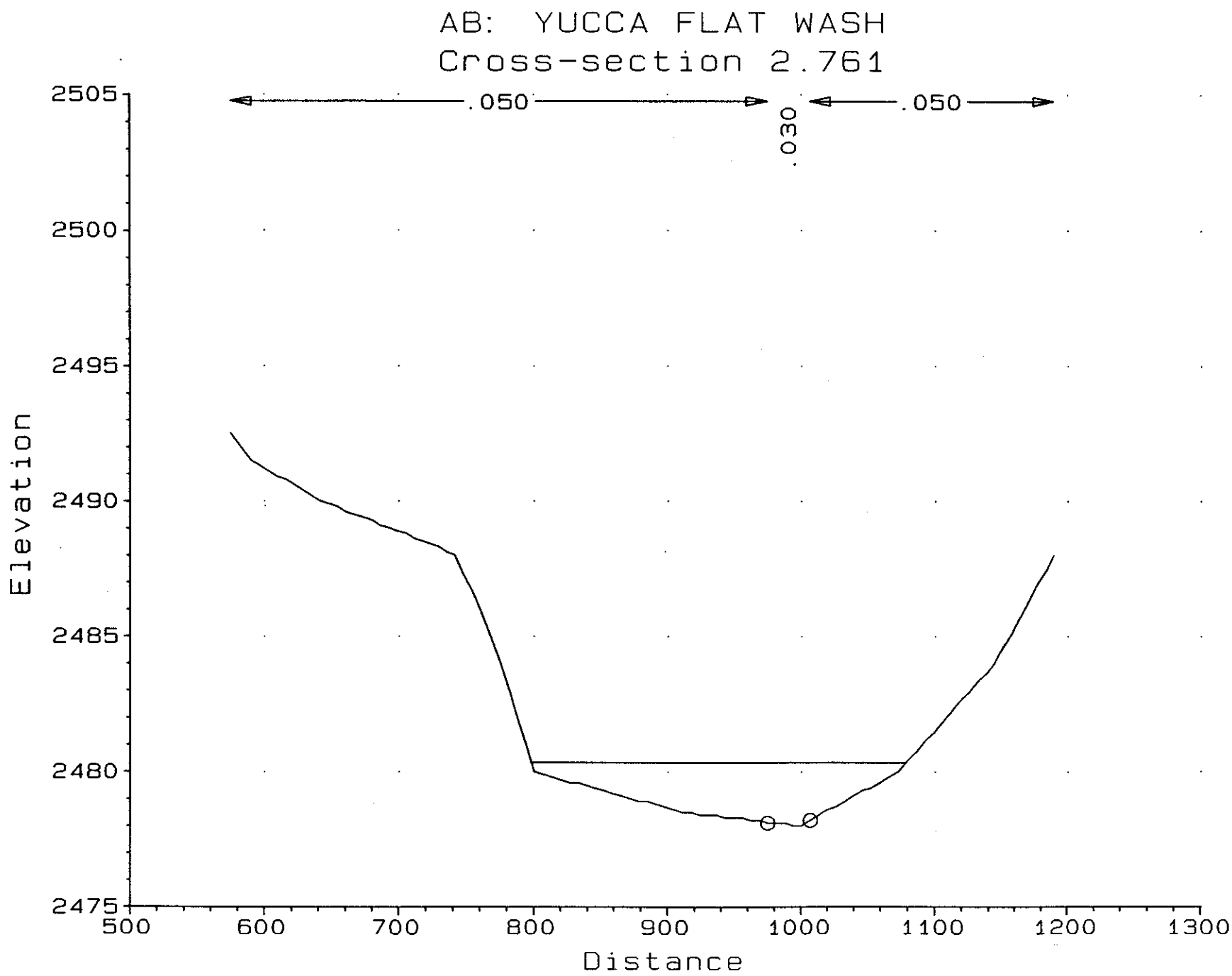
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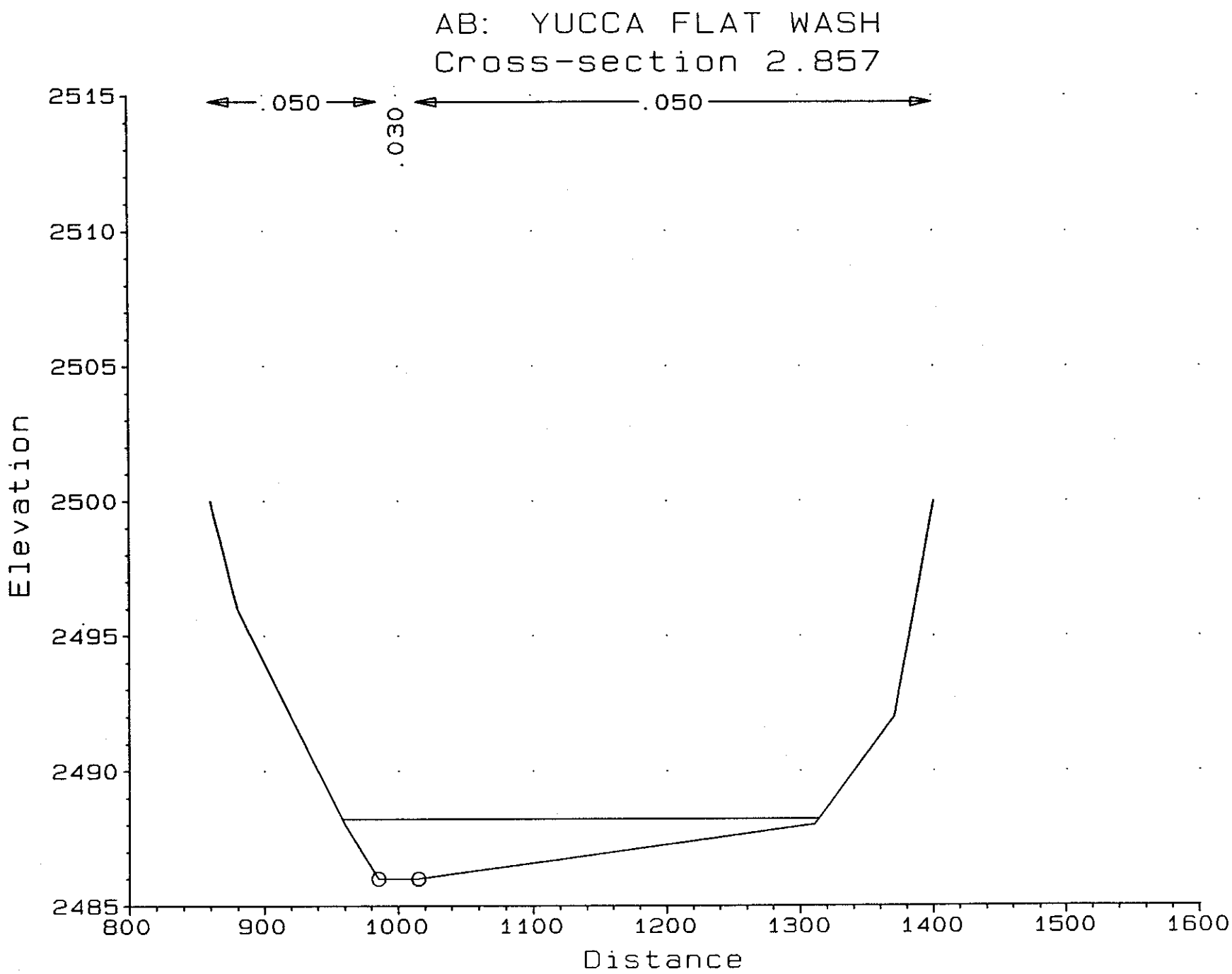
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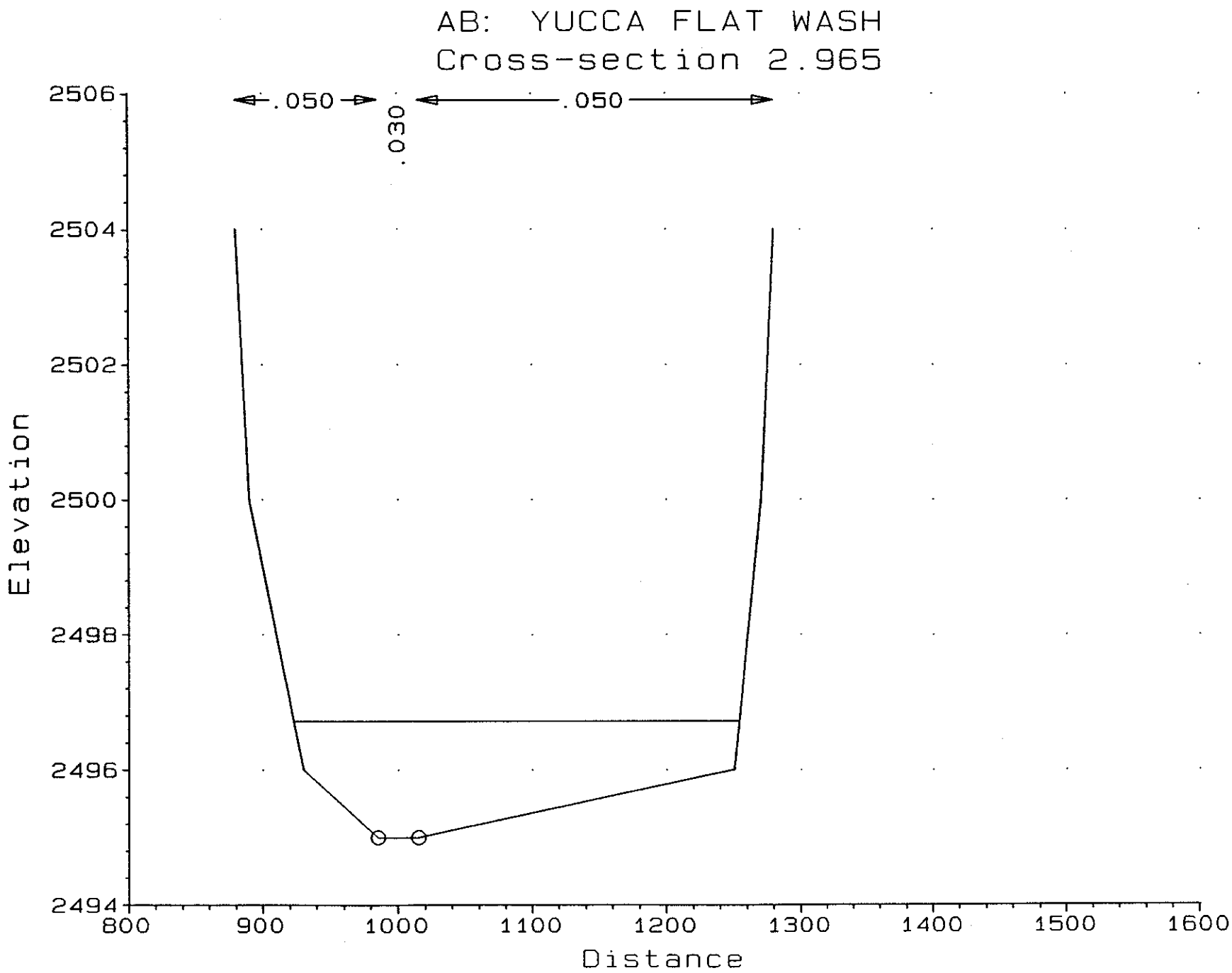
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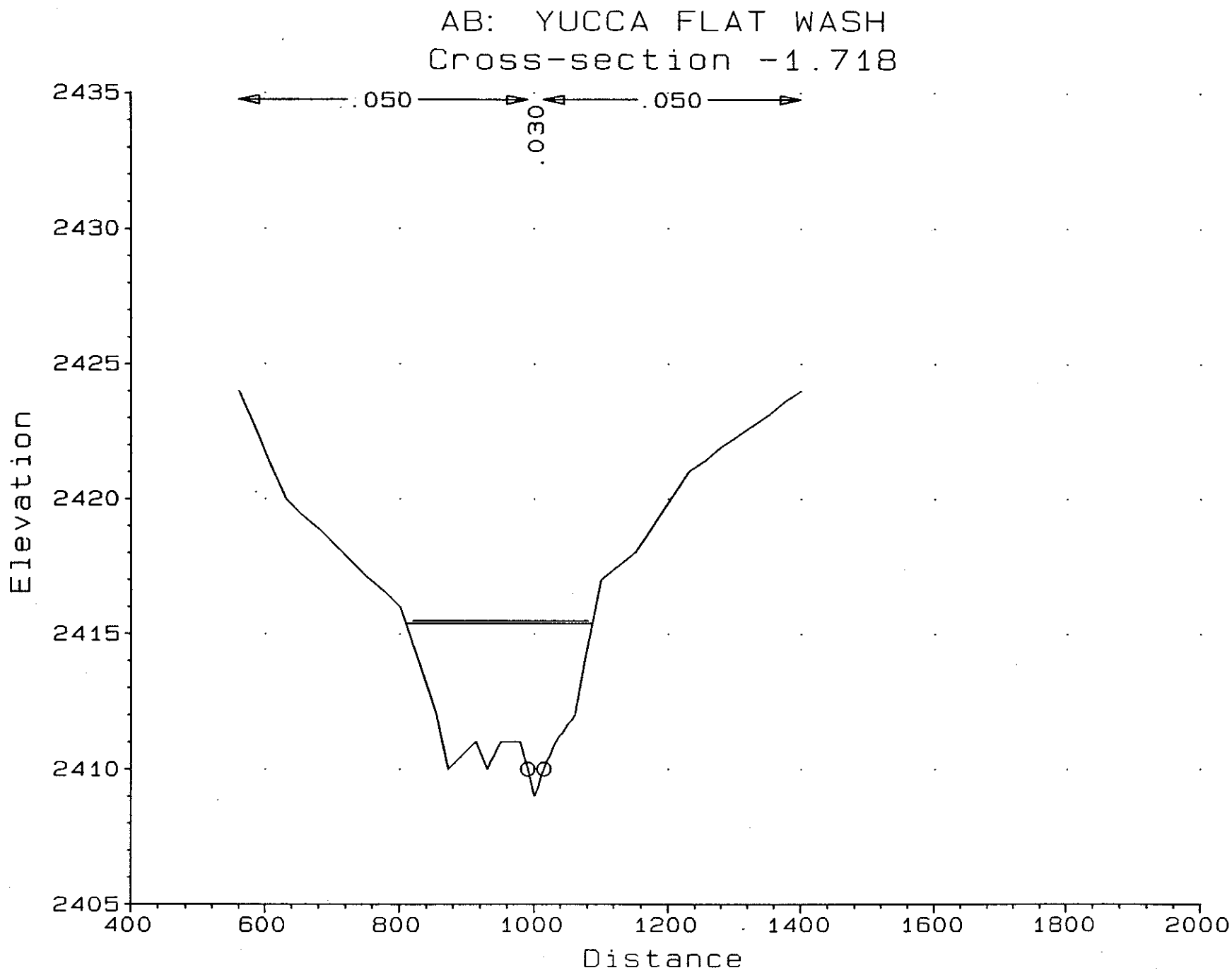
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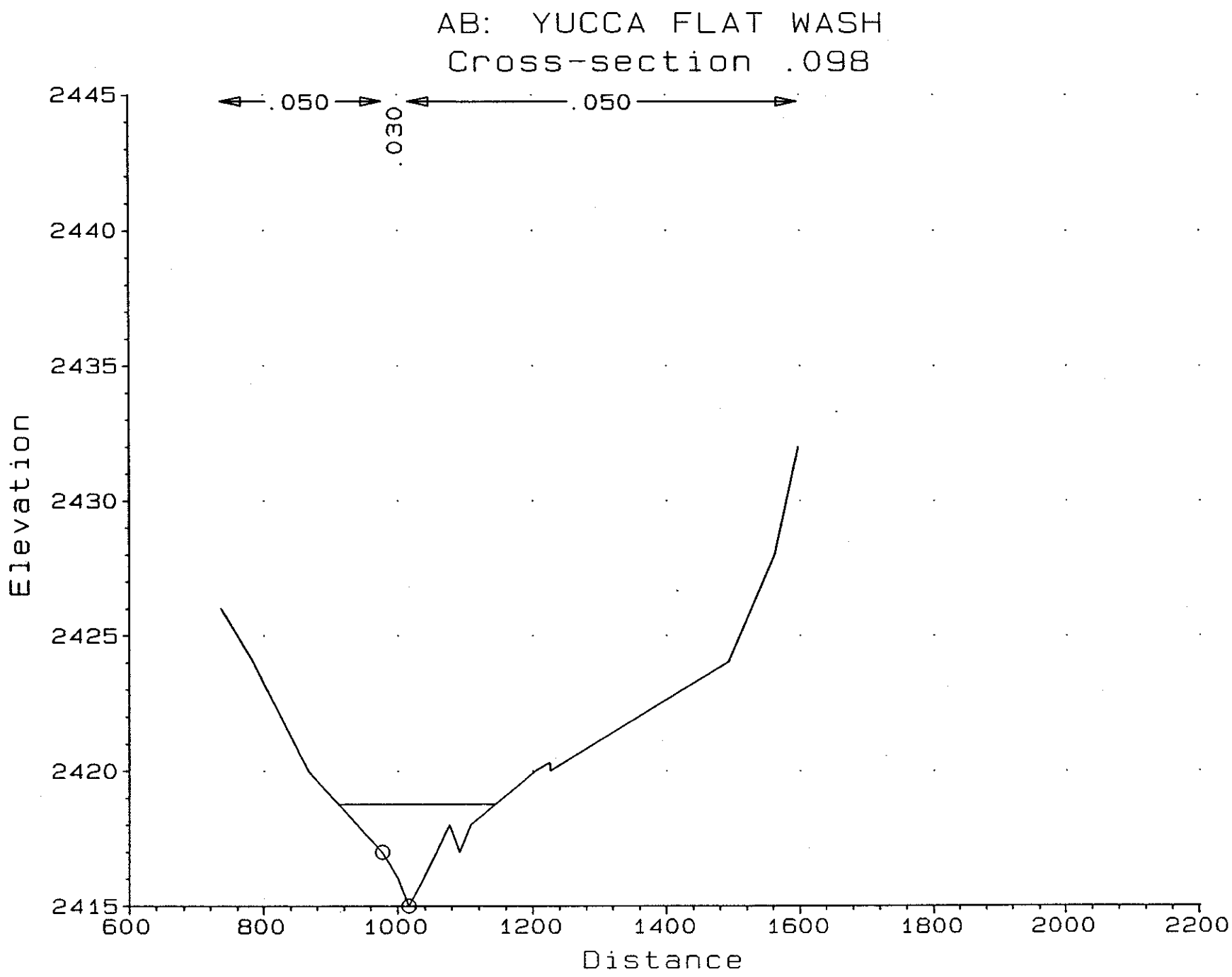
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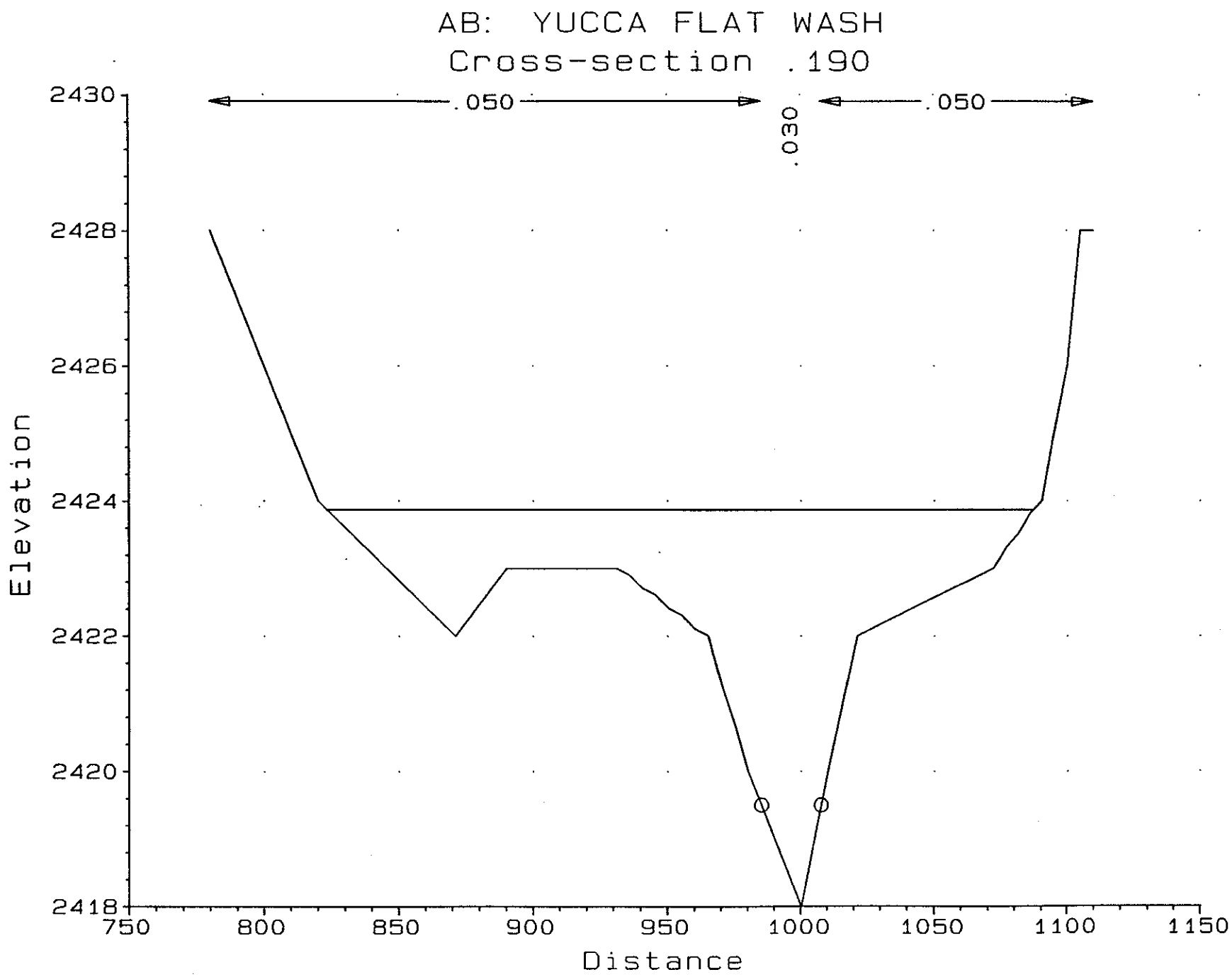
AB: YUCCA FLAT WASH
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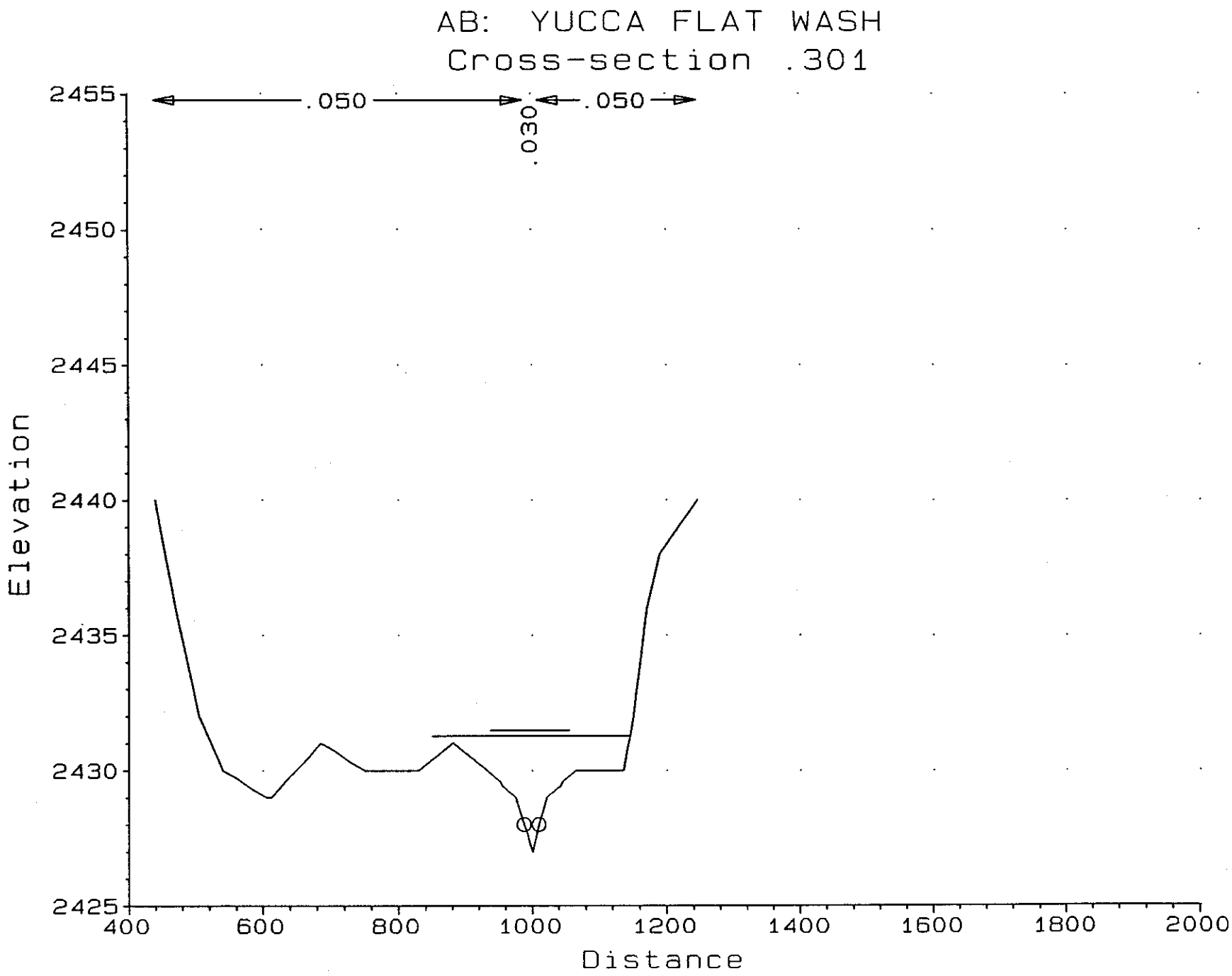
AB: YUCCA FLAT WASH
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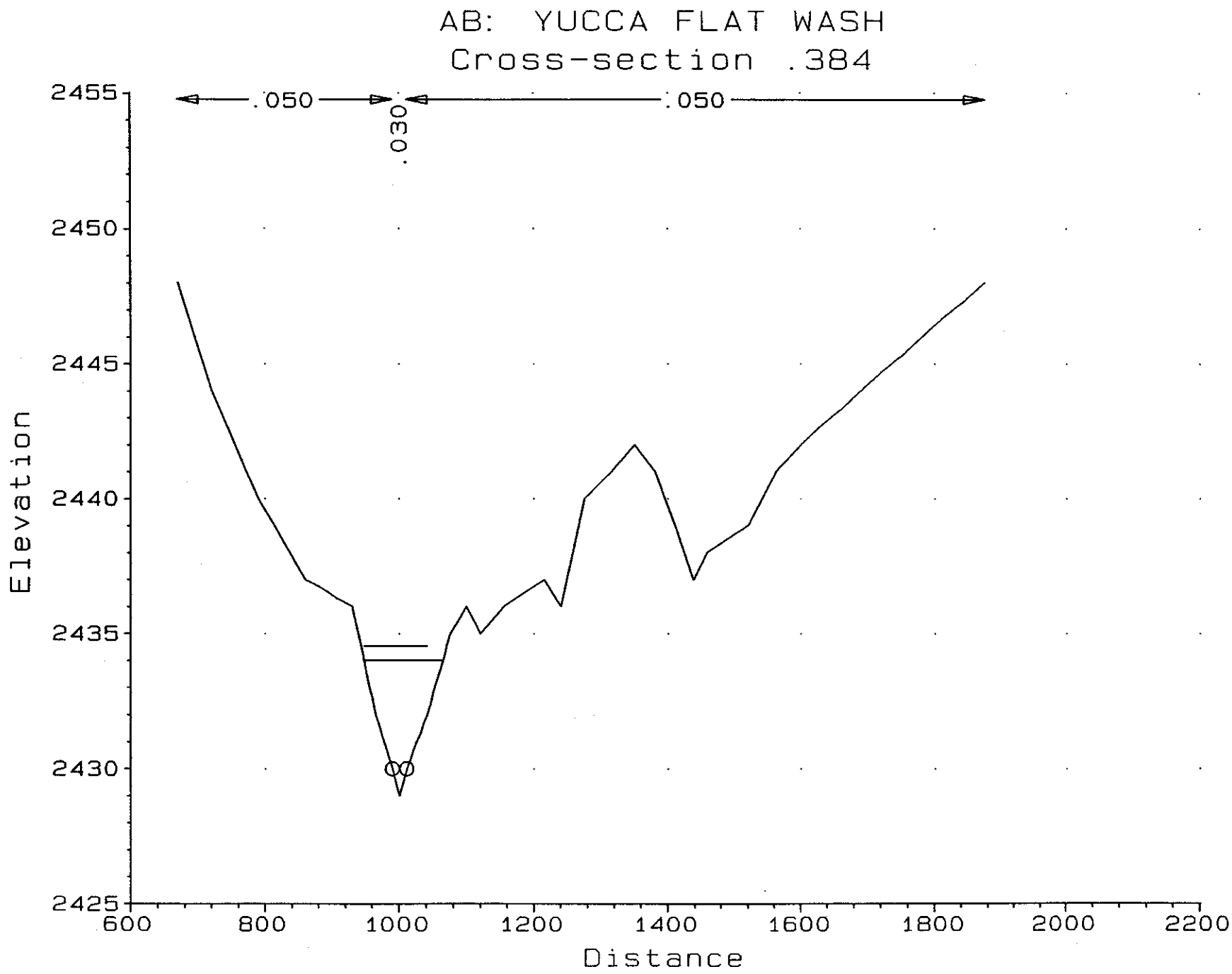
AB: YUCCA FLAT WASH
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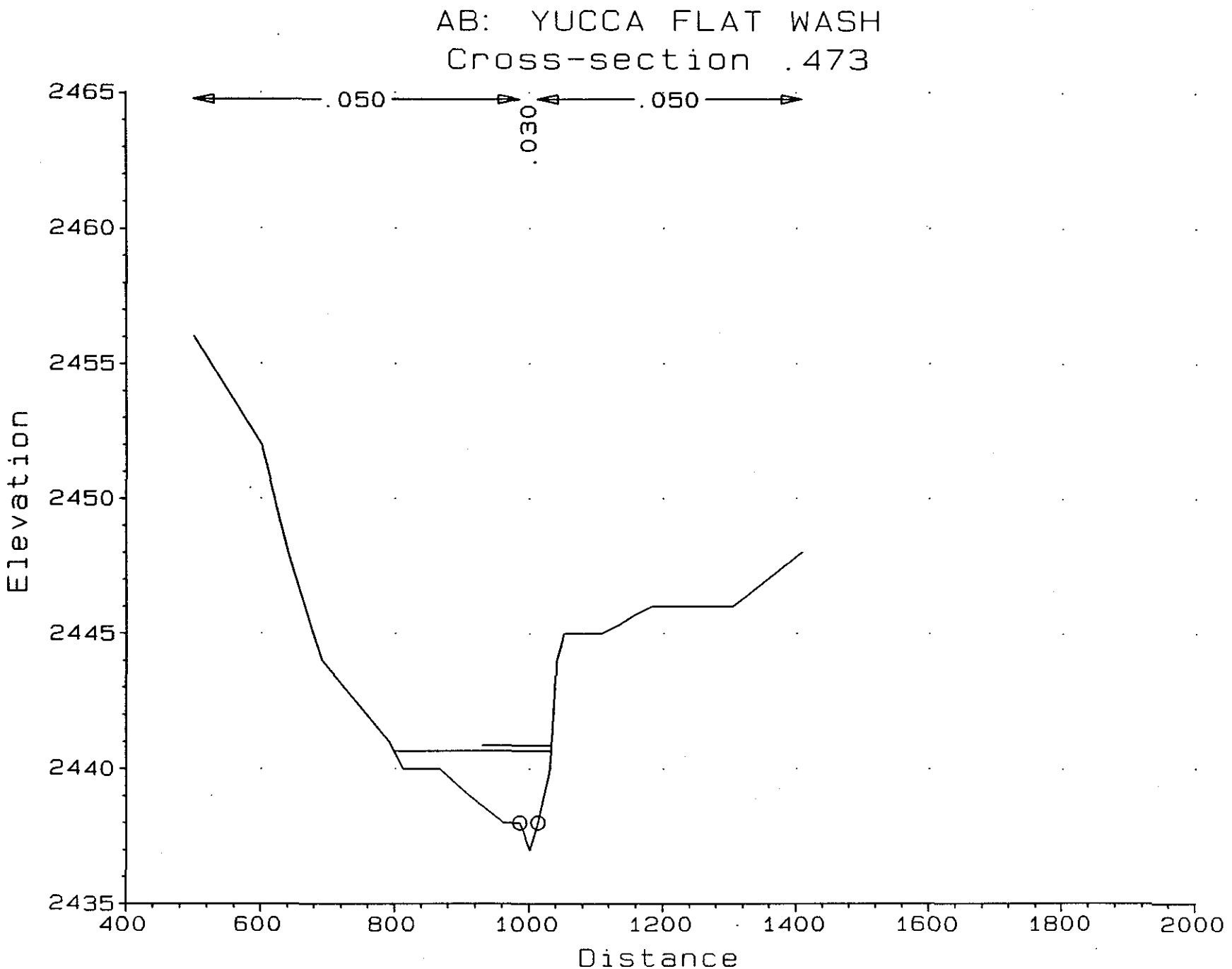
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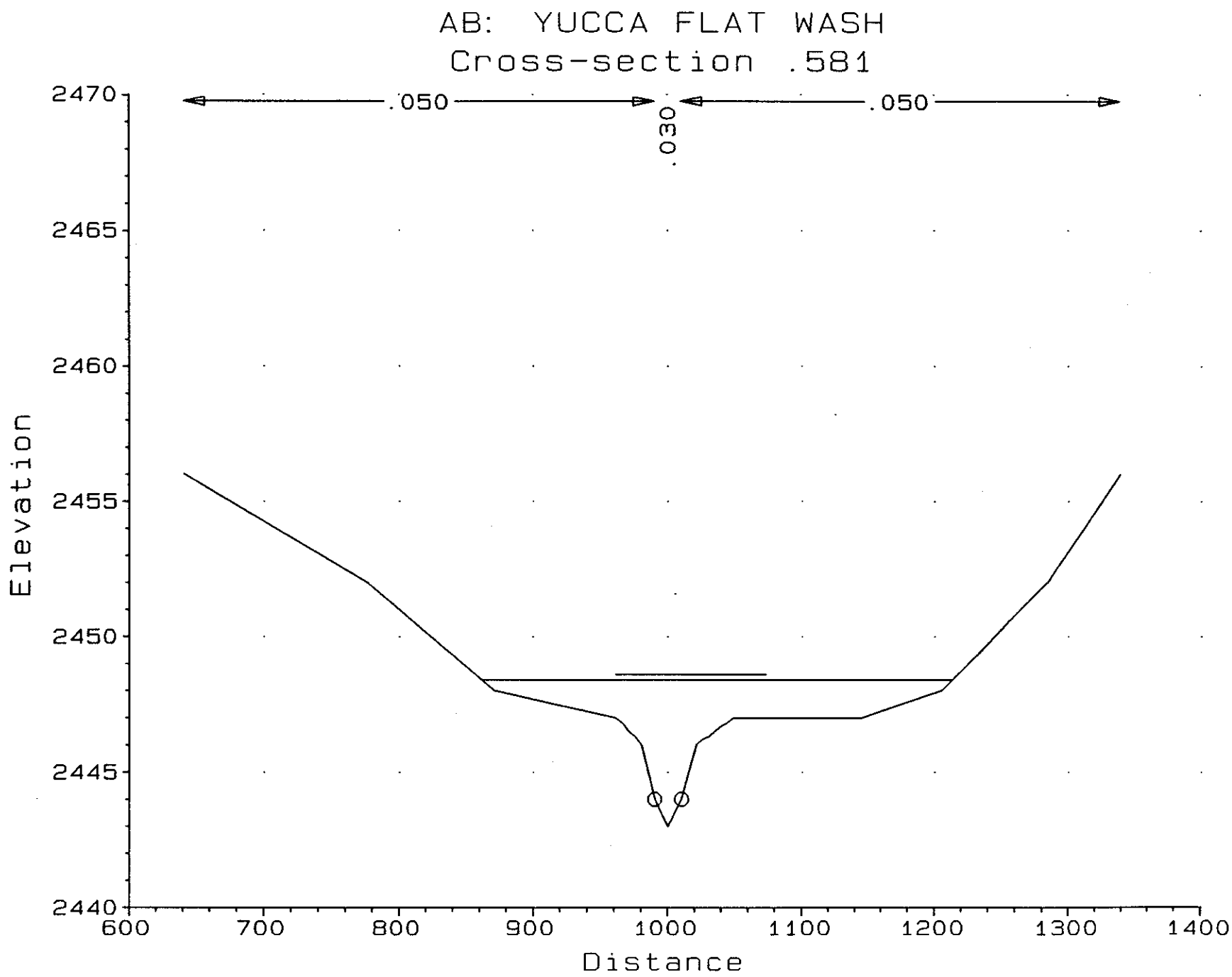
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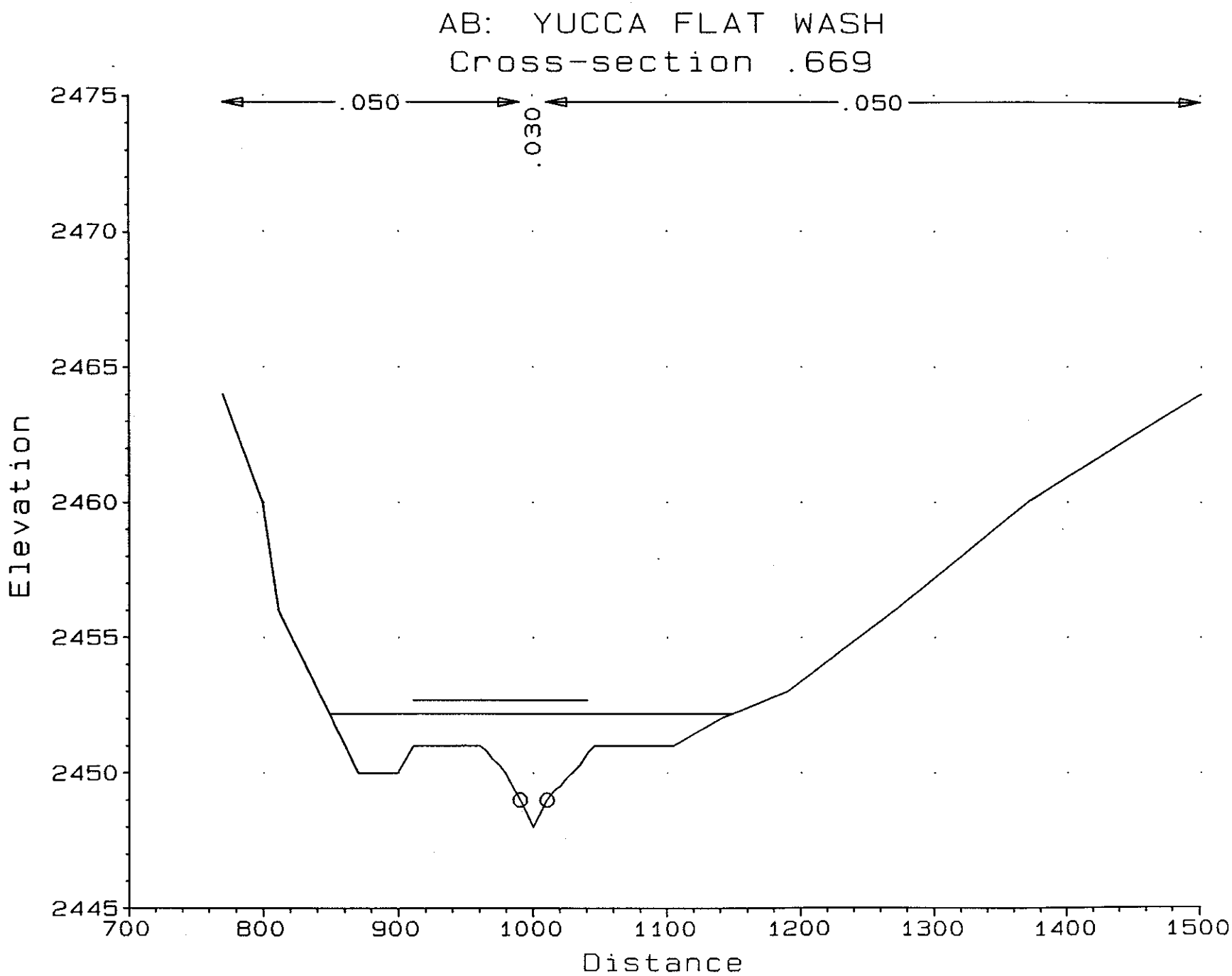
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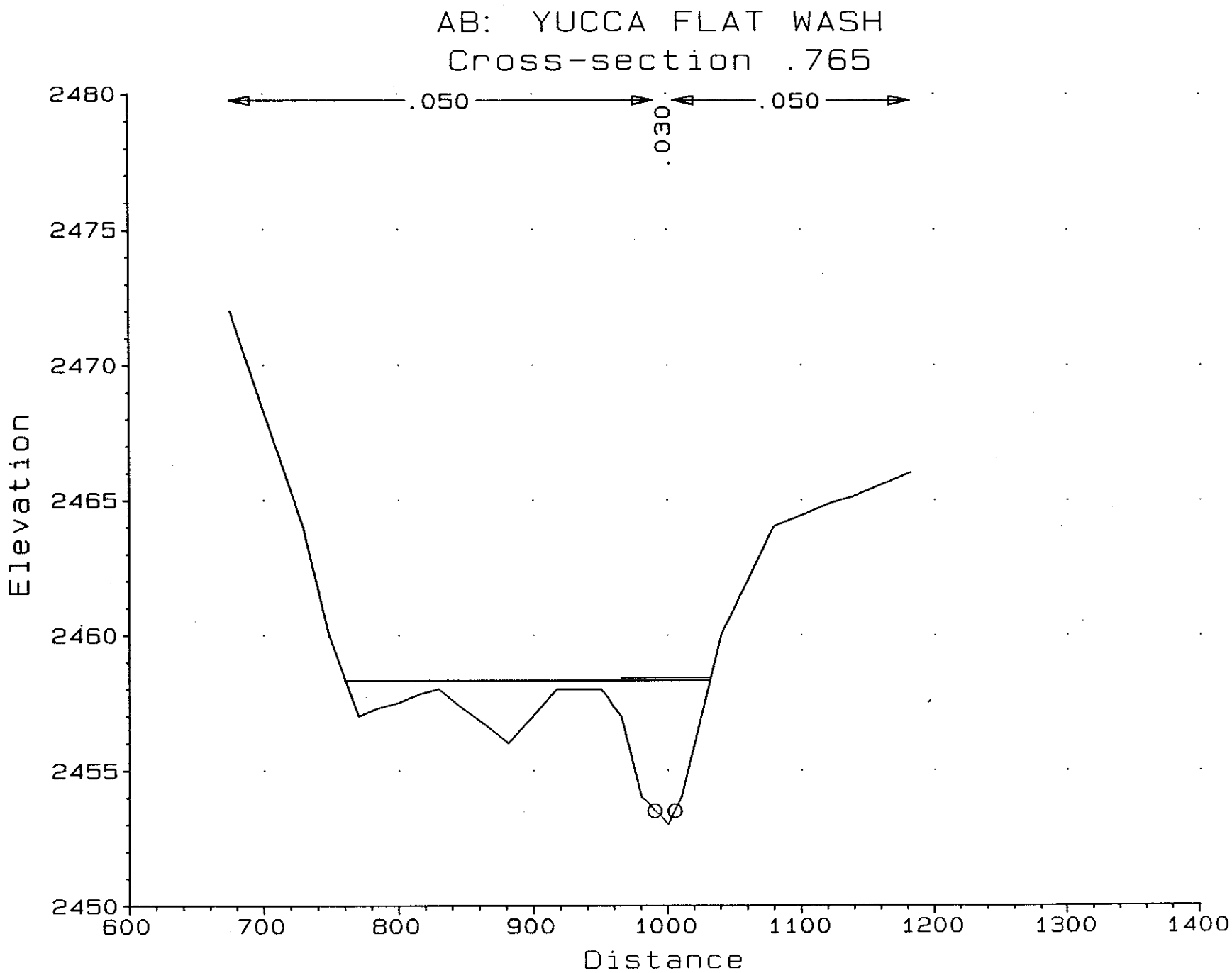
AB: YUCCA FLAT WASH
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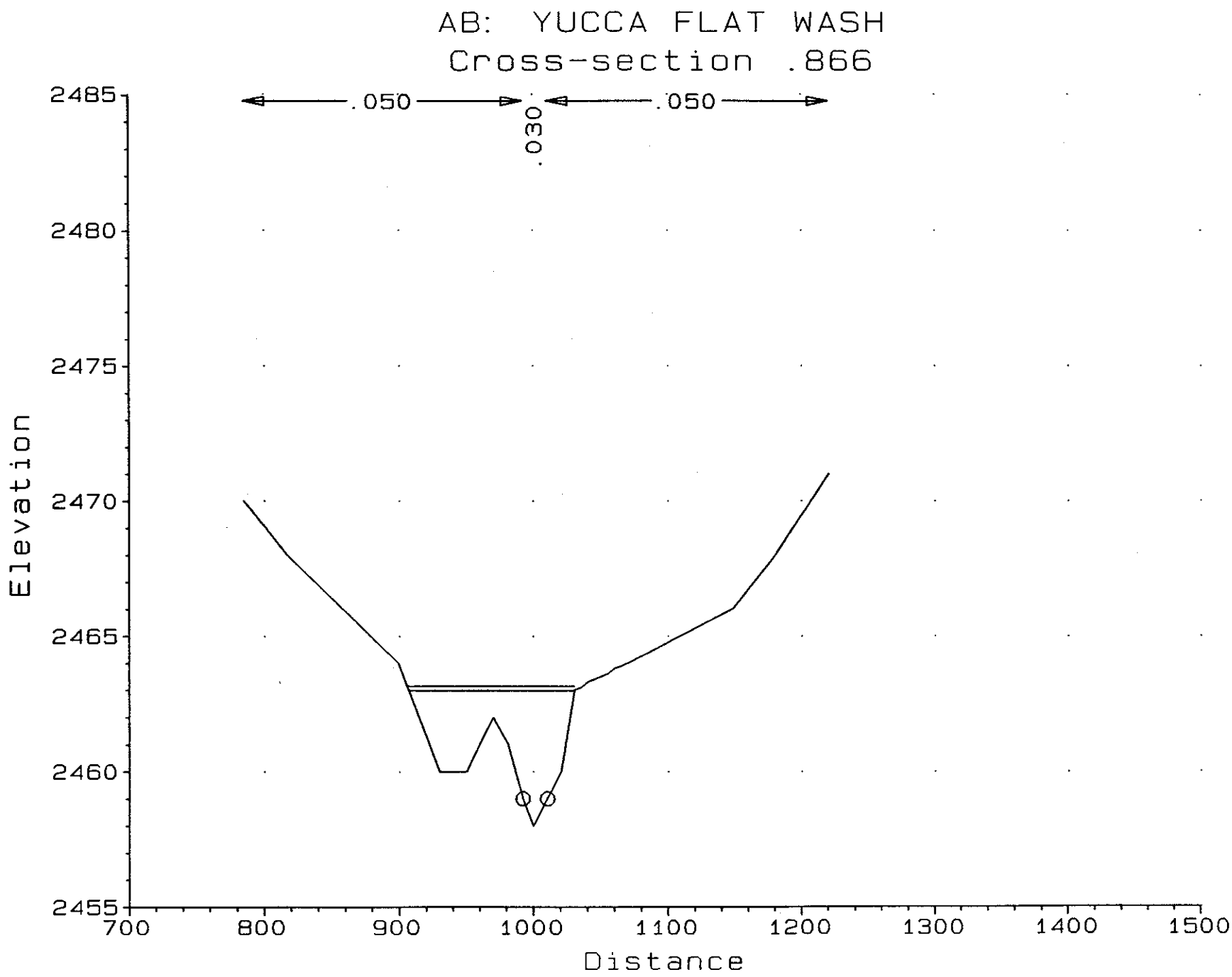
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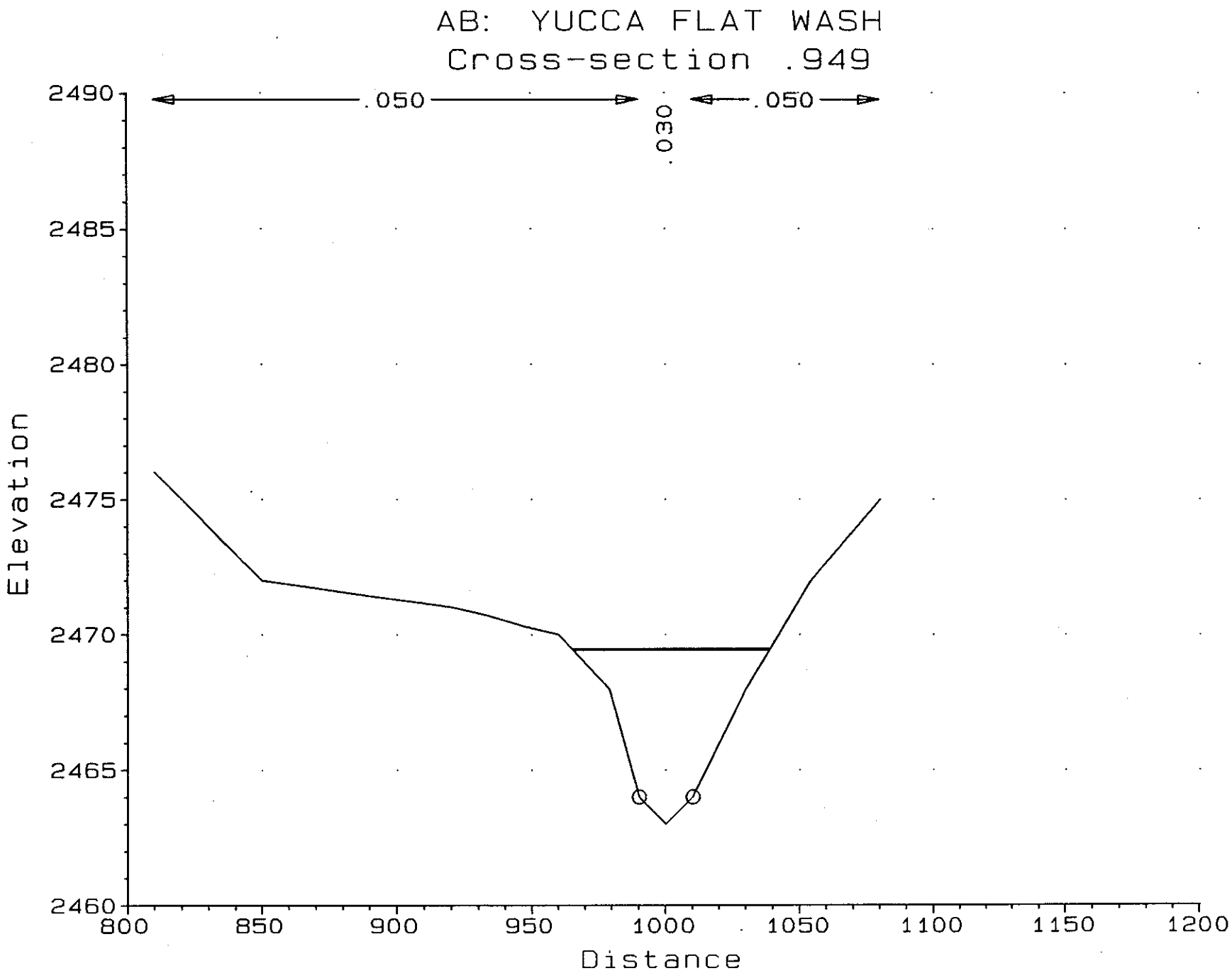
AB: YUCCA FLAT WASH
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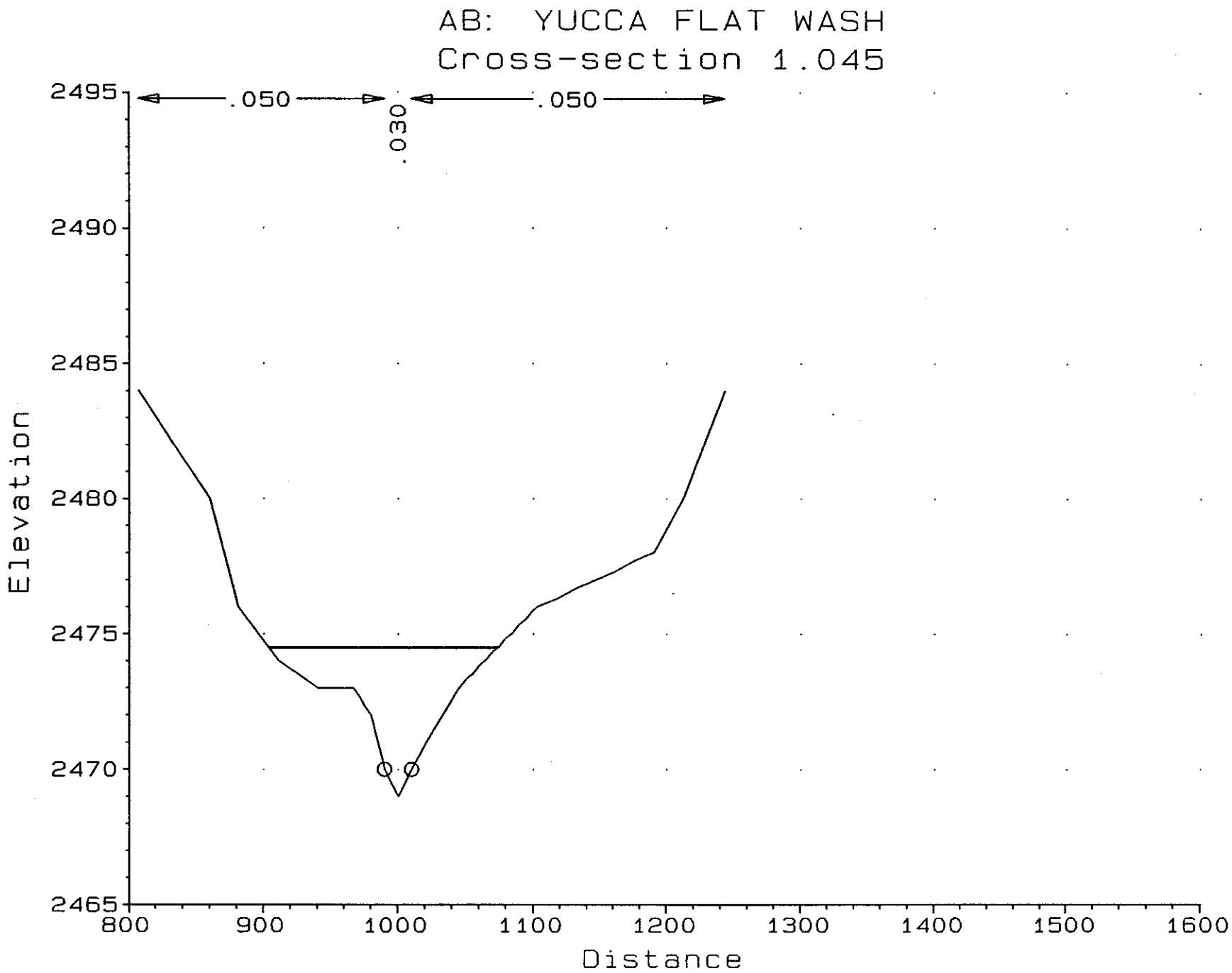
AB: YUCCA FLAT WASH
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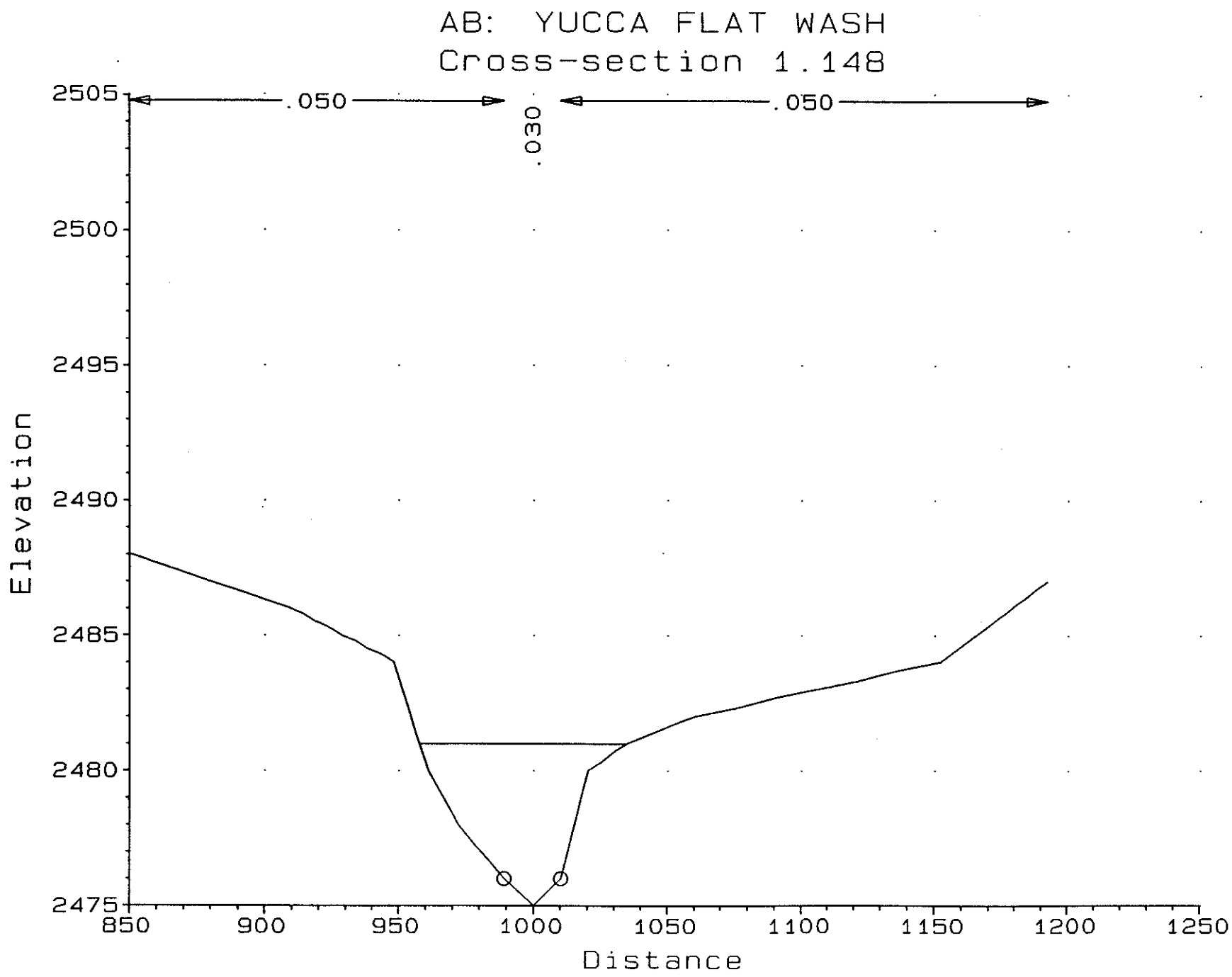
AB: YUCCA FLAT WASH
Cross-section 1.148
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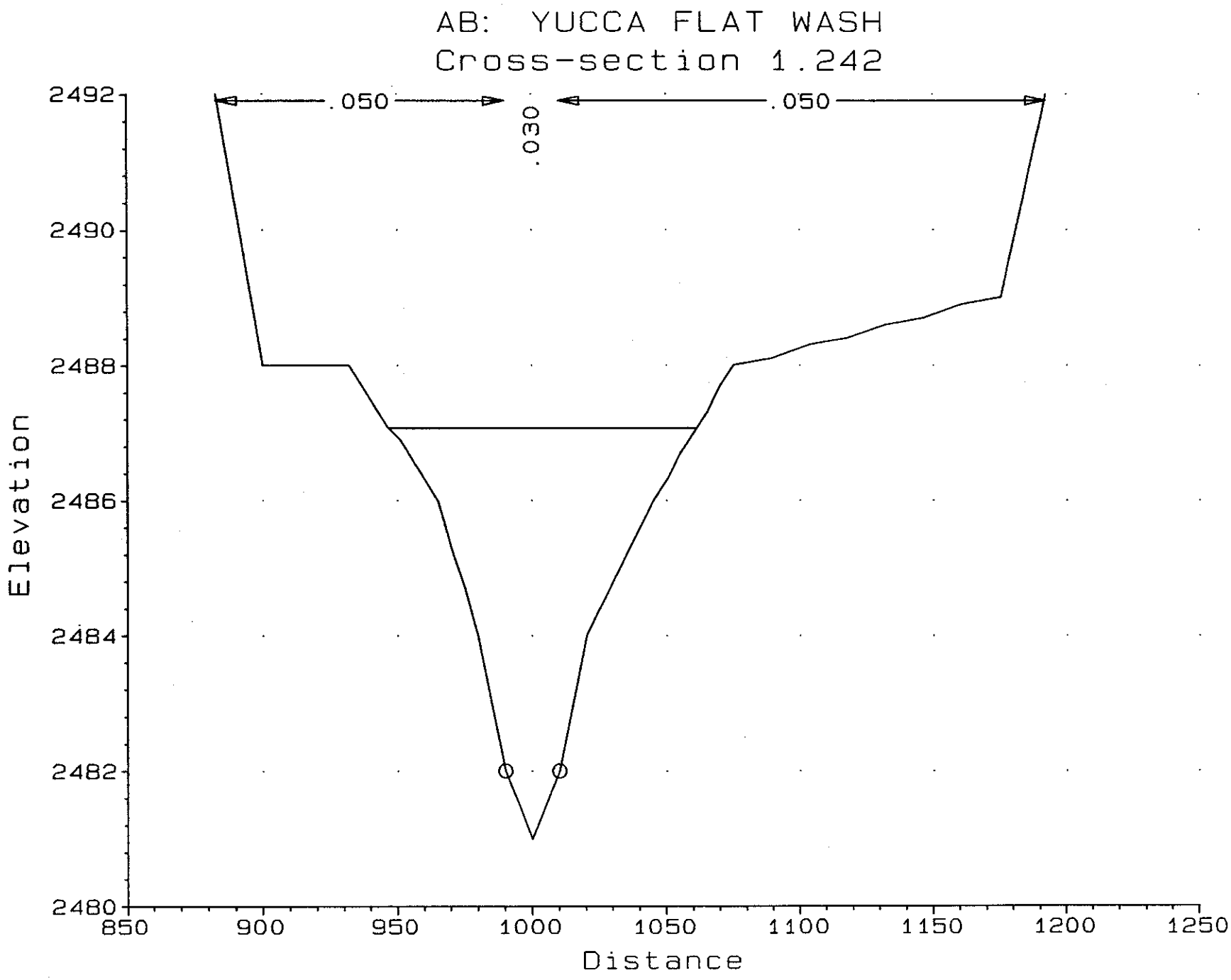
Distance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Cross-section 1.242
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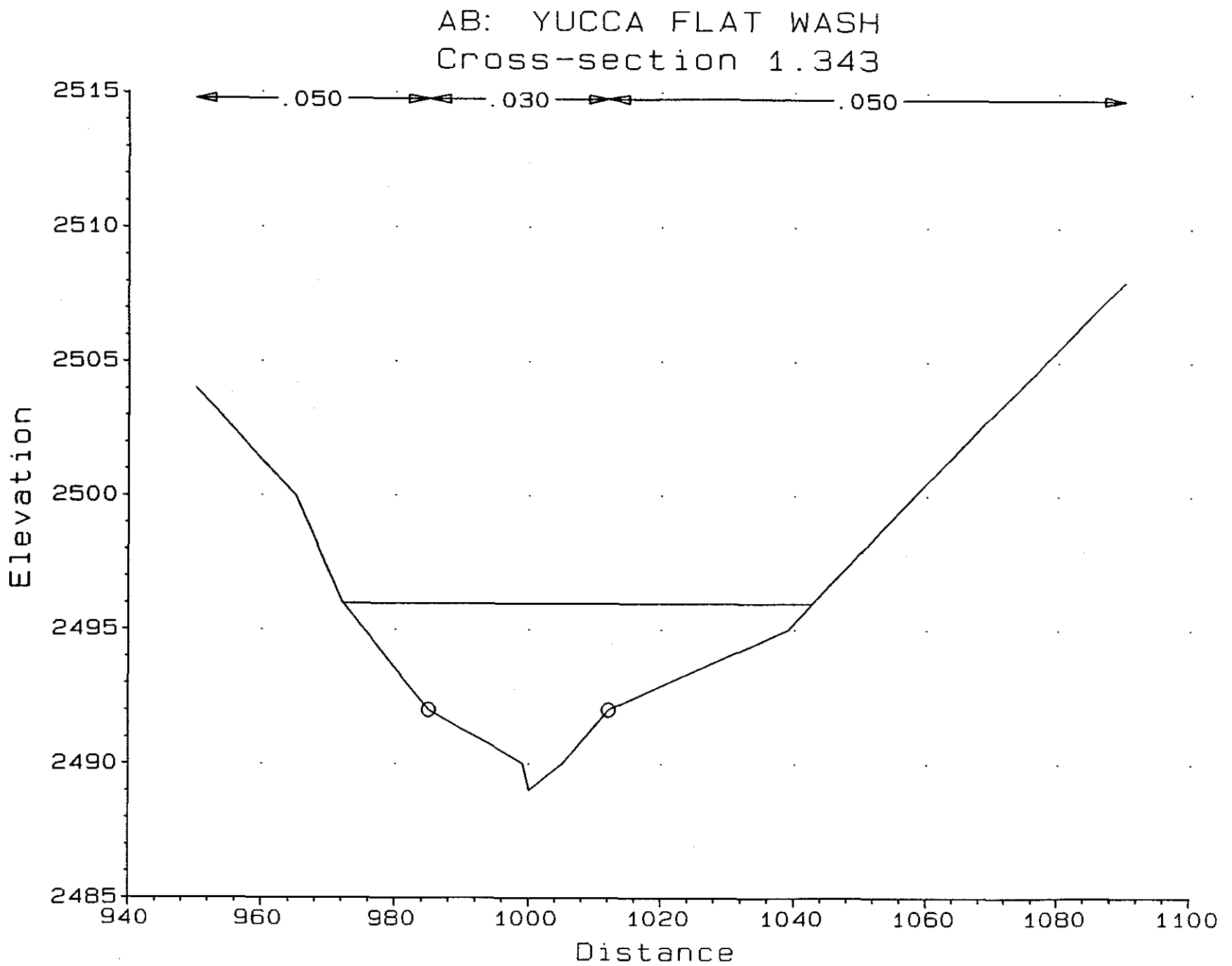
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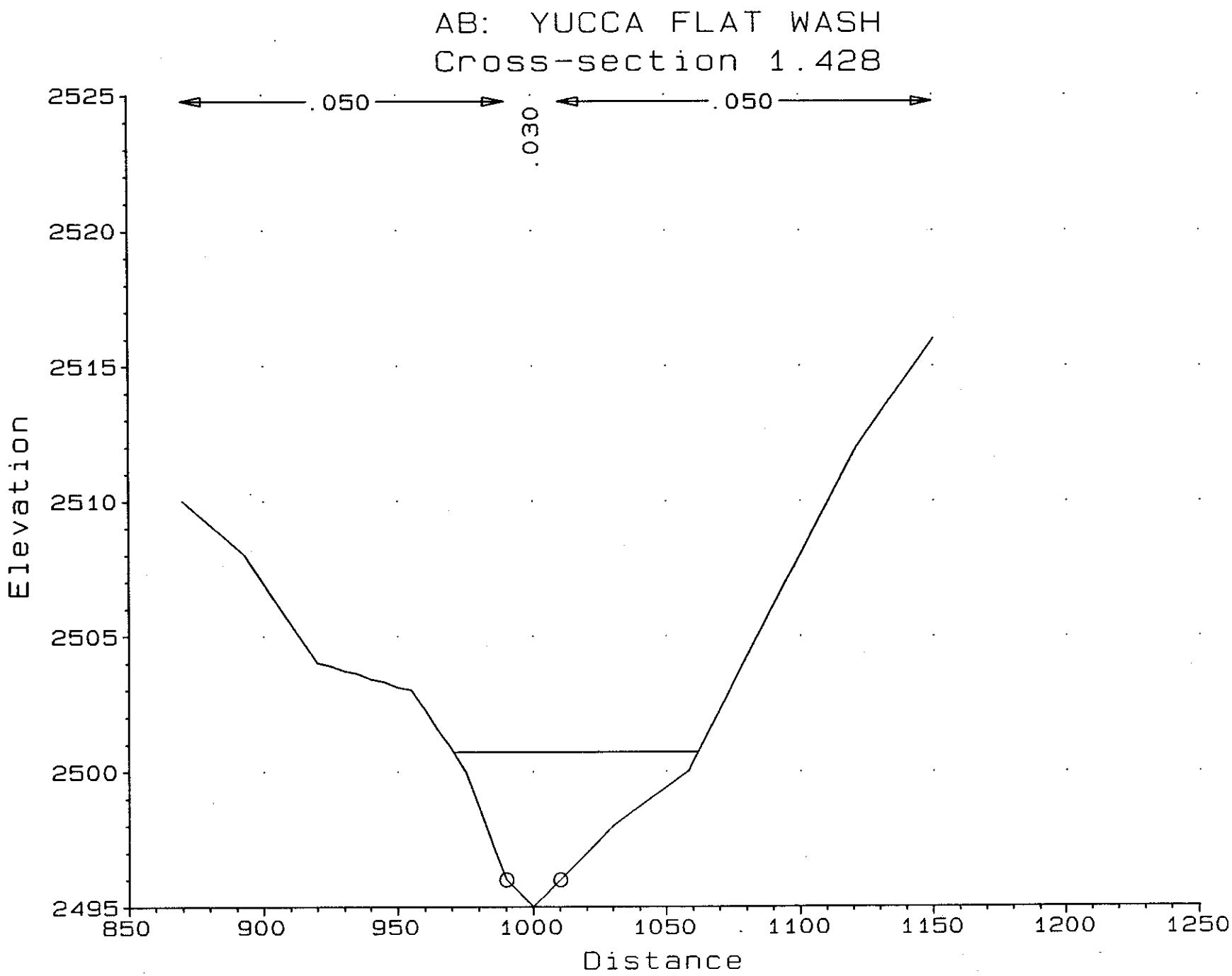
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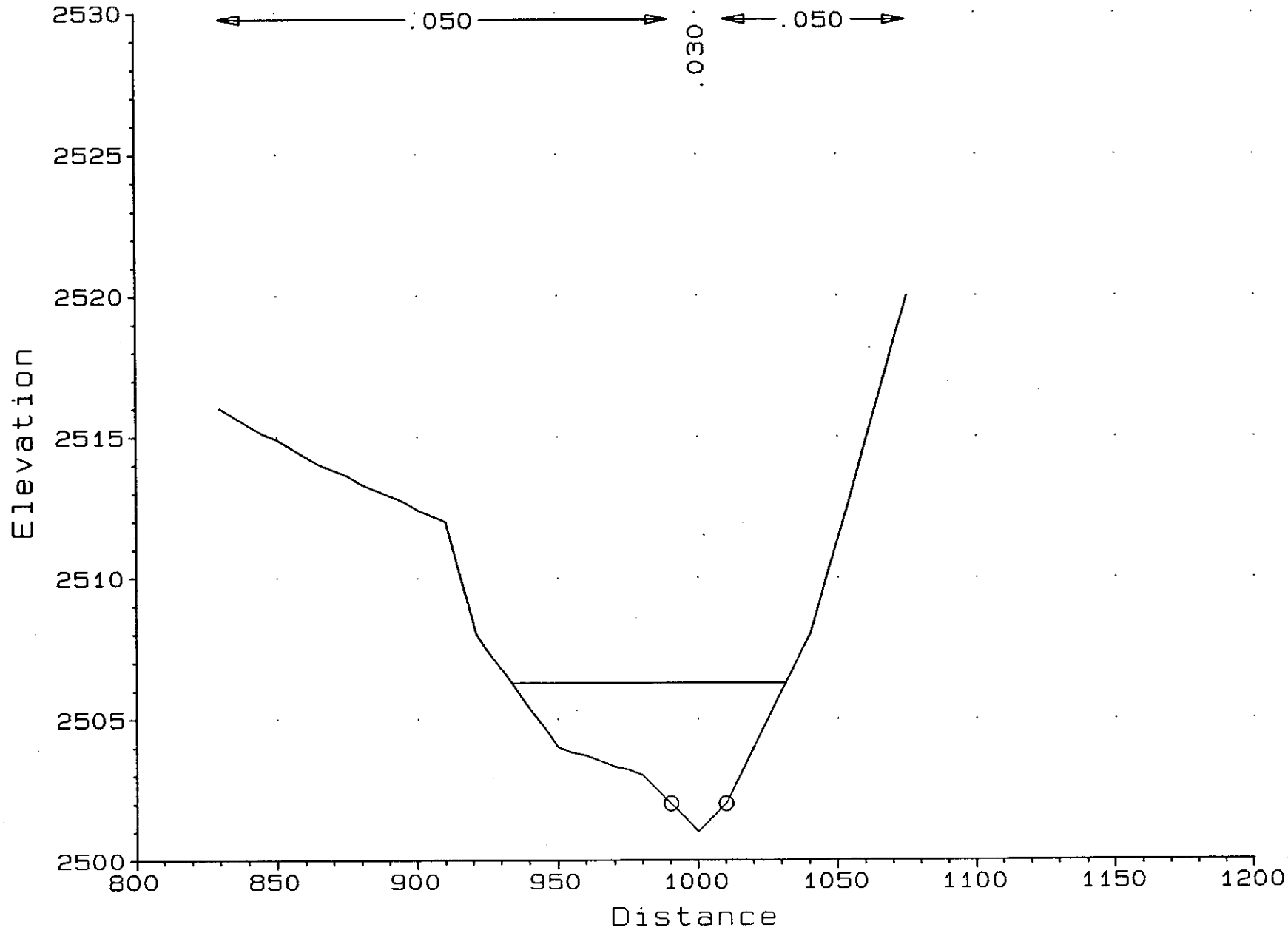
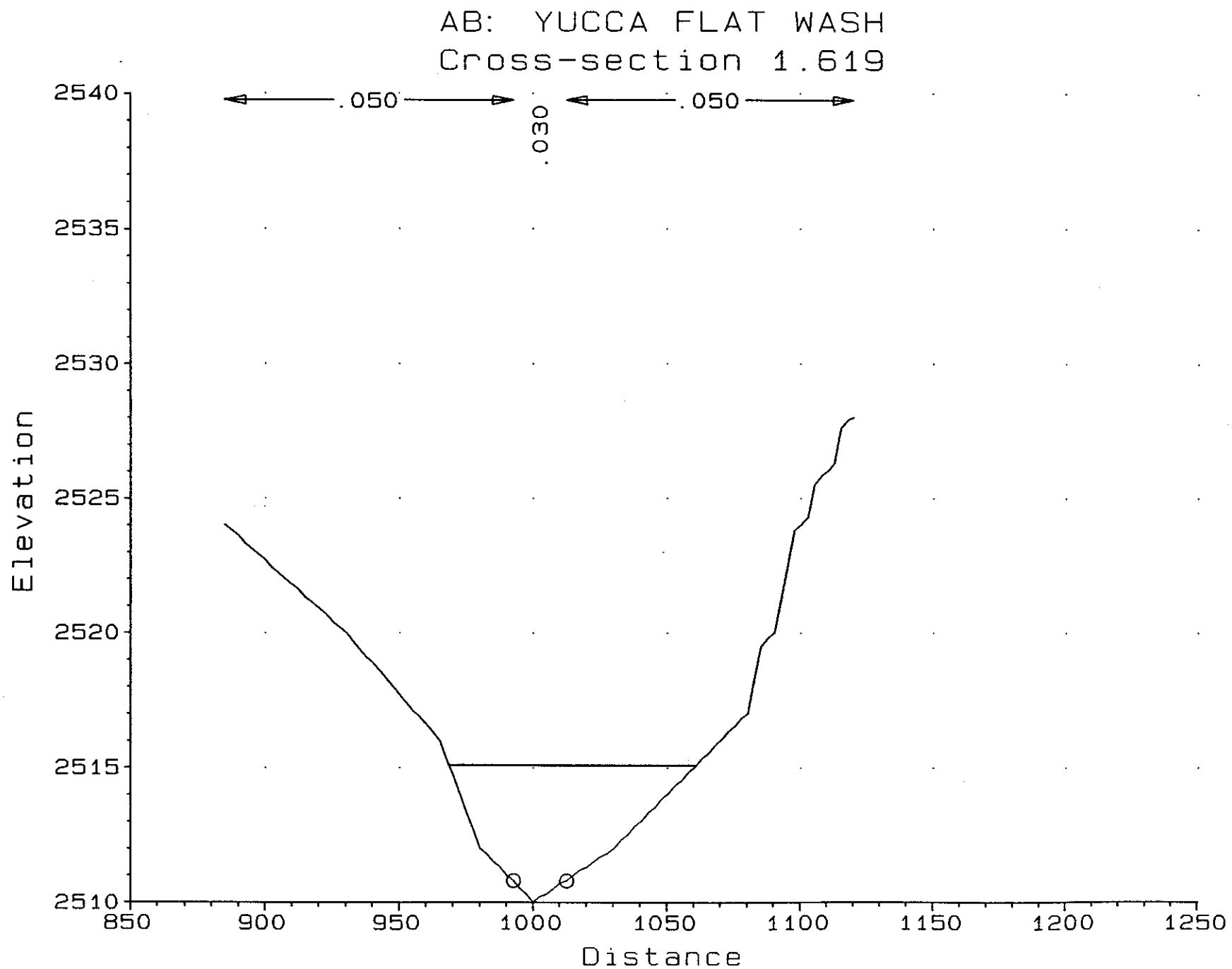
1250
Distance

AB: YUCCA FLAT WASH
Cross-section 1.525

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Elevation
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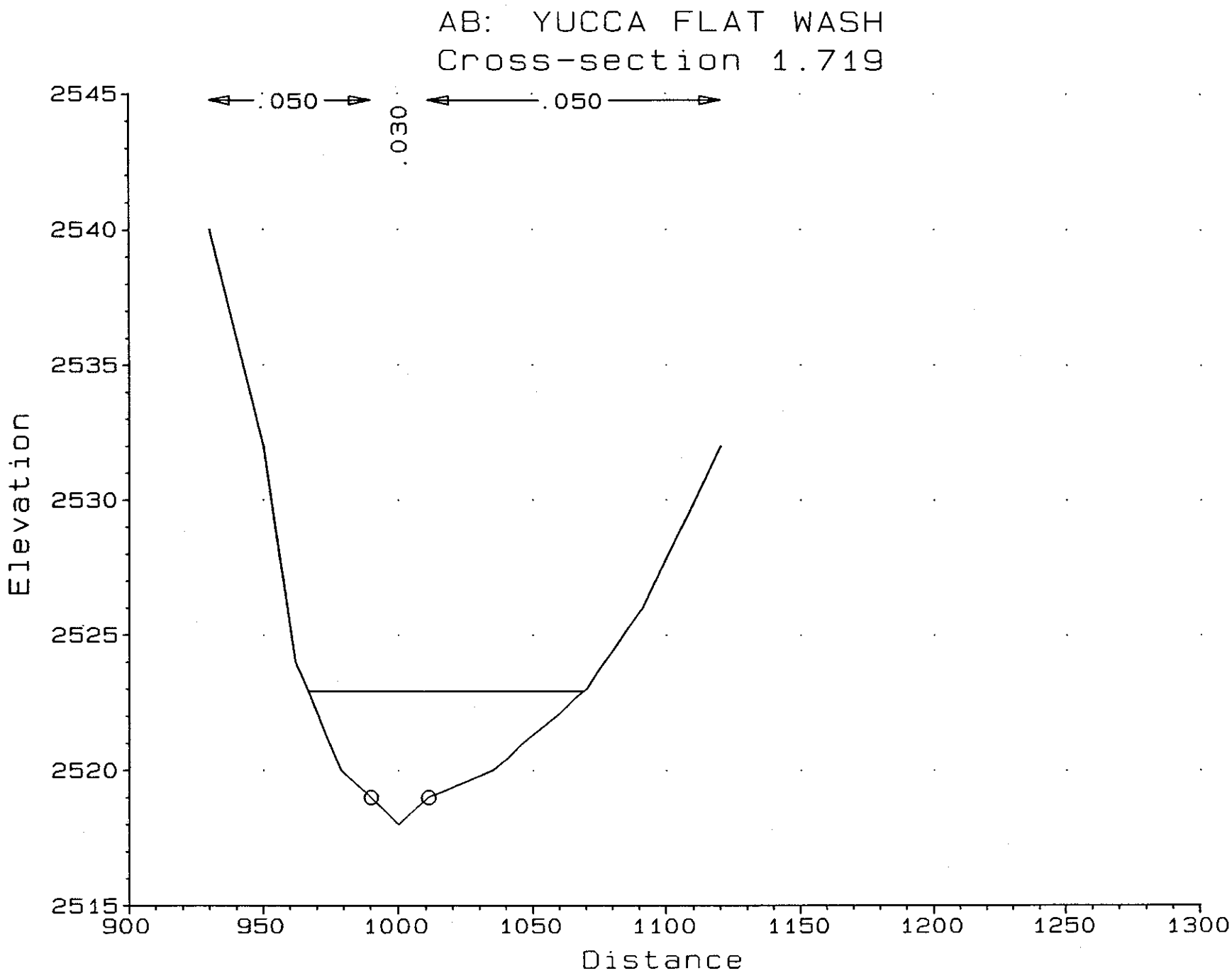
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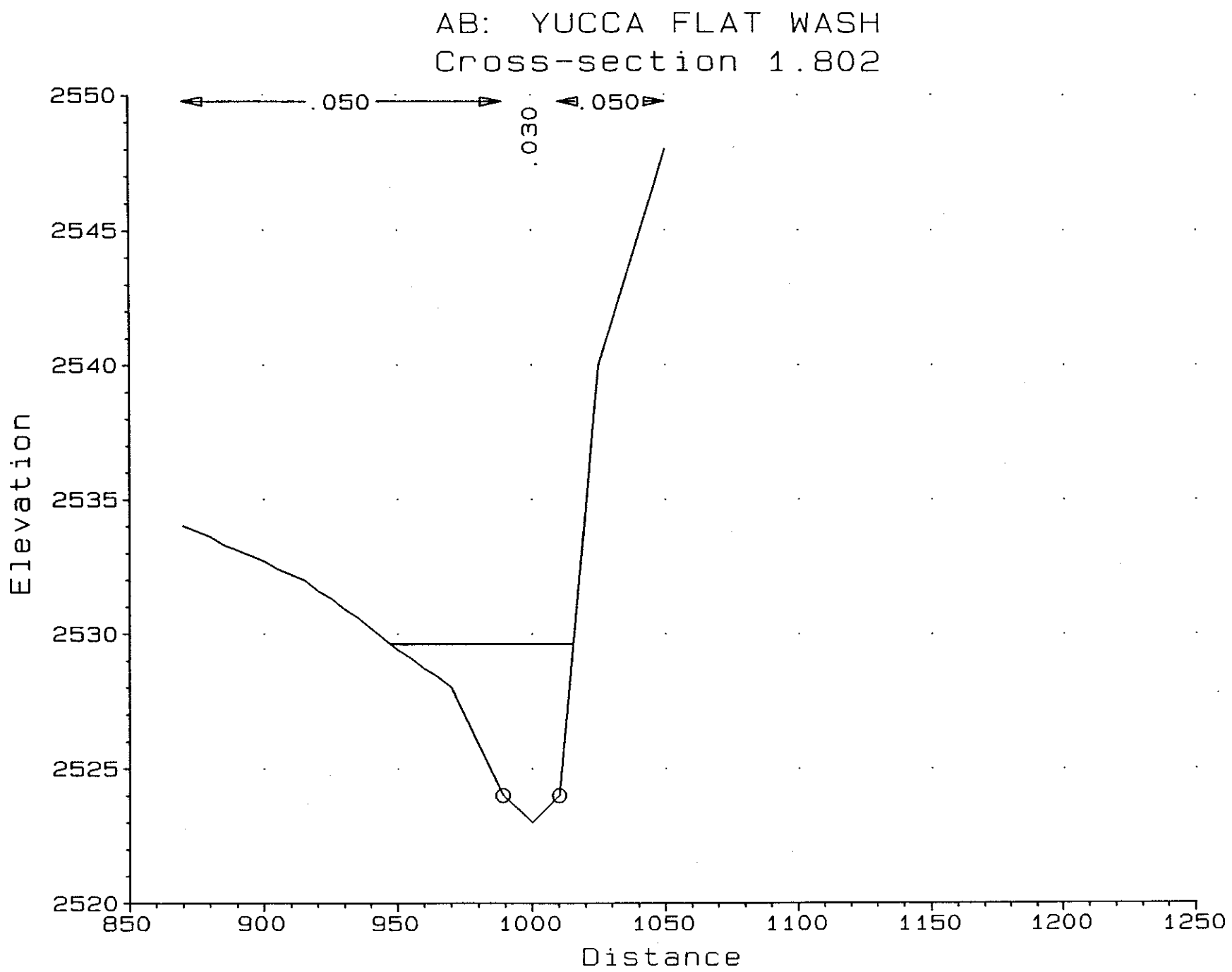
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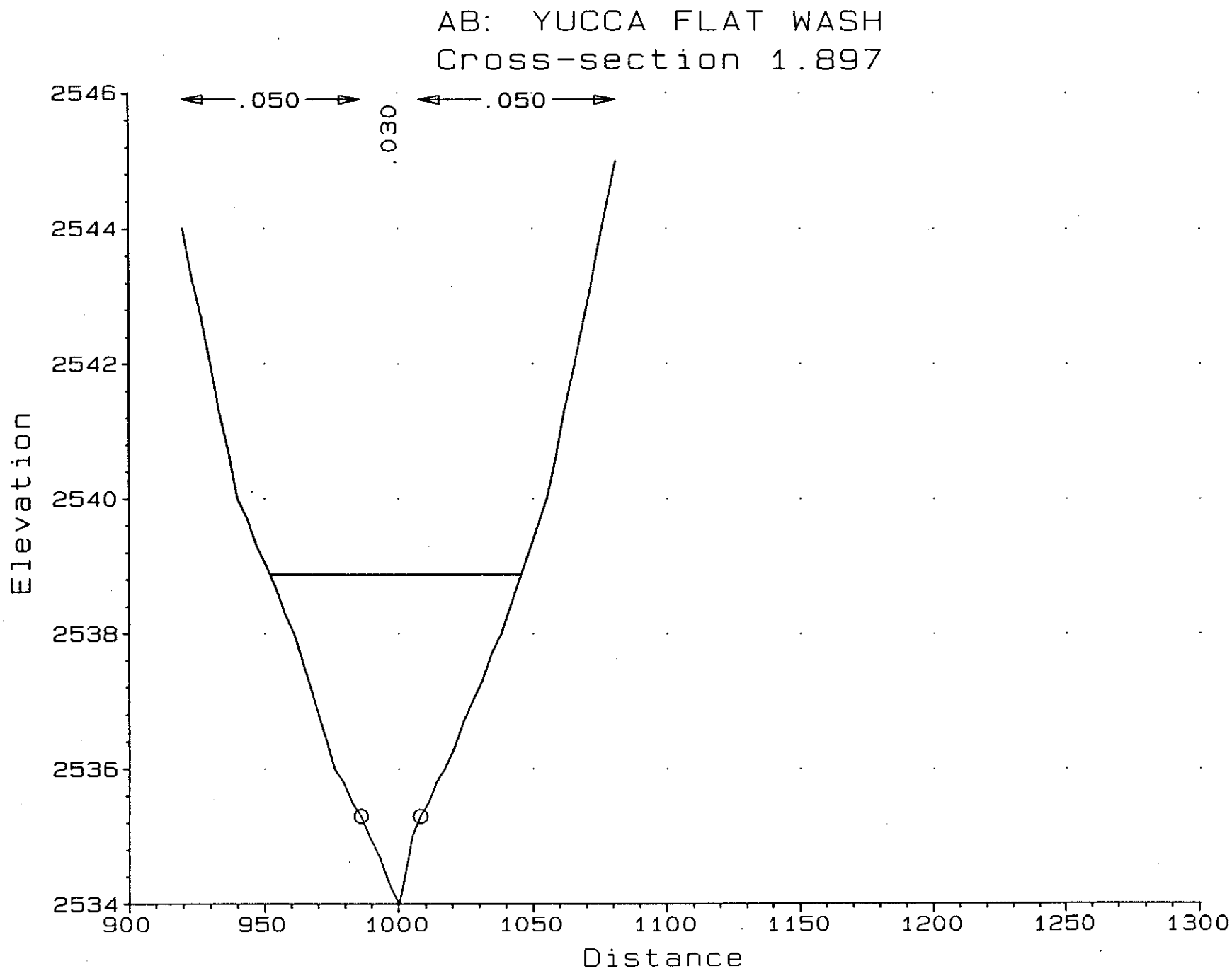
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Elevation
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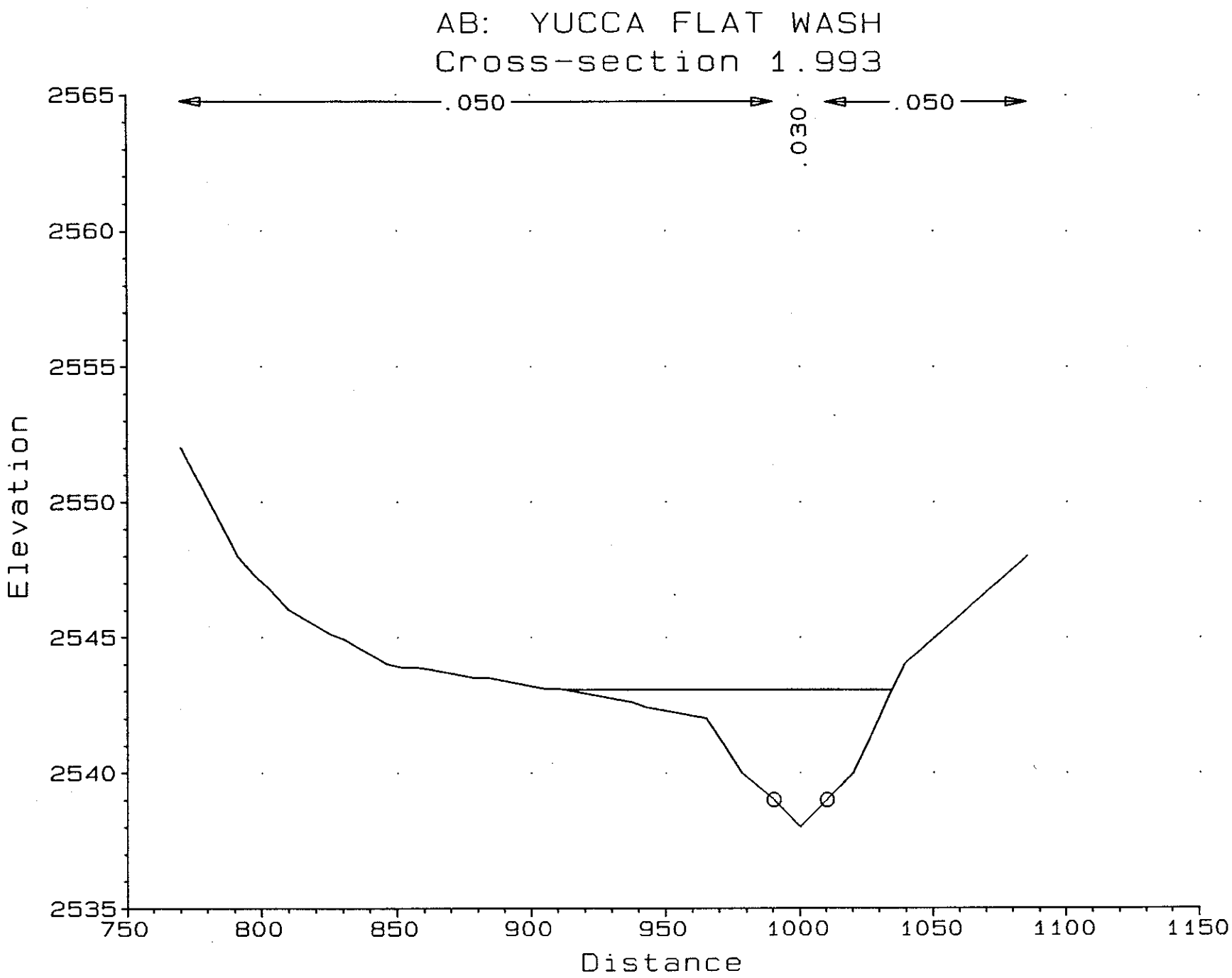
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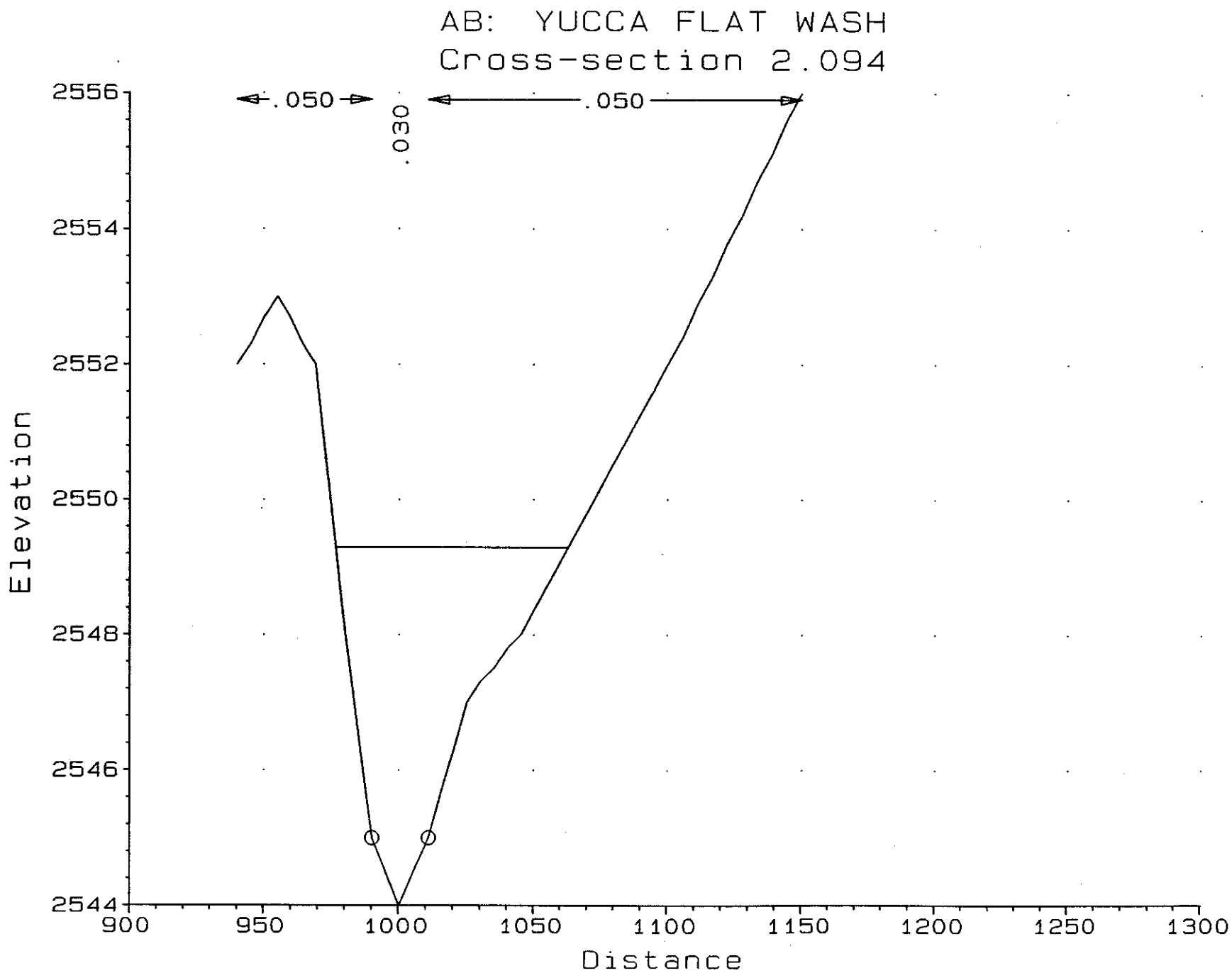
AB: YUCCA FLAT WASH
Cross-section 2.094
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Elevation
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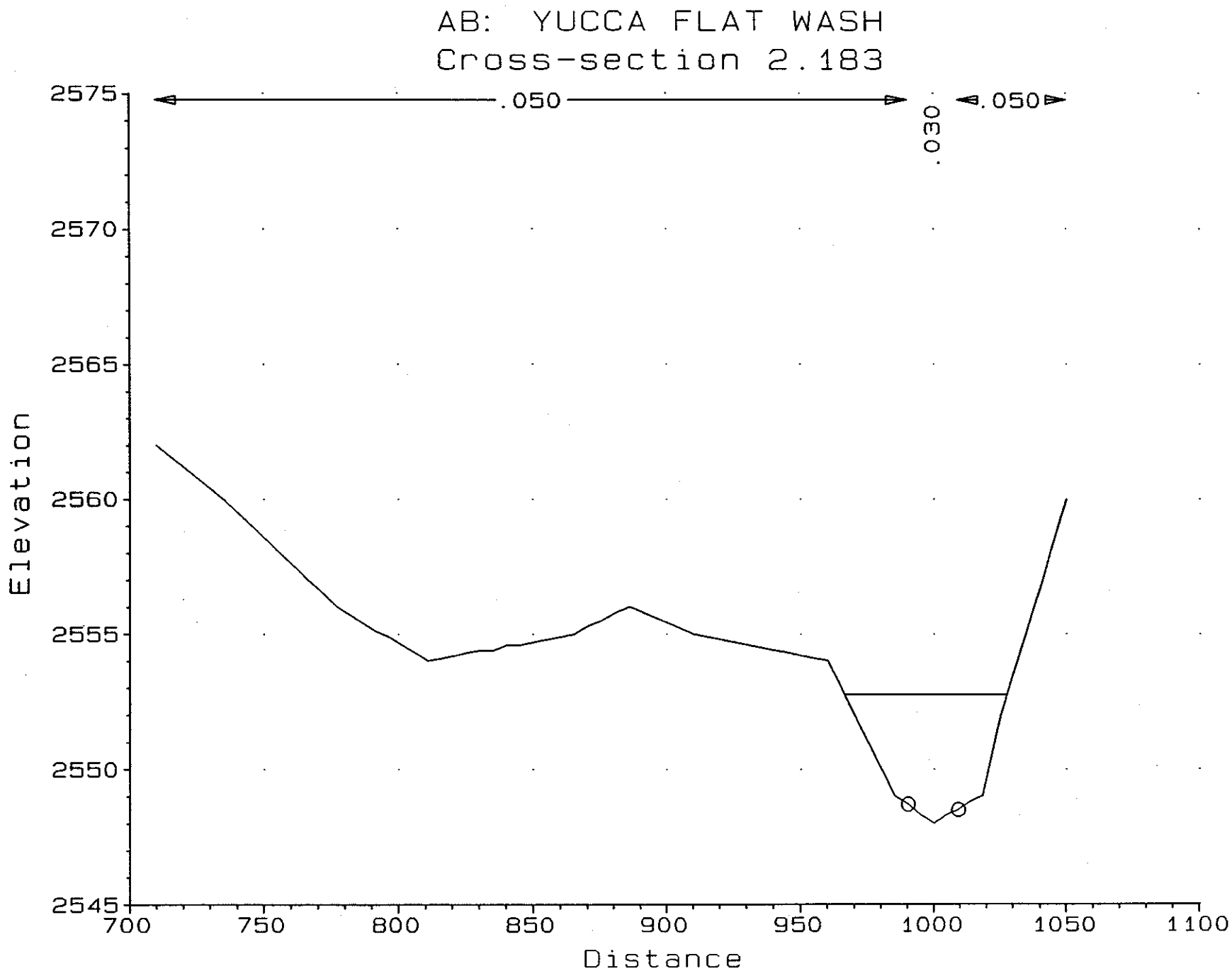
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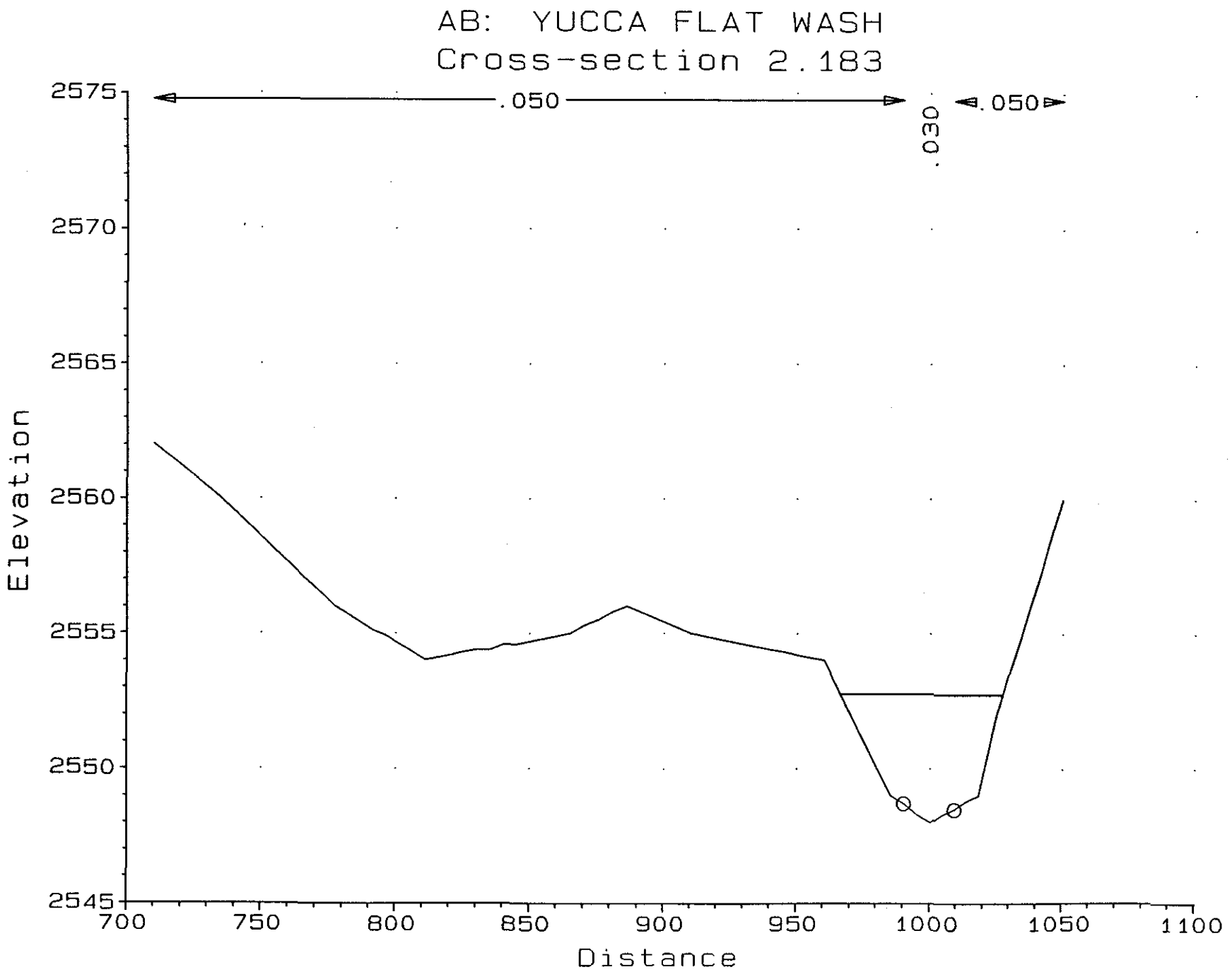
1050
1100
Distance


AB: YUCCA FLAT WASH
Cross-section 2.183
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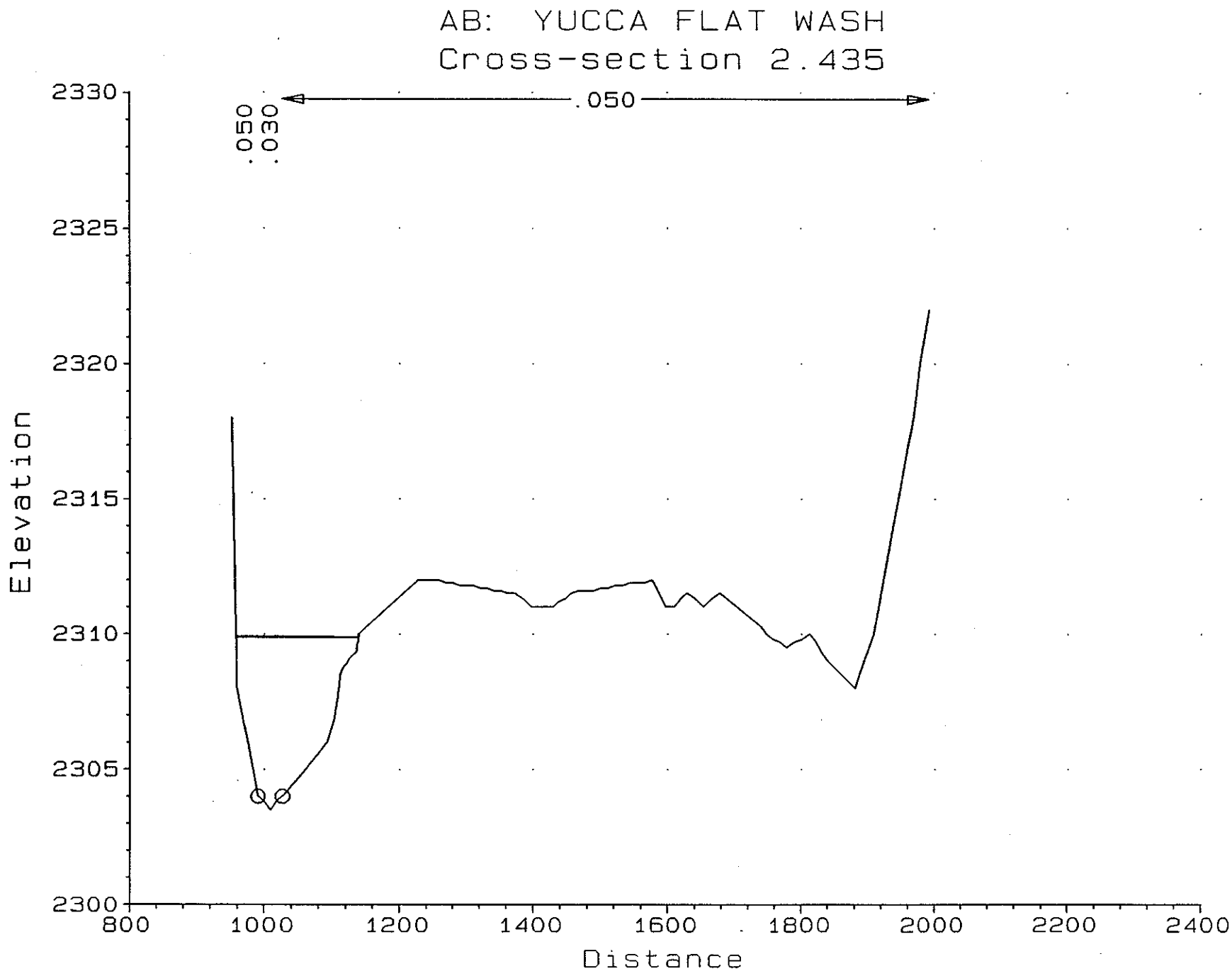
Distance


AB: YUCCA FLAT WASH
Cross-section 2.435
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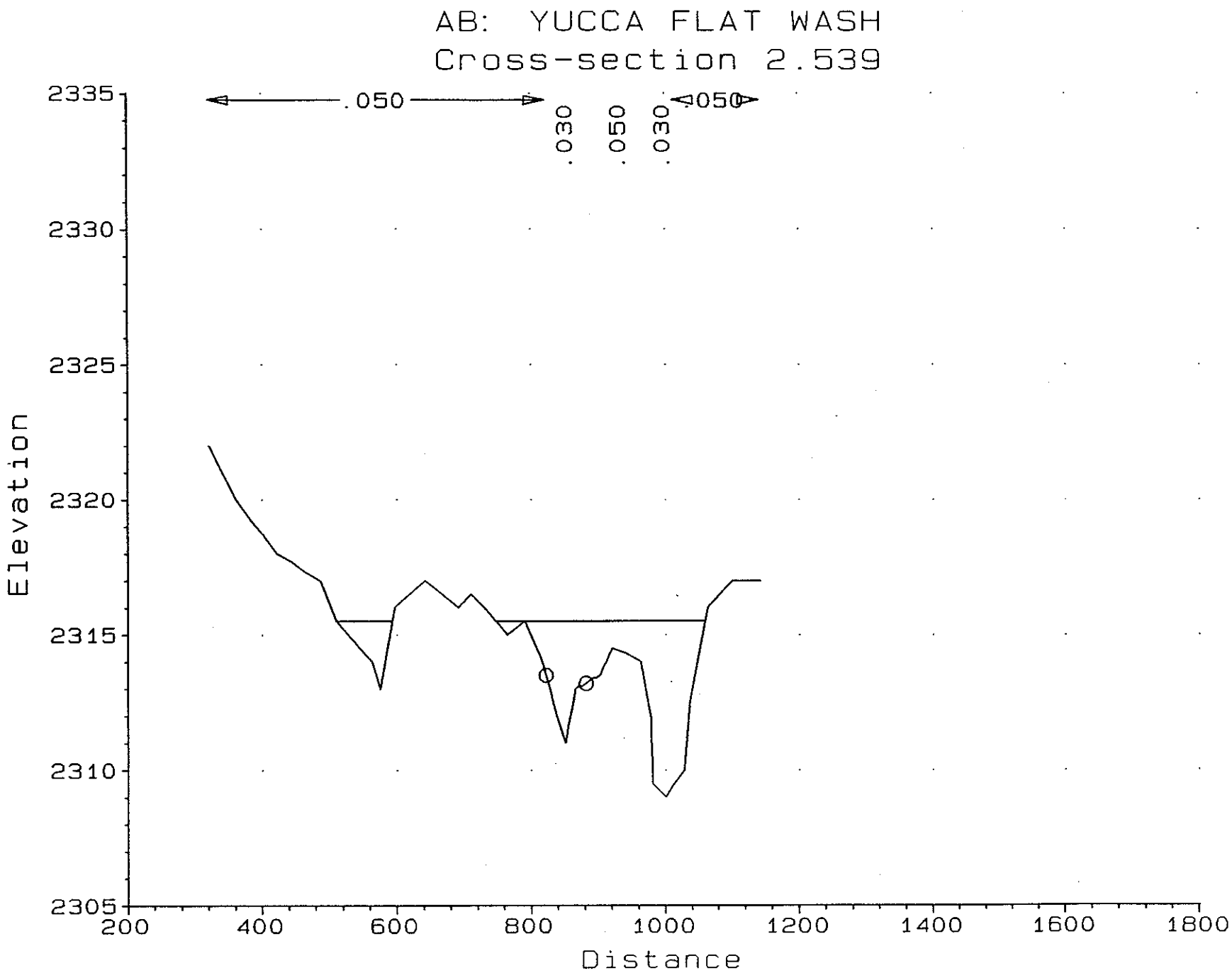
Distance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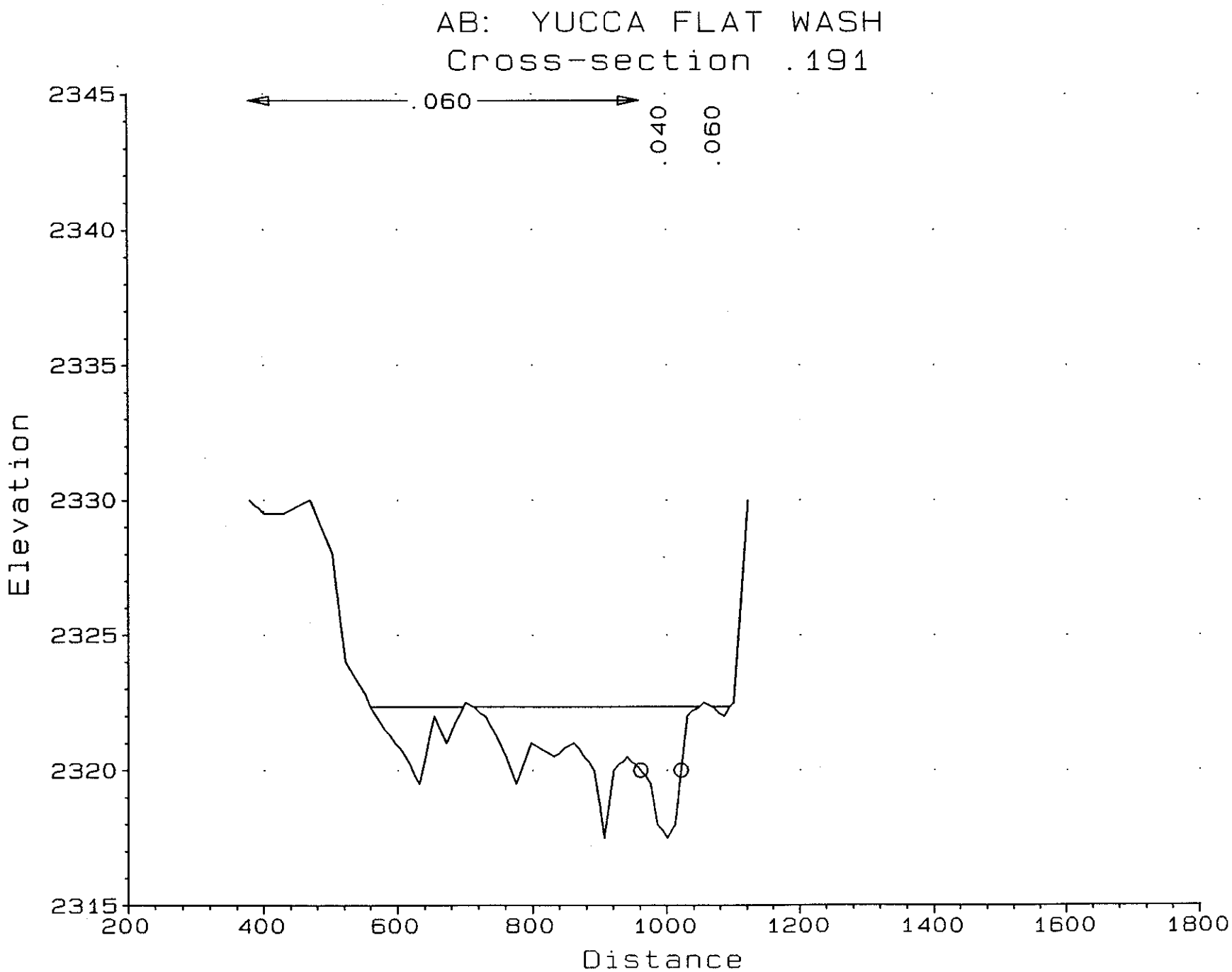
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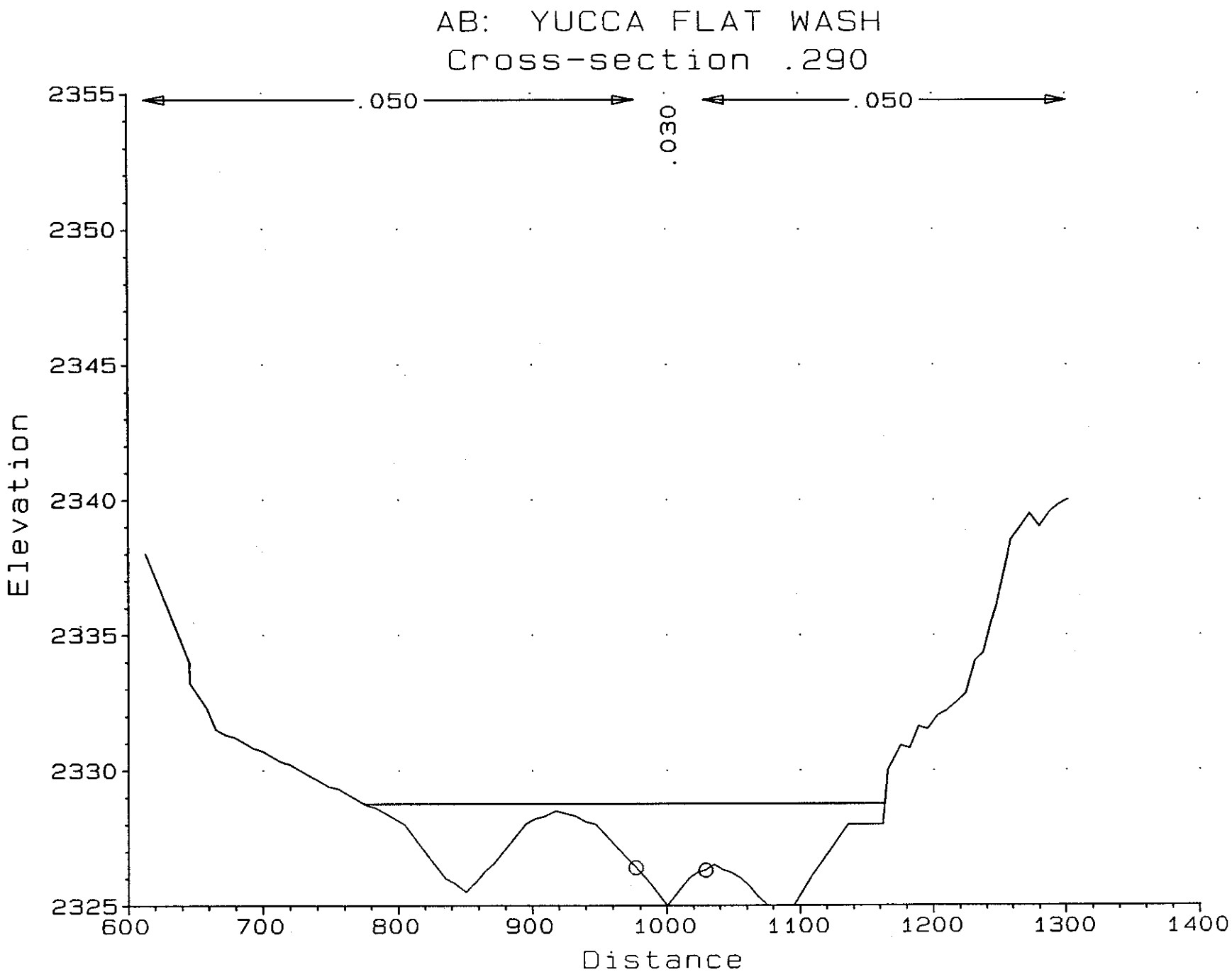
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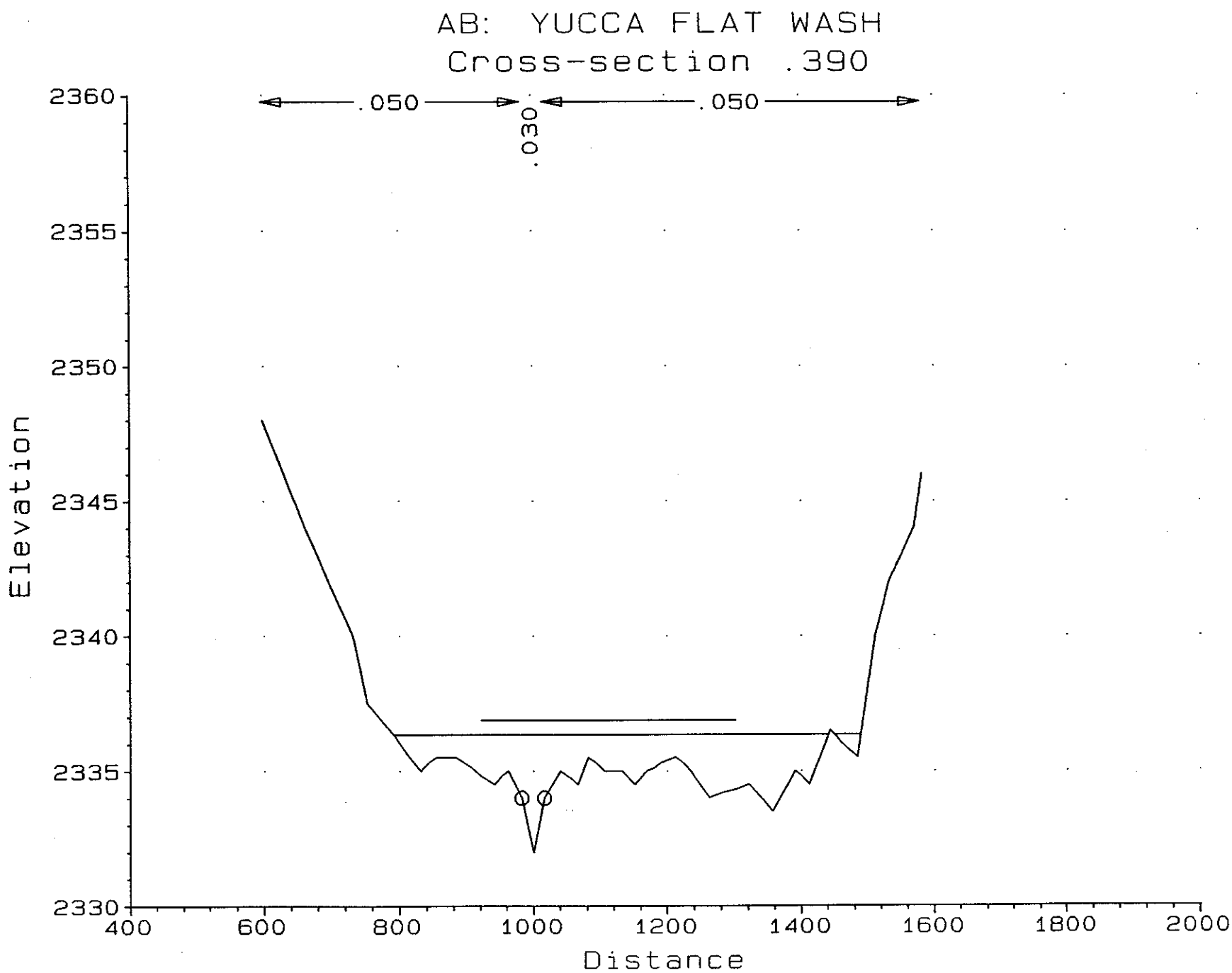
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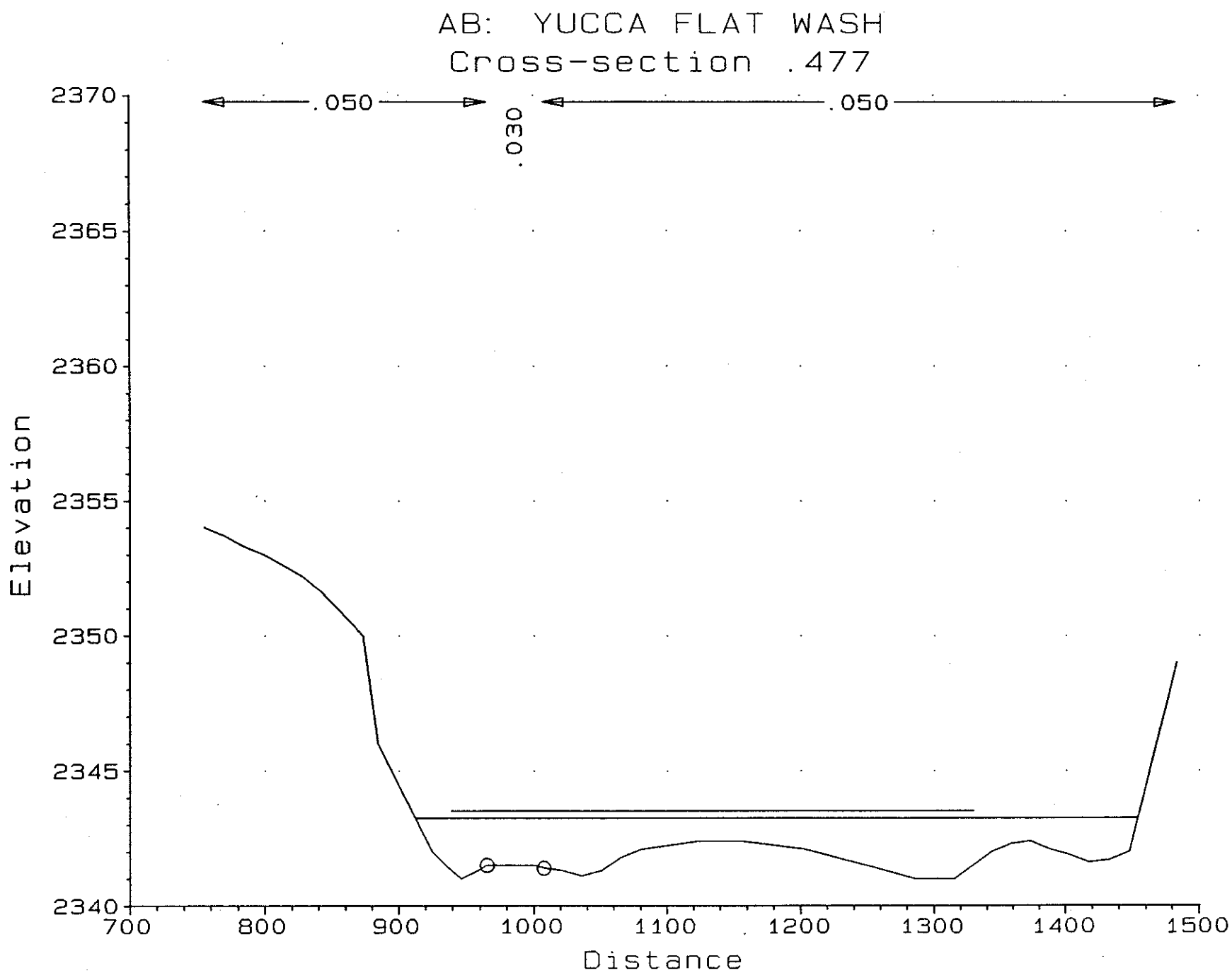
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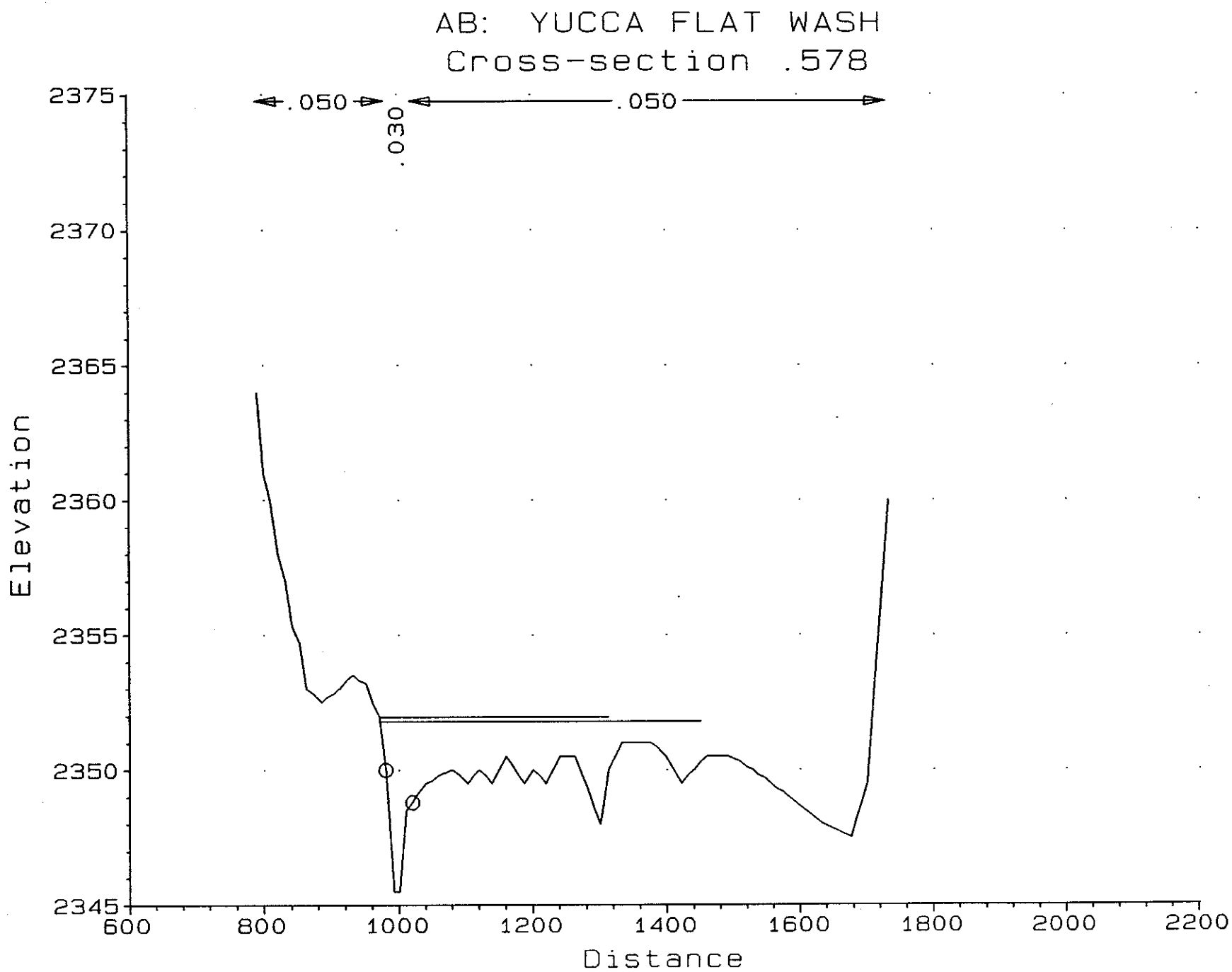
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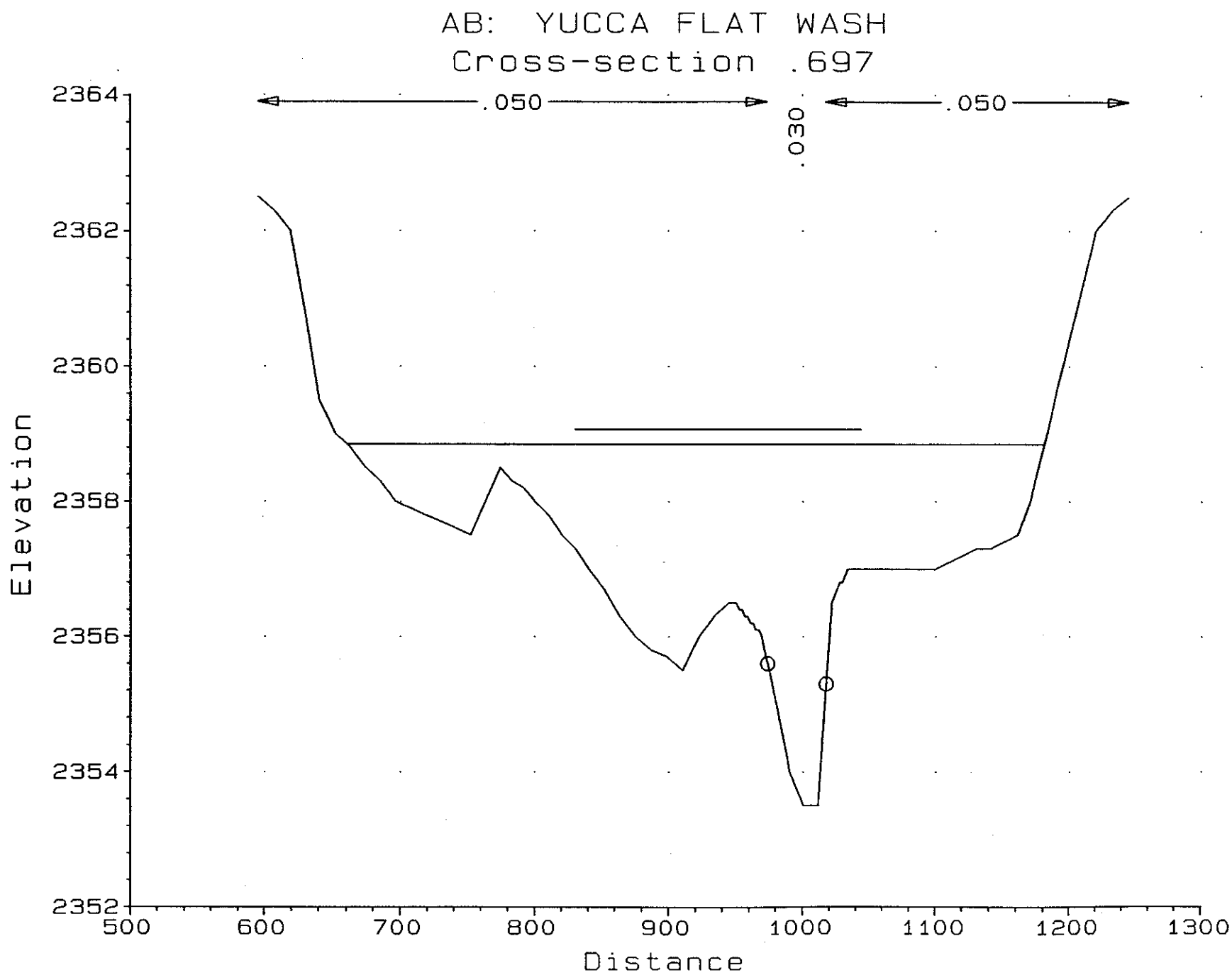
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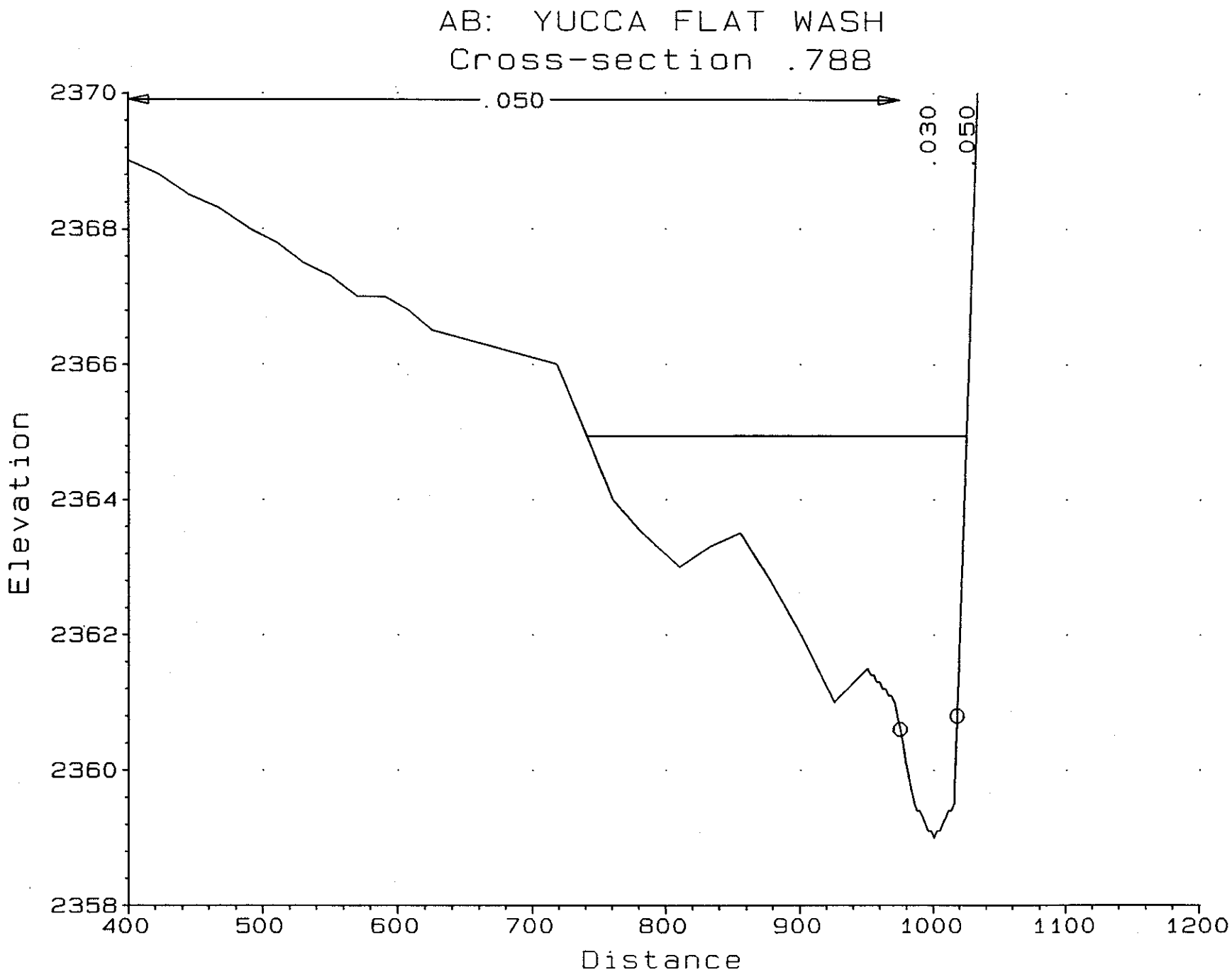
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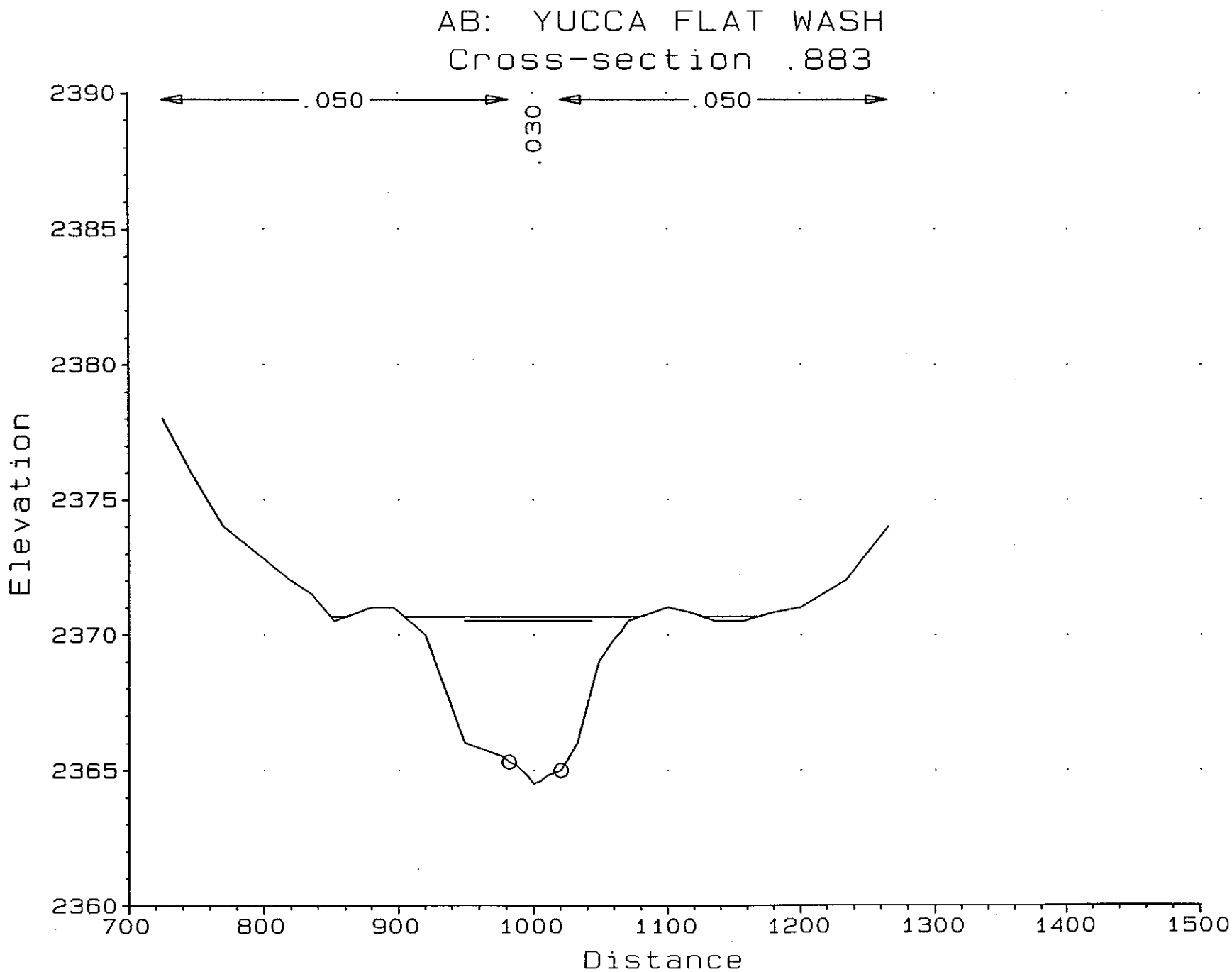
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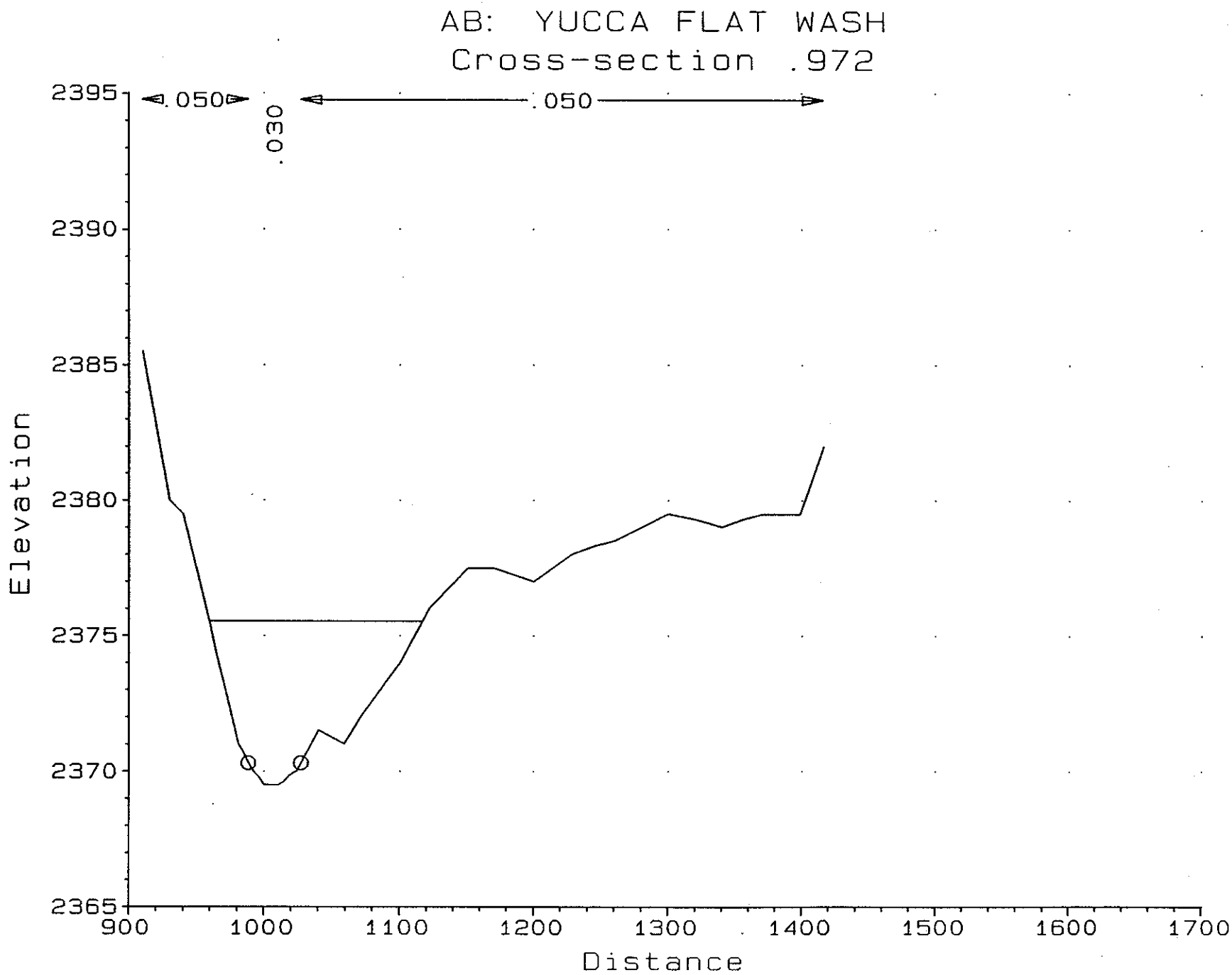
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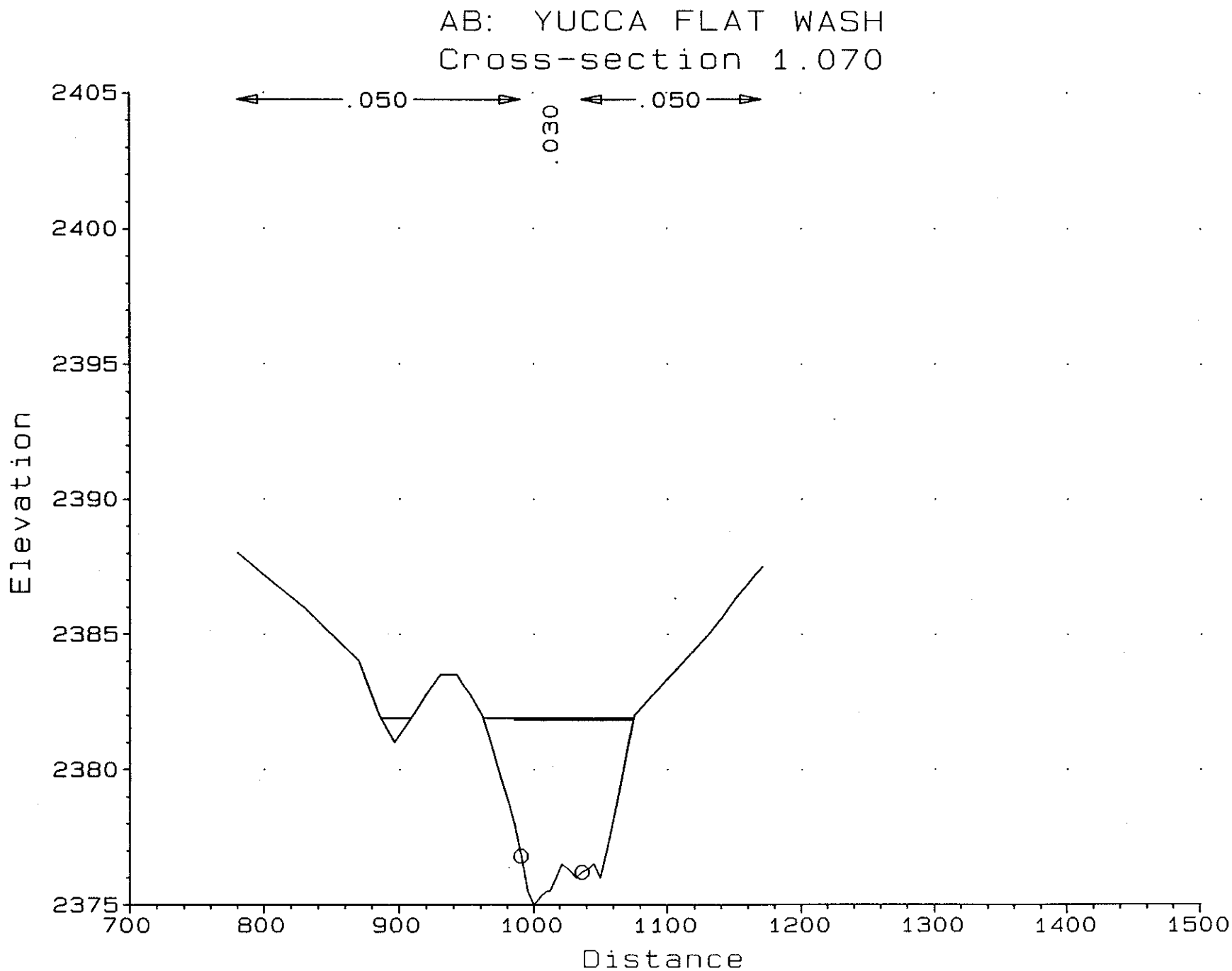
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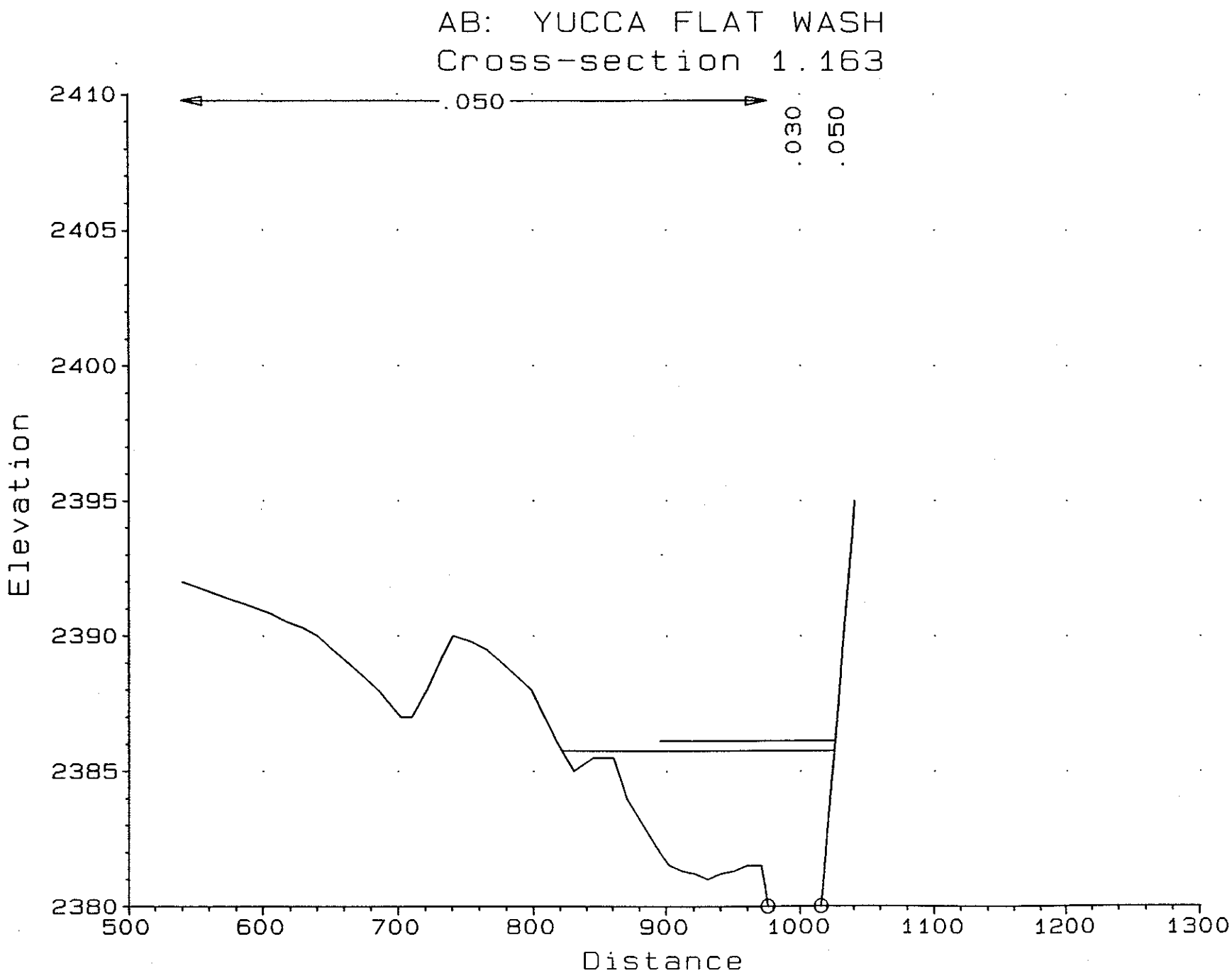
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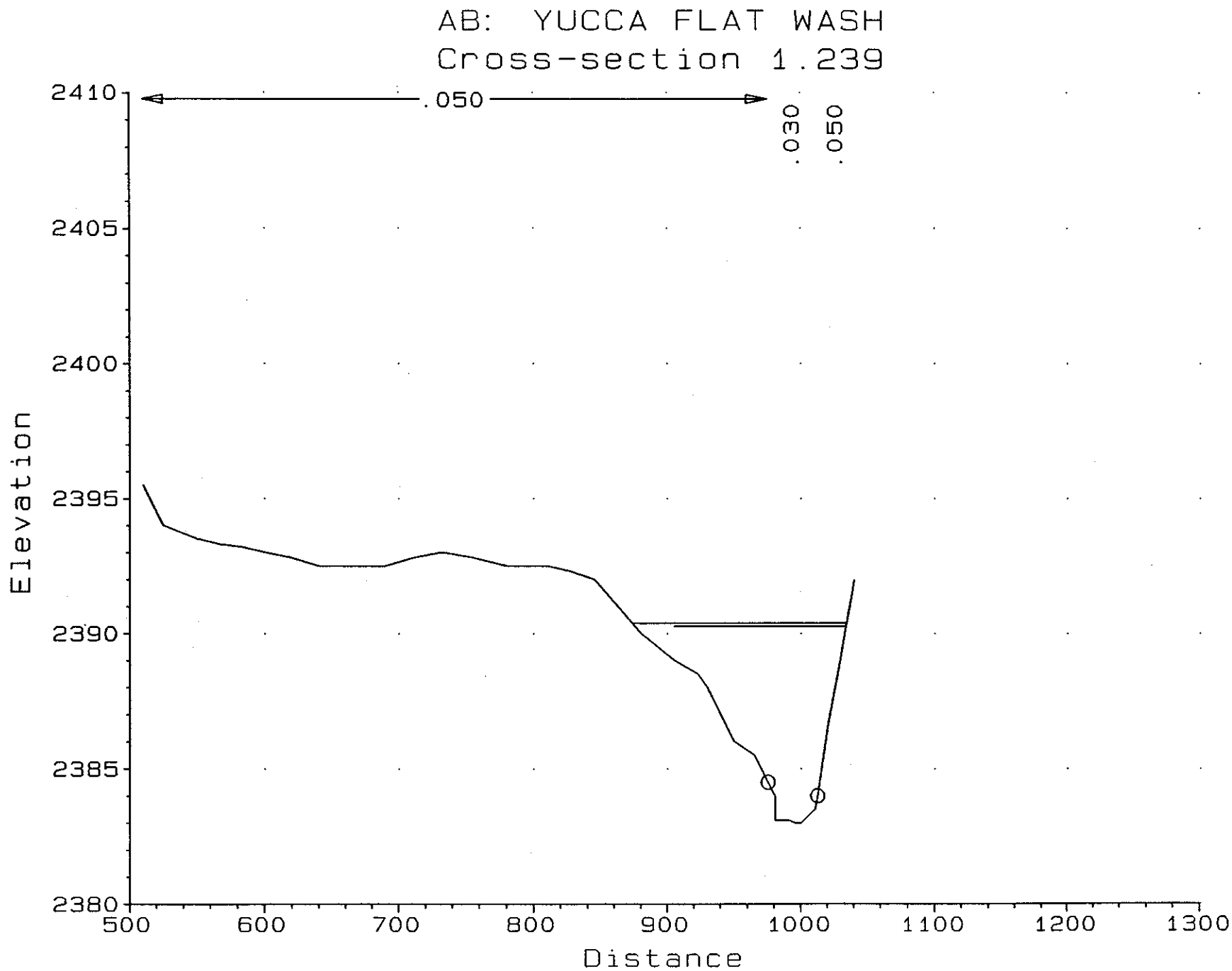
AB: YUCCA FLAT WASH
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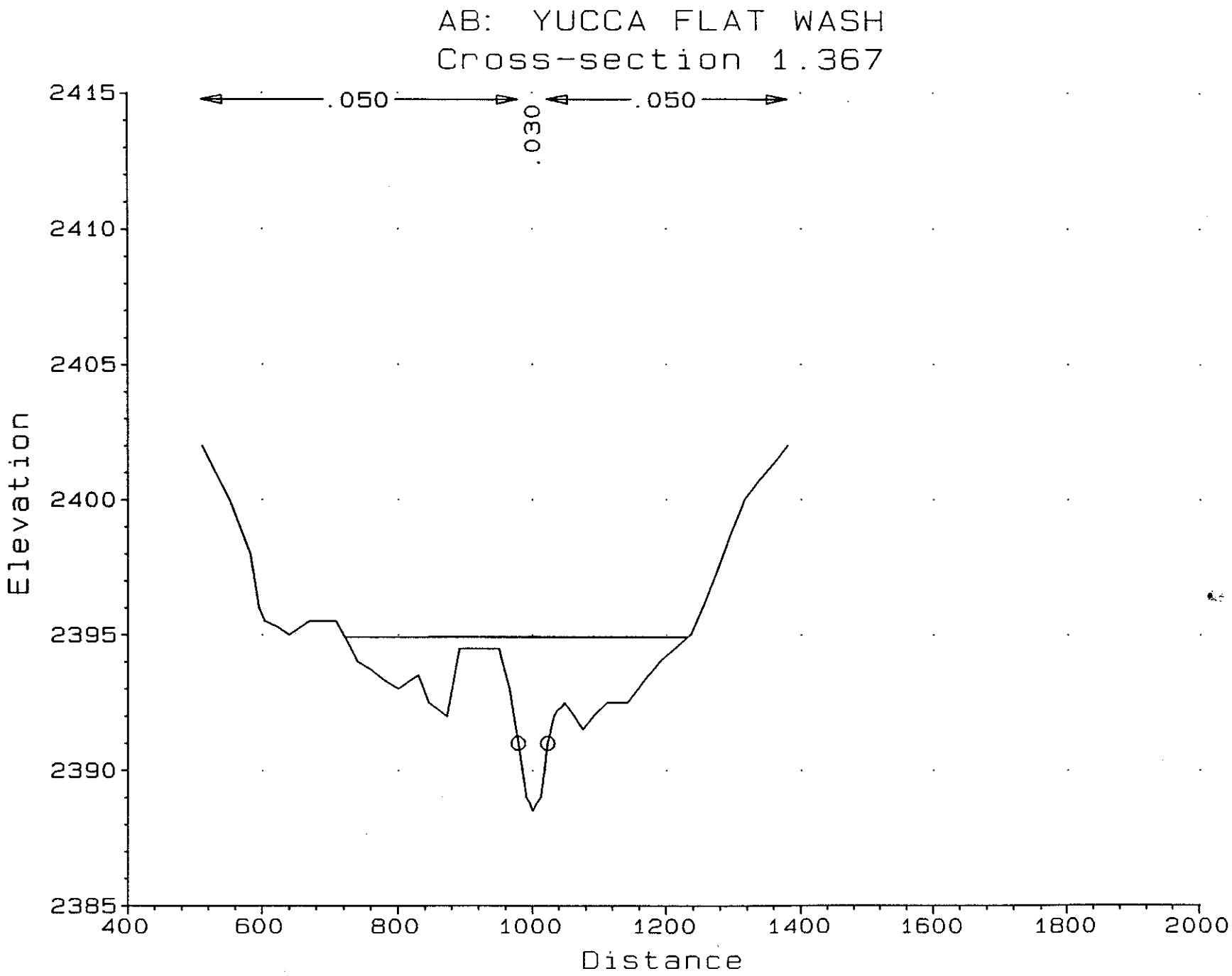
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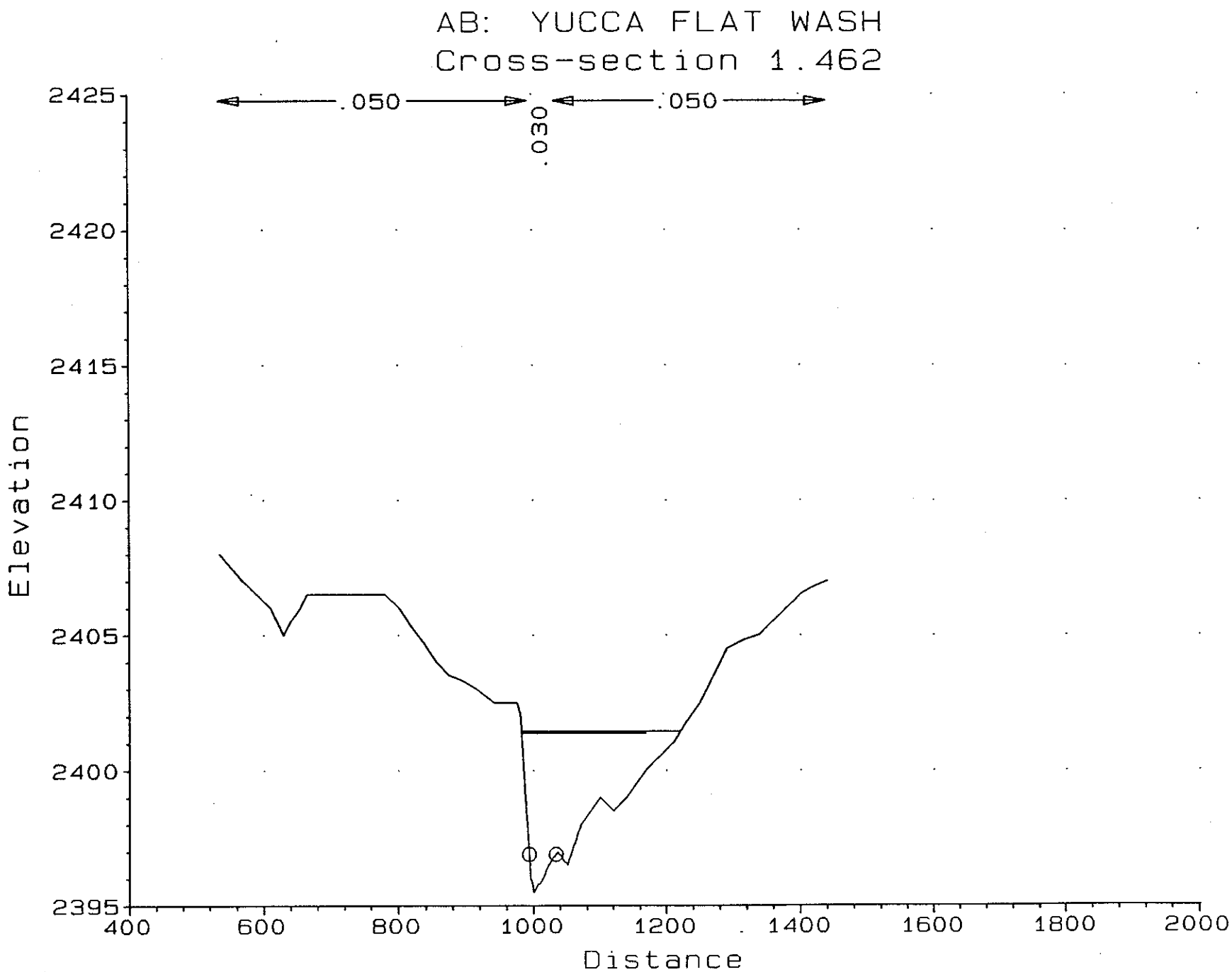
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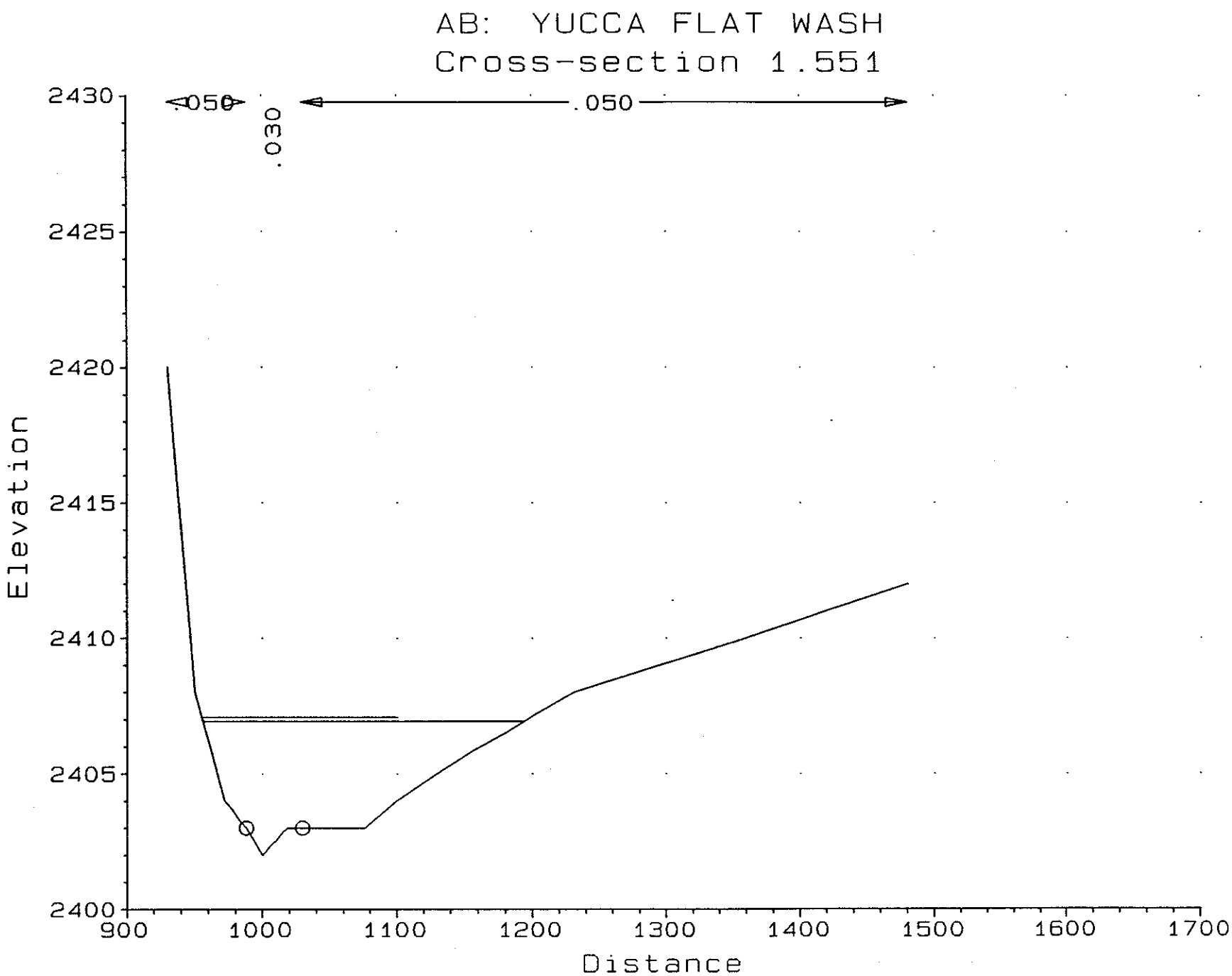
AB: YUCCA FLAT WASH
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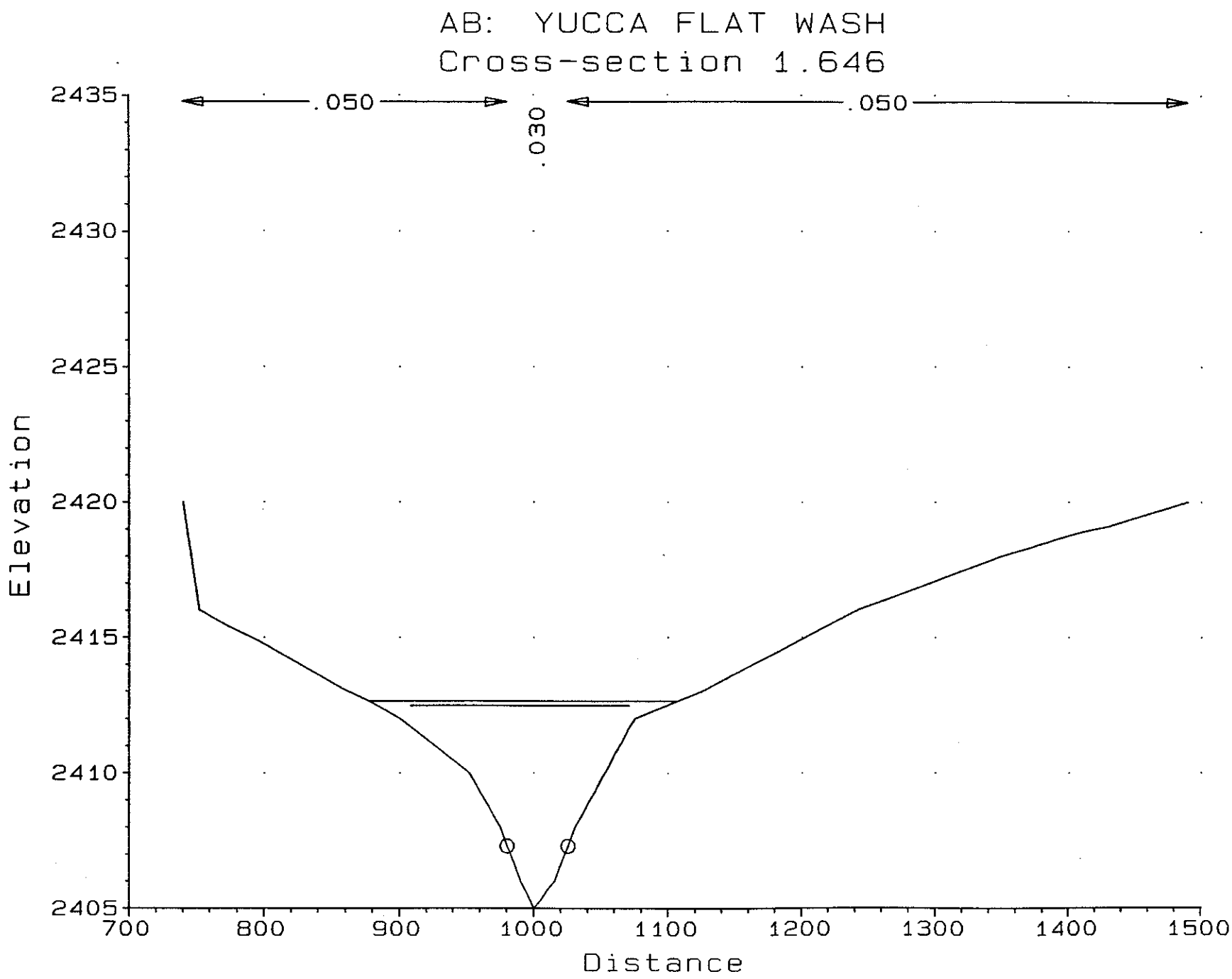
AB: YUCCA FLAT WASH
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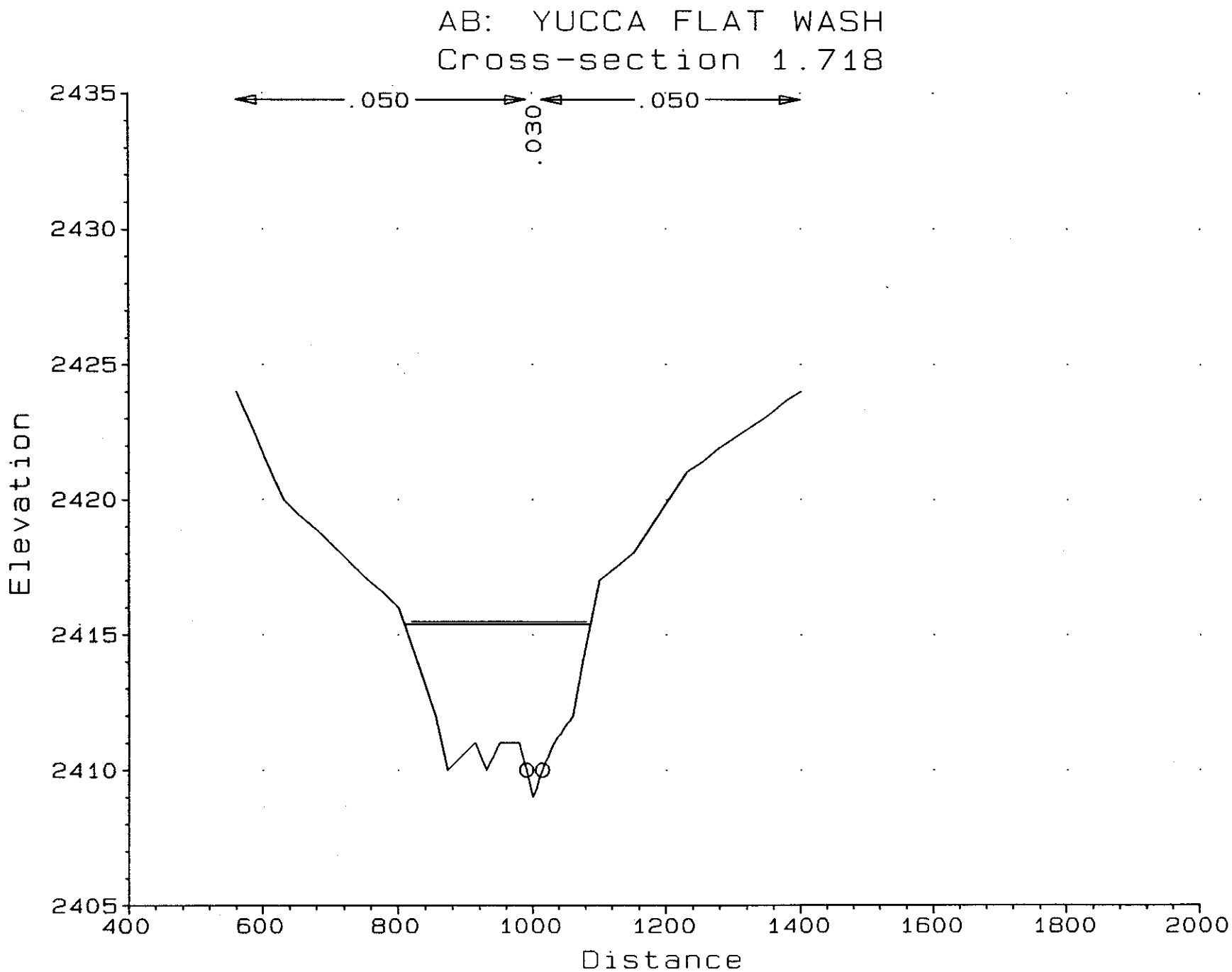
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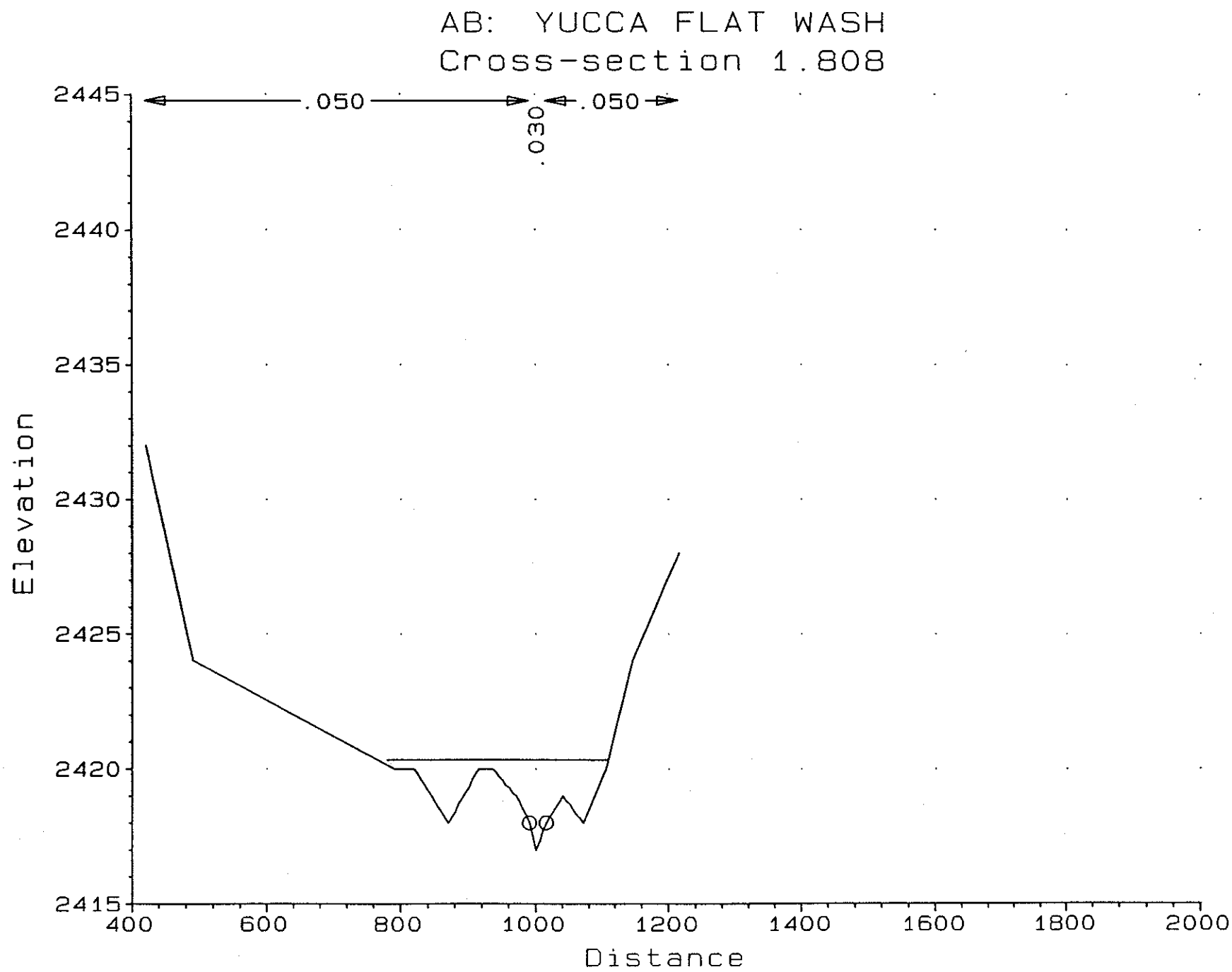
AB: YUCCA FLAT WASH
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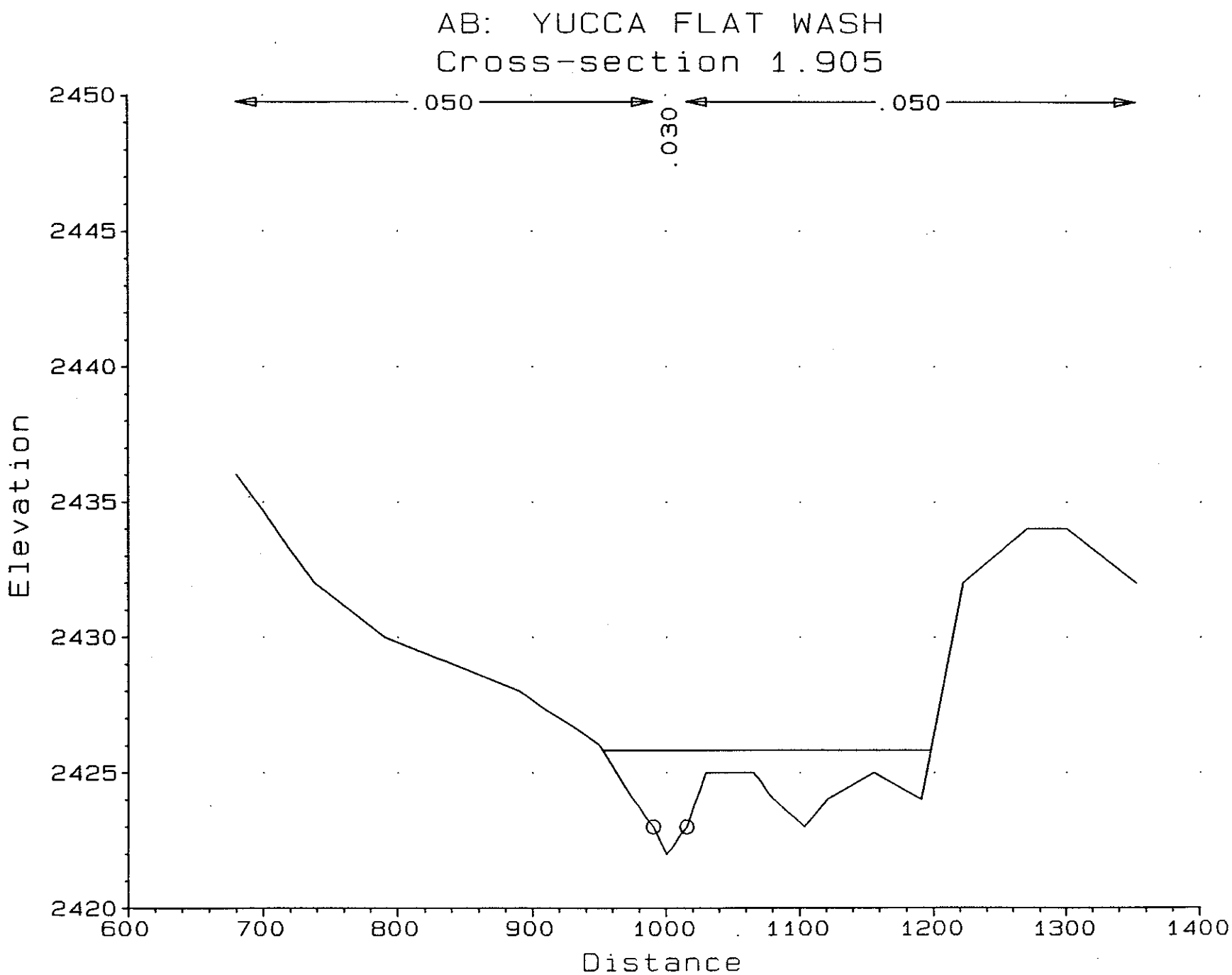
AB: YUCCA FLAT WASH
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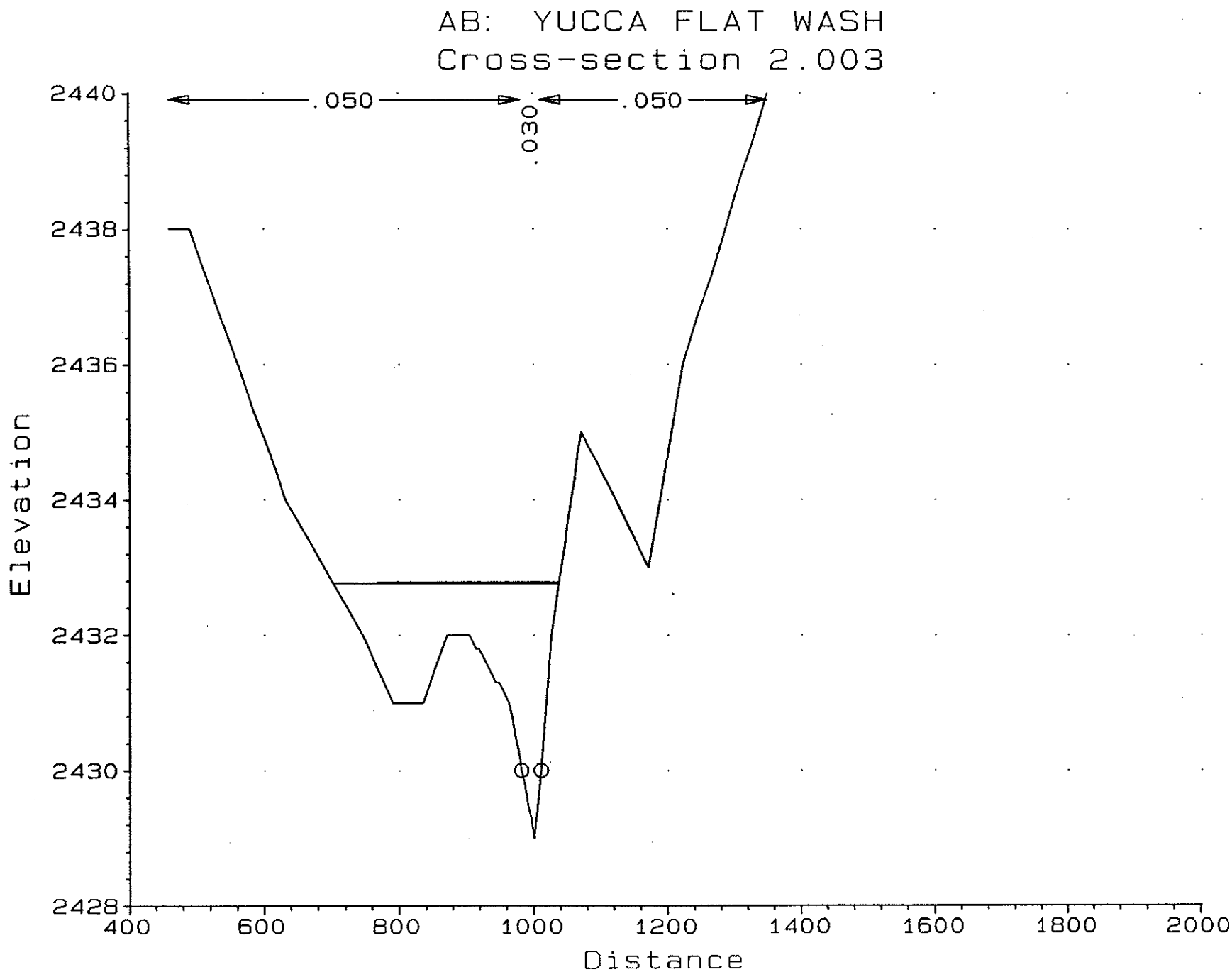
AB: YUCCA FLAT WASH
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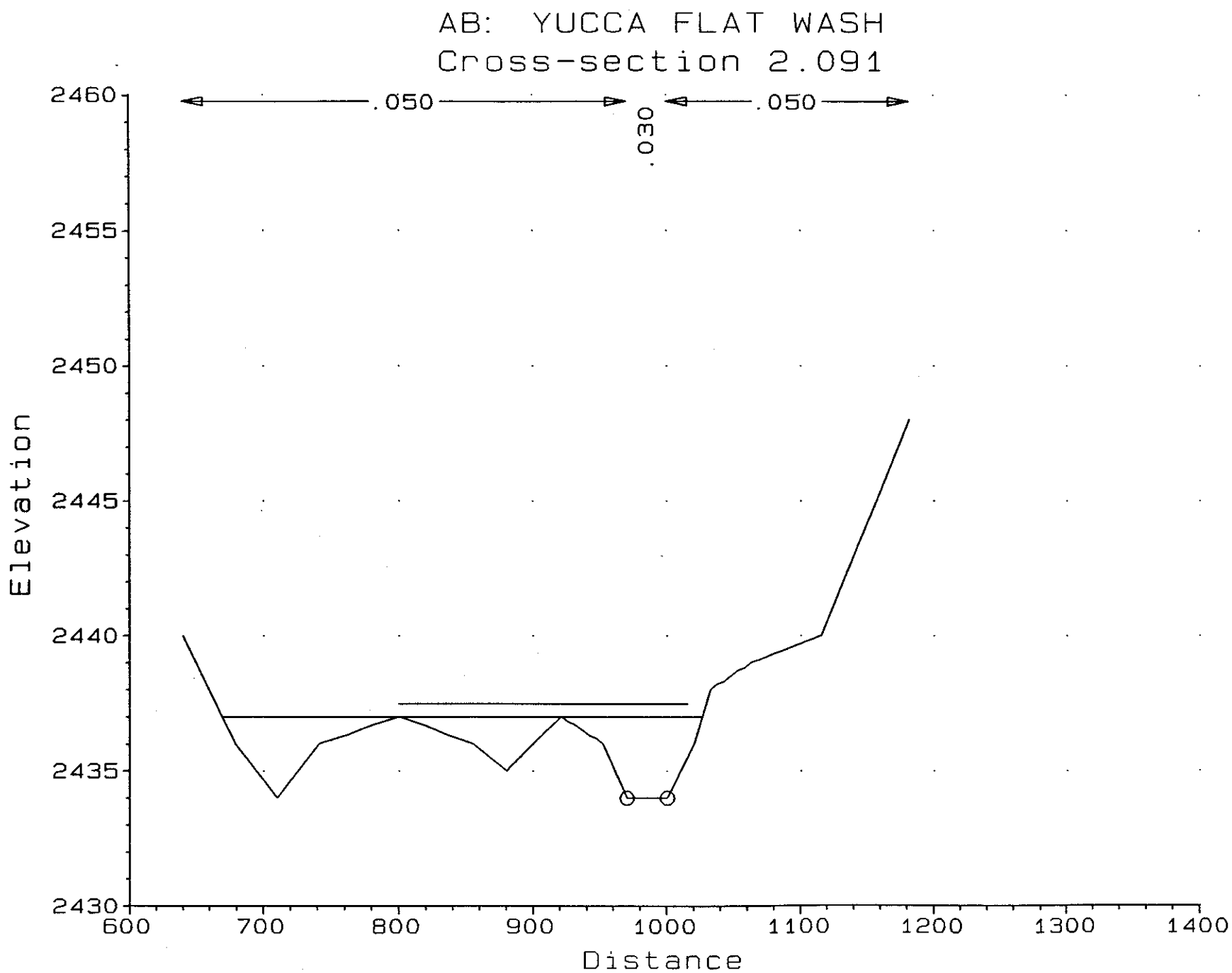
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Cross-section 2.091
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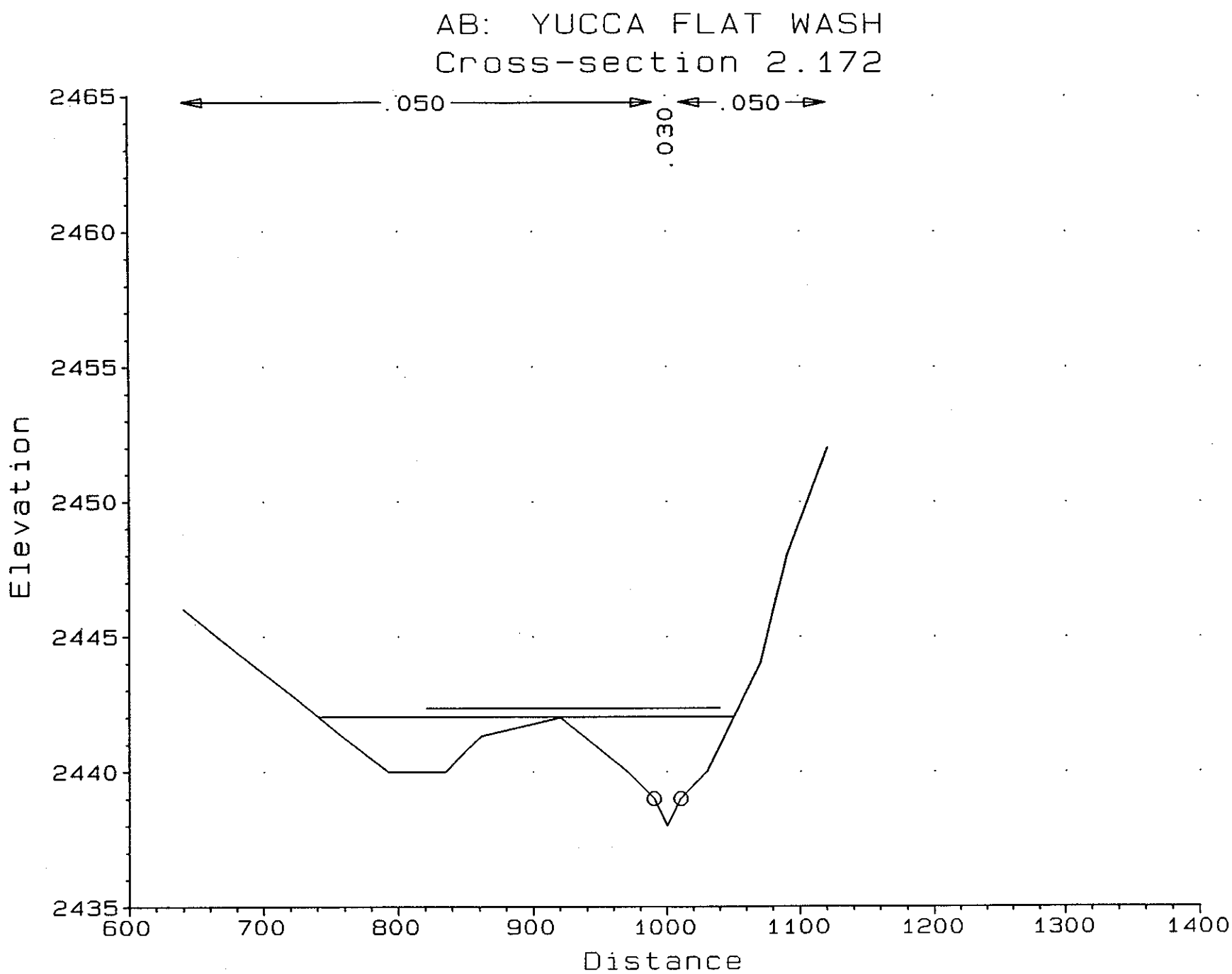
AB: YUCCA FLAT WASH
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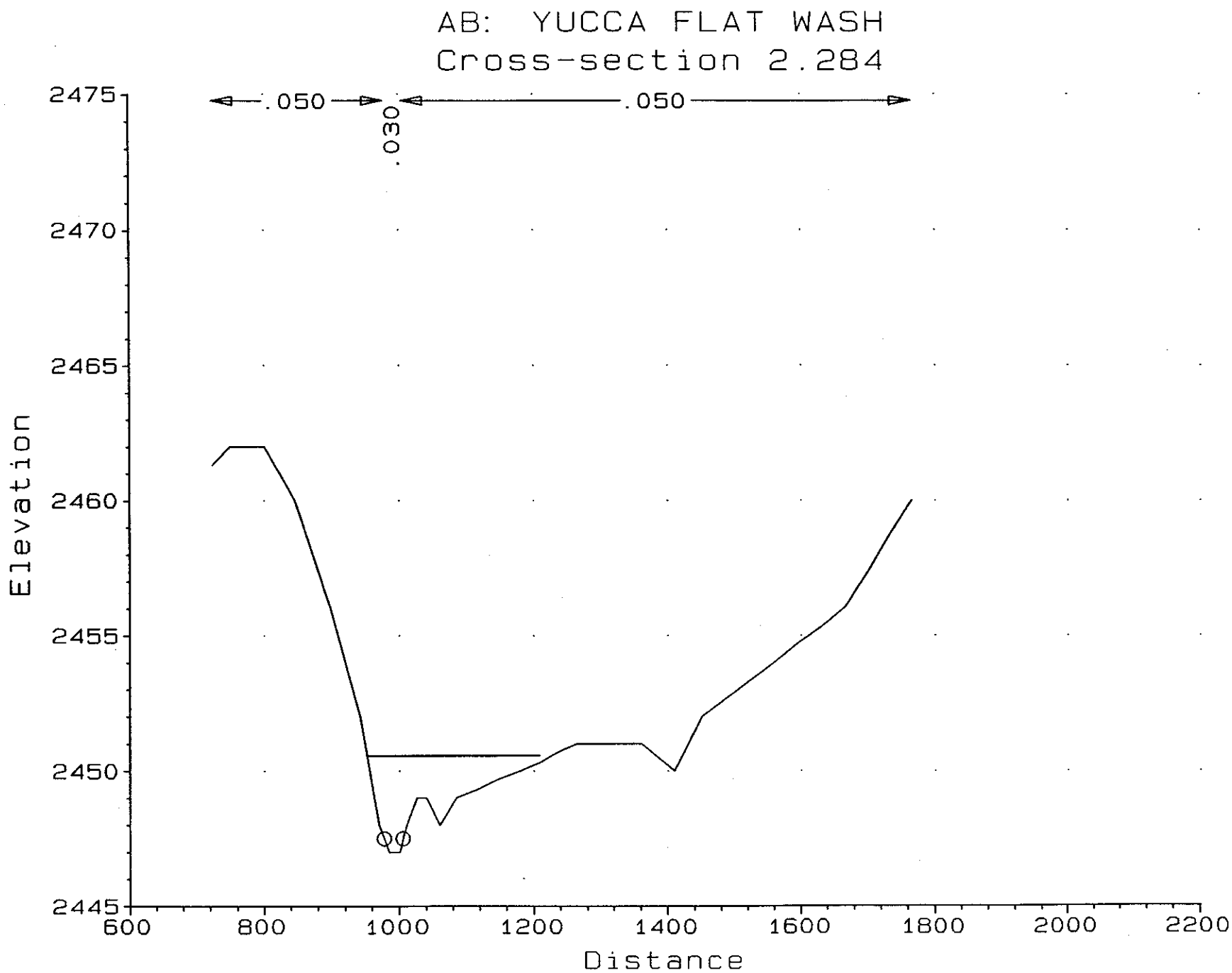
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Cross-section 2.284
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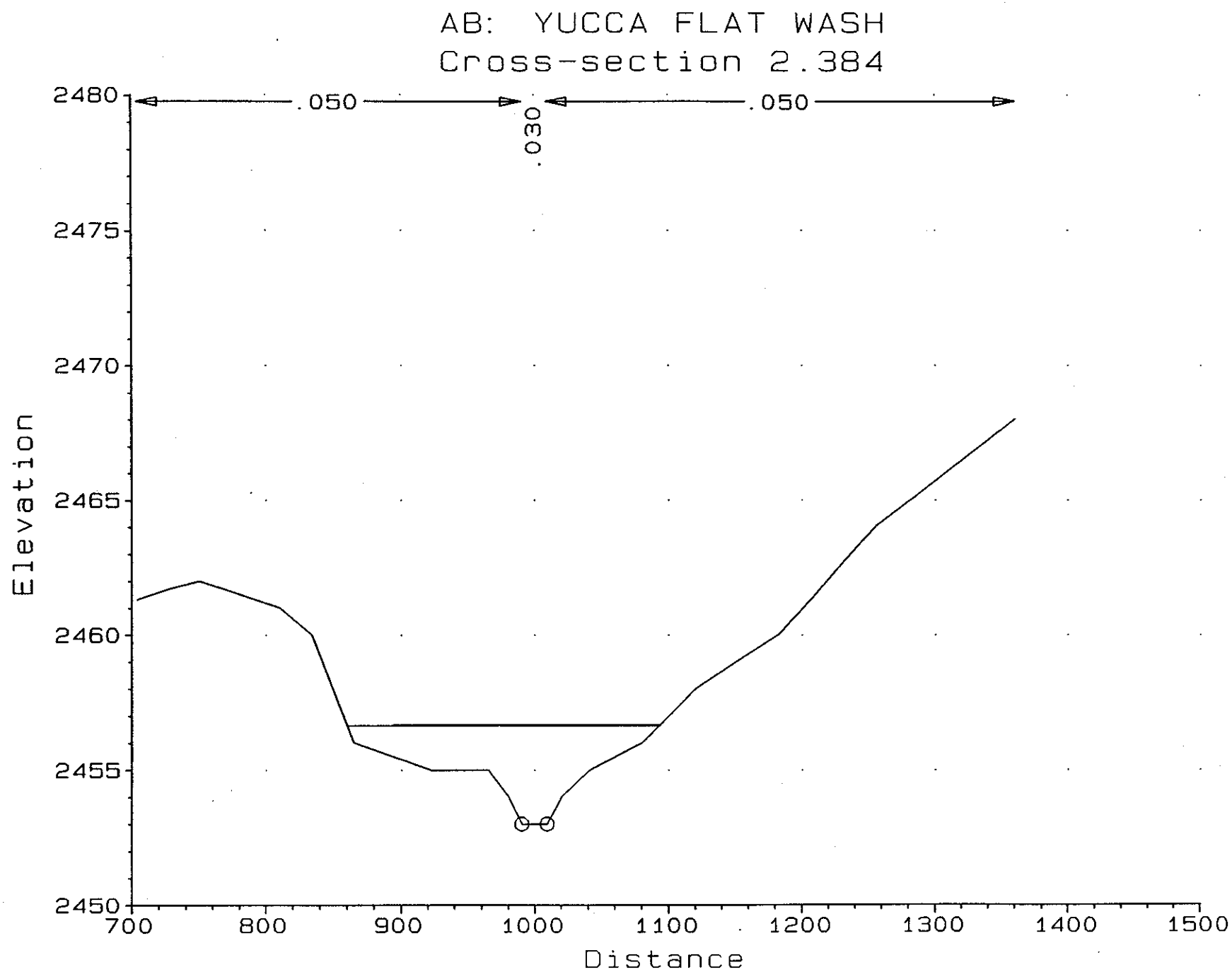
AB: YUCCA FLAT WASH
Cross-section 2.384
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.050
2480
2475
2470
2465
2460
2455
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Elevation
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800
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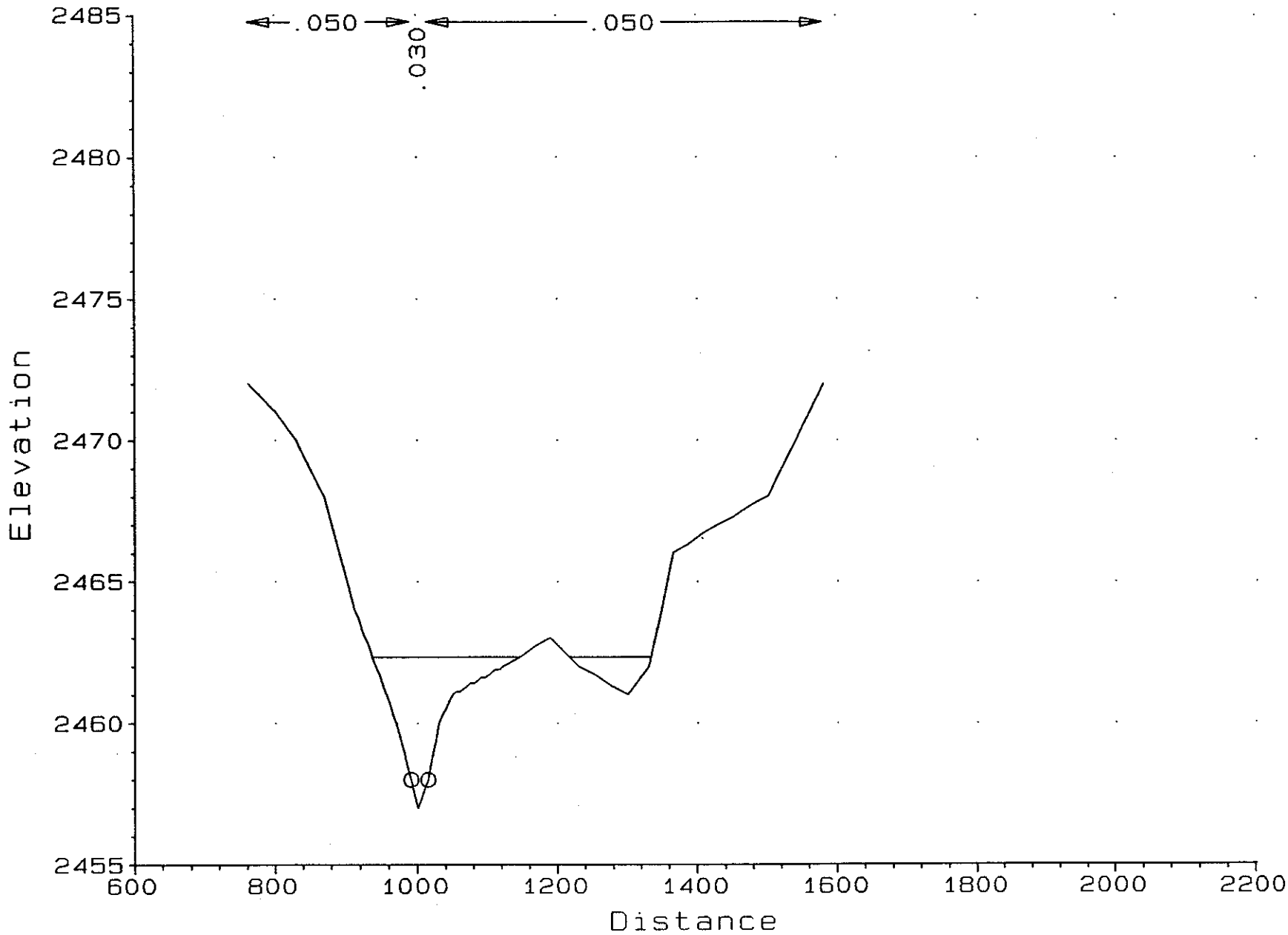
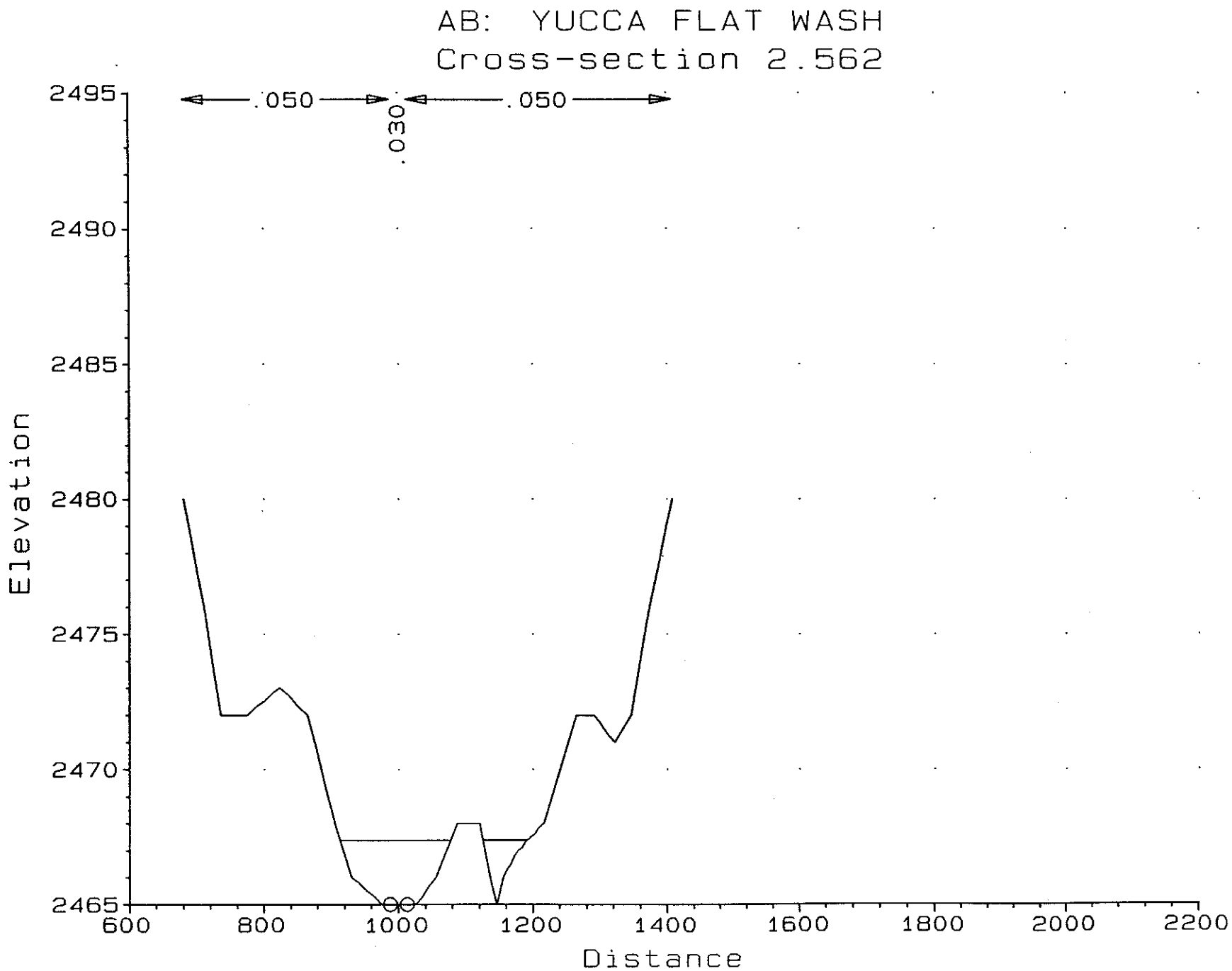
1100
1200
1300
1400
1500
Distance

AB: YUCCA FLAT WASH
Cross-section 2.477

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Cross-section 2.562
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.030
.050
2495
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Elevation
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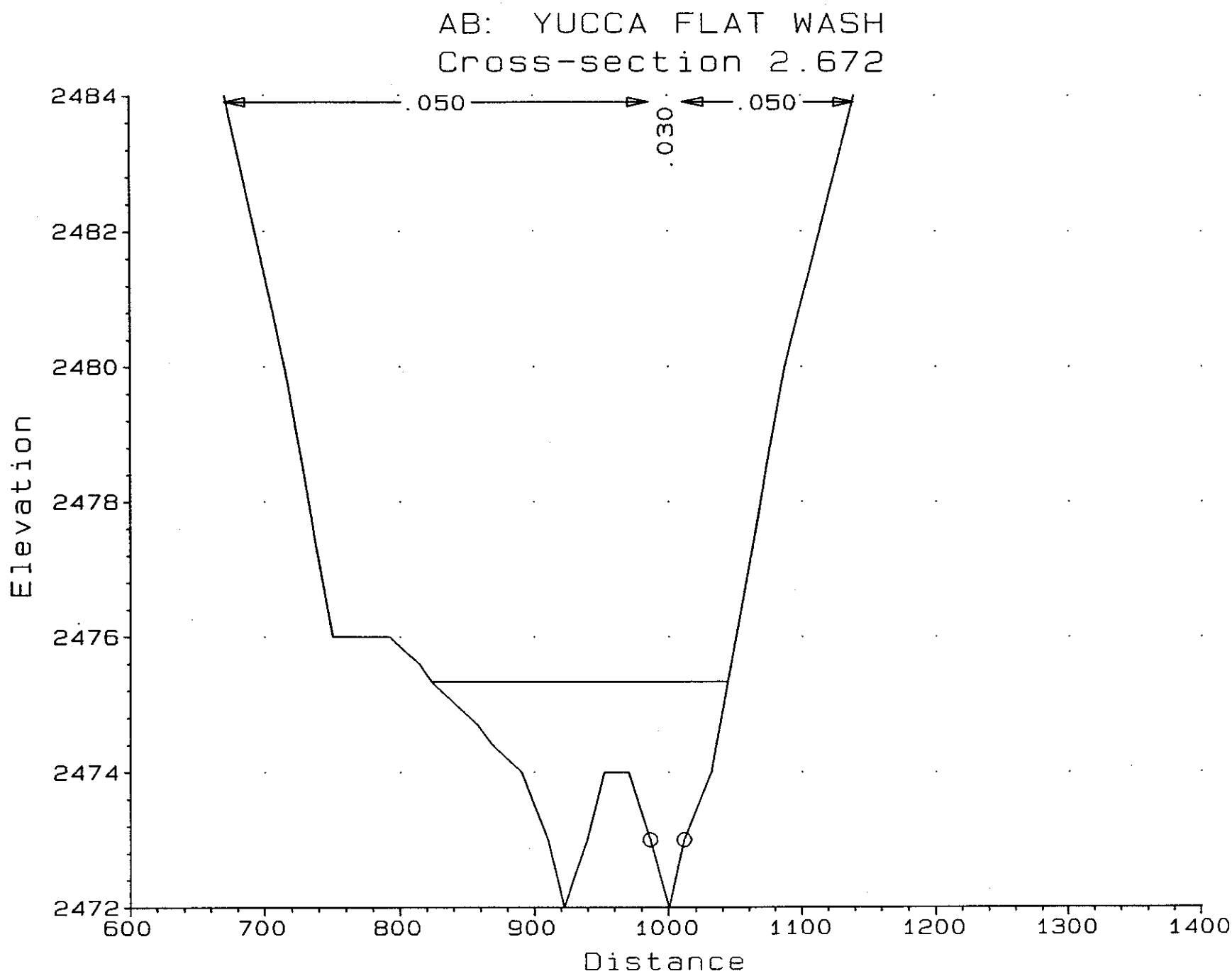
1200
1400
1600
1800
2000
2200
Distance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Cross-section 2.672
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.030
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2484
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Elevation
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900
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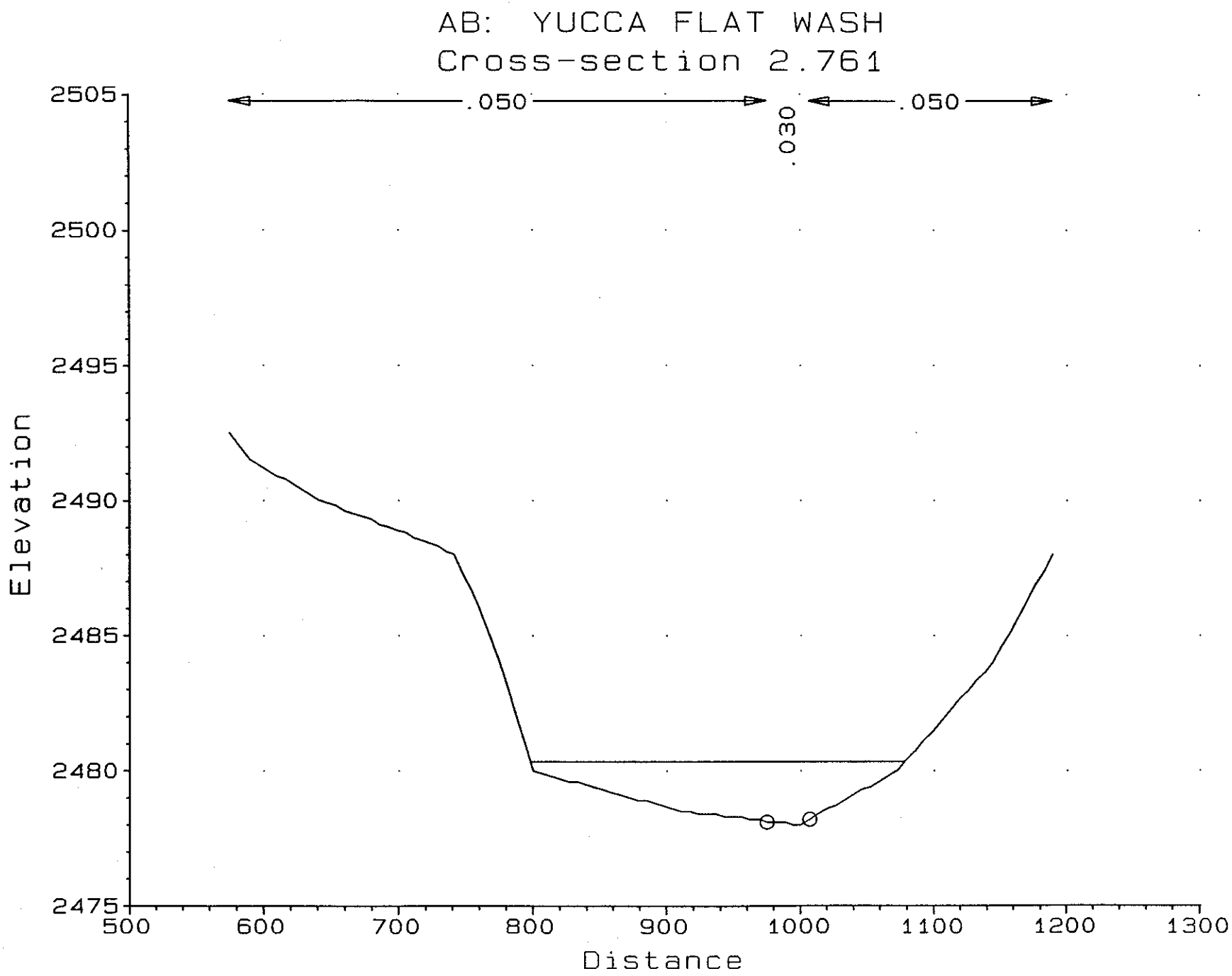
1300
1400
Distance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Cross-section 2.761
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.030
.050
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Elevation
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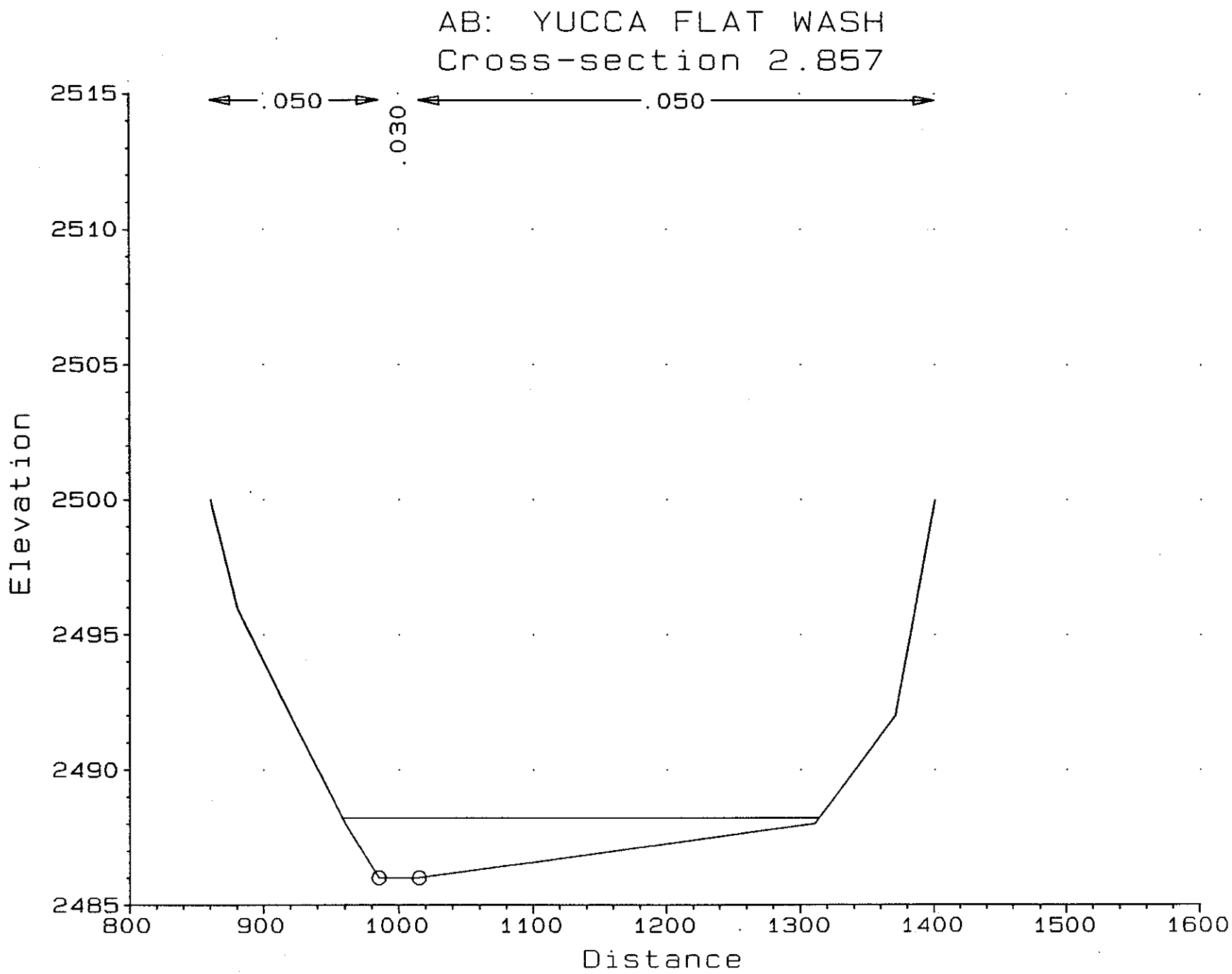
Distance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Cross-section 2.857
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.030
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2515
2510
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2490
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Elevation
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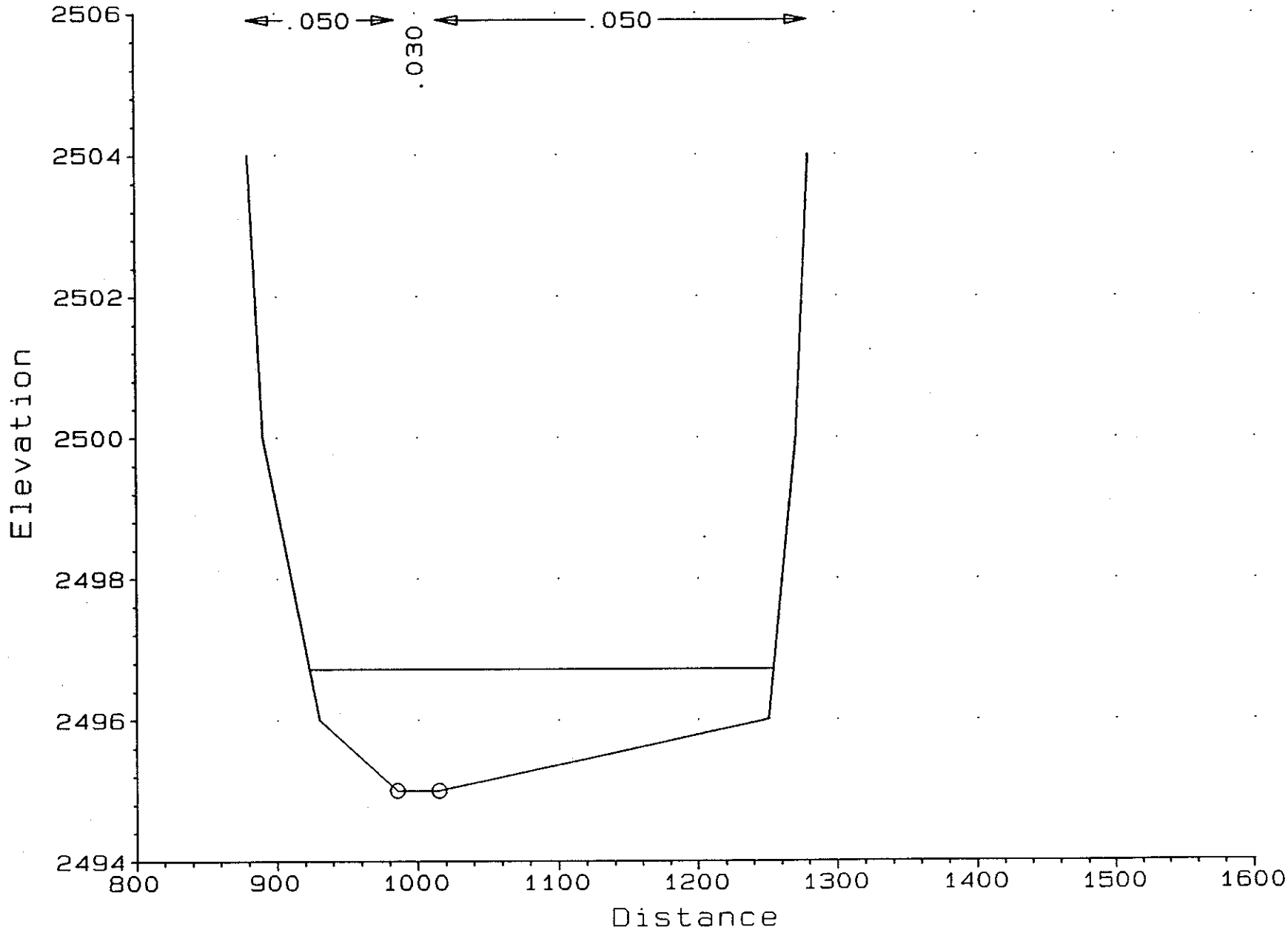
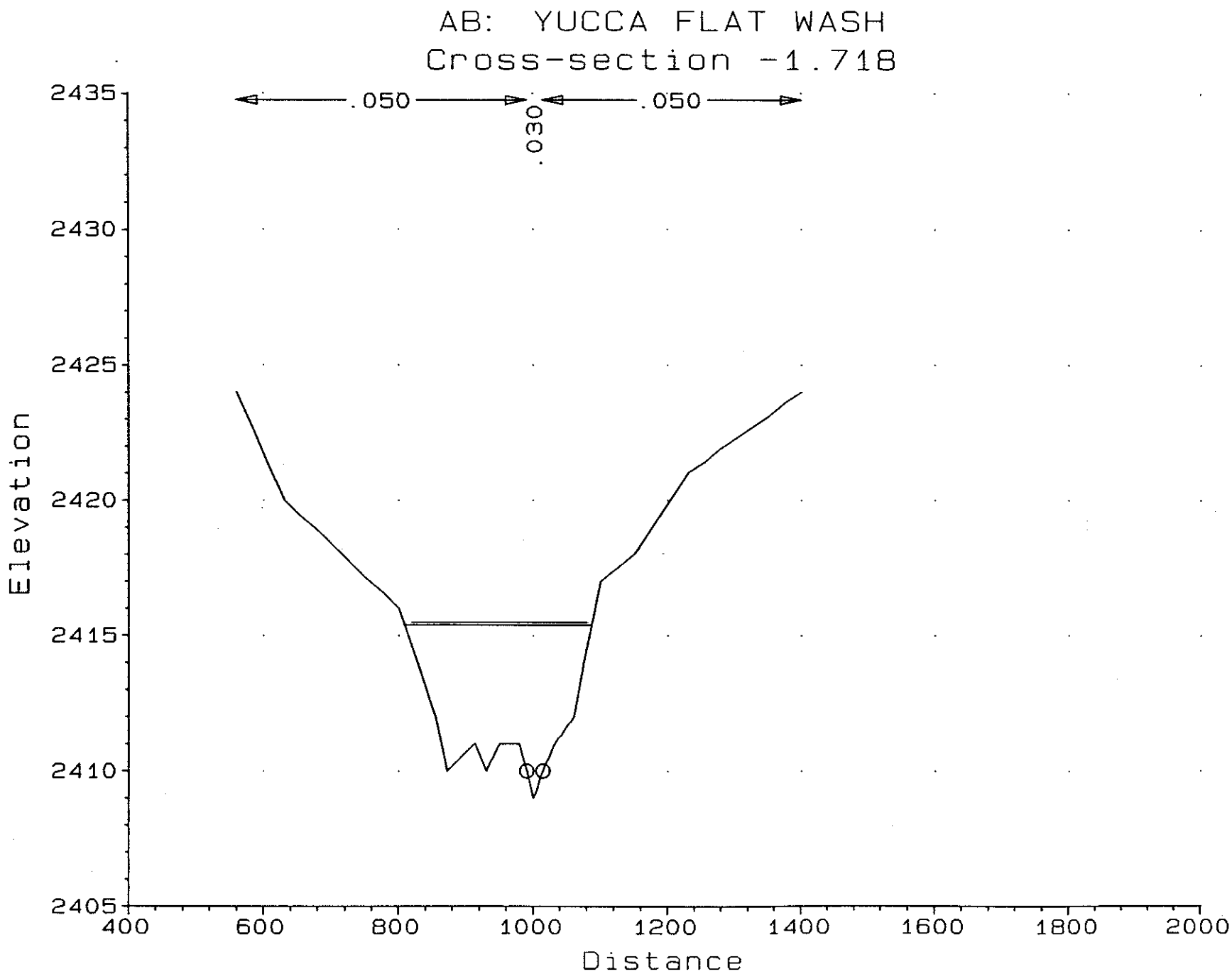
1100
1200
1300
1400
1500
1600
Distance

AB: YUCCA FLAT WASH
Cross-section 2.965

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Cross-section -1.718
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.030
.050
2435
2430
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2420
2415
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Elevation
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800
1000
1200
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1600
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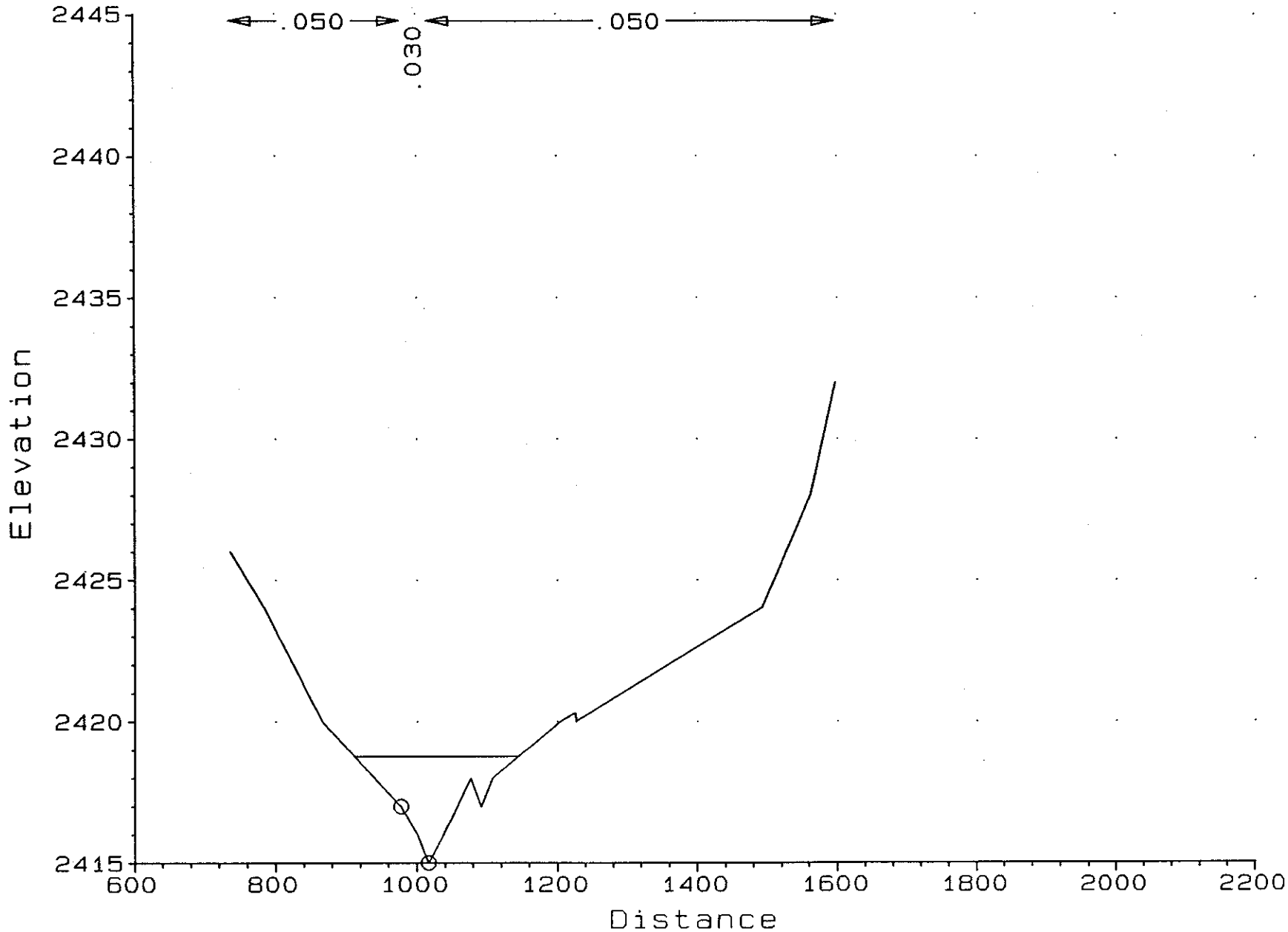
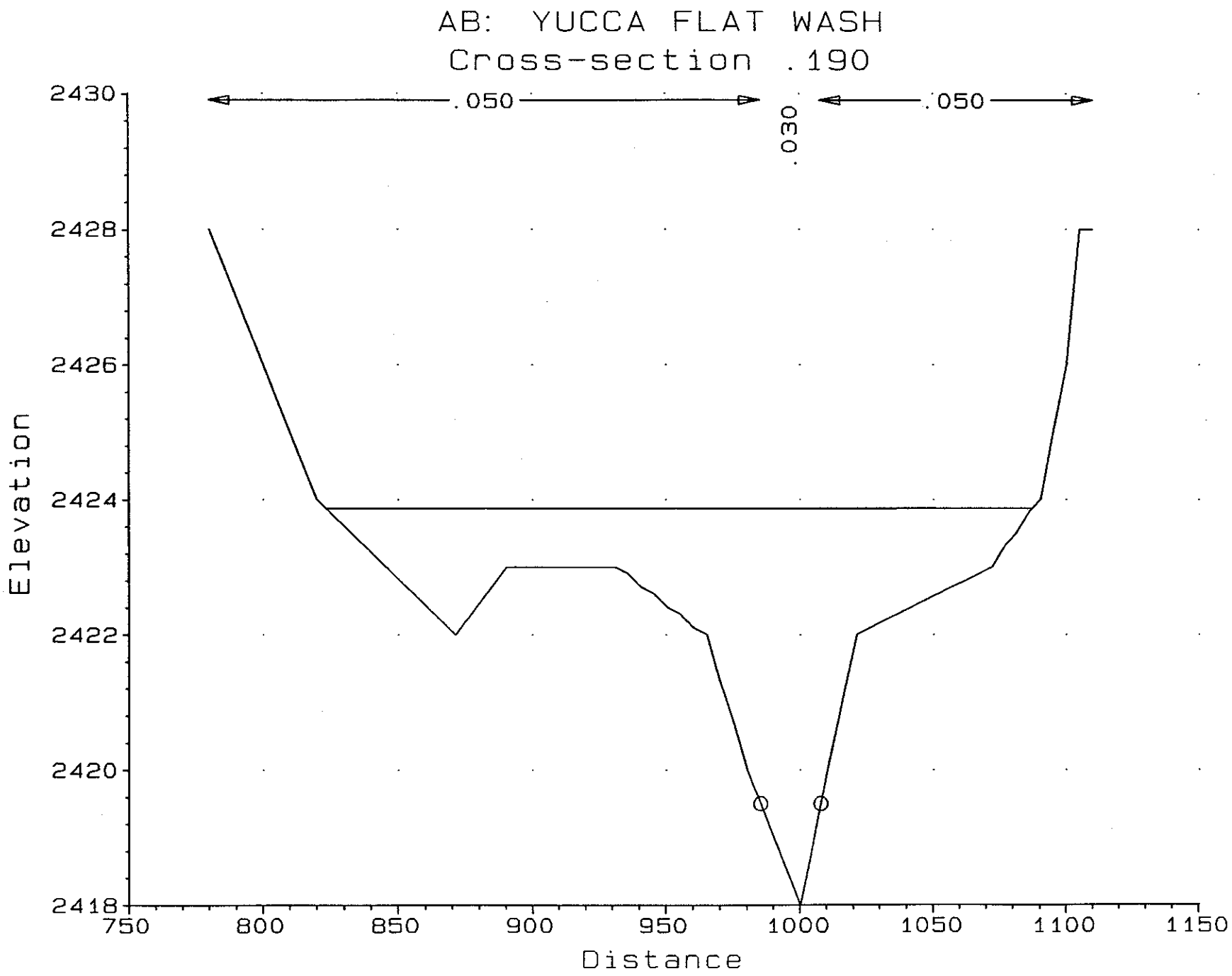
2000
Distance

AB: YUCCA FLAT WASH
Cross-section .098

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Cross-section .190
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.030
.050
Elevation
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2428
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2424
2422
2420
2418
750
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850
900
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1050
1100
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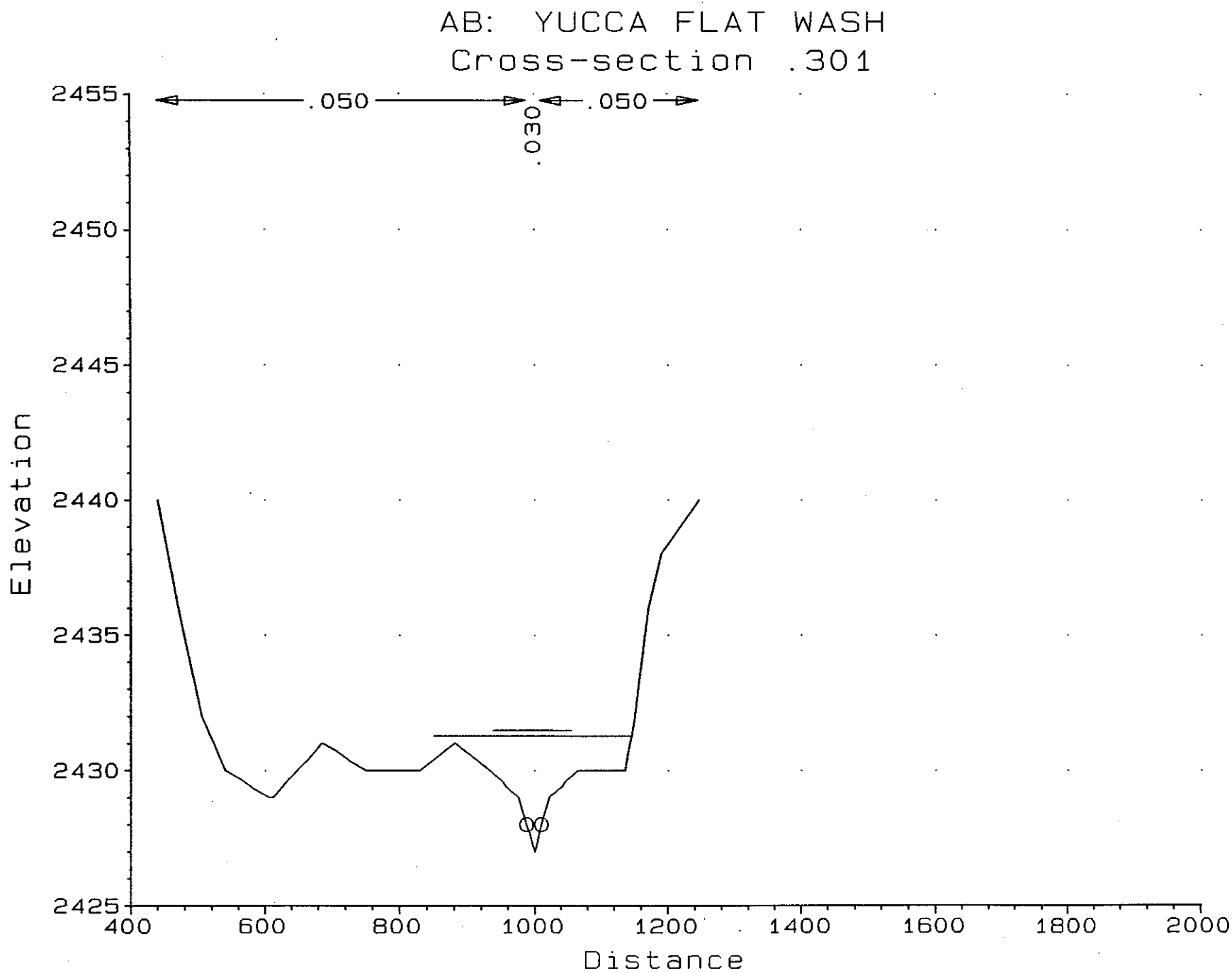
Distance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Cross-section .301
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.030
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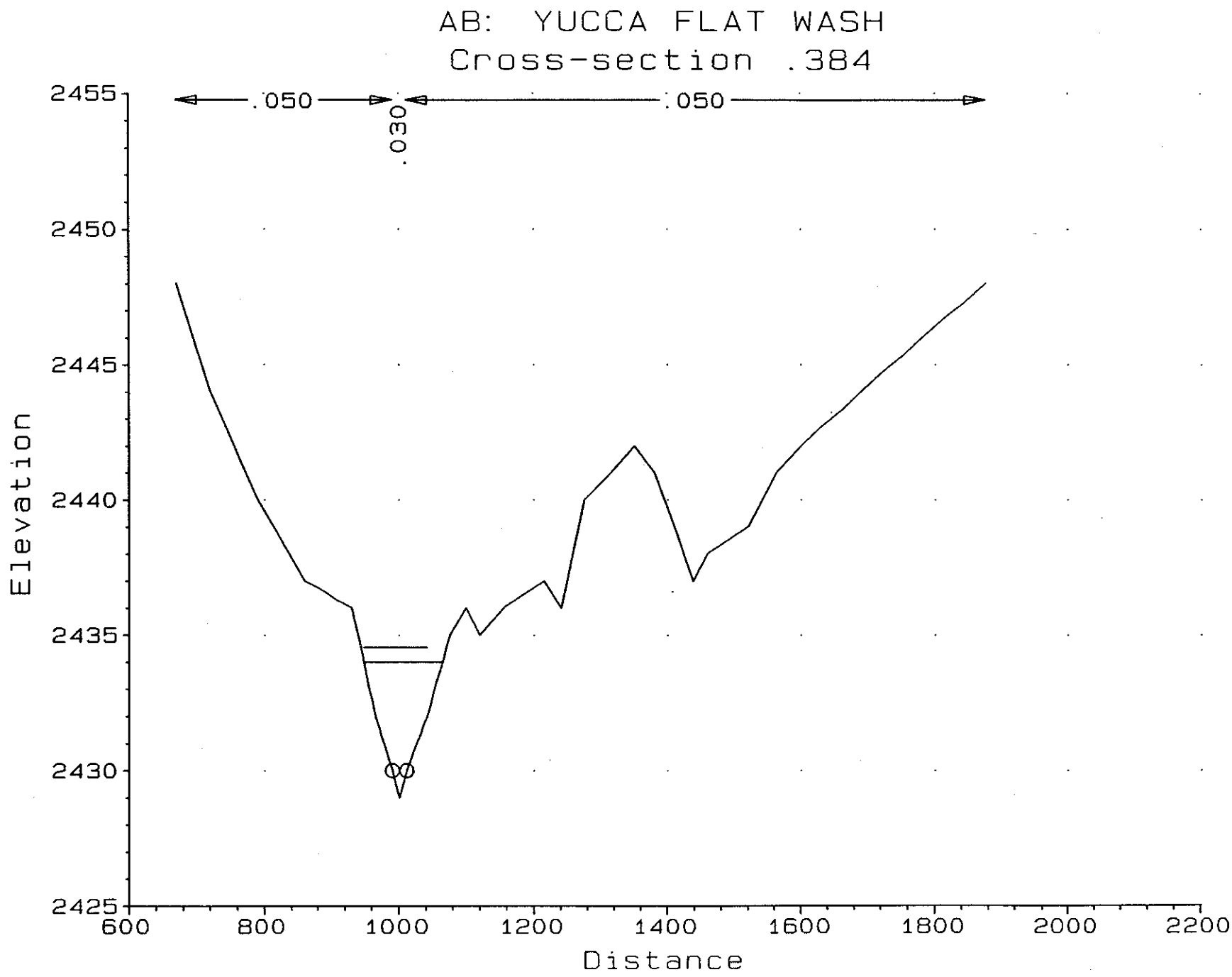
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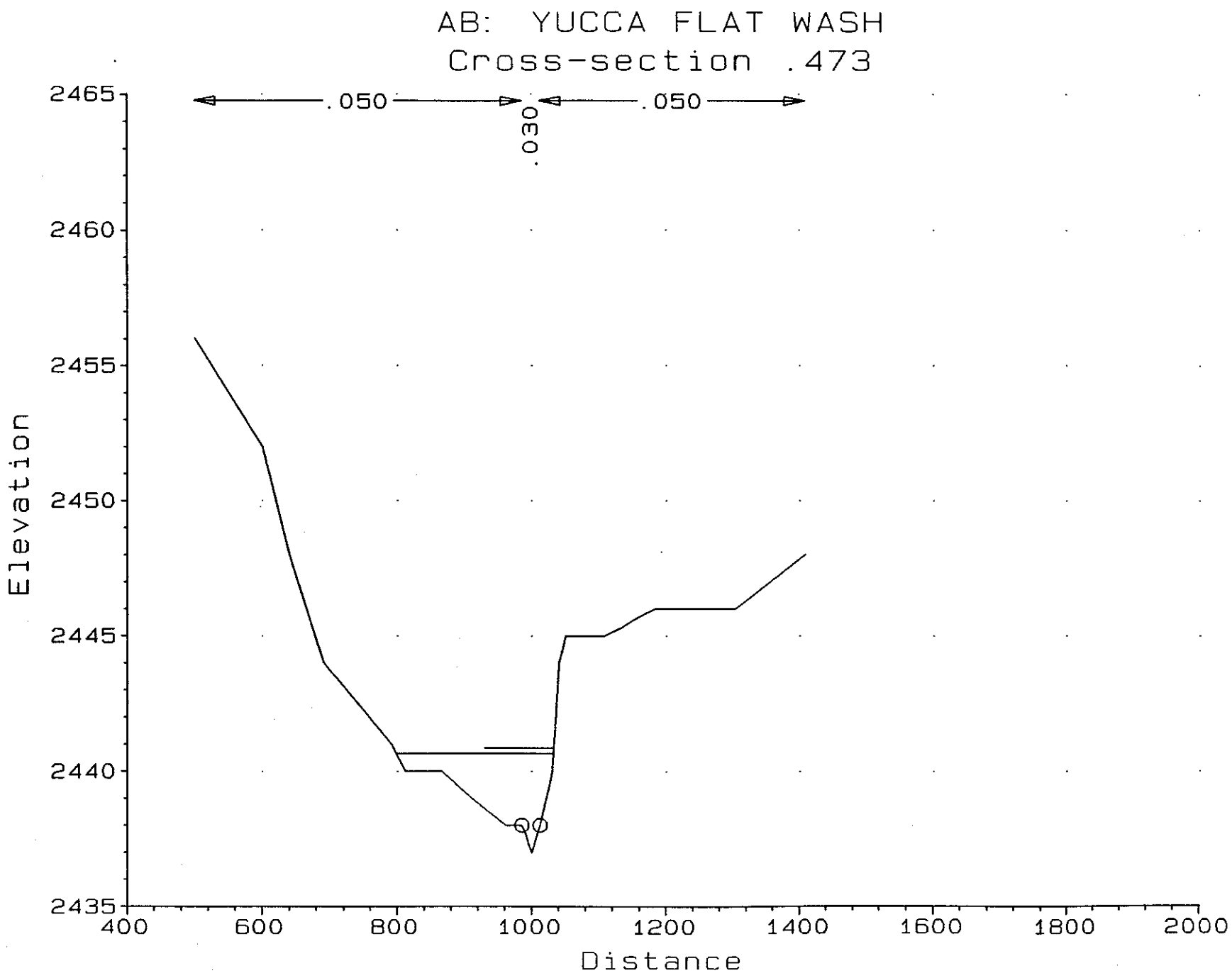
Distance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.030
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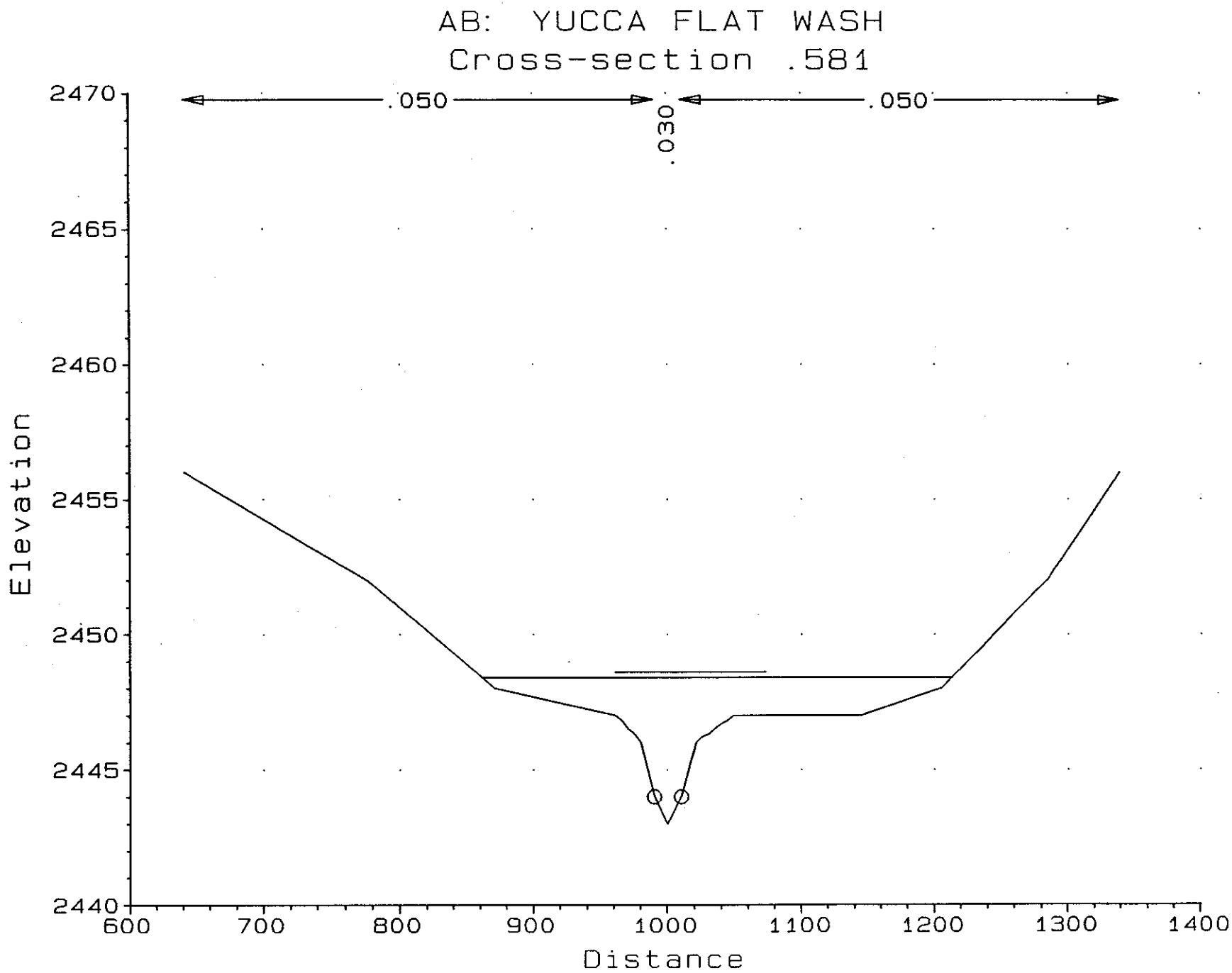
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Cross-section .581
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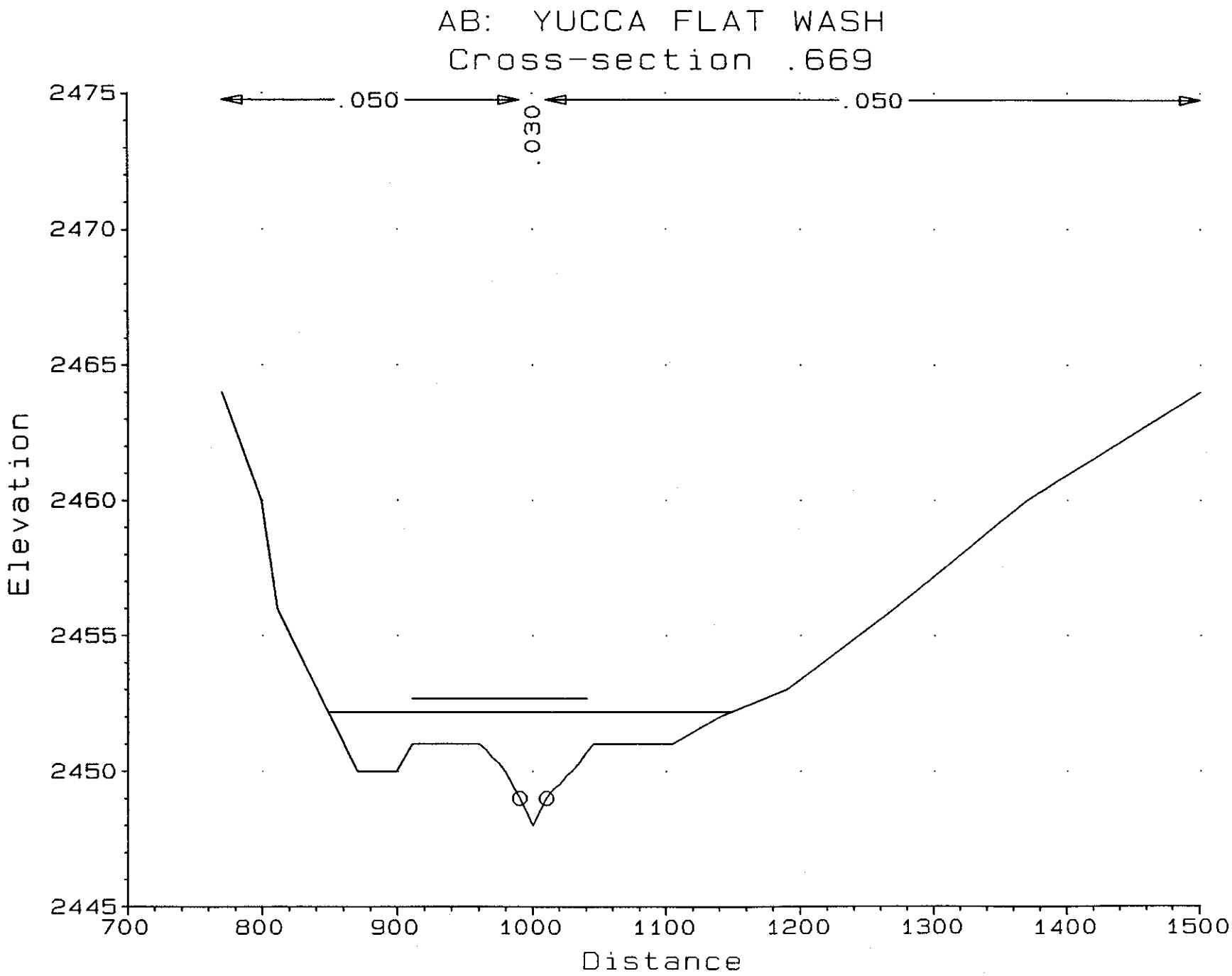
Distance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Cross-section .669
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Elevation
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1200
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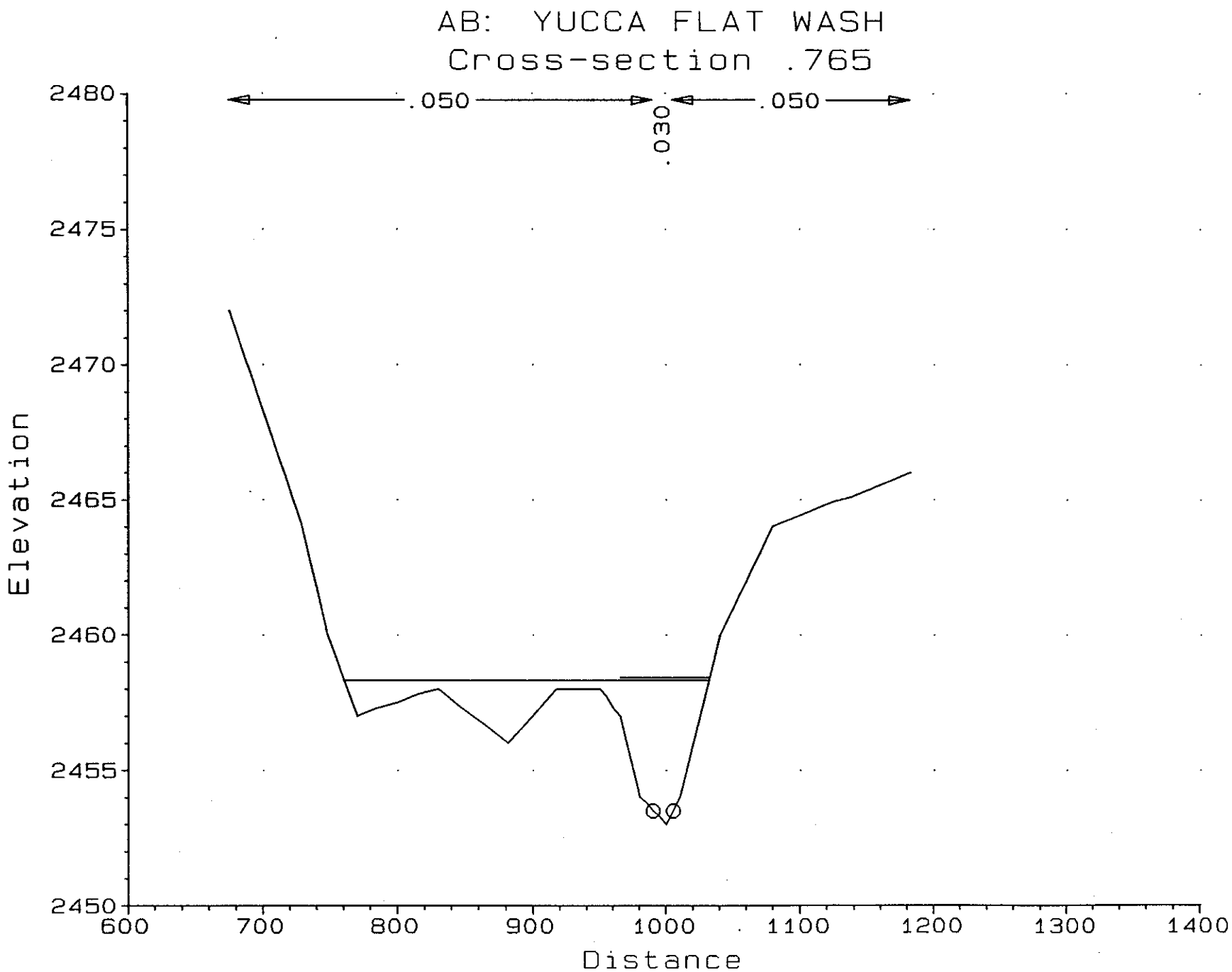
1400
1500
Distance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Cross-section .765
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Elevation
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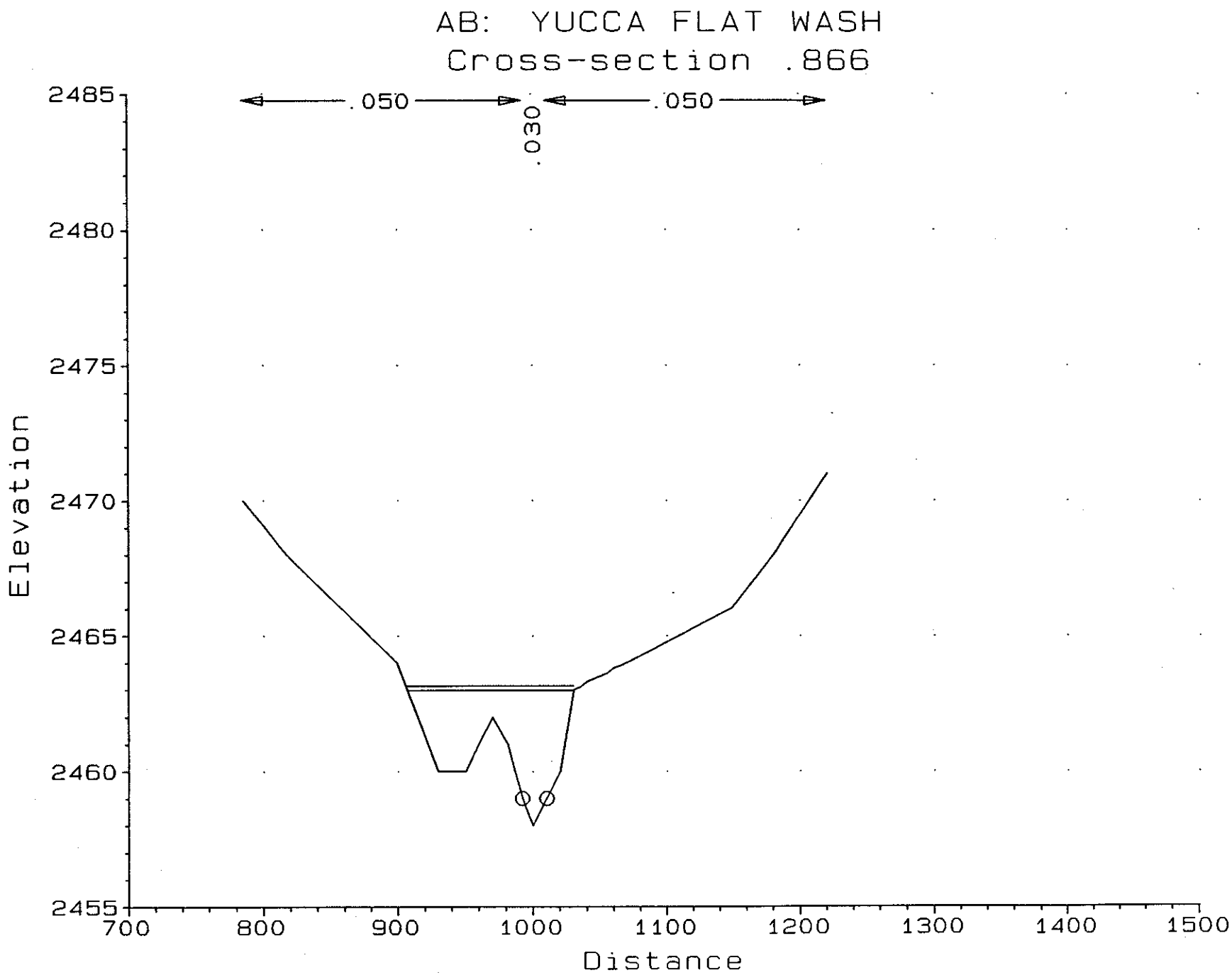
1300
1400
Distance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Cross-section .866
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Elevation
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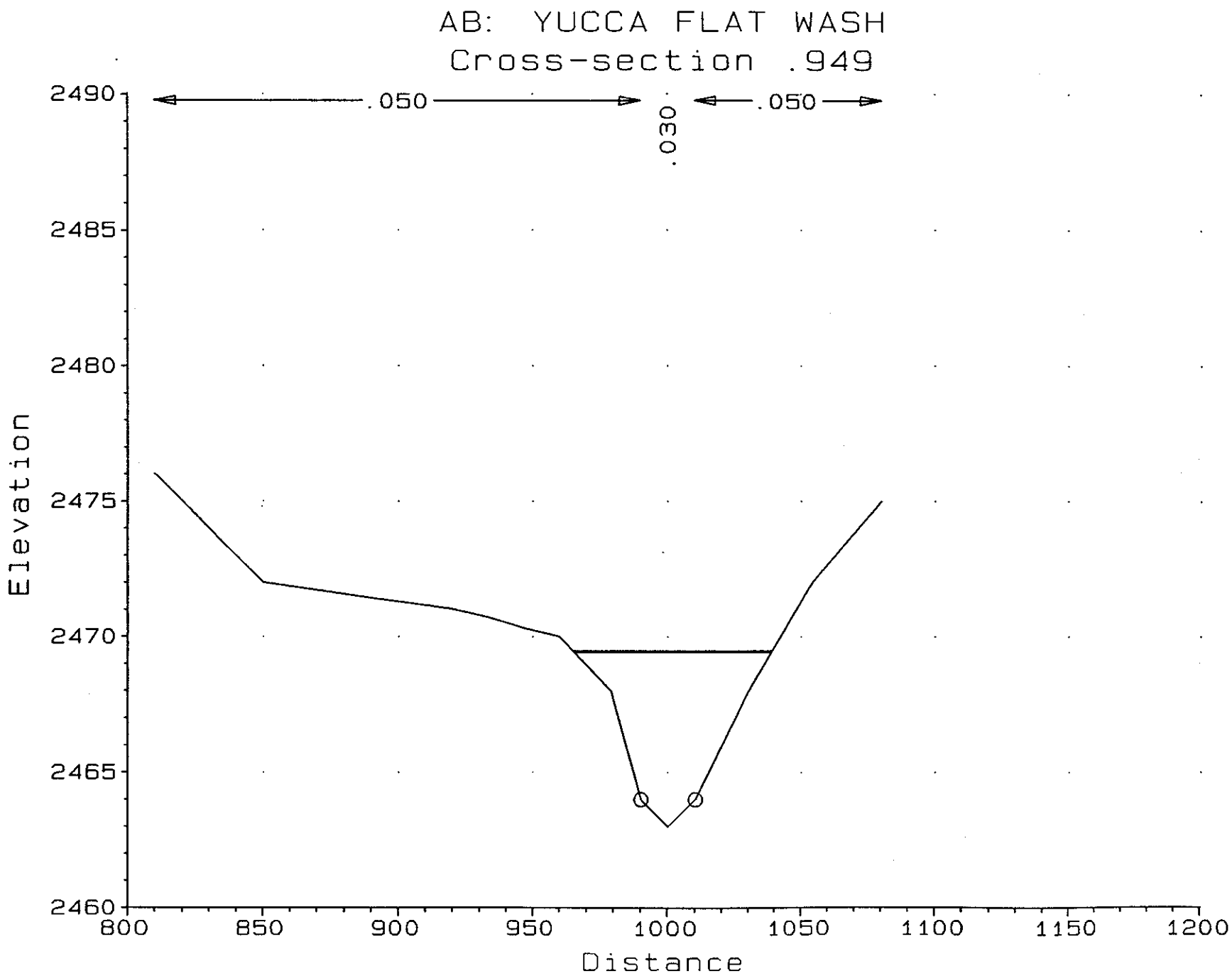
Distance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Elevation
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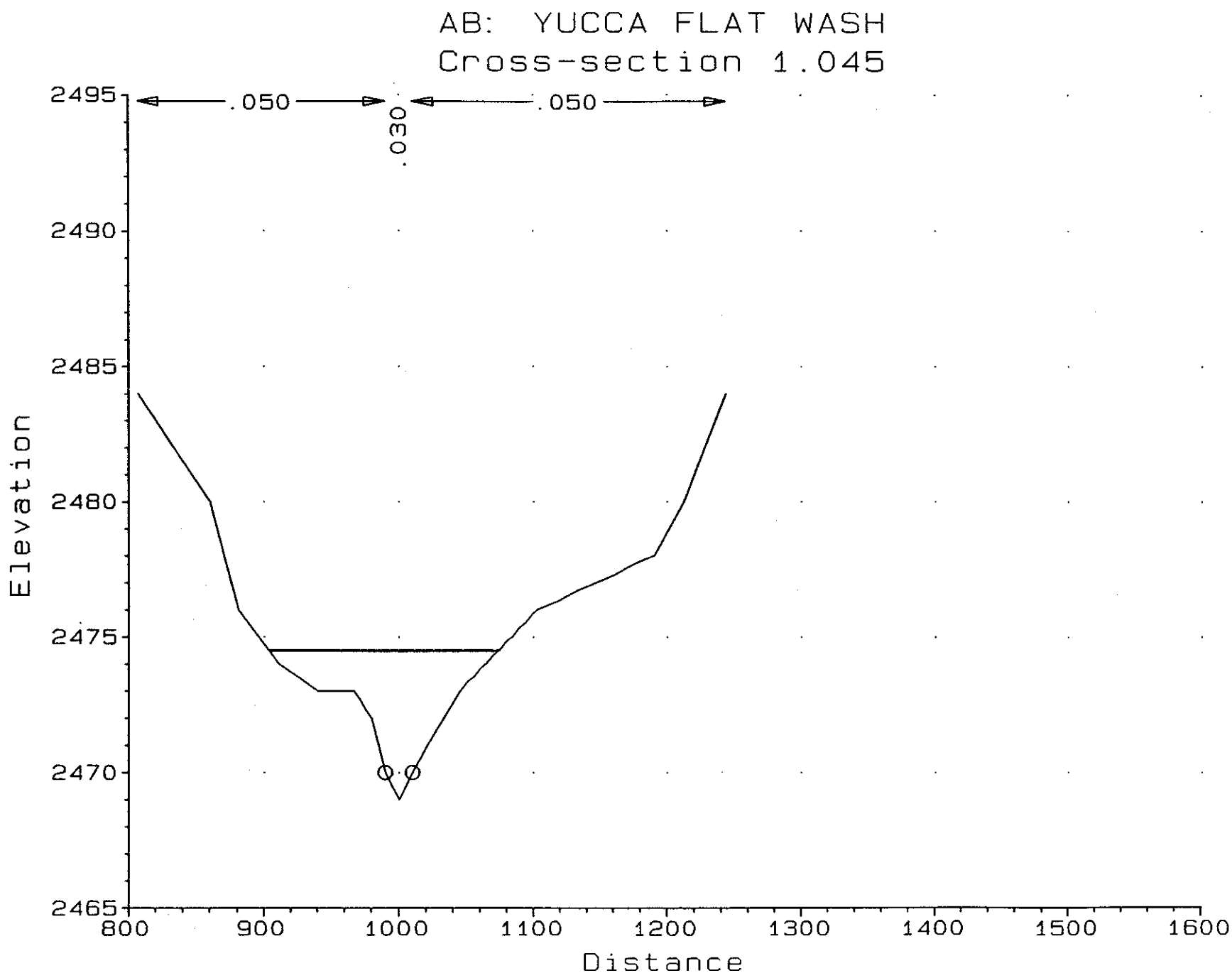
1150
1200
Distance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Cross-section 1.045
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.050
.030
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Elevation
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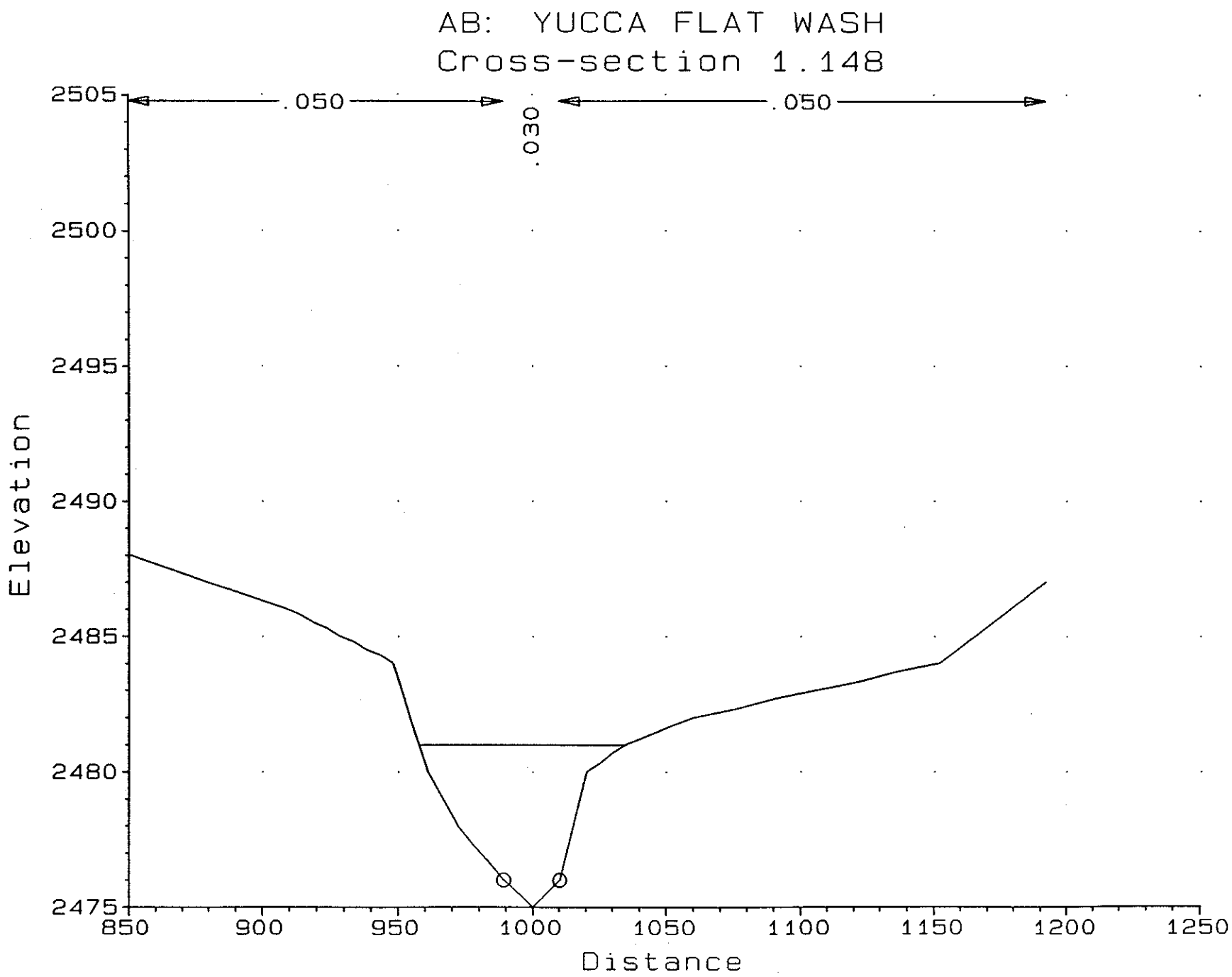
1400
1500
1600
Distance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.030
.050
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Elevation
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1200
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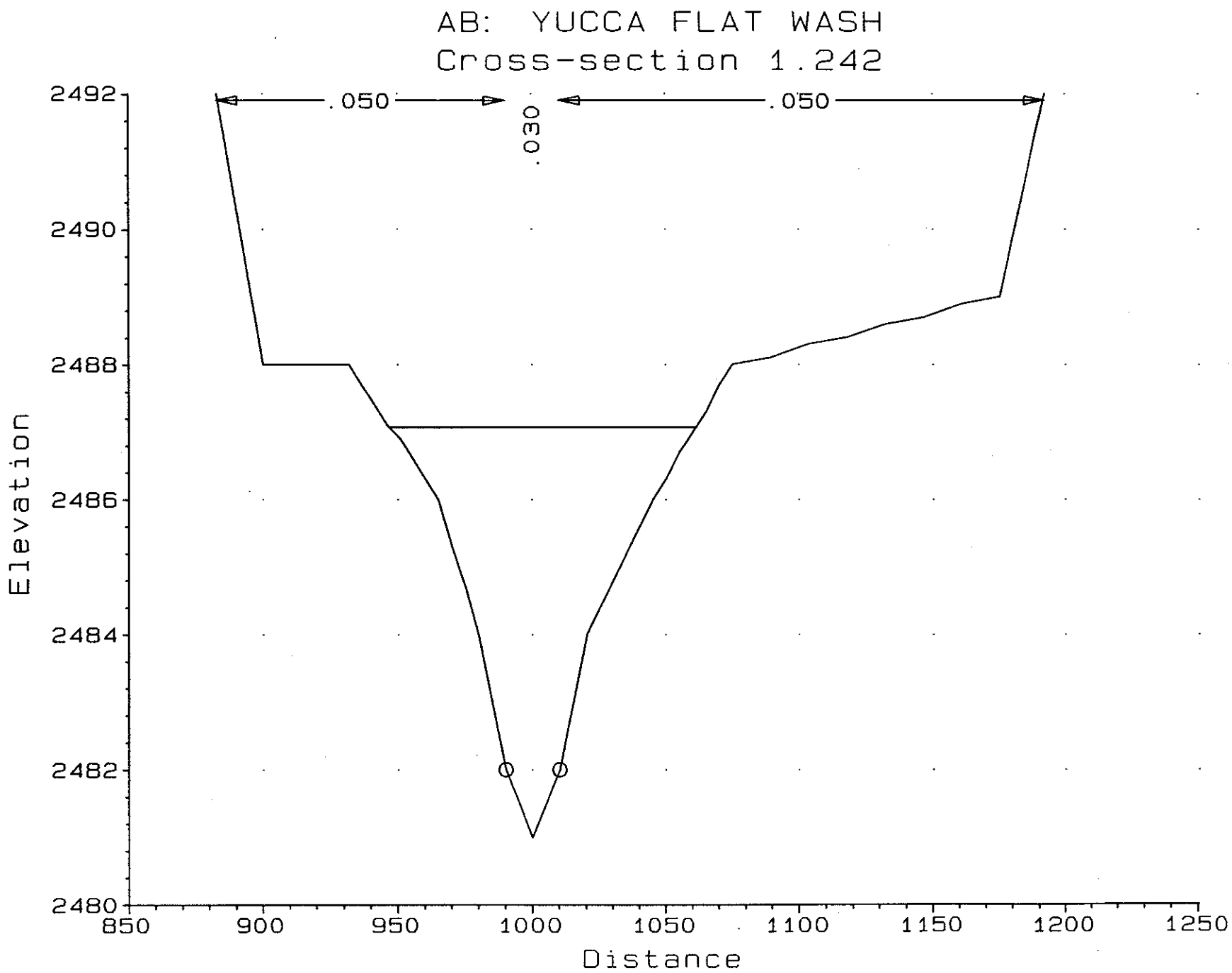
Distance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Cross-section 1.242
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.030
.050
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2490
2488
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2484
2482
2480
Elevation
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1000
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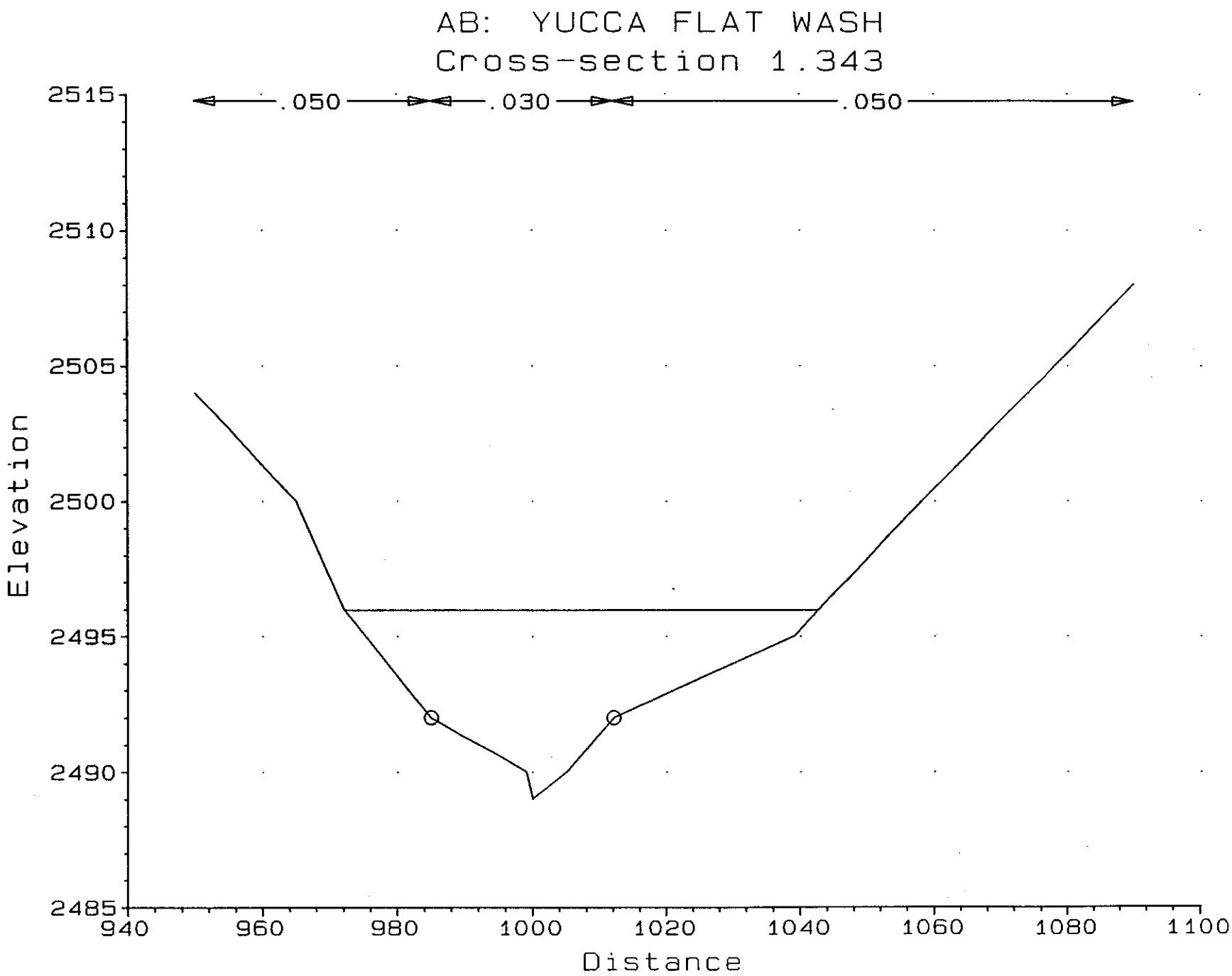
1150
1200
1250
Distance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Cross-section 1.343
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.030
.050
2515
2510
2505
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2495
2490
2485
Elevation
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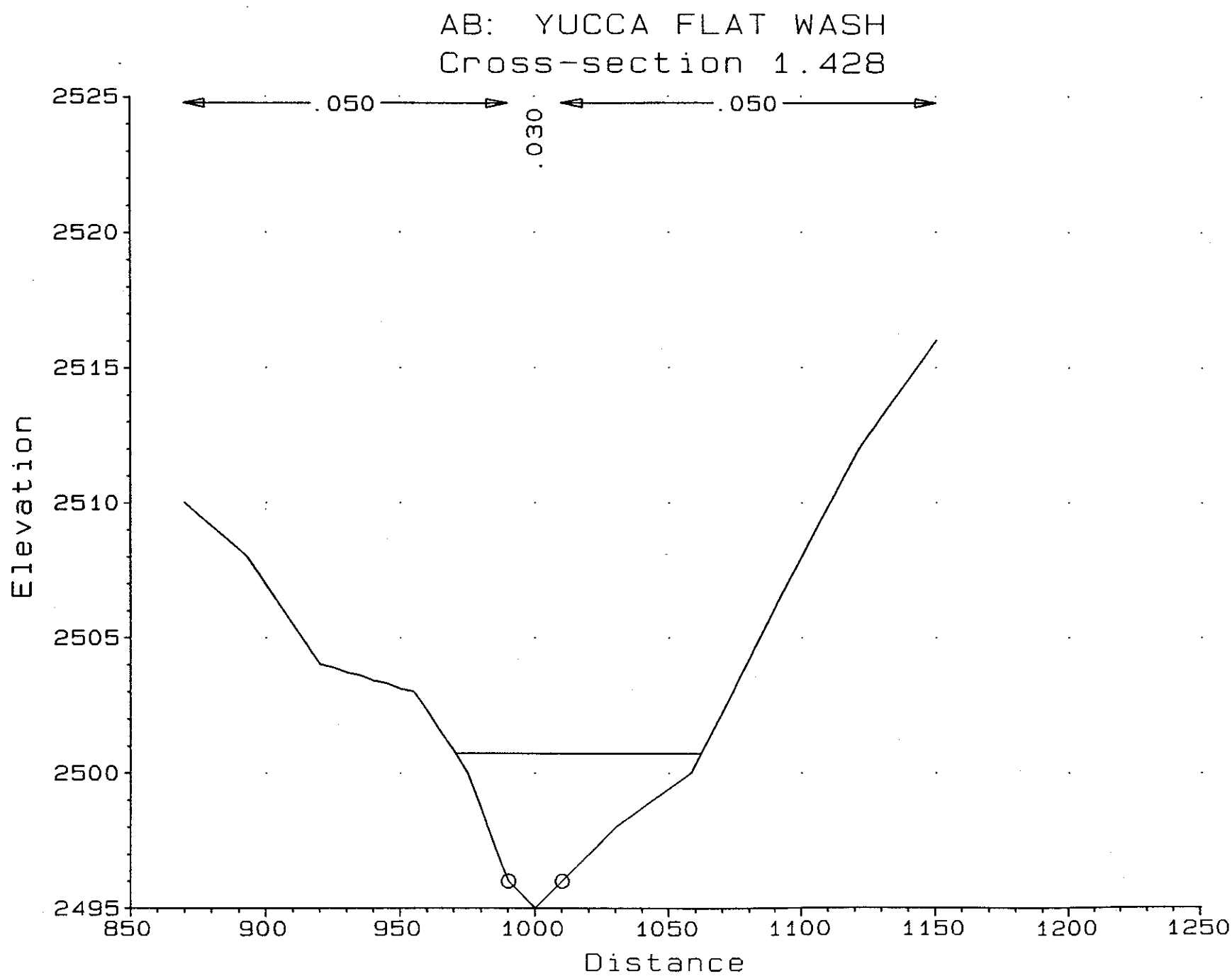
980
1000
1020
1040
1060
1080
1100
Distance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.030
.050
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2505
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Elevation
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1000
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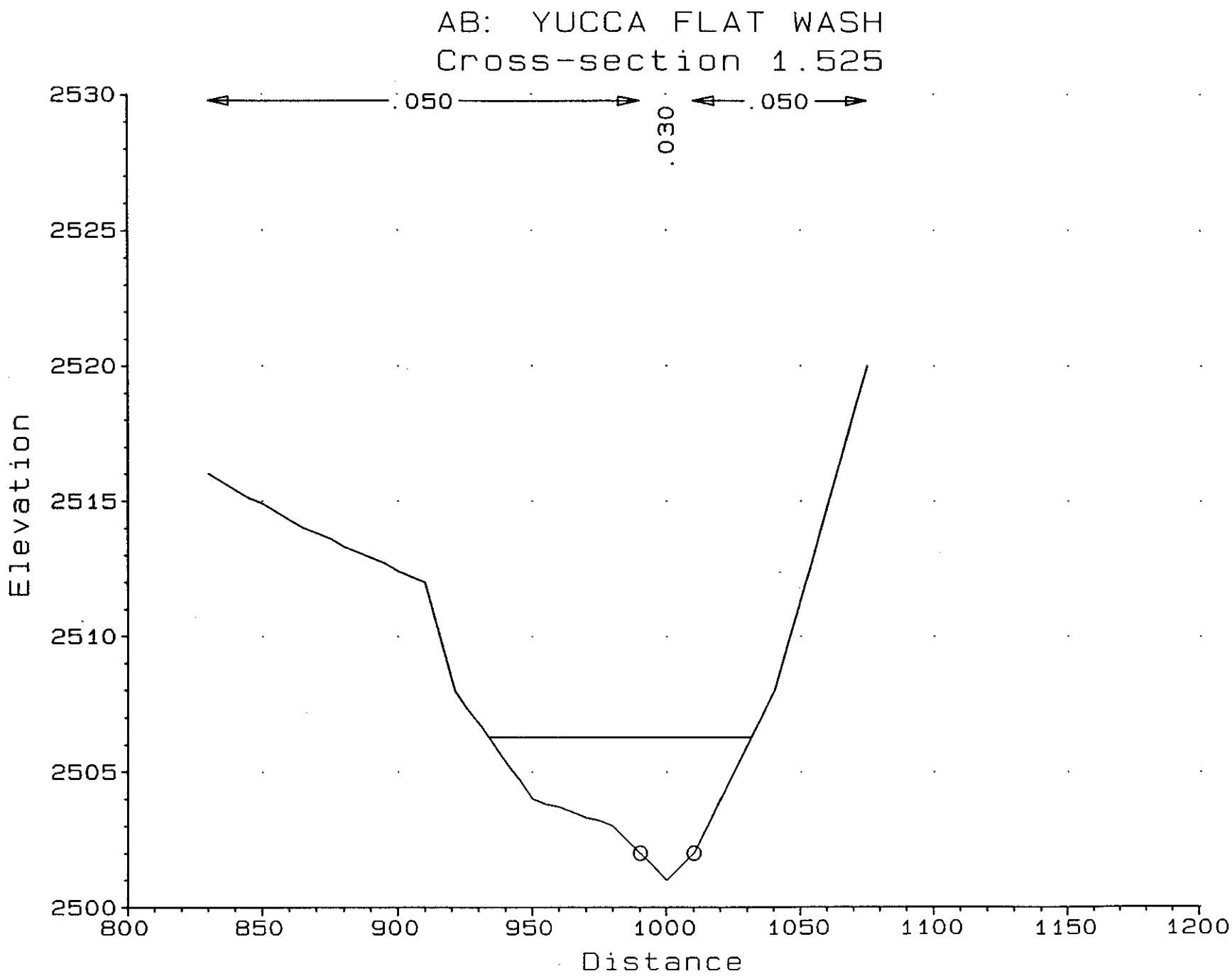
1200
1250
Distance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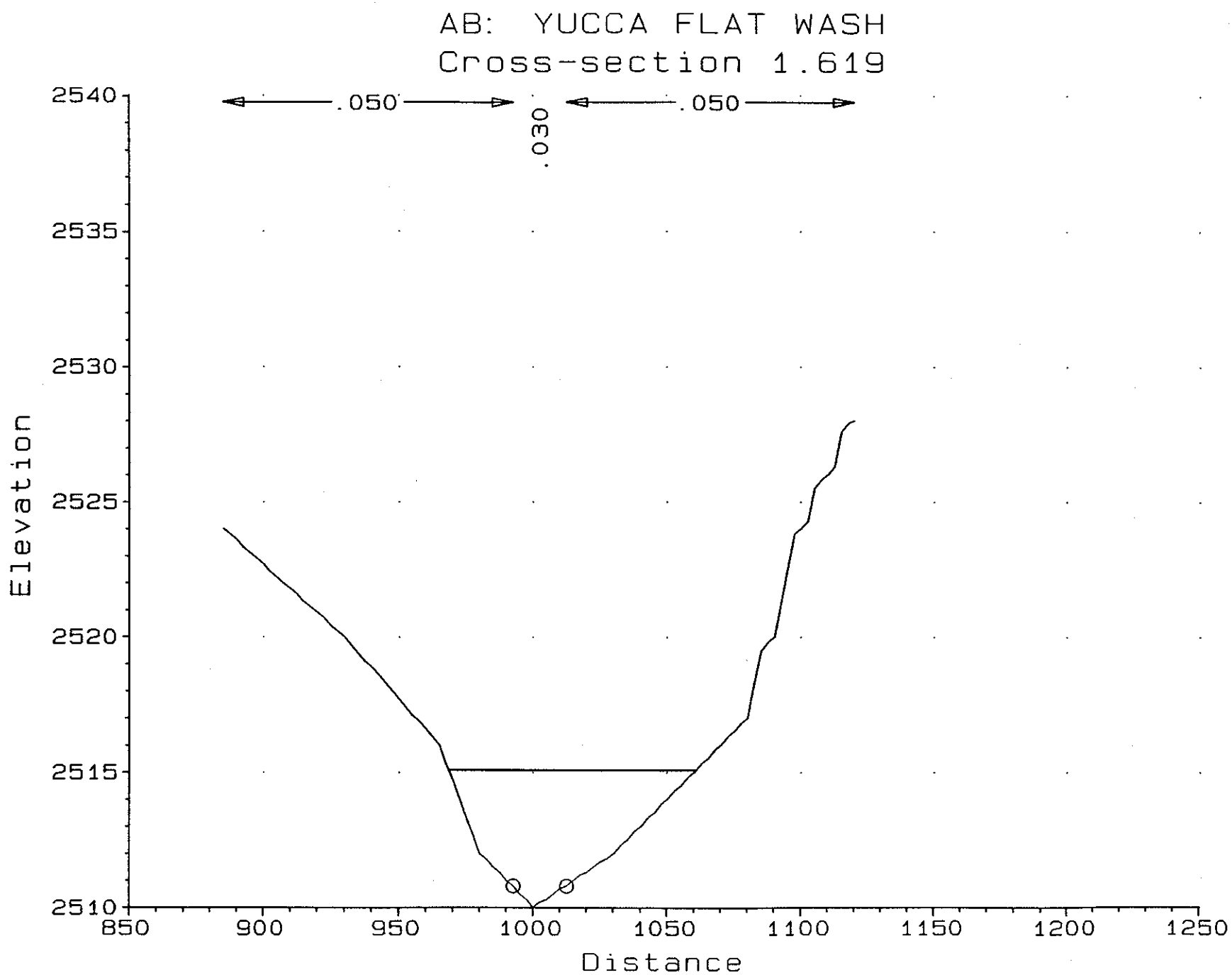
1200
Distance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.050
Elevation
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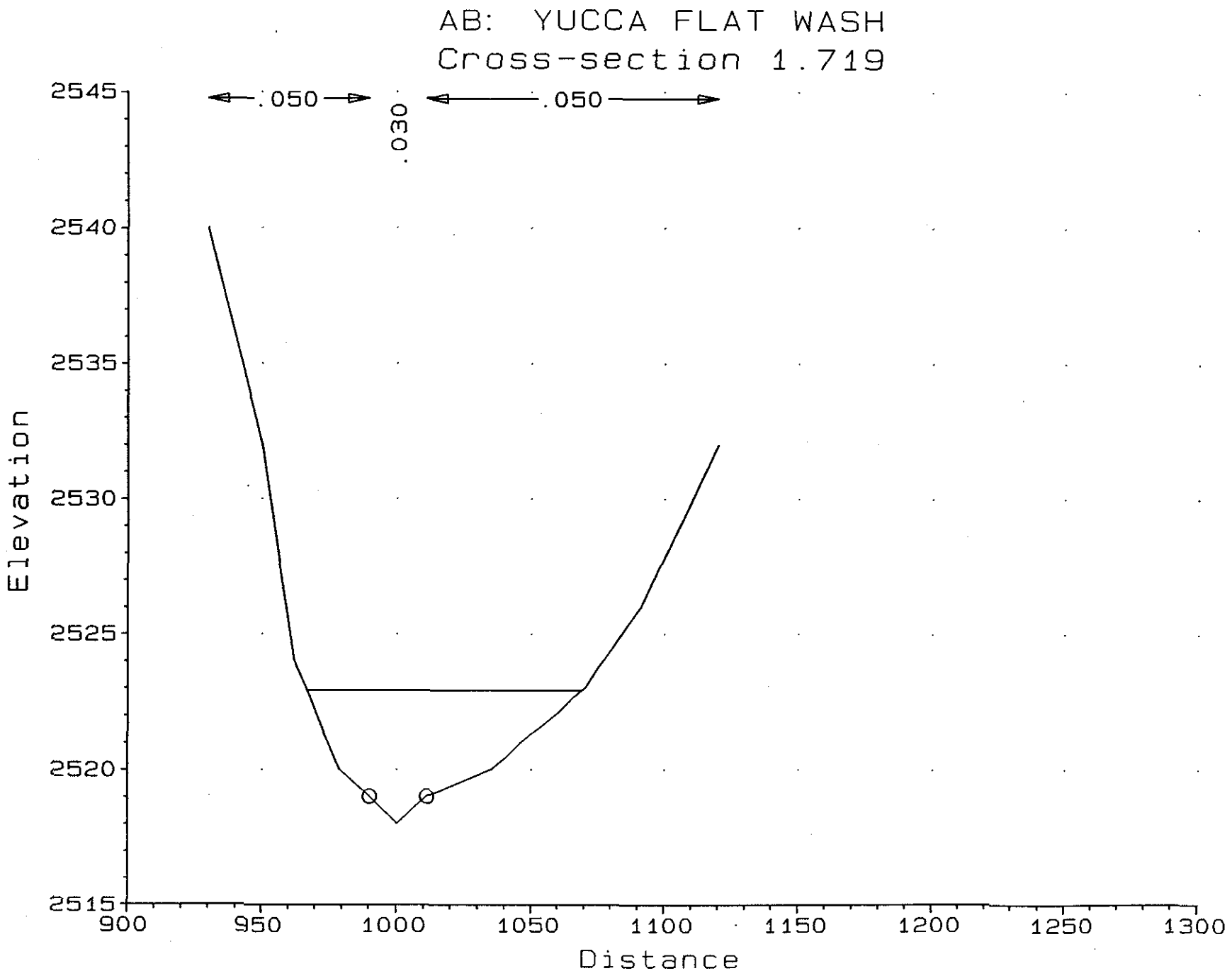
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.030
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Elevation
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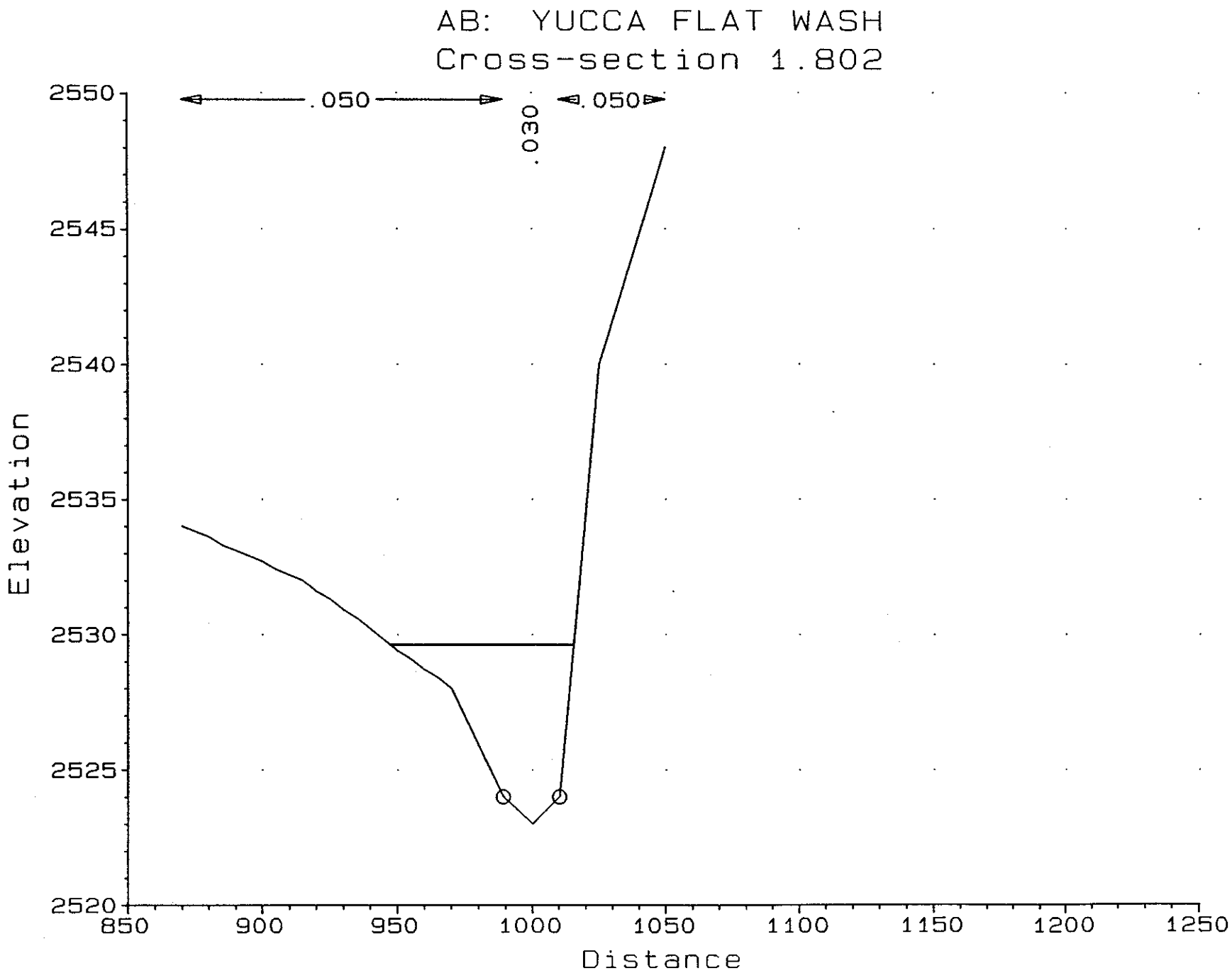
Distance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Cross-section 1.802
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.030
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2550
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Elevation
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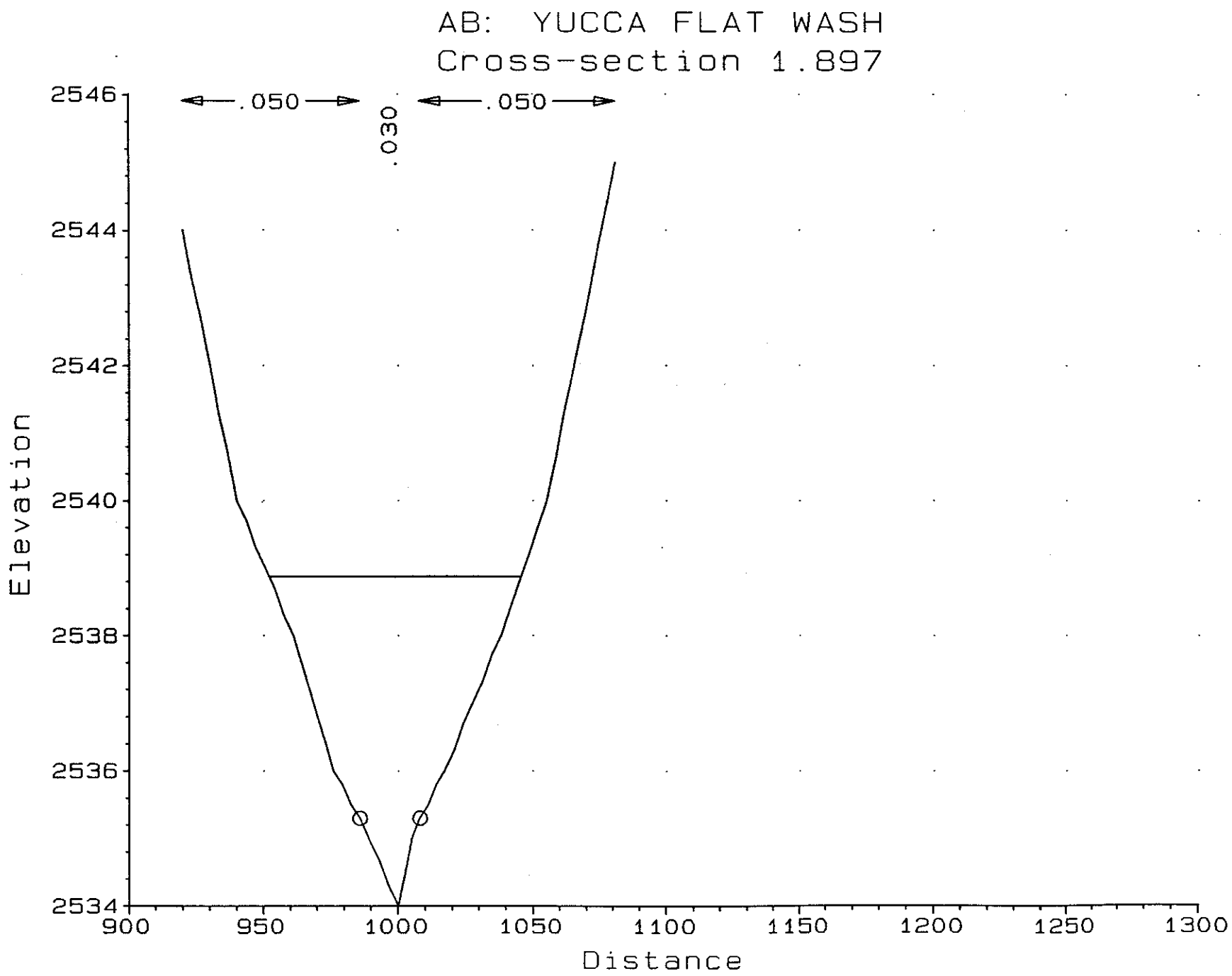
Distance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Cross-section 1.897
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.030
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2546
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Elevation
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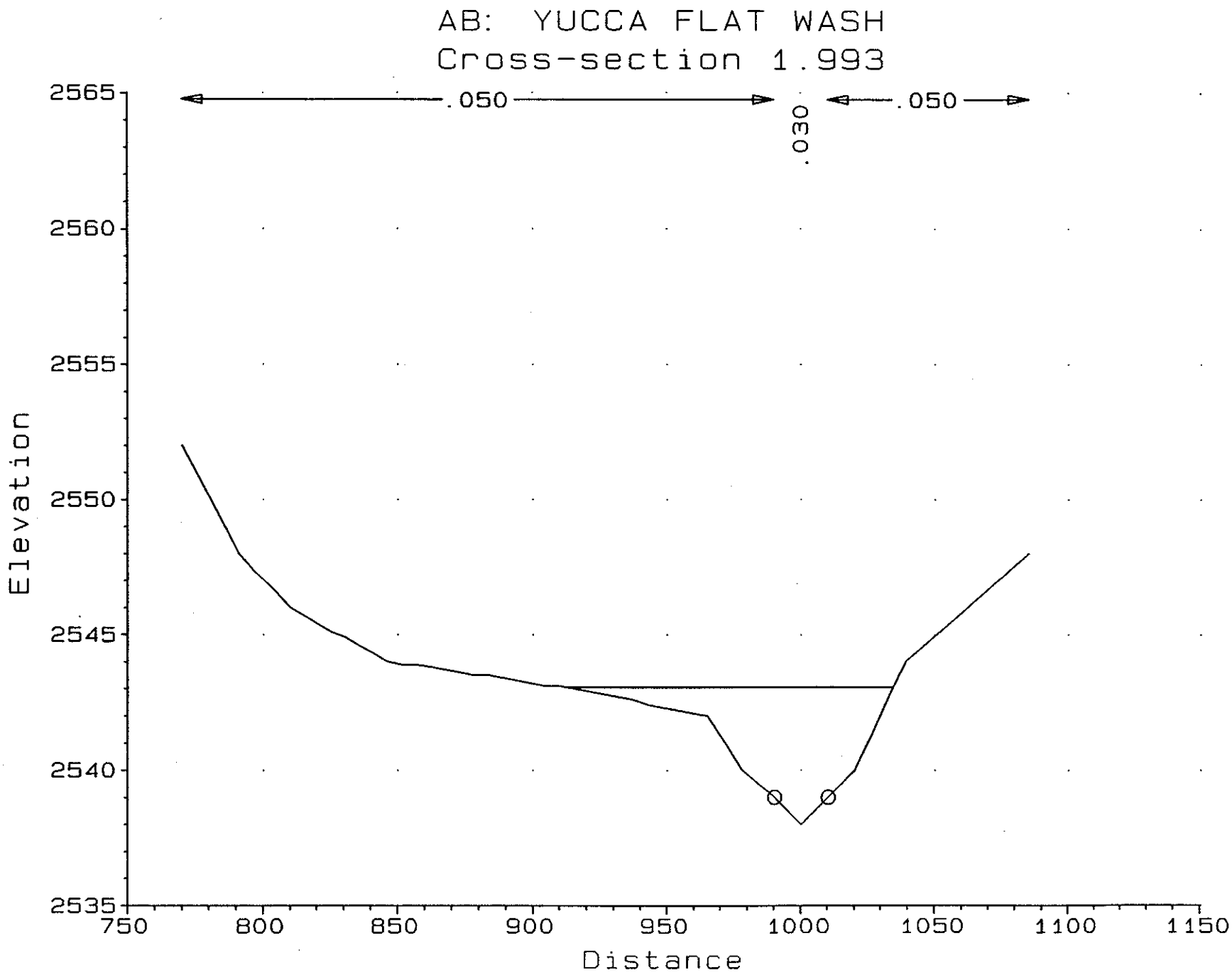
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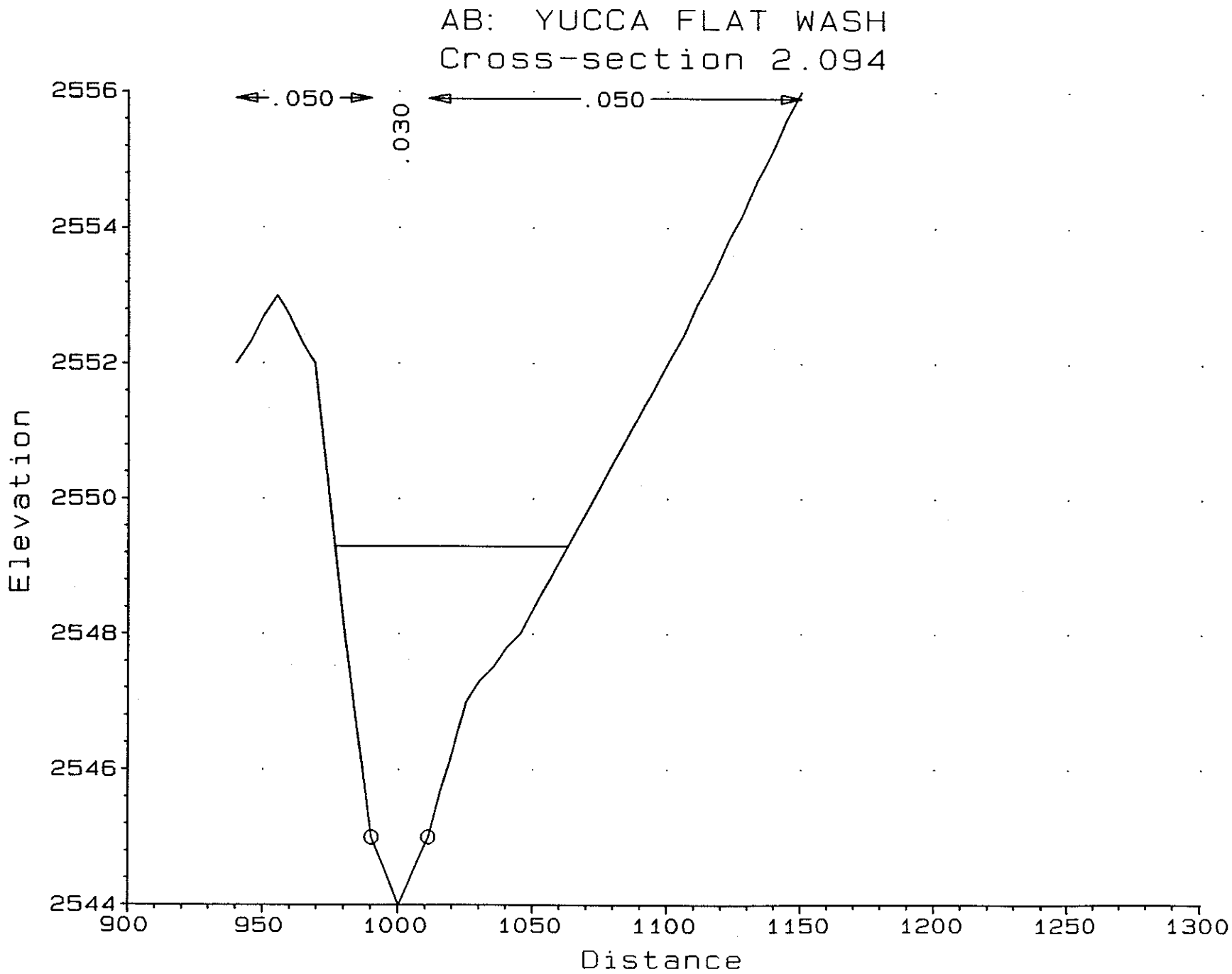
Distance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Cross-section 2.094
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.050
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Elevation
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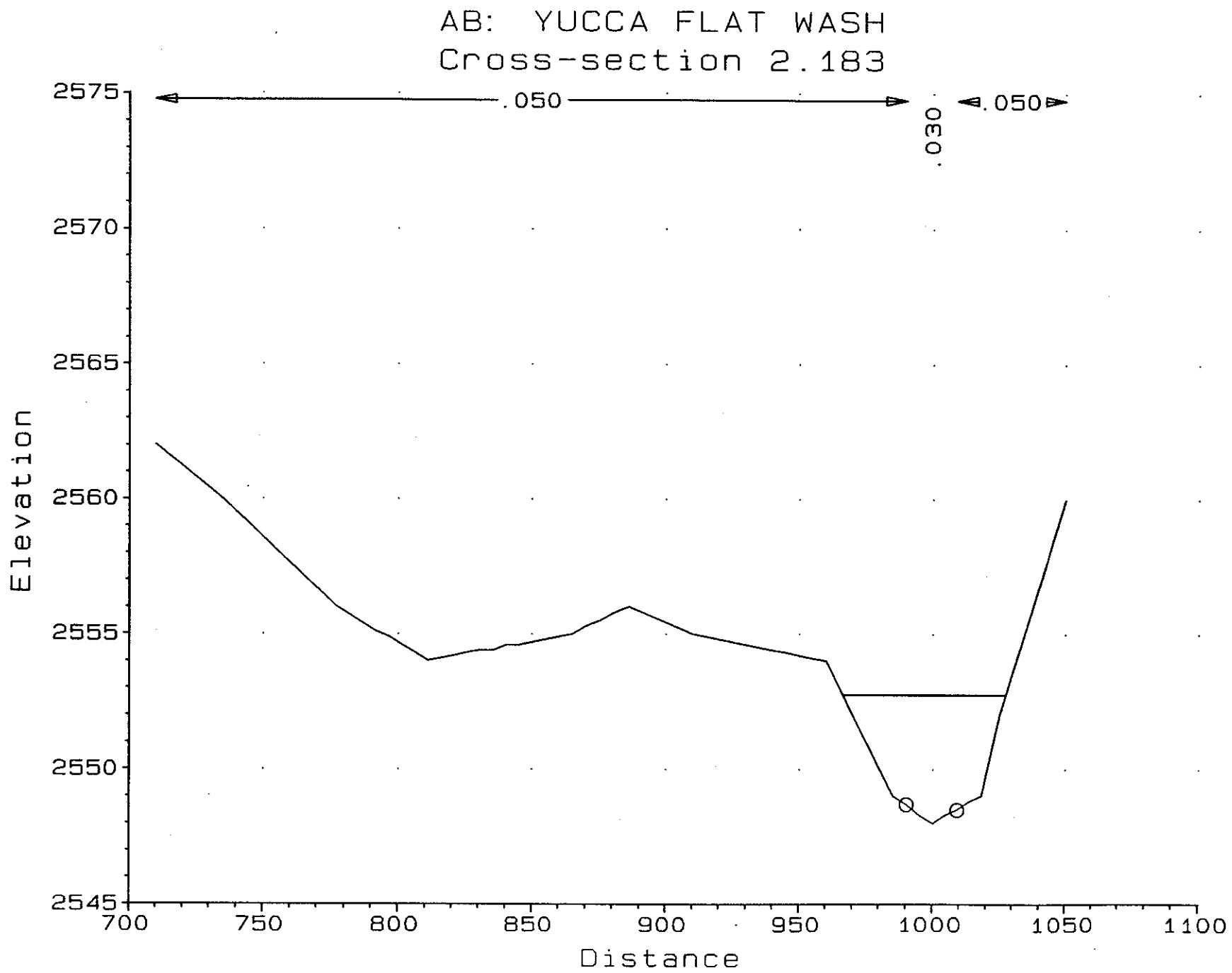
Distance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Cross-section 2.183
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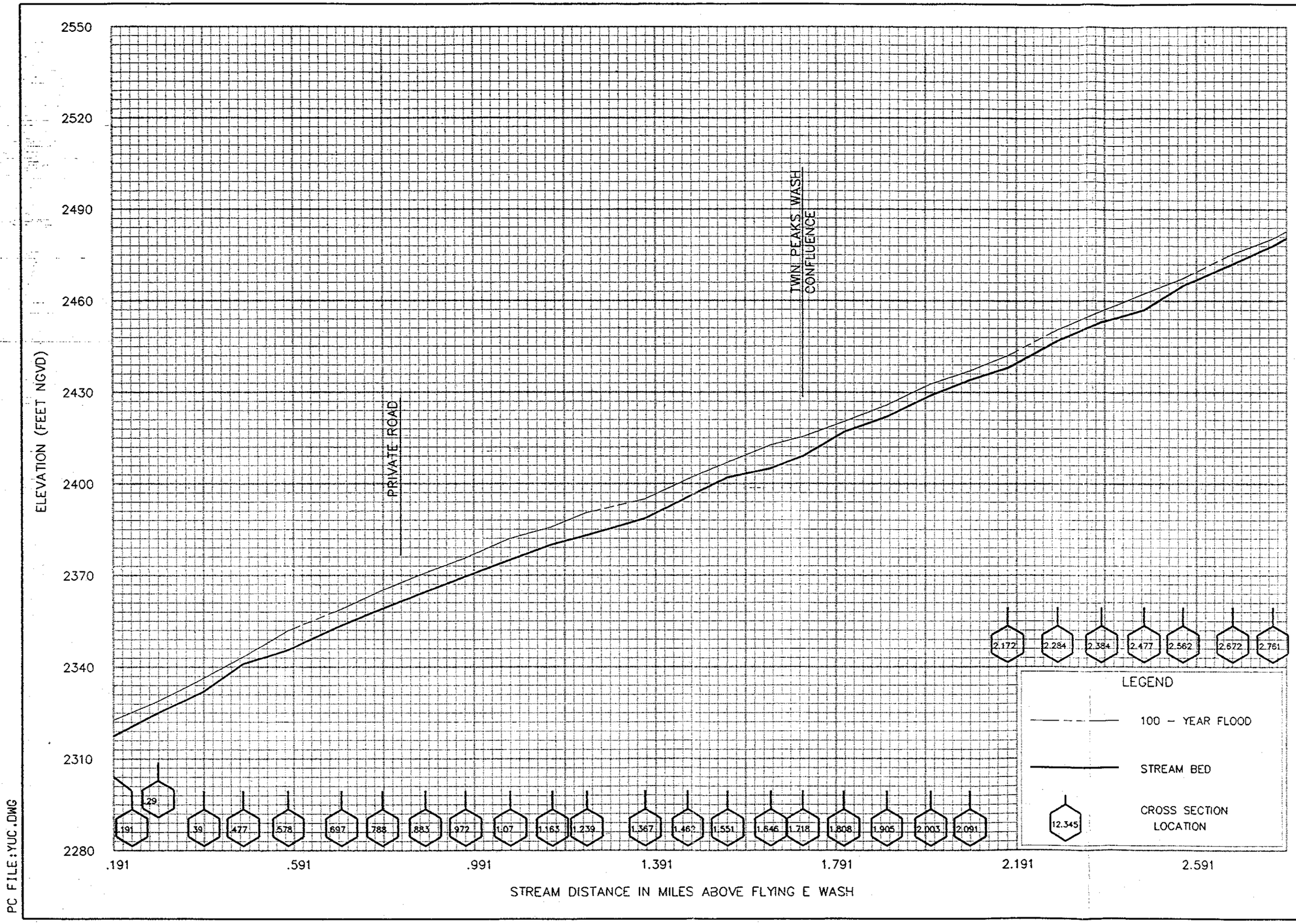


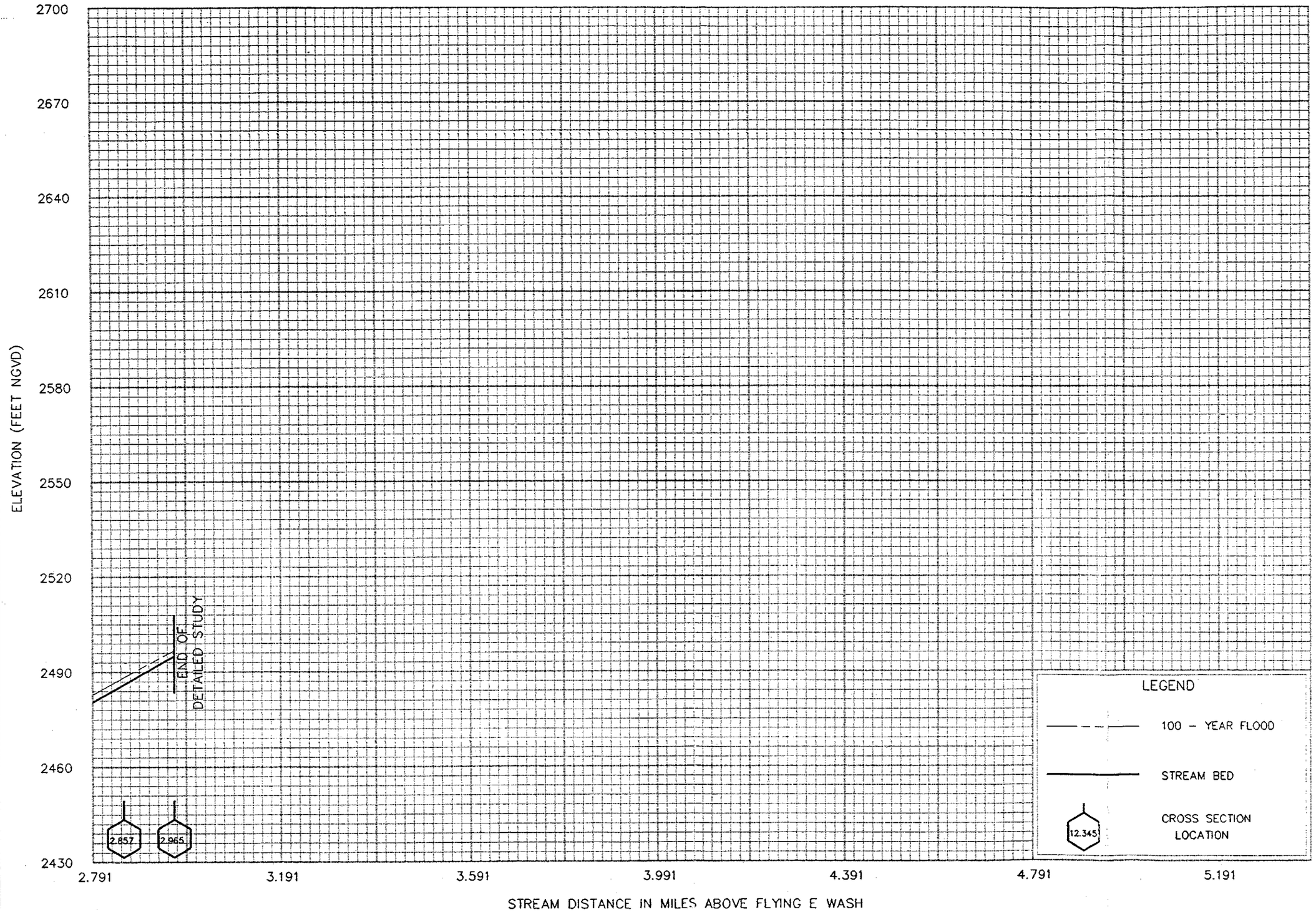

FLOOD PROFILES

YUCCA FLAT WASH

FEDERAL EMERGENCY MANAGEMENT AGENCY

MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

PC FILE:YUC.DWG




FLOOD PROFILES

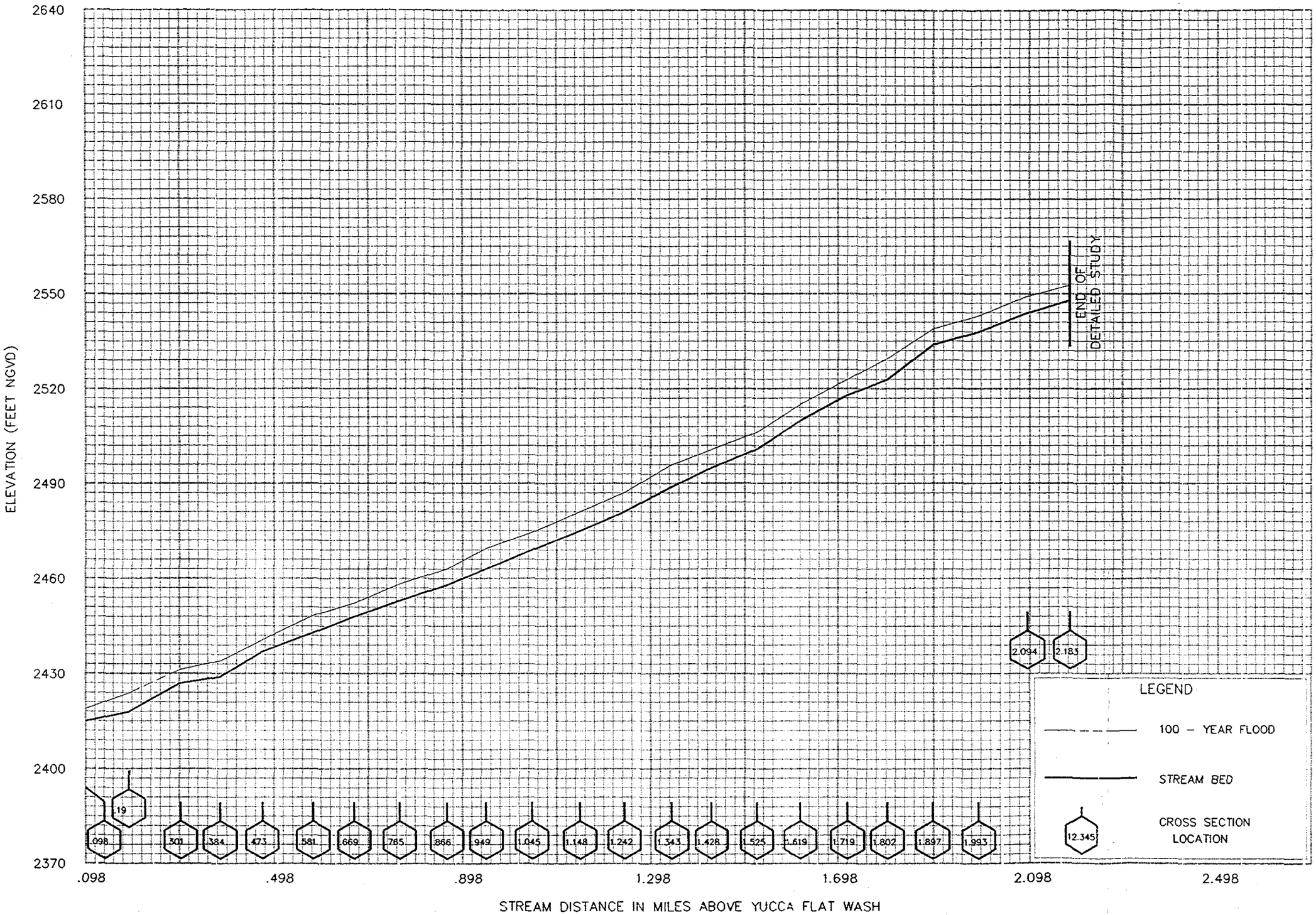
YUCCA FLAT WASH

FEDERAL EMERGENCY MANAGEMENT AGENCY

MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

02/21/94 13:30:10 ACD-12_

PC FILE:YUC.DWG




FLOOD PROFILES

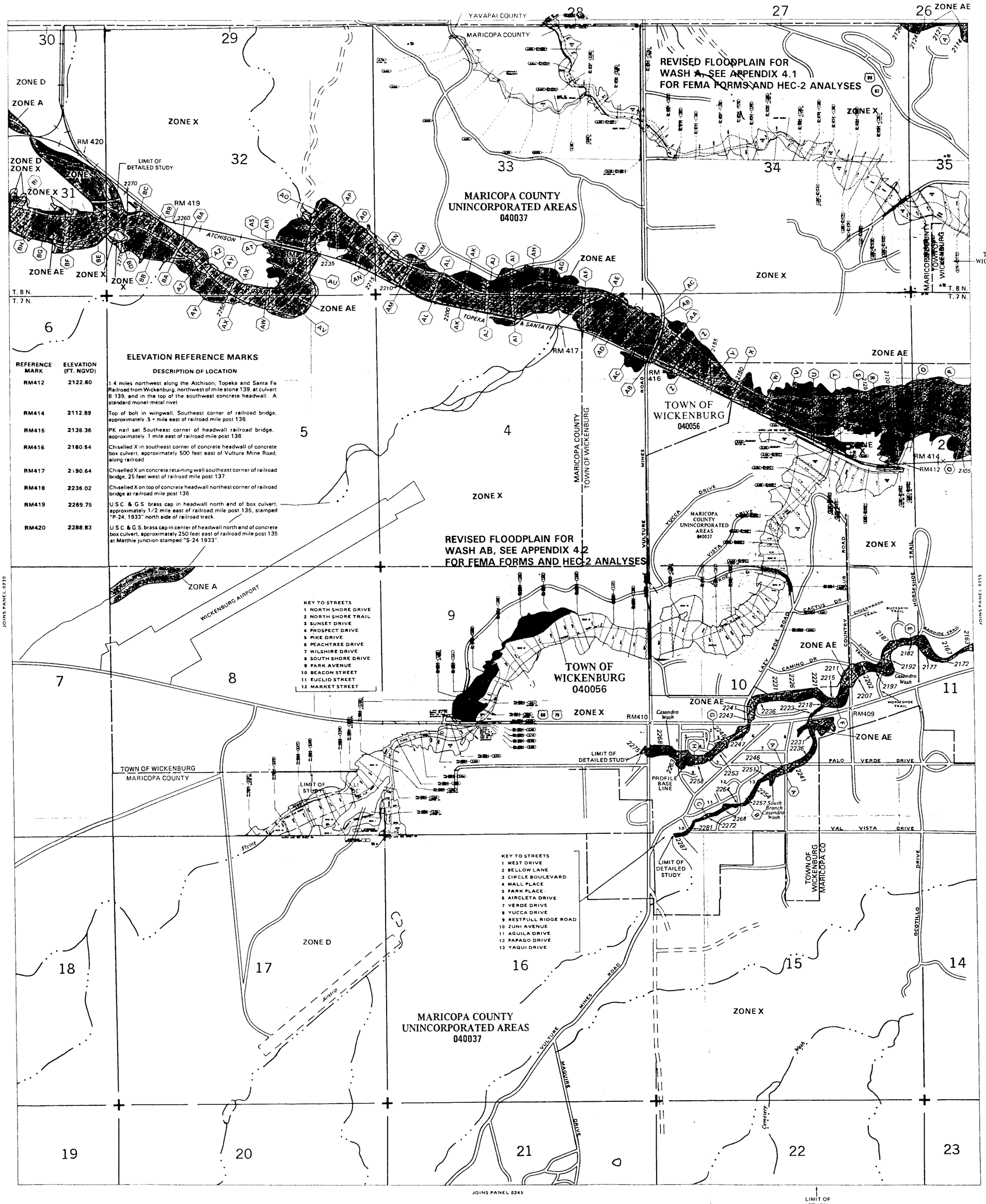
TWIN PEAKS WASH

FEDERAL EMERGENCY MANAGEMENT AGENCY

MARICOPA COUNTY, AZ
AND INCORPORATED AREAS

02/17/94 15:36:54 ACD-12_

PC FILE:TPW.DWG




## ELEVATION REFERENCE MARKS

| REFERENCE MARK | ELEVATION (FT. NGVD) | DESCRIPTION OF LOCATION |
|---|---|---|
| RM412 | 2122.60 | 1.4 miles northwest along the Atchison, Topeka and Santa Fe Railroad from Wickenburg, northwest of mile stone 139, at culvert B 139, and in the top of the southwest concrete headwall. A standard monel-metal rivet |
| RM414 | 2112.89 | Top of bolt in wingwall, Southeast corner of railroad bridge, approximately .5 + mile east of railroad mile post 138. |
| RM415 | 2138.36 | PK nail set Southeast corner of headwall railroad bridge, approximately .1 mile east of railroad mile post 138. |
| RM416 | 2160.54 | Chiselled X in southeast corner of concrete headwall of concrete box culvert, approximately 500 feet east of Vulture Mine Road, along railroad. |
| RM417 | 2190.64 | Chiselled X on concrete retaining wall southeast corner of railroad bridge, 25 feet west of railroad mile post 137. |
| RM418 | 2236.02 | Chiselled X on top of concrete headwall northest corner of railroad bridge at railroad mile post 136. |
| RM419 | 2269.75 | U.S.C. & G.S. brass cap in headwall north end of box culvert, approximately 1/2 mile east of railroad mile post 135, stamped "P-24, 1933" north side of railroad track. |
| RM420 | 2288.83 | U.S.C. & G.S. brass cap in center of headwall north end of concrete box culvert, approximately 250 feet east of railroad mile post 135 at Matthie junction stamped "S-24 1933". |

## LEGEND

SPECIAL FLOOD HAZARD AREAS INUNDATED BY 100-YEAR FLOOD

- **ZONE A** No base flood elevations determined.
- **ZONE AE** Base flood elevations determined.
- **ZONE AH** Flood depths of 1 to 3 feet (usually areas of ponding); base flood elevations determined.
- **ZONE AO** Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.
- **ZONE A99** To be protected from 100-year flood by Federal flood protection system under construction; no base elevations determined.
- **ZONE V** Coastal flood with velocity hazard (wave action); no base flood elevations determined.
- **ZONE VE** Coastal flood with velocity hazard (wave action); base flood elevations determined.

FLOODWAY AREAS IN ZONE AE

OTHER FLOOD AREAS

- **ZONE X** Areas of 500-year flood; areas of 100-year flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 100-year flood.

OTHER AREAS

- **ZONE X** Areas determined to be outside 500-year flood plain.
- **ZONE D** Areas in which flood hazards are undetermined.

Flood Boundary

Floodway Boundary

Zone D Boundary

Boundary Dividing Special Flood Hazard Zones, and Boundary Dividing Areas of Different Coastal Base Flood Elevations Within Special Flood Hazard Zones.

513 — Base Flood Elevation Line; Elevation in Feet*

D — D Cross Section Line

(EL 987) Base Flood Elevation in Feet Where Uniform Within Zone*

RM7 X Elevation Reference Mark

*Referenced to the National Geodetic Vertical Datum of 1929

## NOTES

This map is for use in administering the National Flood Insurance Program; it does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size, or all planimetric features outside Special Flood Hazard Areas.

Areas of special flood hazard (100-year flood) include Zones A, A1-30, AE, AH, AO, A99, V, V1-30 AND VE.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations, with regard to requirements of the Federal Emergency Management Agency.

Floodway widths in some areas may be too narrow to show to scale. Floodway widths are provided in the Flood Insurance Study Report.

Coastal base flood elevations apply only landward of the shoreline.

Corporate limits shown are current as of the date of this map. The user should contact appropriate community officials to determine if corporate limits have changed subsequent to the issuance of the map.

For community map revision history prior to countywide mapping, see Section 6.0 of the Flood Insurance Study Report.

For adjoining map panels see separately printed Map Index.

MAP REPOSITORY

Refer to Repository Listing on Index Map

EFFECTIVE DATE OF COUNTYWIDE FLOOD INSURANCE RATE MAP

APRIL 15, 1988

EFFECTIVE DATE (S) OF REVISION (S) TO THIS PANEL

Map revised SEPTEMBER 29, 1989 to change base flood elevations and special flood hazard areas, to add base flood elevations and special flood hazard areas, to change zone designations, to reflect updated topographic information, to incorporate previously issued letters of map revision and map amendment, and to update map format.

To determine if flood insurance is available, contact an insurance agent or call the National Flood Insurance Program at (800) 638-6620.

N

APPROXIMATE SCALE IN FEET

1000 0 1000

NATIONAL FLOOD INSURANCE PROGRAM

# FIRM
## FLOOD INSURANCE RATE MAP

MARICOPA COUNTY, ARIZONA AND INCORPORATED AREAS

PANEL 235 OF 4350

CONTAINS

| COMMUNITY | NUMBER | PANEL | SUFFIX |
|---|---|---|---|
| MARICOPA COUNTY, UNINCORPORATED AREAS | 040037 | 0235 | E |
| WICKENBURG, TOWN OF | 040056 | 0235 | E |

MAP NUMBER
04013C0235 E

MAP REVISED:
SEPTEMBER 29, 1989

Federal Emergency Management Agency

NOTE: MAP AREA SHOWN ON THIS PANEL IS LOCATED WITHIN TOWNSHIP 7 NORTH, RANGE 5 WEST AND TOWNSHIP 8 NORTH, RANGE 5 WEST