

**ELLIOT ROAD DETENTION BASINS
AND OUTFALL CHANNEL**

Contract FCD 98-44

**Preliminary Floodplain Delineation
West of Ellsworth Road**

draft

Prepared for : **Flood Control District of Maricopa County**
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Exhibit 1 Existing and Interim Condition Preliminary Floodplain Delineation

1.0 INTRODUCTION

Wood/Patel learned during the design evaluation process that the post basin/pipe flows would be concentrated along the selected alignment as shown in the East Mesa Area Drainage Master Plan, FCD #95-32, July 1998, by Dibble and Associates, in a way that might be construed as adversely impacting properties downstream of the outfall. In an attempt to mitigate this potential problem, several elements have been added to the plans. These elements include the postponing of the Crismon Road channel construction to reduce the interim flow at Elliot Road and Ellsworth Road and the addition of a distributary channel west of Ellsworth Road to direct the flows to their historical pathways. In this report, the ADMP selected outfall alignment is identified as the south branch of the historical drainage path and the splitter channel is identified as the north branch of the historical drainage path for the distributary outfall channel system.

This report is prepared as part of the Elliot Basin Outfall Channel Design project to show the impact of the interim conditions on the downstream areas of the outfall channel.

2.0 HYDROLOGY

The hydrologic model of the East Mesa ADMP for the existing conditions provided by FCDMC was used to generate the 100-year peak flow at the southeast corner of Ellsworth Road and Elliot Road. The hydrologic model names used for this analysis are SEMP100S.DAT and SEMP100N.DAT for the portions of the model south and north of the Superstition Freeway, respectively. The models were then modified to simulate the interim conditions.

Three different runoff events (2-yr, 5-yr and 100-yr) were evaluated to determine "interim" flows for the project. Please refer to Exhibits 1, 2 and 3 that depict sub-area boundaries and peak flows at key locations. The following modifications were incorporated into the interim model:

1. This project's proposed drainage facilities were accounted for in the model.
2. The existing condition model was modified to incorporate improvements made within the watershed for the Santa Rita Ranch Development. These include 100-year, 2-hr onsite detention and a collector channel along the south side of Guadalupe Road that intercepts offsite flows from the north (sub-basins 66b and 67c) and outfalls to the west along the SRP corridor 2 miles north of Elliot Road.
3. Only a portion of sub-basins 65a and 65b drain into the east detention basin. Therefore, these sub-basins were divided into two portions (65a1, 65a2 and 65b1, 65b2 respectively). No new sub-basins were created. These new flow distributions were modeled using diversions based on the percentage of each basin area split.
4. At Basin EA, the initial 30 cfs is diverted south into the Elliot Road channel. The remainder of the flow is diverted into the Basin with a maximum storage volume of 32 acre-feet.
5. There are two locations that impact this site where flows from the north side of the CAP canal are hard coded into the HEC-1 model. These flows are based on peak outflow from the CAP overchutes for the existing condition 100-year model. Sub-basin 58 is the contributing area for flows at these locations. In order to determine

flows from the CAP overchutes for different return events, the runoff from this area was calculated based on the precipitation values for these events. For simplicity, a ratio was calculated for the return event runoff (in inches) to the 100-year runoff (in inches). This ratio was then used to calculate the peak flow from the CAP overchutes for different return events.

Conclusion - Hydrology

Based on this analysis, the following hydrologic conclusions can be made:

1. The 100-year flow at Ellsworth Road and Elliot Road is reduced from 2268 cfs in the existing condition model to 2035 cfs in the interim model (see Exhibit 3).
2. The proposed east detention basin (EA) is ineffective in the interim model for events in excess of the 2-year storm. This is mainly due to the fact that the upstream ADMP drainage facilities (Siphon Draw basin and channels) are not in place and the watershed is essentially undeveloped. In this condition, the basin volume (32 acre-feet) is quickly exceeded.
3. The splitter structure at the west basin (WA) is designed to allow a large portion of the initial flow (up to 400cfs) to bypass the basin. In order to reduce the impact of this bypass flow on the interim outfall, the Crismon Road channel will not be constructed with this project. This will allow the flows that outlet from the Santa Rita Ranch and Mesquite Canyon channel to continue to the west toward Ellsworth Road north of Elliot Road in their historical path.
4. Essentially all of the reduction in flow in the interim model for events in excess of the 2-year storm is attributable to the phasing of the Crismon Road channel to postpone the connection with the Santa Rita Ranch and Mesquite Canyon channel until an outfall is available west of Ellsworth Road.

Summary of Flows

Outfall Location West of Ellsworth Road

| Return Event | Existing Condition (cfs) | Interim Condition (cfs) |
|--------------|-----------------------------|----------------------------|
| 2-year | 83 | 69 |
| 5-year | 560 | 550 |
| 100-year | 2268 | 2035 |

draft

3.0 HYDRAULICS

The U.S. Army Corps of Engineer's HEC-RAS model, version 2.2, was used to generate the water surface profiles for the outfall areas. The starting water surface elevations were determined using slope-area method. Please note that these floodplain delineations are preliminary and not the final detailed results.

Topographic mapping for the study areas was the 2-foot contour map provided by the FCDMC.

Local deep depression areas were simulated by placing blocked obstructions within the cross sections to define ineffective flow regions in backwater or ponded areas with the cross section where appropriate. This prevents the HEC-RAS model from putting flow conveyance in areas of low ground near the ends of sections that are outside of the main wash flow path.

The study areas consists of three reaches: the east side along Ellsworth Road alignment south of Elliot Road (approximately 2,000 lf), the north branch of the distributary outfall channel (approximately 3,600 lf), and the south branch of the distributary outfall channel (approximately 3,200 lf).

The total 100-year inflow for the existing conditions at southeast corner of Elliot Road and Ellsworth Road is 2,268 cfs. The modeling purpose of the first reach (east side along Ellsworth Road alignment) is to determine the flow splits between north branch and south branch of the washes west of Ellsworth Road. Ellsworth Road was modeled as a broad-crested weir to account for split flows at depressions along the road. The peak flow values for each of the cross-sections of the HEC-RAS model were determined by trial-and-error method, i.e., first, a series of initial peak flows for all cross-sections were assumed, and the HEC-RAS model was executed, then the computed surface water elevations were used to calculate split flows, and a new flow series were again assigned to cross-sections of the HEC-RAS model. These steps were repeated until the sum of computed split flow and the flow remained at the downstream cross section of the HEC-RAS model was close to flow at the upstream cross section. The final results show that 600 cfs initial flows continue into south branch and 1,668 cfs excess flows breakout into north branch. The split flows computation and HEC-RAS modeling results are shown in Appendix A.

For the interim conditions, all the pipe flow (800 cfs) will be discharged into the south branch, and the remainder of the interim surface flow (1,235 cfs) will overflow into the north branch. This condition can be maintained by putting a dike on the east side of Ellsworth Road before the culvert crossing at Ellsworth Road. The flow in the south branch will split at the north diversion channel so that 500cfs continues to the south and 300cfs flows to the north. The total interim flows at the downstream end of the diversion channels will be approximately 500cfs to the south and 1,535cfs to the north. These flows are less than the existing condition flows of 600cfs to the north and 1,668cfs to the south.

The modeling results for the existing conditions of both north branch and south branch are included in Appendix B, and those for the interim conditions in Appendix C. The preliminary floodplain delineations for the existing and interim conditions are shown on Exhibit 4.

Conclusion - Hydraulics

Based on this analysis, the following hydraulic conclusions can be made:

1. The floodplain for the interim condition has been slightly reduced from the existing condition for both the north and south branches.

draft

Appendix A

Split Flow Computation Table

HEC-RAS Model Results for Existing Conditions

East of Ellsworth Road

Table 1a

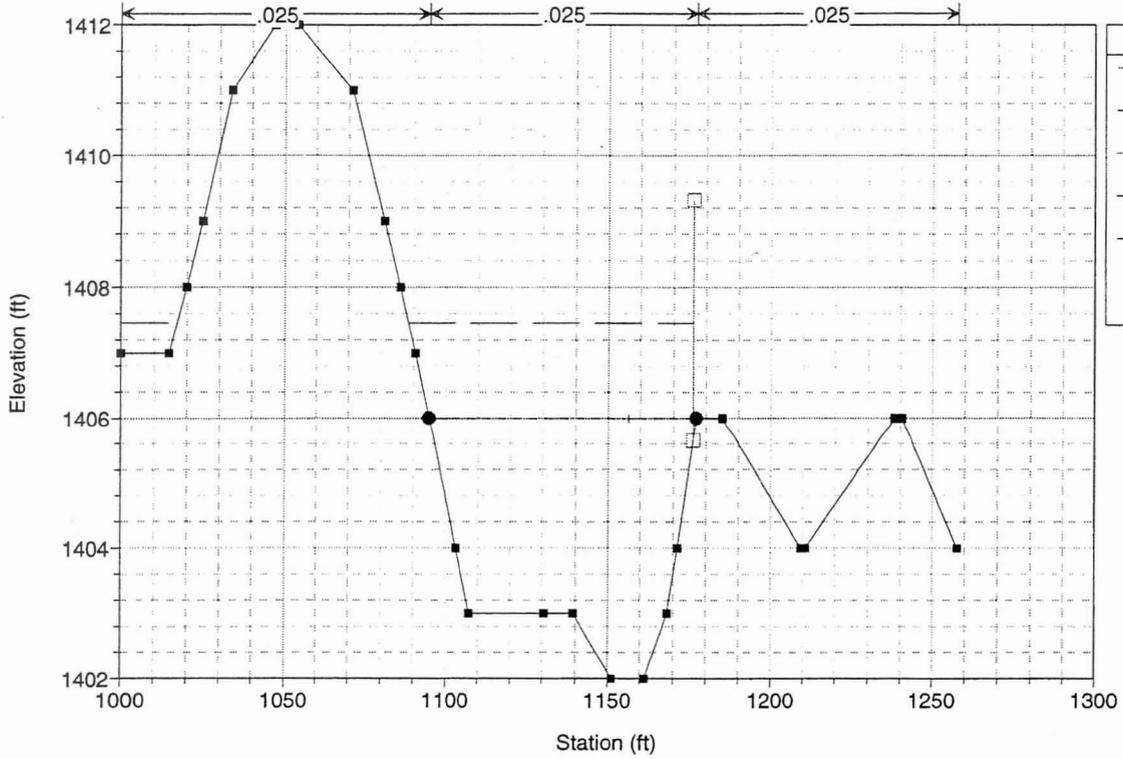
Split Flow Computation along Ellsworth Road (Existing Condition)

| Station | Distance | Bank Elev. | WSEL | Head H | Coef. C | Length L | Weir Qi | Weir Q | Remaining Q | Q in Hec-Ras |
|---------|----------|------------|---------|--------|---------|----------|----------|--------|-------------|--------------|
| | (ft) | (ft) | (ft) | (ft) | | (ft) | (cfs/ft) | (cfs) | (cfs) | (cfs) |
| 1100 | 1545.000 | 1406.00 | 1406.00 | 0.00 | 2.90 | 0 | 0.0 | | 2268 | 2268 |
| 1000 | 1239.000 | 1404.00 | 1405.00 | 1.00 | 2.90 | 306 | 2.9 | 444 | 1824 | 1850 |
| 900 | 1026.000 | 1404.00 | 1404.85 | 0.85 | 2.90 | 213 | 2.3 | 551 | 1273 | 1300 |
| 800 | 857.000 | 1404.00 | 1404.80 | 0.80 | 2.90 | 169 | 2.1 | 367 | 906 | 900 |
| 700 | 693.000 | 1404.00 | 1404.55 | 0.55 | 2.90 | 164 | 1.2 | 267 | 639 | 700 |
| 600 | 554.000 | 1404.00 | 1403.90 | 0.00 | 2.90 | 118 | 0.0 | 70 | 569 | 600 |
| 500 | 469.000 | 1402.00 | 1402.45 | 0.45 | 2.90 | 70 | 0.9 | 30 | 539 | 500 |
| 400 | 332.000 | 1401.00 | 1401.35 | 0.35 | 2.90 | 137 | 0.6 | 101 | 438 | 400 |
| 300 | 210.000 | 1401.00 | 1401.30 | 0.30 | 2.90 | 122 | 0.5 | 66 | 372 | 350 |
| 200 | 115.000 | 1401.00 | 1400.80 | 0.00 | 2.90 | 57 | 0.0 | 14 | 359 | 300 |
| 100 | 0.000 | 1399.00 | 1399.60 | 0.60 | 2.90 | 86 | 1.3 | 58 | 300 | 300 |

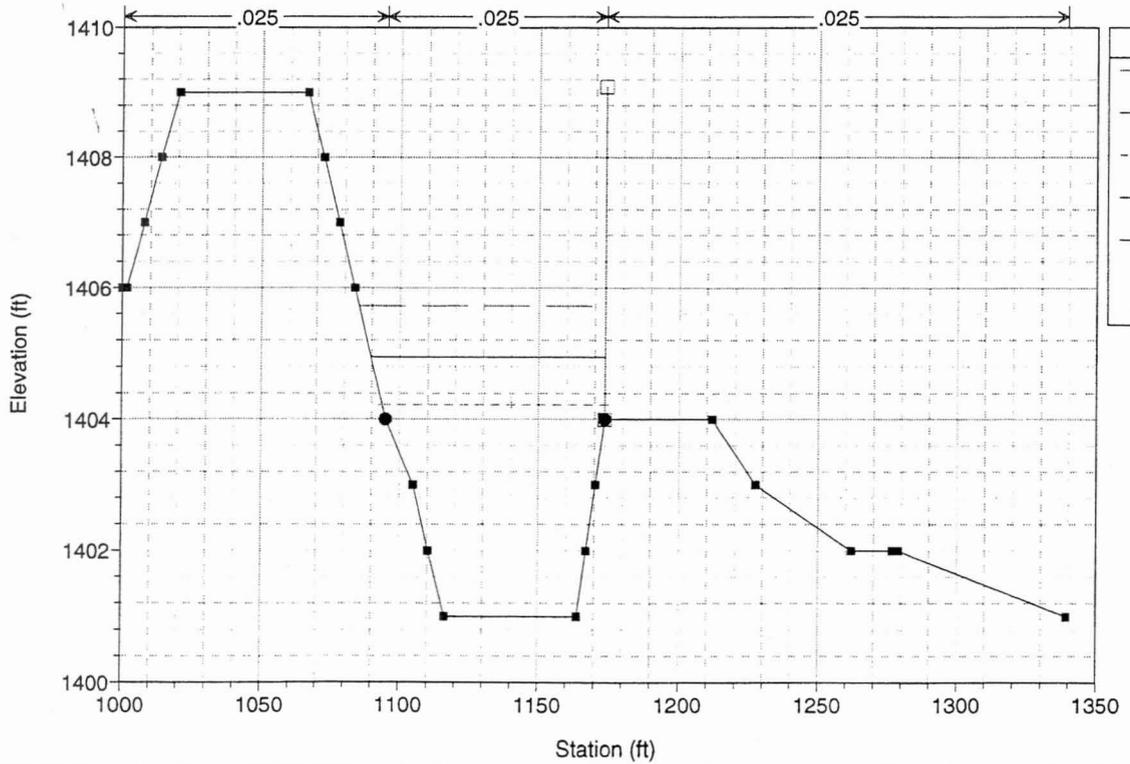
HEC-RAS Plan: Existing River: E-Ellsworth Rd Reach: S.Elliot

| Reach | River Sta | Q Total (cfs) | Min Ch El (ft) | W/S Elev (ft) | Crit W/S (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl |
|----------|-----------|------------------|-------------------|------------------|------------------|-------------------|-----------------------|--------------------|----------------------|-------------------|--------------|
| S.Elliot | 1100 | 2268.00 | 1402.00 | 1406.00 | 1406.00 | 1407.46 | 0.006619 | 9.69 | 234.13 | 81.33 | 1.01 |
| S.Elliot | 1000 | 1850.00 | 1401.00 | 1404.94 | 1404.22 | 1405.73 | 0.002989 | 7.11 | 262.11 | 83.98 | 0.69 |
| S.Elliot | 900 | 1300.00 | 1401.00 | 1404.76 | 1403.47 | 1405.14 | 0.001474 | 4.94 | 265.73 | 89.03 | 0.49 |
| S.Elliot | 800 | 900.00 | 1401.00 | 1404.69 | 1403.01 | 1404.90 | 0.000822 | 3.64 | 248.93 | 83.58 | 0.36 |
| S.Elliot | 700 | 700.00 | 1401.00 | 1404.60 | 1402.85 | 1404.76 | 0.000692 | 3.25 | 216.24 | 74.86 | 0.33 |
| S.Elliot | 600 | 600.00 | 1402.00 | 1403.83 | 1403.83 | 1404.50 | 0.008101 | 6.56 | 91.49 | 67.15 | 0.99 |
| S.Elliot | 500 | 500.00 | 1401.00 | 1402.28 | 1402.61 | 1403.46 | 0.019228 | 8.74 | 57.82 | 56.42 | 1.47 |
| S.Elliot | 400 | 400.00 | 1396.00 | 1401.30 | 1397.90 | 1401.35 | 0.000159 | 1.78 | 225.73 | 65.94 | 0.16 |
| S.Elliot | 300 | 350.00 | 1397.00 | 1401.29 | 1398.79 | 1401.33 | 0.000137 | 1.69 | 270.21 | 133.47 | 0.15 |
| S.Elliot | 200 | 300.00 | 1399.00 | 1400.58 | 1400.58 | 1401.23 | 0.008624 | 6.47 | 46.35 | 36.13 | 1.01 |
| S.Elliot | 100 | 300.00 | 1397.00 | 1399.54 | 1399.09 | 1399.95 | 0.003001 | 5.17 | 60.96 | 37.26 | 0.64 |

Ellsworth Road Wash Existing Scenario 8/30/99
 Geom: Existing Conditions Geometry
 RS = 1100



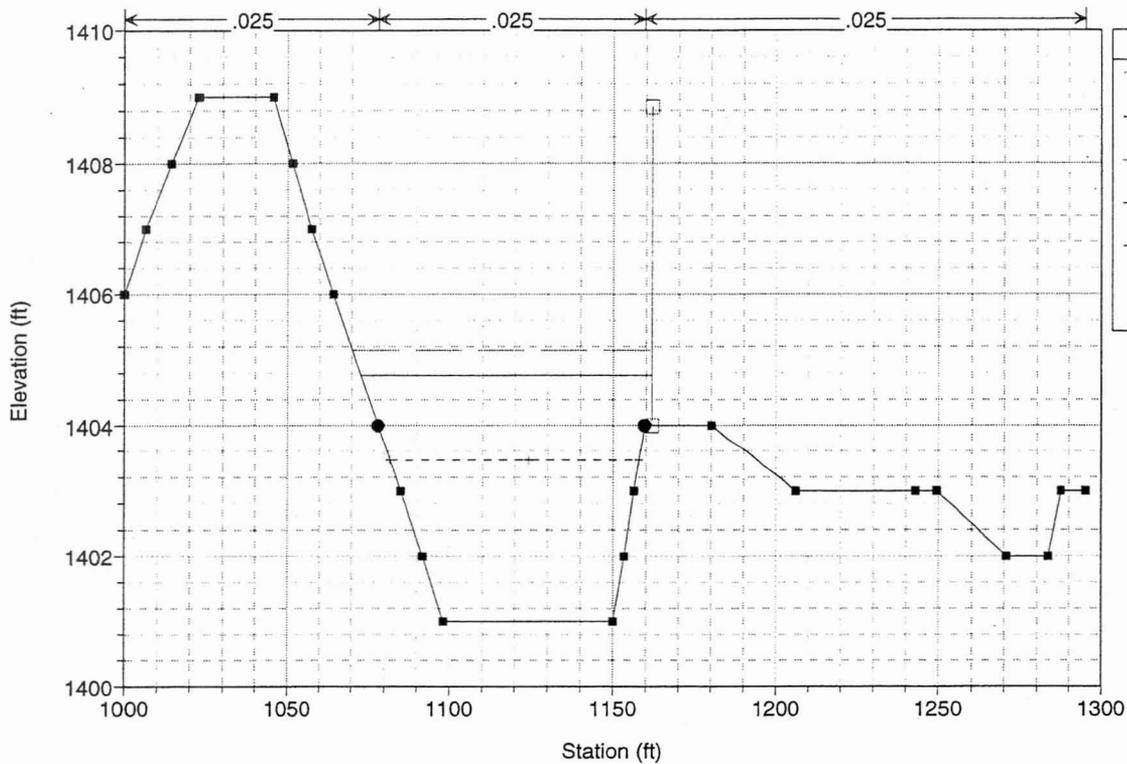
Ellsworth Road Wash Existing Scenario 8/30/99
 Geom: Existing Conditions Geometry
 RS = 1000



Ellsworth Road Wash Existing Scenario 8/30/99

Geom: Existing Conditions Geometry

RS = 900

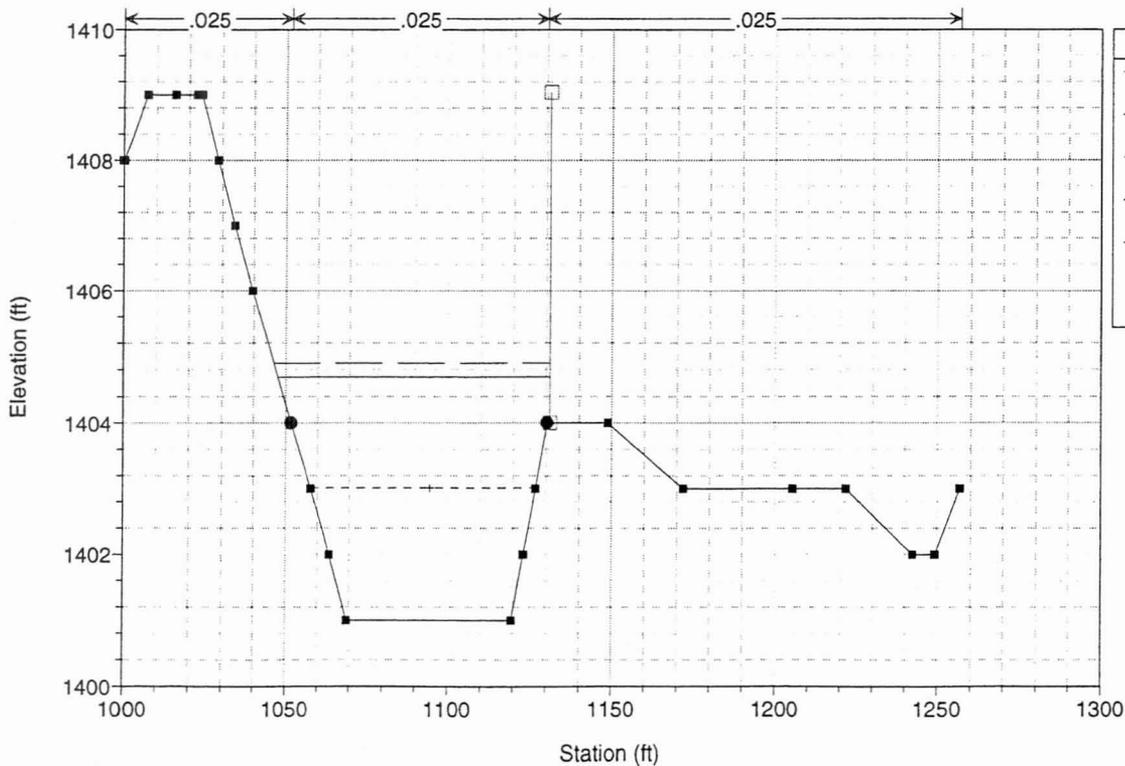


| Legend | |
|-----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Crit PF 1 | — |
| Ground | ■ |
| Levee | □ |
| Bank Sta | ● |

Ellsworth Road Wash Existing Scenario 8/30/99

Geom: Existing Conditions Geometry

RS = 800

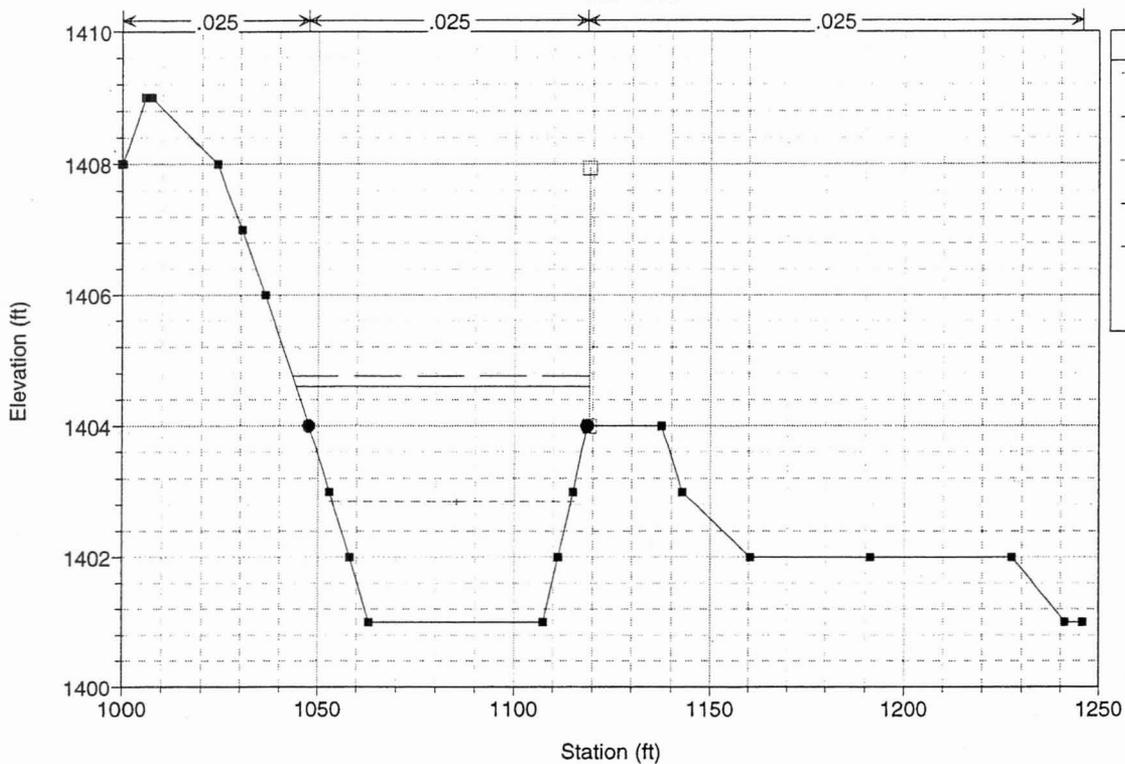


| Legend | |
|-----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Crit PF 1 | — |
| Ground | ■ |
| Levee | □ |
| Bank Sta | ● |

Ellsworth Road Wash Existing Scenario 8/30/99

Geom: Existing Conditions Geometry

RS = 700

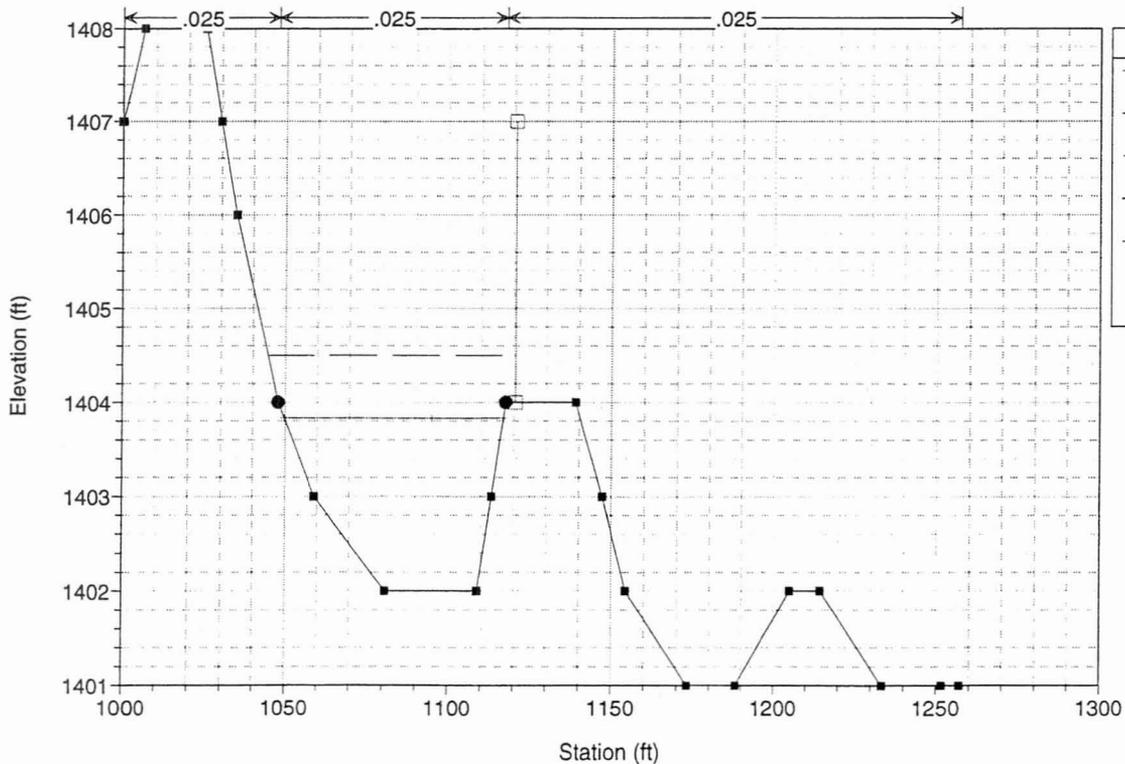


| Legend | |
|-----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Crit PF 1 | — |
| Ground | — |
| Levee | — |
| Bank Sta | ■ |

Ellsworth Road Wash Existing Scenario 8/30/99

Geom: Existing Conditions Geometry

RS = 600

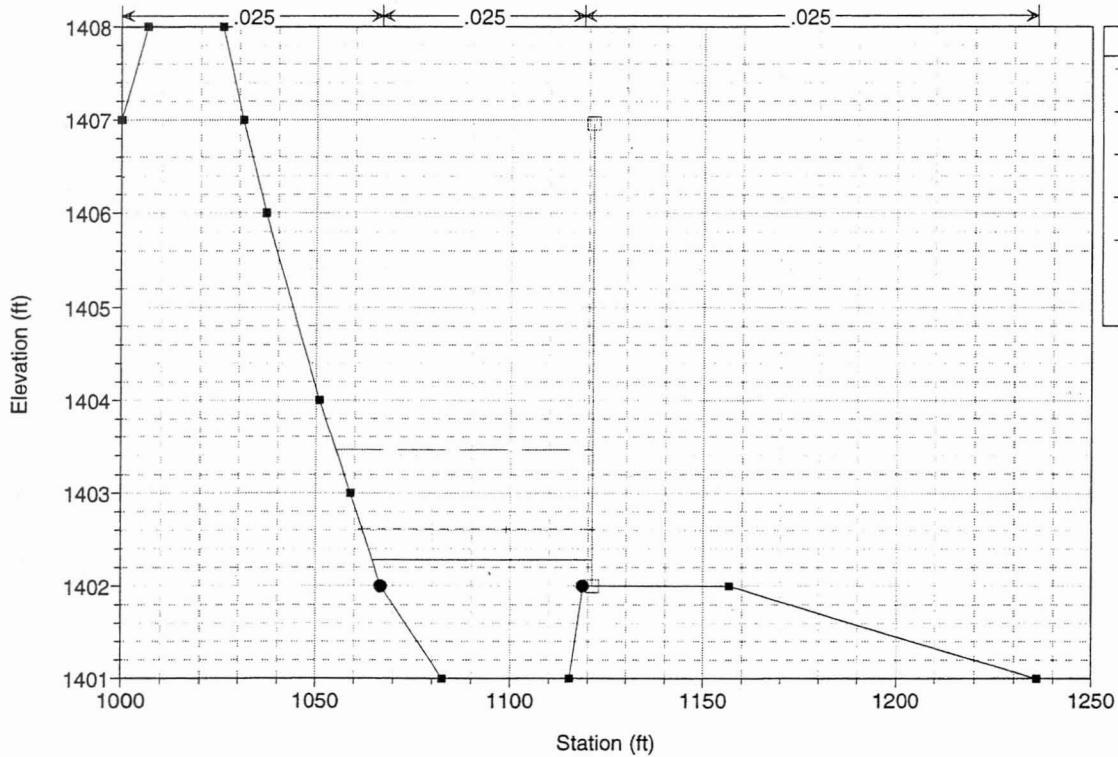


| Legend | |
|-----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Crit PF 1 | — |
| Ground | — |
| Levee | — |
| Bank Sta | ■ |

Ellsworth Road Wash Existing Scenario 8/30/99

Geom: Existing Conditions Geometry

RS = 500

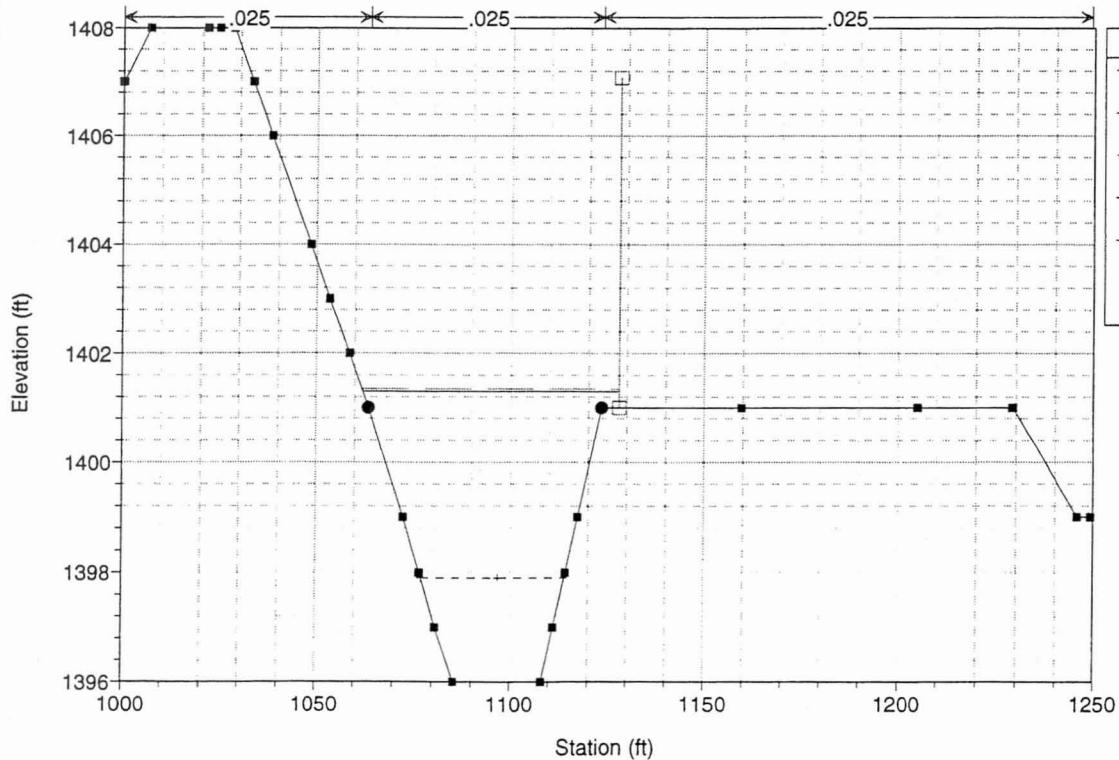


| Legend | |
|-----------|-------------|
| EG PF 1 | --- |
| Crit PF 1 | |
| WS PF 1 | - . - . - . |
| Ground | ■ |
| Levee | □ |
| Bank Sta | ● |

Ellsworth Road Wash Existing Scenario 8/30/99

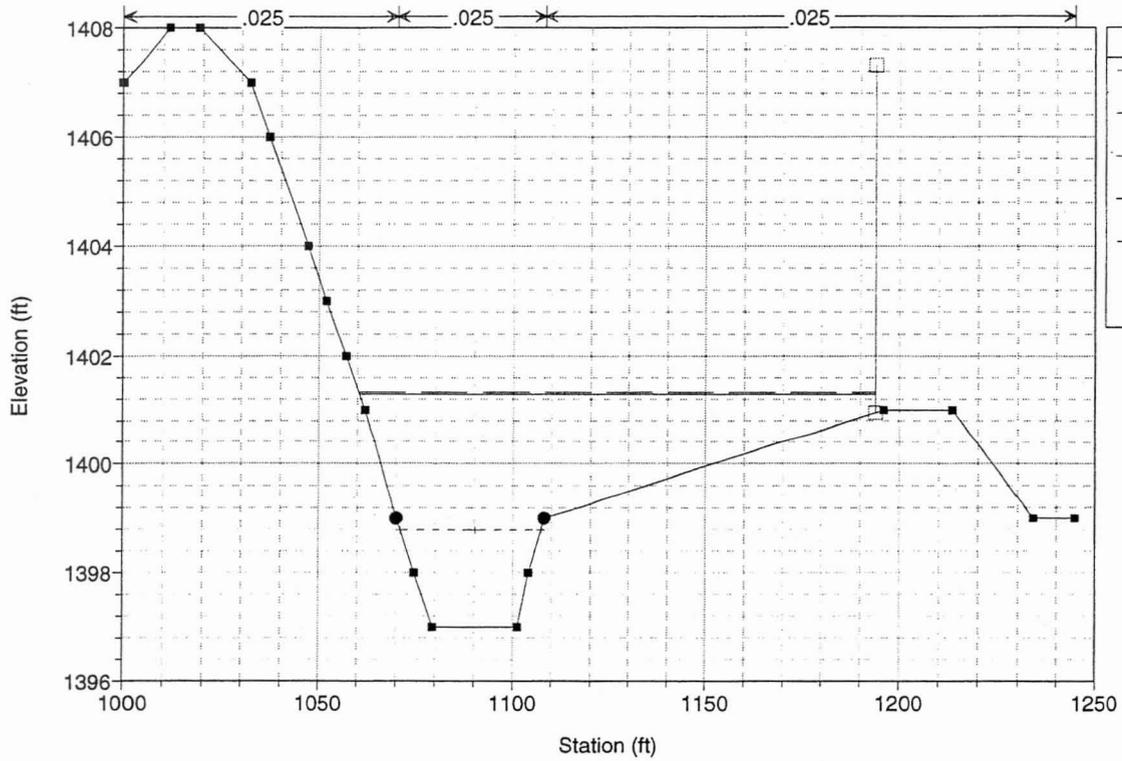
Geom: Existing Conditions Geometry

RS = 400



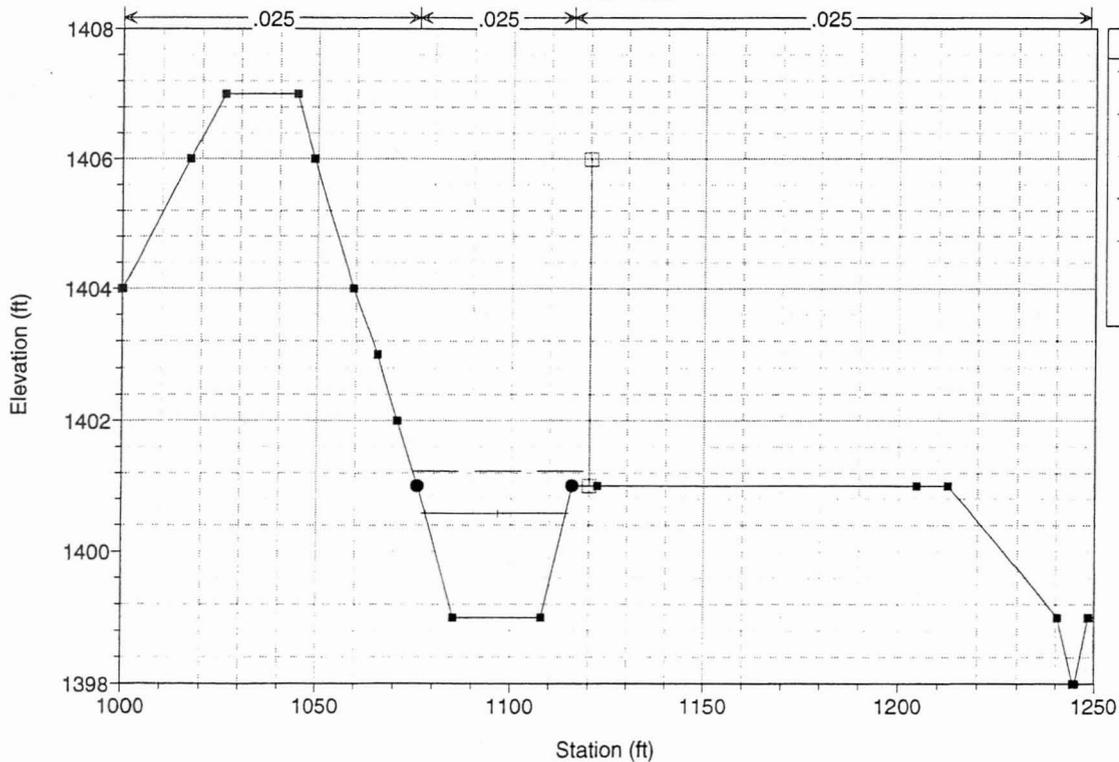
| Legend | |
|-----------|-------------|
| EG PF 1 | --- |
| WS PF 1 | - . - . - . |
| Crit PF 1 | |
| Ground | ■ |
| Levee | □ |
| Bank Sta | ● |

Ellsworth Road Wash Existing Scenario 8/30/99
 Geom: Existing Conditions Geometry
 RS = 300



| Legend | |
|-----------|-------------|
| EG PF 1 | — |
| WS PF 1 | - - - |
| Crit PF 1 | — |
| Ground | —■— |
| Levee | - - -□- - - |
| Bank Sta | —●— |

Ellsworth Road Wash Existing Scenario 8/30/99
 Geom: Existing Conditions Geometry
 RS = 200

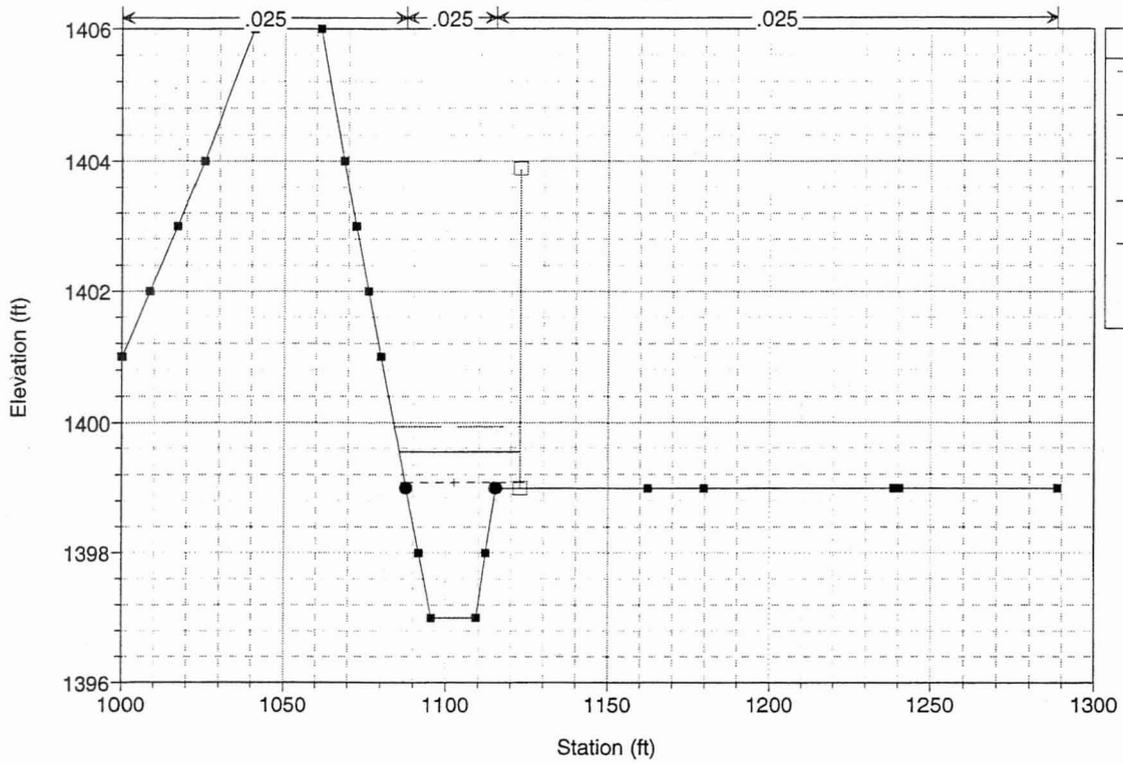


| Legend | |
|-----------|-------------|
| EG PF 1 | — |
| WS PF 1 | - - - |
| Crit PF 1 | — |
| Ground | —■— |
| Levee | - - -□- - - |
| Bank Sta | —●— |

Ellsworth Road Wash Existing Scenario 8/30/99

Geom: Existing Conditions Geometry

RS = 100



draft

Appendix B

HEC-RAS Model Results for Existing Conditions

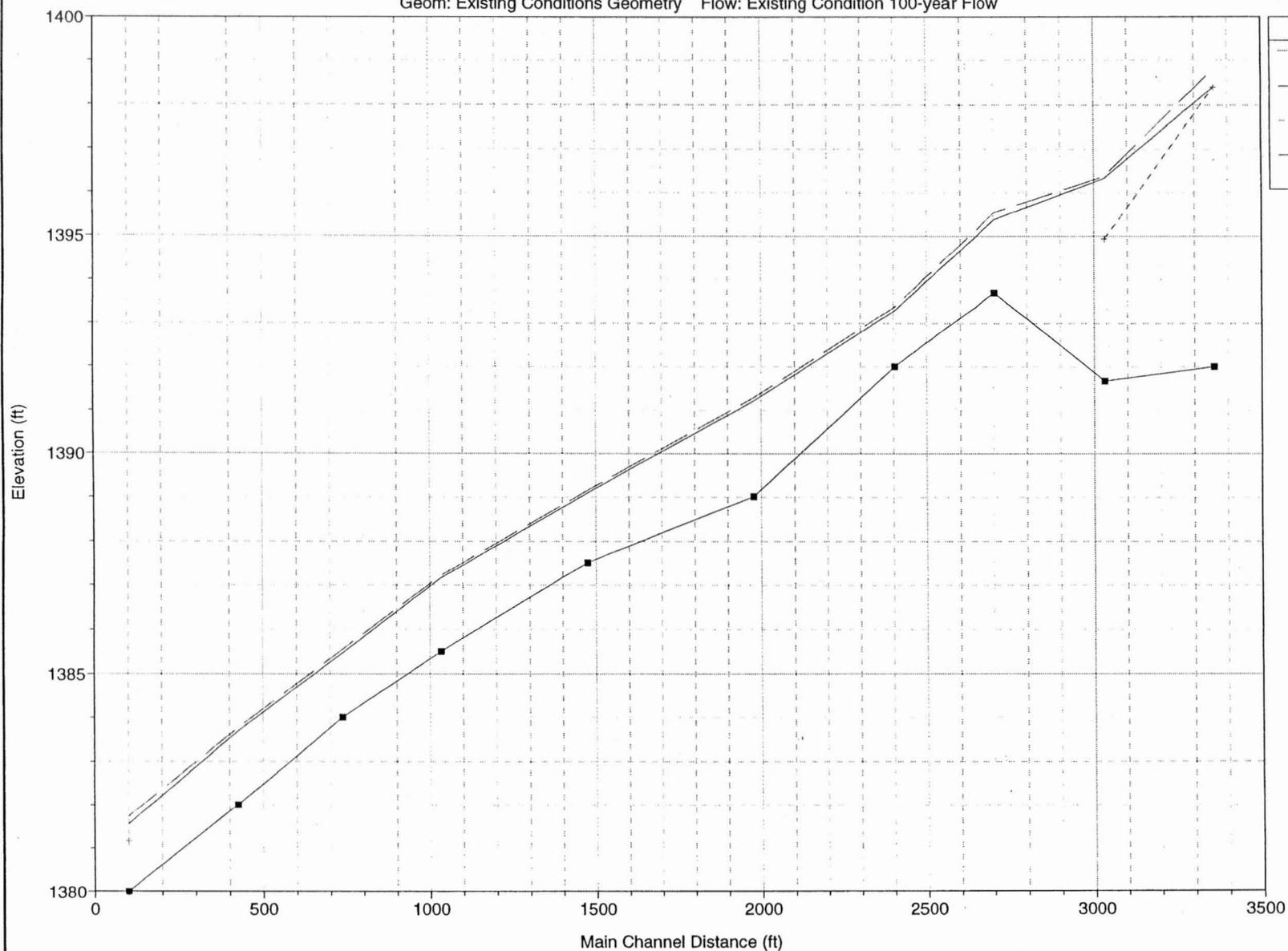
North Branch

South Branch

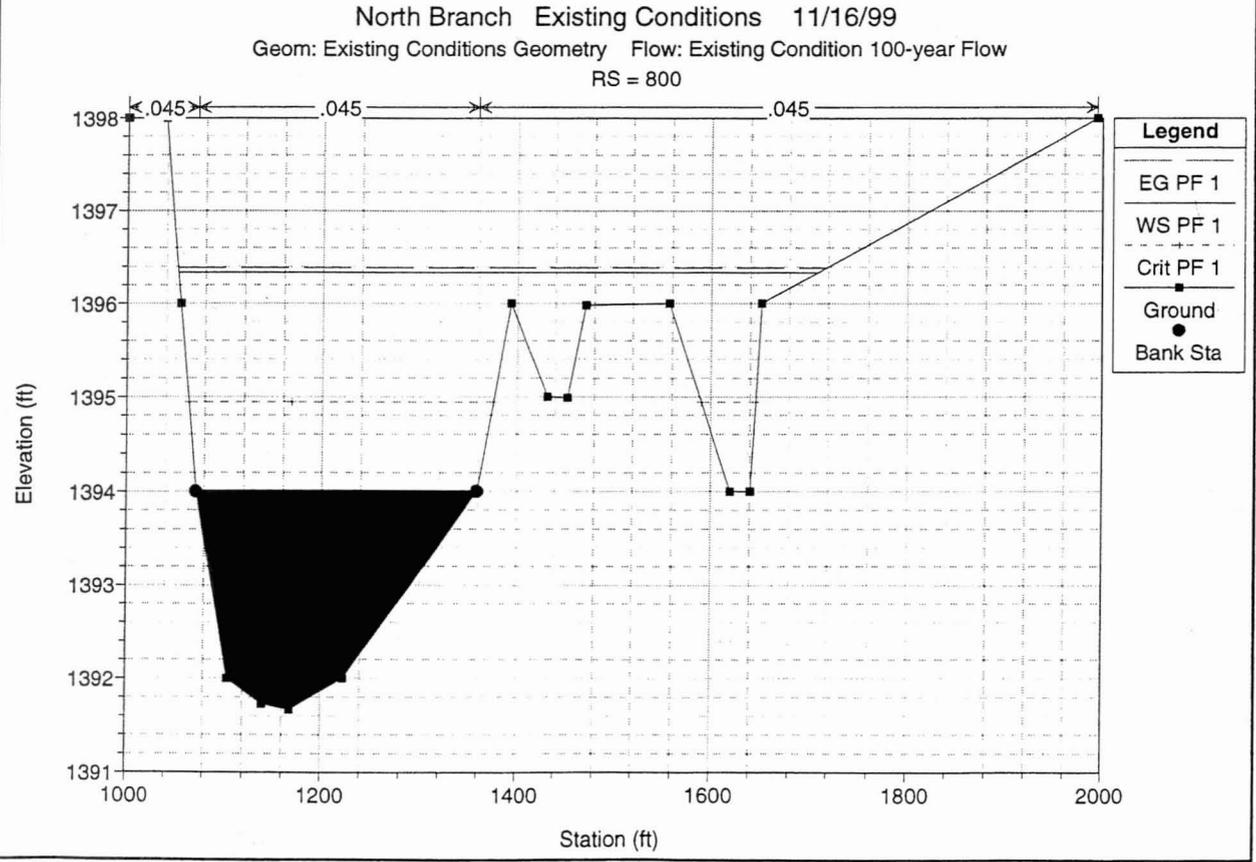
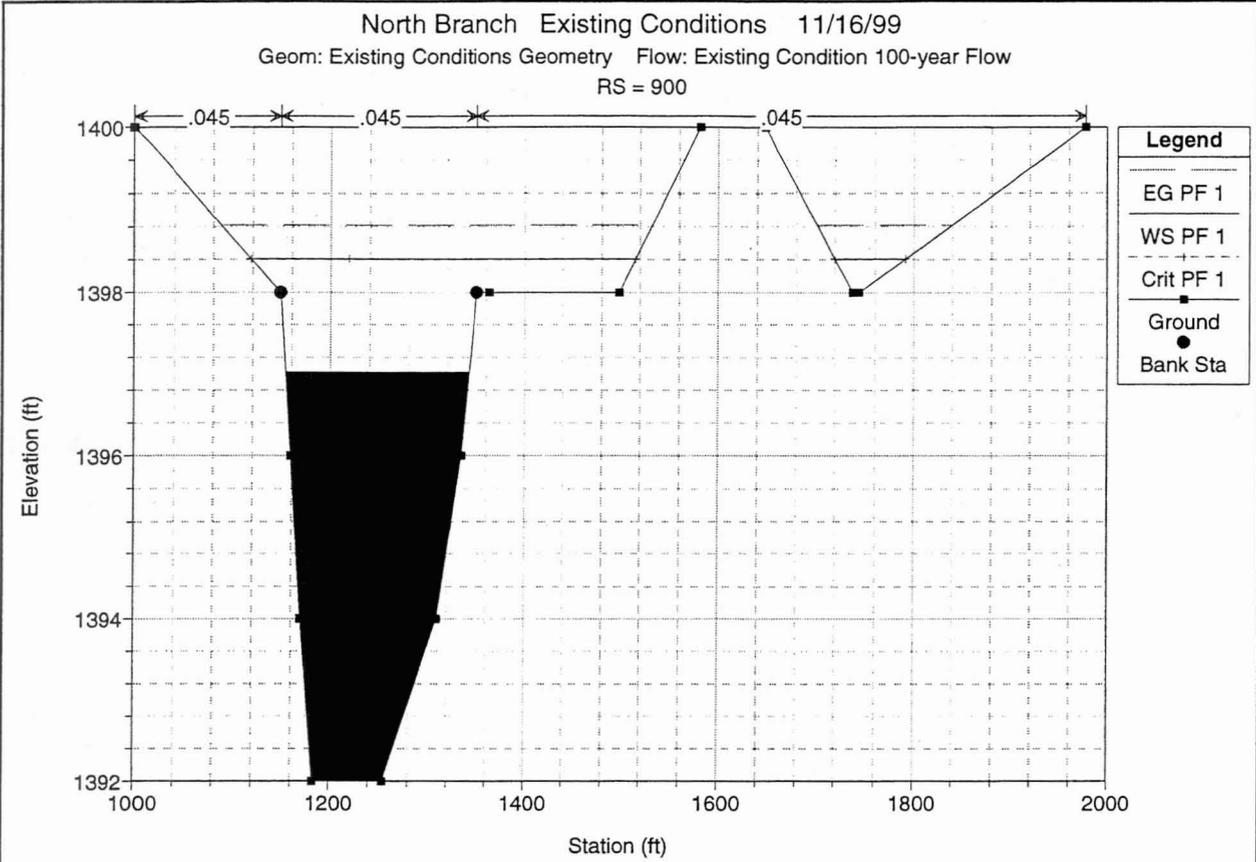
HEC-RAS Plan: Existing River: N-Branch Reach: W-Ellsworth

| Reach | River Sta | Q Total (cfs) | Min Chl El (ft) | W.S. Elev (ft) | Crit W.S (ft) | E.G. Elev. (ft) | E.G. Slope (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl |
|-------------|-----------|------------------|--------------------|-------------------|------------------|--------------------|-----------------------|--------------------|----------------------|-------------------|--------------|
| W-Ellsworth | 100 | 1668.00 | 1380.00 | 1381.56 | 1381.17 | 1381.73 | 0.008006 | 3.68 | 514.10 | 493.35 | 0.55 |
| W-Ellsworth | 200 | 1668.00 | 1382.00 | 1383.68 | | 1383.76 | 0.004788 | 2.21 | 761.72 | 812.79 | 0.40 |
| W-Ellsworth | 300 | 1668.00 | 1384.00 | 1385.47 | | 1385.55 | 0.006870 | 2.30 | 725.04 | 940.71 | 0.46 |
| W-Ellsworth | 400 | 1668.00 | 1385.51 | 1387.16 | | 1387.22 | 0.004671 | 1.97 | 848.76 | 1044.38 | 0.38 |
| W-Ellsworth | 450 | 1668.00 | 1387.51 | 1389.09 | | 1389.15 | 0.004170 | 1.96 | 848.88 | 959.56 | 0.37 |
| W-Ellsworth | 500 | 1668.00 | 1389.02 | 1391.21 | | 1391.28 | 0.004321 | 2.17 | 769.94 | 771.62 | 0.38 |
| W-Ellsworth | 600 | 1668.00 | 1392.00 | 1393.29 | | 1393.38 | 0.005815 | 2.41 | 691.43 | 737.30 | 0.44 |
| W-Ellsworth | 700 | 1668.00 | 1393.71 | 1395.39 | | 1395.55 | 0.009013 | 3.21 | 518.93 | 499.77 | 0.56 |
| W-Ellsworth | 800 | 1668.00 | 1393.89 | 1396.34 | 1394.94 | 1396.39 | 0.001164 | 1.98 | 999.00 | 656.75 | 0.23 |
| W-Ellsworth | 900 | 1668.00 | 1397.02 | 1398.41 | 1398.41 | 1398.82 | 0.017859 | 5.41 | 360.28 | 469.32 | 0.82 |

North Branch Existing Conditions 11/16/99
Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow

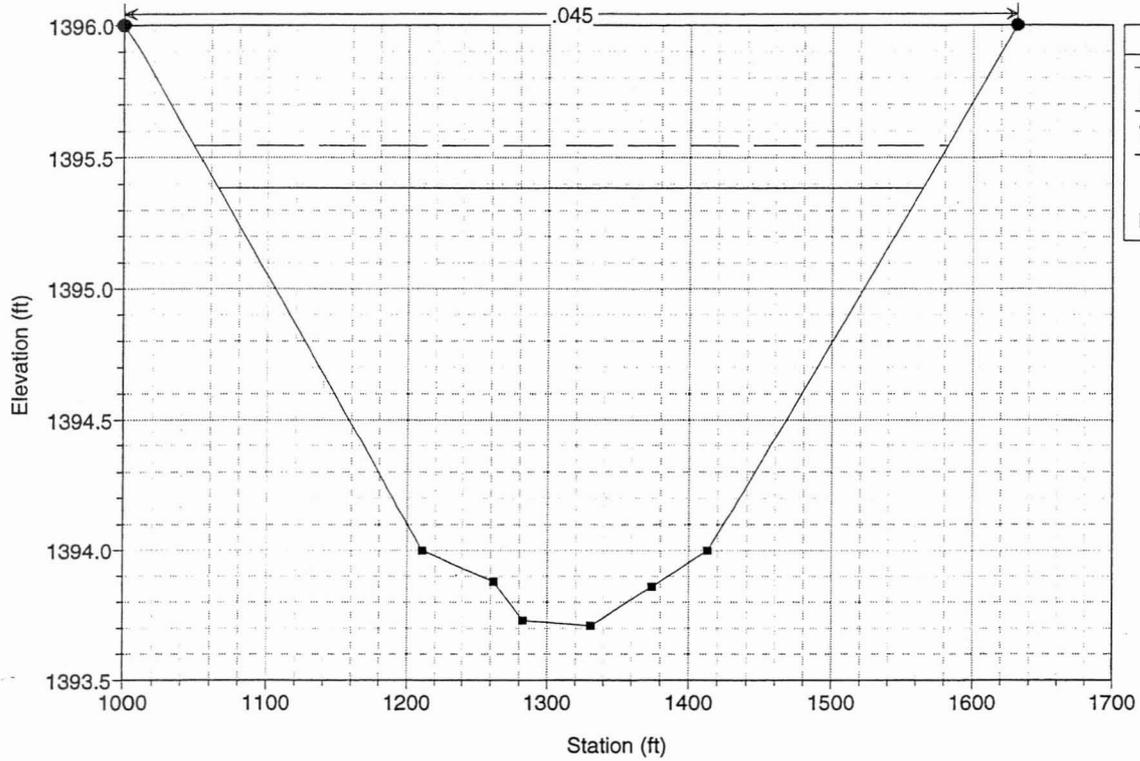


| Legend | |
|-----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Crit PF 1 | — |
| Ground | ■ |



North Branch Existing Conditions 11/16/99

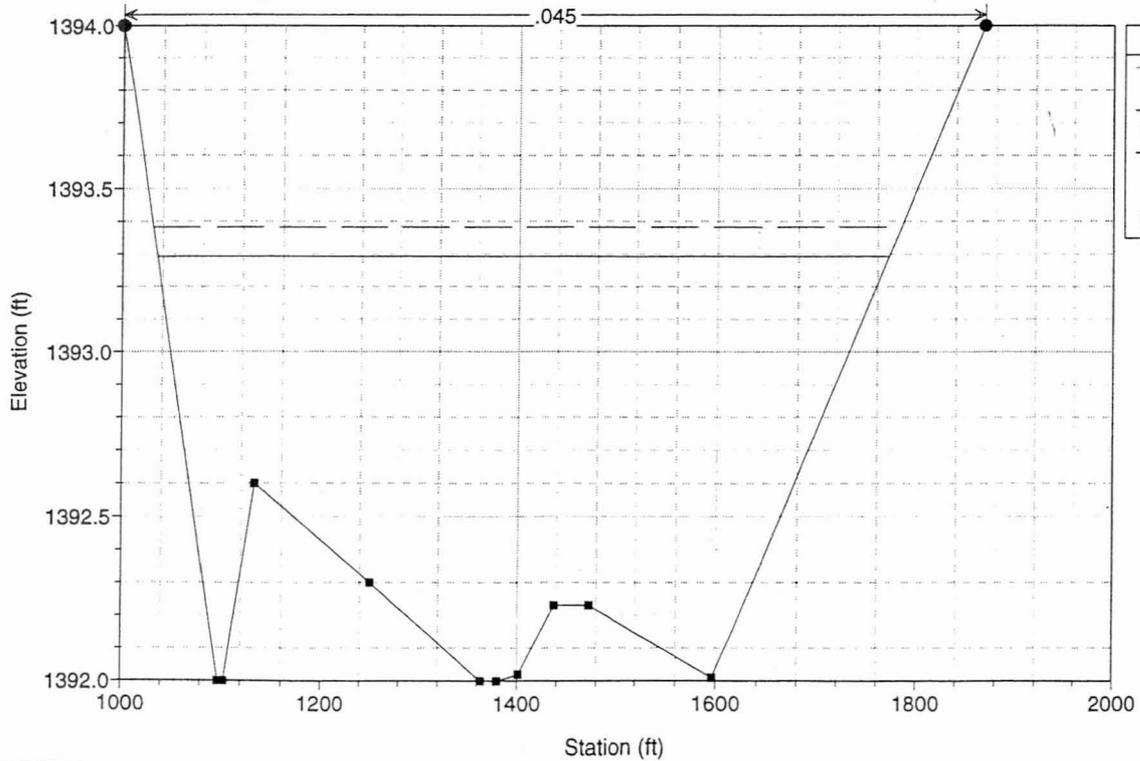
Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow
RS = 700



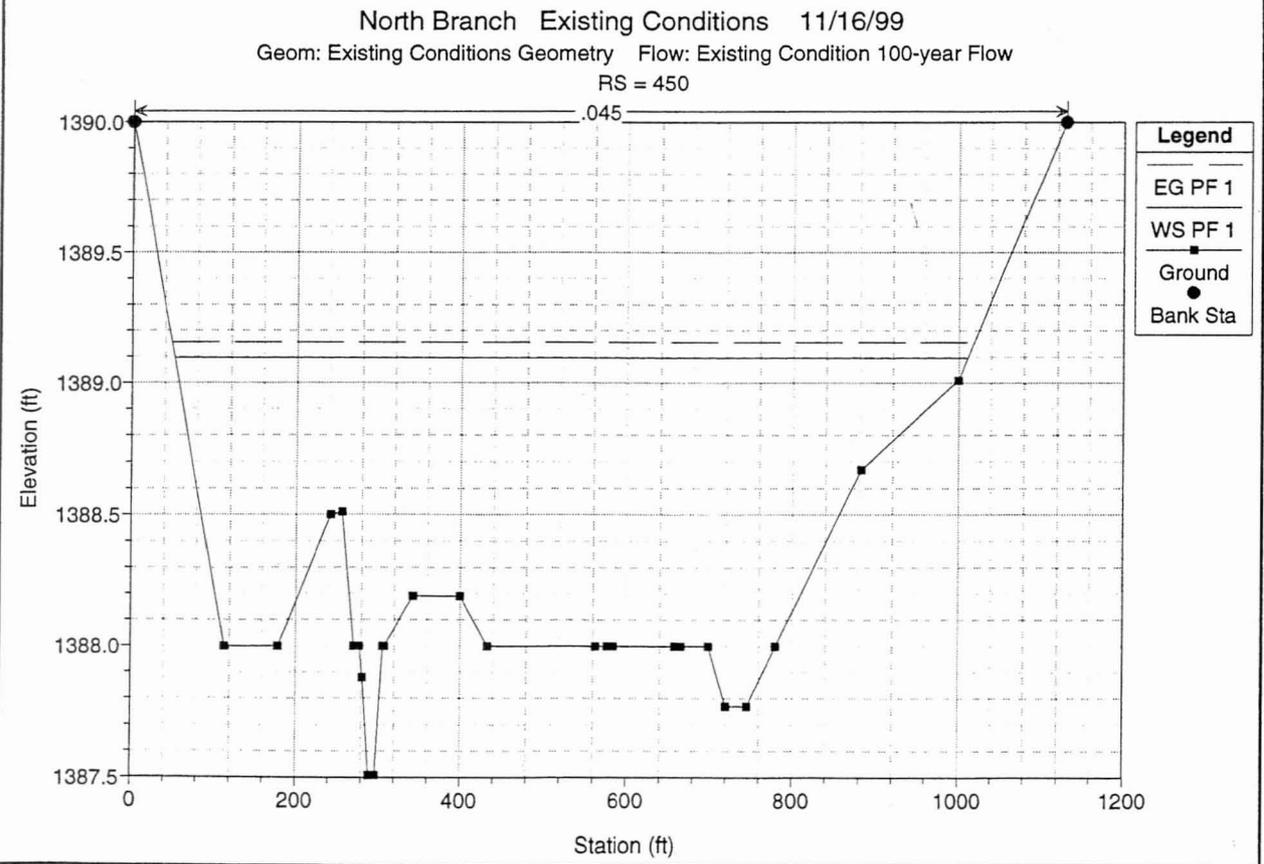
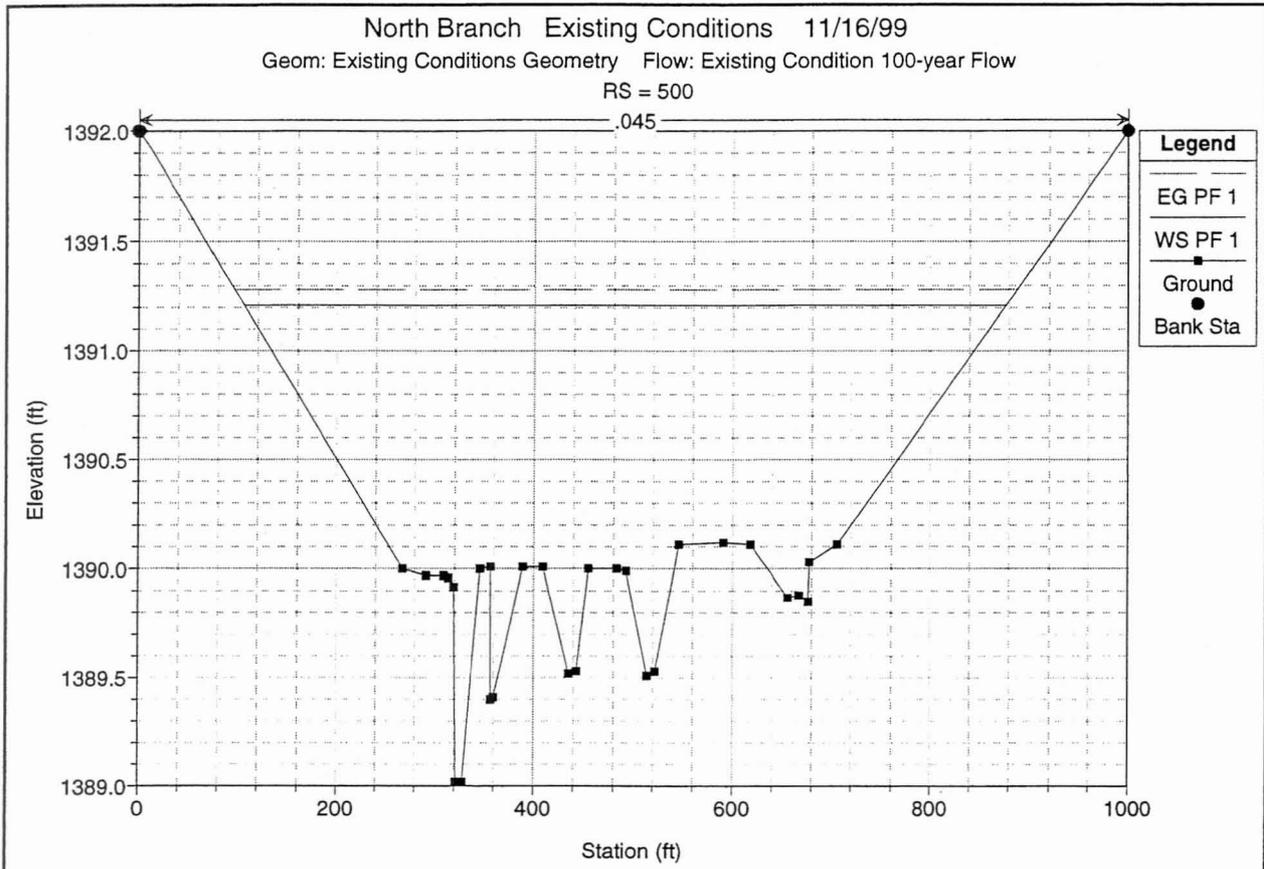
- Legend**
- EG PF 1
 - WS PF 1
 - Ground
 - Bank Sta

North Branch Existing Conditions 11/16/99

Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow
RS = 600

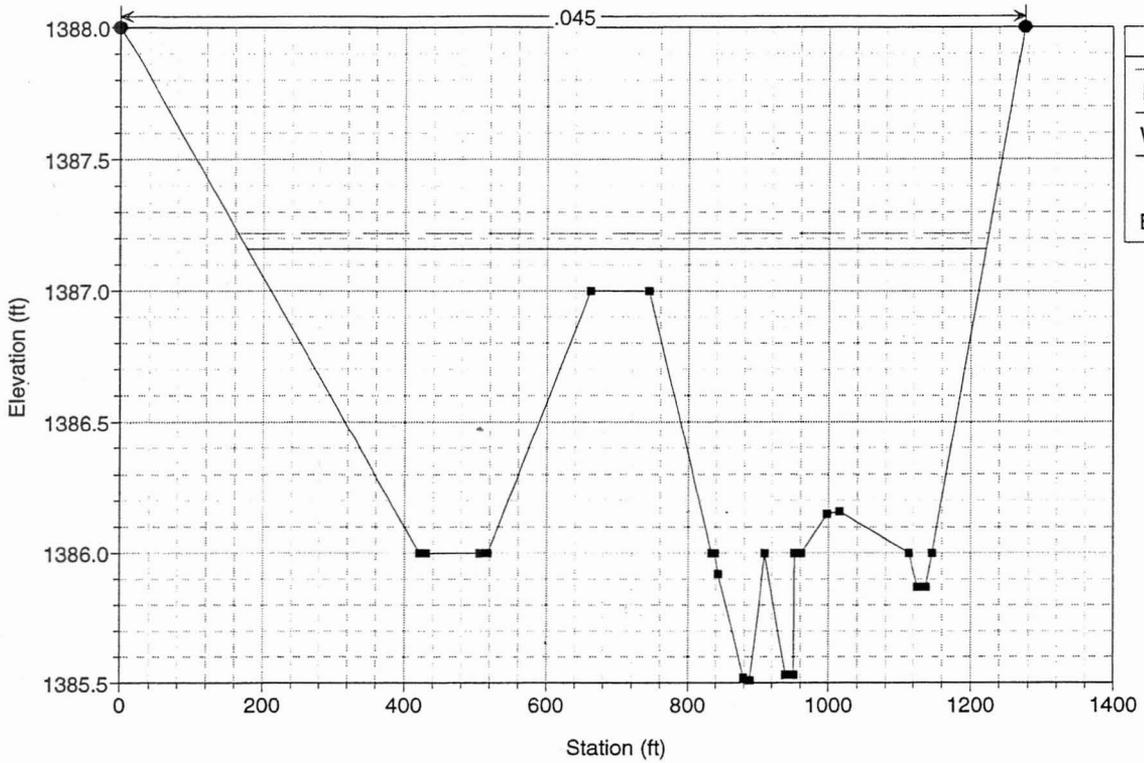


- Legend**
- EG PF 1
 - WS PF 1
 - Ground
 - Bank Sta



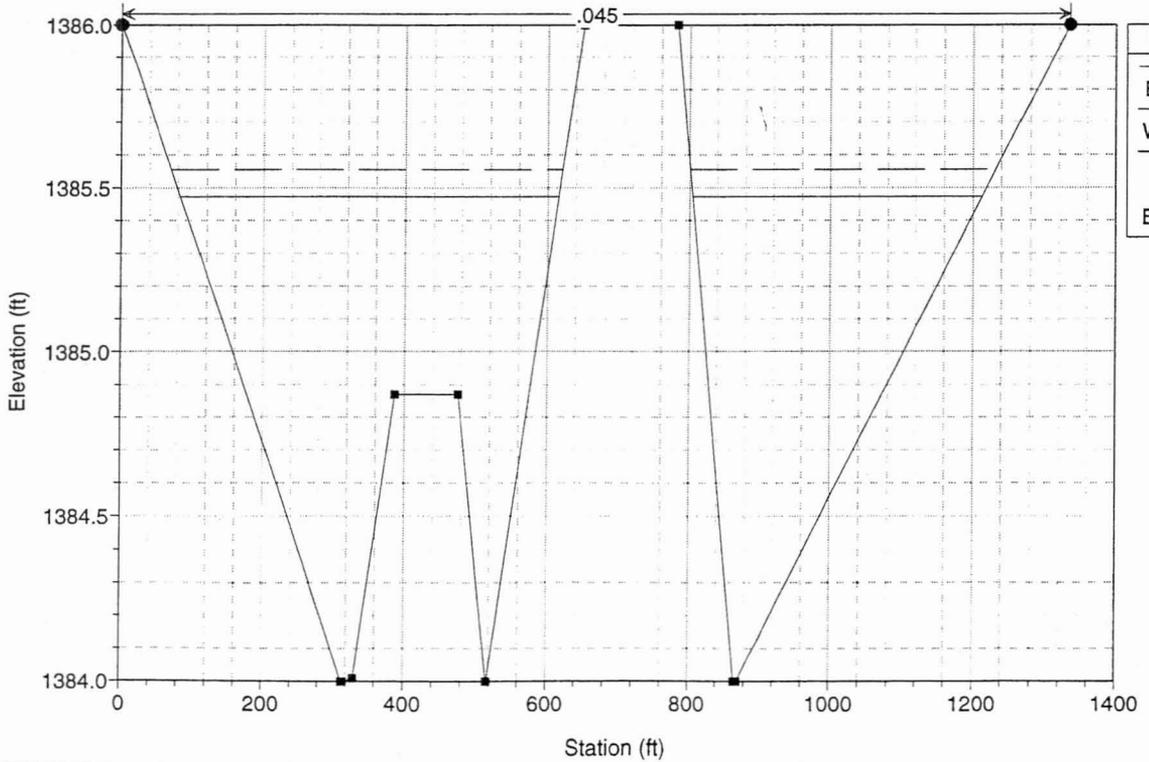
North Branch Existing Conditions 11/16/99

Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow
RS = 400



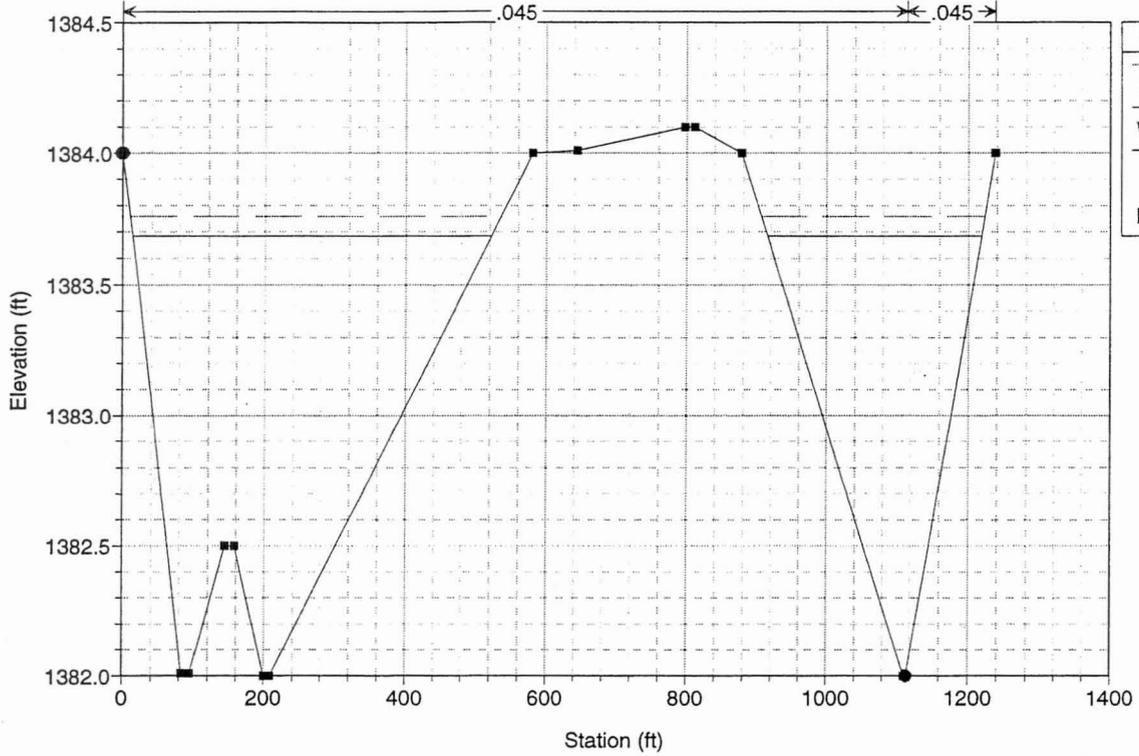
North Branch Existing Conditions 11/16/99

Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow
RS = 300



North Branch Existing Conditions 11/16/99

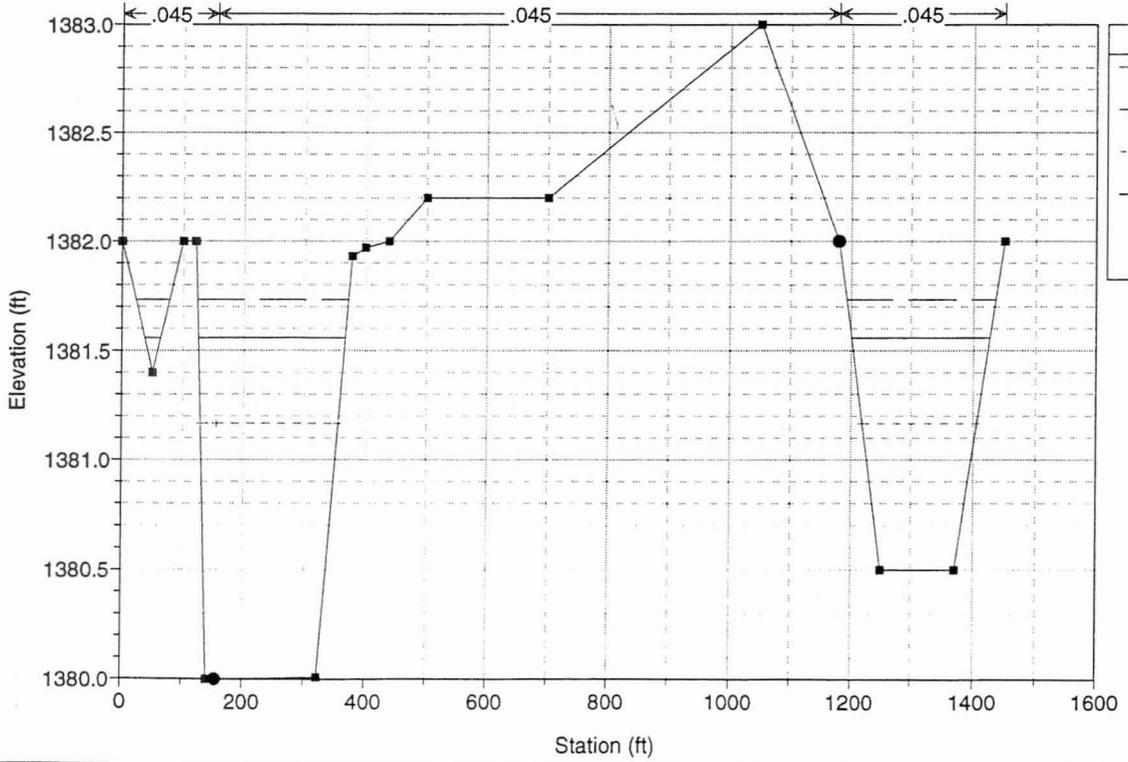
Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow
RS = 200



| Legend | |
|--------|----------|
| — | EG PF 1 |
| — | WS PF 1 |
| ■ | Ground |
| ● | Bank Sta |

North Branch Existing Conditions 11/16/99

Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow
RS = 100

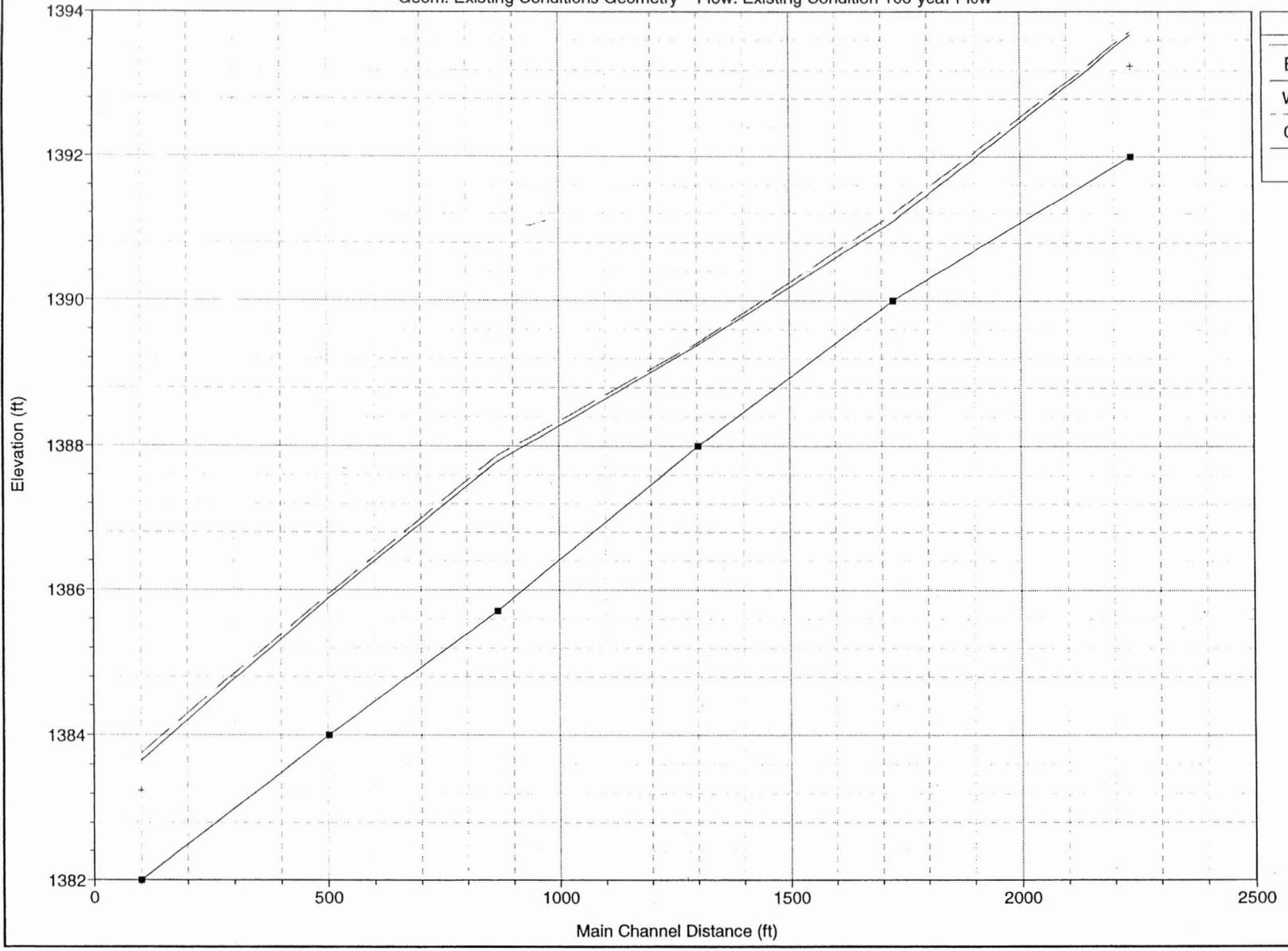


| Legend | |
|--------|-----------|
| — | EG PF 1 |
| — | WS PF 1 |
| — | Crit PF 1 |
| ■ | Ground |
| ● | Bank Sta |

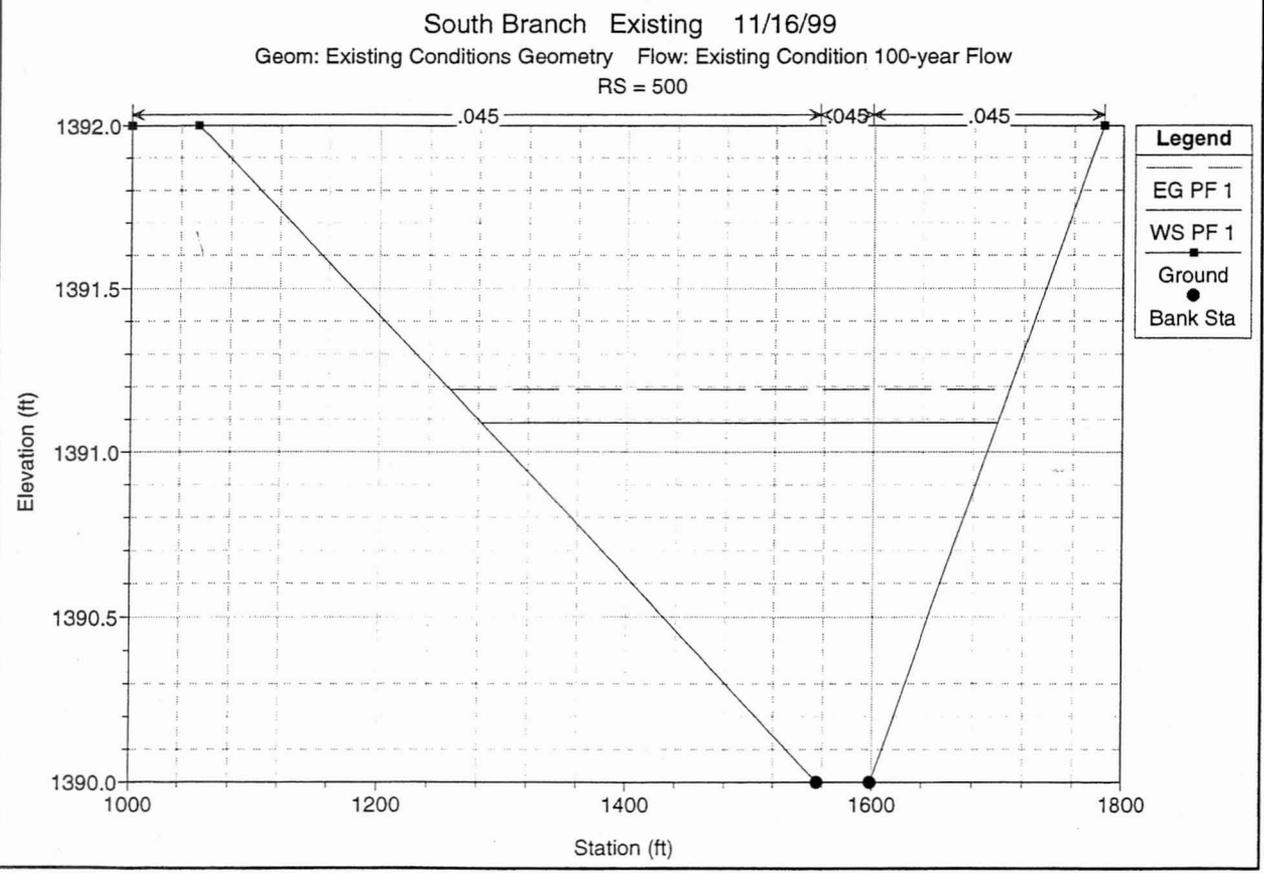
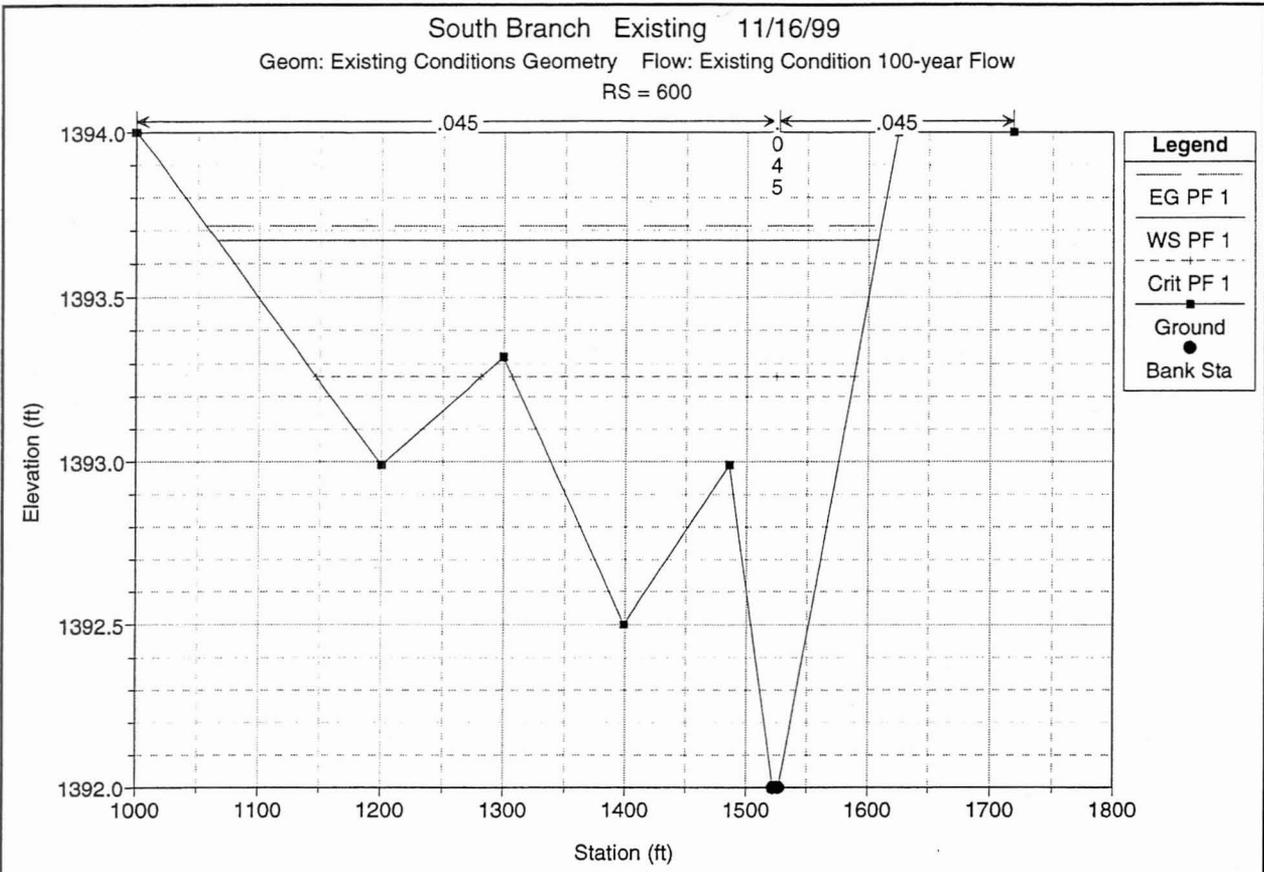
HEC-RAS Plan: Existing River: S-Branch Reach: W-Ellsworth

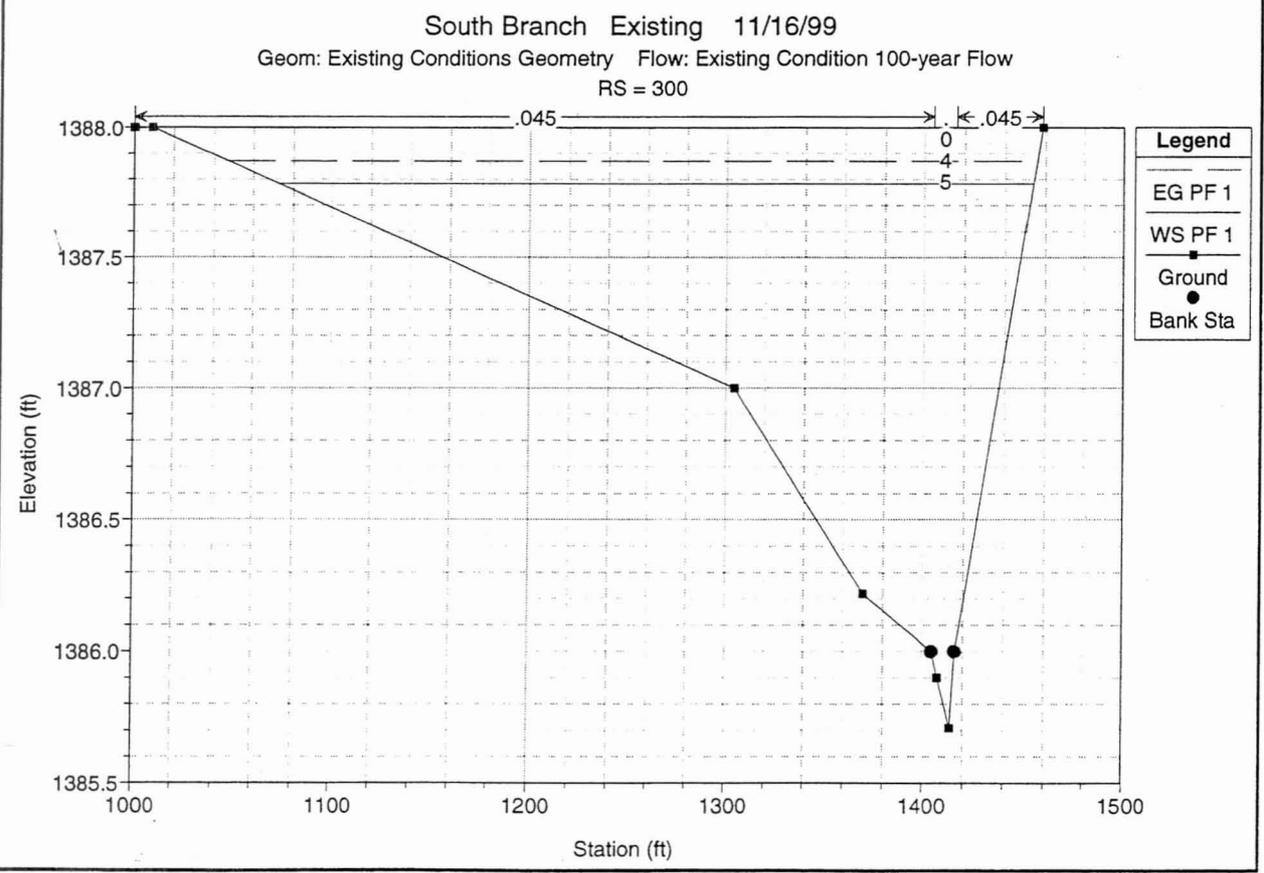
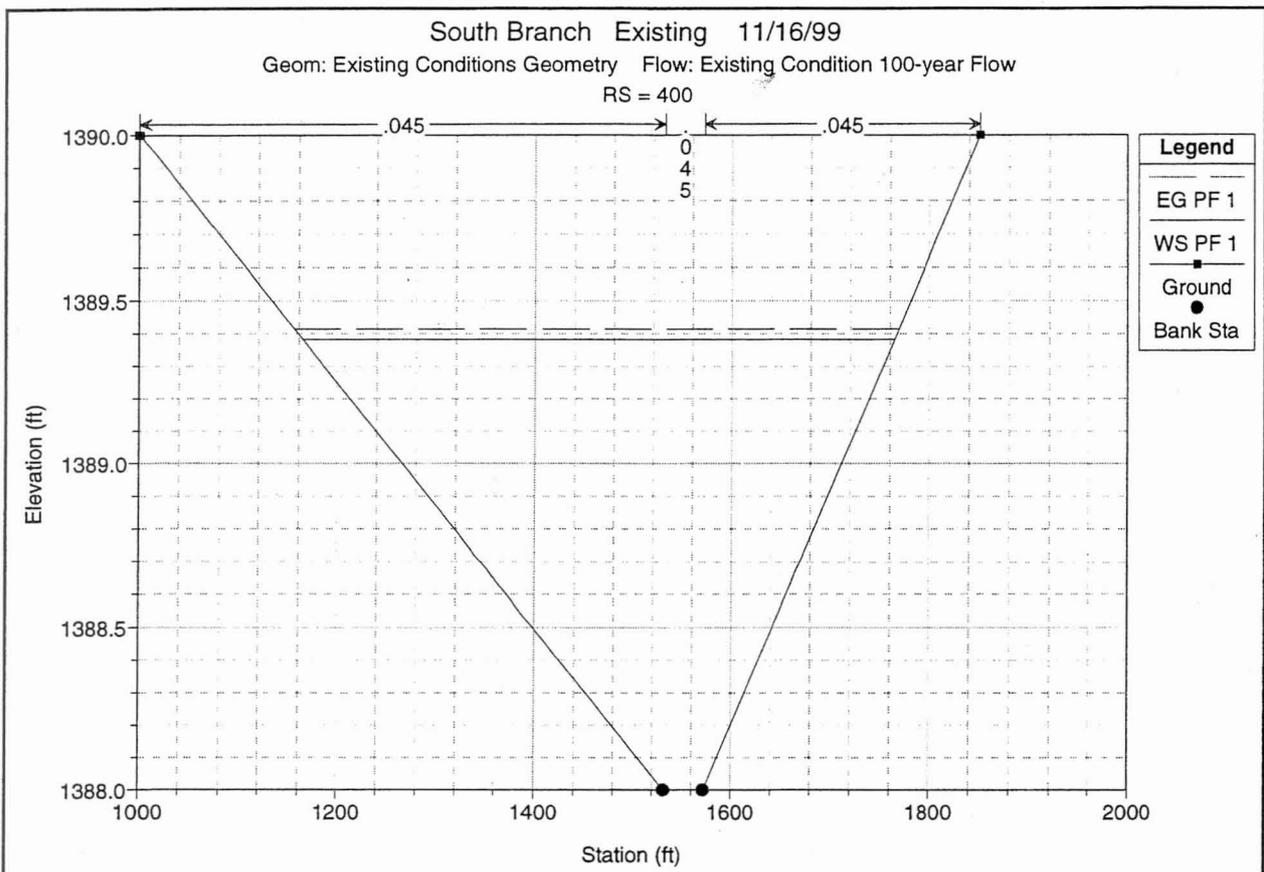
| Reach | River Sta | Q Total (cfs) | Mn Ch El (ft) | W.S. Elev (ft) | Crit W.S. (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl |
|-------------|-----------|------------------|------------------|-------------------|-------------------|-------------------|-----------------------|--------------------|----------------------|-------------------|--------------|
| W-Ellsworth | 100 | 600.00 | 1382.00 | 1383.65 | 1383.24 | 1383.75 | 0.007009 | 3.86 | 246.86 | 413.81 | 0.53 |
| W-Ellsworth | 200 | 600.00 | 1384.00 | 1385.89 | | 1385.94 | 0.004362 | 3.33 | 341.45 | 507.15 | 0.43 |
| W-Ellsworth | 300 | 600.00 | 1385.71 | 1387.78 | | 1387.87 | 0.005736 | 3.88 | 281.71 | 381.44 | 0.49 |
| W-Ellsworth | 400 | 600.00 | 1388.00 | 1389.38 | | 1389.41 | 0.002392 | 2.00 | 442.64 | 600.24 | 0.30 |
| W-Ellsworth | 500 | 600.00 | 1390.00 | 1391.09 | | 1391.19 | 0.009599 | 3.43 | 250.59 | 417.11 | 0.58 |
| W-Ellsworth | 600 | 600.00 | 1392.00 | 1393.67 | 1393.26 | 1393.71 | 0.003840 | 2.88 | 372.25 | 543.32 | 0.39 |

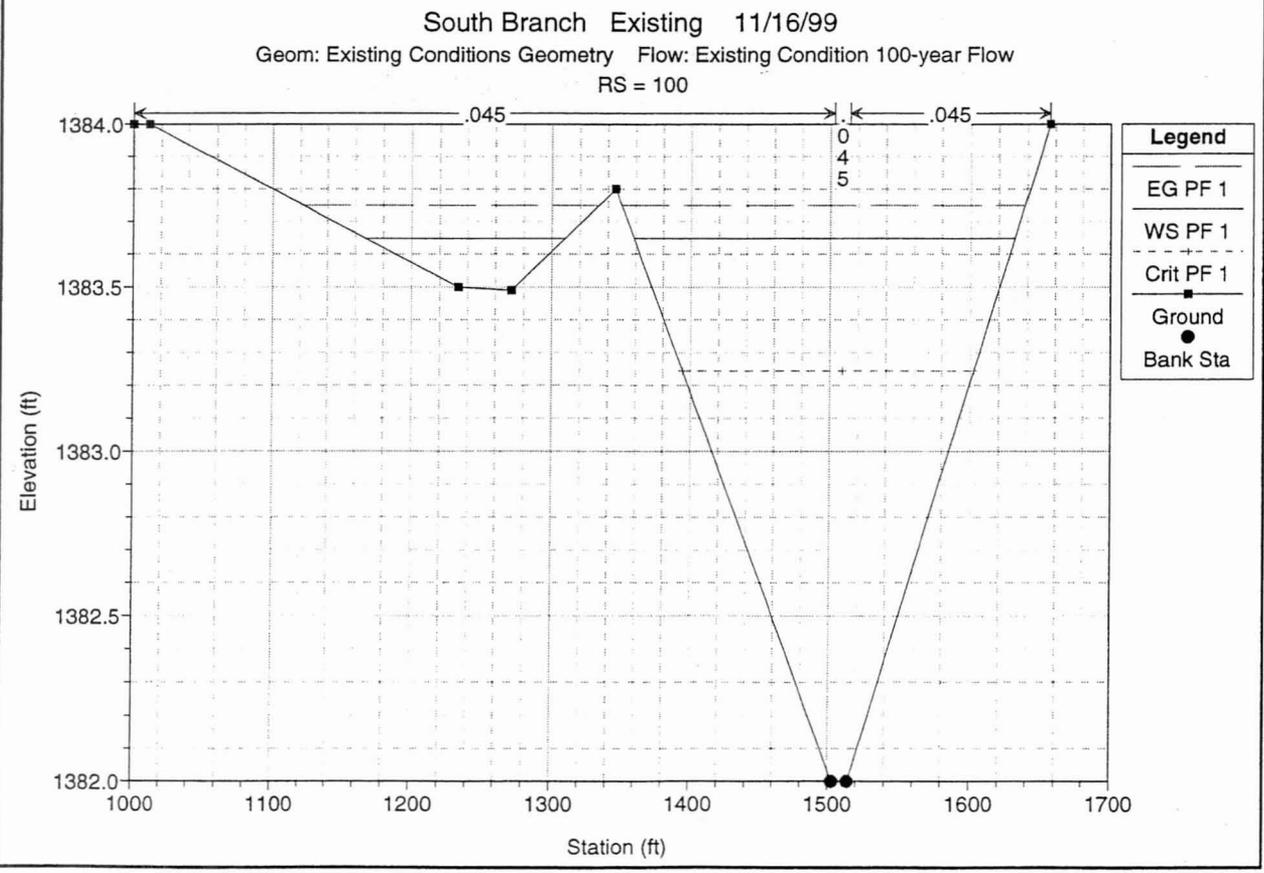
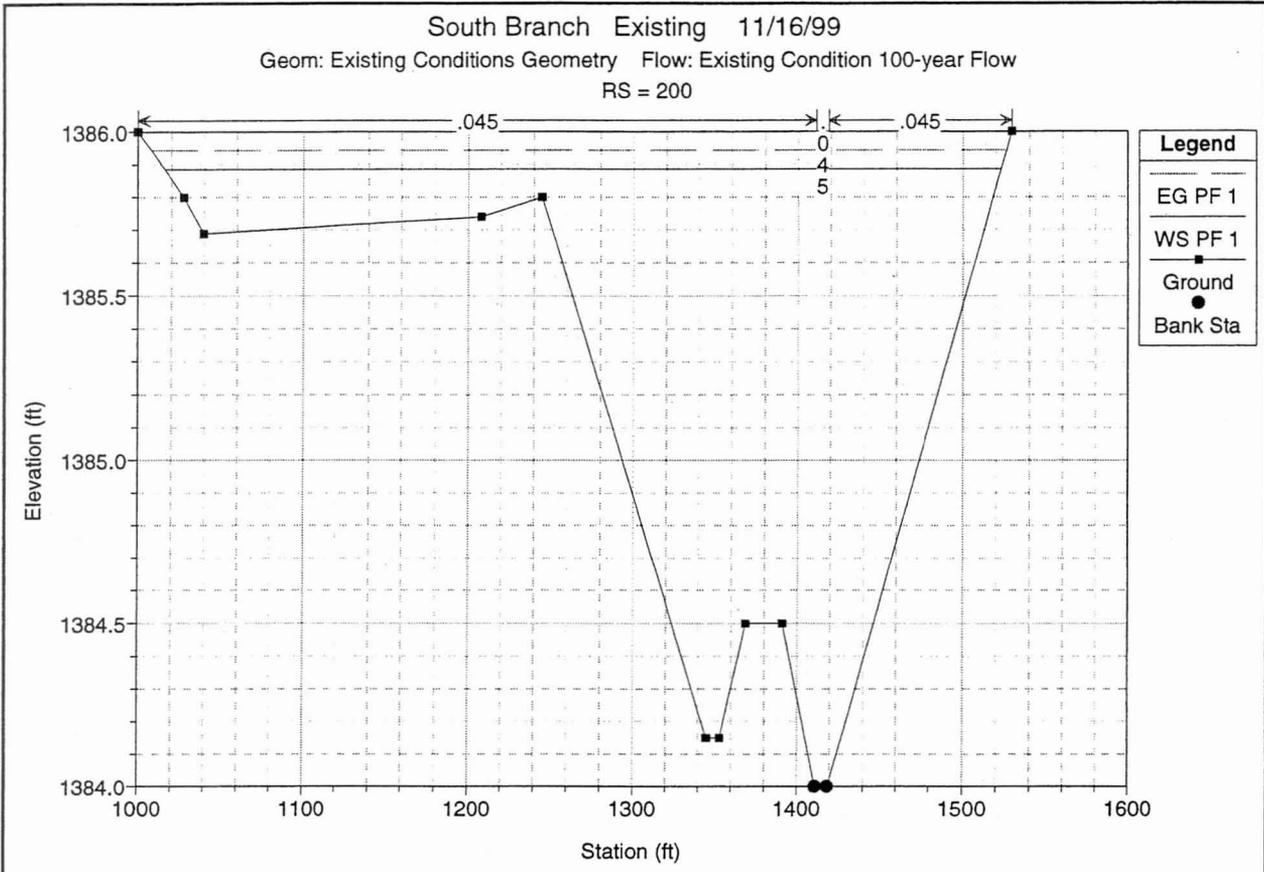
South Branch Existing 11/16/99
Geom: Existing Conditions Geometry Flow: Existing Condition 100-year Flow



| Legend | |
|-----------|-------|
| EG PF 1 | — |
| WS PF 1 | - - - |
| Crit PF 1 | — |
| Ground | ■ |







draft

Appendix C

HEC-RAS Model Results for Interim Conditions

North Branch

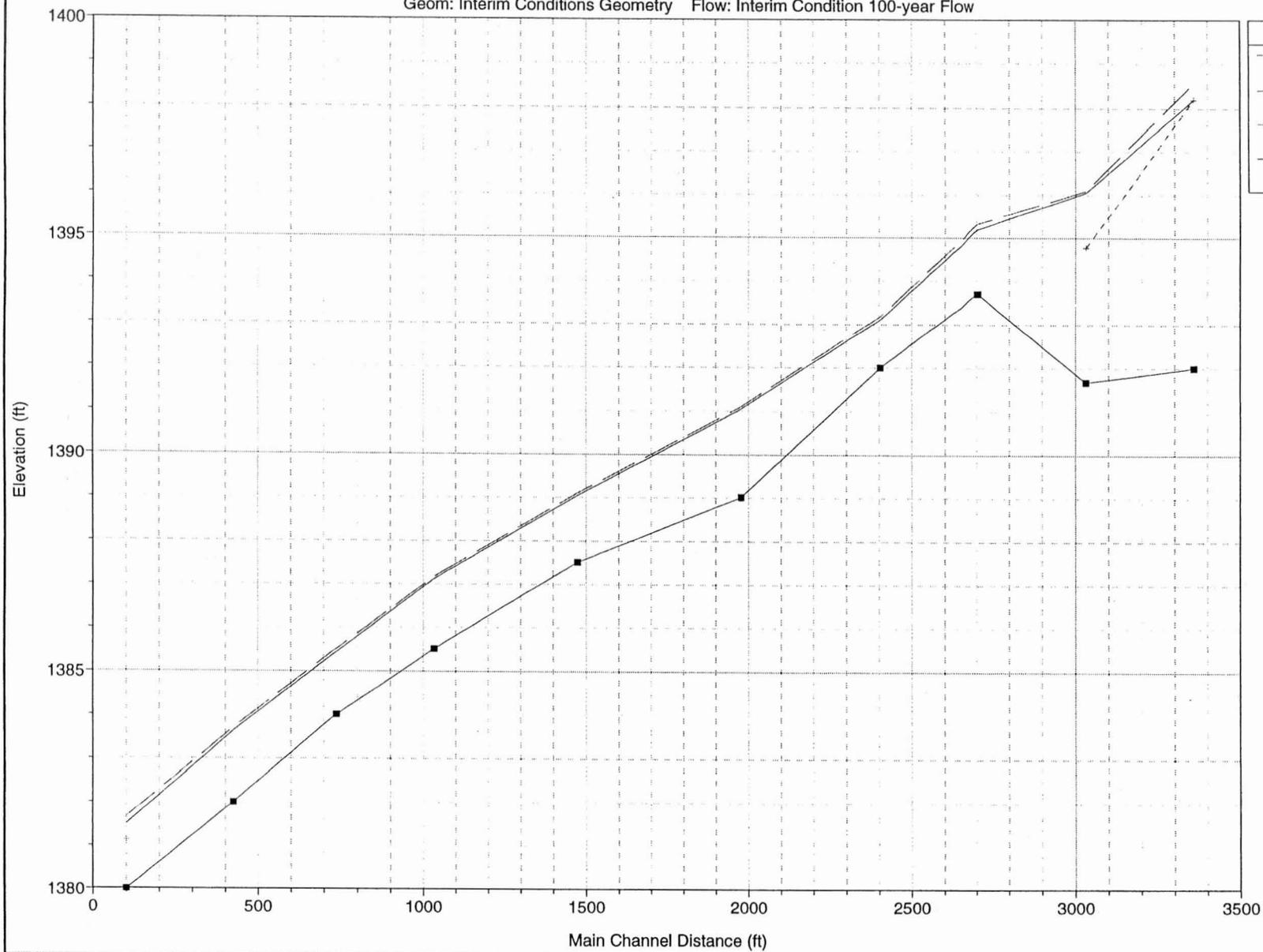
South Branch

HEC-RAS Plan: Interim River: N-Branch Reach: W-Ellsworth

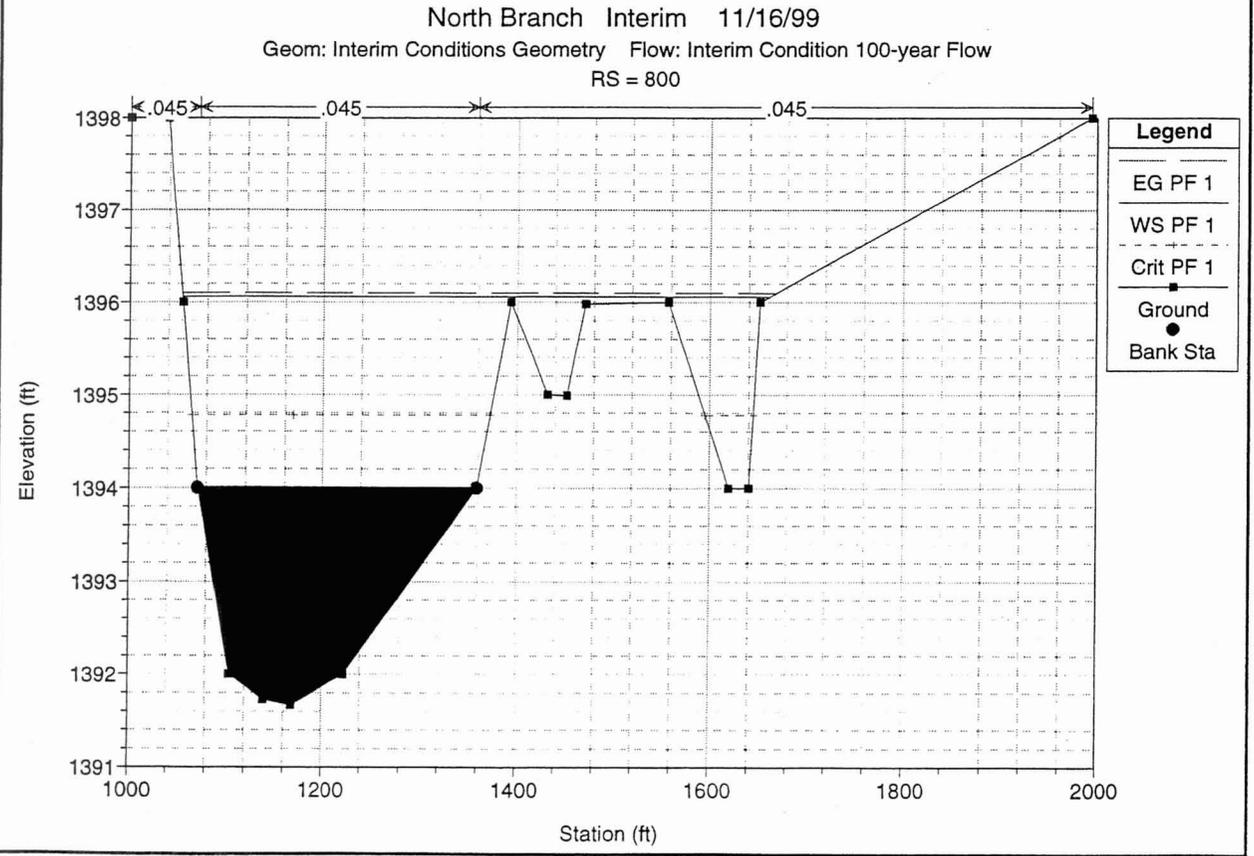
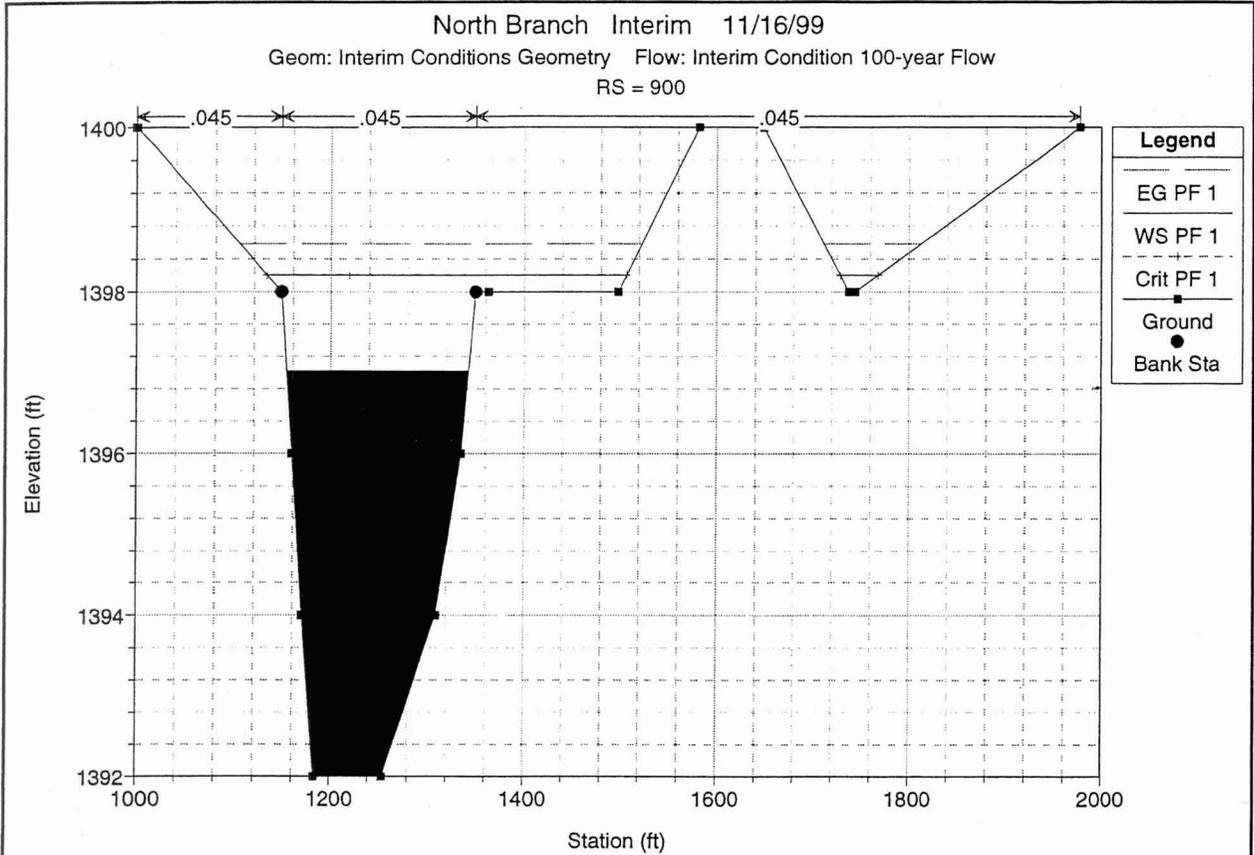
| Reach | River Sta | Q Total (cfs) | Min Ch El (ft) | W/S Elev (ft) | Crit W/S (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl |
|-------------|-----------|------------------|-------------------|------------------|------------------|-------------------|-----------------------|--------------------|----------------------|-------------------|--------------|
| W-Ellsworth | 100 | 1535.00 | 1380.00 | 1381.49 | 1381.12 | 1381.66 | 0.008011 | 3.59 | 483.86 | 474.33 | 0.55 |
| W-Ellsworth | 200 | 1535.00 | 1382.00 | 1383.63 | | 1383.70 | 0.004825 | 2.17 | 714.31 | 788.70 | 0.40 |
| W-Ellsworth | 300 | 1535.00 | 1384.00 | 1385.43 | | 1385.50 | 0.006910 | 2.25 | 681.72 | 917.48 | 0.46 |
| W-Ellsworth | 400 | 1535.00 | 1385.51 | 1387.12 | | 1387.17 | 0.004671 | 1.91 | 803.76 | 1032.42 | 0.38 |
| W-Ellsworth | 450 | 1535.00 | 1387.51 | 1389.05 | | 1389.11 | 0.004156 | 1.91 | 805.50 | 951.02 | 0.36 |
| W-Ellsworth | 500 | 1235.00 | 1389.02 | 1391.05 | | 1391.11 | 0.003843 | 1.90 | 649.53 | 725.09 | 0.35 |
| W-Ellsworth | 600 | 1235.00 | 1392.00 | 1393.10 | | 1393.18 | 0.006198 | 2.22 | 555.50 | 702.33 | 0.44 |
| W-Ellsworth | 700 | 1235.00 | 1393.71 | 1395.20 | | 1395.32 | 0.008408 | 2.89 | 427.54 | 458.80 | 0.53 |
| W-Ellsworth | 800 | 1235.00 | 1393.89 | 1396.06 | 1394.78 | 1396.10 | 0.001072 | 1.74 | 824.13 | 607.06 | 0.21 |
| W-Ellsworth | 900 | 1235.00 | 1397.02 | 1398.21 | 1398.21 | 1398.59 | 0.019321 | 5.05 | 271.04 | 413.08 | 0.83 |

North Branch Interim 11/16/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow



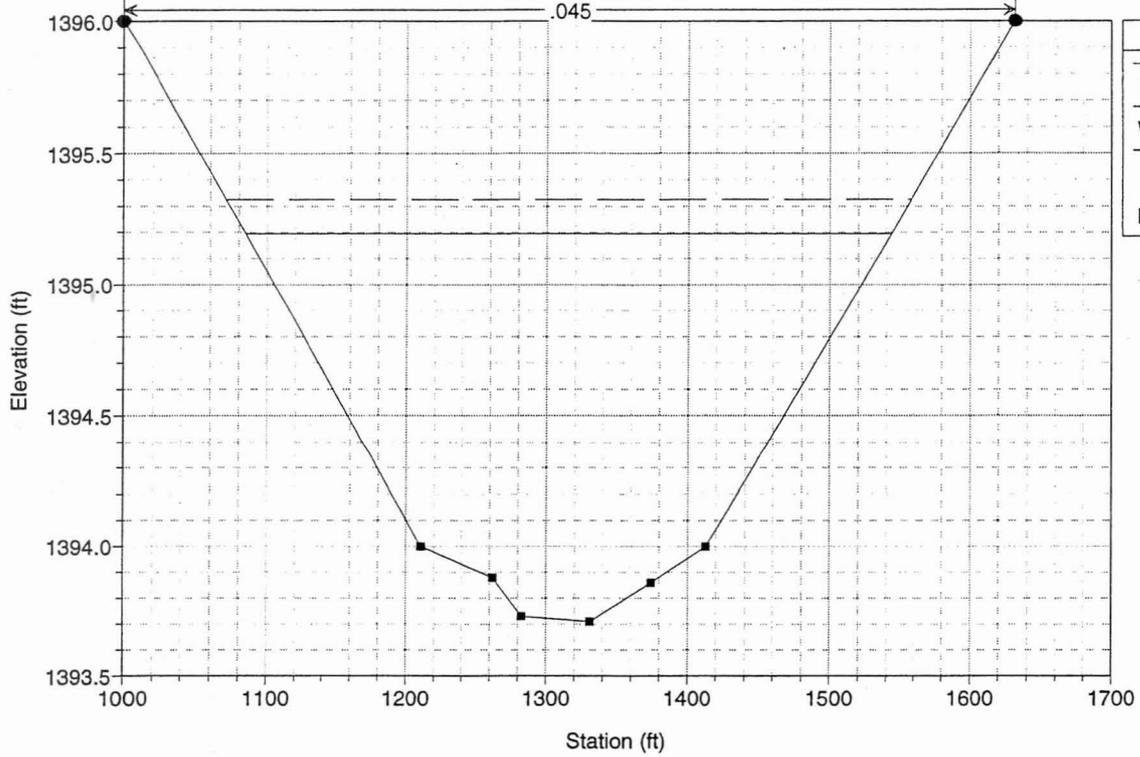
| Legend | |
|-----------|----------------------------------|
| EG PF 1 | (Solid line) |
| WS PF 1 | (Dashed line) |
| Crit PF 1 | (Dotted line) |
| Ground | (Solid line with square markers) |



North Branch Interim 11/16/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 700

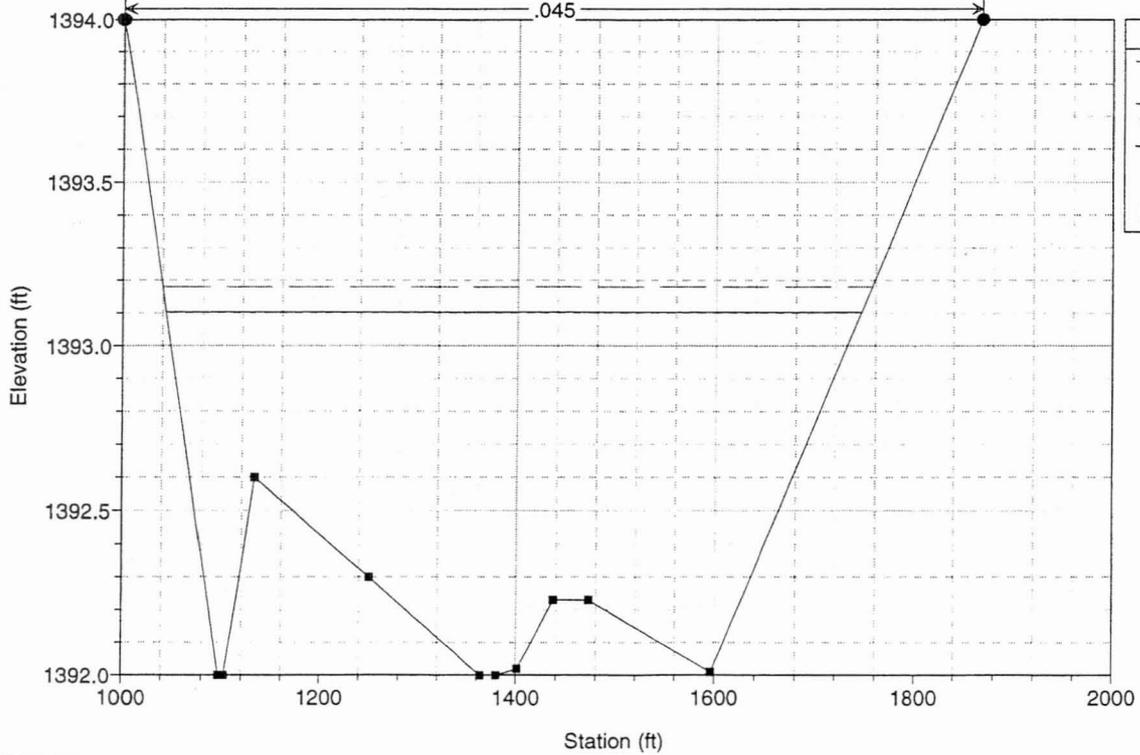


| Legend | |
|----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Ground | ■ |
| Bank Sta | ● |

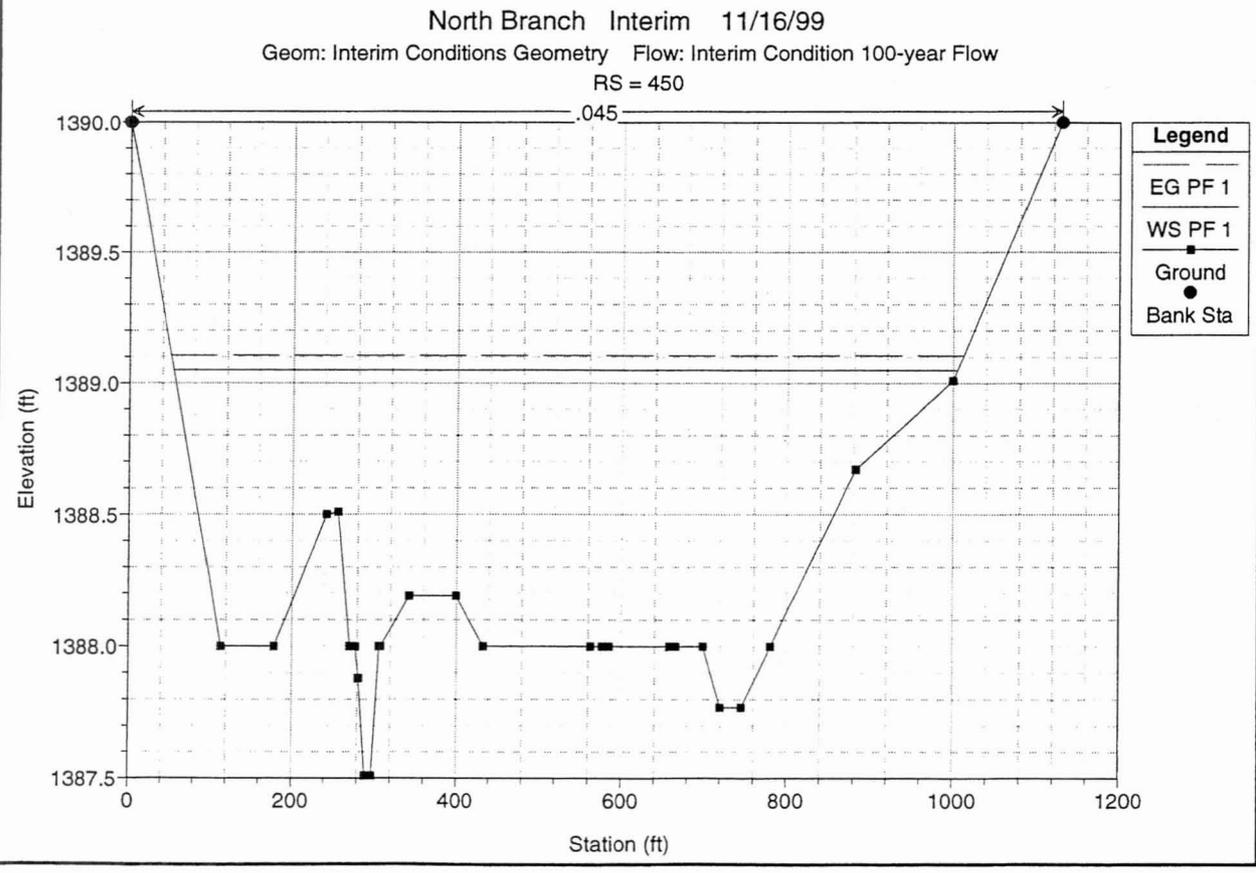
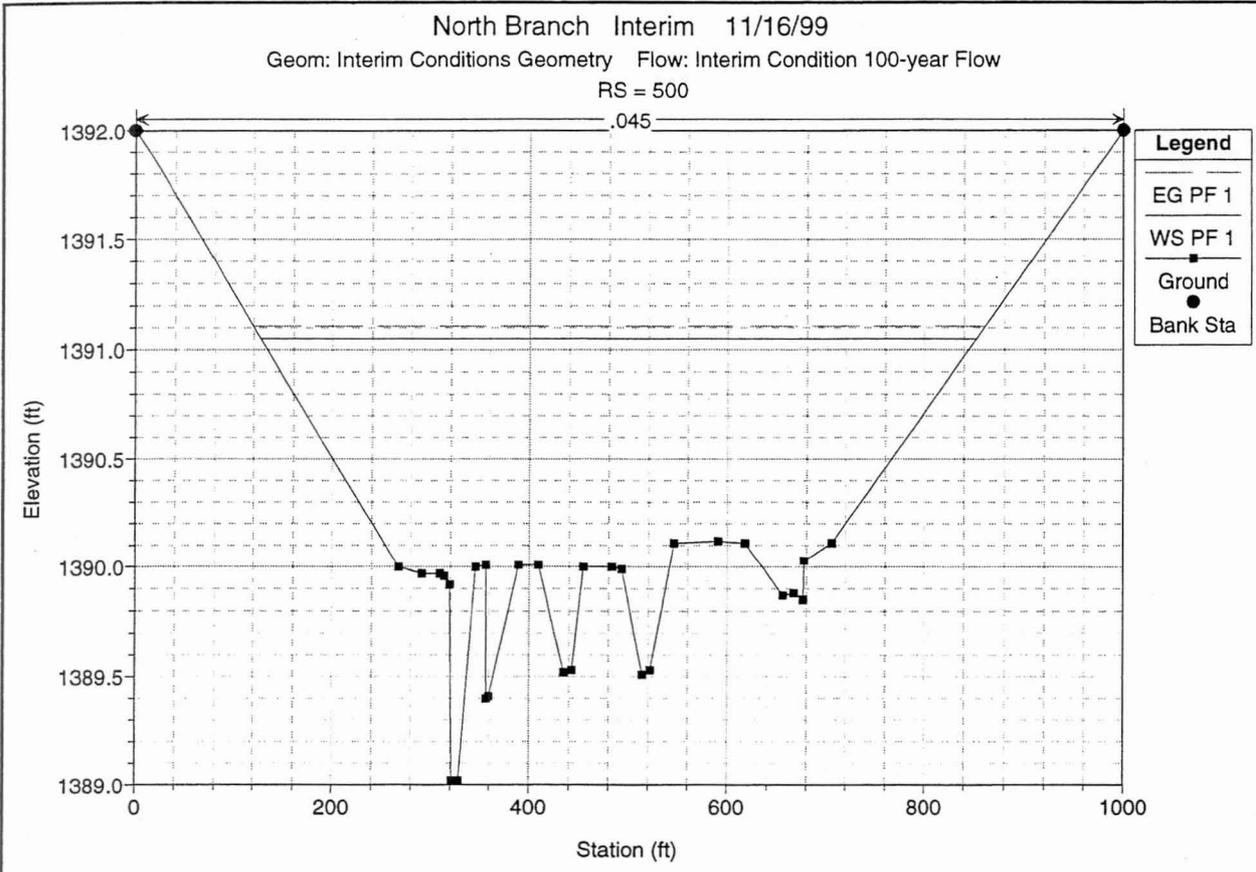
North Branch Interim 11/16/99

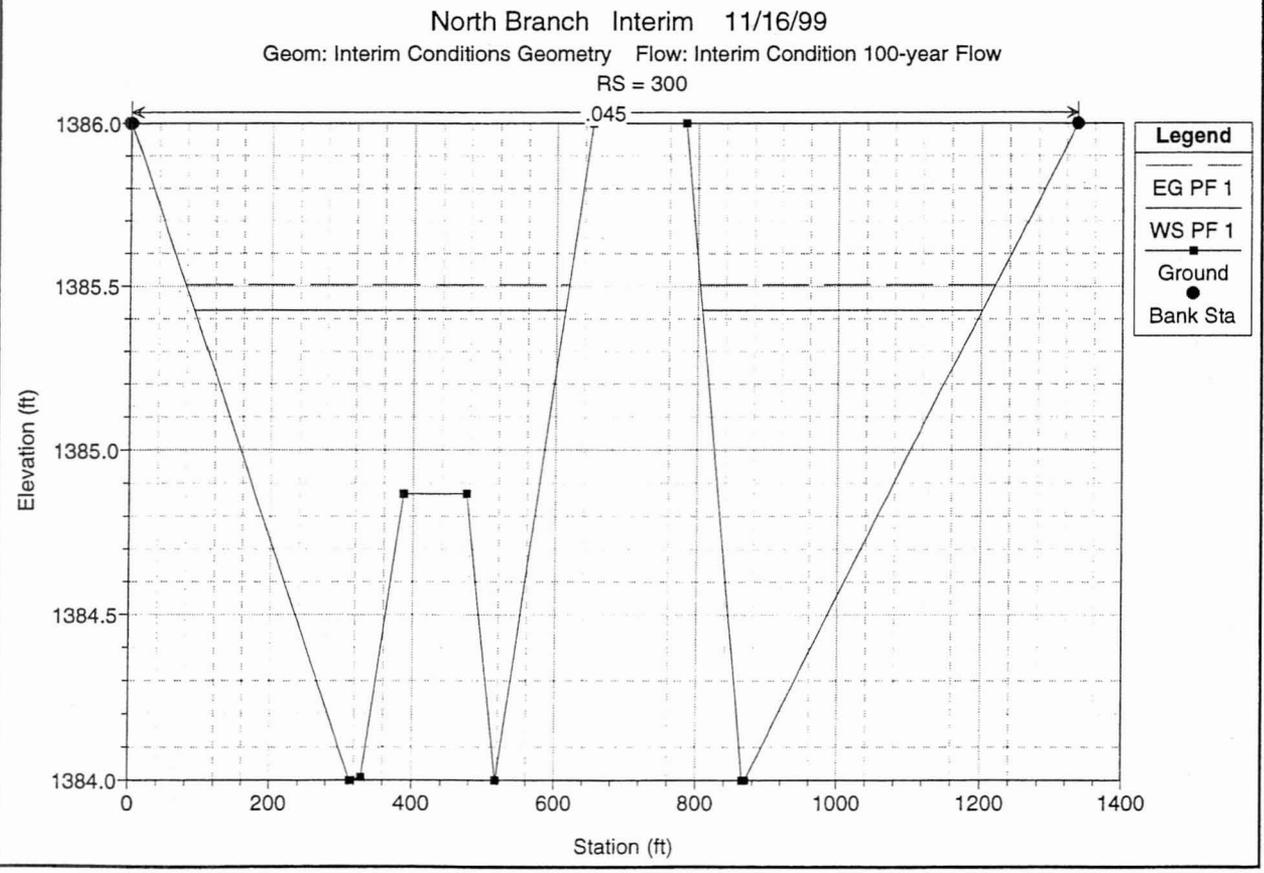
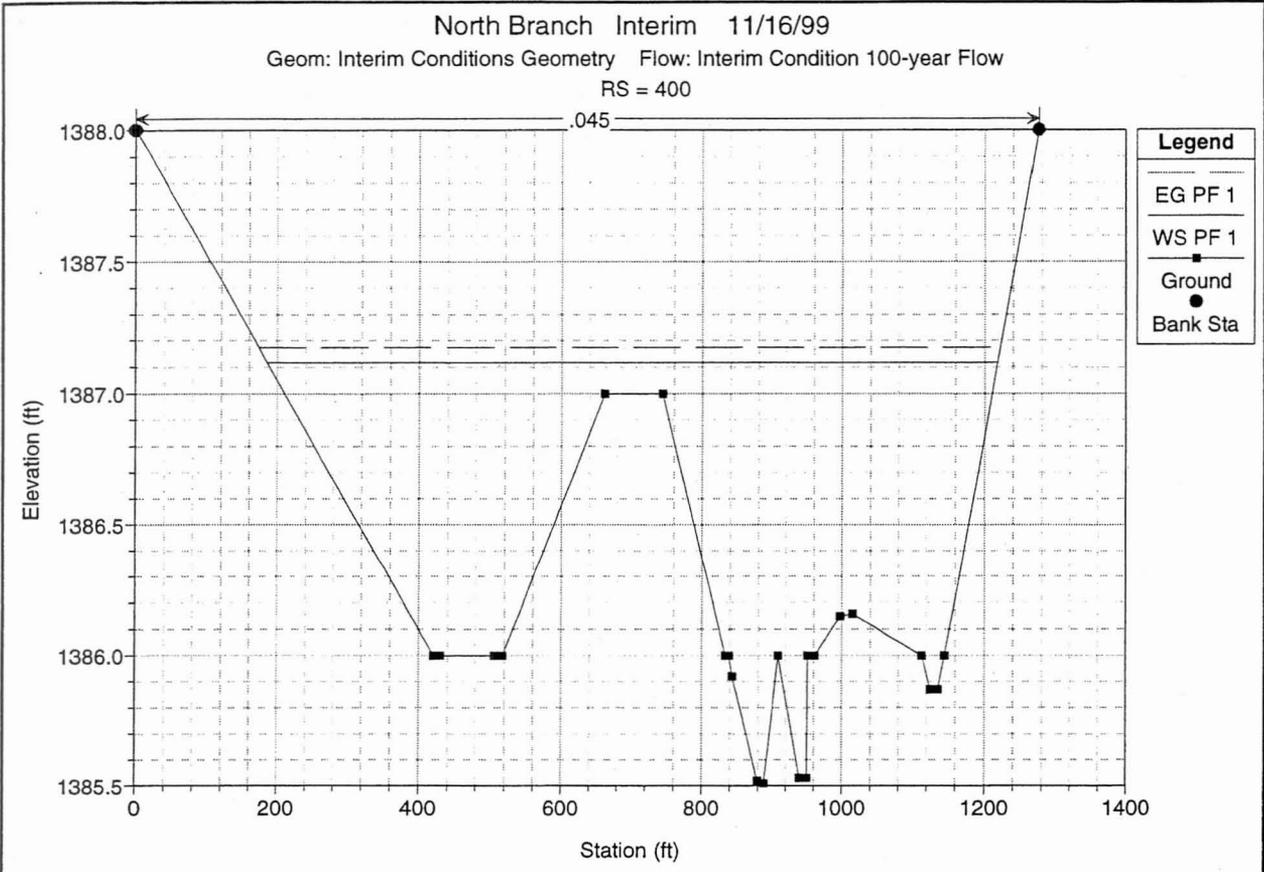
Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 600



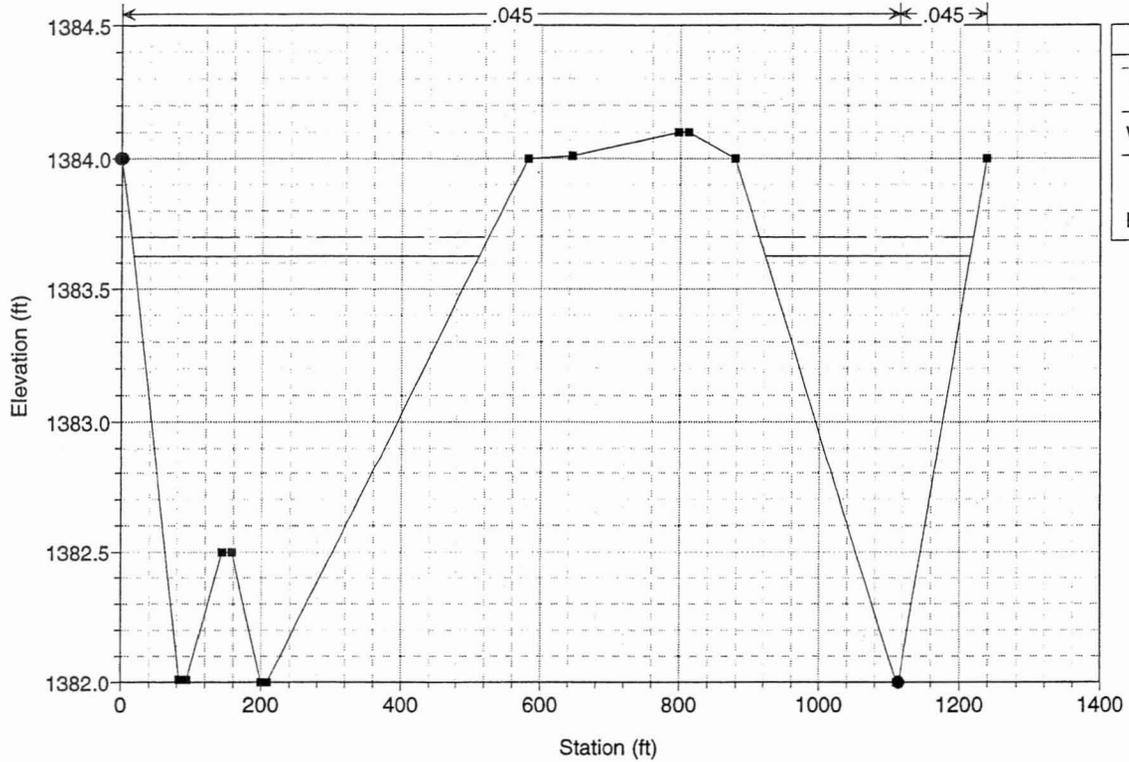
| Legend | |
|----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Ground | ■ |
| Bank Sta | ● |





North Branch Interim 11/16/99

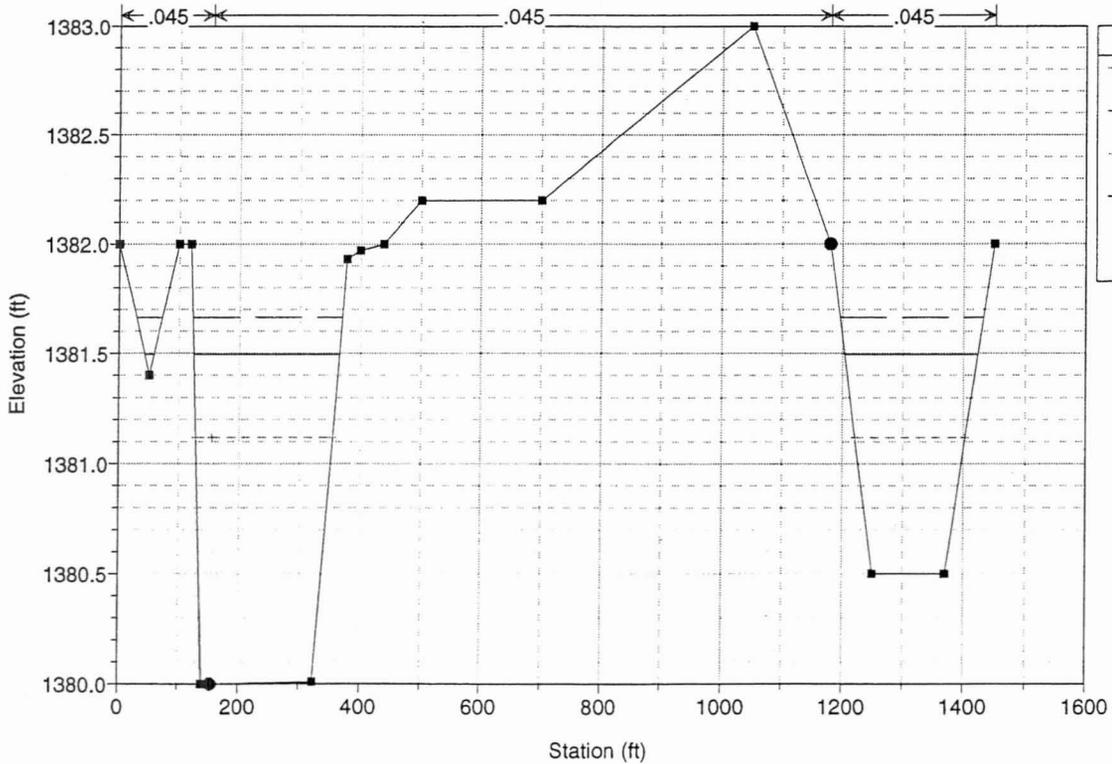
Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow
RS = 200



| Legend | |
|--------|----------|
| — | EG PF 1 |
| - - - | WS PF 1 |
| ■ | Ground |
| ● | Bank Sta |

North Branch Interim 11/16/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow
RS = 100



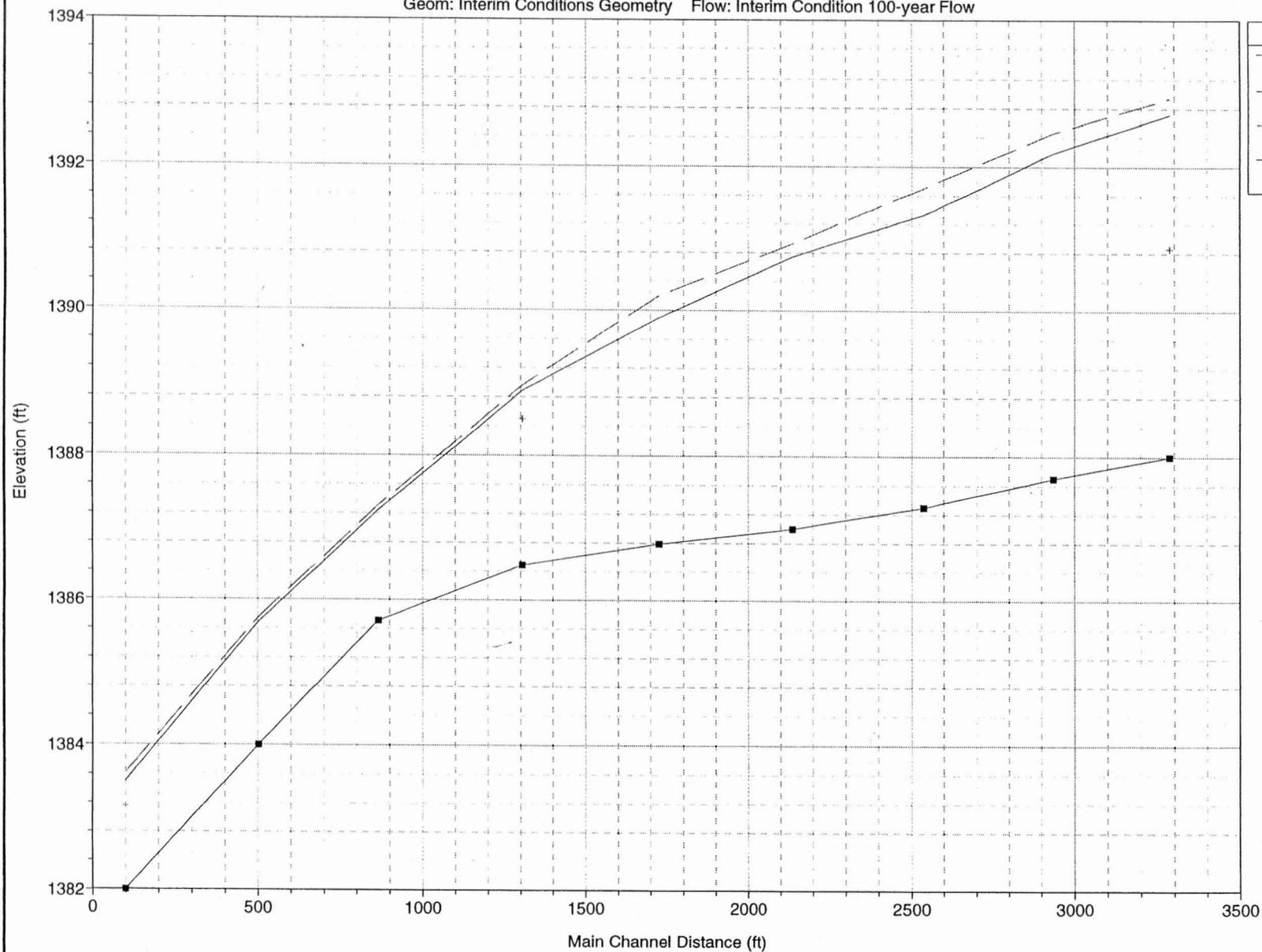
| Legend | |
|--------|-----------|
| — | EG PF 1 |
| - - - | WS PF 1 |
| ■ | Crit PF 1 |
| ● | Ground |
| ● | Bank Sta |

HEC-RAS Plan: Interim River: S-Branch Reach: W-Ellsworth

| Reach | River Sta | Q Total (cfs) | Min Chl El (ft) | W.S. Elev (ft) | Crit W/S (ft) | E.G. Elev (ft) | E.G. Slope (ft/ft) | Vel Chnl (ft/s) | Flow Area (sq ft) | Top Width (ft) | Froude # Chl |
|-------------|-----------|------------------|--------------------|-------------------|------------------|-------------------|-----------------------|--------------------|----------------------|-------------------|--------------|
| W-Ellsworth | 100 | 500.00 | 1382.00 | 1383.50 | 1383.15 | 1383.61 | 0.008002 | 3.88 | 195.57 | 291.22 | 0.56 |
| W-Ellsworth | 200 | 500.00 | 1384.00 | 1385.68 | | 1385.75 | 0.003699 | 2.84 | 251.48 | 259.87 | 0.39 |
| W-Ellsworth | 300 | 500.00 | 1385.71 | 1387.24 | | 1387.31 | 0.004765 | 2.33 | 251.28 | 325.28 | 0.40 |
| W-Ellsworth | 400 | 500.00 | 1386.49 | 1388.88 | 1388.50 | 1388.96 | 0.003019 | 3.25 | 300.79 | 427.28 | 0.37 |
| W-Ellsworth | 500 | 500.00 | 1386.79 | 1389.89 | | 1390.20 | 0.002612 | 5.05 | 121.23 | 58.12 | 0.51 |
| W-Ellsworth | 600 | 500.00 | 1387.00 | 1390.74 | | 1390.92 | 0.001230 | 3.93 | 158.92 | 64.92 | 0.36 |
| W-Ellsworth | 700 | 800.00 | 1387.30 | 1391.32 | | 1391.70 | 0.002387 | 5.74 | 174.90 | 66.94 | 0.50 |
| W-Ellsworth | 800 | 800.00 | 1387.70 | 1392.19 | | 1392.47 | 0.001522 | 4.93 | 205.91 | 71.68 | 0.41 |
| W-Ellsworth | 900 | 800.00 | 1388.00 | 1392.72 | 1390.86 | 1392.94 | 0.001190 | 4.50 | 227.73 | 76.59 | 0.37 |

South Branch Interim Conditions 11/17/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

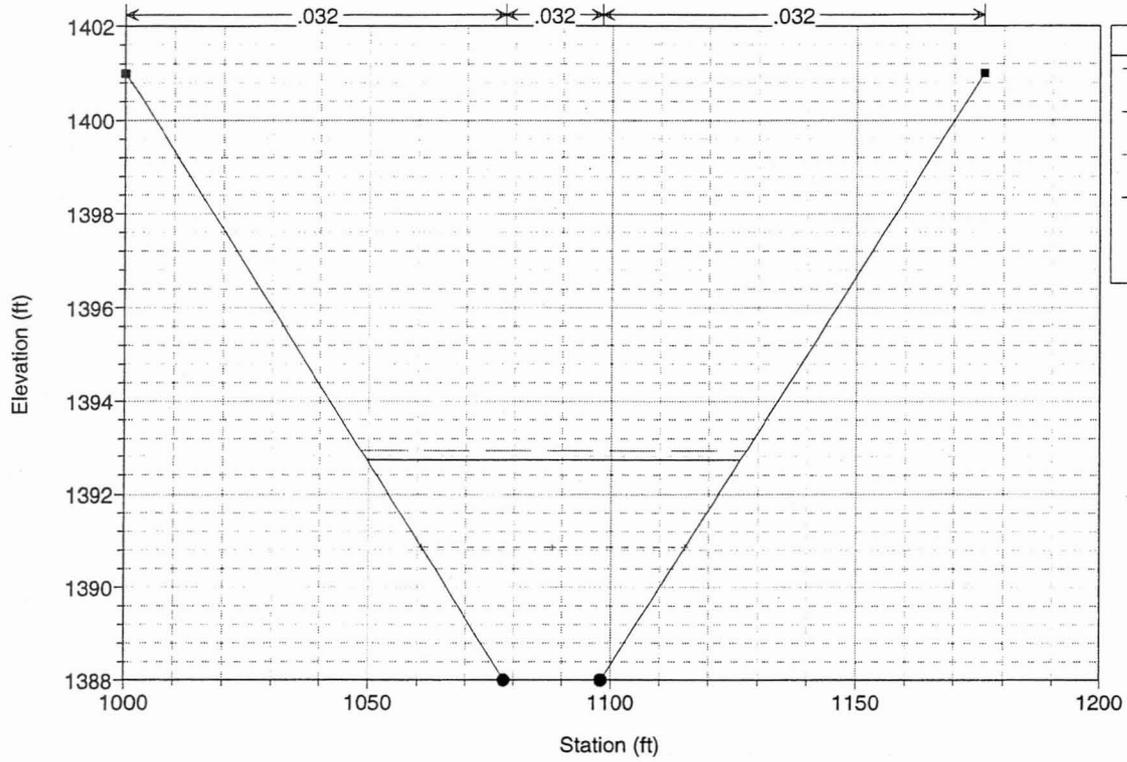


| Legend | |
|-----------|----------------------------------|
| EG PF 1 | (Dashed line) |
| WS PF 1 | (Solid line) |
| Crit PF 1 | (Dotted line) |
| Ground | (Solid line with square markers) |

South Branch Interim Conditions 11/17/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 900

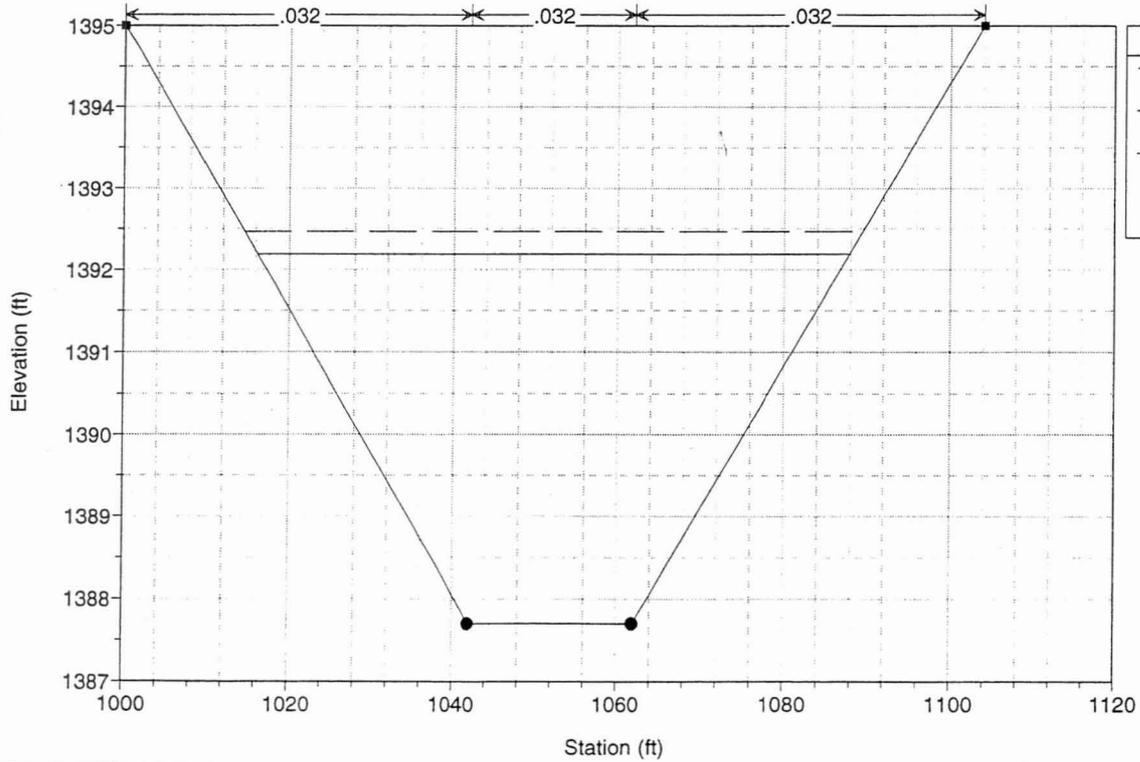


| Legend | |
|--------|-----------|
| — | EG PF 1 |
| - - - | WS PF 1 |
| ■ | Crit PF 1 |
| ● | Ground |
| ● | Bank Sta |

South Branch Interim Conditions 11/17/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 800

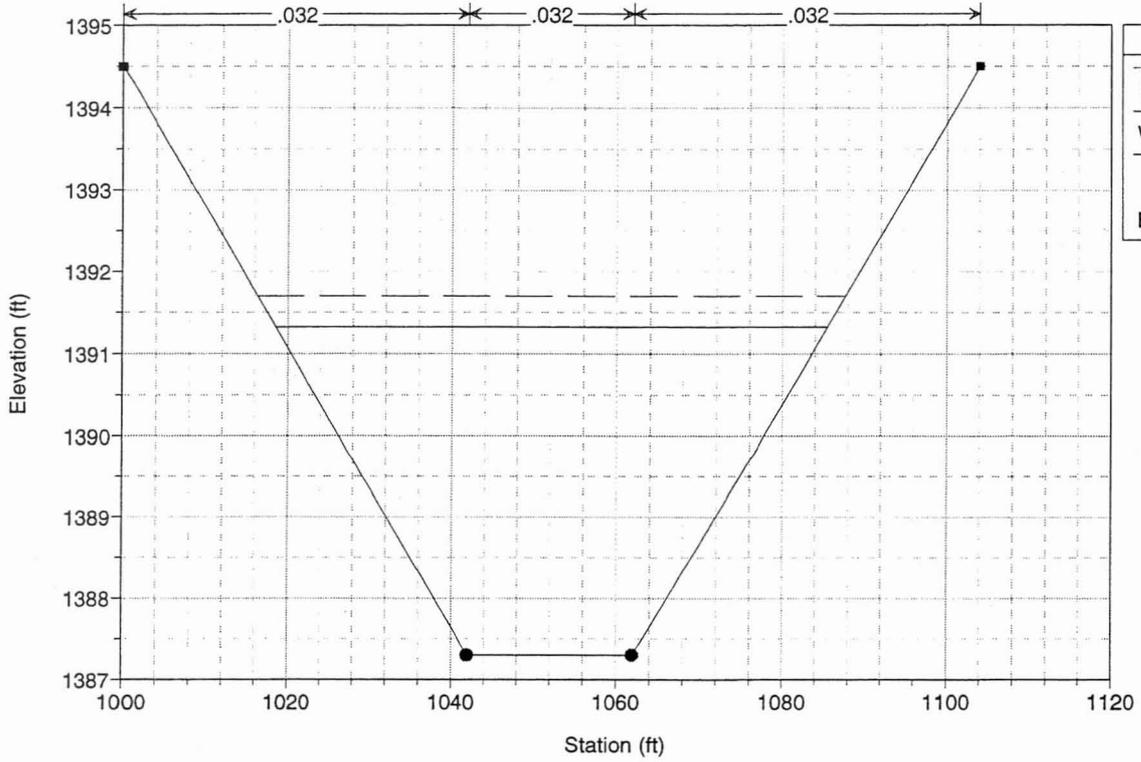


| Legend | |
|--------|-----------|
| — | EG PF 1 |
| - - - | WS PF 1 |
| ■ | Crit PF 1 |
| ● | Ground |
| ● | Bank Sta |

South Branch Interim Conditions 11/17/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

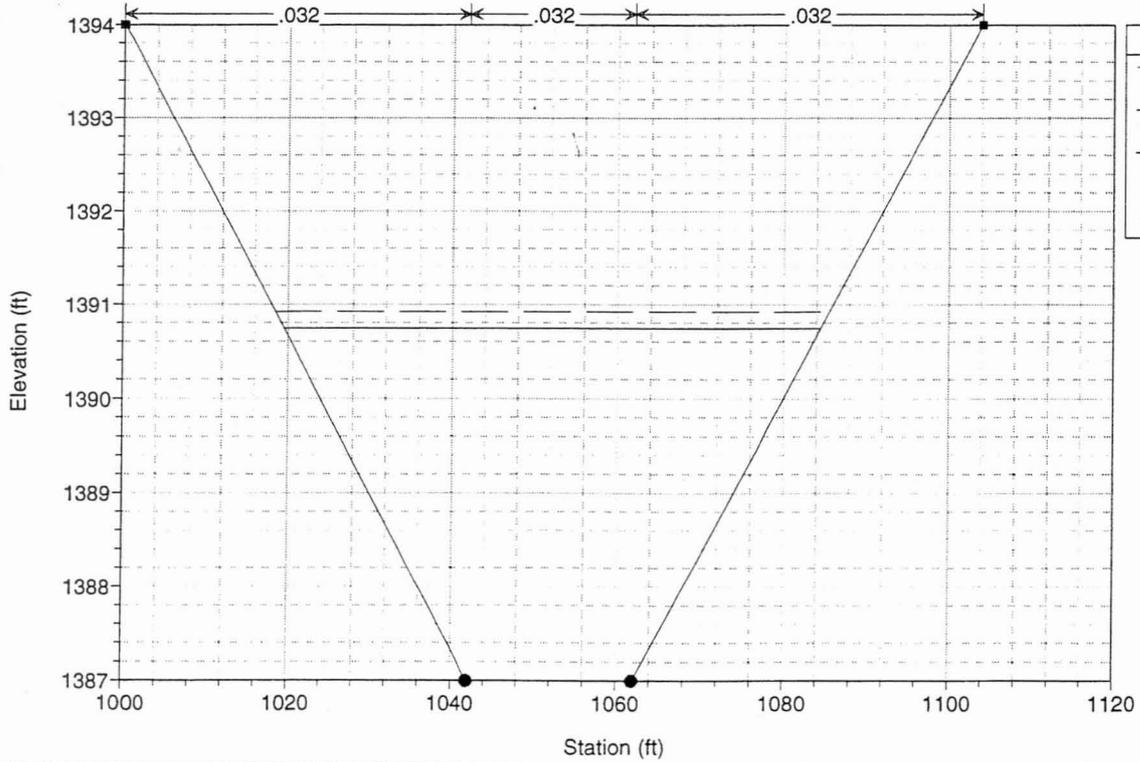
RS = 700

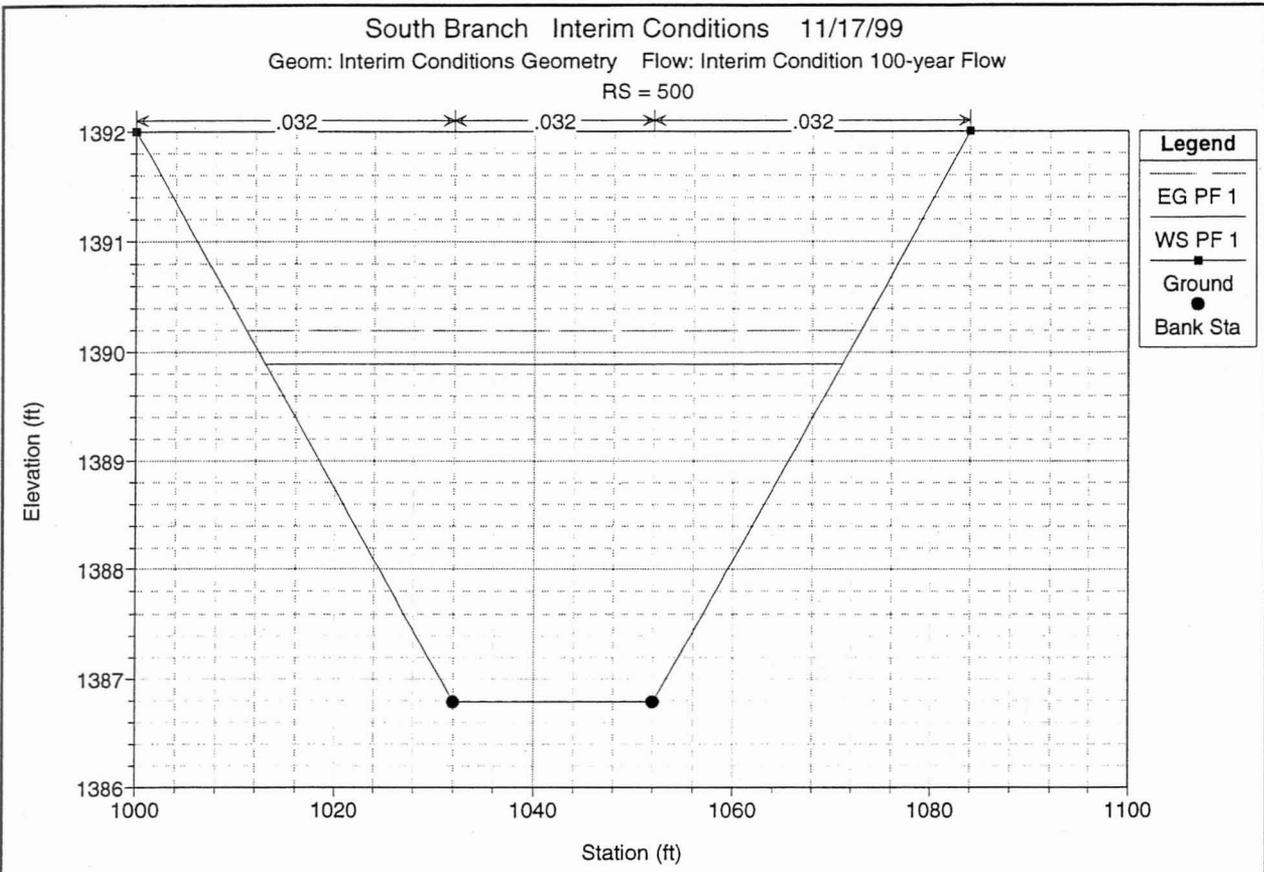


South Branch Interim Conditions 11/17/99

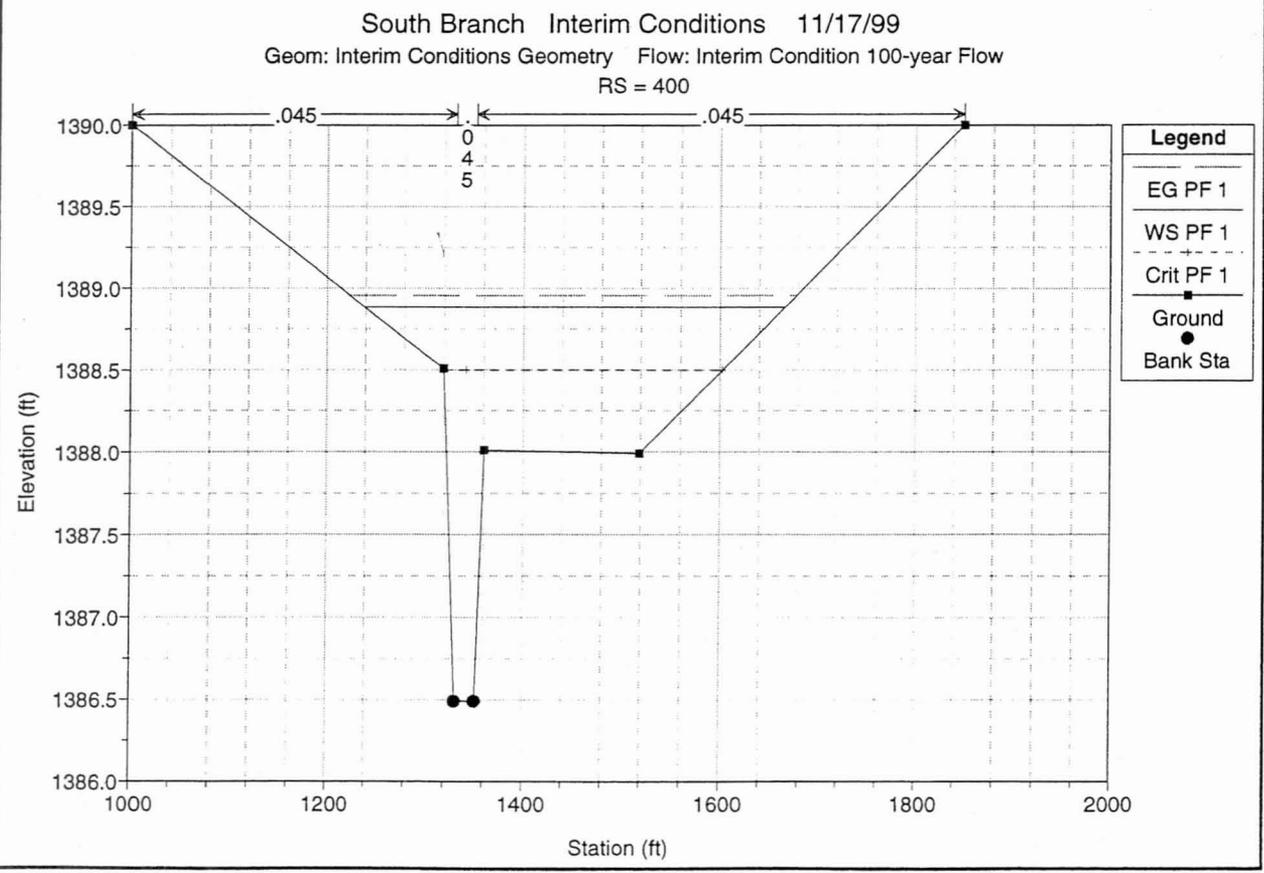
Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 600





| Legend | |
|----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Ground | ● |
| Bank Sta | ■ |

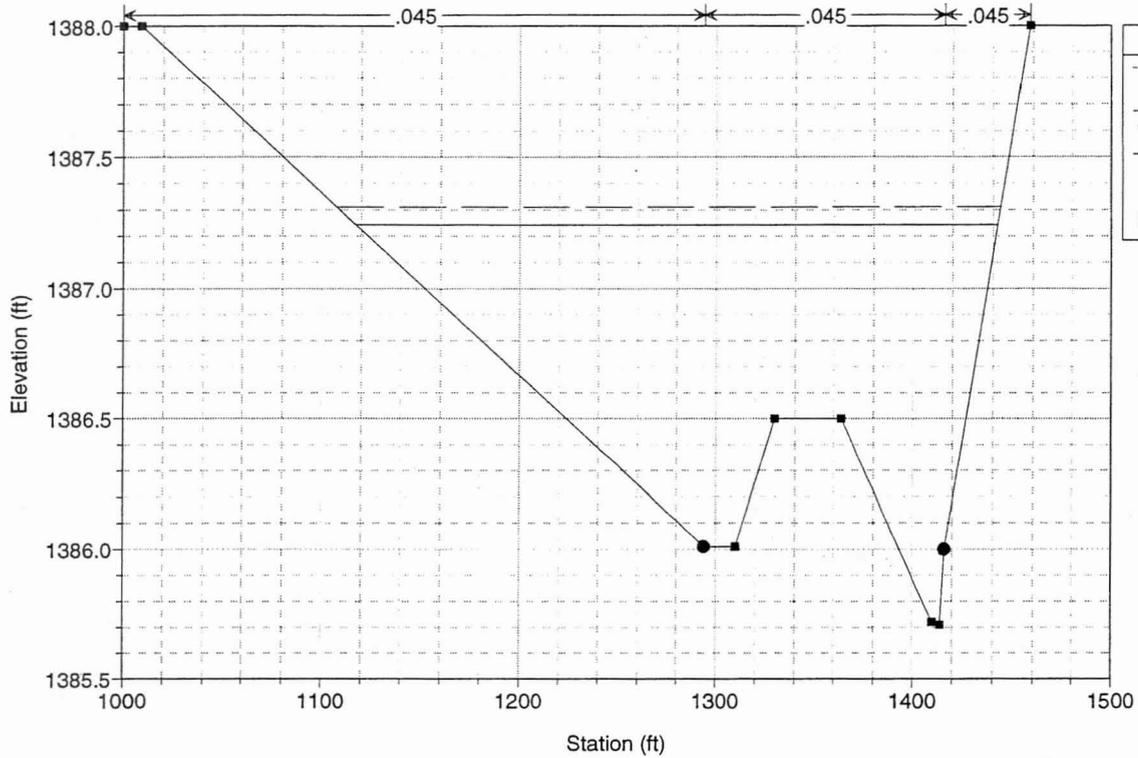


| Legend | |
|-----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Crit PF 1 | — |
| Ground | ● |
| Bank Sta | ■ |

South Branch Interim Conditions 11/17/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 300

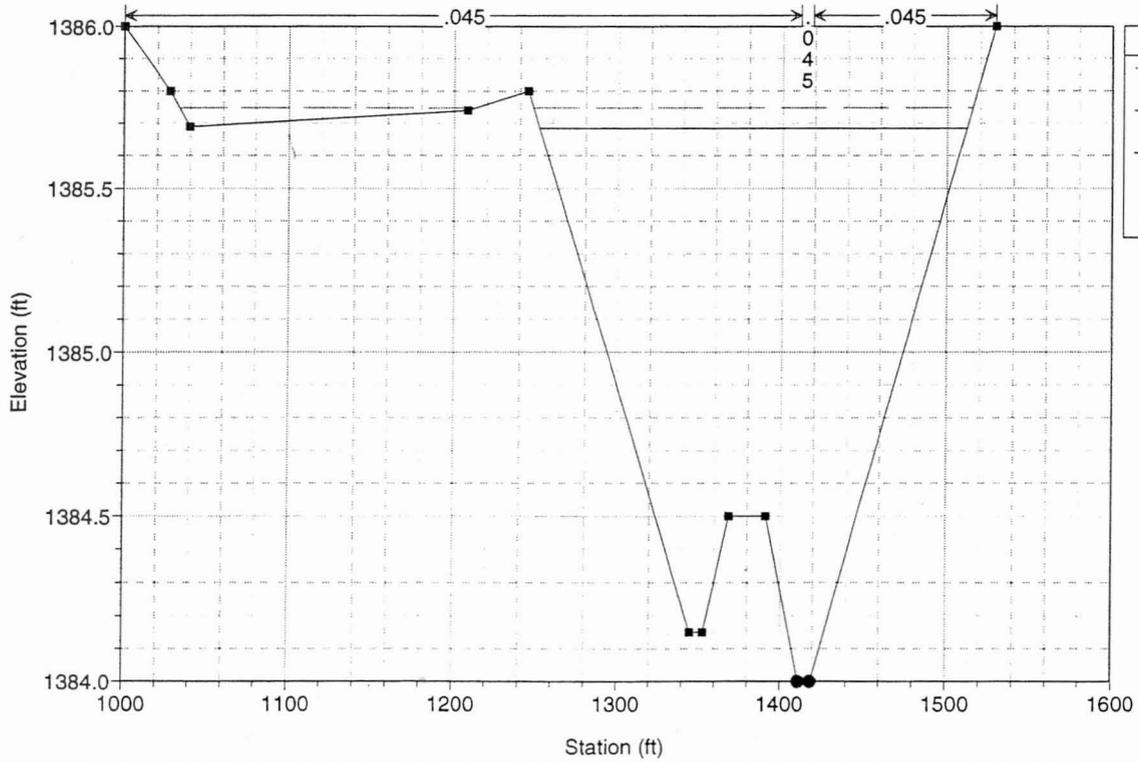


| Legend | |
|----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Ground | ● |
| Bank Sta | ■ |

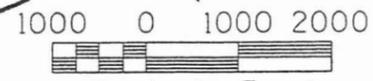
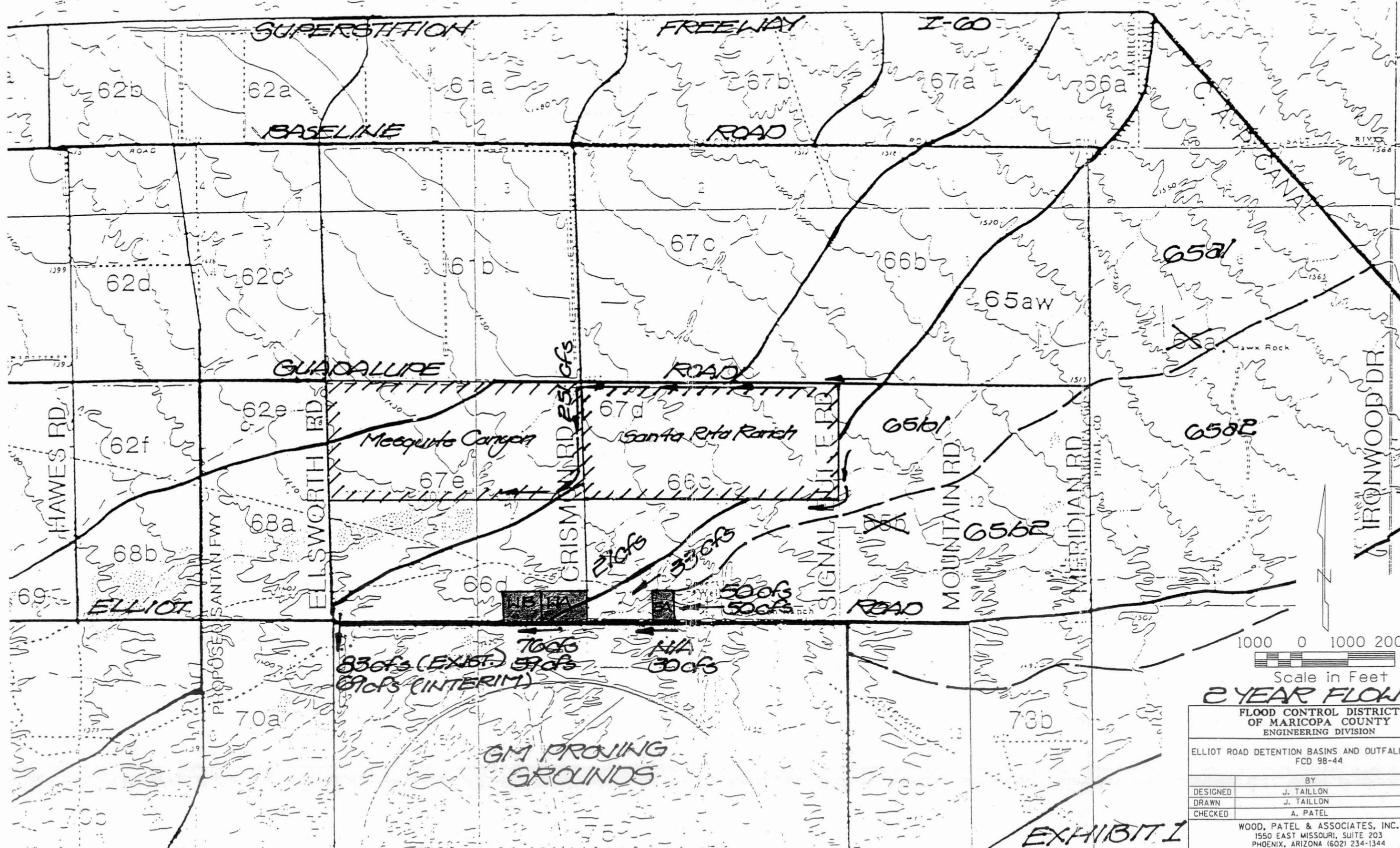
South Branch Interim Conditions 11/17/99

Geom: Interim Conditions Geometry Flow: Interim Condition 100-year Flow

RS = 200



| Legend | |
|----------|---|
| EG PF 1 | — |
| WS PF 1 | — |
| Ground | ● |
| Bank Sta | ■ |



Scale in Feet
2 YEAR FLOWS

FLOOD CONTROL DISTRICT
 OF MARICOPA COUNTY
 ENGINEERING DIVISION

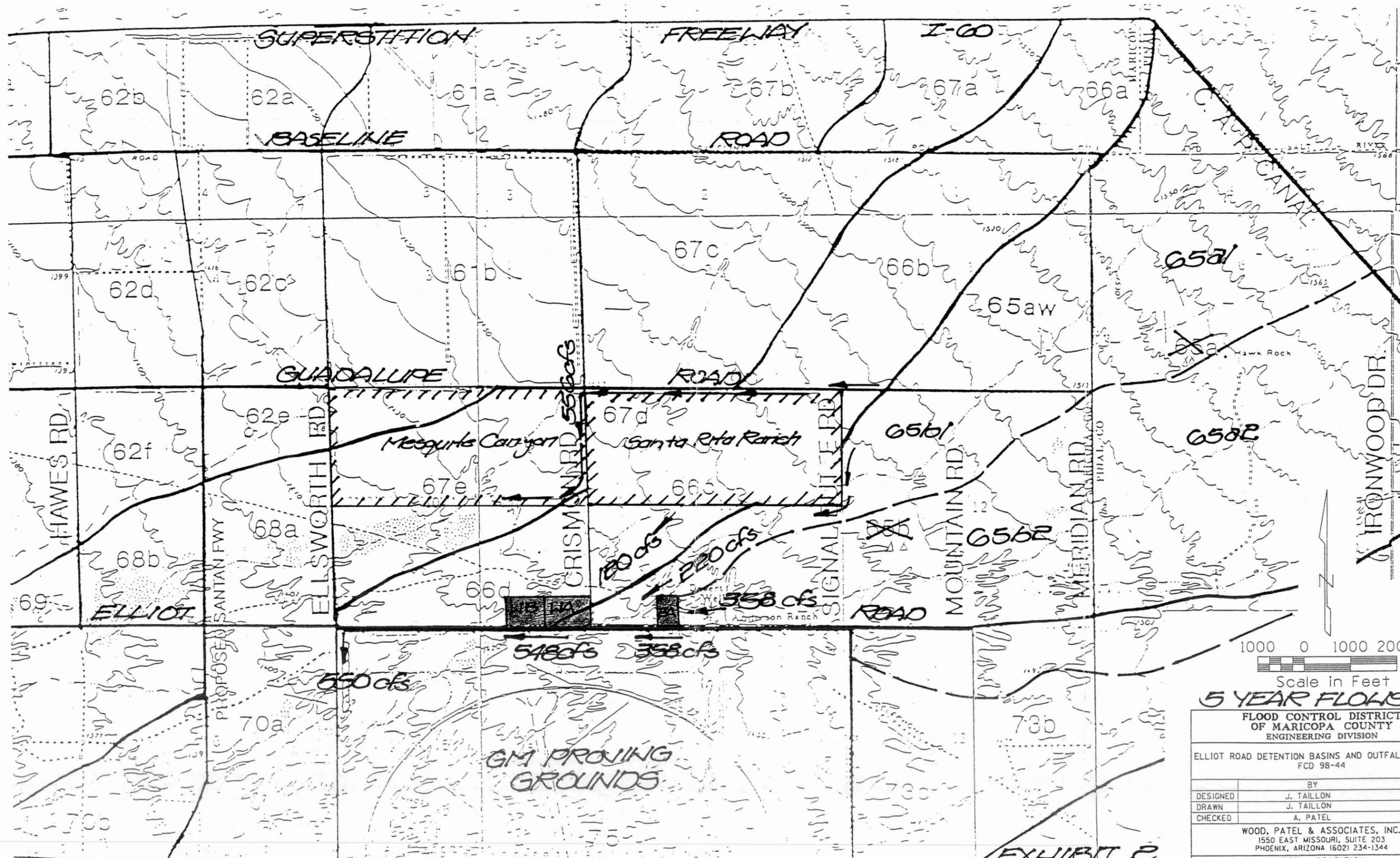
ELLIOT ROAD DETENTION BASINS AND OUTFALL CHANNEL
 FCD 98-44

| | BY | DATE |
|----------|------------|-------|
| DESIGNED | J. TAILLON | 11/99 |
| DRAWN | J. TAILLON | 11/99 |
| CHECKED | A. PATEL | 11/99 |

WOOD, PATEL & ASSOCIATES, INC.
 1550 EAST MISSOURI, SUITE 203
 PHOENIX, ARIZONA (602) 234-1344

INTERIM CONDITION
 HYDROLOGY

SHEET OF
 1 1



1000 0 1000 2000
 Scale in Feet

5 YEAR FLOODS

FLOOD CONTROL DISTRICT
 OF MARICOPA COUNTY
 ENGINEERING DIVISION

ELLIOT ROAD DETENTION BASINS AND OUTFALL CHANNEL
 FCD 98-44

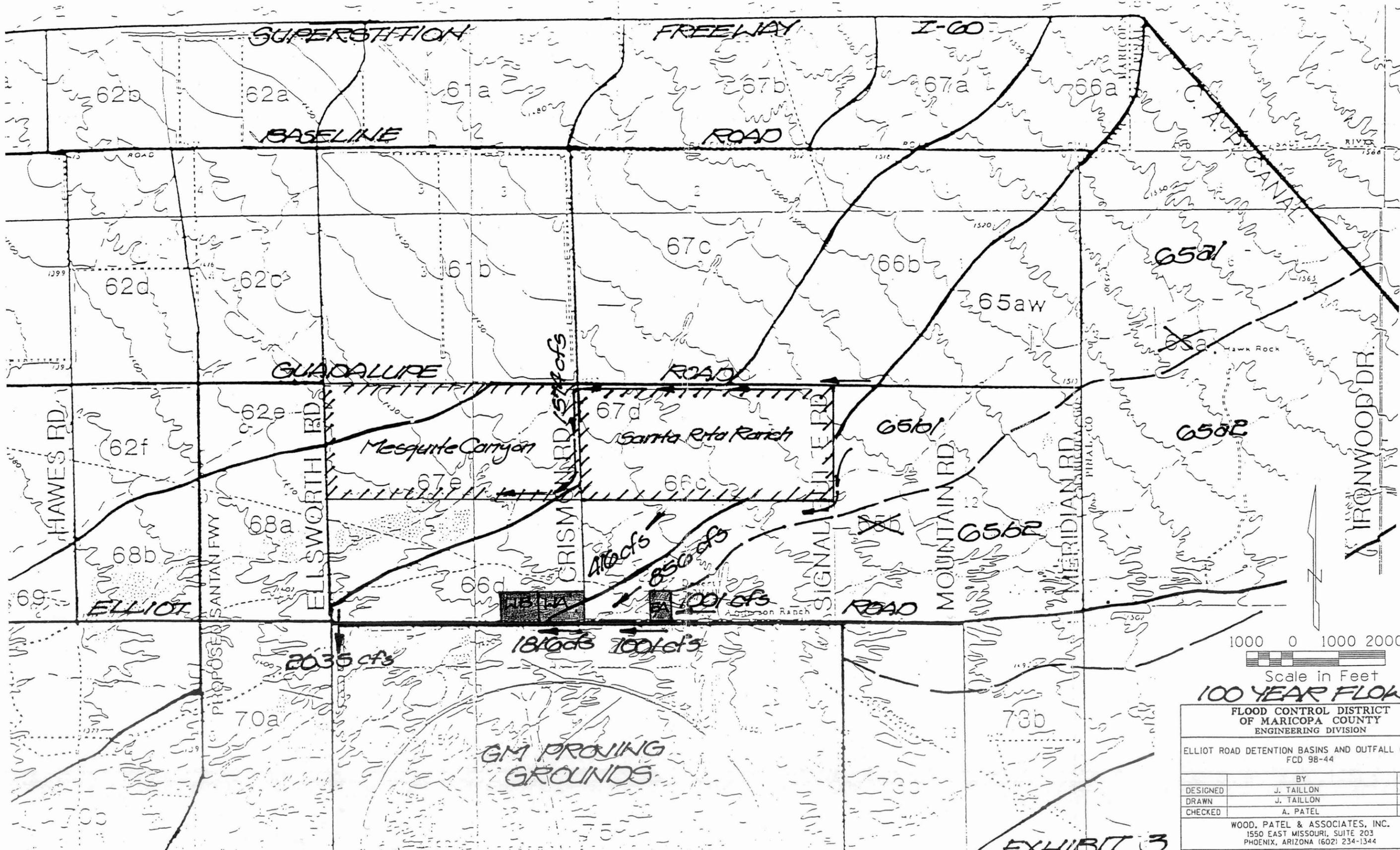
| | BY | DATE |
|----------|------------|-------|
| DESIGNED | J. TAILLON | 11/99 |
| DRAWN | J. TAILLON | 11/99 |
| CHECKED | A. PATEL | 11/99 |

WOOD, PATEL & ASSOCIATES, INC.
 1550 EAST MISSOURI, SUITE 203
 PHOENIX, ARIZONA (602) 234-1344

INTERIM CONDITION
 HYDROLOGY

SHEET OF
 1 1

EXHIBIT 2



1000 0 1000 2000
 Scale in Feet
100 YEAR FLOWS

FLOOD CONTROL DISTRICT
 OF MARICOPA COUNTY
 ENGINEERING DIVISION

ELLIOT ROAD DETENTION BASINS AND OUTFALL CHANNEL
 FCD 98-44

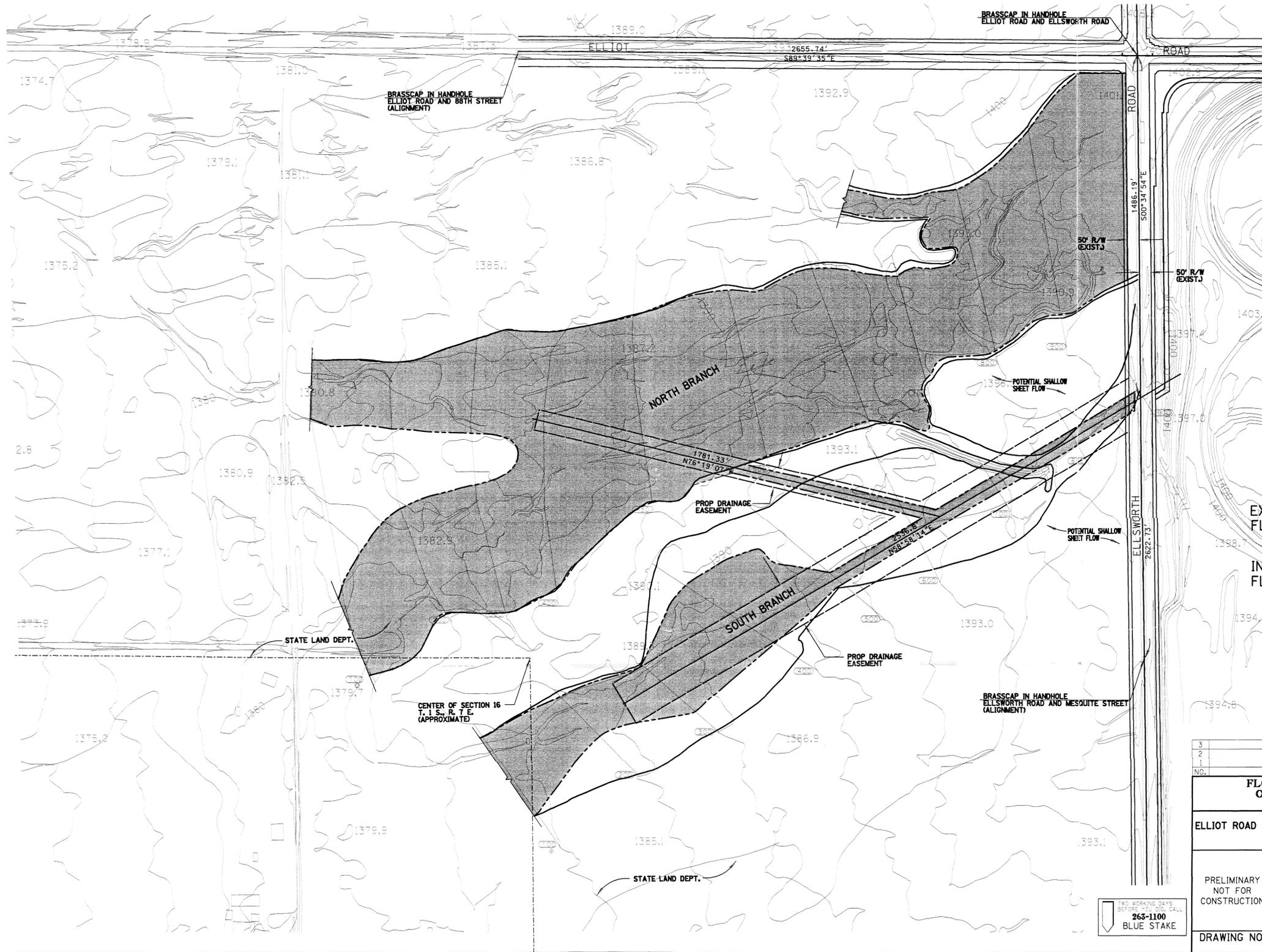
| | BY | DATE |
|----------|------------|-------|
| DESIGNED | J. TAILLON | 11/99 |
| DRAWN | J. TAILLON | 11/99 |
| CHECKED | A. PATEL | 11/99 |

WOOD, PATEL & ASSOCIATES, INC.
 1550 EAST MISSOURI, SUITE 203
 PHOENIX, ARIZONA (602) 234-1344

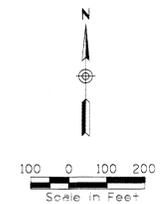
INTERIM CONDITION
 HYDROLOGY

SHEET OF
 1 1

EXHIBIT 3



RAILROAD SPIKE CENTERLINE
ELLIOT ROAD AND 96TH STREET
(ALIGNMENT)



EXISTING CONDITION (100-YR)
FLOODPLAIN LIMITS

INTERIM CONDITION (100-YR)
FLOODPLAIN LIMITS

EXHIBIT 4

| | | | |
|---|----------|---|-----------------|
| 3 | | | |
| 2 | | | |
| 1 | | | |
| NO. | REVISION | BY | DATE |
| FLOOD CONTROL DISTRICT OF MARICOPA COUNTY ENGINEERING DIVISION | | | |
| ELLIOT ROAD DETENTION BASINS AND OUTFALL CHANNEL FCD 98-44 | | | |
| PRELIMINARY NOT FOR CONSTRUCTION | DESIGNED | J. TAILLON | 1/00 |
| | DRAWN | S. RASMUSSEN | 1/00 |
| | CHECKED | A. PATEL | 1/00 |
| DRAWING NO. | | EXISTING AND INTERIM CONDITION PRELIMINARY FLOODPLAIN DELINEATIONS | SHEET OF 1 1 |

180 WORKING DAYS
BEFORE YOU CAN CALL
263-1100
BLUE STAKE

V:\1999\980510\FD\sub\FD\11s-fp.dgn

PCN