

FINAL REPORT

TASK ASSIGNMENT #1 FCD2014C001

PECOS ROAD CHANNEL AND BASIN DESIGN CONCEPT REPORT



PREPARED FOR FLOOD CONTROL DISTRICT OF MARICOPA COUNTY

JAN 2015 » PREPARED BY

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Pecos Road Channel and Basin Design Concept Report

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EXECUTIVE SUMMARY

The purpose of the Pecos Road Channel and Basin Design Concept Report (DCR) is to define a recommended drainage system to mitigate the flooding along the Pecos Road corridor between Meridian Road and Ellsworth Road in Mesa, Arizona. The alternatives developed as part of this project were based on Alternative 1 from the East Mesa Area Drainage Master Plan Update completed in February 2014 by Entellus.

Each alternative consisted of proposed channels along the Meridian Road alignment to convey runoff north and south to a proposed basin at the southwest corner of Pecos and Meridian Road. From the basin at Pecos and Meridian Roads, the following changes to the alternatives were formulated:

1. A channel on the north side of Pecos Road to convey flows from Pecos/Meridian Basin west to the Ellsworth Channel.
2. A storm drain to convey flows from Pecos/Meridian Basin west to 222nd Street to discharge to a channel along the north side of Pecos Road. The channel to convey flows to the Ellsworth Channel.
3. A storm drain to convey flows from Pecos/Meridian Basin west to a proposed basin at the northeast corner of Pecos Road and 222nd Street. The basin to outlet to a storm drain to the Ellsworth Channel.

A hydrologic and hydraulic analysis was conducted for each alternative to determine the size and cost of each alternative. Preliminary opinions of probable cost were developed for each alternative to assist in the alternatives evaluation.

The alternatives were presented to the land owners and businesses in the vicinity at a public meeting held September 18, 2014. The attendees expressed a strong unanimous preference for Alternative 3. The Flood Control District of Maricopa County (District) and the City of Mesa evaluated the alternatives using the following criteria:

- Construction cost
- Right-of-way acquisition cost
- Public/Stakeholder preferences
- Environmental and aesthetic impacts – industrial/commercial context
- Maintenance and life cycle costs

Based on a comparison of each alternative, Alternative 3 was selected to go forward as the DCR Drainage System. Further refinements were made to the hydrologic and hydraulic analysis of this alternative and a revised opinion of probable cost was developed. Several changes were made to Alternative 3 based on comments from the public meeting and review comments from the City of Mesa and the District. Conceptual design plans (15% level) were prepared for the DCR Drainage System (**Appendix H**). These concept plans identify the sizes, slopes, profiles, alignments, and cross sections of the proposed storm drain, channels and basins associated with the DCR Drainage System.

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The final DCR Drainage System consists of a proposed channel along the McKenzie Road alignment to the north and the Meridian Road alignment to the south that convey runoff to a proposed basin at the southwest corner of Pecos and Meridian Road. A storm drain conveys flows from the Pecos/Meridian Basin west to a proposed basin at the northeast corner of Pecos Road and 222nd Street. The basin drains into a storm drain to an open channel approximately 500 feet upstream of the Ellsworth Channel. The channel conveys the runoff to the Ellsworth culverts to the ultimate outfall in the Ellsworth Channel.

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1 INTRODUCTION

The objective of the Pecos Road Channel and Basin Design Concept Report (DCR) is to define a recommended drainage system to mitigate the flooding along the Pecos Road corridor between Meridian Road and Ellsworth Road in Mesa, Arizona. Kimley-Horn and Associates, Inc. (Kimley-Horn) has been retained to perform these services as part of Flood Control District of Maricopa County (District) On-Call Contract FCD 2014C001-1. The City of Mesa is a stakeholder on this project and has provided input and feedback on the alternatives development.

The Pecos Road alignment from Meridian Road to Ellsworth Road is subject to frequent flooding and road closures. This project will advance concepts developed as part of the East Mesa Area Drainage Master Plan Update (EMADMPU) to define a recommended drainage system to mitigate the flooding along this corridor.

2 PROJECT AND DESIGN CRITERIA

The alternatives for this project were developed for the future conditions 100-year, 24-hour storm event, with the Arizona Department of Transportation (ADOT) State Route 24 (SR-24) completed. The following constraints were also used in the alternative development and evaluation:

- Minimize the size of the channel or storm drain through the selection of the most hydraulically efficient materials and cross section
- Maximize the use of the Ellsworth Road Channel
- Do not exceed the capacity of the Ellsworth Road Channel and Powerline Floodway downstream, with the consideration of hydrologic timing of peak flows

The City of Mesa is a stakeholder on this project. The goals of the City are to:

- Reduce the overall project footprint
- Utilize storm drain in the Pecos Corridor wherever feasibly possible
- Minimize the takes on existing right-of-way
- Maximize the use of the existing culverts at Ellsworth Road

The following design manuals, policies, and procedures were followed in the development of the alternatives:

- Drainage Policy and Standards Manual for Maricopa County, Arizona (2007)
- Drainage Design Manual for Maricopa County Volume I Hydrology (2013)
- Drainage Design Manual for Maricopa County Volume II Hydraulics (2013)
- Drainage Design Manual for Maricopa County Volume III Erosion Control (2013)
- Policy for the Aesthetic Treatment and Landscaping of Flood Control Projects (1992)

3 HYDROLOGY

This section includes a discussion of the hydrology completed for the Alternative Analysis. Discussion of the modifications to the Alternative Analysis hydrology that were completed for the DCR Drainage System is included in Section 6.1.

The future conditions 100-year, 24-hour HEC-1 model that was developed as part of the EMADMPU Alternative 1 was modified and used to evaluate the alternatives. Areas outside of the Pecos Road DCR study area were removed from the EMADMPU model. This generally includes areas north of the future SR-24 alignment, south of the East Ranch Road alignment (2,300 feet south of Germann Road), and west of Ellsworth Road. The model was also modified to provide storage routing for the proposed Pecos/Meridian Basin in place of a diversion. The basin depth was decreased from ten feet so that the basin would be able to be fully drained by gravity outflow.

The City of Mesa conducted an analysis of their retention storage requirements concurrent to the beginning of this study. The goal was to determine whether the 100-year, 2-hour retention requirements should be based on NOAA 14 values (2.2 inches) or the older NOAA 2 value (2.7 inches). It was determined that future retention requirements in this project area that is within the City of Mesa limits will be based on 2.7 inches of rainfall. The EMADMPU Alternative 1 HEC-1 model already accounted for this retention requirement so no additional changes were made to the model.

This modified hydrology model was used to evaluate the alternatives. Changes were limited to parameters that were significantly relevant to the performance of the alternatives. See **Appendix A** for the HEC-1 schematic and **Appendix B** for hydrology models.

4 HYDRAULICS AND SEDIMENTATION

This section includes a discussion of the hydraulics for the Alternative Analysis only. Discussion of the modifications to the hydraulics that were completed for the DCR Drainage System is included in Section 6.2.

Preliminary channel hydraulic calculations were completed using normal depth calculations in FlowMaster. Channel slopes were approximated by dropping the upstream elevation to appropriately capture flow while maintaining the existing downstream elevation. Drop structures were applied in the design where necessary to maintain Froude numbers less than 0.86 per District guidelines (Section 6.8.3 of the Policy and Standards Manual). Manning's n-values were obtained from Table 7.6 of the District's Drainage Design Manual – Hydraulics (2013). Three different channel types were used based on the zoning. Concrete channels were used in industrial areas, riprap channels were used in mixed use areas and an existing earthen channel was analyzed west of Matheson Gas (Note this channel was not used in the DCR Drainage System, a new channel was proposed east of Meridian Road, see Section 6.2). The channels were designed with a foot of freeboard.

Preliminary storm drain hydraulic calculations were performed using StormCAD. The storm drain slope was approximated by setting the upstream elevation to match the bottom elevation of the proposed Meridian and 222nd Street detention basins and using the existing downstream elevation of the Ellsworth culverts. Junction losses were not modeled for each alternative but the hydraulic grade line was kept no less than two feet below ground to allow for losses. Losses were modeled for the DCR Drainage System storm drain, as discussed in **Section 6.2**. The tailwater condition was calculated by comparing water surface elevations at the locations presented in **Table 1**. The headwater at the upstream end of the Ellsworth Channel resulted in the highest tailwater, which was used for the storm drain model.

Table 1. Tailwater Determination for DCR Drainage System Storm Drain

Location	Elevation [ft]
In Ellsworth Channel downstream of the Ellsworth culverts	1384.10
Headwater at the upstream end of the Ellsworth Channel using HY-8 and the DCR Drainage System flow	1384.51
Normal depth in the outfall channel downstream of the DCR Drainage System outlet	1381.23

Stage-storage-discharge rating tables were developed assuming a flat basin bottom with 4:1 side slopes. The average-end area method was used to determine the volume. The discharge was calculated using the Manning’s equation until the depths reached 1.2 times the height of the outlet. The orifice equation was used for greater depths. The basin was designed with a foot of freeboard. Hydraulic calculations are included in **Appendix D**.

The District provided a planning-level sedimentation memo for the basin at Pecos and Meridian. A more detailed analysis should be completed at final design to quantify anticipated sedimentation amounts and future maintenance plans and needs. The analysis was based on a future conditions flow of 697 cfs obtained from the EMADMPU. The annual sediment yield is 0.087 ac-ft and the 100-year sediment yield is 1.582 ac-ft. A copy of the Sediment Yield Drainage Memo is provided in **Appendix E**. No information was provided for the 222nd Street basin and should be completed for final design.

5 ALTERNATIVE ANALYSIS

Alternative 1 of the EMADMPU was used as the starting point for the alternatives development. This baseline alternative consisted of the following drainage elements:

- Meridian Channel
- Pecos/Meridian Basin
- Pecos Channel

The proposed Meridian Channel in the EMADMPU was divided into two segments: the north segment, which extends from the proposed SR-24 alignment to the Pecos/Meridian Basin,

and the south segment, which extends from approximately 5,000 feet south of Germann Road to the Pecos/Meridian Basin. The proposed top width for the north segment was 120 feet, while the south segment varied from 50 to 110 feet, depending on the location. The total right-of-way for the Meridian Channel, which included a 14-ft maintenance road and 10-ft landscape setbacks on both sides of the channel, varied from 105 to 150 feet. Runoff is conveyed in the Meridian Channel to the Pecos/Meridian Basin.

The proposed EMADMPU Pecos/Meridian Basin was to be an offline detention basin located at the southwest corner of Pecos Road and Meridian Road. The basin was to be 10 ft deep with a capacity of 150 ac-ft. Runoff was discharged from the Pecos/Meridian Basin to the Pecos Channel.

The proposed Pecos Channel was planned to convey runoff from the Pecos/Meridian Basin west to the existing Ellsworth Channel. The proposed channel was to be located on the south side of Pecos Road from the Pecos/Meridian Basin to Crismon Road. At Crismon Road, the Pecos Channel crossed under Pecos Road to the north side of Pecos Road to the Ellsworth Channel. The proposed top width for the Pecos Channel varied from 85 to 105 feet. The total right-of-way width varied from 160 to 185 feet, which included a 14-ft maintenance road and 30-ft landscape setbacks on both sides of the channel.

With the City of Mesa's project goals in mind, the baseline alternative was modified with the consideration of channels, storm drains, additional detention basins, and alignment. A meeting was held on August 4, 2014 to discuss the options and develop alternatives. From the brainstorming meeting, the following alternatives were formulated:

1. A channel on the north side of Pecos Road to convey discharge from Pecos/Meridian Basin west to the Ellsworth Channel.
2. A storm drain to convey flows from Pecos/Meridian Basin west to 222nd Street and discharge to a channel along the north side of Pecos Road. The channel will convey flows to the Ellsworth Channel.
3. A storm drain to convey flows from Pecos/Meridian Basin west to a proposed basin at the northwest corner of Pecos Road and 222nd Street. The basin will outlet to a storm drain that will discharge to the Ellsworth Channel.

A preliminary evaluation of each alternative is presented in subsequent sections. Further guidelines were also established during the meeting. It was determined that to reduce the total right-of-way impacts, the landscape setbacks would be reduced to 30 ft on one side of the channel only. A concrete channel was also specified in the industrial areas, which allowed for steeper channel side slopes and a reduction in required right-of-way.

5.1 Alternative 1

Alternative 1 consisted of the following major drainage elements:

- Meridian Channel
- Pecos/Meridian Basin
- Pecos Channel

See the **Alternative 1** exhibit in **Appendix A** for an overview of the alternative. The proposed Meridian Channel was divided into two segments: the north segment, which extended from approximately 1,750 feet north of Pecos Road to the Pecos/Meridian Basin, and the south segment, from approximately 2,300 feet south of Germann Road to the Pecos/Meridian Basin. The proposed top widths for the north and south segments were 62 feet and 56 feet, respectively. The total right-of-way for the Meridian Channel, which included a 14-ft maintenance road and a 30-ft landscape setback, was 106 and 100 feet for the north and south segments, respectively.

The proposed Pecos/Meridian Basin was to be an inline detention basin located at the southwest corner of Pecos Road and Meridian Road. The basin was 7 ft deep with a capacity of 150 ac-ft. Runoff was discharged from the Pecos/Meridian Basin through a 60-in reinforced concrete pipe (RCP) to the Pecos Channel.

The proposed Pecos Channel conveyed runoff from the Pecos/Meridian Basin west to the existing Ellsworth Channel along the north side of Pecos Road. The proposed channel was concrete-lined in the industrial areas from Pecos/Meridian Basin to 222nd Street. West of 222nd Street the channel lining was riprap due to the change in zoning to mixed use. It was pointed out during the alternative review process that if this section of channel was revised to concrete there could be additional right-of-way savings. The proposed top width for Pecos Channel varied from 21 to 32 feet in the concrete segment and was 66 feet in the riprap segment. The total right-of-way width varied from 65 to 110 feet, which included a 14-ft maintenance road and a 30-ft landscape setback.

5.2 Alternative 2

Alternative 2 consisted of the following major drainage elements:

- Meridian Channel
- Pecos/Meridian Basin
- Pecos Storm Drain
- Pecos Channel

See the **Alternative 2** exhibit in **Appendix A** for an overview of Alternative 2. The proposed Meridian Channel and Pecos/Meridian Basin elements were the same as presented for Alternative 1.

The proposed Pecos Storm Drain conveyed runoff from the Pecos/Meridian Basin west to the proposed Pecos Channel along the north side of Pecos Road. The proposed storm drain was a single barrel 60-in RCP from the Pecos/Meridian Basin to Mountain Road. From Mountain Road to 222nd Avenue the storm drain increased to 2-60-inch RCP. West of 222nd Avenue the storm drain discharged to the Pecos Channel.

The proposed Pecos Channel conveyed runoff from the Pecos Storm Drain west to the existing Ellsworth Channel along the north side of Pecos Road. The proposed channel lining was riprap. The proposed top width for Pecos Channel was 66 feet with a total right-of-way width of 110 feet, which included a 14-ft maintenance road and a 30-ft landscape setback.

5.3 Alternative 3

Alternative 3 consisted of the following major drainage elements:

- Meridian Channel
- Pecos/Meridian Basin
- Pecos Storm Drain
- 222nd Street Basin

See the **Alternative 3** exhibit in **Appendix A** for an overview of Alternative 3. The proposed Meridian Channel and Pecos/Meridian Basin elements were the same as presented for Alternatives 1 and 2.

The proposed Pecos Storm Drain is divided into two segments: the east segment and the west segment. The east segment conveyed runoff from the Pecos/Meridian Basin west to the proposed 222nd Street Basin along the north side of Pecos Road. The proposed storm drain was a single barrel 60-in RCP from the Pecos/Meridian Basin to Mountain Road. From Mountain Road to the 222nd Street the storm drain increased to 2 – 60-inch RCP. West of 222nd Street the storm drain discharged to the 222nd Street Basin. The 222nd Street Basin discharged into the west segment of the Pecos Storm Drain. The west segment consisted of 2 – 72-inch RCP from the 222nd Street Basin to the existing Ellsworth Channel.

5.4 Opinions of Probable Cost

Opinions of probable cost (OPC) were determined for each of the alternatives. Construction costs were estimated for major construction items based on recent ADOT project estimates. Right-of-way costs were determined per acre, assuming a cost per acre of \$125,000. Potential utility relocations were identified based on horizontal alignments. A summary of the opinions of probable cost is presented in **Table 2**. These costs were revised for the DCR Drainage System. A more detailed analysis is included in **Appendix E**.

Table 2. Summary of Alternatives Opinions of Probable Cost

Alternative	Construction Cost [\$ MM]	Right-of-Way Cost [\$ MM]	Potential Utility Relocation Cost [\$ MM]	Total Cost [\$ MM]
1	8.7	8.1	0.093	17.8
2	9.4	7.1	0.085	17.5
3	10.7	5.3	0.160	17.2

The total cost for all three alternatives differed from Alternative 1 to 3 by \$600,000 or 3%. While Alternative 1, all channels, had lower construction cost, that was offset by the additional right-of-way cost. Alternative 3 was all storm drain within the ultimate right-of-way, so the overall right-of-way acquisition cost was less than the other alternatives. The OPC above did not include contingency or the additional cost of roadway.

6 DCR DRAINAGE SYSTEM

Kimley-Horn and the District developed a set of criteria that were used to evaluate the alternatives. These evaluation criteria were:

- Construction cost
- Right-of-way acquisition cost
- Public/Stakeholder preferences
- Environmental and aesthetic impacts – industrial/commercial context
- Maintenance and life cycle costs

A comparison of each alternative in relation to the evaluation criteria is provided in **Table 3**.

Table 3. Alternatives Comparison

Criteria	Alternative 1	Alternative 2	Alternative 3
Construction cost	Lowest cost	Medium cost	Highest cost
Right-of-way acquisition cost	Highest cost	Medium cost	Lowest cost
Public/Stakeholder preference	City and public prefer storm drain	City and public prefer storm drain	City and public prefer storm drain
Environmental and aesthetic impacts	Fits in commercial context, but not as pleasing as underground pipe	Fits in commercial context, but not as pleasing as underground pipe	Most pleasing (underground)
Maintenance and life cycle costs	Highest cost	Medium cost	Lowest cost

In addition to the evaluation criteria noted above, the functionality of each alternative with a phasing plan was assessed. The extra burden required to maintain driveway culverts was considered with Alternatives 1 and 2. There was also a potential cost savings in Alternative 3 to use the earth excavated from the basins as cover for the pipes. Another important factor in making the selection of the preferred alternative was the right-of-way take. Alternative 1 had the highest take, while Alternative 3 had the lowest right-of-way take. A further savings was proposed by the District staff to revise the riprap channel west of 222nd Street to concrete to reduce the cost of right-of-way.

Based on a comparison of each alternative, Alternative 3 was selected as the DCR Drainage System. See the DCR Drainage System exhibit in **Appendix A**. In the initial evaluation of each alternative, the earthen channel west of Matheson Gas was being considered for use as the northern Meridian Channel. As part of the alternatives evaluation process, it was decided that the existing earthen channel west of Matheson Gas would not be used as the northern Meridian Channel alignment. An alternative location was selected adjacent to McKenzie Road to protect existing homes east of Meridian Road. This channel will intercept additional flow and was analyzed as a concrete channel. Landscape concepts outlined in **Section 7**

should be integrated with the design plans in final design. See Conceptual Plans in **Appendix H**.

6.1 Hydrology

Once the DCR Drainage System was selected, further refinements were made to the hydrology model to revise the storage volumes for the proposed basins at Meridian Road and 222nd Street to match the conceptual grading. The depth of the basin at Meridian Road was increased from 7 feet to 9 feet. Both basins were graded with a minimum slope of 0.15% and side slopes of 6:1. Adjustments were also made to move the subbasin boundary between E24B and E28B, E25 and E29B from Signal Butte Road to 222nd Street. Soil and land use parameters for each revised subbasin were estimated from the EMADMP shapefile data. Loss parameters and unit hydrographs for each subbasin were calculated using DDMSW. A DCR Drainage System HEC-1 Schematic showing the revised basin boundaries is provided in **Appendix A**.

Adjusting the subbasin boundary required the retention volumes for each of the modified subbasins to be revised. Because basin E25 and E24B are already partially developed with existing retention, a direct calculation of volume based on area was not done. Instead, the revised retention volumes were calculated by estimating the retention volume for the area between Signal Butte and 222nd Street. That retention volume was added to the subbasins that increased in area and subtracted from the subbasins that decreased in area. The change in retention volume was calculated by determining the retention volume per area being provided in the EMADMPU model and then multiplying by the change in area. Refined hydrology model output is included in **Appendix F**.

6.2 Hydraulics

Further refinements were also made to the hydraulic analysis. Manholes were added to the storm drain model with appropriate junction losses. Storm drain slopes were adjusted to match the revised detention basin grading. Pipes downstream of the 222nd Street basin were lowered to avoid utility conflicts where possible. Flow from the HEC-1 model was prorated based on area to calculate how much flow would be conveyed to the storm drain each quarter mile. Pipe diameters were adjusted based on the refined flow calculations, larger pipes were designed to replace some double pipes. Lowering the storm drain and revising double pipes to larger single diameter pipes resulted in approximately \$2 MM in cost savings.

The outfall channel between the storm drain and Ellsworth Road is an earthen channel with riprap side slopes. Riprap was sized assuming a maximum velocity of 9 fps. There may be opportunity to reduce the riprap size with a riprap basin and final design of the storm drain. Refined hydraulic calculations are included in **Appendix F**. In most locations runoff will enter all of the proposed channels as sheet flow perpendicular to the channel. In these areas collector v-ditches or swales at the upstream side of the channel bank could be beneficial to aid in reduction of erosion or undercutting of the side slopes of the channels. This concept could be evaluated in final design.

The impacts to the Ellsworth Channel were also assessed by modifying the flow in the EllsworthChannel.prj HEC-RAS model provided from the *Final Drainage Report, Ellsworth Road – Phase I – Germann Road to Ray Road* (Ellsworth Road Drainage Report). According to the Ellsworth Road Drainage Report, this model represents the ultimate design conditions with full CIP flows included. Due to the attenuation of flow in Ellsworth Channel and the timing of peak flows, the flow decreases in Ellsworth Channel downstream of Pecos Road. The flow at Pecos Road was modeled for the entire channel. Because the flows do not increase downstream of Pecos Road, the Ellsworth Channel capacity is not exceeded. The revised HEC-RAS model is provided electronically with this report.

6.3 Implementation Plan

The DCR Drainage System may be implemented in four phases, see **Table 4** and **Appendix A** for the DCR Drainage System with Implementation Phasing exhibit. This phasing plan would allow the infrastructure to be built in stages, which may assist in project funding. It also provides an opportunity to build the highest priority drainage elements first. Because the most downstream elements are not built first, an interim outlet structure will be needed at the basin at Pecos and Meridian.

Table 4. Phases of the Implementation Plan for the DCR Drainage System

Phase	Features
Phase 1	<ul style="list-style-type: none"> • Detention basin at the southwest corner of Pecos and Meridian Roads • Northern Meridian Road channel segment
Phase 2	<ul style="list-style-type: none"> • Detention basin at 222nd Street and Pecos Road • Storm drain and channel from the 222nd Street detention basin to Ellsworth Road
Phase 3	<ul style="list-style-type: none"> • Storm drain from the detention basin at Meridian Road west to the 222nd Street basin
Phase 4	<ul style="list-style-type: none"> • Southern segment of the Meridian Road channel

An alternative implementation plan could follow a more traditional approach to build the system from the downstream portion first, see **Table 5**.

Table 5. Traditional Implementation Plan for the DCR Drainage System

Phase	Features
Phase 1	<ul style="list-style-type: none"> • Detention basin at 222nd Street and Pecos Road • Storm drain and channel from the 222nd Street detention basin to Ellsworth Road
Phase 2	<ul style="list-style-type: none"> • Detention basin at the southwest corner of Pecos and Meridian Roads • Southern segment of the Meridian Road channel • Storm drain from the detention basin at Meridian Road west to the 222nd Street basin
Phase 3	<ul style="list-style-type: none"> • Northern Meridian Road channel segment

The greatest disadvantage to following this traditional implementation plan is that the basin at Pecos and Meridian, which provides the most significant benefit to the area, is not built in the first phase. Instead, the first phase focuses on the downstream area which is not yet developed and where there is not as great of an immediate concern to relieve flooding.

A revised OPC was prepared for the DCR Drainage System based on the refinements and modifications discussed. The cost of each phase is provided as well as the overall project cost. A summary of the revised OPC is provided in **Table 6** and a detailed OPC is included in **Appendix F**.

Table 6. Summary of DCR Drainage System Opinion of Probable Cost

Phase	Construction Cost [\$ MM]	Potential Utility Relocation Cost [\$ MM]	Right-of-Way Cost [\$ MM]	Total Cost [\$ MM]
1	3.7	0.03	5.4	10.2
2	3.4	0.05	1.3	5.8
3	1.9	0.22	0.0	2.7
4	3.0	0.01	1.6	5.6
Total	12.1	0.30	8.3	24.3

The primary increases in cost from the Alternatives Analysis costs in **Table 2** are detailed in **Table 7**.

Table 7. Changes to OPC from Alternatives Analysis to the DCR Drainage System

Item	Reason for Change
Channel Excavation	<ul style="list-style-type: none"> • Meridian North Channel is now longer. • More refined grading was prepared that includes daylighting to existing ground.
Earthwork for Retention Basins	<ul style="list-style-type: none"> • Pecos Basin is deeper to help with peak flow attenuation. • More refined grading with sloping basin bottoms.
Riprap, D ₅₀ =9 inches	<ul style="list-style-type: none"> • Added to plan for the outfall channel near Ellsworth Road.
Reinforced concrete channel, 6 inches thick	<ul style="list-style-type: none"> • Meridian North Channel is now concrete and longer. Includes 90 degree bend into Pinal County.
24" RGRCP, Class IV – Area Drain Laterals	<ul style="list-style-type: none"> • An allowance was added to the OPC for future laterals.
Storm Drain	<ul style="list-style-type: none"> • Storm drain downstream of 222nd Street basin lowered and revised from double to single larger pipe where practical.
ROW Cost	<ul style="list-style-type: none"> • Meridian North Channel is longer and is now farther east from Pecos Road Basin, into Pinal County.
20% Contingency	<ul style="list-style-type: none"> • Added to OPC.

7. LANDSCAPE CONCEPTS

7.1 Introduction

As described in the Policy for the Aesthetic Treatment and Landscaping of Flood Control Projects (December 16, 1992), Landscape Aesthetics & Multiple-Use Design Guidelines for Flood Control Basins, Channels, and Flood Retarding Structures (December 23, 2004), and other various Context Sensitive Flood Hazard Mitigation design approach documents, the District Policy is to consider and incorporate aesthetic treatment in the design of new structures. The Policy provides direction for the development of aesthetic features and the allowable limits for funding these enhancements. The key is to integrally incorporate enhancements such as revegetation efforts (tall pot trees, native seed, salvage plants), earthwork and landform contouring, and bio-swales and rainwater harvesting swales to improve project aesthetics and enhance revegetation. Structural aesthetic treatments include the use of concrete form liners, organic shaped structures, integral color rip rap, and the use of a desert varnish stain or paint to provide a natural coloration to built objects. Basins can be screened by landscape screening, more effectively achieved with right of way acquisition to provide adequate buffer widths. Treatments can also apply to channels, in the way of side slope and channel meandering.

Important in the evaluation of design approaches is the context in which the project will exist. Both the current and future context are important in assessing the potential visual impact of the work. Since flood control projects are long term public works projects and exist for an indefinite amount of time, the initial investment in aesthetic improvements and revegetation can be shown to pay off over the lifetime of the project. Simple approaches such as easing the steepness of a sideslope can effect a profound visual improvement.

Other approaches that do have a positive visual impact come from the need to prevent erosion. Effective erosion control techniques are used integrally within the site, not just at the site perimeter, and are woven into the project design. These techniques include the use of seed mix and tall pot planting to reestablish vegetation on fresh earth, the use of angular rip rap on slopes or concentration points, building terraced or benched slopes, the use of wattles or erosion control fabric on exposed earth slopes to control water movement, the use of a low flow channel with higher earth mounds adjacent to it, and finally the use of a customized seed mix based on site specific study and observation. The goal is to create a native plant composition that seamlessly blends into the natural context.

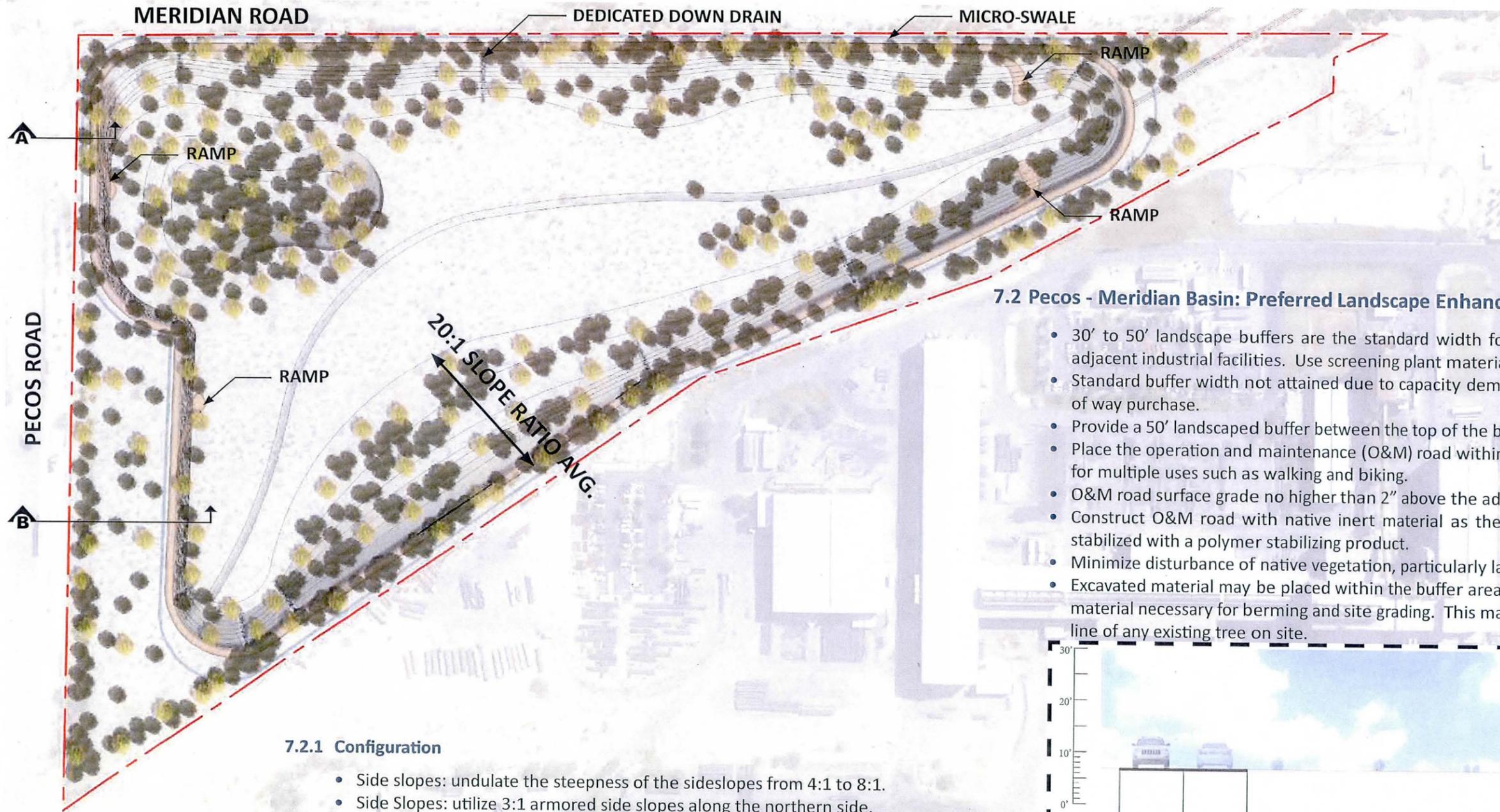
The Pecos Road project area will consist of two large detention basins and several channels conveying stormwater into and between the basins, then onward to the rest of the stormwater management system. Each basin will have an inlet point or two, and one outletting point. These points are anticipated to be constructed of concrete, necessary due to the volume and velocity of the flowing water. The size, shape, location, and composition of basins and channels present certain opportunities and constraints that may be possible for this project.

7.1.1 Opportunities

- Location: the project area is in eastern Maricopa County, an area that receives more rain than other areas in the county, which increases the potential success of revegetation approaches.
- Location: this site is adjacent to a large area of State Land, which can currently be accessed for equestrian and recreational use by permit.
- Recreation: the project area will create areas that can support passive recreation such as walking, hiking, and birdwatching.
- Vegetation: the project construction activities may be able to preserve some existing plant materials.
- Vegetation: when preservation is not possible the project construction, may be able to salvage and replant healthy plant material.
- Vegetation: the project will provide opportunities for collection and salvaging site seed, then and hand broadcasting in select areas to promote revegetation.
- Rainwater harvesting: the project can employ undulation of the ground plane, which can yield different amounts of captured rainwater and therefore non-uniform densities of vegetation.

7.1.2 Constraints

- Site Area: Available area is limited to the current available site. The City of Mesa would like to minimize the take of additional right of way.
- Budget: the budget is to be focused on executing the flood hazard mitigation demands of the project.
- Site Area: the site is projected to be sufficient in size for flood mitigation with a 15-ft perimeter buffer, not the 30 – 50 ft buffer specified in the Landscape Aesthetics & Multiple-Use Design Guidelines for Flood Control Basins, Channels, and Flood Retarding Structures.
- Recreation: the site is not near regional trail corridors, nor other heavily used areas such as parks, bodies of water, or other open spaces.
- Future Uses: the site is bounded on one side by State Land. While that land is currently open space, the future development timeline and development type is undetermined, and this future use may be a detriment to the natural and aesthetic quality of this Pecos Road project).
- Industrial Context: the industrial context, both current and future projected land uses, do not provide incentive to the District or local partners to embellish the aesthetic enhancements of these sites.

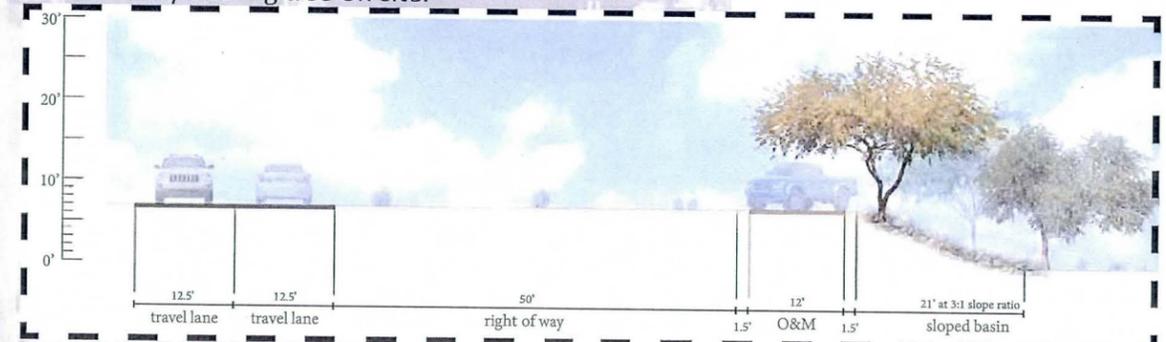


7.2 Pecos - Meridian Basin: Preferred Landscape Enhancement Techniques

- 30' to 50' landscape buffers are the standard width for screening hardened facilities and adjacent industrial facilities. Use screening plant material, berms, and micro basins.
- Standard buffer width not attained due to capacity demand of basin and no additional right of way purchase.
- Provide a 50' landscaped buffer between the top of the basin and adjacent development.
- Place the operation and maintenance (O&M) road within the buffer area and design to allow for multiple uses such as walking and biking.
- O&M road surface grade no higher than 2" above the adjacent grade.
- Construct O&M road with native inert material as the finished surface. Material will be stabilized with a polymer stabilizing product.
- Minimize disturbance of native vegetation, particularly large trees, in the buffer zone.
- Excavated material may be placed within the buffer area to reduce the quantity of imported material necessary for berming and site grading. This material should be kept out of the drip line of any existing tree on site.

7.2.1 Configuration

- Side slopes: undulate the steepness of the sideslopes from 4:1 to 8:1.
- Side Slopes: utilize 3:1 armored side slopes along the northern side.
- Undulate the sides of the basin, every 300' to 500'.

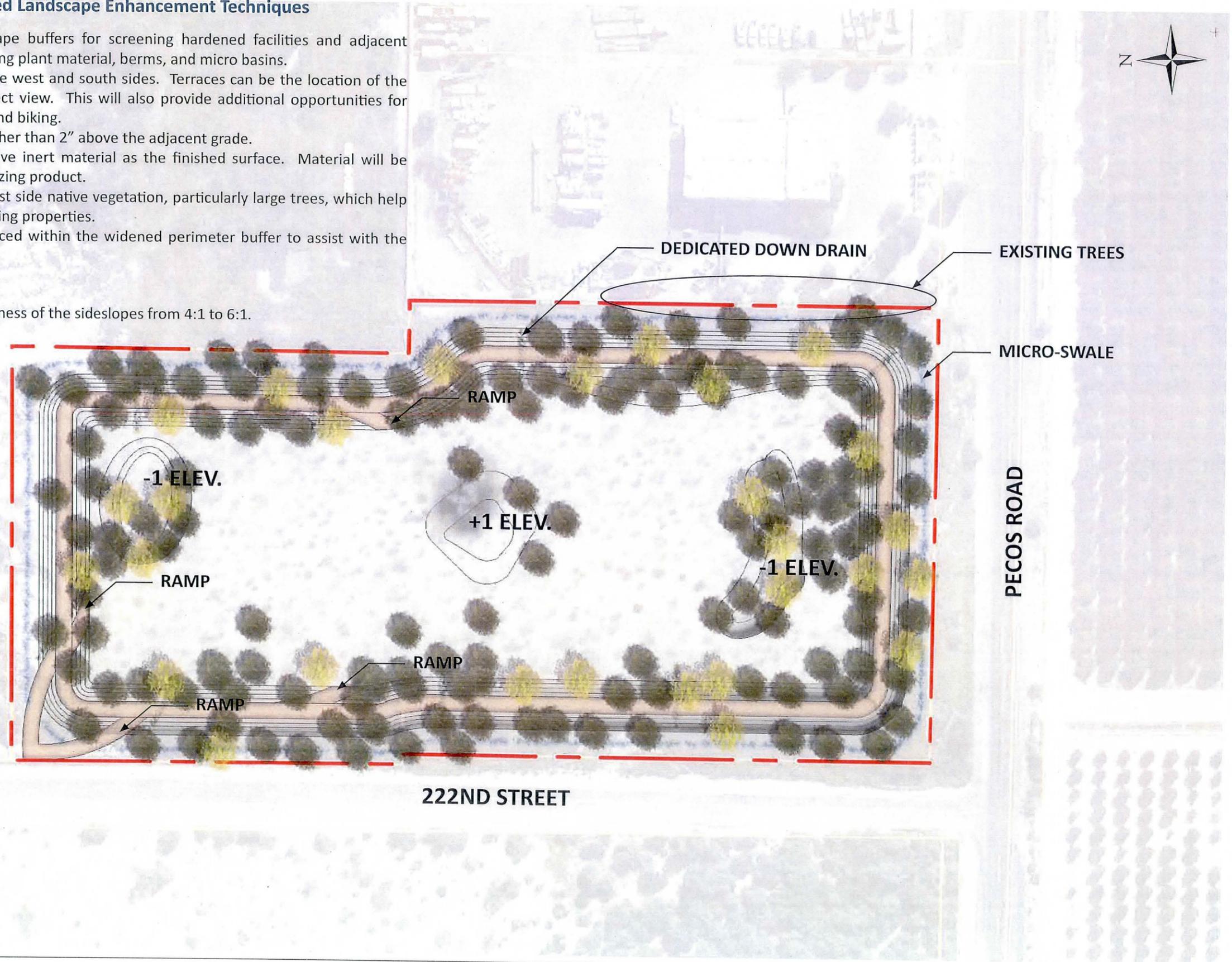


7.3 Pecos - 222nd St Basin: Preferred Landscape Enhancement Techniques

- Incorporate 30' to 50' landscape buffers for screening hardened facilities and adjacent industrial facilities. Use screening plant material, berms, and micro basins.
- Provide a terraced buffer on the west and south sides. Terraces can be the location of the O&M road to screen from direct view. This will also provide additional opportunities for multiple uses such as walking and biking.
- O&M road surface grade no higher than 2" above the adjacent grade.
- Construct O&M road with native inert material as the finished surface. Material will be stabilized with a polymer stabilizing product.
- Minimize disturbance of the east side native vegetation, particularly large trees, which help screen the basin from neighboring properties.
- Excavated material may be placed within the widened perimeter buffer to assist with the undulation of the basin form.

7.3.1 Configuration

- Side slopes: undulate the steepness of the sideslopes from 4:1 to 6:1.
- Side Slopes: utilize a terraced approach on west and southern sides.
- Undulate the sides of the basin, every 300' to 500'.
- Dedicated down drains
- Rainwater harvesting micro-swale at basin rim



7.4 Both Basins and Channels

7.4.1 Pre-Construction Activities

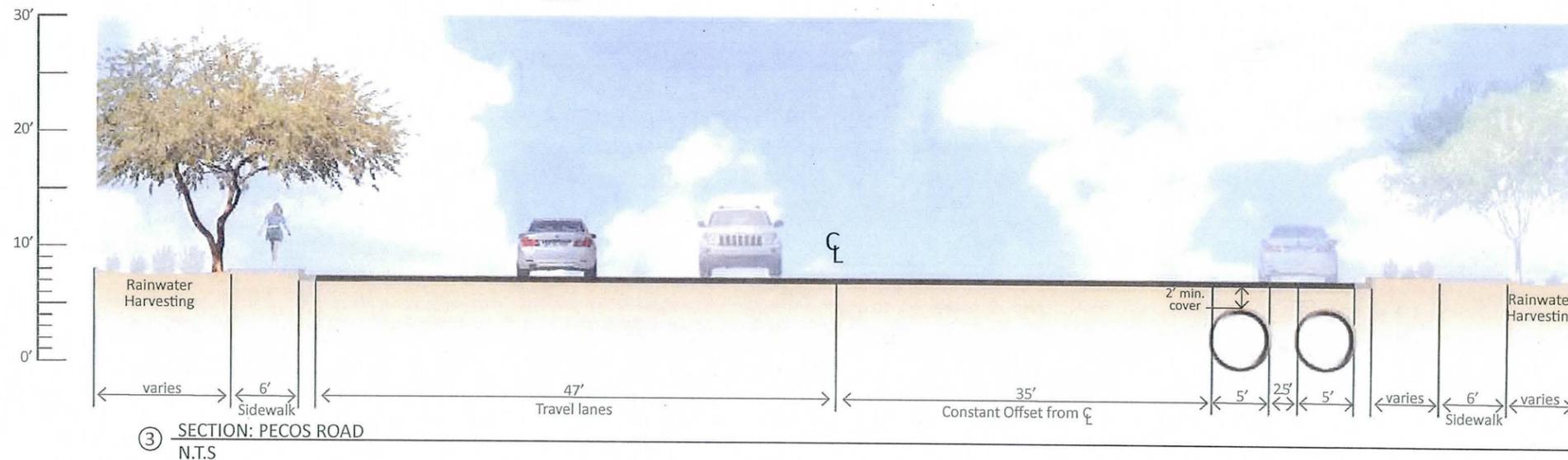
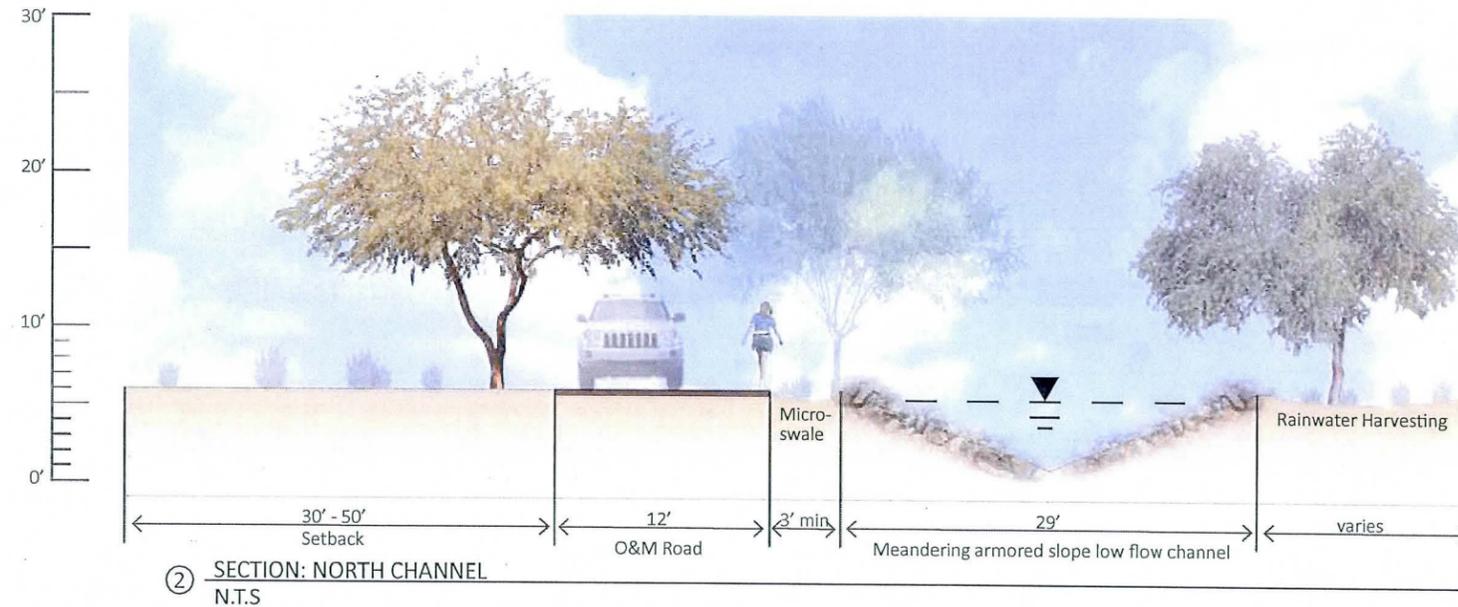
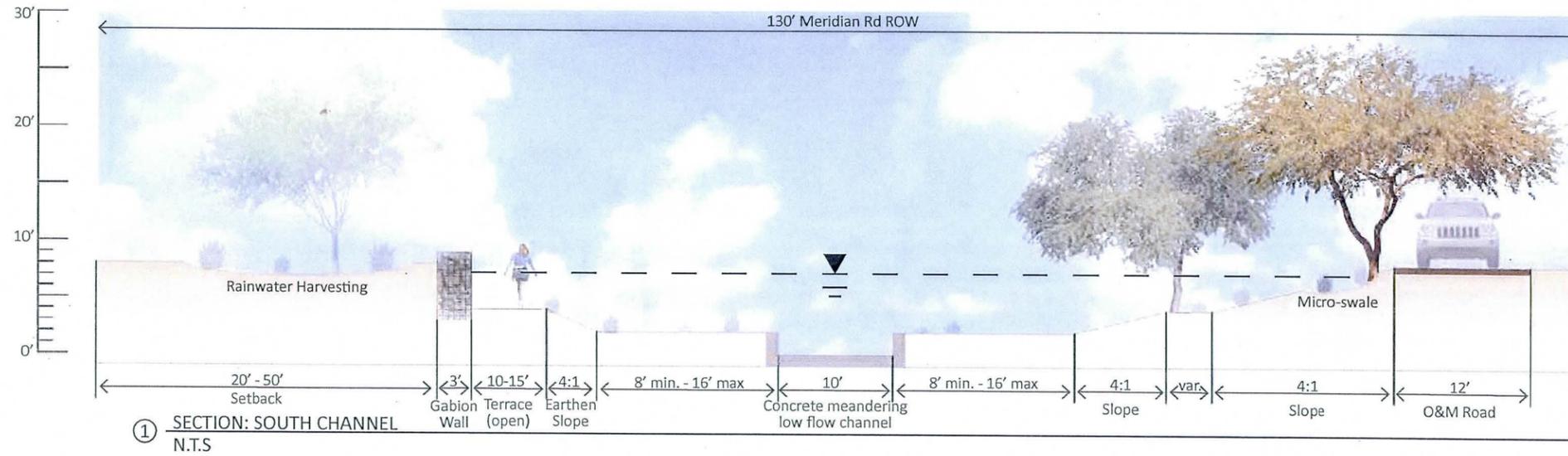
- Inventory existing trees at perimeter of site to determine which, if any, areas should be preserved from disturbance.
- Submit a Notice of Intent to Clear to Arizona State Land Department and make the site available for native plant salvage 30 to 90 days before the start of construction. Access to the site can be limited to specific dates, times and access points.
- Stockpile site boulders from surface and excavated soil for use at basin perimeters.

7.4.2 Vegetation

- Install hydroseed and tall pot trees at densities comparable to the existing perimeters. These basins are not temporary basins and therefore can be revegetated.
- Revegetation will not be supported by supplemental irrigation.
- Use Sonoran desert plant material in landscape buffer. A plant list has been developed for this project, and will utilize tall pot trees and native desert shrubs known to germinate from seed mix.
- Plant List includes plants identified as appropriate for the Natural Sonoran Desert Hydriparian character unit.
- Select specific species native to the basin locations to respond to the context of the landscape character.
- Salvage native trees and plants including Saguaro and small cactus species. Maintain for replanting in the landscape or make available for sale by auction.
- Design the buffer landscape to transition the density, type, size, form, color, and texture of the plant material with the species found in the surrounding landscape.
- Locate vegetation along both sides of the O&M road to break the view of the line of the road alignment and provide shade.
- Trees, shrubs, and groundcovers should be arranged in an irregular pattern along the sides, bottom, and top of the basin side slopes to complement the character of the surrounding natural landscape.

7.4.3 Inlet / Outlet Structures

- Design the structures to use the materials, shapes, colors, and textures that blend with the surrounding desert.
- Colors of materials should blend with the desert's darker color tones.
- Design structures using form liners to provide textures to blend with surrounding desert.



- Concrete low flow necessary due to flat site.
- Gabion wall necessary to provide area for terrace.
- 130' ROW.
- Micro-swales in the buffer areas for erosion protection, water harvesting, and vegetation reestablishment.

- 44' ROW needed.
- Revegetation needed outside of ROW.
- Setback not in ROW.

- RCP are constantly 35' north of ROW center line.
- RCP are located under 2'-0" of cover.
- Width assumes Mesa's widest arterial, per Mesa Transportation Plan.

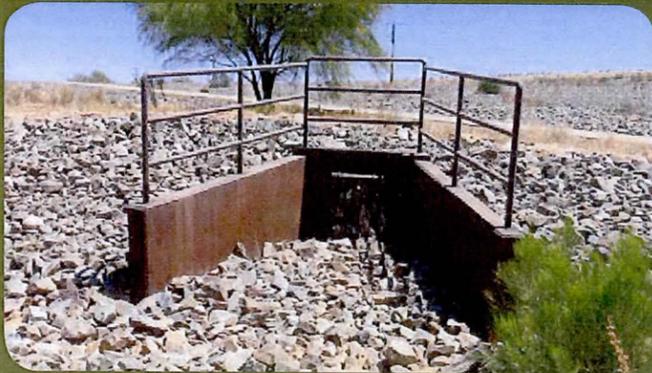
WALLS



FORMLINED NATURAL CONCRETE



ROCK FILLED GABION WALLS



NATURAL COLORED HEADWALL / WINGWALL

RIP RAP



NATURAL DARK COLOR



CONTEXT COLOR WITH MIXED SIZE



RIP RAP AND GROUNDPLANE COLOR

DECOMPOSED GRANITE



COLOR SELECTION

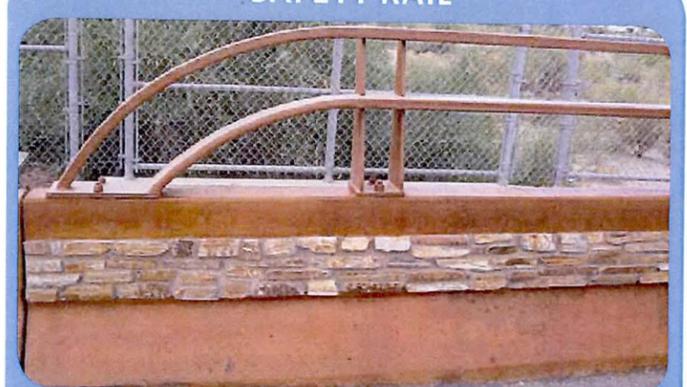


EROSION PROTECTION



STABILIZED FOR ACCESS WAYS

SAFETY RAIL



ORGANIC GEOMETRIES



BROWN COLORS



UNOBTRUSIVE

HYDRORIPARIAN

XERORIPARIAN

TREE



CATCLAW ACACIA
Acacia constricta

Yellow puffballs are fragrant and are formed in clusters

SHRUBS



HACKBERRY
Celtis spp

Attractive orange berries, excellent wildlife plant

WILDFLOWER



DESERT MARI GOLD
Baileya multiradiata

Undemanding, reseeds easily, long period of color

SHRUBS



BRITTLE BUSH
Encelia farinosa

Blooms are yellow and daisylike winter - spring, seeds attract birds

TREE



WHITETHORN ACACIA
Acacia constricta

Great for naturalistic landscapes, attracts birds



IRONWOOD TREE
Olneya tesota

Bears masses of 1/2" wide lavender-pink blossoms in late spring



WOLFBERRY
Lycium berlandieri

Long lived shrub, produces red berries for consumption by wildlife



SACRED DATURA
Datura wrightii

Boasts ornamental flowers that are sweetly fragrant



CREOSOTE
Larrea tridentata

Fragrant with rain, yellow flowers early spring and with monsoons



IRONWOOD TREE
Olneya tesota

Fine textured gray-green foliage, flowers dusty lavender late spring



NETLEAF HACKBERRY
Celtis reticulata

Birds relish the tiny red berries, nubby protrusions form on bark



GRAYTHORN
Zizyphus obtusifolia

Great for wildlife, blue-black fruits attract birds



DESERT GLOBE MALLOW
Sphaeralcea ambigua subsp. Ambigua

Orange, white, pink, or lavender blooms in the spring



DESERT BROOM
Baccharis sarothroides

Female plants develop dense clusters of white cottony seeds



VELVET MESQUITE
Prosopis velutina

Yellow catkinlike flower clusters hang from branches in spring



VELVET MESQUITE
Prosopis velutina

Excellent wildlife plant, larger thorns in its early years



FOUR WING SALT BUSH
Atriplex canescens

Tolerates tough conditions, excellent wildlife plant



DESERT SENNA
Cassia covesii

Showy flowers occur mostly after spring and summer rains



TRIANGLE LEAF BURSAGE
Ambrosia deltoidea

Evergreen perennial, great for erosion control



BLUE PALO VERDE
Parkinsonia florida

Vivid spring color, nesting for birds

7.5 Plant List

HYDRORIPARIAN	
Trees	
Catclaw Acacia	<i>Acacia greggii</i>
Netleaf Hackberry	<i>Celtis reticulata</i>
Ironwood tree	<i>Olneya tesota</i>
Velvet Mesquite	<i>Prosopis velutina</i>
Shrubs	
Triangle leaf Bursage	<i>Ambrosia deltoidea</i>
Four wing Saltbush	<i>Atriplex canescens</i>
Desert Broom	<i>Baccharis sarothroides</i>
Hackberry	<i>Celtis spp</i>
Wolfberry	<i>Lycium berlandieri</i>
Graythorn	<i>Zizyphus obtusifolia</i>
Wildflowers/Forbs	
Desert Marigold	<i>Baileya multiradiata</i>
Sacred Datura	<i>Datura wrightii</i>
Arizona evening primrose	<i>Oenothera arizonica</i>
Arrow-weed	<i>Pluchea sericea</i>
Desert globe mallow	<i>Sphaeralcea ambigua subsp. Ambigua</i>

XERORIPARIAN	
Trees	
Whitethorn acacia	<i>Acacia constricta</i>
Ironwood tree	<i>Olneya tesota</i>
Velvet Mesquite	<i>Prosopis velutina</i>
Shrubs	
Triangle leaf Bursage	<i>Ambrosia deltoidea</i>
Desert Broom	<i>Baccharis sarothroides</i>
Brittle bush	<i>Encelia farinosa</i>
Creosote	<i>Larrea tridentada</i>
Wolfberry	<i>Lycium berlandieri</i>
Graythorn	<i>Zizyphus obtusifolia</i>
Wildflowers/Forbs	
Desert Marigold	<i>Baileya multiradiata</i>
Desert Senna	<i>Cassia covesii</i>
Sacred Datura	<i>Datura wrightii</i>
Gordon's bladderpod	<i>Lesquerella gordonii</i>
Spanish needles	<i>Palafoxia arida var. arida</i>
Desert globe mallow	<i>Sphaeralcea ambigua subsp. Ambigua</i>
Desert zinnia	<i>Zinnia acerosa</i>

• This is a partial list of plant materials to be considered in the overall design of future facilities.

8 PUBLIC INVOLVEMENT

Kimley-Horn, the District, and the City of Mesa presented the three alternatives to the land owners and businesses along the Pecos Road corridor on September 18, 2014. A summary of the project, the purpose and location were presented in addition to the general hydrology and components of each alternative. The meeting was then opened up for questions and comments from the attendees. The attendees expressed a strong unanimous preference for Alternative 3. Several questions were asked regarding the selection and timing of the improvements. Written comments were also collected at the meeting. The meeting notes, comments, and sign-in sheets are provided in **Appendix G**.

Kimley-Horn, the District, and the City of Mesa presented the DCR Drainage System 15% plans to land owners and businesses along the Pecos Road corridor on December 18, 2014. The plans were presented in roll plot format. Several questions were asked regarding the funding and timing of the improvements. In general the plan was well received by the attendees. The meeting invitation and sign-in sheets are provided in **Appendix G**.

9 SUMMARY

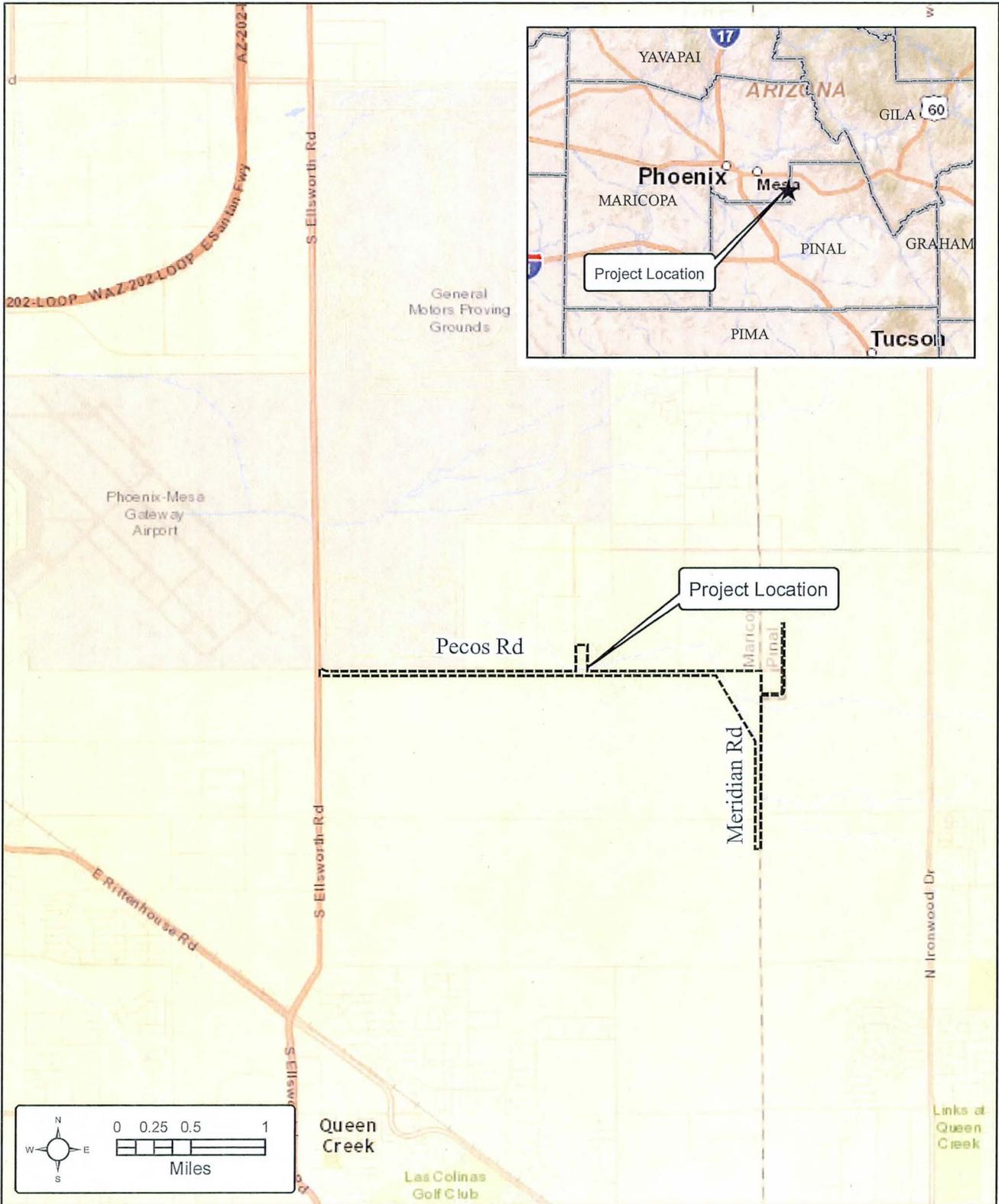
1. The DCR Drainage System meets the project objectives, including the goals outlined by the City of Mesa to reduce the overall project footprint, minimize the takes on existing right-of-way and maximize the use of the existing culverts at Ellsworth Road.
2. Offsite runoff is conveyed in proposed concrete channels along the Meridian and McKenzie Road alignments in subcritical conditions with one foot of freeboard.
3. The basin at the southwest corner of Pecos and Meridian Road attenuates flow from approximately 1160 cfs to 180 cfs. The basin was designed with a minimum slope of 0.15% and one foot of freeboard. The basin includes a concrete low flow channel.
4. The basin at the southeast corner of Pecos and 222nd Street attenuates flow from approximately 350 cfs to 215 cfs. The basin was designed with a minimum slope of 0.15% and one foot of freeboard.
5. Runoff is conveyed along Pecos Road in a storm drain within the ultimate roadway alignment. The hydraulic grade line is a minimum of one foot below the ground.
6. The opinion of probable cost for the DCR Drainage System is \$24.3M. This cost includes construction, utility relocation, right-of-way, design, and contingency costs.
7. The DCR Drainage System assumes that the future SR-24 is in place. Once it is, this project will decrease the existing runoff at Ellsworth and Pecos Road from approximately 1500 cfs to 570 cfs. The proposed discharge from Pecos Road will not negatively impact the Ellsworth Road channel or the Powerline Floodway.

10 REFERENCES

- Flood Control District of Maricopa County, *Drainage Design Manual for Maricopa County Volume I Hydrology*, August 2013.
- Flood Control District of Maricopa County, *Drainage Design Manual for Maricopa County Volume II Hydraulics*, August 2013.
- Flood Control District of Maricopa County, *Drainage Design Manual for Maricopa County Volume III Erosion Control*, August 2013.
- Flood Control District of Maricopa County, *Drainage Policy and Standards Manual for Maricopa County*, January 2007.
- Flood Control District of Maricopa County, Drainage Memo – Sediment Yield Analysis for Pecos Road Detention Basin, July 2014.
- Flood Control District of Maricopa County, East Mesa Area Drainage Master Plan Update – Hydrologic Analysis, August 2011.
- Flood Control District of Maricopa County, *East Mesa Area Drainage Master Plan Update – Proposed Alternative Development*, prepared by Entellus, February 2014.
- Flood Control District of Maricopa County, Policy for the Aesthetic Treatment and Landscaping of Flood Control Projects, December 1992.
- Maricopa County Department of Transportation, *Final Drainage Report, Ellsworth Road - Phase 1 - Germann Road to Ray Road*, prepared by Amec, May 2005.

Appendix A. Exhibits

- Location Map
- HEC-1 Schematic – Alternatives
- HEC-1 Schematic – DCR Drainage System
- Alternative 1
- Alternative 2
- Alternative 3
- DCR Drainage System
- DCR Drainage System with Implementation Phasing



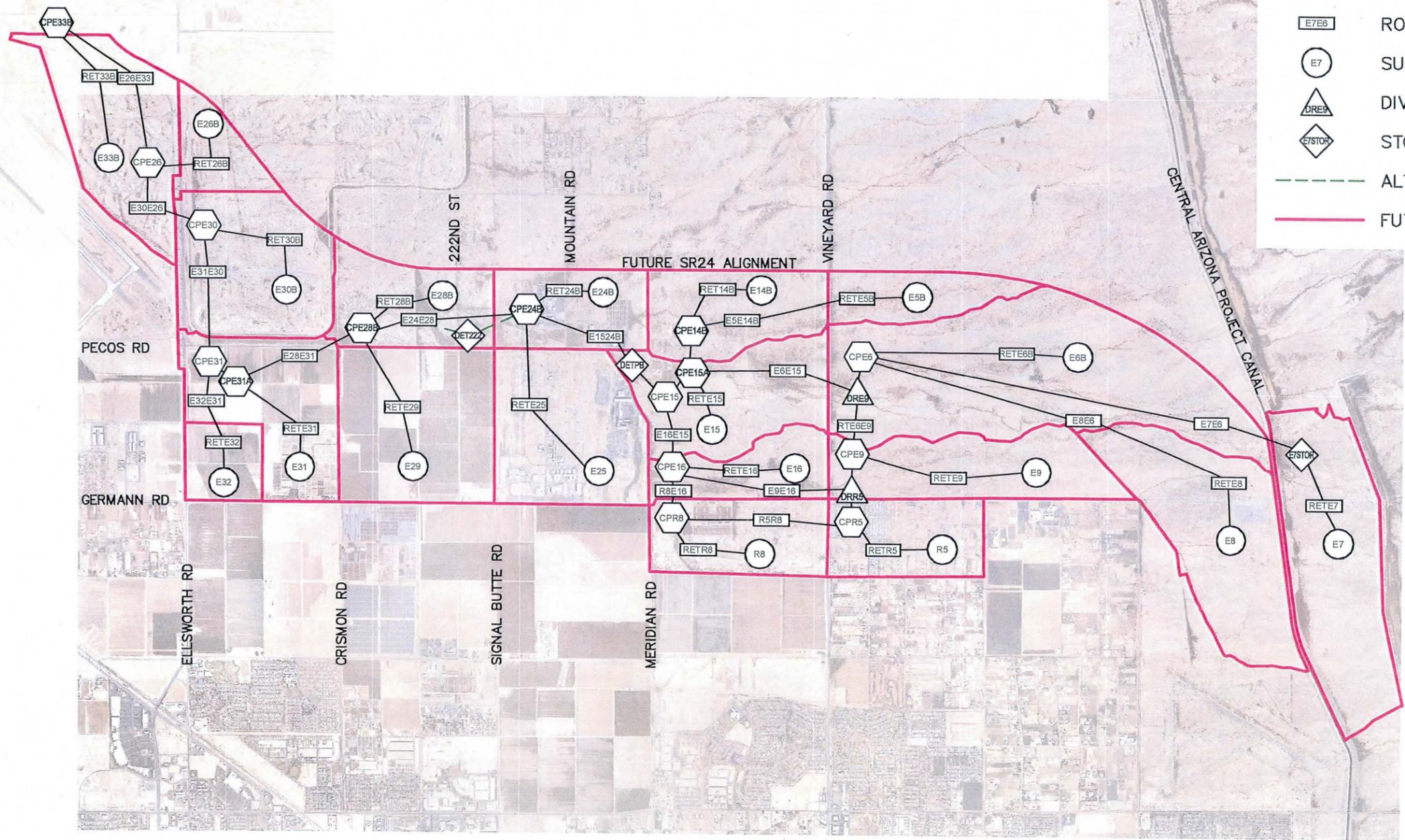
Kimley»Horn

Pecos Road Channel and Basin Design Concept Report

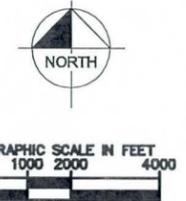
Maricopa County, Arizona

Location Map

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XREFS: XAERIAL-091131024



LEGEND	
	CONCENTRATION POINT
	RETENTION
	ROUTING PATH
	SUBBASIN
	DIVERSION
	STORAGE
	ALTERNATIVE 3 ROUTING PATH
	FUTURE SUBBASIN BOUNDARY

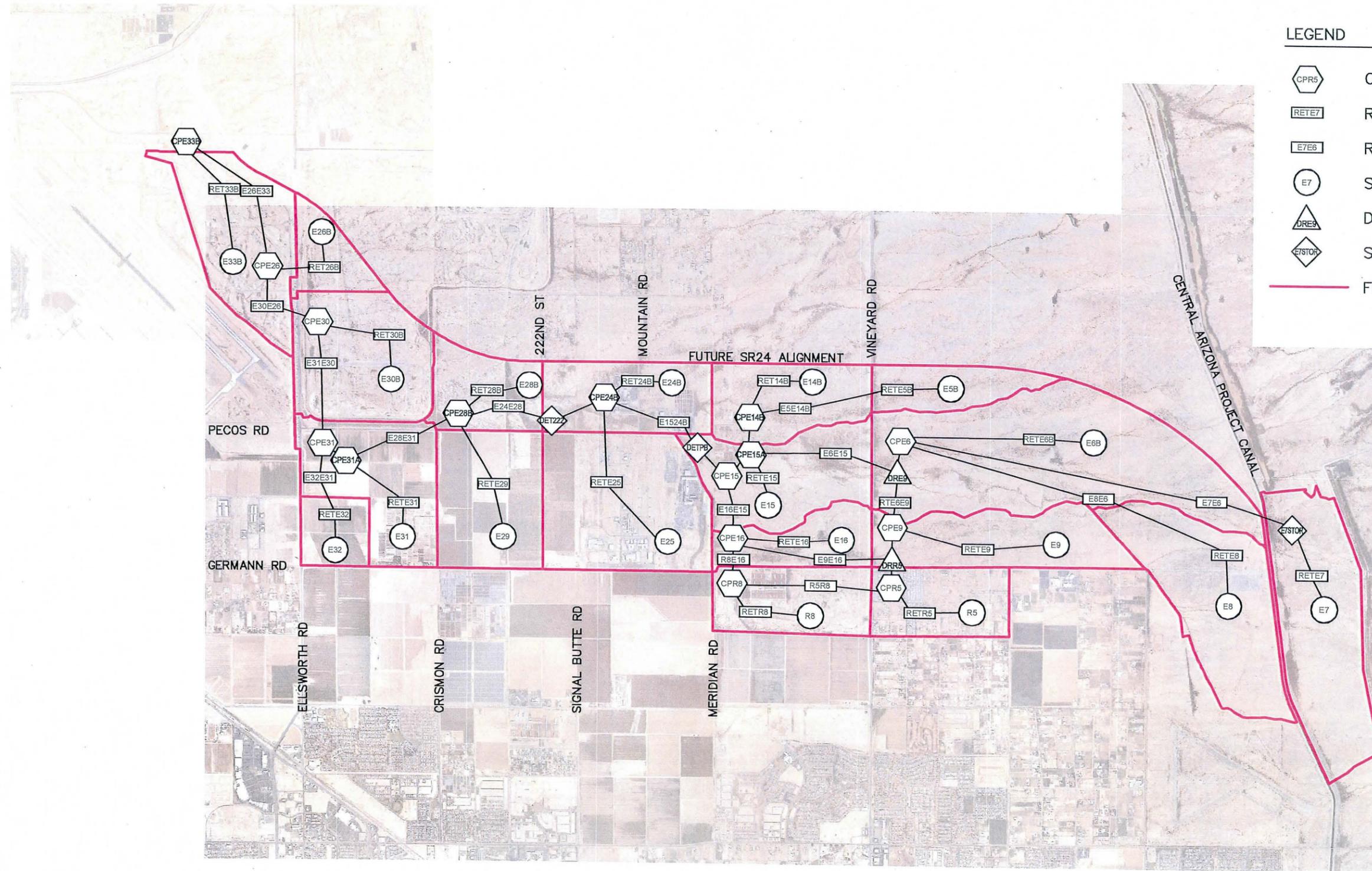


PECOS ROAD CHANNEL AND BASIN DESIGN CONCEPT REPORT

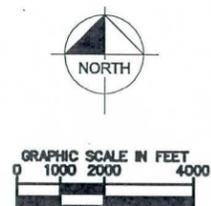
FUTURE CONDITIONS
HEC-1 SCHEMATIC
ALTERNATIVES ANALYSIS



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XREFS: XAERIAL_091131024



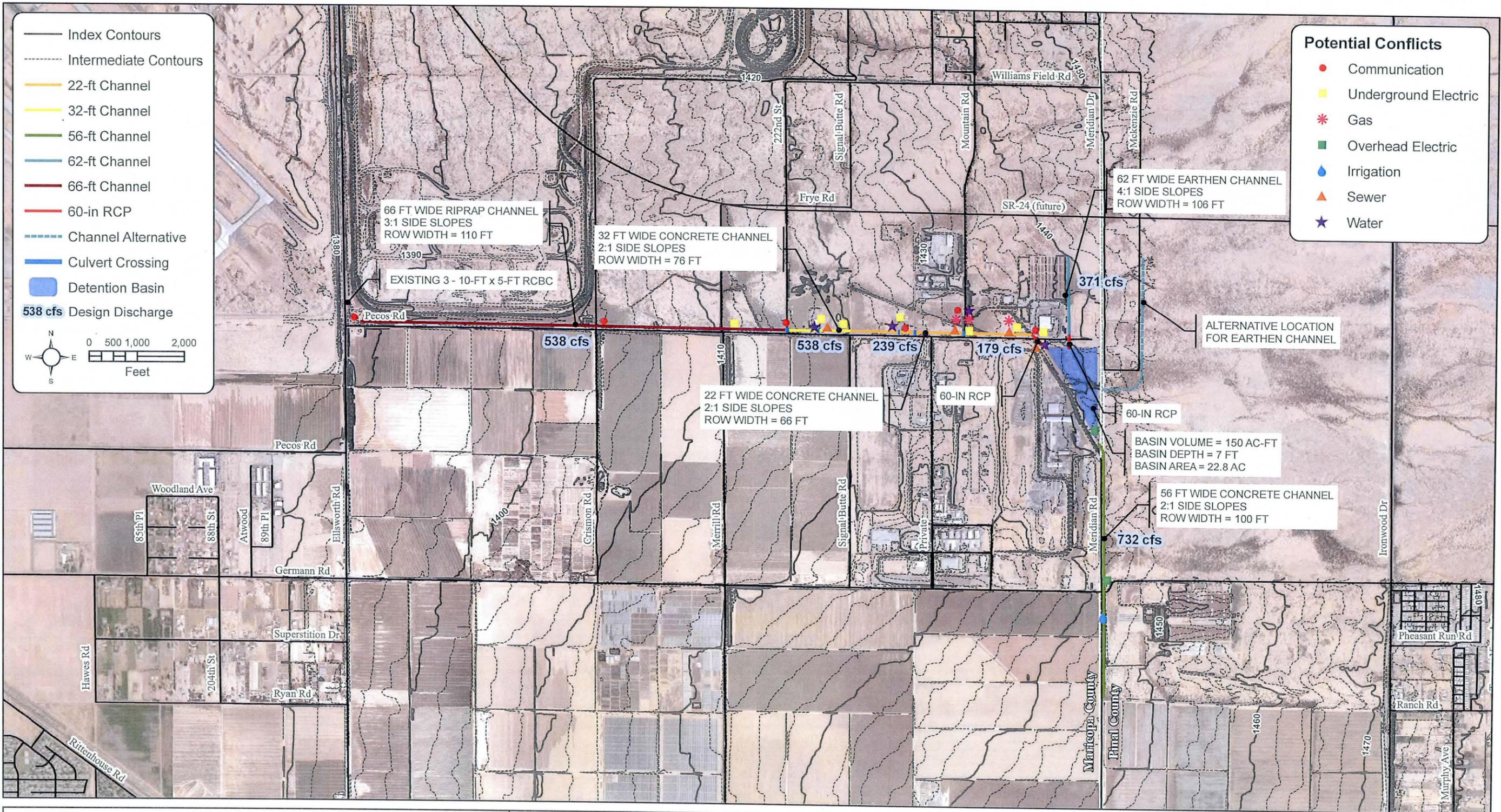
- LEGEND
-  CONCENTRATION POINT
 -  RETENTION
 -  ROUTING PATH
 -  SUBBASIN
 -  DIVERSION
 -  STORAGE
 -  FUTURE SUBBASIN BOUNDARY

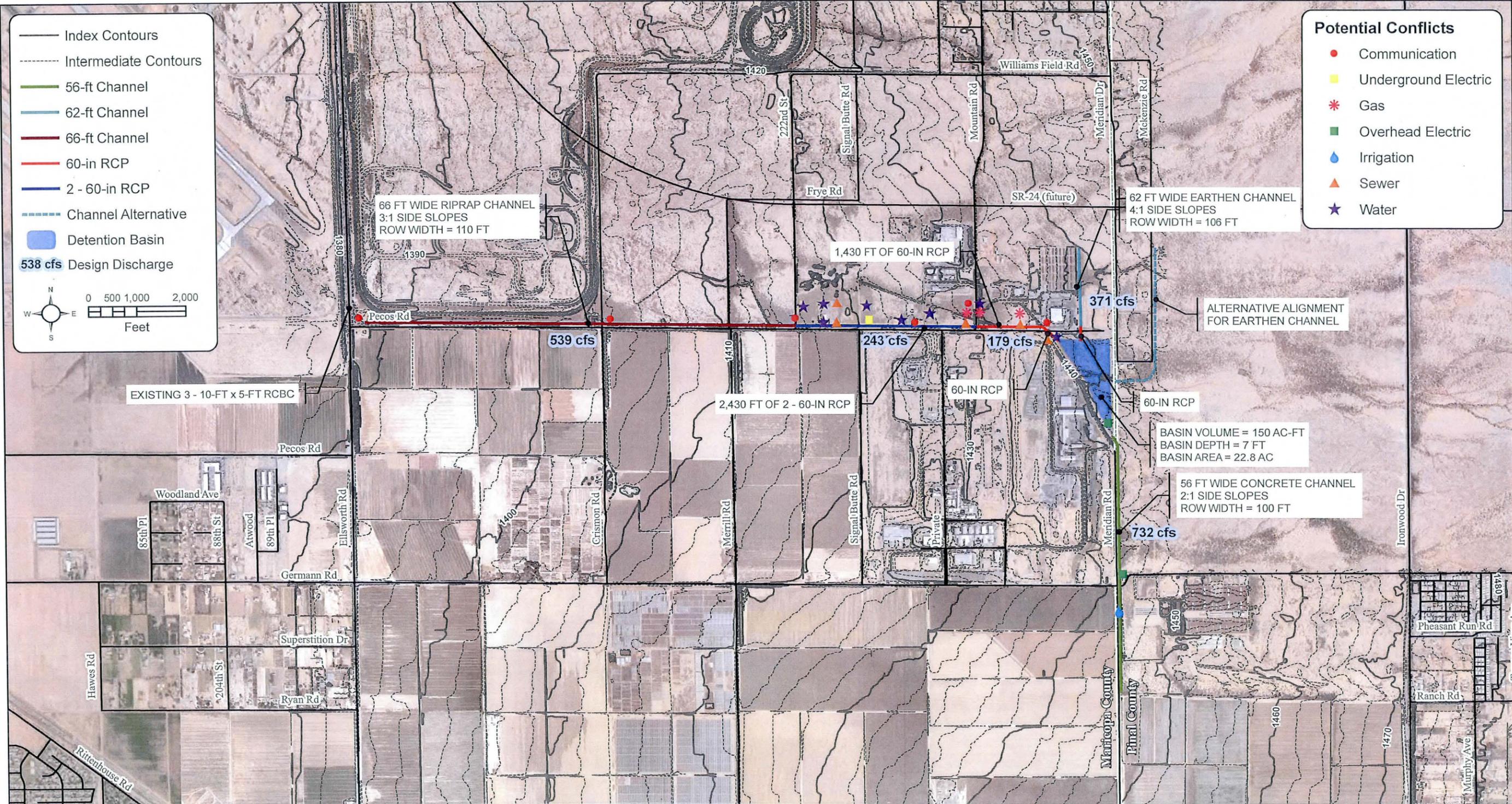


PECOS ROAD CHANNEL AND BASIN
DESIGN CONCEPT REPORT

FUTURE CONDITIONS
HEC-1 SCHEMATIC
DCR DRAINAGE SYSTEM





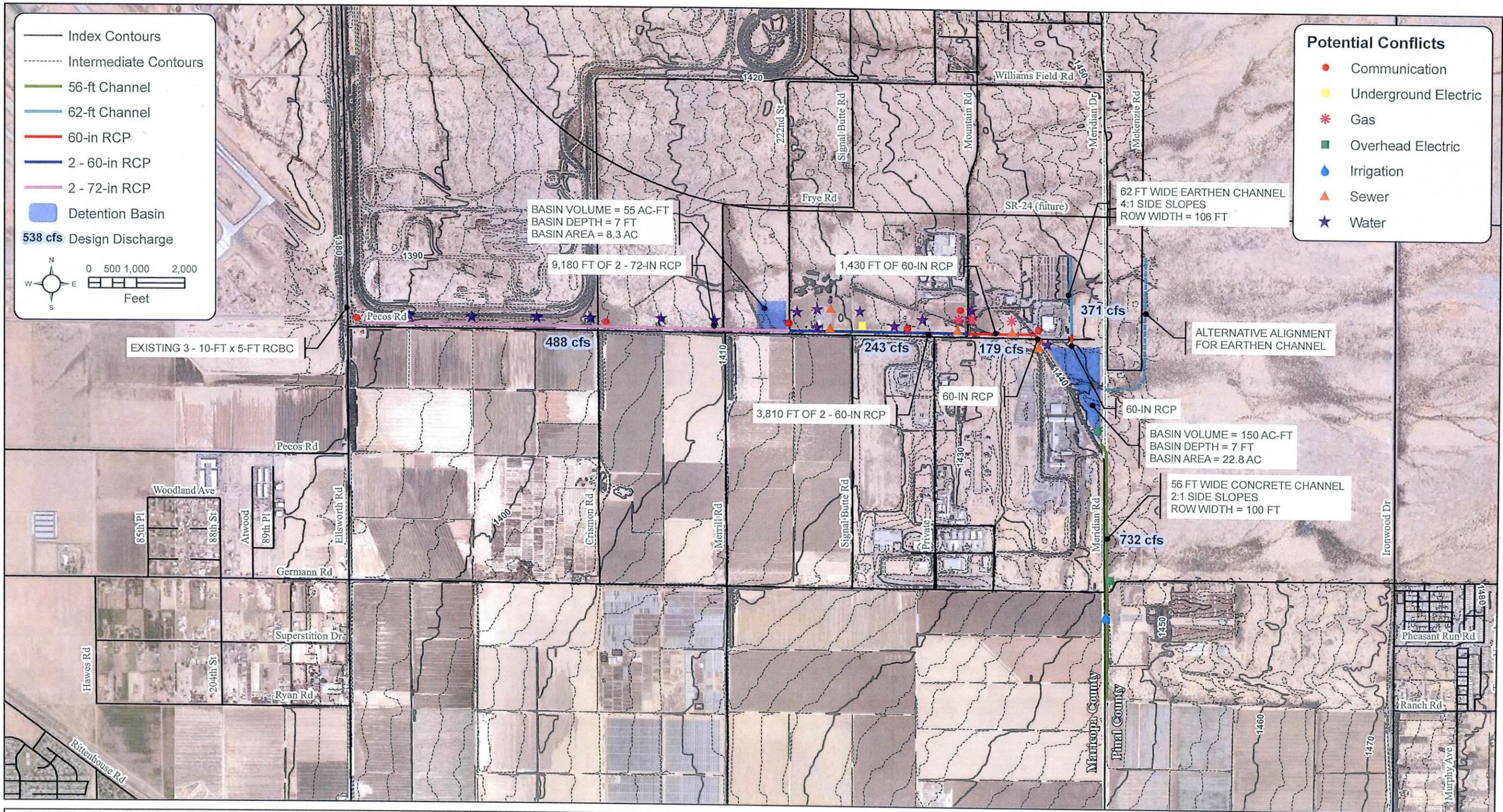


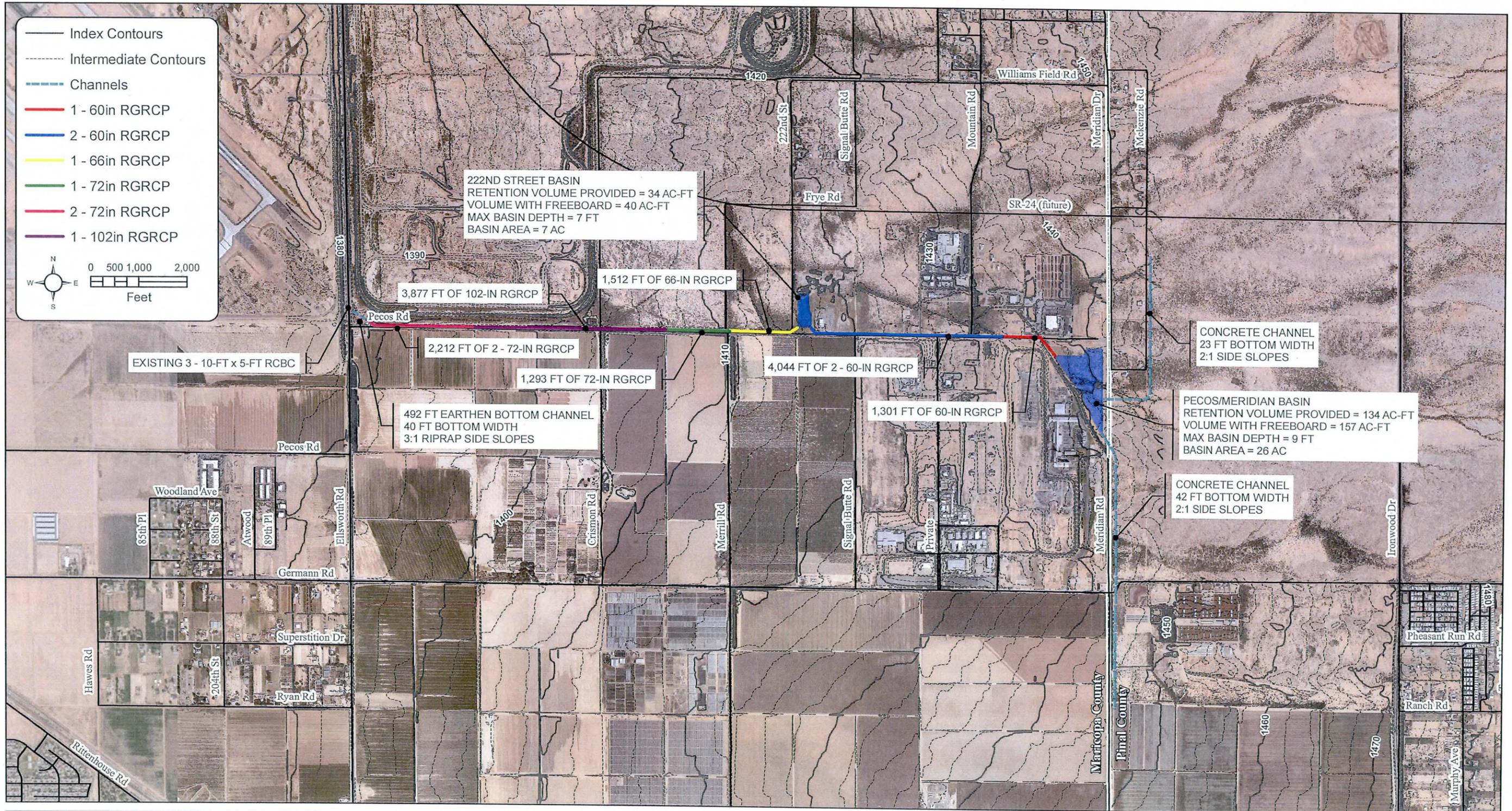
Kimley»Horn

Pecos Road Channel and Basin Design Concept Report

Flood Control District of Maricopa County
City of Mesa

Alternative 2



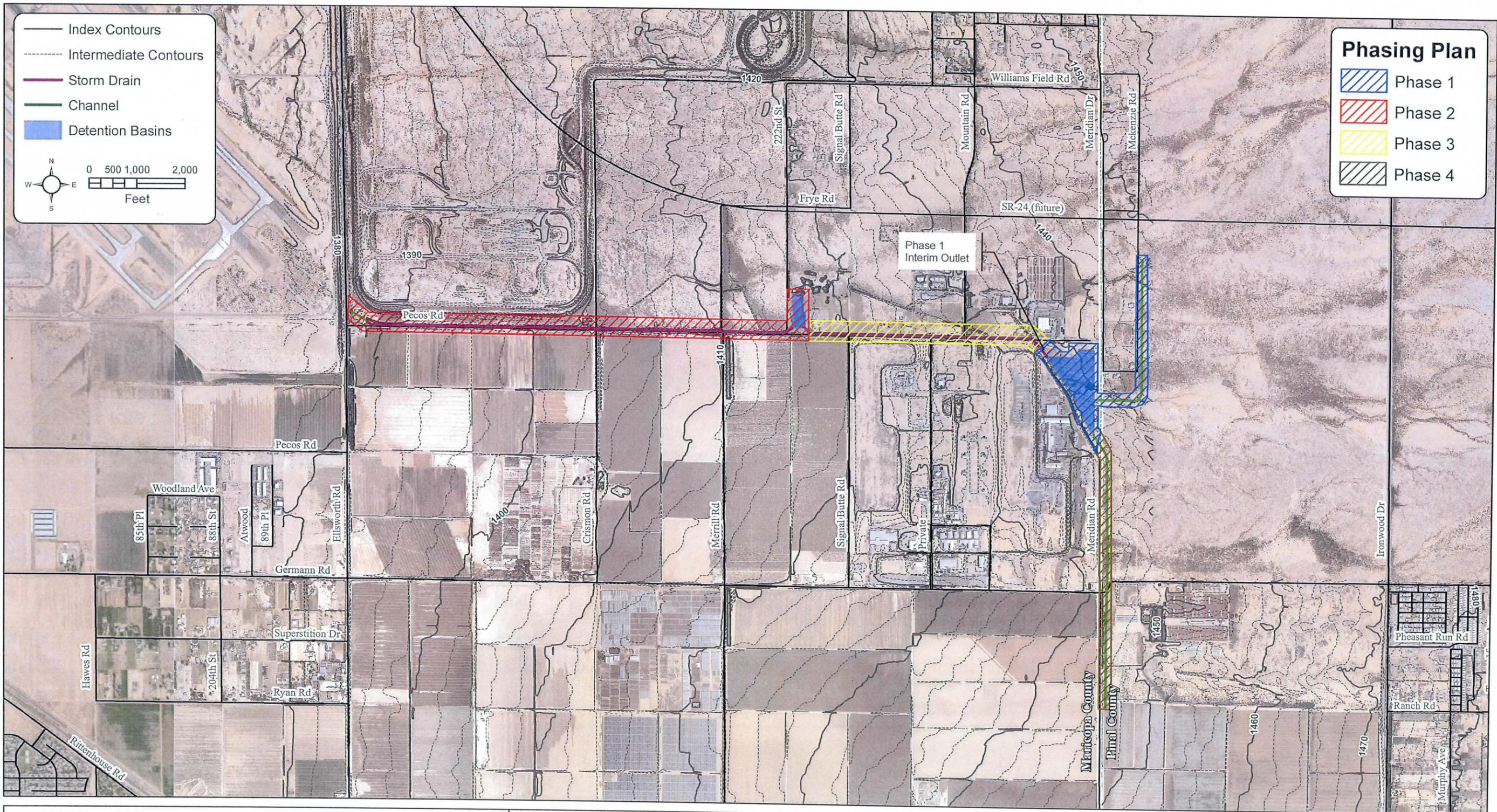


Kimley»Horn

Pecos Road Channel and Basin Design Concept Report

Flood Control District of Maricopa County
City of Mesa

DCR Drainage System



Kimley»Horn

Pecos Road Channel and
Basin Design Concept Report

Flood Control District of Maricopa County
City of Mesa

DCR Drainage System with Implementation Phasing

Appendix B. Alternatives Hydrology

- Alternative 1 HEC-1 Model Output
- Alternative 2 HEC-1 Model Output
- Alternative 3 HEC-1 Model Output

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 28AUG14 TIME 08:56:01
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Pecos Road Channel and Basin Design Concept Report
2 ID Alternative Analysis
3 ID Future Conditions
4 ID
5 ID Prepared for the Flood Control District of Maricopa County
6 ID District Project Number FCD 2014C001
7 ID
8 ID Prepared by Kimley-Horn and Associates, Inc.
9 ID Kimley Horn Project Number 091131024
10 ID August 2014
11 ID
12 ID Model based on the East Mesa Area Drainage Master Plan Update (EMADMPU)
13 ID for Alternative 1. The model was revised to include only those areas
14 ID contributing to the Ellsworth Channel.
15 ID
16 ID List of Changes:
17 ID - Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card
18 ID to a storage routing card with stage-storage-discharge data; the name
19 ID was changed from DIVPB to DETPB to reflect the change.
20 ID - Routing reach from CPR9 to CPR8 was eliminated
21 ID - Powerline section of the model was deleted (all subbasins north of the
22 ID future SR24 alignment).
23 ID - All subbasins south and east of R5 and R8 have been deleted.
24 ID - All comments from the East Mesa Area Drainage Master Plan Update that do
25 ID pertain to the Ellsworth Channel model have been deleted.
26 ID - Area has been adjusted on HC cards to account for reduction in area due
27 ID retention diversions.
28 ID
29 ID
30 ID
31 ID *****
32 ID ***** EAST MESA ADMPU *****
33 ID *****
34 ID
35 ID PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
36 ID CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
37 ID PREPARED BY: ENTELLUS, INC.
38 ID PROJECT NO: FCD 2011C017 ENTELLUS 310.057
39 ID MODIFIED DATE: 9/12/2012
40 ID MODELER: RLJ
41 ID
42 ID STORM: 100-YEAR 24-HOUR
43 ID
44 ID ALTERNATIVE: 1
45 ID
46 ID DEVELOPMENT CONDITIONS: FUTURE LAND USE
47 ID INCREASED FUTURE RETENTION (2.19->2.70 IN)
48 ID
49 ID PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
50 ID MERIDIAN CHANNEL
51 ID PECOS CHANNEL
52 ID MERIDIAN AND PECOS RETENTION BASIN
53 ID GERMANN CHANNEL
54 ID
55 ID MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
    
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1 HEC-1 INPUT PAGE 2

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
56 ID 100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
57 ID VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
58 ID SUBBASINS:
59 ID
60 ID E28B E29 E30B
61 ID E31 E32 E33B
62 ID
63 ID MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
64 ID RETOUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
65 ID WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
66 ID PROPOSED RETENTION AT MERIDIAN AND PECOS.
67 ID
68 ID MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
69 ID COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
70 ID WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
71 ID DEFINED ON PECOS ROAD.
72 ID
73 ID MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
74 ID DIVVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS
75 ID
76 ID
77 ID
78 ID *****
79 ID ***** EAST MESA ADMPU *****
80 ID *****
81 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
82 ID Flood Control District of Maricopa County
83 ID 100 YEAR
84 ID 24 Hour Storm
85 ID Unit Hydrograph: S-Graph
86 ID 08/05/2011
87 ID *****
88 IT 5 12Aug14 0 2000 2000
89 IN 15
90 IO 5
*DIAGRAM
*
91 JD 3.579 0.0001
92 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
93 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
94 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
95 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
96 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
97 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
98 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
99 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
100 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
101 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
102 JD 3.561 1.0
103 JD 3.490 5.0
104 JD 3.400 10.0
105 JD 3.286 20.0
106 JD 3.221 30.0
107 JD 3.175 40.0
108 JD 3.139 50.0
    
```

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```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
109 JD 3.114 60.0
*
110 KK E7 BASIN
111 KM Runoff from subbasin E7
112 BA 1.124
113 LG 0.24 0.26 5.10 0.32 35
114 UI 0 64 64 102 224 281 328 369 416 477
115 UI 561 725 814 670 575 512 449 390 339 300
116 UI 226 159 113 106 99 64 64 46 20 20
117 UI 20 20 20 20 20 20 0 0 0 0
118 UI 0 0 0 0 0 0 0 0 0 0
*
119 KK DIVE7 DIVERT
120 KM Divert the required retention volume for the subbasin out of the model
121 DT RETE7 85.5 0.0
122 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
123 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
124 KK E7STOR STORAGE
125 RS 1 STOR
126 SV 22.82 34.23 45.64 78.34 111.03 143.72 176.42 230.23 284.04
127 SQ 1.75 5.50 11.00 17.70 25.70 34.20 43.00 51.70
128 SE 1566.0 1567.00 1567.50 1568.00 1568.50 1569.00 1569.50 1570.00 1570.50 1571.00
129 ST 1574.0 10000.0 3.0 1.5
*
130 KK E7E6 ROUTE
    
```

```

131      KM      Route outfall from E7STOR to CPE6
132      RS      23      FLOW
133      RC      0.035  0.030  0.030  16362  0.0062  5.50
134      RX      0.00  500.00  980.00  1003.00  1007.00  1031.00  1511.00  2011.00
135      RY      5.50  4.50  4.00  1.00  1.00  4.00  4.50  5.50
      *

136      KK      E6B  BASIN
137      KM      Runoff from subbasin E6B
138      BA      1.949
139      LG      0.14  0.25  6.00  0.24  59
140      UI      0  174  277  677  898  1079  1330  1853  2099  1602
141      UI      1321  1068  853  594  331  288  192  162  53  53
142      UI      53  53  53  0  0  0  0  0  0  0
143      UI      0  0  0  0  0  0  0  0  0  0
144      UI      0  0  0  0  0  0  0  0  0  0
      *

145      KK      DIVE6B  DIVERT
146      KM      Divert the required retention volume for the subbasin out of the model
147      DT      RETE6B  179.9  0.0
148      DI      0.0  10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
149      DQ      0.0  10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

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1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

150      KK      E8  BASIN
151      KM      Runoff from subbasin E8
152      BA      1.099
153      LG      0.21  0.25  4.50  0.44  39
154      UI      0  75  75  201  313  383  441  514  604  798
155      UI      955  771  649  563  475  401  337  241  145  127
156      UI      114  75  75  28  23  23  23  23  23  23
157      UI      0  0  0  0  0  0  0  0  0  0
158      UI      0  0  0  0  0  0  0  0  0  0
      *
    
```

```

159      KK      DIVE8  DIVERT
160      KM      Divert the required retention volume for the subbasin out of the model
161      DT      RETE8  80.9  0.0
162      DI      0.0  10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
163      DQ      0.0  10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

164      KK      E8E6  ROUTE
165      KM      Route runoff from subbasin E8 that is not retained to CPE6
166      RS      9      FLOW
167      RC      0.060  0.035  0.060  9833  0.0052  5.50
168      RX      0.00  500.00  980.00  1003.00  1007.00  1031.00  1511.00  2011.00
169      RY      5.50  4.50  4.00  1.00  1.00  4.00  4.50  5.50
      *
    
```

```

170      KK      CPE6 COMBINE
171      KM      Combine routed flow from E7STOR and subbasin E8 with unretained runoff from
172      KM      subbasin E6B.
173      HC      3  3.05
      *
    
```

```

174      KK      DE6S  DIVERT
175      KM      Flow split diversion, DRE9 to the south, DE6S to the west
176      DT      DRE9  0.0  0.0
177      DI      0.0  236.0  682.0  1141.0  1670.0  2261.0  2886.0  0.0  0.0  0.0
178      DQ      0.0  1.0  13.0  212.0  633.0  1096.0  1568.0  0.0  0.0  0.0
      *
    
```

```

179      KK      E6E15  ROUTE
180      KM      Route remaining flow from flow split at DE6S west to CPE15A
181      RS      7      FLOW
182      RC      0.035  0.030  0.035  8259  0.0042  5.50
183      RX      950.00  975.00  991.00  1003.00  1007.00  1019.00  1030.00  1065.00
184      RY      5.50  4.50  4.00  1.00  1.00  4.00  4.50  5.50
      *
    
```

```

185      KK      E5B  BASIN
186      KM      Runoff from subbasin E5B
187      BA      0.286
188      LG      0.14  0.25  3.95  0.64  62
189      UI      0  64  225  342  567  435  287  148  74  36
190      UI      15  15  0  0  0  0  0  0  0  0
191      UI      0  0  0  0  0  0  0  0  0  0
      *
    
```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

192      UI      0  0  0  0  0  0  0  0  0  0
193      UI      0  0  0  0  0  0  0  0  0  0
      *
    
```

```

194      KK      DIVE5B  DIVERT
195      KM      Divert the required retention volume for the subbasin out of the model
    
```

196 DT RETE5B 25.0 0.0
 197 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 198 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

199 KK E5E14B ROUTE
 200 KM Route runoff from subbasin E5B that is not retained to CP14B
 201 RS 5 FLOW
 202 RC 0.035 0.030 0.035 6256 0.0054 5.50
 203 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1050.00
 204 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

205 KK E14B BASIN
 206 KM Runoff from subbasin E14B
 207 BA 0.528
 208 LG 0.14 0.25 5.60 0.29 60
 209 UI 0 125 435 667 1086 785 512 237 126 53
 210 UI 29 29 0 0 0 0 0 0 0 0
 211 UI 0 0 0 0 0 0 0 0 0 0
 212 UI 0 0 0 0 0 0 0 0 0 0
 213 UI 0 0 0 0 0 0 0 0 0 0
 *

214 KK DIV14B DIVERT
 215 KM Divert the required retention volume for the subbasin out of the model
 216 DT RET14B 48.4 0.0
 217 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 218 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

219 KK CP14B COMBINE
 220 KM Combine routed flow from E5B with unretained runoff from subbasin E14B.
 221 HC 2
 *

222 KK E14E15 ROUTE
 223 KM Route combined runoff from CP14B to CPE15A
 224 RS 2 FLOW
 225 RC 0.04 0.03 0.04 1840 0.0018
 226 RX 0 9 18 29 40 51 59 68
 227 RY 4 2 0 0 0 0 2 4
 *

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1
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

228 KK E15 BASIN
 229 KM Runoff from subbasin E15
 230 BA 0.777
 231 LG 0.15 0.25 5.10 0.35 57
 232 UI 0 106 363 582 791 1239 1004 734 522 273
 233 UI 171 106 36 32 32 0 0 0 0 0
 234 UI 0 0 0 0 0 0 0 0 0 0
 235 UI 0 0 0 0 0 0 0 0 0 0
 236 UI 0 0 0 0 0 0 0 0 0 0
 *

237 KK DIVE15 DIVERT
 238 KM Divert the required retention volume for the subbasin out of the model
 239 DT RETE15 67.7 0.0
 240 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 241 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

242 KK CPE15A COMBINE
 243 KM Combine routed flow from split at CPE6 (DRE9, DE6S) and CP14B with unretained
 244 KM runoff from subbasin E15.
 245 HC 3 4.29
 *

246 KK DRE9RETRIEVE
 247 KM Retrieve flow from split at DRE9 that goes to the south
 248 DR DRE9
 *

249 KK RTE6E9 ROUTE
 250 KM Route split flow from CPE6 (DRE9) south to CPE9
 251 RS 5 FLOW
 252 RC 0.035 0.030 0.025 2200 0.0035 6.00
 253 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 254 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

255 KK E9 BASIN
 256 KM Runoff from subbasin E9
 257 BA 0.723
 258 LG 0.14 0.25 5.40 0.30 58
 259 UI 0 88 253 450 585 836 1040 754 570 416
 260 UI 225 148 92 48 27 27 27 0 0 0
 261 UI 0 0 0 0 0 0 0 0 0 0
 262 UI 0 0 0 0 0 0 0 0 0 0

263 UI 0 0 0 0 0 0 0 0 0 0 0
 *
 264 KK DIVE9 DIVERT
 265 KM Divert the required retention volume for the subbasin out of the model
 266 DT RETE9 65.4 0.0
 267 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 268 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

269 KK CPE9 COMBINE
 270 KM Combine routed flow from split at CPE6 (DRE9) with unretained runoff from
 271 KM subbasin E9
 272 HC 2 1.07
 *
 273 KK DE9S DIVERT
 274 KM Flow split diversion, DRR5 to the south, DE9S to the west
 275 DT DRR5 0.0 0.0
 276 DI 0.0 78.0 163.0 440.0 936.0 1475.0 2024.0 0.0 0.0 0.0
 277 DQ 0.0 1.0 43.0 245.0 670.0 1157.0 1661.0 0.0 0.0 0.0
 *

278 KK E9E16 ROUTE
 279 KM Route remaining flow from flow split at DE9S west to CPE16
 280 RS 6 FLOW
 281 RC 0.035 0.030 0.035 6751 0.0040 5.50
 282 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1060.00
 283 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

284 KK DRR5RETRIEVE
 285 KM Retrieve flow from split at DRR5 that goes to the south
 286 DR DRR5
 *

287 KK R5 BASIN
 288 KM Runoff from subbasin R5
 289 BA 0.504
 290 LG 0.29 0.25 5.40 0.27 21
 291 UI 0 53 120 241 310 393 574 608 455 358
 292 UI 277 189 98 80 53 26 16 16 16 16
 293 UI 0 0 0 0 0 0 0 0 0 0
 294 UI 0 0 0 0 0 0 0 0 0 0
 295 UI 0 0 0 0 0 0 0 0 0 0
 *

296 KK DIVR5 DIVERT
 297 KM Divert the required retention volume for the subbasin out of the model
 298 DT RETR5 1.0 0.0
 299 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 300 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

301 KK CPR5 COMBINE
 302 KM Combine routed flow from split at CPE9 (DRR5) with unretained runoff from
 303 KM subbasin R5
 304 HC 2 1.07
 *

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

305 KK R5R8 ROUTE
 306 KM Route combined runoff from CPR5 to CPR8
 307 RS 5 FLOW
 308 RC 0.040 0.035 0.040 6587 0.0043 5.00
 309 RX 966.00 986.00 994.00 1006.00 1012.00 1024.00 1032.00 1052.00
 310 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
 *

311 KK R8 BASIN
 312 KM Runoff from subbasin R8
 313 BA 0.554
 314 LG 0.16 0.25 4.60 0.45 64
 315 UI 0 69 208 360 471 695 788 567 421 299
 316 UI 149 105 69 23 21 21 21 0 0 0
 317 UI 0 0 0 0 0 0 0 0 0 0
 318 UI 0 0 0 0 0 0 0 0 0 0
 319 UI 0 0 0 0 0 0 0 0 0 0
 *

320 KK DIVR8 DIVERT
 321 KM Divert the required retention volume for the subbasin out of the model
 322 DT RETR8 50.5 0.0
 323 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 324 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

```

325      KK   CPR8 COMBINE
326      KM   Combine routed runoff from CPR5 with unretained runoff from subbasin R8
327      HC   2   1.62
      *

328      KK   R8E16 ROUTE
329      KM   Route combined flows from CPR8 to CPE16 in the proposed MERIDIAN SOUTH CHANNE
330      RS   3   FLOW
331      RC   0.03  0.04  0.03  2660  0.001
332      RX   0   16   33   45   58   71   87   103
333      RY   7   3   0   0   0   0   3   7
      *

334      KK   E16  BASIN
335      KM   Runoff from subbasin E16
336      BA   0.396
337      LG   0.15  0.25  5.10  0.35  57
338      UI   0   58   224  342  497  684  480  338  207  100
339      UI   64   26   18   18   0   0   0   0   0   0
340      UI   0   0   0   0   0   0   0   0   0   0
341      UI   0   0   0   0   0   0   0   0   0   0
342      UI   0   0   0   0   0   0   0   0   0   0
      *
    
```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

343      KK   DIVE16 DIVERT
344      KM   Divert the required retention volume for the subbasin out of the model
345      DT   RETE16  35.1  0.0
346      DI   0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
347      DQ   0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

348      KK   CPE16 COMBINE
349      KM   Combine routed flow from split at CPE9 (DRR5, DE9S) and routed flow from CPR8
350      KM   with unretained runoff from subbasin E16.
351      HC   3   2.52
      *
    
```

```

352      KK   E16E15 ROUTE
353      KM   Route combined flows from CPE16 to CPE15 in the MERIDIAN SOUTH CHANNEL
354      RS   4   FLOW
355      RC   0.03  0.04  0.03  4120  0.001
356      RX   0   16   33   44   56   68   84   100
357      RY   7   3   0   0   0   0   3   7
      *
    
```

```

358      KK   CPE15 COMBINE
359      KM   Combine routed flows from CPE16 in the MERIDIAN SOUTH CHANNEL with flows
360      KM   from the north and east at the southwest corner of Pecos and Meridian. These
361      KM   flows combine in the proposed Pecos Basin (DETPB)
362      HC   2   6.81
      *
    
```

```

363      KK   DETPB STORAGE
364      KM   Proposed offline retention basin at SWC Meridian and Pecos
365      KM   Basin is 7-ft deep basin, but the top foot is not included (freeboard)
366      KM   Side slopes are 4:1, outlet pipe is 60-in, overflow spillway at 6 ft
367      KO   3
368      RS   1   STOR
369      SV   0   21.9  43.9  66.1  88.4  110.8  133.3  144.7  156.0
370      SQ   0   15   60   119  173  176  177  189  201
371      SE   0   1   2   3   4   5   6   6.5  7
      *
    
```

```

372      KK   E1524B ROUTE
373      KM   Route discharge from basin DETPB in PECOS CHANNEL to Signal Butte & Pecos
374      RS   3   FLOW
375      RC   0.035  0.035  0.035  3800  0.0035
376      RX   0   11   21   23   25   27   38   48
377      RY   7   4   0   0   0   0   4   7
      *
    
```

```

378      KK   E25  BASIN
379      KM   Runoff from subbasin E25
380      BA   0.932
381      LG   0.15  0.25  5.40  0.30  55
382      UI   0   86   146  342  451  546  683  986  969  749
383      UI   613  490  383  234  148  125  86  51  26  26
384      UI   26  26  0   0   0   0   0   0   0   0
      *
    
```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

385      UI   0   0   0   0   0   0   0   0   0   0
386      UI   0   0   0   0   0   0   0   0   0   0
      *
    
```

```

387      KK   DIVE25 DIVERT
388      KM   Divert the required retention volume for the subbasin out of the model
    
```

389	KM	MODIFIED MAX VOLUME FROM 110.7 TO 89.8										
390	DT	RETE25	89.8	0.0								
391	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
392	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	*											
393	KK	E24B	BASIN									
394	KM	Runoff from subbasin E24B										
395	BA	0.464										
396	LG	0.15	0.15	7.30	0.14	57						
397	UI	0	92	339	513	852	731	493	294	133	76	
398	UI	24	24	0	0	0	0	0	0	0	0	
399	UI	0	0	0	0	0	0	0	0	0	0	
400	UI	0	0	0	0	0	0	0	0	0	0	
401	UI	0	0	0	0	0	0	0	0	0	0	
	*											
402	KK	DIV24B	DIVERT									
403	KM	Divert the required retention volume for the subbasin out of the model										
404	KM	MODIFIED MAX VOLUME FROM 38.7 TO 44.4										
405	DT	RET24B	44.4	0.0								
406	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
407	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	*											
408	KK	CPE24B	COMBINE									
409	KM	Combine routed discharge from basin DETPB with unretained runoff from										
410	KM	subbasins E25 and E24B in PECOS CHANNEL at Signal Butte & Pecos										
411	HC	3	8.20									
	*											
412	KK	E24E28	ROUTE									
413	KM	Route combined flows from CPE24B in PECOS CHANNEL to CPE28B at Crismon										
414	KM	and Pecos										
415	RS	4	FLOW									
416	RC	0.035	0.035	0.035	5320	0.0035						
417	RX	0	11	21	24	28	31	42	52			
418	RY	7	4	0	0	0	0	4	7			
	*											
419	KK	E28B	BASIN									
420	KM	Runoff from subbasin E28B										
421	BA	0.539										
422	LG	0.20	0.15	8.40	0.09	51						
423	UI	0	65	183	329	427	606	772	566	430	318	
424	UI	179	110	73	41	20	20	20	0	0	0	
425	UI	0	0	0	0	0	0	0	0	0	0	
426	UI	0	0	0	0	0	0	0	0	0	0	
427	UI	0	0	0	0	0	0	0	0	0	0	
	*											
		HEC-1 INPUT										
1	LINE	ID12345678910
428	KK	DIV28B	DIVERT									
429	KM	Divert the required retention volume for the subbasin out of the model										
430	KM	MODIFIED MAX VOLUME FROM 42.0 TO 51.3										
431	DT	RET28B	51.3	0.0								
432	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
433	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	*											
434	KK	E29	BASIN									
435	KM	Runoff from subbasin E29										
436	BA	1.002										
437	LG	0.15	0.23	6.20	0.22	55						
438	UI	0	103	218	452	586	733	1019	1240	924	737	
439	UI	574	428	229	172	116	82	31	31	31	31	
440	UI	0	0	0	0	0	0	0	0	0	0	
441	UI	0	0	0	0	0	0	0	0	0	0	
442	UI	0	0	0	0	0	0	0	0	0	0	
	*											
443	KK	DIVE29	DIVERT									
444	KM	Divert the required retention volume for the subbasin out of the model										
445	KM	MODIFIED MAX VOLUME FROM 73.9 TO 90.2										
446	DT	RETE29	90.2	0.0								
447	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
448	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
	*											
449	KK	CPE28B	COMBINE									
450	KM	Combine routed flow from CPE24B with unretained runoff from subbasins E28B										
451	KM	and E29 in the PECOS CHANNEL at Crismon and Pecos										
452	HC	3	9.74									
	*											
453	KK	E28E31	ROUTE									
454	KM	Route flows in the PECOS CHANNEL from CPE28B to CPE31 at Ellsworth and Pecos										
455	RS	3	FLOW									
456	RC	0.035	0.035	0.035	5400	0.0035						
457	RX	0	11	21	25	29	33	44	54			

```

458      RY      7      4      0      0      0      0      4      7
      *
459      KK      E31  BASIN
460      KM      Runoff from subbasin E31
461      BA      0.810
462      LG      0.15  0.25  4.80  0.39  55
463      UI      0      86  197  391  504  641  943  970  728  571
464      UI      441  296  151  126  86  37  26  26  26  0
465      UI      0      0      0      0      0      0      0      0      0      0
466      UI      0      0      0      0      0      0      0      0      0      0
467      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

1 HEC-1 INPUT PAGE 12

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

468      KK  DIVE31  DIVERT
469      KM  Divert the required retention volume for the subbasin out of the model
470      KM  MODIFIED MAX VOLUME FROM 56.5 TO 68.9
471      DT  RETE31  68.9  0.0
472      DI  0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
473      DQ  0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

474      KK  CPE31A COMBINE
475      KM  Combine routed flows from CPE28B with unretained runoff from subbasin E31 at
476      KM  in the PECOS CHANNEL at Ellsworth and Pecos
477      HC  2  10.55
      *
    
```

```

478      KK      E32  BASIN
479      KM      Runoff from subbasin E32
480      BA      0.246
481      LG      0.14  0.25  4.25  0.55  58
482      UI      0      72  238  387  535  337  190  78  37  15
483      UI      15  0      0      0      0      0      0      0      0      0
484      UI      0      0      0      0      0      0      0      0      0      0
485      UI      0      0      0      0      0      0      0      0      0      0
486      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

```

487      KK  DIVE32  DIVERT
488      KM  Divert the required retention volume for the subbasin out of the model
489      KM  MODIFIED MAX VOLUME FROM 17.2 TO 20.9
490      DT  RETE32  20.9  0.0
491      DI  0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
492      DQ  0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

493      KK  E32E31  ROUTE
494      KM  Route unretained runoff from subbasin E32 to CPE31
495      RS  5  FLOW
496      RC  0.025  0.060  0.025  3272  0.0028  1388.60
497      RX  100.00  110.00  128.00  149.80  160.00  191.50  209.20  210.00
498      RY  1388.3  1388.32  1388.32  1380.37  1380.17  1388.04  1388.39  1388.60
      *
    
```

```

499      KK  CPE31 COMBINE
500      KM  Combine unretained runoff from subbasin E32 with the flows from the PECOS
501      KM  CHANNEL at CPE31 - Ellsworth and Pecos
502      HC  2  10.80
      *
    
```

```

503      KK  E31E30  ROUTE
504      KM  Route runoff from CPE31 north in the Ellsworth Channel to CPE30
505      RS  5  FLOW
506      RC  0.025  0.045  0.025  4404  0.0008  1387.00
507      RX  100.00  107.00  112.50  144.90  175.10  201.50  225.90  244.00
508      RY  1386.1  1386.09  1386.09  1377.99  1377.99  1384.59  1385.08  1387.00
      *
    
```

1 HEC-1 INPUT PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

509      KK      E30B  BASIN
510      KM      Runoff from subbasin E30B
511      BA      0.882
512      LG      0.24  0.15  8.40  0.09  47
513      UI      0      56  56  128  217  272  314  357  416  500
514      UI      668  683  552  475  416  355  303  261  191  124
515      UI      98  92  66  56  44  17  17  17  17  17
516      UI      17  17  0  0  0  0  0  0  0  0
517      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

```

518      KK  DIV30B  DIVERT
519      KM  Divert the required retention volume for the subbasin out of the model
520      KM  MODIFIED MAX VOLUME FROM 67.1 TO 81.9
521      DT  RET30B  81.9  0.0
522      DI  0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
    
```

```

523      DQ      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
      *

524      KK      CPE30 COMBINE
525      KM      Combine routed flow from CPE31 in the Ellsworth Channel with unretained
526      KM      runoff from subbasin E30B
527      HC      2      11.68
      *

528      KK      E30E26 ROUTE
529      KM      Route combined runoff from CPE30 to CPE26 in the Ellsworth Channel
530      RS      1      FLOW
531      RC      0.025      0.035      0.025      822      0.0005      1387.00
532      RX      100.00      105.00      108.50      149.90      220.10      251.30      279.10      285.10
533      RY      1387.0      1387.00      1386.66      1376.31      1376.31      1384.11      1384.66      1386.00
      *

534      KK      E26B BASIN
535      KM      Runoff from subbasin E26B
536      BA      0.259
537      LG      0.24      0.15      8.80      0.07      48
538      UI      0      38      145      222      320      448      315      222      139      65
539      UI      43      18      12      12      0      0      0      0      0      0
540      UI      0      0      0      0      0      0      0      0      0      0
541      UI      0      0      0      0      0      0      0      0      0      0
542      UI      0      0      0      0      0      0      0      0      0      0
      *

543      KK      DIV26B DIVERT
544      KM      Divert the required retention volume for the subbasin out of the model
545      KM      MODIFIED MAX VOLUME FROM 20.1 TO 24.5
546      DT      RET26B      24.5      0.0
547      DI      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
548      DQ      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
      *
    
```

HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

549      KK      CPE26 COMBINE
550      KM      Combined routed flows from CPE30 with unretained runoff from subbasin E26B
551      HC      2      11.94
      *

552      KK      E26E33 ROUTE
553      KM      Route combine flows from CPE26 to CPE33 in the Ellsworth Channel
554      RS      5      FLOW
555      RC      0.025      0.030      0.025      8929      0.0028      1379.67
556      RX      100.00      100.50      102.50      134.90      205.10      237.50      253.50      255.00
557      RY      1379.1      1379.12      1379.35      1371.25      1371.25      1379.35      1379.67      1379.67
      *

558      KK      E33B BASIN
559      KM      Runoff from subbasin E33B
560      BA      0.851
561      LG      0.15      0.15      7.30      0.14      56
562      UI      0      117      409      651      892      1385      1087      793      558      278
563      UI      179      110      36      36      36      0      0      0      0      0
564      UI      0      0      0      0      0      0      0      0      0      0
565      UI      0      0      0      0      0      0      0      0      0      0
566      UI      0      0      0      0      0      0      0      0      0      0
      *

567      KK      DIV33B DIVERT
568      KM      Divert the required retention volume for the subbasin out of the model
569      KM      MODIFIED MAX VOLUME FROM 66.8 TO 81.5
570      DT      RET33B      81.5      0.0
571      DI      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
572      DQ      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
      *

573      KK      CPE33B COMBINE
574      KM      Combine routed flows in the Ellsworth Channel from CPE26 with unretained
575      KM      runoff from subbasin E33B. Note this CP also receives flow from the
576      KM      Powerline model but that flow is not included in this model.
577      HC      2      12.79
      *

578      ZZ
    
```

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

110      E7
      .
121      .-----> RETE7
119      DIVE7
      V
      V
    
```

```
124 E7STOR
    V
    V
130 E7E6
    .
136 . E6B
    .
147 . -----> RETE6B
145 . DIVE6B
    .
150 . E8
    .
161 . -----> RETE8
159 . DIVE8
    V
164 . E8E6
    .
170 CPE6.....
    .
176 . -----> DRE9
174 DE6S
    V
179 E6E15
    .
185 . E5B
    .
196 . -----> RETE5B
194 . DIVE5B
    V
199 . E5E14B
    .
205 . E14B
    .
216 . -----> RET14B
214 . DIV14B
    .
219 . CP14B.....
    V
222 E14E15
    .
228 . E15
    .
239 . -----> RETE15
237 . DIVE15
    .
242 CPE15A.....
    .
248 . <----- DRE9
246 . DRE9
    V
249 . RTE6E9
    .
255 . E9
    .
266 . -----> RETE9
264 . DIVE9
    .
269 . CPE9.....
    .
275 . -----> DRR5
273 . DE9S
    V
278 E9E16
    .
286 . <----- DRR5
284 . DRR5
    .
```

```
287 . . . . . R5
. . . . .
298 . . . . . -----> RETR5
296 . . . . . DIVR5
. . . . .
301 . . . . . CPR5.....
. . . . . V
. . . . . V
305 . . . . . R5R8
. . . . .
311 . . . . . R8
. . . . .
322 . . . . . -----> RETR8
320 . . . . . DIVR8
. . . . .
325 . . . . . CPR8.....
. . . . . V
. . . . . V
328 . . . . . R8E16
. . . . .
334 . . . . . E16
. . . . .
345 . . . . . -----> RETE16
343 . . . . . DIVE16
. . . . .
348 . . . . . CPE16.....
. . . . . V
. . . . . V
352 . . . . . E16E15
. . . . .
358 . . . . . CPE15.....
. . . . . V
. . . . . V
363 . . . . . DETPB
. . . . . V
. . . . . V
372 . . . . . E1524B
. . . . .
378 . . . . . E25
. . . . .
390 . . . . . -----> RETE25
387 . . . . . DIVE25
. . . . .
393 . . . . . E24B
. . . . .
405 . . . . . -----> RET24B
402 . . . . . DIV24B
. . . . .
408 . . . . . CPE24B.....
. . . . . V
. . . . . V
412 . . . . . E24E28
. . . . .
419 . . . . . E28B
. . . . .
431 . . . . . -----> RET28B
428 . . . . . DIV28B
. . . . .
434 . . . . . E29
. . . . .
446 . . . . . -----> RETE29
443 . . . . . DIVE29
. . . . .
449 . . . . . CPE28B.....
. . . . . V
. . . . . V
453 . . . . . E28E31
. . . . .
459 . . . . . E31
. . . . .
471 . . . . . -----> RETE31
```

```

468      .      DIVE31
      .      .
474      CPE31A.....
      .      .
478      .      E32
      .      .
490      .      .-----> RETE32
487      .      DIVE32
      .      V
      .      V
493      .      E32E31
      .      .
499      CPE31.....
      .      V
      .      V
503      E31E30
      .      .
509      .      E30B
      .      .
521      .      .-----> RET30B
518      .      DIV30B
      .      .
524      CPE30.....
      .      V
      .      V
528      E30E26
      .      .
534      .      E26B
      .      .
546      .      .-----> RET26B
543      .      DIV26B
      .      .
549      CPE26.....
      .      V
      .      V
552      E26E33
      .      .
558      .      E33B
      .      .
570      .      .-----> RET33B
567      .      DIV33B
      .      .
573      CPE33B.....
    
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998                   *
*   VERSION 4.1                 *
*
* RUN DATE  28AUG14  TIME  08:56:01 *
*
*****
    
```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
*   609 SECOND STREET          *
* DAVIS, CALIFORNIA 95616      *
*   (916) 756-1104             *
*
*****
    
```

Pecos Road Channel and Basin Design Concept Report
 Alternative Analysis
 Future Conditions

Prepared for the Flood Control District of Maricopa County
 District Project Number FCD 2014C001

Prepared by Kimley-Horn and Associates, Inc.
 Kimley Horn Project Number 091131024
 August 2014

Model based on the East Mesa Area Drainage Master Plan Update (EMADMPU)
 for Alternative 1. The model was revised to include only those areas
 contributing to the Ellsworth Channel.

List of Changes:

- Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card to a storage routing card with stage-storage-discharge data; the name was changed from DIVPB to DETPB to reflect the change.
- Routing reach from CPR9 to CPR8 was eliminated
- Powerline section of the model was deleted (all subbasins north of the

- future SR24 alignment).
- All subbasins south and east of R5 and R8 have been deleted.
- All comments from the East Mesa Area Drainage Master Plan Update that do pertain to the Ellsworth Channel model have been deleted.
- Area has been adjusted on HC cards to account for reduction in area due retention diversions.

 ***** EAST MESA ADMPU *****

PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
 CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
 PREPARED BY: ENTELLUS, INC.
 PROJECT NO: FCD 2011C017 ENTELLUS 310.057
 MODIFIED DATE: 9/12/2012
 MODELER: RLJ

STORM: 100-YEAR 24-HOUR

ALTERNATIVE: 1

DEVELOPMENT CONDITIONS: FUTURE LAND USE INCREASED FUTURE RETENTION (2.19->2.70 IN)

PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
 MERIDIAN CHANNEL
 PECOS CHANNEL
 MERIDIAN AND PECOS RETENTION BASIN
 GERMANN CHANNEL

MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
 100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
 VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
 SUBBASINS:

E28B	E29	E32	E30B	E33B
E31				

MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
 RETOUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
 WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
 PROPOSED RETENTION AT MERIDIAN AND PECOS.

MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
 COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
 WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
 DEFINED ON PECOS ROAD.

MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
 DIVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS

 ***** EAST MESA ADMPU *****

FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
 Flood Control District of Maricopa County
 100 YEAR
 24 Hour Storm
 Unit Hydrograph: S-Graph
 08/05/2011

90 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 12Aug14 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 2000 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 18 14 ENDING DATE
 NDTIME 2235 ENDING TIME
 ICENT 20 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 166.58 HOURS

ENGLISH UNITS
 DRAINAGE AREA SQUARE MILES
 PRECIPITATION DEPTH INCHES
 LENGTH, ELEVATION FEET
 FLOW CUBIC FEET PER SECOND
 STORAGE VOLUME ACRE-FEET
 SURFACE AREA ACRES
 TEMPERATURE DEGREES FAHRENHEIT

HYDROGRAPH ROUTING DATA

STATION	ROUTING METHOD	STOR	TYPE OF INITIAL CONDITION	INITIAL CONDITION	WORKING R AND D COEFFICIENT					
368 RS	STORAGE ROUTING	1	NUMBER OF SUBREACHES							
				.00						
				.00						
369 SV	STORAGE	.0	21.9	43.9	66.1	88.4	110.8	133.3	144.7	156.0
370 SQ	DISCHARGE	0.	15.	60.	119.	173.	176.	177.	189.	201.
371 SE	ELEVATION	.00	1.00	2.00	3.00	4.00	5.00	6.00	6.50	7.00

HYDROGRAPH AT STATION
 TRANSPOSITION AREA

DETPB
 .0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)	(CFS)				
+	199.	17.33	195.	139.	51.	22.	
			(INCHES)	.266	.759	.837	.848
			(AC-FT)	97.	276.	304.	308.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	166.58-HR
+	(AC-FT)	(HR)				
+	154.	17.33	150.	97.	39.	17.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	166.58-HR
+	(FEET)	(HR)				
+	6.92	17.33	6.74	4.39	1.77	.78

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION
 TRANSPOSITION AREA

DETPB
 1.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)	(CFS)				
+	196.	17.42	191.	137.	50.	22.	
			(INCHES)	.261	.746	.823	.833
			(AC-FT)	95.	271.	299.	303.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	166.58-HR
+	(AC-FT)	(HR)				
+	151.	17.42	147.	95.	38.	17.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	166.58-HR
+	(FEET)	(HR)				
+	6.77	17.42	6.60	4.29	1.73	.77

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION
 TRANSPOSITION AREA

DETPB
 5.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW				
			6-HR	24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)	(CFS)				
+	182.	17.75	179.	128.	47.	20.	
			(INCHES)	.244	.697	.767	.776
			(AC-FT)	89.	253.	279.	282.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	166.58-HR
+	(AC-FT)	(HR)				
+	138.	17.75	134.	86.	35.	15.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	166.58-HR
+	(FEET)	(HR)				
+	6.19	17.75	6.04	3.91	1.58	.70

CUMULATIVE AREA = 6.81 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 10.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)	(CFS)				
+ 176.	17.67		176.	117.	43.	19.
		(INCHES)	.241	.637	.699	.703
		(AC-FT)	87.	231.	254.	255.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)					
+ 119.	17.75		115.	73.	30.	13.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)					
+ 5.34	17.83		5.19	3.32	1.36	.59

CUMULATIVE AREA = 6.81 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 20.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)	(CFS)				
+ 174.	17.58		173.	102.	37.	16.
		(INCHES)	.237	.557	.614	.619
		(AC-FT)	86.	202.	223.	225.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)					
+ 96.	17.67		93.	60.	25.	11.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)					
+ 4.36	17.67		4.20	2.74	1.15	.50

CUMULATIVE AREA = 6.81 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 30.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)	(CFS)				
+ 169.	17.75		161.	93.	35.	15.
		(INCHES)	.220	.510	.566	.570
		(AC-FT)	80.	185.	206.	207.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
			6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)					
+ 87.	17.75		84.	56.	24.	10.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
			6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)					
+ 3.92	17.75		3.79	2.53	1.07	.47

CUMULATIVE AREA = 6.81 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 40.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)	(CFS)				
+ 156.	18.25		149.	87.	32.	14.
		(INCHES)	.204	.476	.532	.536
		(AC-FT)	74.	173.	193.	195.

+		RETE7	820.	12.92	159.	43.	14.	1.12
	HYDROGRAPH AT							
+		DIVE7	234.	13.67	43.	13.	4.	1.12
	ROUTED TO							
+		E7STOR	1.	25.67	1.	1.	0.	1.12
	ROUTED TO							
+		E7E6	1.	30.00	1.	1.	0.	1.12
	HYDROGRAPH AT							
+		E6B	2187.	12.58	400.	132.	44.	1.95
	DIVERSION TO							
+		RETE6B	2187.	12.58	326.	91.	30.	1.95
	HYDROGRAPH AT							
+		DIVE6B	897.	13.00	131.	41.	14.	1.95
	HYDROGRAPH AT							
+		E8	901.	12.75	180.	57.	19.	1.10
	DIVERSION TO							
+		RETE8	901.	12.75	149.	41.	14.	1.10
	HYDROGRAPH AT							
+		DIVE8	378.	13.25	52.	16.	5.	1.10
	ROUTED TO							
+		E8E6	191.	14.00	50.	16.	5.	1.10
	3 COMBINED AT							
+		CPE6	897.	13.00	176.	57.	19.	3.05
	DIVERSION TO							
+		DRE9	104.	13.00	3.	1.	0.	3.05
	HYDROGRAPH AT							
+		DE6S	788.	13.00	169.	55.	18.	3.05
	ROUTED TO							
+		E6E15	497.	13.58	165.	55.	18.	3.05
	HYDROGRAPH AT							
+		E5B	447.	12.25	57.	19.	6.	.29
	DIVERSION TO							
+		RETE5B	447.	12.25	45.	13.	4.	.29
	HYDROGRAPH AT							
+		DIVE5B	204.	12.50	21.	7.	2.	.29
	ROUTED TO							
+		E5E14B	89.	12.92	20.	7.	2.	.29
	HYDROGRAPH AT							
+		E14B	884.	12.25	109.	36.	12.	.53
	DIVERSION TO							
+		RET14B	884.	12.25	88.	24.	8.	.53
	HYDROGRAPH AT							
+		DIV14B	372.	12.50	37.	12.	4.	.53
	2 COMBINED AT							
+		CP14B	371.	12.50	57.	18.	6.	.81
	ROUTED TO							
+		E14E15	210.	12.67	56.	18.	6.	.81
	HYDROGRAPH AT							
+		E15	1096.	12.33	154.	51.	17.	.78
	DIVERSION TO							
+		RETE15	1096.	12.33	122.	34.	11.	.78
	HYDROGRAPH AT							
+		DIVE15	431.	12.67	54.	17.	6.	.78
	3 COMBINED AT							
+		CPE15A	638.	13.58	256.	87.	29.	4.29
	HYDROGRAPH AT							
+		DRE9	104.	13.00	3.	1.	0.	3.05
	ROUTED TO							
+		RTE6E9	26.	13.42	3.	1.	0.	3.05
	HYDROGRAPH AT							
+		E9	968.	12.42	147.	48.	16.	.72
	DIVERSION TO							

+		RETE9	968.	12.42	118.	33.	11.	.72
+	HYDROGRAPH AT	DIVE9	372.	12.75	49.	15.	5.	.72
+	2 COMBINED AT	CPE9	372.	12.75	52.	16.	5.	1.07
+	DIVERSION TO	DRR5	195.	12.75	9.	2.	1.	1.07
+	HYDROGRAPH AT	DE9S	176.	12.75	43.	14.	5.	1.07
+	ROUTED TO	E9E16	121.	13.25	41.	14.	5.	1.07
+	HYDROGRAPH AT	DRR5	195.	12.75	9.	2.	1.	1.07
+	HYDROGRAPH AT	R5	546.	12.50	72.	21.	7.	.50
+	DIVERSION TO	RETR5	4.	4.67	2.	1.	0.	.50
+	HYDROGRAPH AT	DIVR5	546.	12.50	72.	21.	7.	.50
+	2 COMBINED AT	CPR5	545.	12.50	81.	23.	8.	1.07
+	ROUTED TO	R5R8	472.	12.92	81.	23.	8.	1.07
+	HYDROGRAPH AT	R8	741.	12.42	115.	39.	13.	.55
+	DIVERSION TO	RETR8	741.	12.42	91.	25.	8.	.55
+	HYDROGRAPH AT	DIVR8	366.	12.67	42.	13.	4.	.55
+	2 COMBINED AT	CPR8	732.	12.67	119.	36.	12.	1.62
+	ROUTED TO	R8E16	649.	13.00	119.	36.	12.	1.62
+	HYDROGRAPH AT	E16	582.	12.33	79.	26.	9.	.40
+	DIVERSION TO	RETE16	582.	12.33	64.	18.	6.	.40
+	HYDROGRAPH AT	DIVE16	213.	12.58	26.	8.	3.	.40
+	3 COMBINED AT	CPE16	721.	13.00	180.	56.	19.	2.52
+	ROUTED TO	E16E15	679.	13.33	177.	56.	19.	2.52
+	2 COMBINED AT	CPE15	1161.	13.50	405.	136.	45.	6.81
+	ROUTED TO	DETPB	179.	17.75	178.	123.	45.	6.81
+	ROUTED TO	E1524B	179.	17.92	178.	123.	45.	6.81
+	HYDROGRAPH AT	E25	1038.	12.50	184.	60.	20.	.93
+	DIVERSION TO	RETE25	1038.	12.50	164.	45.	15.	.93
+	HYDROGRAPH AT	DIVE25	240.	13.17	46.	15.	5.	.93
+	HYDROGRAPH AT	E24B	788.	12.25	100.	32.	11.	.46
+	DIVERSION TO	RET24B	788.	12.25	81.	22.	7.	.46
+	HYDROGRAPH AT	DIV24B	274.	12.58	32.	10.	3.	.46
+	3 COMBINED AT							

+		CPE24B	239.	14.58	217.	140.	51.	8.20
+	ROUTED TO	E24E28	237.	14.83	216.	139.	51.	8.20
+	HYDROGRAPH AT	E28B	773.	12.42	116.	37.	12.	.54
+	DIVERSION TO	RET28B	773.	12.42	95.	26.	9.	.54
+	HYDROGRAPH AT	DIV28B	316.	12.75	35.	11.	4.	.54
+	HYDROGRAPH AT	E29	1237.	12.50	203.	66.	22.	1.00
+	DIVERSION TO	RETE29	1237.	12.50	164.	45.	15.	1.00
+	HYDROGRAPH AT	DIVE29	573.	12.83	66.	21.	7.	1.00
+	3 COMBINED AT	CPE28B	538.	12.92	274.	163.	58.	9.74
+	ROUTED TO	E28E31	399.	13.25	270.	162.	58.	9.74
+	HYDROGRAPH AT	E31	964.	12.42	157.	52.	17.	.81
+	DIVERSION TO	RETE31	964.	12.42	125.	35.	12.	.81
+	HYDROGRAPH AT	DIVE31	402.	12.83	54.	17.	6.	.81
+	2 COMBINED AT	CPE31A	493.	13.25	302.	174.	62.	10.55
+	HYDROGRAPH AT	E32	404.	12.25	48.	16.	5.	.25
+	DIVERSION TO	RETE32	404.	12.25	38.	11.	4.	.25
+	HYDROGRAPH AT	DIVE32	136.	12.50	17.	5.	2.	.25
+	ROUTED TO	E32E31	68.	12.92	16.	5.	2.	.25
+	2 COMBINED AT	CPE31	523.	13.25	314.	177.	63.	10.80
+	ROUTED TO	E31E30	425.	13.75	307.	176.	63.	10.80
+	HYDROGRAPH AT	E30B	844.	12.83	186.	58.	19.	.88
+	DIVERSION TO	RET30B	844.	12.83	151.	41.	14.	.88
+	HYDROGRAPH AT	DIV30B	401.	13.33	55.	17.	6.	.88
+	2 COMBINED AT	CPE30	569.	13.75	343.	187.	67.	11.68
+	ROUTED TO	E30E26	549.	13.83	341.	187.	67.	11.68
+	HYDROGRAPH AT	E26B	415.	12.33	56.	18.	6.	.26
+	DIVERSION TO	RET26B	415.	12.33	45.	12.	4.	.26
+	HYDROGRAPH AT	DIV26B	146.	12.67	17.	5.	2.	.26
+	2 COMBINED AT	CPE26	557.	13.83	347.	189.	68.	11.94
+	ROUTED TO	E26E33	458.	14.50	337.	188.	68.	11.94
+	HYDROGRAPH AT	E33B	1304.	12.33	183.	59.	20.	.85
+	DIVERSION TO							

+		RET33B	1304.	12.33	149.	41.	14.	.85
+	HYDROGRAPH AT	DIV33B	526.	12.67	57.	18.	6.	.85
+	2 COMBINED AT	CPE33B	478.	14.50	356.	198.	72.	12.79

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1567.20	.00	27.	1.	.00	25.75	.00

PLAN 2			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1567.17	.00	27.	1.	.00	25.75	.00

PLAN 3			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1567.06	.00	24.	0.	.00	26.00	.00

PLAN 4			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.91	.00	21.	0.	.00	.00	.00

PLAN 5			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.72	.00	16.	0.	.00	.00	.00

PLAN 6			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.61	.00	14.	0.	.00	.00	.00

PLAN 7			INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION		1566.00		1574.00		1574.00	
	STORAGE		0.		607.		607.	
	OUTFLOW		0.		104.		104.	

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.53	.00	12.	0.	.00	.00	.00

PLAN 8	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
		1566.00	1574.00	1574.00
		0.	607.	607.
		0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.47	.00	11.	0.	.00	.00	.00

PLAN 9	ELEVATION STORAGE OUTFLOW	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
		1566.00	1574.00	1574.00
		0.	607.	607.
		0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.43	.00	10.	0.	.00	.00	.00

*** NORMAL END OF HEC-1 ***

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 28AUG14 TIME 09:00:07
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
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X X X X X
X X X X X
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Pecos Road Channel and Basin Design Concept Report
2 ID Alternative Analysis
3 ID Future Conditions
4 ID
5 ID Alternative 3: Storm drain from the Pecos Basin to the Ellsworth Channel
6 ID
7 ID Prepared for the Flood Control District of Maricopa County
8 ID District Project Number FCD 2014C001
9 ID
10 ID Prepared by Kimley-Horn and Associates, Inc.
11 ID Kimley Horn Project Number 091131024
12 ID August 2014
13 ID
14 ID Model based on the East Mesa Area Drainage Master Plan Update (EMADMPU)
15 ID for Alternative 1. The model was revised to include only those areas
16 ID contributing to the Ellsworth Channel.
17 ID
18 ID List of Changes:
19 ID - Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card
20 ID to a storage routing card with stage-storage-discharge data; the name
21 ID was changed from DIVPB to DETPB to reflect the change.
22 ID - Routing reach from CPR9 to CPR8 was eliminated
23 ID - Powerline section of the model was deleted (all subbasins north of the
24 ID future SR24 alignment).
25 ID - All subbasins south and east of R5 and R8 have been deleted.
26 ID - All comments from the East Mesa Area Drainage Master Plan Update that do
27 ID pertain to the Ellsworth Channel model have been deleted.
28 ID - Area has been adjusted on HC cards to account for reduction in area due
29 ID retention diversions.
30 ID
31 ID
32 ID
33 ID *****
34 ID ***** EAST MESA ADMPU *****
35 ID *****
36 ID
37 ID PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
38 ID CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
39 ID PREPARED BY: ENTELLUS, INC.
40 ID PROJECT NO: FCD 2011C017 ENTELLUS 310.057
41 ID MODIFIED DATE: 9/12/2012
42 ID MODELER: RLJ
43 ID
44 ID STORM: 100-YEAR 24-HOUR
45 ID
46 ID ALTERNATIVE: 1
47 ID
48 ID DEVELOPMENT CONDITIONS: FUTURE LAND USE
49 ID INCREASED FUTURE RETENTION (2.19->2.70 IN)
50 ID
51 ID PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
52 ID MERIDIAN CHANNEL
53 ID PECOS CHANNEL
54 ID MERIDIAN AND PECOS RETENTION BASIN
55 ID GERMANN CHANNEL
    
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HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

56 ID
 57 ID
 58 ID MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
 59 ID 100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
 60 ID VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
 61 ID SUBBASINS:
 62 ID
 63 ID E28B E29 E30B
 64 ID E31 E32 E33B
 65 ID
 66 ID MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
 67 ID RETOURED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
 68 ID WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
 69 ID PROPOSED RETENTION AT MERIDIAN AND PECOS.
 70 ID
 71 ID MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
 72 ID COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
 73 ID WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
 74 ID DEFINED ON PECOS ROAD.
 75 ID
 76 ID MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
 77 ID DIVVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS
 78 ID
 79 ID
 80 ID *****
 81 ID ***** EAST MESA ADMPU *****
 82 ID *****
 83 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
 84 ID Flood Control District of Maricopa County
 85 ID 100 YEAR
 86 ID 24 Hour Storm
 87 ID Unit Hydrograph: S-Graph
 88 ID 08/05/2011
 89 ID *****
 90 IT 5 12Aug14 0 2000 2000
 91 IN 15
 92 IO 5
 *DIAGRAM
 *
 93 JD 3.579 0.0001
 94 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
 95 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
 96 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
 97 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
 98 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
 99 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
 100 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
 101 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
 102 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
 103 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
 104 JD 3.561 1.0
 105 JD 3.490 5.0
 106 JD 3.400 10.0
 107 JD 3.286 20.0
 108 JD 3.221 30.0

HEC-1 INPUT

1

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109 JD 3.175 40.0
 110 JD 3.139 50.0
 111 JD 3.114 60.0
 *
 112 KK E7 BASIN
 113 KM Runoff from subbasin E7
 114 BA 1.124
 115 LG 0.24 0.26 5.10 0.32 35
 116 UI 0 64 64 102 224 281 328 369 416 477
 117 UI 561 725 814 670 575 512 449 390 339 300
 118 UI 226 159 113 106 99 64 64 46 20 20
 119 UI 20 20 20 20 20 20 0 0 0 0
 120 UI 0 0 0 0 0 0 0 0 0 0
 *
 121 KK DIVE7 DIVERT
 122 KM Divert the required retention volume for the subbasin out of the model
 123 DT RETE7 85.5 0.0
 124 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 125 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *
 126 KK E7STOR STORAGE
 127 RS 1 STOR
 128 SV 22.82 34.23 45.64 78.34 111.03 143.72 176.42 230.23 284.04
 129 SQ 1.75 5.50 11.00 17.70 25.70 34.20 43.00 51.70
 130 SE 1566.0 1567.00 1567.50 1568.00 1568.50 1569.00 1569.50 1570.00 1570.50 1571.00
 131 ST 1574.0 10000.0 3.0 1.5
 *

132 KK E7E6 ROUTE
 133 KM Route outfall from E7STOR to CPE6
 134 RS 23 FLOW
 135 RC 0.035 0.030 0.030 16362 0.0062 5.50
 136 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 137 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

138 KK E6B BASIN
 139 KM Runoff from subbasin E6B
 140 BA 1.949
 141 LG 0.14 0.25 6.00 0.24 59
 142 UI 0 174 277 677 898 1079 1330 1853 2099 1602
 143 UI 1321 1068 853 594 331 288 192 162 53 53
 144 UI 53 53 53 0 0 0 0 0 0 0
 145 UI 0 0 0 0 0 0 0 0 0 0
 146 UI 0 0 0 0 0 0 0 0 0 0
 *

1 HEC-1 INPUT PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

147 KK DIVE6B DIVERT
 148 KM Divert the required retention volume for the subbasin out of the model
 149 DT RETE6B 179.9 0.0
 150 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 151 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

152 KK E8 BASIN
 153 KM Runoff from subbasin E8
 154 BA 1.099
 155 LG 0.21 0.25 4.50 0.44 39
 156 UI 0 75 75 201 313 383 441 514 604 798
 157 UI 955 771 649 563 475 401 337 241 145 127
 158 UI 114 75 75 28 23 23 23 23 23 23
 159 UI 0 0 0 0 0 0 0 0 0 0
 160 UI 0 0 0 0 0 0 0 0 0 0
 *

161 KK DIVE8 DIVERT
 162 KM Divert the required retention volume for the subbasin out of the model
 163 DT RETE8 80.9 0.0
 164 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 165 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

166 KK E8E6 ROUTE
 167 KM Route runoff from subbasin E8 that is not retained to CPE6
 168 RS 9 FLOW
 169 RC 0.060 0.035 0.060 9833 0.0052 5.50
 170 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 171 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

172 KK CPE6 COMBINE
 173 KM Combine routed flow from E7STOR and subbasin E8 with unretained runoff from
 174 KM subbasin E6B.
 175 HC 3 3.05
 *

176 KK DE6S DIVERT
 177 KM Flow split diversion, DRE9 to the south, DE6S to the west
 178 DT DRE9 0.0 0.0
 179 DI 0.0 236.0 682.0 1141.0 1670.0 2261.0 2886.0 0.0 0.0 0.0
 180 DQ 0.0 1.0 13.0 212.0 633.0 1096.0 1568.0 0.0 0.0 0.0
 *

181 KK E6E15 ROUTE
 182 KM Route remaining flow from flow split at DE6S west to CPE15A
 183 RS 7 FLOW
 184 RC 0.035 0.030 0.035 8259 0.0042 5.50
 185 RX 950.00 975.00 991.00 1003.00 1007.00 1019.00 1030.00 1065.00
 186 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1 HEC-1 INPUT PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

187 KK E5B BASIN
 188 KM Runoff from subbasin E5B
 189 BA 0.286
 190 LG 0.14 0.25 3.95 0.64 62
 191 UI 0 64 225 342 567 435 287 148 74 36
 192 UI 15 15 0 0 0 0 0 0 0 0
 193 UI 0 0 0 0 0 0 0 0 0 0
 194 UI 0 0 0 0 0 0 0 0 0 0
 195 UI 0 0 0 0 0 0 0 0 0 0
 *

196 KK DIVE5B DIVERT
 197 KM Divert the required retention volume for the subbasin out of the model
 198 DT RETE5B 25.0 0.0
 199 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 200 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

201 KK E5E14B ROUTE
 202 KM Route runoff from subbasin E5B that is not retained to CP14B
 203 RS 5 FLOW
 204 RC 0.035 0.030 0.035 6256 0.0054 5.50
 205 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1050.00
 206 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

207 KK E14B BASIN
 208 KM Runoff from subbasin E14B
 209 BA 0.528
 210 LG 0.14 0.25 5.60 0.29 60
 211 UI 0 125 435 667 1086 785 512 237 126 53
 212 UI 29 29 0 0 0 0 0 0 0 0
 213 UI 0 0 0 0 0 0 0 0 0 0
 214 UI 0 0 0 0 0 0 0 0 0 0
 215 UI 0 0 0 0 0 0 0 0 0 0
 *

216 KK DIV14B DIVERT
 217 KM Divert the required retention volume for the subbasin out of the model
 218 DT RET14B 48.4 0.0
 219 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 220 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

221 KK CP14B COMBINE
 222 KM Combine routed flow from E5B with unretained runoff from subbasin E14B.
 223 HC 2
 *

1 HEC-1 INPUT PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

224 KK E14E15 ROUTE
 225 KM Route combined runoff from CP14B to CPE15A
 226 RS 2 FLOW
 227 RC 0.04 0.03 0.04 1840 0.0018
 228 RX 0 9 18 29 40 51 59 68
 229 RY 4 2 0 0 0 0 2 4
 *

230 KK E15 BASIN
 231 KM Runoff from subbasin E15
 232 BA 0.777
 233 LG 0.15 0.25 5.10 0.35 57
 234 UI 0 106 363 582 791 1239 1004 734 522 273
 235 UI 171 106 36 32 0 0 0 0 0 0
 236 UI 0 0 0 0 0 0 0 0 0 0
 237 UI 0 0 0 0 0 0 0 0 0 0
 238 UI 0 0 0 0 0 0 0 0 0 0
 *

239 KK DIVE15 DIVERT
 240 KM Divert the required retention volume for the subbasin out of the model
 241 DT RETE15 67.7 0.0
 242 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 243 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

244 KK CPE15A COMBINE
 245 KM Combine routed flow from split at CPE6 (DRE9, DE6S) and CP14B with unretained
 246 KM runoff from subbasin E15.
 247 HC 3 4.29
 *

248 KK DRE9RETRIEVE
 249 KM Retrieve flow from split at DRE9 that goes to the south
 250 DR DRE9
 *

251 KK RTE6E9 ROUTE
 252 KM Route split flow from CPE6 (DRE9) south to CPE9
 253 RS 5 FLOW
 254 RC 0.035 0.030 0.025 2200 0.0035 6.00
 255 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 256 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

257 KK E9 BASIN
 258 KM Runoff from subbasin E9
 259 BA 0.723
 260 LG 0.14 0.25 5.40 0.30 58
 261 UI 0 88 253 450 585 836 1040 754 570 416
 262 UI 225 148 92 48 27 27 27 0 0 0

263 UI 0 0 0 0 0 0 0 0 0 0 0
 264 UI 0 0 0 0 0 0 0 0 0 0 0
 265 UI 0 0 0 0 0 0 0 0 0 0 0
 *

1 HEC-1 INPUT PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

266 KK DIVE9 DIVERT
 267 KM Divert the required retention volume for the subbasin out of the model
 268 DT RETE9 65.4 0.0
 269 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 270 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

271 KK CPE9 COMBINE
 272 KM Combine routed flow from split at CPE6 (DRE9) with unretained runoff from
 273 KM subbasin E9
 274 HC 2 1.07
 *

275 KK DE9S DIVERT
 276 KM Flow split diversion, DRR5 to the south, DE9S to the west
 277 DT DRR5 0.0 0.0
 278 DI 0.0 78.0 163.0 440.0 936.0 1475.0 2024.0 0.0 0.0 0.0
 279 DQ 0.0 1.0 43.0 245.0 670.0 1157.0 1661.0 0.0 0.0 0.0
 *

280 KK E9E16 ROUTE
 281 KM Route remaining flow from flow split at DE9S west to CPE16
 282 RS 6 FLOW
 283 RC 0.035 0.030 0.035 6751 0.0040 5.50
 284 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1060.00
 285 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

286 KK DRR5RETRIEVE
 287 KM Retrieve flow from split at DRR5 that goes to the south
 288 DR DRR5
 *

289 KK R5 BASIN
 290 KM Runoff from subbasin R5
 291 BA 0.504
 292 LG 0.29 0.25 5.40 0.27 21
 293 UI 0 53 120 241 310 393 574 608 455 358
 294 UI 277 189 98 80 53 26 16 16 16 16
 295 UI 0 0 0 0 0 0 0 0 0 0
 296 UI 0 0 0 0 0 0 0 0 0 0
 297 UI 0 0 0 0 0 0 0 0 0 0
 *

298 KK DIVR5 DIVERT
 299 KM Divert the required retention volume for the subbasin out of the model
 300 DT RETR5 1.0 0.0
 301 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 302 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1 HEC-1 INPUT PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

303 KK CPR5 COMBINE
 304 KM Combine routed flow from split at CPE9 (DRR5) with unretained runoff from
 305 KM subbasin R5
 306 HC 2 1.07
 *

307 KK R5R8 ROUTE
 308 KM Route combined runoff from CPR5 to CPR8
 309 RS 5 FLOW
 310 RC 0.040 0.035 0.040 6587 0.0043 5.00
 311 RX 966.00 986.00 994.00 1006.00 1012.00 1024.00 1032.00 1052.00
 312 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
 *

313 KK R8 BASIN
 314 KM Runoff from subbasin R8
 315 BA 0.554
 316 LG 0.16 0.25 4.60 0.45 64
 317 UI 0 69 208 360 471 695 788 567 421 299
 318 UI 149 105 69 23 21 21 21 0 0 0
 319 UI 0 0 0 0 0 0 0 0 0 0
 320 UI 0 0 0 0 0 0 0 0 0 0
 321 UI 0 0 0 0 0 0 0 0 0 0
 *

322 KK DIVR8 DIVERT
 323 KM Divert the required retention volume for the subbasin out of the model
 324 DT RETR8 50.5 0.0
 325 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

386 KK DIVE25 DIVERT
 387 KM Divert the required retention volume for the subbasin out of the model
 388 KM MODIFIED MAX VOLUME FROM 110.7 TO 89.8
 389 DT RETE25 89.8 0.0
 390 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 391 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

392 KK E24B BASIN
 393 KM Runoff from subbasin E24B
 394 BA 0.464
 395 LG 0.15 0.15 7.30 0.14 57
 396 UI 0 92 339 513 852 731 493 294 133 76
 397 UI 24 24 0 0 0 0 0 0 0 0
 398 UI 0 0 0 0 0 0 0 0 0 0
 399 UI 0 0 0 0 0 0 0 0 0 0
 400 UI 0 0 0 0 0 0 0 0 0 0
 *

401 KK DIV24B DIVERT
 402 KM Divert the required retention volume for the subbasin out of the model
 403 KM MODIFIED MAX VOLUME FROM 38.7 TO 44.4
 404 DT RET24B 44.4 0.0
 405 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 406 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

407 KK CPE24B COMBINE
 408 KM Combine routed discharge from basin DETPB with unretained runoff from
 409 KM subbasins E25 and E24B in PECOS CHANNEL at Signal Butte & Pecos
 410 HC 3 8.20
 *

411 KK E24E28 ROUTE
 412 KM Route combined flows from CPE24B in PECOS CHANNEL to CPE28B at Crismon
 413 KM and Pecos
 414 RS 4 FLOW
 415 RC 0.035 0.035 0.035 5320 0.0035
 416 RX 0 11 21 24 28 31 42 52
 417 RY 7 4 0 0 0 0 4 7
 *

418 KK E28B BASIN
 419 KM Runoff from subbasin E28B
 420 BA 0.539
 421 LG 0.20 0.15 8.40 0.09 51
 422 UI 0 65 183 329 427 606 772 566 430 318
 423 UI 179 110 73 41 20 20 20 0 0 0
 424 UI 0 0 0 0 0 0 0 0 0 0
 425 UI 0 0 0 0 0 0 0 0 0 0
 HEC-1 INPUT

1 PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 426 UI 0 0 0 0 0 0 0 0 0 0
 *

427 KK DIV28B DIVERT
 428 KM Divert the required retention volume for the subbasin out of the model
 429 KM MODIFIED MAX VOLUME FROM 42.0 TO 51.3
 430 DT RET28B 51.3 0.0
 431 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 432 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

433 KK E29 BASIN
 434 KM Runoff from subbasin E29
 435 BA 1.002
 436 LG 0.15 0.23 6.20 0.22 55
 437 UI 0 103 218 452 586 733 1019 1240 924 737
 438 UI 574 428 229 172 116 82 31 31 31 31
 439 UI 0 0 0 0 0 0 0 0 0 0
 440 UI 0 0 0 0 0 0 0 0 0 0
 441 UI 0 0 0 0 0 0 0 0 0 0
 *

442 KK DIVE29 DIVERT
 443 KM Divert the required retention volume for the subbasin out of the model
 444 KM MODIFIED MAX VOLUME FROM 73.9 TO 90.2
 445 DT RETE29 90.2 0.0
 446 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 447 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

448 KK CPE28B COMBINE
 449 KM Combine routed flow from CPE24B with unretained runoff from subbasins E28B
 450 KM and E29 in the PECOS STORM DRAIN at Crismon and Pecos
 451 HC 3 9.74
 *

452 KK E28E31 ROUTE
 453 KM Route flows in the PECOS CHANNEL from CPE28B to CPE31 at Ellsworth and Pecos

```

454      RS      3      FLOW
455      RC      0.035  0.035  0.035  5400  0.0035
456      RX      0      11      21      25      29      33      44      54
457      RY      7      4      0      0      0      0      4      7
      *
458      KK      E31      BASIN
459      KM      Runoff from subbasin E31
460      BA      0.810
461      LG      0.15      0.25      4.80      0.39      55
462      UI      0      86      197      391      504      641      943      970      728      571
463      UI      441      296      151      126      86      37      26      26      26      0
464      UI      0      0      0      0      0      0      0      0      0      0
465      UI      0      0      0      0      0      0      0      0      0      0
466      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

467      KK      DIVE31  DIVERT
468      KM      Divert the required retention volume for the subbasin out of the model
469      KM      MODIFIED MAX VOLUME FROM 56.5 TO 68.9
470      DT      RETE31  68.9      0.0
471      DI      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
472      DQ      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

473      KK      CPE31A  COMBINE
474      KM      Combine routed flows from CPE28B with unretained runoff from subbasin E31 at
475      KM      in the PECOS CHANNEL at Ellsworth and Pecos
476      HC      2      10.55
      *
    
```

```

477      KK      E32      BASIN
478      KM      Runoff from subbasin E32
479      BA      0.246
480      LG      0.14      0.25      4.25      0.55      58
481      UI      0      72      238      387      535      337      190      78      37      15
482      UI      15      0      0      0      0      0      0      0      0      0
483      UI      0      0      0      0      0      0      0      0      0      0
484      UI      0      0      0      0      0      0      0      0      0      0
485      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

```

486      KK      DIVE32  DIVERT
487      KM      Divert the required retention volume for the subbasin out of the model
488      KM      MODIFIED MAX VOLUME FROM 17.2 TO 20.9
489      DT      RETE32  20.9      0.0
490      DI      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
491      DQ      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

492      KK      E32E31  ROUTE
493      KM      Route unretained runoff from subbasin E32 to CPE31
494      RS      5      FLOW
495      RC      0.025  0.060  0.025  3272  0.0028  1388.60
496      RX      100.00  110.00  128.00  149.80  160.00  191.50  209.20  210.00
497      RY      1388.3  1388.32  1388.32  1380.37  1380.17  1388.04  1388.39  1388.60
      *
    
```

```

498      KK      CPE31  COMBINE
499      KM      Combine unretained runoff from subbasin E32 with the flows from the PECOS
500      KM      CHANNEL at CPE31 - Ellsworth and Pecos
501      HC      2      10.80
      *
    
```

```

502      KK      E31E30  ROUTE
503      KM      Route runoff from CPE31 north in the Ellsworth Channel to CPE30
504      RS      5      FLOW
505      RC      0.025  0.045  0.025  4404  0.0008  1387.00
506      RX      100.00  107.00  112.50  144.90  175.10  201.50  225.90  244.00
507      RY      1386.1  1386.09  1386.09  1377.99  1377.99  1384.59  1385.08  1387.00
      *
    
```

1 HEC-1 INPUT PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

508      KK      E30B  BASIN
509      KM      Runoff from subbasin E30B
510      BA      0.882
511      LG      0.24      0.15      8.40      0.09      47
512      UI      0      56      56      128      217      272      314      357      416      500
513      UI      668      683      552      475      416      355      303      261      191      124
514      UI      98      92      66      56      44      17      17      17      17      0
515      UI      17      17      0      0      0      0      0      0      0      0
516      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

```

517      KK      DIV30B  DIVERT
518      KM      Divert the required retention volume for the subbasin out of the model
    
```

```

519      KM   MODIFIED MAX VOLUME FROM 67.1 TO 81.9
520      DT   RET30B   81.9   0.0
521      DI   0.0 10000.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
522      DQ   0.0 10000.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
*
523      KK   CPE30 COMBINE
524      KM   Combine routed flow from CPE31 in the Ellsworth Channel with unretained
525      KM   runoff from subbasin E30B
526      HC   2   11.68
*
527      KK   E30E26  ROUTE
528      KM   Route combined runoff from CPE30 to CPE26 in the Ellsworth Channel
529      RS   1   FLOW
530      RC   0.025 0.035 0.025 822 0.0005 1387.00
531      RX   100.00 105.00 108.50 149.90 220.10 251.30 279.10 285.10
532      RY   1387.0 1387.00 1386.66 1376.31 1376.31 1384.11 1384.66 1386.00
*
533      KK   E26B  BASIN
534      KM   Runoff from subbasin E26B
535      BA   0.259
536      LG   0.24 0.15 8.80 0.07 48
537      UI   0 38 145 222 320 448 315 222 139 65
538      UI   43 18 12 12 0 0 0 0 0 0
539      UI   0 0 0 0 0 0 0 0 0 0
540      UI   0 0 0 0 0 0 0 0 0 0
541      UI   0 0 0 0 0 0 0 0 0 0
*
542      KK   DIV26B  DIVERT
543      KM   Divert the required retention volume for the subbasin out of the model
544      KM   MODIFIED MAX VOLUME FROM 20.1 TO 24.5
545      DT   RET26B   24.5   0.0
546      DI   0.0 10000.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
547      DQ   0.0 10000.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
*
    
```

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

548      KK   CPE26 COMBINE
549      KM   Combined routed flows from CPE30 with unretained runoff from subbasin E26B
550      HC   2   11.94
*
551      KK   E26E33  ROUTE
552      KM   Route combine flows from CPE26 to CPE33 in the Ellsworth Channel
553      RS   5   FLOW
554      RC   0.025 0.030 0.025 8929 0.0028 1379.67
555      RX   100.00 100.50 102.50 134.90 205.10 237.50 253.50 255.00
556      RY   1379.1 1379.12 1379.35 1371.25 1371.25 1379.35 1379.67 1379.67
*
557      KK   E33B  BASIN
558      KM   Runoff from subbasin E33B
559      BA   0.851
560      LG   0.15 0.15 7.30 0.14 56
561      UI   0 117 409 651 892 1385 1087 793 558 278
562      UI   179 110 36 36 36 0 0 0 0 0
563      UI   0 0 0 0 0 0 0 0 0 0
564      UI   0 0 0 0 0 0 0 0 0 0
565      UI   0 0 0 0 0 0 0 0 0 0
*
566      KK   DIV33B  DIVERT
567      KM   Divert the required retention volume for the subbasin out of the model
568      KM   MODIFIED MAX VOLUME FROM 66.8 TO 81.5
569      DT   RET33B   81.5   0.0
570      DI   0.0 10000.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
571      DQ   0.0 10000.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
*
572      KK   CPE33B COMBINE
573      KM   Combine routed flows in the Ellsworth Channel from CPE26 with unretained
574      KM   runoff from subbasin E33B. Note this CP also receives flow from the
575      KM   Powerline model but that flow is not included in this model.
576      HC   2   12.79
*
577      ZZ
    
```

1 SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
112 E7
.
.
123 .-----> RETE7
    
```

```
121  DIVE7  
    V  
    V  
126  E7STOR  
    V  
    V  
132  E7E6  
    .  
138  .      E6B  
    .  
149  .      .-----> RETE6B  
147  .      DIVE6B  
    .  
152  .      .      E8  
    .      .  
163  .      .      .-----> RETE8  
161  .      .      DIVE8  
    .      .      V  
    .      .      V  
166  .      .      E8E6  
    .      .  
172  CPE6.....  
    .  
178  .-----> DRE9  
176  DE6S  
    V  
    V  
181  E6E15  
    .  
187  .      E5B  
    .  
198  .      .-----> RETE5B  
196  .      DIVE5B  
    .      V  
    .      V  
201  .      E5E14B  
    .  
207  .      .      E14B  
    .      .  
218  .      .      .-----> RET14B  
216  .      .      DIV14B  
    .      .  
221  .      CP14B.....  
    .      V  
    .      V  
224  .      E14E15  
    .  
230  .      .      E15  
    .      .  
241  .      .      .-----> RETE15  
239  .      .      DIVE15  
    .      .  
244  CPE15A.....  
    .  
250  .      .<----- DRE9  
248  .      DRE9  
    .      V  
    .      V  
251  .      RTE6E9  
    .  
257  .      .      E9  
    .      .  
268  .      .      .-----> RETE9  
266  .      .      DIVE9  
    .      .  
271  .      CPE9.....  
    .  
277  .      .-----> DRR5  
275  .      DE9S  
    .      V  
    .      V  
280  .      E9E16  
    .  
    .
```

```
288 . . . . . <----- DRR5
286 . . . . . DRR5
. . . . .
289 . . . . . R5
. . . . .
300 . . . . . -----> RETR5
298 . . . . . DIVR5
. . . . .
303 . . . . . CPR5.....
. . . . . V
. . . . . V
307 . . . . . R5R8
. . . . .
313 . . . . . R8
. . . . .
324 . . . . . -----> RETR8
322 . . . . . DIVR8
. . . . .
327 . . . . . CPR8.....
. . . . . V
. . . . . V
330 . . . . . R8E16
. . . . .
336 . . . . . E16
. . . . .
347 . . . . . -----> RETE16
345 . . . . . DIVE16
. . . . .
350 . . . . . CPE16.....
. . . . . V
. . . . . V
354 . . . . . E16E15
. . . . .
360 . . . . . CPE15.....
. . . . . V
. . . . . V
365 . . . . . DETPB
. . . . . V
. . . . . V
374 . . . . . E1524B
. . . . .
377 . . . . . E25
. . . . .
389 . . . . . -----> RETE25
386 . . . . . DIVE25
. . . . .
392 . . . . . E24B
. . . . .
404 . . . . . -----> RET24B
401 . . . . . DIV24B
. . . . .
407 . . . . . CPE24B.....
. . . . . V
. . . . . V
411 . . . . . E24E28
. . . . .
418 . . . . . E28B
. . . . .
430 . . . . . -----> RET28B
427 . . . . . DIV28B
. . . . .
433 . . . . . E29
. . . . .
445 . . . . . -----> RETE29
442 . . . . . DIVE29
. . . . .
448 . . . . . CPE28B.....
. . . . . V
. . . . . V
452 . . . . . E28E31
. . . . .
458 . . . . . E31
```

```

470 . . . . .
467 . . . . . DIVE31 -----> RETE31
473 CPE31A.....
477 . . . . . E32
489 . . . . .
486 . . . . . DIVE32 -----> RETE32
492 . . . . . V
492 . . . . . V
492 . . . . . E32E31
498 CPE31.....
498 . . . . . V
502 . . . . . V
502 E31E30
508 . . . . . E30B
520 . . . . .
517 . . . . . DIV30B -----> RET30B
523 CPE30.....
527 . . . . . V
527 . . . . . V
527 E30E26
533 . . . . . E26B
545 . . . . .
542 . . . . . DIV26B -----> RET26B
548 CPE26.....
551 . . . . . V
551 . . . . . V
551 E26E33
557 . . . . . E33B
569 . . . . .
566 . . . . . DIV33B -----> RET33B
572 CPE33B.....
    
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

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1*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 28AUG14 TIME 09:00:07 *
* *****
    
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*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
* *****
    
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Pecos Road Channel and Basin Design Concept Report
 Alternative Analysis
 Future Conditions

Alternative 3: Storm drain from the Pecos Basin to the Ellsworth Channel

Prepared for the Flood Control District of Maricopa County
 District Project Number FCD 2014C001

Prepared by Kimley-Horn and Associates, Inc.
 Kimley Horn Project Number 091131024
 August 2014

Model based on the East Mesa Area Drainage Master Plan Update (EMADMPU)
 for Alternative 1. The model was revised to include only those areas
 contributing to the Ellsworth Channel.

List of Changes:

- Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card to a storage routing card with stage-storage-discharge data; the name was changed from DIVPB to DETPB to reflect the change.
- Routing reach from CPR9 to CPR8 was eliminated
- Powerline section of the model was deleted (all subbasins north of the future SR24 alignment).
- All subbasins south and east of R5 and R8 have been deleted.
- All comments from the East Mesa Area Drainage Master Plan Update that do pertain to the Ellsworth Channel model have been deleted.
- Area has been adjusted on HC cards to account for reduction in area due retention diversions.

***** EAST MESA ADMPU *****

PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
PREPARED BY: ENTELLUS, INC.
PROJECT NO: FCD 2011C017 ENTELLUS 310.057
MODIFIED DATE: 9/12/2012
MODELER: RLJ

STORM: 100-YEAR 24-HOUR

ALTERNATIVE: 1

DEVELOPMENT CONDITIONS: FUTURE LAND USE INCREASED FUTURE RETENTION (2.19->2.70 IN)

PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
MERIDIAN CHANNEL
PECOS CHANNEL
MERIDIAN AND PECOS RETENTION BASIN
GERMANN CHANNEL

MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
SUBBASINS:

E28B	E29	E30B
E31	E32	E33B

MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
RETOUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
PROPOSED RETENTION AT MERIDIAN AND PECOS.

MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
DEFINED ON PECOS ROAD.

MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
DIVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS

***** EAST MESA ADMPU *****

FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
Flood Control District of Maricopa County
100 YEAR
24 Hour Storm
Unit Hydrograph: S-Graph
08/05/2011

92 IO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLST 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 5 MINUTES IN COMPUTATION INTERVAL
IDATE 12Aug14 STARTING DATE
ITIME 0000 STARTING TIME
NQ 2000 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 18 14 ENDING DATE
NDTIME 2235 ENDING TIME
ICENT 20 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
TOTAL TIME BASE 166.58 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET

369 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

370 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP STOR TYPE OF INITIAL CONDITION
 RSVRIC .00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

371 SV STORAGE .0 21.9 43.9 66.1 88.4 110.8 133.3 144.7 156.0
 372 SQ DISCHARGE 0. 15. 60. 119. 173. 176. 177. 189. 201.
 373 SE ELEVATION .00 1.00 2.00 3.00 4.00 5.00 6.00 6.50 7.00

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA .0 SQ MI

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 166.58-HR
 + 199. 17.33 (CFS) 195. 139. 51. 22.
 (INCHES) .266 .759 .837 .848
 (AC-FT) 97. 276. 304. 308.

PEAK STORAGE TIME MAXIMUM AVERAGE STORAGE
 + (AC-FT) (HR) 6-HR 24-HR 72-HR 166.58-HR
 154. 17.33 150. 97. 39. 17.

PEAK STAGE TIME MAXIMUM AVERAGE STAGE
 + (FEET) (HR) 6-HR 24-HR 72-HR 166.58-HR
 6.92 17.33 6.74 4.39 1.77 .78

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 1.0 SQ MI

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 166.58-HR
 + 196. 17.42 (CFS) 191. 137. 50. 22.
 (INCHES) .261 .746 .823 .833
 (AC-FT) 95. 271. 299. 303.

PEAK STORAGE TIME MAXIMUM AVERAGE STORAGE
 + (AC-FT) (HR) 6-HR 24-HR 72-HR 166.58-HR
 151. 17.42 147. 95. 38. 17.

PEAK STAGE TIME MAXIMUM AVERAGE STAGE
 + (FEET) (HR) 6-HR 24-HR 72-HR 166.58-HR
 6.77 17.42 6.60 4.29 1.73 .77

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 5.0 SQ MI

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
 + (CFS) (HR) 6-HR 24-HR 72-HR 166.58-HR
 + 182. 17.75 (CFS) 179. 128. 47. 20.
 (INCHES) .244 .697 .767 .776
 (AC-FT) 89. 253. 279. 282.

PEAK STORAGE TIME MAXIMUM AVERAGE STORAGE
 + (AC-FT) (HR) 6-HR 24-HR 72-HR 166.58-HR
 138. 17.75 134. 86. 35. 15.

PEAK STAGE TIME MAXIMUM AVERAGE STAGE

		6-HR	24-HR	72-HR	166.58-HR
+	(FEET)				
	6.19	17.75	6.04	3.91	1.58
					.70

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 10.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+	(CFS)				
	176.	17.67	176.	117.	43.
			.241	.637	.699
		(INCHES)	87.	231.	254.
		(AC-FT)			255.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+	(AC-FT)				
	119.	17.75	115.	73.	30.
					13.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+	(FEET)				
	5.34	17.83	5.19	3.32	1.36
					.59

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 20.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+	(CFS)				
	174.	17.58	173.	102.	37.
			.237	.557	.614
		(INCHES)	86.	202.	223.
		(AC-FT)			225.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+	(AC-FT)				
	96.	17.67	93.	60.	25.
					11.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+	(FEET)				
	4.36	17.67	4.20	2.74	1.15
					.50

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 30.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+	(CFS)				
	169.	17.75	161.	93.	35.
			.220	.510	.566
		(INCHES)	80.	185.	206.
		(AC-FT)			207.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+	(AC-FT)				
	87.	17.75	84.	56.	24.
					10.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+	(FEET)				
	3.92	17.75	3.79	2.53	1.07
					.47

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 40.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+	(CFS)				

156.	18.25	(CFS)	149.	87.	32.	14.
		(INCHES)	.204	.476	.532	.536
		(AC-FT)	74.	173.	193.	195.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
	81.	18.17	79.	53.	23.	10.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)		6-HR	24-HR	72-HR	166.58-HR
	3.69	18.25	3.56	2.42	1.03	.45

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 50.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+ 146.	18.50	(CFS)	140.	82.	31.	13.
		(INCHES)	.192	.450	.505	.509
		(AC-FT)	70.	164.	183.	185.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
	77.	18.50	75.	51.	22.	10.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)		6-HR	24-HR	72-HR	166.58-HR
	3.51	18.50	3.40	2.33	1.00	.44

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 60.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+ 140.	18.75	(CFS)	134.	79.	30.	13.
		(INCHES)	.183	.432	.487	.491
		(AC-FT)	67.	157.	177.	178.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
	75.	18.75	72.	50.	21.	9.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)		6-HR	24-HR	72-HR	166.58-HR
	3.39	18.75	3.28	2.27	.98	.43

CUMULATIVE AREA = 6.81 SQ MI

INTERPOLATED HYDROGRAPH AT DETPB

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+ (CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+ 179.	17.75	(CFS)	178.	123.	45.	20.
		(INCHES)	.243	.670	.737	.744
		(AC-FT)	88.	243.	268.	270.

CUMULATIVE AREA = 6.81 SQ MI

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			

+	HYDROGRAPH AT	E7	820.	12.92	182.	56.	19.	1.12
+	DIVERSION TO	RETE7	820.	12.92	159.	43.	14.	1.12
+	HYDROGRAPH AT	DIVE7	234.	13.67	43.	13.	4.	1.12
+	ROUTED TO	E7STOR	1.	25.67	1.	1.	0.	1.12
+	ROUTED TO	E7E6	1.	30.00	1.	1.	0.	1.12
+	HYDROGRAPH AT	E6B	2187.	12.58	400.	132.	44.	1.95
+	DIVERSION TO	RETE6B	2187.	12.58	326.	91.	30.	1.95
+	HYDROGRAPH AT	DIVE6B	897.	13.00	131.	41.	14.	1.95
+	HYDROGRAPH AT	E8	901.	12.75	180.	57.	19.	1.10
+	DIVERSION TO	RETE8	901.	12.75	149.	41.	14.	1.10
+	HYDROGRAPH AT	DIVE8	378.	13.25	52.	16.	5.	1.10
+	ROUTED TO	E8E6	191.	14.00	50.	16.	5.	1.10
+	3 COMBINED AT	CPE6	897.	13.00	176.	57.	19.	3.05
+	DIVERSION TO	DRE9	104.	13.00	3.	1.	0.	3.05
+	HYDROGRAPH AT	DE6S	788.	13.00	169.	55.	18.	3.05
+	ROUTED TO	E6E15	497.	13.58	165.	55.	18.	3.05
+	HYDROGRAPH AT	E5B	447.	12.25	57.	19.	6.	.29
+	DIVERSION TO	RETE5B	447.	12.25	45.	13.	4.	.29
+	HYDROGRAPH AT	DIVE5B	204.	12.50	21.	7.	2.	.29
+	ROUTED TO	E5E14B	89.	12.92	20.	7.	2.	.29
+	HYDROGRAPH AT	E14B	884.	12.25	109.	36.	12.	.53
+	DIVERSION TO	RET14B	884.	12.25	88.	24.	8.	.53
+	HYDROGRAPH AT	DIV14B	372.	12.50	37.	12.	4.	.53
+	2 COMBINED AT	CP14B	371.	12.50	57.	18.	6.	.81
+	ROUTED TO	E14E15	210.	12.67	56.	18.	6.	.81
+	HYDROGRAPH AT	E15	1096.	12.33	154.	51.	17.	.78
+	DIVERSION TO	RETE15	1096.	12.33	122.	34.	11.	.78
+	HYDROGRAPH AT	DIVE15	431.	12.67	54.	17.	6.	.78
+	3 COMBINED AT	CPE15A	638.	13.58	256.	87.	29.	4.29
+	HYDROGRAPH AT	DRE9	104.	13.00	3.	1.	0.	3.05
+	ROUTED TO	RTE6E9	26.	13.42	3.	1.	0.	3.05

+	HYDROGRAPH AT	E9	968.	12.42	147.	48.	16.	.72
	DIVERSION TO							
+		RETE9	968.	12.42	118.	33.	11.	.72
	HYDROGRAPH AT							
+		DIVE9	372.	12.75	49.	15.	5.	.72
	2 COMBINED AT							
+		CPE9	372.	12.75	52.	16.	5.	1.07
	DIVERSION TO							
+		DRR5	195.	12.75	9.	2.	1.	1.07
	HYDROGRAPH AT							
+		DE9S	176.	12.75	43.	14.	5.	1.07
	ROUTED TO							
+		E9E16	121.	13.25	41.	14.	5.	1.07
	HYDROGRAPH AT							
+		DRR5	195.	12.75	9.	2.	1.	1.07
	HYDROGRAPH AT							
+		R5	546.	12.50	72.	21.	7.	.50
	DIVERSION TO							
+		RETR5	4.	4.67	2.	1.	0.	.50
	HYDROGRAPH AT							
+		DIVR5	546.	12.50	72.	21.	7.	.50
	2 COMBINED AT							
+		CPR5	545.	12.50	81.	23.	8.	1.07
	ROUTED TO							
+		R5R8	472.	12.92	81.	23.	8.	1.07
	HYDROGRAPH AT							
+		R8	741.	12.42	115.	39.	13.	.55
	DIVERSION TO							
+		RETR8	741.	12.42	91.	25.	8.	.55
	HYDROGRAPH AT							
+		DIVR8	366.	12.67	42.	13.	4.	.55
	2 COMBINED AT							
+		CPR8	732.	12.67	119.	36.	12.	1.62
	ROUTED TO							
+		R8E16	649.	13.00	119.	36.	12.	1.62
	HYDROGRAPH AT							
+		E16	582.	12.33	79.	26.	9.	.40
	DIVERSION TO							
+		RETE16	582.	12.33	64.	18.	6.	.40
	HYDROGRAPH AT							
+		DIVE16	213.	12.58	26.	8.	3.	.40
	3 COMBINED AT							
+		CPE16	721.	13.00	180.	56.	19.	2.52
	ROUTED TO							
+		E16E15	679.	13.33	177.	56.	19.	2.52
	2 COMBINED AT							
+		CPE15	1161.	13.50	405.	136.	45.	6.81
	ROUTED TO							
+		DETPB	179.	17.75	178.	123.	45.	6.81
	ROUTED TO							
+		E1524B	179.	17.83	178.	123.	45.	6.81
	HYDROGRAPH AT							
+		E25	1038.	12.50	184.	60.	20.	.93
	DIVERSION TO							
+		RETE25	1038.	12.50	164.	45.	15.	.93
	HYDROGRAPH AT							
+		DIVE25	240.	13.17	46.	15.	5.	.93
	HYDROGRAPH AT							
+		E24B	788.	12.25	100.	32.	11.	.46
	DIVERSION TO							
+		RET24B	788.	12.25	81.	22.	7.	.46

+	HYDROGRAPH AT	DIV24B	274.	12.58	32.	10.	3.	.46
+	3 COMBINED AT	CPE24B	243.	14.42	219.	140.	51.	8.20
+	ROUTED TO	E24E28	242.	14.67	218.	140.	51.	8.20
+	HYDROGRAPH AT	E28B	773.	12.42	116.	37.	12.	.54
+	DIVERSION TO	RET28B	773.	12.42	95.	26.	9.	.54
+	HYDROGRAPH AT	DIV28B	316.	12.75	35.	11.	4.	.54
+	HYDROGRAPH AT	E29	1237.	12.50	203.	66.	22.	1.00
+	DIVERSION TO	RETE29	1237.	12.50	164.	45.	15.	1.00
+	HYDROGRAPH AT	DIVE29	573.	12.83	66.	21.	7.	1.00
+	3 COMBINED AT	CPE28B	539.	12.92	279.	163.	58.	9.74
+	ROUTED TO	E28E31	400.	13.25	274.	162.	58.	9.74
+	HYDROGRAPH AT	E31	964.	12.42	157.	52.	17.	.81
+	DIVERSION TO	RETE31	964.	12.42	125.	35.	12.	.81
+	HYDROGRAPH AT	DIVE31	402.	12.83	54.	17.	6.	.81
+	2 COMBINED AT	CPE31A	495.	13.25	306.	174.	62.	10.55
+	HYDROGRAPH AT	E32	404.	12.25	48.	16.	5.	.25
+	DIVERSION TO	RETE32	404.	12.25	38.	11.	4.	.25
+	HYDROGRAPH AT	DIVE32	136.	12.50	17.	5.	2.	.25
+	ROUTED TO	E32E31	68.	12.92	16.	5.	2.	.25
+	2 COMBINED AT	CPE31	524.	13.25	318.	178.	64.	10.80
+	ROUTED TO	E31E30	427.	13.75	312.	177.	63.	10.80
+	HYDROGRAPH AT	E30B	844.	12.83	186.	58.	19.	.88
+	DIVERSION TO	RET30B	844.	12.83	151.	41.	14.	.88
+	HYDROGRAPH AT	DIV30B	401.	13.33	55.	17.	6.	.88
+	2 COMBINED AT	CPE30	571.	13.75	348.	187.	67.	11.68
+	ROUTED TO	E30E26	551.	13.83	345.	187.	67.	11.68
+	HYDROGRAPH AT	E26B	415.	12.33	56.	18.	6.	.26
+	DIVERSION TO	RET26B	415.	12.33	45.	12.	4.	.26
+	HYDROGRAPH AT	DIV26B	146.	12.67	17.	5.	2.	.26
+	2 COMBINED AT	CPE26	559.	13.83	351.	189.	68.	11.94
+	ROUTED TO	E26E33	463.	14.50	342.	189.	68.	11.94

+	HYDROGRAPH AT	E33B	1304.	12.33	183.	59.	20.	.85
+	DIVERSION TO	RET33B	1304.	12.33	149.	41.	14.	.85
+	HYDROGRAPH AT	DIV33B	526.	12.67	57.	18.	6.	.85
+	2 COMBINED AT	CPE33B	483.	14.58	361.	199.	72.	12.79

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR STORM = 1	STORM AREA (SQ MI) =			.00					
E1524B	MANE	5.00	199.12	1045.00	.85	5.00	199.12	1045.00	.85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3078E+03 EXCESS= .0000E+00 OUTFLOW= .3078E+03 BASIN STORAGE= .7116E-02 PERCENT ERROR= .0

FOR STORM = 2	STORM AREA (SQ MI) =			1.00					
E1524B	MANE	5.00	195.58	1050.00	.83	5.00	195.58	1050.00	.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3025E+03 EXCESS= .0000E+00 OUTFLOW= .3025E+03 BASIN STORAGE= .7037E-02 PERCENT ERROR= .0

FOR STORM = 3	STORM AREA (SQ MI) =			5.00					
E1524B	MANE	5.00	181.59	1070.00	.78	5.00	181.59	1070.00	.78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2818E+03 EXCESS= .0000E+00 OUTFLOW= .2818E+03 BASIN STORAGE= .6933E-02 PERCENT ERROR= .0

FOR STORM = 4	STORM AREA (SQ MI) =			10.00					
E1524B	MANE	5.00	176.34	1070.00	.70	5.00	176.34	1070.00	.70

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2555E+03 EXCESS= .0000E+00 OUTFLOW= .2555E+03 BASIN STORAGE= .6368E-03 PERCENT ERROR= .0

FOR STORM = 5	STORM AREA (SQ MI) =			20.00					
E1524B	MANE	5.00	174.08	1065.00	.62	5.00	174.08	1065.00	.62

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2247E+03 EXCESS= .0000E+00 OUTFLOW= .2247E+03 BASIN STORAGE= .6066E-03 PERCENT ERROR= .0

FOR STORM = 6	STORM AREA (SQ MI) =			30.00					
E1524B	MANE	5.00	168.82	1070.00	.57	5.00	168.82	1070.00	.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2071E+03 EXCESS= .0000E+00 OUTFLOW= .2071E+03 BASIN STORAGE= .6004E-03 PERCENT ERROR= .0

FOR STORM = 7	STORM AREA (SQ MI) =			40.00					
E1524B	MANE	5.00	156.05	1100.00	.54	5.00	156.05	1100.00	.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1947E+03 EXCESS= .0000E+00 OUTFLOW= .1947E+03 BASIN STORAGE= .5998E-03 PERCENT ERROR= .0

FOR STORM = 8	STORM AREA (SQ MI) =			50.00					
E1524B	MANE	5.00	146.46	1115.00	.51	5.00	146.46	1115.00	.51

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1850E+03 EXCESS= .0000E+00 OUTFLOW= .1850E+03 BASIN STORAGE= .6009E-03 PERCENT ERROR= .0

FOR STORM = 9	STORM AREA (SQ MI) =			60.00					
E1524B	MANE	5.00	140.00	1130.00	.49	5.00	140.00	1130.00	.49

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1783E+03 EXCESS= .0000E+00 OUTFLOW= .1783E+03 BASIN STORAGE= .6007E-03 PERCENT ERROR= .0

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	1566.00	1574.00	1574.00
STORAGE	0.	607.	607.
OUTFLOW	0.	104.	104.

	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.20	.00	27.	1.	.00	25.75	.00
PLAN 2			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.17	.00	27.	1.	.00	25.75	.00
PLAN 3			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.06	.00	24.	0.	.00	26.00	.00
PLAN 4			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.91	.00	21.	0.	.00	.00	.00
PLAN 5			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.72	.00	16.	0.	.00	.00	.00
PLAN 6			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.61	.00	14.	0.	.00	.00	.00
PLAN 7			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.53	.00	12.	0.	.00	.00	.00
PLAN 8			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	1566.00	1574.00	1574.00			
		STORAGE	0.	607.	607.			
		OUTFLOW	0.	104.	104.			

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.47	.00	11.	0.	.00	.00	.00

PLAN 9	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	1566.00	1566.00	1574.00	1574.00
	STORAGE	0.	607.	607.
	OUTFLOW	0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.43	.00	10.	0.	.00	.00	.00

*** NORMAL END OF HEC-1 ***

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 28AUG14 TIME 09:02:10
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Pecos Road Channel and Basin Design Concept Report
2 ID Alternative Analysis
3 ID Future Conditions
4 ID
5 ID Alternative 3: Storm drain from the Pecos Basin to the Ellsworth Channel
6 ID
7 ID Prepared for the Flood Control District of Maricopa County
8 ID District Project Number FCD 2014C001
9 ID
10 ID Prepared by Kimley-Horn and Associates, Inc.
11 ID Kimley Horn Project Number 091131024
12 ID August 2014
13 ID
14 ID Model based on the East Mesa Area Drainage Master Plan Update (EMADMPU)
15 ID for Alternative 1. The model was revised to include only those areas
16 ID contributing to the Ellsworth Channel.
17 ID
18 ID List of Changes:
19 ID - Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card
20 ID to a storage routing card with stage-storage-discharge data; the name
21 ID was changed from DIVPB to DETPB to reflect the change.
22 ID - Routing reach from CPR9 to CPR8 was eliminated
23 ID - Powerline section of the model was deleted (all subbasins north of the
24 ID future SR24 alignment).
25 ID - All subbasins south and east of R5 and R8 have been deleted.
26 ID - All comments from the East Mesa Area Drainage Master Plan Update that do
27 ID pertain to the Ellsworth Channel model have been deleted.
28 ID - Area has been adjusted on HC cards to account for reduction in area due
29 ID retention diversions.
30 ID
31 ID
32 ID
33 ID *****
34 ID ***** EAST MESA ADMPU *****
35 ID *****
36 ID
37 ID PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
38 ID CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
39 ID PREPARED BY: ENTELLUS, INC.
40 ID PROJECT NO: FCD 2011C017 ENTELLUS 310.057
41 ID MODIFIED DATE: 9/12/2012
42 ID MODELER: RLJ
43 ID
44 ID STORM: 100-YEAR 24-HOUR
45 ID
46 ID ALTERNATIVE: 1
47 ID
48 ID DEVELOPMENT CONDITIONS: FUTURE LAND USE
49 ID INCREASED FUTURE RETENTION (2.19->2.70 IN)
50 ID
51 ID PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
52 ID MERIDIAN CHANNEL
53 ID PECOS CHANNEL
54 ID MERIDIAN AND PECOS RETENTION BASIN
55 ID GERMANN CHANNEL
    
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HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

56 ID
 57 ID
 58 ID MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
 59 ID 100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
 60 ID VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
 61 ID SUBBASINS:
 62 ID
 63 ID E28B E29 E30B
 64 ID E31 E32 E33B
 65 ID
 66 ID MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
 67 ID RETOUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
 68 ID WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
 69 ID PROPOSED RETENTION AT MERIDIAN AND PECOS.
 70 ID
 71 ID MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
 72 ID COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
 73 ID WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
 74 ID DEFINED ON PECOS ROAD.
 75 ID
 76 ID MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
 77 ID DIVVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS
 78 ID
 79 ID
 80 ID *****
 81 ID ***** EAST MESA ADMPU *****
 82 ID *****
 83 ID FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
 84 ID Flood Control District of Maricopa County
 85 ID 100 YEAR
 86 ID 24 Hour Storm
 87 ID Unit Hydrograph: S-Graph
 88 ID 08/05/2011
 89 ID *****
 90 IT 5 12Aug14 0 2000 2000
 91 IN 15
 92 IO 5
 *DIAGRAM
 *
 93 JD 3.579 0.0001
 94 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
 95 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
 96 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
 97 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
 98 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
 99 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
 100 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
 101 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
 102 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
 103 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
 104 JD 3.561 1.0
 105 JD 3.490 5.0
 106 JD 3.400 10.0
 107 JD 3.286 20.0
 108 JD 3.221 30.0

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

109 JD 3.175 40.0
 110 JD 3.139 50.0
 111 JD 3.114 60.0
 *
 112 KK E7 BASIN
 113 KM Runoff from subbasin E7
 114 BA 1.124
 115 LG 0.24 0.26 5.10 0.32 35
 116 UI 0 64 64 102 224 281 328 369 416 477
 117 UI 561 725 814 670 575 512 449 390 339 300
 118 UI 226 159 113 106 99 64 64 46 20 20
 119 UI 20 20 20 20 20 20 0 0 0 0
 120 UI 0 0 0 0 0 0 0 0 0 0
 *
 121 KK DIVE7 DIVERT
 122 KM Divert the required retention volume for the subbasin out of the model
 123 DT RETE7 85.5 0.0
 124 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 125 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *
 126 KK E7STOR STORAGE
 127 RS 1 STOR
 128 SV 22.82 34.23 45.64 78.34 111.03 143.72 176.42 230.23 284.04
 129 SQ 1.75 5.50 11.00 17.70 25.70 34.20 43.00 51.70
 130 SE 1566.0 1567.00 1567.50 1568.00 1568.50 1569.00 1569.50 1570.00 1570.50 1571.00
 131 ST 1574.0 10000.0 3.0 1.5
 *

132 KK E7E6 ROUTE
 133 KM Route outfall from E7STOR to CPE6
 134 RS 23 FLOW
 135 RC 0.035 0.030 0.030 16362 0.0062 5.50
 136 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 137 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

138 KK E6B BASIN
 139 KM Runoff from subbasin E6B
 140 BA 1.949
 141 LG 0.14 0.25 6.00 0.24 59
 142 UI 0 174 277 677 898 1079 1330 1853 2099 1602
 143 UI 1321 1068 853 594 331 288 192 162 53 53
 144 UI 53 53 53 0 0 0 0 0 0 0
 145 UI 0 0 0 0 0 0 0 0 0 0
 146 UI 0 0 0 0 0 0 0 0 0 0
 *

1 HEC-1 INPUT PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

147 KK DIVE6B DIVERT
 148 KM Divert the required retention volume for the subbasin out of the model
 149 DT RETE6B 179.9 0.0
 150 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 151 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

152 KK E8 BASIN
 153 KM Runoff from subbasin E8
 154 BA 1.099
 155 LG 0.21 0.25 4.50 0.44 39
 156 UI 0 75 75 201 313 383 441 514 604 798
 157 UI 955 771 649 563 475 401 337 241 145 127
 158 UI 114 75 75 28 23 23 23 23 23 23
 159 UI 0 0 0 0 0 0 0 0 0 0
 160 UI 0 0 0 0 0 0 0 0 0 0
 *

161 KK DIVE8 DIVERT
 162 KM Divert the required retention volume for the subbasin out of the model
 163 DT RETE8 80.9 0.0
 164 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 165 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

166 KK E8E6 ROUTE
 167 KM Route runoff from subbasin E8 that is not retained to CPE6
 168 RS 9 FLOW
 169 RC 0.060 0.035 0.060 9833 0.0052 5.50
 170 RX 0.00 500.00 980.00 1003.00 1007.00 1031.00 1511.00 2011.00
 171 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

172 KK CPE6 COMBINE
 173 KM Combine routed flow from E7STOR and subbasin E8 with unretained runoff from
 174 KM subbasin E6B.
 175 HC 3 3.05
 *

176 KK DE6S DIVERT
 177 KM Flow split diversion, DRE9 to the south, DE6S to the west
 178 DT DRE9 0.0 0.0
 179 DI 0.0 236.0 682.0 1141.0 1670.0 2261.0 2886.0 0.0 0.0 0.0
 180 DQ 0.0 1.0 13.0 212.0 633.0 1096.0 1568.0 0.0 0.0 0.0
 *

181 KK E6E15 ROUTE
 182 KM Route remaining flow from flow split at DE6S west to CPE15A
 183 RS 7 FLOW
 184 RC 0.035 0.030 0.035 8259 0.0042 5.50
 185 RX 950.00 975.00 991.00 1003.00 1007.00 1019.00 1030.00 1065.00
 186 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

1 HEC-1 INPUT PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

187 KK E5B BASIN
 188 KM Runoff from subbasin E5B
 189 BA 0.286
 190 LG 0.14 0.25 3.95 0.64 62
 191 UI 0 64 225 342 567 435 287 148 74 36
 192 UI 15 15 0 0 0 0 0 0 0 0
 193 UI 0 0 0 0 0 0 0 0 0 0
 194 UI 0 0 0 0 0 0 0 0 0 0
 195 UI 0 0 0 0 0 0 0 0 0 0
 *

196 KK DIVE5B DIVERT
 197 KM Divert the required retention volume for the subbasin out of the model
 198 DT RETE5B 25.0 0.0
 199 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 200 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

201 KK E5E14B ROUTE
 202 KM Route runoff from subbasin E5B that is not retained to CP14B
 203 RS 5 FLOW
 204 RC 0.035 0.030 0.035 6256 0.0054 5.50
 205 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1050.00
 206 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

207 KK E14B BASIN
 208 KM Runoff from subbasin E14B
 209 BA 0.528
 210 LG 0.14 0.25 5.60 0.29 60
 211 UI 0 125 435 667 1086 785 512 237 126 53
 212 UI 29 29 0 0 0 0 0 0 0 0
 213 UI 0 0 0 0 0 0 0 0 0 0
 214 UI 0 0 0 0 0 0 0 0 0 0
 215 UI 0 0 0 0 0 0 0 0 0 0
 *

216 KK DIV14B DIVERT
 217 KM Divert the required retention volume for the subbasin out of the model
 218 DT RET14B 48.4 0.0
 219 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 220 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

221 KK CP14B COMBINE
 222 KM Combine routed flow from E5B with unretained runoff from subbasin E14B.
 223 HC 2
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

224 KK E14E15 ROUTE
 225 KM Route combined runoff from CP14B to CPE15A
 226 RS 2 FLOW
 227 RC 0.04 0.03 0.04 1840 0.0018
 228 RX 0 9 18 29 40 51 59 68
 229 RY 4 2 0 0 0 0 2 4
 *

230 KK E15 BASIN
 231 KM Runoff from subbasin E15
 232 BA 0.777
 233 LG 0.15 0.25 5.10 0.35 57
 234 UI 0 106 363 582 791 1239 1004 734 522 273
 235 UI 171 106 36 32 32 0 0 0 0 0
 236 UI 0 0 0 0 0 0 0 0 0 0
 237 UI 0 0 0 0 0 0 0 0 0 0
 238 UI 0 0 0 0 0 0 0 0 0 0
 *

239 KK DIVE15 DIVERT
 240 KM Divert the required retention volume for the subbasin out of the model
 241 DT RETE15 67.7 0.0
 242 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 243 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

244 KK CPE15A COMBINE
 245 KM Combine routed flow from split at CPE6 (DRE9, DE6S) and CP14B with unretained
 246 KM runoff from subbasin E15.
 247 HC 3 4.29
 *

248 KK DRE9RETRIEVE
 249 KM Retrieve flow from split at DRE9 that goes to the south
 250 DR DRE9
 *

251 KK RTE6E9 ROUTE
 252 KM Route split flow from CPE6 (DRE9) south to CPE9
 253 RS 5 FLOW
 254 RC 0.035 0.030 0.025 2200 0.0035 6.00
 255 RX 0.00 100.00 700.00 1050.00 1090.00 1110.00 1140.00 1240.00
 256 RY 0.00 6.00 4.00 1.00 1.00 5.00 6.00 6.00
 *

257 KK E9 BASIN
 258 KM Runoff from subbasin E9
 259 BA 0.723
 260 LG 0.14 0.25 5.40 0.30 58
 261 UI 0 88 253 450 585 836 1040 754 570 416
 262 UI 225 148 92 48 27 27 27 0 0 0

263 UI 0 0 0 0 0 0 0 0 0 0 0
 264 UI 0 0 0 0 0 0 0 0 0 0 0
 265 UI 0 0 0 0 0 0 0 0 0 0 0
 *

1 HEC-1 INPUT PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

266 KK DIVE9 DIVERT
 267 KM Divert the required retention volume for the subbasin out of the model
 268 DT RETE9 65.4 0.0
 269 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 270 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

271 KK CPE9 COMBINE
 272 KM Combine routed flow from split at CPE6 (DRE9) with unretained runoff from
 273 KM subbasin E9
 274 HC 2 1.07
 *

275 KK DE9S DIVERT
 276 KM Flow split diversion, DRR5 to the south, DE9S to the west
 277 DT DRR5 0.0 0.0
 278 DI 0.0 78.0 163.0 440.0 936.0 1475.0 2024.0 0.0 0.0 0.0
 279 DQ 0.0 1.0 43.0 245.0 670.0 1157.0 1661.0 0.0 0.0 0.0
 *

280 KK E9E16 ROUTE
 281 KM Route remaining flow from flow split at DE9S west to CPE16
 282 RS 6 FLOW
 283 RC 0.035 0.030 0.035 6751 0.0040 5.50
 284 RX 950.00 985.00 991.00 1003.00 1007.00 1019.00 1025.00 1060.00
 285 RY 5.50 4.50 4.00 1.00 1.00 4.00 4.50 5.50
 *

286 KK DRR5RETRIEVE
 287 KM Retrieve flow from split at DRR5 that goes to the south
 288 DR DRR5
 *

289 KK R5 BASIN
 290 KM Runoff from subbasin R5
 291 BA 0.504
 292 LG 0.29 0.25 5.40 0.27 21
 293 UI 0 53 120 241 310 393 574 608 455 358
 294 UI 277 189 98 80 53 26 16 16 16 16
 295 UI 0 0 0 0 0 0 0 0 0 0
 296 UI 0 0 0 0 0 0 0 0 0 0
 297 UI 0 0 0 0 0 0 0 0 0 0
 *

298 KK DIVR5 DIVERT
 299 KM Divert the required retention volume for the subbasin out of the model
 300 DT RETR5 1.0 0.0
 301 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 302 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

1 HEC-1 INPUT PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

303 KK CPR5 COMBINE
 304 KM Combine routed flow from split at CPE9 (DRR5) with unretained runoff from
 305 KM subbasin R5
 306 HC 2 1.07
 *

307 KK R5R8 ROUTE
 308 KM Route combined runoff from CPR5 to CPR8
 309 RS 5 FLOW
 310 RC 0.040 0.035 0.040 6587 0.0043 5.00
 311 RX 966.00 986.00 994.00 1006.00 1012.00 1024.00 1032.00 1052.00
 312 RY 5.00 4.50 4.00 1.00 1.00 4.00 4.50 5.00
 *

313 KK R8 BASIN
 314 KM Runoff from subbasin R8
 315 BA 0.554
 316 LG 0.16 0.25 4.60 0.45 64
 317 UI 0 69 208 360 471 695 788 567 421 299
 318 UI 149 105 69 23 21 21 21 0 0 0
 319 UI 0 0 0 0 0 0 0 0 0 0
 320 UI 0 0 0 0 0 0 0 0 0 0
 321 UI 0 0 0 0 0 0 0 0 0 0
 *

322 KK DIVR8 DIVERT
 323 KM Divert the required retention volume for the subbasin out of the model
 324 DT RETR8 50.5 0.0
 325 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0

```

326      DQ      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
      *
327      KK      CPR8 COMBINE
328      KM      Combine routed runoff from CPR5 with unretained runoff from subbasin R8
329      HC      2      1.62
      *
330      KK      R8E16 ROUTE
331      KM      Route combined flows from CPR8 to CPE16 in the proposed MERIDIAN SOUTH CHANNE
332      RS      3      FLOW
333      RC      0.03      0.04      0.03      2660      0.001
334      RX      0      16      33      45      58      71      87      103
335      RY      7      3      0      0      0      0      3      7
      *
336      KK      E16 BASIN
337      KM      Runoff from subbasin E16
338      BA      0.396
339      LG      0.15      0.25      5.10      0.35      57
340      UI      0      58      224      342      497      684      480      338      207      100
341      UI      64      26      18      18      0      0      0      0      0      0
342      UI      0      0      0      0      0      0      0      0      0      0
343      UI      0      0      0      0      0      0      0      0      0      0
344      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

345      KK      DIVE16 DIVERT
346      KM      Divert the required retention volume for the subbasin out of the model
347      DT      RETE16      35.1      0.0
348      DI      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
349      DQ      0.0 10000.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0      0.0
      *
    
```

```

350      KK      CPE16 COMBINE
351      KM      Combine routed flow from split at CPE9 (DRR5, DE9S) and routed flow from CPR8
352      KM      with unretained runoff from subbasin E16.
353      HC      3      2.52
      *
    
```

```

354      KK      E16E15 ROUTE
355      KM      Route combined flows from CPE16 to CPE15 in the MERIDIAN SOUTH CHANNEL
356      RS      4      FLOW
357      RC      0.03      0.04      0.03      4120      0.001
358      RX      0      16      33      44      56      68      84      100
359      RY      7      3      0      0      0      0      3      7
      *
    
```

```

360      KK      CPE15 COMBINE
361      KM      Combine routed flows from CPE16 in the MERIDIAN SOUTH CHANNEL with flows
362      KM      from the north and east at the southwest corner of Pecos and Meridian. These
363      KM      flows combine in the proposed Pecos Basin (DETPB)
364      HC      2      6.81
      *
    
```

```

365      KK      DETPB STORAGE
366      KM      Proposed inline retention basin at SWC Meridian and Pecos
367      KM      Basin is 7-ft deep basin, but the top foot is not included (freeboard)
368      KM      Side slopes are 4:1, outlet pipe is 60-in RCP
369      KO      3
370      RS      1      STOR
371      SV      0      21.9      43.9      66.1      88.4      110.8      133.3      144.7      156.0
372      SQ      0      15      60      119      173      176      177      189      201
373      SE      0      1      2      3      4      5      6      6.5      7
      *
    
```

```

374      KK      E1524B ROUTE
375      KM      Route discharge from basin DETPB in PECOS STORM DRAIN to Signal Butte & Pecos
376      RD      3800      0.0035      0.013      CIRC      7
      *
    
```

```

377      KK      E25 BASIN
378      KM      Runoff from subbasin E25
379      BA      0.932
380      LG      0.15      0.25      5.40      0.30      55
381      UI      0      86      146      342      451      546      683      986      969      749
382      UI      613      490      383      234      148      125      86      51      26      26
383      UI      26      26      0      0      0      0      0      0      0      0
384      UI      0      0      0      0      0      0      0      0      0      0
385      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

386      KK      DIVE25 DIVERT
387      KM      Divert the required retention volume for the subbasin out of the model
388      KM      MODIFIED MAX VOLUME FROM 110.7 TO 89.8
    
```



```

*
458 KK E28E31 ROUTE
459 KM Route flows in the PECOS STORM DRAIN from CPE28B to CPE31 at Ellsworth and Pe
460 RD 5400 0.0035 0.013 CIRC 9
*
HEC-1 INPUT
PAGE 12
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

461 KK E31 BASIN
462 KM Runoff from subbasin E31
463 BA 0.810
464 LG 0.15 0.25 4.80 0.39 55
465 UI 0 86 197 391 504 641 943 970 728 571
466 UI 441 296 151 126 86 37 26 26 26 0
467 UI 0 0 0 0 0 0 0 0 0 0
468 UI 0 0 0 0 0 0 0 0 0 0
469 UI 0 0 0 0 0 0 0 0 0 0
*

470 KK DIVE31 DIVERT
471 KM Divert the required retention volume for the subbasin out of the model
472 KM MODIFIED MAX VOLUME FROM 56.5 TO 68.9
473 DT RETE31 68.9 0.0
474 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
475 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
    
```

```

476 KK CPE31A COMBINE
477 KM Combine routed flows from CPE28B with unretained runoff from subbasin E31 at
478 KM in the PECOS CHANNEL at Ellsworth and Pecos
479 HC 2 10.55
*
    
```

```

480 KK E32 BASIN
481 KM Runoff from subbasin E32
482 BA 0.246
483 LG 0.14 0.25 4.25 0.55 58
484 UI 0 72 238 387 535 337 190 78 37 15
485 UI 15 0 0 0 0 0 0 0 0 0
486 UI 0 0 0 0 0 0 0 0 0 0
487 UI 0 0 0 0 0 0 0 0 0 0
488 UI 0 0 0 0 0 0 0 0 0 0
*
    
```

```

489 KK DIVE32 DIVERT
490 KM Divert the required retention volume for the subbasin out of the model
491 KM MODIFIED MAX VOLUME FROM 17.2 TO 20.9
492 DT RETE32 20.9 0.0
493 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
494 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
*
    
```

```

495 KK E32E31 ROUTE
496 KM Route unretained runoff from subbasin E32 to CPE31
497 RS 5 FLOW
498 RC 0.025 0.060 0.025 3272 0.0028 1388.60
499 RX 100.00 110.00 128.00 149.80 160.00 191.50 209.20 210.00
500 RY 1388.3 1388.32 1388.32 1380.37 1380.17 1388.04 1388.39 1388.60
*
    
```

HEC-1 INPUT PAGE 13
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

501 KK CPE31 COMBINE
502 KM Combine unretained runoff from subbasin E32 with the flows from the PECOS
503 KM CHANNEL at CPE31 - Ellsworth and Pecos
504 HC 2 10.80
*
    
```

```

505 KK E31E30 ROUTE
506 KM Route runoff from CPE31 north in the Ellsworth Channel to CPE30
507 RS 5 FLOW
508 RC 0.025 0.045 0.025 4404 0.0008 1387.00
509 RX 100.00 107.00 112.50 144.90 175.10 201.50 225.90 244.00
510 RY 1386.1 1386.09 1386.09 1377.99 1377.99 1384.59 1385.08 1387.00
*
    
```

```

511 KK E30B BASIN
512 KM Runoff from subbasin E30B
513 BA 0.882
514 LG 0.24 0.15 8.40 0.09 47
515 UI 0 56 56 128 217 272 314 357 416 500
516 UI 668 683 552 475 416 355 303 261 191 124
517 UI 98 92 66 56 44 17 17 17 17 17
518 UI 17 17 0 0 0 0 0 0 0 0
519 UI 0 0 0 0 0 0 0 0 0 0
*
    
```

```

520 KK DIV30B DIVERT
    
```

521 KM Divert the required retention volume for the subbasin out of the model
 522 KM MODIFIED MAX VOLUME FROM 67.1 TO 81.9
 523 DT RET30B 81.9 0.0
 524 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 525 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

526 KK CPE30 COMBINE
 527 KM Combine routed flow from CPE31 in the Ellsworth Channel with unretained
 528 KM runoff from subbasin E30B
 529 HC 2 11.68
 *

530 KK E30E26 ROUTE
 531 KM Route combined runoff from CPE30 to CPE26 in the Ellsworth Channel
 532 RS 1 FLOW
 533 RC 0.025 0.035 0.025 822 0.0005 1387.00
 534 RX 100.00 105.00 108.50 149.90 220.10 251.30 279.10 285.10
 535 RY 1387.0 1387.00 1386.66 1376.31 1376.31 1384.11 1384.66 1386.00
 *

536 KK E26B BASIN
 537 KM Runoff from subbasin E26B
 538 BA 0.259
 539 LG 0.24 0.15 8.80 0.07 48
 540 UI 0 38 145 222 320 448 315 222 139 65
 541 UI 43 18 12 12 0 0 0 0 0 0
 542 UI 0 0 0 0 0 0 0 0 0 0
 HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
 543 UI 0 0 0 0 0 0 0 0 0 0
 544 UI 0 0 0 0 0 0 0 0 0 0
 *

545 KK DIV26B DIVERT
 546 KM Divert the required retention volume for the subbasin out of the model
 547 KM MODIFIED MAX VOLUME FROM 20.1 TO 24.5
 548 DT RET26B 24.5 0.0
 549 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 550 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

551 KK CPE26 COMBINE
 552 KM Combined routed flows from CPE30 with unretained runoff from subbasin E26B
 553 HC 2 11.94
 *

554 KK E26E33 ROUTE
 555 KM Route combine flows from CPE26 to CPE33 in the Ellsworth Channel
 556 RS 5 FLOW
 557 RC 0.025 0.030 0.025 8929 0.0028 1379.67
 558 RX 100.00 100.50 102.50 134.90 205.10 237.50 253.50 255.00
 559 RY 1379.1 1379.12 1379.35 1371.25 1371.25 1379.35 1379.67 1379.67
 *

560 KK E33B BASIN
 561 KM Runoff from subbasin E33B
 562 BA 0.851
 563 LG 0.15 0.15 7.30 0.14 56
 564 UI 0 117 409 651 892 1385 1087 793 558 278
 565 UI 179 110 36 36 36 0 0 0 0 0
 566 UI 0 0 0 0 0 0 0 0 0 0
 567 UI 0 0 0 0 0 0 0 0 0 0
 568 UI 0 0 0 0 0 0 0 0 0 0
 *

569 KK DIV33B DIVERT
 570 KM Divert the required retention volume for the subbasin out of the model
 571 KM MODIFIED MAX VOLUME FROM 66.8 TO 81.5
 572 DT RET33B 81.5 0.0
 573 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 574 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

575 KK CPE33B COMBINE
 576 KM Combine routed flows in the Ellsworth Channel from CPE26 with unretained
 577 KM runoff from subbasin E33B. Note this CP also receives flow from the
 578 KM Powerline model but that flow is not included in this model.
 579 HC 2 12.79
 *
 580 ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
 112 E7

```
123      .----->  RETE7
121      DIVE7
          V
          V
126      E7STOR
          V
          V
132      E7E6
          .
138      .          E6B
          .
149      .          .----->  RETE6B
147      .          DIVE6B
          .
152      .          .          E8
          .          .
163      .          .          .----->  RETE8
161      .          .          DIVE8
          .          .          V
          .          .          V
166      .          .          E8E6
          .          .
172      CPE6.....
          .
178      .----->  DRE9
176      DE6S
          V
          V
181      E6E15
          .
187      .          E5B
          .
198      .          .----->  RETE5B
196      .          DIVE5B
          .          V
          .          V
201      .          E5E14B
          .
207      .          .          E14B
          .          .
218      .          .          .----->  RET14B
216      .          .          DIV14B
          .          .
221      .          .          CP14B.....
          .          .          V
          .          .          V
224      .          .          E14E15
          .          .
230      .          .          E15
          .          .
241      .          .          .----->  RETE15
239      .          .          DIVE15
          .          .
244      CPE15A.....
          .
250      .          .-----<  DRE9
248      .          DRE9
          .          V
          .          V
251      .          RTE6E9
          .
257      .          .          E9
          .          .
268      .          .          .----->  RETE9
266      .          .          DIVE9
          .          .
271      .          .          CPE9.....
          .
277      .          .----->  DRR5
275      .          DE9S
          .          V
          .          V
280      .          .          E9E16
          .          .
```

```
288 . . . . . <----- DRR5
286 . . . . . DRR5
. . . . .
289 . . . . . R5
. . . . .
300 . . . . . -----> RETR5
298 . . . . . DIVR5
. . . . .
303 . . . . . CPR5.....
. . . . . V
. . . . . V
307 . . . . . R5R8
. . . . .
313 . . . . . R8
. . . . .
324 . . . . . -----> RETR8
322 . . . . . DIVR8
. . . . .
327 . . . . . CPR8.....
. . . . . V
. . . . . V
330 . . . . . R8E16
. . . . .
336 . . . . . E16
. . . . .
347 . . . . . -----> RETE16
345 . . . . . DIVE16
. . . . .
350 . . . . . CPE16.....
. . . . . V
. . . . . V
354 . . . . . E16E15
. . . . .
360 . . . . . CPE15.....
. . . . . V
. . . . . V
365 . . . . . DETPB
. . . . . V
. . . . . V
374 . . . . . E1524B
. . . . .
377 . . . . . E25
. . . . .
389 . . . . . -----> RETE25
386 . . . . . DIVE25
. . . . .
392 . . . . . E24B
. . . . .
404 . . . . . -----> RET24B
401 . . . . . DIV24B
. . . . .
407 . . . . . CPE24B.....
. . . . . V
. . . . . V
411 . . . . . DET222
. . . . . V
. . . . . V
420 . . . . . E24E28
. . . . .
424 . . . . . E28B
. . . . .
436 . . . . . -----> RET28B
433 . . . . . DIV28B
. . . . .
439 . . . . . E29
. . . . .
451 . . . . . -----> RETE29
448 . . . . . DIVE29
. . . . .
454 . . . . . CPE28B.....
. . . . . V
. . . . . V
```

```

458 E28E31
      .
461 .      E31
      .
473 .      .-----> RETE31
470 .      DIVE31
      .
476 CPE31A.....
      .
480 .      E32
      .
492 .      .-----> RETE32
489 .      DIVE32
      .
      V
495 .      E32E31
      .
501 CPE31.....
      .
      V
505 E31E30
      .
511 .      E30B
      .
523 .      .-----> RET30B
520 .      DIV30B
      .
526 CPE30.....
      .
      V
530 E30E26
      .
536 .      E26B
      .
548 .      .-----> RET26B
545 .      DIV26B
      .
551 CPE26.....
      .
      V
554 E26E33
      .
560 .      E33B
      .
572 .      .-----> RET33B
569 .      DIV33B
      .
575 CPE33B.....
    
```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*   JUN 1998 *
*   VERSION 4.1 *
* RUN DATE 28AUG14 TIME 09:02:10 *
*
*****
    
```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*
*****
    
```

Pecos Road Channel and Basin Design Concept Report
 Alternative Analysis
 Future Conditions

Alternative 3: Storm drain from the Pecos Basin to the Ellsworth Channel

Prepared for the Flood Control District of Maricopa County
 District Project Number FCD 2014C001

Prepared by Kimley-Horn and Associates, Inc.
 Kimley Horn Project Number 091131024
 August 2014

Model based on the East Mesa Area Drainage Master Plan Update (EMADMPU)

for Alternative 1. The model was revised to include only those areas contributing to the Ellsworth Channel.

List of Changes:

- Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card to a storage routing card with stage-storage-discharge data; the name was changed from DIVPB to DETPB to reflect the change.
- Routing reach from CPR9 to CPR8 was eliminated
- Powerline section of the model was deleted (all subbasins north of the future SR24 alignment).
- All subbasins south and east of R5 and R8 have been deleted.
- All comments from the East Mesa Area Drainage Master Plan Update that do pertain to the Ellsworth Channel model have been deleted.
- Area has been adjusted on HC cards to account for reduction in area due retention diversions.

 ***** EAST MESA ADMPU *****

PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
 CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
 PREPARED BY: ENTELLUS, INC.
 PROJECT NO: FCD 2011C017 ENTELLUS 310.057
 MODIFIED DATE: 9/12/2012
 MODELER: RLJ

STORM: 100-YEAR 24-HOUR

ALTERNATIVE: 1

DEVELOPMENT CONDITIONS: FUTURE LAND USE
 INCREASED FUTURE RETENTION (2.19->2.70 IN)

PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
 MERIDIAN CHANNEL
 PECOS CHANNEL
 MERIDIAN AND PECOS RETENTION BASIN
 GERMANN CHANNEL

MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
 100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
 VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
 SUBBASINS:

E28B	E29	E30B	
E31	E32	E33B	

MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
 RETOUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
 WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
 PROPOSED RETENTION AT MERIDIAN AND PECOS.

MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
 COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
 WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
 DEFINED ON PECOS ROAD.

MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
 DIVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS

 ***** EAST MESA ADMPU *****

FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
 Flood Control District of Maricopa County
 100 YEAR
 24 Hour Storm
 Unit Hydrograph: S-Graph
 08/05/2011

92 IO OUTPUT CONTROL VARIABLES
 IPRNT 5 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 5 MINUTES IN COMPUTATION INTERVAL
 IDATE 12Aug14 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 2000 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 18 14 ENDING DATE
 NDTIME 2235 ENDING TIME
 ICENT 20 CENTURY MARK

COMPUTATION INTERVAL .08 HOURS
 TOTAL TIME BASE 166.58 HOURS

365 KK * *
 * DETPB * STORAGE
 * *

369 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

370 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP STOR TYPE OF INITIAL CONDITION
 RSVRIC .00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

371 SV	STORAGE	.0	21.9	43.9	66.1	88.4	110.8	133.3	144.7	156.0
372 SQ	DISCHARGE	0.	15.	60.	119.	173.	176.	177.	189.	201.
373 SE	ELEVATION	.00	1.00	2.00	3.00	4.00	5.00	6.00	6.50	7.00

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA .0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	199.	17.33	(CFS)			
			195.	139.	51.	22.
		(INCHES)	.266	.759	.837	.848
		(AC-FT)	97.	276.	304.	308.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	154.	17.33				
			150.	97.	39.	17.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+	(FEET)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	6.92	17.33				
			6.74	4.39	1.77	.78

CUMULATIVE AREA = 6.81 SQ MI

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 1.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	196.	17.42	(CFS)			
			191.	137.	50.	22.
		(INCHES)	.261	.746	.823	.833
		(AC-FT)	95.	271.	299.	303.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	151.	17.42				
			147.	95.	38.	17.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+	(FEET)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	6.77	17.42				
			6.60	4.29	1.73	.77

CUMULATIVE AREA = 6.81 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 5.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+	182.	17.75	(CFS)			
			179.	128.	47.	20.
		(INCHES)	.244	.697	.767	.776
		(AC-FT)	89.	253.	279.	282.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+	(AC-FT)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+						

+ (AC-FT) (HR) 138. 17.75 134. 86. 35. 15.

PEAK STAGE TIME 6-HR MAXIMUM AVERAGE STAGE 24-HR 72-HR 166.58-HR

+ (FEET) (HR) 6.19 17.75 6.04 3.91 1.58 .70

CUMULATIVE AREA = 6.81 SQ MI

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 10.0 SQ MI

PEAK FLOW TIME 6-HR MAXIMUM AVERAGE FLOW 24-HR 72-HR 166.58-HR

+ (CFS) (HR) (CFS) 176. 17.67 176. 117. 43. 19.

(INCHES) .241 .637 .699 .703
 (AC-FT) 87. 231. 254. 255.

PEAK STORAGE TIME 6-HR MAXIMUM AVERAGE STORAGE 24-HR 72-HR 166.58-HR

+ (AC-FT) (HR) 119. 17.75 115. 73. 30. 13.

PEAK STAGE TIME 6-HR MAXIMUM AVERAGE STAGE 24-HR 72-HR 166.58-HR

+ (FEET) (HR) 5.34 17.83 5.19 3.32 1.36 .59

CUMULATIVE AREA = 6.81 SQ MI

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 20.0 SQ MI

PEAK FLOW TIME 6-HR MAXIMUM AVERAGE FLOW 24-HR 72-HR 166.58-HR

+ (CFS) (HR) (CFS) 174. 17.58 173. 102. 37. 16.

(INCHES) .237 .557 .614 .619
 (AC-FT) 86. 202. 223. 225.

PEAK STORAGE TIME 6-HR MAXIMUM AVERAGE STORAGE 24-HR 72-HR 166.58-HR

+ (AC-FT) (HR) 96. 17.67 93. 60. 25. 11.

PEAK STAGE TIME 6-HR MAXIMUM AVERAGE STAGE 24-HR 72-HR 166.58-HR

+ (FEET) (HR) 4.36 17.67 4.20 2.74 1.15 .50

CUMULATIVE AREA = 6.81 SQ MI

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 30.0 SQ MI

PEAK FLOW TIME 6-HR MAXIMUM AVERAGE FLOW 24-HR 72-HR 166.58-HR

+ (CFS) (HR) (CFS) 169. 17.75 161. 93. 35. 15.

(INCHES) .220 .510 .566 .570
 (AC-FT) 80. 185. 206. 207.

PEAK STORAGE TIME 6-HR MAXIMUM AVERAGE STORAGE 24-HR 72-HR 166.58-HR

+ (AC-FT) (HR) 87. 17.75 84. 56. 24. 10.

PEAK STAGE TIME 6-HR MAXIMUM AVERAGE STAGE 24-HR 72-HR 166.58-HR

+ (FEET) (HR) 3.92 17.75 3.79 2.53 1.07 .47

CUMULATIVE AREA = 6.81 SQ MI

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 40.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR
+	(CFS)	(HR)				
		(CFS)				
+	156.	18.25	149.	87.	32.	14.
		(INCHES)	.204	.476	.532	.536
		(AC-FT)	74.	173.	193.	195.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR
+	(AC-FT)	(HR)				
		(HR)				
+	81.	18.17	79.	53.	23.	10.
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE 24-HR	72-HR	166.58-HR
+	(FEET)	(HR)				
		(HR)				
+	3.69	18.25	3.56	2.42	1.03	.45
CUMULATIVE AREA =			6.81 SQ MI			

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 50.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR
+	(CFS)	(HR)				
		(CFS)				
+	146.	18.50	140.	82.	31.	13.
		(INCHES)	.192	.450	.505	.509
		(AC-FT)	70.	164.	183.	185.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR
+	(AC-FT)	(HR)				
		(HR)				
+	77.	18.50	75.	51.	22.	10.
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE 24-HR	72-HR	166.58-HR
+	(FEET)	(HR)				
		(HR)				
+	3.51	18.50	3.40	2.33	1.00	.44
CUMULATIVE AREA =			6.81 SQ MI			

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 60.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR
+	(CFS)	(HR)				
		(CFS)				
+	140.	18.75	134.	79.	30.	13.
		(INCHES)	.183	.432	.487	.491
		(AC-FT)	67.	157.	177.	178.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR
+	(AC-FT)	(HR)				
		(HR)				
+	75.	18.75	72.	50.	21.	9.
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE 24-HR	72-HR	166.58-HR
+	(FEET)	(HR)				
		(HR)				
+	3.39	18.75	3.28	2.27	.98	.43
CUMULATIVE AREA =			6.81 SQ MI			

INTERPOLATED HYDROGRAPH AT DETPB

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR
+	(CFS)	(HR)				
		(CFS)				
+	179.	17.75	178.	123.	45.	20.
		(INCHES)	.243	.670	.737	.744
		(AC-FT)	88.	243.	268.	270.
CUMULATIVE AREA =			6.81 SQ MI			

PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)						
	48.	24.17	48.	34.	13.		6.

PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)						
	6.17	24.17	6.09	4.32	1.67		.73

CUMULATIVE AREA = 8.20 SQ MI

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 10.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)						
	191.	24.17					
			(CFS)				
			188.	133.	49.		21.
			(INCHES)	.602	.671		.676
			(AC-FT)	93.	263.	294.	296.

PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)						
	47.	24.17	46.	30.	12.		5.

PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)						
	6.01	24.17	5.89	3.89	1.51		.66

CUMULATIVE AREA = 8.20 SQ MI

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 20.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)						
	181.	21.75					
			(CFS)				
			176.	115.	43.		19.
			(INCHES)	.523	.586		.591
			(AC-FT)	87.	229.	256.	258.

PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)						
	43.	21.75	42.	26.	10.		4.

PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)						
	5.57	21.75	5.39	3.31	1.30		.57

CUMULATIVE AREA = 8.20 SQ MI

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 30.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)						
	168.	21.42					
			(CFS)				
			163.	105.	40.		17.
			(INCHES)	.477	.538		.542
			(AC-FT)	81.	209.	235.	237.

PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)						
	39.	21.42	38.	23.	9.		4.

PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)						
	5.02	21.42	4.88	2.96	1.17		.51

CUMULATIVE AREA = 8.20 SQ MI

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 40.0 SQ MI

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	166.58-HR	
+ (CFS)	(HR)					
+ 155.	22.00	151.	98.	37.	16.	
		(INCHES)	.171	.444	.504	.508
		(AC-FT)	75.	194.	220.	222.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE				
		6-HR	24-HR	72-HR	166.58-HR	
+ (AC-FT)	(HR)					
+ 36.	22.00	35.	21.	8.	4.	
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE				
		6-HR	24-HR	72-HR	166.58-HR	
+ (FEET)	(HR)					
+ 4.61	22.00	4.47	2.71	1.09	.47	
CUMULATIVE AREA =		8.20 SQ MI				
***	***	***	***	***	***	

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 50.0 SQ MI

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	166.58-HR	
+ (CFS)	(HR)					
+ 144.	22.75	141.	92.	35.	15.	
		(INCHES)	.160	.418	.477	.481
		(AC-FT)	70.	183.	209.	210.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE				
		6-HR	24-HR	72-HR	166.58-HR	
+ (AC-FT)	(HR)					
+ 33.	22.75	32.	19.	8.	3.	
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE				
		6-HR	24-HR	72-HR	166.58-HR	
+ (FEET)	(HR)					
+ 4.25	22.75	4.11	2.50	1.01	.44	
CUMULATIVE AREA =		8.20 SQ MI				
***	***	***	***	***	***	

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 60.0 SQ MI

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	166.58-HR	
+ (CFS)	(HR)					
+ 141.	26.58	138.	88.	34.	15.	
		(INCHES)	.156	.401	.458	.462
		(AC-FT)	68.	175.	200.	202.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE				
		6-HR	24-HR	72-HR	166.58-HR	
+ (AC-FT)	(HR)					
+ 30.	23.33	29.	18.	7.	3.	
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE				
		6-HR	24-HR	72-HR	166.58-HR	
+ (FEET)	(HR)					
+ 3.88	23.33	3.74	2.31	.95	.41	
CUMULATIVE AREA =		8.20 SQ MI				
***	***	***	***	***	***	

INTERPOLATED HYDROGRAPH AT DET222

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
		6-HR	24-HR	72-HR	166.58-HR	
+ (CFS)	(HR)					
+ 192.	24.17	190.	137.	51.	22.	
		(INCHES)	.215	.619	.691	.697
		(AC-FT)	94.	271.	302.	305.
CUMULATIVE AREA =		8.20 SQ MI				

+		CPE15A	638.	13.58	256.	87.	29.	4.29
	HYDROGRAPH AT							
+		DRE9	104.	13.00	3.	1.	0.	3.05
	ROUTED TO							
+		RTE6E9	26.	13.42	3.	1.	0.	3.05
	HYDROGRAPH AT							
+		E9	968.	12.42	147.	48.	16.	.72
	DIVERSION TO							
+		RETE9	968.	12.42	118.	33.	11.	.72
	HYDROGRAPH AT							
+		DIVE9	372.	12.75	49.	15.	5.	.72
	2 COMBINED AT							
+		CPE9	372.	12.75	52.	16.	5.	1.07
	DIVERSION TO							
+		DRR5	195.	12.75	9.	2.	1.	1.07
	HYDROGRAPH AT							
+		DE9S	176.	12.75	43.	14.	5.	1.07
	ROUTED TO							
+		E9E16	121.	13.25	41.	14.	5.	1.07
	HYDROGRAPH AT							
+		DRR5	195.	12.75	9.	2.	1.	1.07
	HYDROGRAPH AT							
+		R5	546.	12.50	72.	21.	7.	.50
	DIVERSION TO							
+		RETR5	4.	4.67	2.	1.	0.	.50
	HYDROGRAPH AT							
+		DIVR5	546.	12.50	72.	21.	7.	.50
	2 COMBINED AT							
+		CPR5	545.	12.50	81.	23.	8.	1.07
	ROUTED TO							
+		R5R8	472.	12.92	81.	23.	8.	1.07
	HYDROGRAPH AT							
+		R8	741.	12.42	115.	39.	13.	.55
	DIVERSION TO							
+		RETR8	741.	12.42	91.	25.	8.	.55
	HYDROGRAPH AT							
+		DIVR8	366.	12.67	42.	13.	4.	.55
	2 COMBINED AT							
+		CPR8	732.	12.67	119.	36.	12.	1.62
	ROUTED TO							
+		R8E16	649.	13.00	119.	36.	12.	1.62
	HYDROGRAPH AT							
+		E16	582.	12.33	79.	26.	9.	.40
	DIVERSION TO							
+		RETE16	582.	12.33	64.	18.	6.	.40
	HYDROGRAPH AT							
+		DIVE16	213.	12.58	26.	8.	3.	.40
	3 COMBINED AT							
+		CPE16	721.	13.00	180.	56.	19.	2.52
	ROUTED TO							
+		E16E15	679.	13.33	177.	56.	19.	2.52
	2 COMBINED AT							
+		CPE15	1161.	13.50	405.	136.	45.	6.81
	ROUTED TO							
+		DETPB	179.	17.75	178.	123.	45.	6.81
	ROUTED TO							
+		E1524B	179.	17.83	178.	123.	45.	6.81
	HYDROGRAPH AT							
+		E25	1038.	12.50	184.	60.	20.	.93
	DIVERSION TO							
+		RETE25	1038.	12.50	164.	45.	15.	.93
	HYDROGRAPH AT							

+		DIVE25	240.	13.17	46.	15.	5.	.93
	HYDROGRAPH AT							
+		E24B	788.	12.25	100.	32.	11.	.46
	DIVERSION TO							
+		RET24B	788.	12.25	81.	22.	7.	.46
	HYDROGRAPH AT							
+		DIV24B	274.	12.58	32.	10.	3.	.46
	3 COMBINED AT							
+		CPE24B	243.	14.42	219.	140.	51.	8.20
	ROUTED TO							
+		DET222	192.	24.17	190.	137.	51.	8.20
	ROUTED TO							
+		E24E28	192.	24.25	190.	137.	51.	8.20
	HYDROGRAPH AT							
+		E28B	773.	12.42	116.	37.	12.	.54
	DIVERSION TO							
+		RET28B	773.	12.42	95.	26.	9.	.54
	HYDROGRAPH AT							
+		DIV28B	316.	12.75	35.	11.	4.	.54
	HYDROGRAPH AT							
+		E29	1237.	12.50	203.	66.	22.	1.00
	DIVERSION TO							
+		RETE29	1237.	12.50	164.	45.	15.	1.00
	HYDROGRAPH AT							
+		DIVE29	573.	12.83	66.	21.	7.	1.00
	3 COMBINED AT							
+		CPE28B	488.	12.92	210.	159.	58.	9.74
	ROUTED TO							
+		E28E31	495.	13.08	210.	159.	58.	9.74
	HYDROGRAPH AT							
+		E31	964.	12.42	157.	52.	17.	.81
	DIVERSION TO							
+		RETE31	964.	12.42	125.	35.	12.	.81
	HYDROGRAPH AT							
+		DIVE31	402.	12.83	54.	17.	6.	.81
	2 COMBINED AT							
+		CPE31A	642.	13.08	238.	171.	62.	10.55
	HYDROGRAPH AT							
+		E32	404.	12.25	48.	16.	5.	.25
	DIVERSION TO							
+		RETE32	404.	12.25	38.	11.	4.	.25
	HYDROGRAPH AT							
+		DIVE32	136.	12.50	17.	5.	2.	.25
	ROUTED TO							
+		E32E31	68.	12.92	16.	5.	2.	.25
	2 COMBINED AT							
+		CPE31	669.	13.08	250.	174.	63.	10.80
	ROUTED TO							
+		E31E30	418.	13.67	241.	173.	63.	10.80
	HYDROGRAPH AT							
+		E30B	844.	12.83	186.	58.	19.	.88
	DIVERSION TO							
+		RET30B	844.	12.83	151.	41.	14.	.88
	HYDROGRAPH AT							
+		DIV30B	401.	13.33	55.	17.	6.	.88
	2 COMBINED AT							
+		CPE30	593.	13.67	278.	184.	67.	11.68
	ROUTED TO							
+		E30E26	560.	13.75	276.	184.	67.	11.68
	HYDROGRAPH AT							
+		E26B	415.	12.33	56.	18.	6.	.26
	DIVERSION TO							

+		RET26B	415.	12.33	45.	12.	4.	.26
+	HYDROGRAPH AT	DIV26B	146.	12.67	17.	5.	2.	.26
+	2 COMBINED AT	CPE26	570.	13.75	282.	186.	68.	11.94
+	ROUTED TO	E26E33	437.	14.42	273.	185.	68.	11.94
+	HYDROGRAPH AT	E33B	1304.	12.33	183.	59.	20.	.85
+	DIVERSION TO	RET33B	1304.	12.33	149.	41.	14.	.85
+	HYDROGRAPH AT	DIV33B	526.	12.67	57.	18.	6.	.85
+	2 COMBINED AT	CPE33B	461.	14.42	293.	195.	72.	12.79

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME (IN)	
						DT (MIN)	PEAK (CFS)		
FOR STORM = 1	STORM AREA (SQ MI) =			.00					
E1524B	MANE	5.00	199.12	1045.00	.85	5.00	199.12	1045.00	.85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3078E+03 EXCESS= .0000E+00 OUTFLOW= .3078E+03 BASIN STORAGE= .7116E-02 PERCENT ERROR= .0

FOR STORM = 2	STORM AREA (SQ MI) =		1.00						
E1524B	MANE	5.00	195.58	1050.00	.83	5.00	195.58	1050.00	.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3025E+03 EXCESS= .0000E+00 OUTFLOW= .3025E+03 BASIN STORAGE= .7037E-02 PERCENT ERROR= .0

FOR STORM = 3	STORM AREA (SQ MI) =		5.00						
E1524B	MANE	5.00	181.59	1070.00	.78	5.00	181.59	1070.00	.78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2818E+03 EXCESS= .0000E+00 OUTFLOW= .2818E+03 BASIN STORAGE= .6933E-02 PERCENT ERROR= .0

FOR STORM = 4	STORM AREA (SQ MI) =		10.00						
E1524B	MANE	5.00	176.34	1070.00	.70	5.00	176.34	1070.00	.70

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2555E+03 EXCESS= .0000E+00 OUTFLOW= .2555E+03 BASIN STORAGE= .6368E-03 PERCENT ERROR= .0

FOR STORM = 5	STORM AREA (SQ MI) =		20.00						
E1524B	MANE	5.00	174.08	1065.00	.62	5.00	174.08	1065.00	.62

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2247E+03 EXCESS= .0000E+00 OUTFLOW= .2247E+03 BASIN STORAGE= .6066E-03 PERCENT ERROR= .0

FOR STORM = 6	STORM AREA (SQ MI) =		30.00						
E1524B	MANE	5.00	168.82	1070.00	.57	5.00	168.82	1070.00	.57

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2071E+03 EXCESS= .0000E+00 OUTFLOW= .2071E+03 BASIN STORAGE= .6004E-03 PERCENT ERROR= .0

FOR STORM = 7	STORM AREA (SQ MI) =		40.00						
E1524B	MANE	5.00	156.05	1100.00	.54	5.00	156.05	1100.00	.54

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1947E+03 EXCESS= .0000E+00 OUTFLOW= .1947E+03 BASIN STORAGE= .5998E-03 PERCENT ERROR= .0

FOR STORM = 8	STORM AREA (SQ MI) =		50.00						
E1524B	MANE	5.00	146.46	1115.00	.51	5.00	146.46	1115.00	.51

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1850E+03 EXCESS= .0000E+00 OUTFLOW= .1850E+03 BASIN STORAGE= .6009E-03 PERCENT ERROR= .0

FOR STORM = 9	STORM AREA (SQ MI) =		60.00						
E1524B	MANE	5.00	140.00	1130.00	.49	5.00	140.00	1130.00	.49

CONTINUITY SUMMARY (AC-FT) - INFLOW= .1783E+03 EXCESS= .0000E+00 OUTFLOW= .1783E+03 BASIN STORAGE= .6007E-03 PERCENT ERROR= .0

FOR STORM = 1	STORM AREA (SQ MI) =	.00								
E24E28	MANE	5.00	206.13	1290.00	.82	5.00	206.13	1290.00	.82	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3582E+03 EXCESS= .0000E+00 OUTFLOW= .3582E+03 BASIN STORAGE= .9821E-02 PERCENT ERROR= .0										
FOR STORM = 2	STORM AREA (SQ MI) =	1.00								
E24E28	MANE	5.00	203.36	1290.00	.80	5.00	203.36	1290.00	.80	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3518E+03 EXCESS= .0000E+00 OUTFLOW= .3518E+03 BASIN STORAGE= .9685E-02 PERCENT ERROR= .0										
FOR STORM = 3	STORM AREA (SQ MI) =	5.00								
E24E28	MANE	5.00	194.80	1455.00	.75	5.00	194.80	1455.00	.75	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3270E+03 EXCESS= .0000E+00 OUTFLOW= .3270E+03 BASIN STORAGE= .9503E-02 PERCENT ERROR= .0										
FOR STORM = 4	STORM AREA (SQ MI) =	10.00								
E24E28	MANE	5.00	191.20	1460.00	.68	5.00	191.20	1460.00	.68	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2956E+03 EXCESS= .0000E+00 OUTFLOW= .2956E+03 BASIN STORAGE= .1059E-02 PERCENT ERROR= .0										
FOR STORM = 5	STORM AREA (SQ MI) =	20.00								
E24E28	MANE	5.00	180.58	1315.00	.59	5.00	180.58	1315.00	.59	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2584E+03 EXCESS= .0000E+00 OUTFLOW= .2584E+03 BASIN STORAGE= .1009E-02 PERCENT ERROR= .0										
FOR STORM = 6	STORM AREA (SQ MI) =	30.00								
E24E28	MANE	5.00	167.59	1290.00	.54	5.00	167.59	1290.00	.54	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2371E+03 EXCESS= .0000E+00 OUTFLOW= .2371E+03 BASIN STORAGE= .9942E-03 PERCENT ERROR= .0										
FOR STORM = 7	STORM AREA (SQ MI) =	40.00								
E24E28	MANE	5.00	154.82	1330.00	.51	5.00	154.82	1330.00	.51	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2221E+03 EXCESS= .0000E+00 OUTFLOW= .2221E+03 BASIN STORAGE= .9873E-03 PERCENT ERROR= .0										
FOR STORM = 8	STORM AREA (SQ MI) =	50.00								
E24E28	MANE	5.00	143.84	1375.00	.48	5.00	143.84	1375.00	.48	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2104E+03 EXCESS= .0000E+00 OUTFLOW= .2104E+03 BASIN STORAGE= .9817E-03 PERCENT ERROR= .0										
FOR STORM = 9	STORM AREA (SQ MI) =	60.00								
E24E28	MANE	5.00	140.97	1100.00	.46	5.00	140.97	1100.00	.46	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2023E+03 EXCESS= .0000E+00 OUTFLOW= .2022E+03 BASIN STORAGE= .9777E-03 PERCENT ERROR= .0										
FOR STORM = 1	STORM AREA (SQ MI) =	.00								
E28E31	MANE	5.00	728.97	775.00	.81	5.00	728.97	775.00	.81	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4219E+03 EXCESS= .0000E+00 OUTFLOW= .4217E+03 BASIN STORAGE= .9981E-02 PERCENT ERROR= .0										
FOR STORM = 2	STORM AREA (SQ MI) =	1.00								
E28E31	MANE	5.00	698.45	780.00	.80	5.00	698.45	780.00	.80	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4144E+03 EXCESS= .0000E+00 OUTFLOW= .4142E+03 BASIN STORAGE= .9840E-02 PERCENT ERROR= .0										
FOR STORM = 3	STORM AREA (SQ MI) =	5.00								
E28E31	MANE	5.00	609.14	780.00	.74	5.00	609.14	780.00	.74	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3850E+03 EXCESS= .0000E+00 OUTFLOW= .3849E+03 BASIN STORAGE= .9653E-02 PERCENT ERROR= .0										
FOR STORM = 4	STORM AREA (SQ MI) =	10.00								
E28E31	MANE	5.00	494.24	785.00	.67	5.00	494.24	785.00	.67	
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3478E+03 EXCESS= .0000E+00 OUTFLOW= .3477E+03 BASIN STORAGE= .1089E-02 PERCENT ERROR= .0										

	STORAGE	0.		607.		607.	
	OUTFLOW	0.		104.		104.	
RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.72	.00	16.	0.	.00	.00	.00

PLAN 6

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	1566.00	1574.00	1574.00
STORAGE	0.	607.	607.
OUTFLOW	0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.61	.00	14.	0.	.00	.00	.00

PLAN 7

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	1566.00	1574.00	1574.00
STORAGE	0.	607.	607.
OUTFLOW	0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.53	.00	12.	0.	.00	.00	.00

PLAN 8

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	1566.00	1574.00	1574.00
STORAGE	0.	607.	607.
OUTFLOW	0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.47	.00	11.	0.	.00	.00	.00

PLAN 9

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	1566.00	1574.00	1574.00
STORAGE	0.	607.	607.
OUTFLOW	0.	104.	104.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1566.43	.00	10.	0.	.00	.00	.00

*** NORMAL END OF HEC-1 ***

*Appendix C. Alternatives Hydraulic
Calculations*

- Normal depth calculations
- Storm drain calculations
- Stage-storage-discharge table

Worksheet for Meridian Channel - North Segment

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.035	
Channel Slope	0.00174	ft/ft
Left Side Slope	4.00	ft/ft (H:V)
Right Side Slope	4.00	ft/ft (H:V)
Bottom Width	30.00	ft
Discharge	371.00	ft ³ /s

Results

Normal Depth	2.92	ft
Flow Area	121.90	ft ²
Wetted Perimeter	54.11	ft
Hydraulic Radius	2.25	ft
Top Width	53.39	ft
Critical Depth	1.56	ft
Critical Slope	0.01642	ft/ft
Velocity	3.04	ft/s
Velocity Head	0.14	ft
Specific Energy	3.07	ft
Froude Number	0.36	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.92	ft
Critical Depth	1.56	ft
Channel Slope	0.00174	ft/ft

Worksheet for Meridian Channel - North Segment

GVF Output Data

Critical Slope 0.01642 ft/ft

Messages

Notes

This slope is set assuming the channel drops 5' from existing ground. A 5' drop was chosen so there would be cover over a crossing to take these flows to the basin south of Pecos Road.

There is approximately 120' available for offsite flows west of Matheson Tri-Gas (MTG). This 62' top width (including 1' of freeboard) allows room for a 14' access road and an additional 44', which can be used as a landscape buffer if desired.

Cross Section for Meridian Channel - North Segment

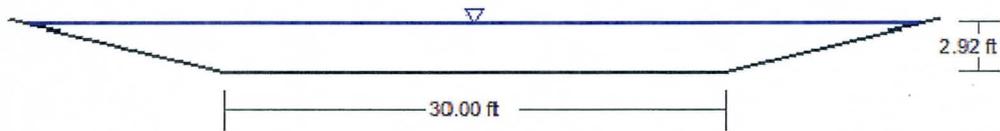
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.035
Channel Slope	0.00174 ft/ft
Normal Depth	2.92 ft
Left Side Slope	4.00 ft/ft (H:V)
Right Side Slope	4.00 ft/ft (H:V)
Bottom Width	30.00 ft
Discharge	371.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Meridian Channel - South Segment

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.00154	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	42.00	ft
Discharge	732.00	ft ³ /s

Results

Normal Depth	2.42	ft
Flow Area	113.23	ft ²
Wetted Perimeter	52.81	ft
Hydraulic Radius	2.14	ft
Top Width	51.67	ft
Critical Depth	2.04	ft
Critical Slope	0.00273	ft/ft
Velocity	6.46	ft/s
Velocity Head	0.65	ft
Specific Energy	3.07	ft
Froude Number	0.77	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.42	ft
Critical Depth	2.04	ft
Channel Slope	0.00154	ft/ft

Worksheet for Meridian Channel - South Segment

GVF Output Data

Critical Slope 0.00273 ft/ft

Messages

Notes

With 1' of freeboard, the top width of the channel will be 56'. An additional 44', which includes a 30' landscape buffer and 14' access road, will bring the total ROW required to 100'.

Cross Section for Meridian Channel - South Segment

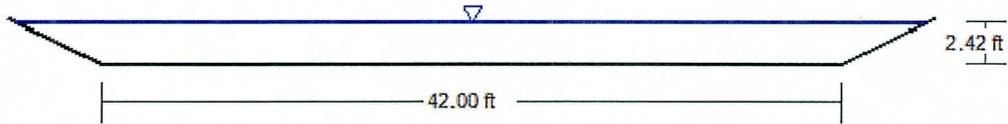
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.00154 ft/ft
Normal Depth	2.42 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	42.00 ft
Discharge	732.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Pecos Channel - Pecos Basin to Mountain Rd

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.00210	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	6.00	ft
Discharge	180.00	ft ³ /s

Results

Normal Depth	2.57	ft
Flow Area	28.58	ft ²
Wetted Perimeter	17.48	ft
Hydraulic Radius	1.63	ft
Top Width	16.27	ft
Critical Depth	2.33	ft
Critical Slope	0.00306	ft/ft
Velocity	6.30	ft/s
Velocity Head	0.62	ft
Specific Energy	3.18	ft
Froude Number	0.84	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.57	ft
Critical Depth	2.33	ft
Channel Slope	0.00210	ft/ft

Worksheet for Pecos Channel - Pecos Basin to Mountain Rd

GVF Output Data

Critical Slope 0.00306 ft/ft

Messages

Notes

With 1' of freeboard, the top width of the channel will be 21'. An additional 44', which includes a 30' landscape buffer and 14' access road, will bring the total ROW required to 65'.

Cross Section for Pecos Channel - Pecos Basin to Mountain Rd

Project Description

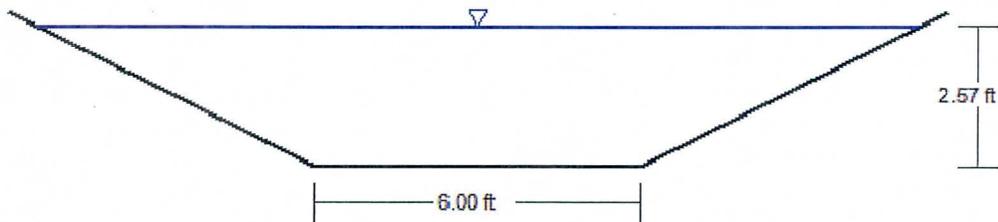
Friction Method Manning Formula

Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.00210 ft/ft
Normal Depth	2.57 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	6.00 ft
Discharge	180.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Pecos Channel - Mountain Rd to Signal Butte Rd

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.00206	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	6.00	ft
Discharge	239.00	ft ³ /s

Results

Normal Depth	2.97	ft
Flow Area	35.43	ft ²
Wetted Perimeter	19.27	ft
Hydraulic Radius	1.84	ft
Top Width	17.87	ft
Critical Depth	2.72	ft
Critical Slope	0.00295	ft/ft
Velocity	6.75	ft/s
Velocity Head	0.71	ft
Specific Energy	3.68	ft
Froude Number	0.84	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.97	ft
Critical Depth	2.72	ft
Channel Slope	0.00206	ft/ft

Worksheet for Pecos Channel - Mountain Rd to Signal Butte Rd

GVF Output Data

Critical Slope 0.00295 ft/ft

Messages

Notes

With 1' of freeboard, the top width of the channel will be 22'. An additional 44', which includes a 30' landscape buffer and 14' access road, will bring the total ROW required to 66'.

Cross Section for Pecos Channel - Mountain Rd to Signal Butte Rd

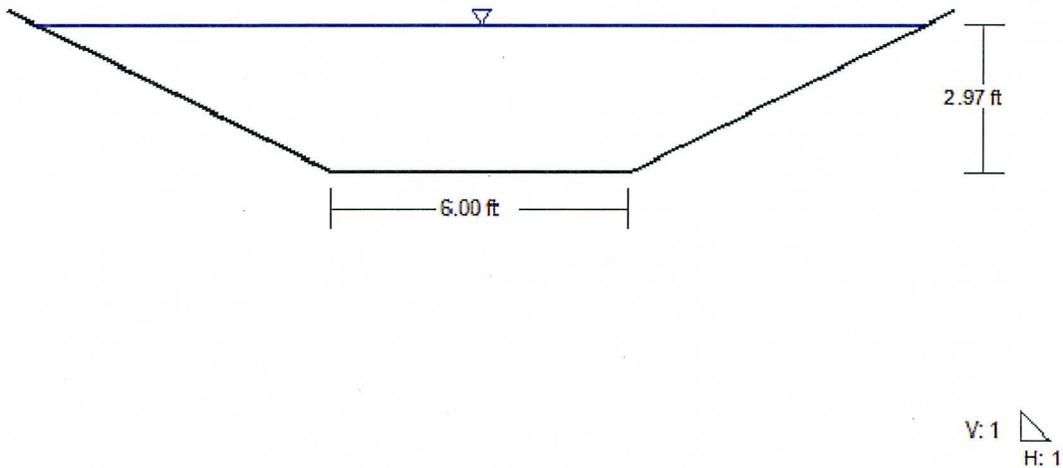
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.00206 ft/ft
Normal Depth	2.97 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	6.00 ft
Discharge	239.00 ft ³ /s

Cross Section Image



Worksheet for Pecos Channel - Signal Butte Rd to 222nd St

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.00152	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	12.00	ft
Discharge	538.00	ft ³ /s

Results

Normal Depth	3.79	ft
Flow Area	74.33	ft ²
Wetted Perimeter	28.97	ft
Hydraulic Radius	2.57	ft
Top Width	27.18	ft
Critical Depth	3.28	ft
Critical Slope	0.00264	ft/ft
Velocity	7.24	ft/s
Velocity Head	0.81	ft
Specific Energy	4.61	ft
Froude Number	0.77	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.79	ft
Critical Depth	3.28	ft
Channel Slope	0.00152	ft/ft

Worksheet for Pecos Channel - Signal Butte Rd to 222nd St

GVF Output Data

Critical Slope 0.00264 ft/ft

Messages

Notes

With 1' of freeboard, the top width of the channel will be 32'. An additional 44', which includes a 30' landscape buffer and 14' access road, will bring the total ROW required to 76'.

Cross Section for Pecos Channel - Signal Butte Rd to 222nd St

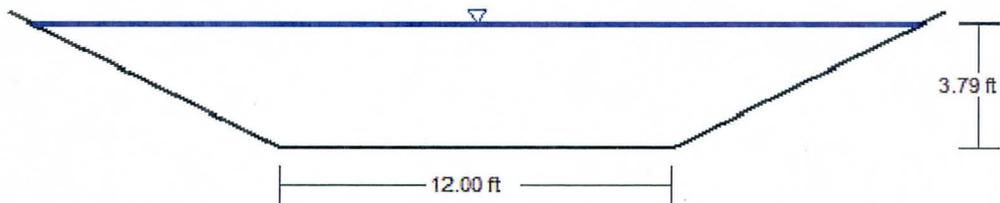
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.00152 ft/ft
Normal Depth	3.79 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	12.00 ft
Discharge	538.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Pecos Channel - 222nd St to Crismon Rd

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.050	
Channel Slope	0.00303	ft/ft
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Bottom Width	40.00	ft
Discharge	539.00	ft ³ /s

Results

Normal Depth	3.36	ft
Flow Area	168.07	ft ²
Wetted Perimeter	61.23	ft
Hydraulic Radius	2.74	ft
Top Width	60.14	ft
Critical Depth	1.70	ft
Critical Slope	0.03208	ft/ft
Velocity	3.21	ft/s
Velocity Head	0.16	ft
Specific Energy	3.52	ft
Froude Number	0.34	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.36	ft
Critical Depth	1.70	ft
Channel Slope	0.00303	ft/ft

Worksheet for Pecos Channel - 222nd St to Crismon Rd

GVF Output Data

Critical Slope 0.03208 ft/ft

Messages

Notes

With 1' of freeboard, the top width of the channel will be 66'. An additional 44', which includes a 30' landscape buffer and 14' access road, will bring the total ROW required to 110'.

Cross Section for Pecos Channel - 222nd St to Crismon Rd

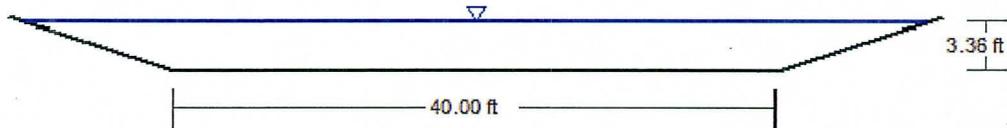
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.00303 ft/ft
Normal Depth	3.36 ft
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	40.00 ft
Discharge	539.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Pecos Channel - Crismon Rd to Ellsworth Rd

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.050	
Channel Slope	0.00341	ft/ft
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Bottom Width	40.00	ft
Discharge	539.00	ft ³ /s

Results

Normal Depth	3.25	ft
Flow Area	161.48	ft ²
Wetted Perimeter	60.53	ft
Hydraulic Radius	2.67	ft
Top Width	59.48	ft
Critical Depth	1.70	ft
Critical Slope	0.03208	ft/ft
Velocity	3.34	ft/s
Velocity Head	0.17	ft
Specific Energy	3.42	ft
Froude Number	0.36	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.25	ft
Critical Depth	1.70	ft
Channel Slope	0.00341	ft/ft

Worksheet for Pecos Channel - Crismon Rd to Ellsworth Rd

GVF Output Data

Critical Slope 0.03208 ft/ft

Messages

Notes

With 1' of freeboard, the top width of the channel will be 66'. An additional 44', which includes a 30' landscape buffer and 14' access road, will bring the total ROW required to 110'.

Cross Section for Pecos Channel - Crismon Rd to Ellsworth Rd

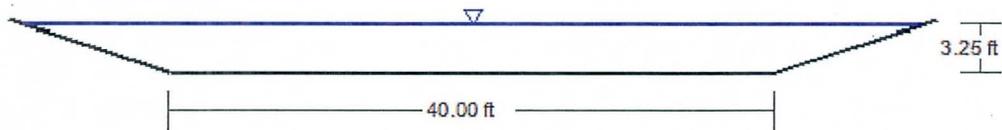
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.050
Channel Slope	0.00341 ft/ft
Normal Depth	3.25 ft
Left Side Slope	3.00 ft/ft (H:V)
Right Side Slope	3.00 ft/ft (H:V)
Bottom Width	40.00 ft
Discharge	539.00 ft ³ /s

Cross Section Image

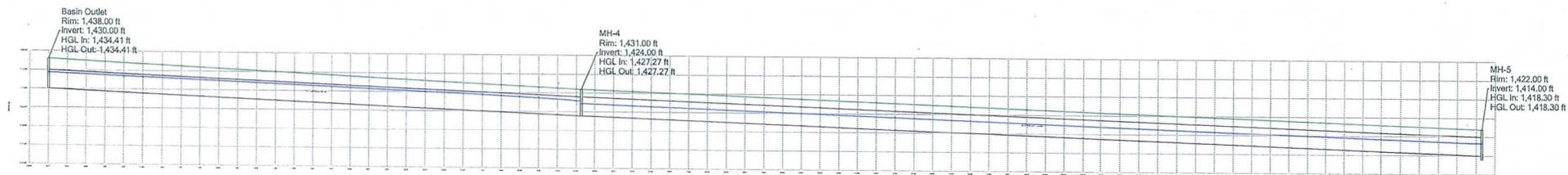


V: 1
H: 1

FlexTable: Conduit Table

Label	Start Node	Stop Node	Length (Unified) (ft)	Manning's n	Slope (ft/ft)	Diameter (in)	Total Flow (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Invert (U/S) (ft)	Invert (D/S) (ft)
CO-1	Basin Outlet	MH-4	1,414.3	0.013	0.004	60.0	179.00	9.77	1,438.00	1,431.00	1,434.41	1,427.83	1,430.00	1,424.00
CO-2	MH-4	MH-5	2,401.4	0.013	0.004	60.0	243.00	8.94	1,431.00	1,422.00	1,427.27	1,418.30	1,424.00	1,415.00
CO-3	MH-5	222nd St Outfall	1,342.0	0.013	0.004	72.0	488.00	11.27	1,422.00	1,416.00	1,418.30	1,412.28	1,414.00	1,408.00
CO-5	Mountain Rd Inlet	MH-4	36.9	0.013	0.014	60.0	64.00	12.24	1,431.00	1,431.00	1,427.02	1,427.27	1,424.50	1,424.00
CO-6	Signal Butte Rd Inlet	MH-5	29.2	0.013	0.017	60.0	245.00	15.94	1,422.00	1,422.00	1,418.66	1,418.30	1,415.50	1,415.00

Profile Report
Engineering Profile - Profile - 1 (Pecos Road Network_Alt2.stsw)



FlexTable: Conduit Table

Label	Start Node	Stop Node	Length (Unified) (ft)	Manning's n	Slope (ft/ft)	Diameter (in)	Total Flow (cfs)	Velocity (ft/s)	Elevation Ground (Start) (ft)	Elevation Ground (Stop) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Invert (U/S) (ft)	Invert (D/S) (ft)
CO-1	Basin Outlet	MH-4	1,414.3	0.013	0.004	60.0	179.00	9.77	1,438.00	1,431.00	1,434.41	1,427.83	1,430.00	1,424.00
CO-2	MH-4	MH-5	2,401.4	0.013	0.004	60.0	243.00	8.94	1,431.00	1,422.00	1,427.27	1,418.30	1,424.00	1,415.00
CO-3	MH-5	MH-6	1,342.0	0.013	0.004	72.0	488.00	11.27	1,422.00	1,416.00	1,418.30	1,413.09	1,414.00	1,408.00
CO-4	MH-6	Ellsworth Outfall	8,934.7	0.013	0.003	72.0	488.00	9.54	1,416.00	1,388.00	1,413.09	1,384.28	1,408.00	1,380.00
CO-5	Mountain Rd Inlet	MH-4	36.9	0.013	0.014	60.0	64.00	12.24	1,431.00	1,431.00	1,427.02	1,427.27	1,424.50	1,424.00
CO-6	Signal Butte Rd Inlet	MH-5	29.2	0.013	0.017	60.0	245.00	15.94	1,422.00	1,422.00	1,418.66	1,418.30	1,415.50	1,415.00

Profile Report
Engineering Profile - Profile - 1 (Pecos Road Network.stsw)

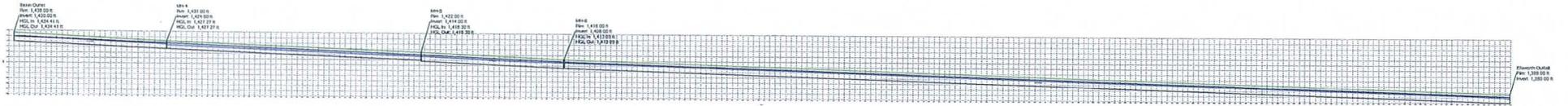
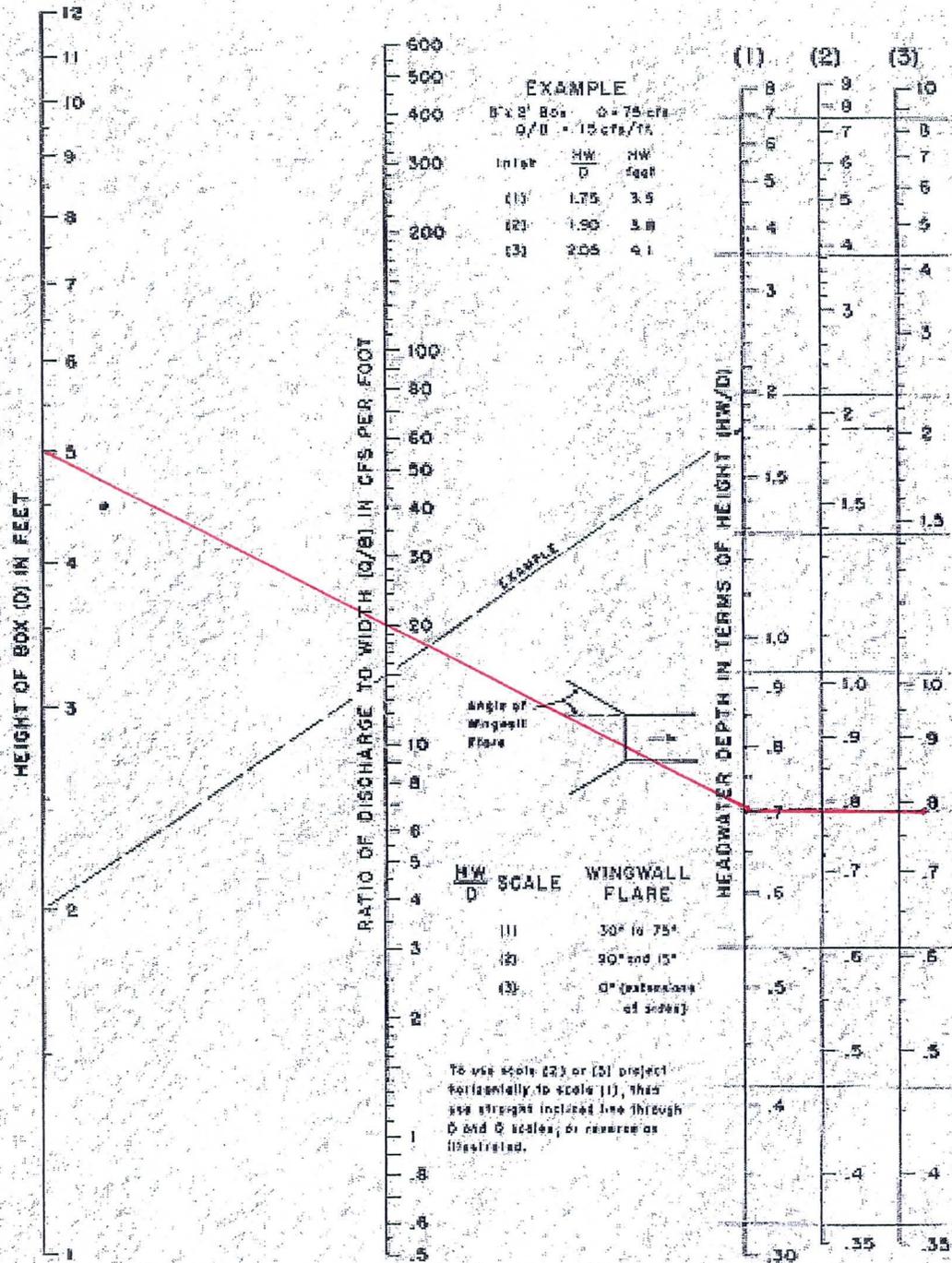


CHART I



HEADWATER DEPTH FOR BOX CULVERTS WITH INLET CONTROL

Project **Pecos Road DCR**

Subject **Proposed Detention Basin Calculations**

Designed by **MAW**

Date **7/30/2014**

Checked by

Date

Project No. 091131024

District Project No: 2014C001

Objective: to estimate the stage-storage-discharge relationship

Detention Basin - SWC Pecos/Meridian

Drains in 51.47 hours

Outlet Diameter 5.00 ft
Outlet Elevation 0 ft

Outlet X-Sect Area 19.635 ft²
No. of Outlet Barrels 1
Outlet Pipe Slope 0.0046 ft/ft

Elevation [ft]	Surface Storage Area [ft ²]	Surface Storage Area [acre]	Average Area [acre]	Δ Elev [ft]	Δ Vol [ac-ft]	Σ Vol [ac-ft]	Δ Time to Drain [hr]	Q _{pipe} [cfs]	Q _{weir} [cfs]	Total Q _{out} [cfs]
0	950,683	21.82				0		0.00	0	0.00
1	956,443	21.96	21.89	1.0	21.89	21.89	34.25	15.47	0	15.47
2	962,219	22.09	22.02	1.0	22.02	43.91	7.11	59.53	0	59.53
3	968,011	22.22	22.16	1.0	22.16	66.07	3.01	118.67	0	118.67
4	973,819	22.36	22.29	1.0	22.29	88.36	1.85	172.66	0	172.66
5	979,643	22.49	22.42	1.0	22.42	110.78	1.55	176.64	0	176.64
6	985,483	22.62	22.56	1.0	22.56	133.34	1.55	176.64	0	176.64
Freeboard										
6.5	988,408	22.69	22.66	0.5	11.33	144.67	0.75	189.08	0.00	189.1
7	991,338	22.76	22.69	1.0	22.69	156.03	1.41	200.55	0.00	200.6

Notes:

Q_{pipe} goes from Mannings Eqn to Orifice Eqn when water surface exceeds 1.2*(Outlet Diameter) per Linsley et al. Water Resources Engineering 4th Edition, pg 652.

Project *Pecos Road DCR*

Subject **Proposed Detention Basin Calculations**

Designed by **MAW**

Date 7/30/2014

Checked by

Date

Project No. 091131024

District Project No: 2014C001

Objective: to estimate the stage-storage-discharge relationship

Detention Basin - NWC Pecos/222nd Street

Drains in 12.66 hours

Outlet Diameter 3.50 ft
Outlet Elevation 0 ft

Outlet X-Sect Area 9.621 ft²
No. of Outlet Barrels 2
Outlet Pipe Slope 0.0046 ft/ft

Elevation [ft]	Surface Storage Area [ft ²]	Surface Storage Area [acre]	Average Area [acre]	Δ Elev [ft]	Δ Vol [ac-ft]	Σ Vol [ac-ft]	Δ Time to Drain [hr]	Q _{pipe} [cfs]	Q _{weir} [cfs]	Total Q _{out} [cfs]
0	327,184	7.51				0		0.00	0	0.00
1	331,776	7.62	7.56	1.0	7.56	7.56	7.53	24.31	0	24.31
2	336,400	7.72	7.67	1.0	7.67	15.23	1.70	84.98	0	84.98
3	341,056	7.83	7.78	1.0	7.78	23.01	0.83	141.48	0	141.48
4	345,744	7.94	7.88	1.0	7.88	30.89	0.69	136.47	0	136.47
5	350,464	8.05	7.99	1.0	7.99	38.88	0.64	167.03	0	167.03
6	355,216	8.15	8.10	1.0	8.10	46.98	0.55	191.00	0	191.00
Freeboard										
6.5	357,604	8.21	8.18	0.5	4.09	51.08	0.25	201.93	0.00	201.9
7	360,000	8.26	8.21	1.0	8.21	55.19	0.48	212.29	0.00	212.3

Notes:

Q_{pipe} goes from Mannings Eqn to Orifice Eqn when water surface exceeds 1.2*(Outlet Diameter) per Linsley et al. Water Resources Engineering 4th Edition, pg 652.

Appendix D. Sediment Yield Analysis

Drainage Memo – Sediment Yield Analysis
for Pecos Road Detention Basin, prepared
by the Flood Control District of Maricopa
County

Drainage Memo

Sediment Yield Analysis For Pecos Road Detention Basin

Prepared by



Raj Shrestha, PE, CFM
Engineering Application Development & River Mechanics Branch
Engineering Division
Flood Control District of Maricopa County

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Phoenix, Arizona 85009-6399
Phone: 602-506-1501
Fax: 602 506 4601

July 2014



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Appendices

- Appendix A: Design Discharge and HEC-1 Output
- Appendix B: Soil and Land Use
- Appendix C: DDMSW Output





1 Background and Scope

Pecos Road Detention Basin (Pecos Basin) is located at the southwest corner of Pecos Road and Meridian Road intersection (Figure 1). It is one of the alternative measures to reduce the flooding along Pecos Road. The Pecos Basin and its watershed fall within the study area of East Mesa Area Drainage Master Plan Update (EMADMPU) completed by Flood Control District of Maricopa County (FCDMC, 2011). The purpose of this study is to perform a planning-level analysis to determine the sediment accumulation on the facility. It is anticipated that a more detailed sediment yield analysis will be performed in future during the design phase of the project. See figure below for the location of the Pecos Basin.

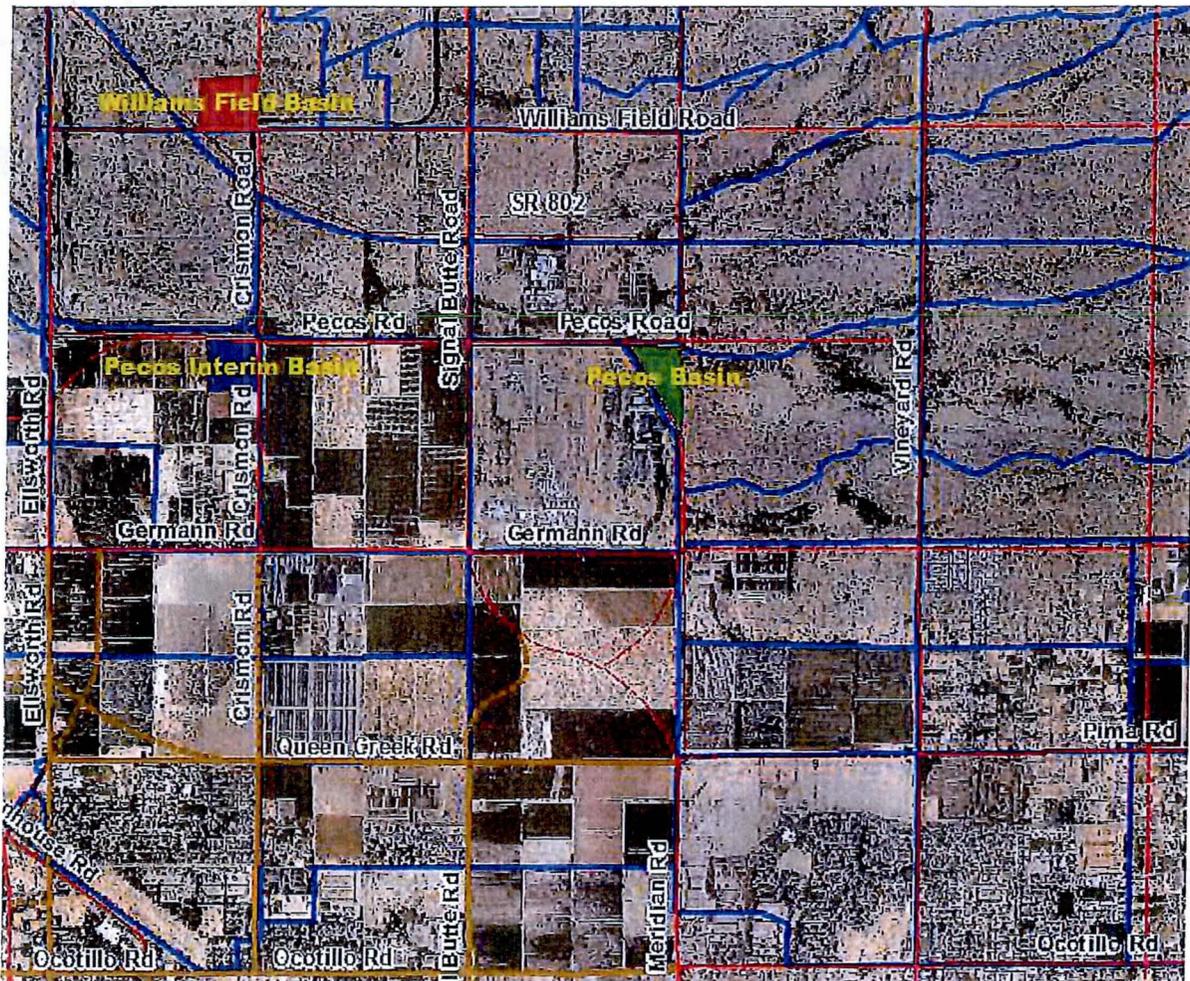


Figure 1: Pecos Basin Location Map



2 Methodology

The sediment yield analysis performed in this memo follows the procedure outlined in River Mechanics Manual for DDMSW, January 2013. DDMSW (Version 4.6.4) software developed by Flood Control District is used to create the sediment yield model. The sediment yield consists of two parts and is defined as the sum of the wash load and the total bed material load delivered to a point of interest. The wash load is calculated with the Modified Universal Soil Loss Equation (MUSLE) method, and the total bed material load is calculated with the Zeller-Fullerton equation (Zeller and Fullerton, 1983), which is based on the assumption that the reach is at an equilibrium condition.

The sediment yield calculation is performed for future condition as requested by Flood Control District Project Manager Mike Duncan. The email conversation regarding the peak discharge and the HEC-1 model for the future condition is attached in "Appendix A: Design Discharge and HEC-1 Output". Peak discharge of 697cfs corresponding to concentration point CPE24B is used as a design peak discharge for the sediment yield model.

3 Parameter Estimation

The majority of the parameters required to calculate the sediment yield were derived from the previous studies completed for the EMADMPU (FCDMC, 2011). However, since the watershed for the basin is located in the Pinal County, DDMSW software does not include some of the soil parameters that fall outside of the Maricopa County Soil Survey Study area. The soil parameters that fall outside of the Maricopa County Study area is obtained from the USDA-NRCS soil data.

3.1 Wash Load

The MUSLE relationship given by SLA (1985) is used to compute the watershed soil loss in tons. MUSLE equation has following form,

$$Y_s = \alpha(Vq_p)^\beta KLSCP$$

Where,

Y_s = watershed soil loss from the storm of a particular return period in tons,

$\alpha = 95$

V = runoff volume for the storm, ac-ft

q_p = peak flow rate for a storm event of a particular return period



$$\beta = 0.56$$

K = soil erodibility factor

LS = topographic factor

C = cover and management factor

P = erosion control practice factor (usually 1.0 for wild land areas)

The topographic factor is defined as,

$$LS = \left(\frac{\lambda}{72.6} \right)^n (0.065 + 0.0454S + 0.0065S^2)$$

Where,

λ = slope length, ft

S = percent slope

3.1.1 Runoff Volume

Runoff volume for the project is obtained from the Future Condition HEC-1 model prepared by Flood Control District on August 2011 for EMADMPU. The 100-year return period runoff volume used for the calculation is 229 ac-ft. See “Appendix A: Design Discharge and HEC-1 Output” for HEC-1 output results.

3.1.2 Peak Flow Rate

Peak flow rate for the project is obtained from the Future Condition HEC-1 model prepared by Flood Control District on August 2011 for EMADMPU. The 100-year return period peak discharge used in the calculation is 697 cfs. See “Appendix A: Design Discharge and HEC-1 Output” for HEC-1 output results.

3.1.3 Soil Erodibility Factor

The soils within the watershed boundary fall into the following three different soil survey area.

- i. Aguila – Carefree Area, Arizona, Parts of Maricopa and Pinal Counties
- ii. Eastern Maricopa and Northern Pinal Counties Area, Arizona
- iii. Eastern Pinal and Southern Gila Counties

The soil erodibility factor for the soils located in Aguila-Carefree Area, and Eastern Maricopa and Northern Pinal Counties Area are already in the DDMSW software. Whereas, the DDMSW software does



not include the soil parameter for the area located outside of the Maricopa County. The soil erodibility factor for the soils located in Eastern Pinal and Southern Gila Counties were obtained from the United States Department of Agriculture – Natural Resources Conservation Service’s Web Soil Survey (WSS). The data obtained from the WSS is entered into the DDMSW software for sediment yield calculation. The website address for the WSS is <http://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm>. The WSS is an interactive web application developed by USDA-NRCS for soil properties database.

3.1.4 Topographic Factor

The topographic factor consists of two components; slope length and percent slope. Slope length is defined as the distance from the point of origin of overland flow to the point where either the slope gradient decreases enough such that deposition begins, or the runoff water enters a well-defined channel that may be part of a drainage network or a constructed channel. Percent slope is the slope for the slope length and is approximated by the average watershed slope excluding the large slope near the mountainous areas. Both slope length and percent slope is estimated from the countywide 10 ft contour obtained from the Flood Control District’s GIS database. For this project, percent slope of 1.10% was used and entered in the DDMSW model, and the slope length was assumed to be 400 feet which is an upper limit for MUSLE method (FCDMC, 2013). The MUSLE equation is best used for slope length of less than 400feet and gradients of 3 to 8 percent.

3.1.5 Cover and Management Factor

The cover and management factor consists of three distinct types of affects as follows

- i. Effects of canopy (C_i)
- ii. Effects of mulch or close-growing vegetation in direct contact with the soil surface (C_{ii})
- iii. Tillage and residual effects of the land use (C_{iii})

The default land use factor obtained from the DDMSW software is further evaluated using the topographic and aerial image of the drainage area and found to be acceptable for this study. Following are the cover and management factor used in the model.



Table 1: Cover and management factor

Land Use Code	Description	Area, sq. mi.	Area Percent	C _i	C _{ii}	C _{iii}	Percent Impervious
140	Medium Lot Residential	1.492	24%	0.73	0.87	0.33	30
230	Community Commercial	0.45	7.2%	0.59	0.81	0.26	80
300	General Industrial	3.71	59.6%	0.67	0.84	0.3	55
610	Transportation	0.422	6.8%	0.59	0.81	0.26	80
900	Vacant	0.153	2.5%	0.86	0.93	0.39	0

3.1.6 Drainage Area

Drainage area corresponding to the concentration point CPE24B is obtained from the watershed area shape file prepared with the EMADMPU. The total contributing sediment drainage area is 6.23 sq.mi.

3.1.7 Specific Weight

Specific weight of soils located in Aguila-Carefree Area, and Eastern Maricopa and Northern Pinal Counties Area were obtained from the DDMSW software, whereas, the specific weight of soils located in Eastern Pinal and Southern Gila Counties were obtained from the United States Department of Agriculture – Natural Resources Conservation Service’s Web Soil Survey. See “Appendix B: Soil and Land Use” for the specific weight values used in this project.

3.2 Bed Load

The Zeller-Fullerton equation, which assumes that the reach is at the equilibrium condition, is used to calculate the total bed material load. It has the form

$$q_s = 0.0064 \left(\frac{n^{1.77} V_a^{4.32} G^{0.45}}{Y_h^{0.3} D_{50}^{0.61}} \right)$$

Where,

Q_s = bed-material discharge in cfs per unit width

n = manning’s roughness coefficient

V_a = average velocity, ft/s

Y_h = hydraulic depth, ft



D_{50} = median diameter, mm

G = gradation coefficient and is as follows

$$G = \frac{1}{2} \left(\frac{D_{84.1}}{D_{50}} + \frac{D_{50}}{D_{15.9}} \right)$$

3.2.1 Sediment Sample

The sediment gradation data used in this study was obtained from the sieve analysis performed for EMADMPU (FCDMC, 2011). Sediment diameters utilized to determine the sediment yield was taken from soil sample B2 which is located at Meridian Road and Pecos Road. Following are the particle size used in this project.

Table 2: Particle size table

Sediment	Size, mm
D_{10}	0.001
D_{16}	0.003
D_{50}	0.052
D_{84}	0.400

3.2.2 Cross Section Geometry and Hydraulics

Cross section geometry and hydraulics were obtained from the future condition HEC-1 model prepared by Flood Control District. The output of the HEC-1 model can be found in “Appendix A: Design Discharge and HEC-1 Output”. The cross section x and y ordinates, slope and manning’s n were taken from routing data E6E15. The cross section input parameters can be found in DDMSW output in “Appendix C: DDMSW Output”.

4 Results and Conclusion

The summary of the annual sediment yield for wash load and bed load for Pecos Basin are presented below in Table 3 on next page. The detailed output from DDMSW can be found in “Appendix C: DDMSW Output”. Queen Creek Sports Complex Basin (Entellus, 2013) sediment yield is also included in the second row for comparison. The typical design sediment volume for detention basin is total annual sediment multiplied by number of sediment removal cycle (years) plus 100-year return event sediment yield. For example, if the sediment removal cycle is 3 years, the design sediment volume is $3 \times 0.087 + 1.582 = 1.843$ ac-ft.



Table 3: Sediment Yield Summary

	Watershed Area, mi ²	Annual Sediment Yield Bed Load, ac.-ft.	Annual Sediment Yield Wash Load, ac.-ft.	Annual Sediment Yield, ac.-ft.	100-Yr Sediment Yield Bed Load, ac.-ft.	100-Yr Sediment Yield Wash Load, ac.-ft.	100-Yr Sediment Yield, ac.-ft.
Pecos Basin	6.2	0.059	0.028	0.087	1.070	0.512	1.582
Queen Creek Sports Complex Basin (Entellus)	6.7	0.110	0.088	0.198	0.949	0.957	1.906

5 References

- i. *Entellus Inc. (December, 2013), Technical Memorandum – Sediment Yield Analysis for Queen Creek Sports Complex Basin.*
- ii. *Flood Control District of Maricopa County (August, 2011), East Mesa Area Drainage Master Plan Update.*
- iii. *Flood Control District of Maricopa County (January, 2013), River Mechanics Manual for DDMSW.*
- iv. *United States Department of Agriculture – Natural Resources Conservation Service’s (USDA-NRCS), Web Soil Survey <http://websoilsurvey.sc.egov.usda.gov/App/HomePage.htm>*

Time (hr)	Design Discharge (cfs)	HEC-1 Output (cfs)	Peak Discharge (cfs)	Time to Peak (hr)	Peak Lag (hr)	Peak Ratio
0	0	0	0	0	0	1.00
1	100	100	100	1	0	1.00
2	200	200	200	2	0	1.00
3	300	300	300	3	0	1.00
4	400	400	400	4	0	1.00
5	500	500	500	5	0	1.00
6	600	600	600	6	0	1.00
7	700	700	700	7	0	1.00
8	800	800	800	8	0	1.00
9	900	900	900	9	0	1.00
10	1000	1000	1000	10	0	1.00
11	1100	1100	1100	11	0	1.00
12	1200	1200	1200	12	0	1.00
13	1300	1300	1300	13	0	1.00
14	1400	1400	1400	14	0	1.00
15	1500	1500	1500	15	0	1.00
16	1600	1600	1600	16	0	1.00
17	1700	1700	1700	17	0	1.00
18	1800	1800	1800	18	0	1.00
19	1900	1900	1900	19	0	1.00
20	2000	2000	2000	20	0	1.00
21	2100	2100	2100	21	0	1.00
22	2200	2200	2200	22	0	1.00
23	2300	2300	2300	23	0	1.00
24	2400	2400	2400	24	0	1.00
25	2500	2500	2500	25	0	1.00
26	2600	2600	2600	26	0	1.00
27	2700	2700	2700	27	0	1.00
28	2800	2800	2800	28	0	1.00
29	2900	2900	2900	29	0	1.00
30	3000	3000	3000	30	0	1.00
31	3100	3100	3100	31	0	1.00
32	3200	3200	3200	32	0	1.00
33	3300	3300	3300	33	0	1.00
34	3400	3400	3400	34	0	1.00
35	3500	3500	3500	35	0	1.00
36	3600	3600	3600	36	0	1.00
37	3700	3700	3700	37	0	1.00
38	3800	3800	3800	38	0	1.00
39	3900	3900	3900	39	0	1.00
40	4000	4000	4000	40	0	1.00
41	4100	4100	4100	41	0	1.00
42	4200	4200	4200	42	0	1.00
43	4300	4300	4300	43	0	1.00
44	4400	4400	4400	44	0	1.00
45	4500	4500	4500	45	0	1.00
46	4600	4600	4600	46	0	1.00
47	4700	4700	4700	47	0	1.00
48	4800	4800	4800	48	0	1.00
49	4900	4900	4900	49	0	1.00
50	5000	5000	5000	50	0	1.00
51	5100	5100	5100	51	0	1.00
52	5200	5200	5200	52	0	1.00
53	5300	5300	5300	53	0	1.00
54	5400	5400	5400	54	0	1.00
55	5500	5500	5500	55	0	1.00
56	5600	5600	5600	56	0	1.00
57	5700	5700	5700	57	0	1.00
58	5800	5800	5800	58	0	1.00
59	5900	5900	5900	59	0	1.00
60	6000	6000	6000	60	0	1.00

Appendix A
Design Discharge and HEC-1 Output

Raj Shrestha - FCDX

From: Michael Duncan - FCDX
Sent: Wednesday, February 26, 2014 4:04 PM
To: Raj Shrestha - FCDX
Cc: Bing Zhao - FCDX; Jennifer Pokorski - FCDX
Subject: RE: Pecos Road DCR - project number
Attachments: 24Fut100.dat; 24Fut100.out

Raj, here is the future model (input and output files) from Cathy Regester's study. I prefer this to the Entellus models, for our purposes. Please do the sediment analysis for concentration point CPE24B, which has 6.23 sq. mi. contributing and a peak of 697 cfs.

This model is on the share drive at:

W:\Hydrology-Hydraulics\cwr\East Mesa ADMPU Plan\HEC-1 with 600 in Powerline\Future Conditions

From: Raj Shrestha - FCDX
Sent: Wednesday, February 26, 2014 10:47 AM
To: Michael Duncan - FCDX
Cc: Bing Zhao - FCDX
Subject: RE: Pecos Road DCR - project number

Mike,

I have been trying to find the final future condition Hec-1 model that should be used for the Pecos Basin sediment analysis. Please see attached email from Jennifer. Per her email the East Mesa ADMP did not require the development of FINAL future condition Model for SR 24 and Ellsworth Systems. The FINAL future condition model is built only for Rittenhouse system. However there is a draft (pre-final) future condition Model that Entellus will be submitting for SR 24 and Ellsworth, and a final future condition model for Pecos system. She has also mentioned that for SR24 and Ellsworth systems, Entellus only prepared preliminary alternatives and the recommended alternative will be prepared with the Pecos Road Channel Project. Cathy also mentioned that the SR24 highway will be built about 20 years down the road and the existing peak discharge is higher than the future condition peak discharge. Do you still think that the sediment analysis should be done for the future condition? If yes, would you like me to use the draft future condition Model prepared by Entellus or would you like me to use the model that will be prepared with recommended alternative.

Thanks,
Raj

From: Michael Duncan - FCDX
Sent: Tuesday, February 11, 2014 12:12 PM
To: Raj Shrestha - FCDX
Cc: Bing Zhao - FCDX
Subject: RE: Pecos Road DCR - project number

Assume future conditions for your analysis, since the related channel and basins will have future conditions as their design criteria.

From: Raj Shrestha - FCDX
Sent: Tuesday, February 11, 2014 11:57 AM
To: Michael Duncan - FCDX
Cc: Bing Zhao - FCDX
Subject: RE: Pecos Road DCR - project number

Mike,

Are you looking for both existing and future condition sediment yield analysis or just for the future condition. Please let us know.

Thanks,

Raj

From: Michael Duncan - FCDX
Sent: Tuesday, February 11, 2014 11:30 AM
To: Raj Shrestha - FCDX
Cc: Bing Zhao - FCDX
Subject: Pecos Road DCR - project number

The PCN number is

A442.03.20 – Pecos Road Channel & Basins DCR

Which is a planning budget item, which comes from the Operations (non-CIP) Budget,
and the timesheet code for this is:

/////FCOPER/

900.00.00 - Flood Control (non-CIP) Operations

*Appendix E. Alternatives Opinions of
Probable Cost*

Preliminary Alternative OPCs



Project: *Pecos Road DCR*

Subject: **Opinion of Probable Cost for Design Alternatives**

Designed by: **DWT**

Date: 9/26/2014

KHA Project No: 091131024

Checked by: **MAW**

Date: 9/26/2014

District Project No: 2014C001-1

Alternative 1: Channel from Meridian to Ellsworth

MAG Item Number	Description	Qty	Unit	Unit Price	Cost
215.01100	Channel Excavation	186,242	CY	\$ 6	\$ 1,117,500
215.01510	Earthwork for Retention Basins	242,000	CY	\$ 6	\$ 1,452,000
220.10300	Riprap, D50=12"	51,408	CY	\$ 80	\$ 4,112,700
523.10160	Headwall, MAG Det. 501, Straight Type, 60" Pipe	6	EACH	\$ 3,500	\$ 21,000
523.10260	Headwall, MAG Det. 501, Straight Type, 2-60" Pipe	8	EACH	\$ 4,000	\$ 32,000
525.03217	Reinforced Concrete Channel, 6" Thick	5,806	CY	\$ 300	\$ 1,741,800
618.20460	60" RGRCP, Class IV	1,270	LF	\$ 175	\$ 222,300
	Concrete Drop Structure	4	EACH	\$ 3,500	\$ 14,000
Construction Subtotal					\$ 8,713,300
Potential Utility Relocation					
	Electric Line Relocation	7	EACH	\$ 3,000	\$ 21,000
	Gas Line Relocation	3	EACH	\$ 4,000	\$ 12,000
	Water Line Relocation - 4"/6"	2	EACH	\$ 5,000	\$ 10,000
	Water Line Relocation - 8"	0	EACH	\$ 10,000	\$ -
	Water Line Relocation - 12"	2	EACH	\$ 15,000	\$ 30,000
	Water Line Relocatoion - 16"	1	EACH	\$ 20,000	\$ 20,000
Potential Utility Relocation Subtotal					\$ 93,000
	Right of Way Cost	65	AC	\$ 125,000	\$ 8,125,000
	Design Cost (10% of Construction Cost)				\$ 871,330
Total					\$ 17,803,000

Notes: Construction costs were determined from ADOT Estimated Engineering Construction Cost E2C2.

Utility relocation estimates based on typical relocation costs.



Project: *Pecos Road DCR*

Subject: **Opinion of Probable Cost for Design Alternatives**

Designed by: **DWT**

Date: 9/26/2014

KHA Project No: 091131024

Checked by: **MAW**

Date: 9/26/2014

District Project No: 2014C001-1

Alternative 2: Storm Drain from Meridian 222nd and Channel from 222nd to Ellsworth

MAG Item Number	Description	Qty	Unit	Unit Price	Cost
215.01100	Channel Excavation	173,429	CY	\$ 6	\$ 1,040,600
215.01510	Earthwork for Retention Basins	242,000	CY	\$ 6	\$ 1,452,000
220.10300	Riprap, D50=12"	51,408	CY	\$ 80	\$ 4,112,700
505.10130	Catch Basin, MAG Det. 533, Type D	6	EACH	\$ 4,500	\$ 27,000
523.10160	Headwall, MAG Det. 501, Straight Type, 60" Pipe	3	EACH	\$ 3,500	\$ 10,500
523.10260	Headwall, MAG Det. 501, Straight Type, 2-60" Pipe	1	EACH	\$ 4,000	\$ 4,000
525.03217	Reinforced Concrete Channel, 6" Thick	3,409	CY	\$ 300	\$ 1,022,700
618.20460	60" RGRCP, Class IV	9,360	LF	\$ 175	\$ 1,638,000
625.01260	Storm Drain Manhole, MAG Det. 521 & 522, 60" Pipe	12	EACH	\$ 3,500	\$ 42,000
	Transition Structure	1	EACH	\$ 10,000	\$ 10,000
Construction Subtotal					\$ 9,359,500
Potential Utility Relocation					
	Electric Line Relocation	1	EACH	\$ 3,000	\$ 3,000
	Gas Line Relocation	3	EACH	\$ 4,000	\$ 12,000
	Water Line Relocation - 4"/6"	1	EACH	\$ 5,000	\$ 5,000
	Water Line Relocation - 8"	3	EACH	\$ 10,000	\$ 30,000
	Water Line Relocation - 12"	1	EACH	\$ 15,000	\$ 15,000
	Water Line Relocatoin - 16"	1	EACH	\$ 20,000	\$ 20,000
Potential Utility Relocation Subtotal					\$ 85,000
	Right of Way Cost	57	AC	\$ 125,000	\$ 7,125,000
	Design Cost (10% of Construction Cost)				\$ 935,950
Total					\$ 17,505,000

Notes: Construction costs were determined from ADOT Estimated Engineering Construction Cost E2C2.

Manholes estimated from 800 ft spacing, as specified in the 2012 City of Mesa Engineering and Design Standards Manual.

Utility relocation estimates based on typical relocation costs.

Project: *Pecos Road DCR*

Subject: **Opinion of Probable Cost for Design Alternatives**

Designed by: **DWT**

Date: 9/26/2014

KHA Project No: 091131024

Checked by: **MAW**

Date: 9/26/2014

District Project No: 2014C001-1

Alternative 3: Storm drain from Meridian to Ellsworth

MAG Item Number	Description	Qty	Unit	Unit Price	Cost
215.01100	Channel Excavation	39,630	CY	\$ 6	\$ 237,800
215.01510	Earthwork for Retention Basins	331,000	CY	\$ 6	\$ 1,986,000
505.10130	Catch Basin, MAG Det. 533, Type D	31	EACH	\$ 4,500	\$ 139,500
523.10160	Headwall, MAG Det. 501, Straight Type, 60" Pipe	3	EACH	\$ 3,500	\$ 10,500
523.10260	Headwall, MAG Det. 501, Straight Type, 2-60" Pipe	1	EACH	\$ 4,000	\$ 4,000
523.10272	Headwall, MAG Det. 501, Straight Type, 2-72" Pipe	2	EACH	\$ 4,200	\$ 8,400
525.03217	Reinforced Concrete Channel, 6" Thick	3,409	CY	\$ 300	\$ 1,022,700
618.20460	60" RGRCP, Class IV	9,360	LF	\$ 175	\$ 1,638,000
618.20472	72" RGRCP, Class IV	18,480	LF	\$ 300	\$ 5,544,000
625.01260	Storm Drain Manhole, MAG Det. 521 & 522, 60" Pipe	36	EACH	\$ 3,500	\$ 126,000
	Transition Structure	1	EACH	\$ 10,000	\$ 10,000
Construction Subtotal					\$ 10,726,900
Potential Utility Relocation					
	Electric Line Relocation	1	EACH	\$ 3,000	\$ 3,000
	Gas Line Relocation	3	EACH	\$ 4,000	\$ 12,000
	Water Line Relocation - 4"/6"	1	EACH	\$ 5,000	\$ 5,000
	Water Line Relocation - 8"	6	EACH	\$ 10,000	\$ 60,000
	Water Line Relocation - 12"	4	EACH	\$ 15,000	\$ 60,000
	Water Line Relocatoin - 16"	1	EACH	\$ 20,000	\$ 20,000
Potential Utility Relocation Subtotal					\$ 160,000
	Right of Way Cost	42	AC	\$ 125,000	\$ 5,250,000
	Design Cost (10% of Construction Cost)				\$ 1,072,690
Total					\$ 17,210,000

Notes: Construction costs were determined from ADOT Estimated Engineering Construction Cost E2C2.

Manholes estimated from 800 ft spacing, as specified in the 2012 City of Mesa Engineering and Design Standards Manual.

Utility relocation estimates based on typical relocation costs.

Appendix F. DCR Drainage System

- Revised HEC-1 Model Output
- Revised stage-storage-discharge tables
- Revised normal depth calculations
- Revised storm drain calculations
- Revised OPC

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 06JAN15 TIME 07:45:05
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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
    
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X X XXXXXXX XXXXX X
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID Pecos Road Channel and Basin Design Concept Report
2 ID DCR System Model
3 ID Future Conditions
4 ID
5 ID DCR System Model: Storm drain from the Pecos Basin to the Ellsworth Channe
6 ID
7 ID Prepared for the Flood Control District of Maricopa County
8 ID District Project Number FCD 2014C001-1
9 ID
10 ID Prepared by Kimley-Horn and Associates, Inc.
11 ID Kimley Horn Project Number 091131024
12 ID January 2015
13 ID
14 ID Model based on Alternative 1 of the East Mesa Area Drainage Master Plan
15 ID Update (EMADMPU). The model was revised to include only those areas
16 ID contributing to the Ellsworth Channel.
17 ID
18 ID List of Changes:
19 ID - Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card
20 ID to a storage routing card with stage-storage-discharge data; the name
21 ID was changed from DIVPB to DETPB to reflect the change.
22 ID - Routing reach from CPR9 to CPR8 was eliminated
23 ID - Powerline section of the model was deleted (all subbasins north of the
24 ID future SR24 alignment).
25 ID - All subbasins south and east of R5 and R8 have been deleted.
26 ID - All comments from the East Mesa Area Drainage Master Plan Update that do
27 ID pertain to the Ellsworth Channel model have been deleted.
28 ID - Area has been adjusted on HC cards to account for reduction in area due
29 ID retention diversions.
30 ID - An additional proposed detention basin was modeled at 222nd Street with
31 ID KK record of DET222.
32 ID - The subbasin boundary between Subbasins E28B and E24B and Subbasins E29
33 ID and E25 have been shifted from Signal Butte Road to 222nd Street to
34 ID more accurately model flows upstream of detention basin DET222.
35 ID - For routing reaches with double pipes a single equivalent diameter pipe
36 ID was modeled.
37 ID
38 ID
39 ID
40 ID *****
41 ID ***** EAST MESA ADMPU *****
42 ID *****
43 ID
44 ID PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
45 ID CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
46 ID PREPARED BY: ENTELLUS, INC.
47 ID PROJECT NO: FCD 2011C017 ENTELLUS 310.057
48 ID MODIFIED DATE: 9/12/2012
49 ID MODELER: RLJ
50 ID
51 ID STORM: 100-YEAR 24-HOUR
52 ID
53 ID DEVELOPMENT CONDITIONS: FUTURE LAND USE INCREASED FUTURE RETENTION (2.19->2.70 IN)
54 ID
55 ID
    
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1 HEC-1 INPUT PAGE 2

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
56        ID          PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
57        ID          MERIDIAN CHANNEL
58        ID          PECOS CHANNEL
59        ID          MERIDIAN AND PECOS RETENTION BASIN
60        ID          GERMANN CHANNEL
61        ID
62        ID          MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
63        ID          100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
64        ID          VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
65        ID          SUBBASINS:
66        ID
67        ID          E28B  E29          E30B
68        ID          E31          E32          E33B
69        ID
70        ID          MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
71        ID          RETOUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
72        ID          WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
73        ID          PROPOSED RETENTION AT MERIDIAN AND PECOS.
74        ID
75        ID          MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
76        ID          COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
77        ID          WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
78        ID          DEFINED ON PECOS ROAD.
79        ID
80        ID          MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
81        ID          DIVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS
82        ID
83        ID
84        ID
85        ID          *****
86        ID          ***** EAST MESA ADMPU *****
87        ID          *****
88        ID          FUTEMADMP24 20110519 - EMADMPU 24-hr Future Conditions 20110519
89        ID          Flood Control District of Maricopa County
90        ID          100 YEAR
91        ID          24 Hour Storm
92        ID          Unit Hydrograph: S-Graph
93        ID          08/05/2011
94        ID          *****
95        IT          5 12Aug14      0      2000      2000
96        IN          15
97        IO          5
          *DIAGRAM
          *
98        JD          3.579  0.0001
99        PC          0.000  0.002  0.005  0.008  0.011  0.014  0.017  0.020  0.023  0.026
100       PC          0.029  0.032  0.035  0.038  0.041  0.044  0.048  0.052  0.056  0.060
101       PC          0.064  0.068  0.072  0.076  0.080  0.085  0.090  0.095  0.100  0.105
102       PC          0.110  0.115  0.120  0.126  0.133  0.140  0.147  0.155  0.163  0.172
103       PC          0.181  0.191  0.203  0.218  0.236  0.257  0.283  0.387  0.663  0.707
104       PC          0.735  0.758  0.776  0.791  0.804  0.815  0.825  0.834  0.842  0.849
105       PC          0.856  0.863  0.869  0.875  0.881  0.887  0.893  0.898  0.903  0.908
106       PC          0.913  0.918  0.922  0.926  0.930  0.934  0.938  0.942  0.946  0.950
107       PC          0.953  0.956  0.959  0.962  0.965  0.968  0.971  0.974  0.977  0.980
108       PC          0.983  0.986  0.989  0.992  0.995  0.998  1.000
    
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1 HEC-1 INPUT PAGE 3

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LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
109       JD          3.561  1.0
110       JD          3.490  5.0
111       JD          3.400  10.0
112       JD          3.286  20.0
113       JD          3.221  30.0
114       JD          3.175  40.0
115       JD          3.139  50.0
116       JD          3.114  60.0
          *
117       KK          E7  BASIN
118       KM          Runoff from subbasin E7
119       BA          1.124
120       LG          0.24  0.26  5.10  0.32  35
121       UI          0      64  64  102  224  281  328  369  416  477
122       UI          561  725  814  670  575  512  449  390  339  300
123       UI          226  159  113  106  99  64  64  46  20  20
124       UI          20  20  20  20  20  20  0  0  0  0
125       UI          0      0  0  0  0  0  0  0  0  0
          *
126       KK          DIVE7  DIVERT
127       KM          Divert the required retention volume for the subbasin out of the model
128       DT          RETE7  85.5  0.0
129       DI          0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
130       DQ          0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
          *
131       KK          E7STOR STORAGE
132       RS          1  STOR
    
```

133	SV	22.82	34.23	45.64	78.34	111.03	143.72	176.42	230.23	284.04
134	SQ		1.75	5.50	11.00	17.70	25.70	34.20	43.00	51.70
135	SE	1566.0	1567.00	1567.50	1568.00	1568.50	1569.00	1569.50	1570.00	1570.50
136	ST	1574.0	10000.0	3.0	1.5					

137	KK	E7E6	ROUTE							
138	KM	Route	outfall	from	E7STOR	to	CPE6			
139	RS	23	FLOW							
140	RC	0.035	0.030	0.030	16362	0.0062	5.50			
141	RX	0.00	500.00	980.00	1003.00	1007.00	1031.00	1511.00	2011.00	
142	RY	5.50	4.50	4.00	1.00	1.00	4.00	4.50	5.50	

143	KK	E6B	BASIN							
144	KM	Runoff	from	subbasin	E6B					
145	BA	1.949								
146	LG	0.14	0.25	6.00	0.24	59				
147	UI	0	174	277	677	898	1079	1330	1853	2099
148	UI	1321	1068	853	594	331	288	192	162	53
149	UI	53	53	53	0	0	0	0	0	0
150	UI	0	0	0	0	0	0	0	0	0
151	UI	0	0	0	0	0	0	0	0	0

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

152	KK	DIVE6B	DIVERT							
153	KM	Divert	the	required	retention	volume	for	the	subbasin	out
154	DT	RETE6B	179.9	0.0						
155	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
156	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

157	KK	E8	BASIN							
158	KM	Runoff	from	subbasin	E8					
159	BA	1.099								
160	LG	0.21	0.25	4.50	0.44	39				
161	UI	0	75	75	201	313	383	441	514	604
162	UI	955	771	649	563	475	401	337	241	145
163	UI	114	75	75	28	23	23	23	23	23
164	UI	0	0	0	0	0	0	0	0	0
165	UI	0	0	0	0	0	0	0	0	0

166	KK	DIVE8	DIVERT							
167	KM	Divert	the	required	retention	volume	for	the	subbasin	out
168	DT	RETE8	80.9	0.0						
169	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
170	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

171	KK	E8E6	ROUTE							
172	KM	Route	runoff	from	subbasin	E8	that	is	not	retained
173	RS	9	FLOW							
174	RC	0.060	0.035	0.060	9833	0.0052	5.50			
175	RX	0.00	500.00	980.00	1003.00	1007.00	1031.00	1511.00	2011.00	
176	RY	5.50	4.50	4.00	1.00	1.00	4.00	4.50	5.50	

177	KK	CPE6	COMBINE							
178	KM	Combine	routed	flow	from	E7STOR	and	subbasin	E8	with
179	KM	subbasin	E6B.							
180	HC	3	3.05							

181	KK	DE6S	DIVERT							
182	KM	Flow	split	diversion,	DRE9	to	the	south,	DE6S	to
183	DT	DRE9	0.0	0.0						
184	DI	0.0	236.0	682.0	1141.0	1670.0	2261.0	2886.0	0.0	0.0
185	DQ	0.0	1.0	13.0	212.0	633.0	1096.0	1568.0	0.0	0.0

186	KK	E6E15	ROUTE							
187	KM	Route	remaining	flow	from	flow	split	at	DE6S	west
188	RS	7	FLOW							
189	RC	0.035	0.030	0.035	8259	0.0042	5.50			
190	RX	950.00	975.00	991.00	1003.00	1007.00	1019.00	1030.00	1065.00	
191	RY	5.50	4.50	4.00	1.00	1.00	4.00	4.50	5.50	

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

192	KK	E5B	BASIN							
193	KM	Runoff	from	subbasin	E5B					
194	BA	0.286								
195	LG	0.14	0.25	3.95	0.64	62				
196	UI	0	64	225	342	567	435	287	148	74
197	UI	15	15	0	0	0	0	0	0	36

263	KM	Runoff from subbasin E9									
264	BA	0.723									
265	LG	0.14	0.25	5.40	0.30	58					
266	UI	0	88	253	450	585	836	1040	754	570	416
267	UI	225	148	92	48	27	27	27	0	0	0
268	UI	0	0	0	0	0	0	0	0	0	0
269	UI	0	0	0	0	0	0	0	0	0	0
270	UI	0	0	0	0	0	0	0	0	0	0
	*										

HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

271	KK	DIVE9 DIVERT									
272	KM	Divert the required retention volume for the subbasin out of the model									
273	DT	RETE9		65.4 0.0							
274	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
275	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*										

276	KK	CPE9 COMBINE									
277	KM	Combine routed flow from split at CPE6 (DRE9) with unretained runoff from									
278	KM	subbasin E9									
279	HC	2	1.07								
	*										

280	KK	DE9S DIVERT									
281	KM	Flow split diversion, DRR5 to the south, DE9S to the west									
282	DT	DRR5		0.0 0.0							
283	DI	0.0	78.0	163.0	440.0	936.0	1475.0	2024.0	0.0	0.0	0.0
284	DQ	0.0	1.0	43.0	245.0	670.0	1157.0	1661.0	0.0	0.0	0.0
	*										

285	KK	E9E16 ROUTE									
286	KM	Route remaining flow from flow split at DE9S west to CPE16									
287	RS	6		FLOW							
288	RC	0.035	0.030	0.035	6751	0.0040	5.50				
289	RX	950.00	985.00	991.00	1003.00	1007.00	1019.00	1025.00	1060.00		
290	RY	5.50	4.50	4.00	1.00	1.00	4.00	4.50	5.50		
	*										

291	KK	DRR5RETRIEVE									
292	KM	Retrieve flow from split at DRR5 that goes to the south									
293	DR	DRR5									
	*										

294	KK	R5 BASIN									
295	KM	Runoff from subbasin R5									
296	BA	0.504									
297	LG	0.29	0.25	5.40	0.27	21					
298	UI	0	53	120	241	310	393	574	608	455	358
299	UI	277	189	98	80	53	26	16	16	16	16
300	UI	0	0	0	0	0	0	0	0	0	0
301	UI	0	0	0	0	0	0	0	0	0	0
302	UI	0	0	0	0	0	0	0	0	0	0
	*										

303	KK	DIVR5 DIVERT									
304	KM	Divert the required retention volume for the subbasin out of the model									
305	DT	RETR5		1.0 0.0							
306	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
307	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*										

HEC-1 INPUT

PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

308	KK	CPR5 COMBINE									
309	KM	Combine routed flow from split at CPE9 (DRR5) with unretained runoff from									
310	KM	subbasin R5									
311	HC	2	1.07								
	*										

312	KK	R5R8 ROUTE									
313	KM	Route combined runoff from CPR5 to CPR8									
314	RS	5		FLOW							
315	RC	0.040	0.035	0.040	6587	0.0043	5.00				
316	RX	966.00	986.00	994.00	1006.00	1012.00	1024.00	1032.00	1052.00		
317	RY	5.00	4.50	4.00	1.00	1.00	4.00	4.50	5.00		
	*										

318	KK	R8 BASIN									
319	KM	Runoff from subbasin R8									
320	BA	0.554									
321	LG	0.16	0.25	4.60	0.45	64					
322	UI	0	69	208	360	471	695	788	567	421	299
323	UI	149	105	69	23	21	21	21	0	0	0
324	UI	0	0	0	0	0	0	0	0	0	0
325	UI	0	0	0	0	0	0	0	0	0	0
326	UI	0	0	0	0	0	0	0	0	0	0
	*										

327 KK DIVR8 DIVERT
 328 KM Divert the required retention volume for the subbasin out of the model
 329 DT RETR8 50.5 0.0
 330 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 331 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

332 KK CPR8 COMBINE
 333 KM Combine routed runoff from CPR5 with unretained runoff from subbasin R8
 334 HC 2 1.62
 *

335 KK R8E16 ROUTE
 336 KM Route combined flows from CPR8 to CPE16 in the proposed MERIDIAN SOUTH CHANNE
 337 RS 3 FLOW
 338 RC 0.03 0.04 0.03 2660 0.001
 339 RX 0 16 33 45 58 71 87 103
 340 RY 7 3 0 0 0 0 3 7
 *

341 KK E16 BASIN
 342 KM Runoff from subbasin E16
 343 BA 0.396
 344 LG 0.15 0.25 5.10 0.35 57
 345 UI 0 58 224 342 497 684 480 338 207 100
 346 UI 64 26 18 18 0 0 0 0 0
 347 UI 0 0 0 0 0 0 0 0 0
 348 UI 0 0 0 0 0 0 0 0 0
 349 UI 0 0 0 0 0 0 0 0 0
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

350 KK DIVE16 DIVERT
 351 KM Divert the required retention volume for the subbasin out of the model
 352 DT RETE16 35.1 0.0
 353 DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 354 DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
 *

355 KK CPE16 COMBINE
 356 KM Combine routed flow from split at CPE9 (DRR5, DE9S) and routed flow from CPR8
 357 KM with unretained runoff from subbasin E16.
 358 HC 3 2.52
 *

359 KK E16E15 ROUTE
 360 KM Route combined flows from CPE16 to CPE15 in the MERIDIAN SOUTH CHANNEL
 361 RS 4 FLOW
 362 RC 0.03 0.04 0.03 4120 0.001
 363 RX 0 16 33 44 56 68 84 100
 364 RY 7 3 0 0 0 0 3 7
 *

365 KK CPE15 COMBINE
 366 KM Combine routed flows from CPE16 in the MERIDIAN SOUTH CHANNEL with flows
 367 KM from the north and east at the southwest corner of Pecos and Meridian. These
 368 KM flows combine in the proposed Pecos Basin (DETPB)
 369 HC 2 6.81
 *

370 KK DETPB STORAGE
 371 KM Proposed inline retention basin at SWC Meridian and Pecos
 372 KM Basin is 9 ft deep with 1 foot provided for freeboard
 373 KM Approximately 134 ac-ft provided (not including freeboard)
 374 KO 3
 375 RS 1 STOR
 376 SV 0 0.7 8.3 25.2 45.8 66.9 88.6 110.9 133.8 157.2
 377 SQ 0 12 45 58 90 120 148 167 184 199
 378 SE 1428 1429 1430 1431 1432 1433 1434 1435 1436 1437
 *

379 KK E1524B ROUTE
 380 KM Route discharge from basin DETPB in PECOS STORM DRAIN to 222nd St & Pecos
 381 KM Pipe size selected based on equivalent size for two pipes
 382 RD 5160 0.0035 0.013 CIRC 7
 *

383 KK E25 BASIN
 384 KM Runoff from subbasin E25
 385 KM Modified as part of the Pecos Road DCR to move the western subbasin boundary
 386 KM from Signal Butte to 222nd Street
 387 BA 1.180
 388 LG 0.15 0.25 5.85 0.25 55
 389 UI 0 137 368 676 870 1180 1677 1273 980 738
 390 UI 494 245 190 130 42 42 42 42 0 0
 391 UI 0 0 0 0 0 0 0 0 0 0
 *

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

392	UI	0	0	0	0	0	0	0	0	0	0
393	UI	0	0	0	0	0	0	0	0	0	0
	*										
394	KK	DIVE25 DIVERT									
395	KM	Divert the required retention volume for the subbasin out of the model									
396	KM	Modified as part of the Pecos Road DCR from 89.8 to 112.1									
397	DT	RETE25	112.1	0.0							
398	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
399	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*										
400	KK	E24B BASIN									
401	KM	Runoff from subbasin E24B									
402	KM	Modified as part of the Pecos Road DCR to move the western subbasin boundary									
403	KM	from Signal Butte to 222nd Street									
404	BA	0.582									
405	LG	0.15	0.15	7.58	0.13	57					
406	UI	0	84	313	483	686	996	717	512	333	154
407	UI	103	50	26	26	0	0	0	0	0	0
408	UI	0	0	0	0	0	0	0	0	0	0
409	UI	0	0	0	0	0	0	0	0	0	0
410	UI	0	0	0	0	0	0	0	0	0	0
	*										
411	KK	DIV24B DIVERT									
412	KM	Divert the required retention volume for the subbasin out of the model									
413	KM	Modified as part of the Pecos Road DCR from 44.4 to 55.8									
414	DT	RET24B	55.8	0.0							
415	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
416	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*										
417	KK	CPE24B COMBINE									
418	KM	Combine routed discharge from basin DETPB with unretained runoff from									
419	KM	subbasins E25 and E24B in PECOS CHANNEL at Signal Butte & Pecos									
420	HC	3 8.20									
	*										
421	KK	DET222 STORAGE									
422	KM	Proposed inline retention basin at NEC 222nd St and Pecos									
423	KM	Basin is 7.9 ft deep with 1 foot provided for freeboard									
424	KM	Approximately 34 ac-ft provided (not including freeboard)									
425	KO	3									
426	RS	1 STOR									
427	SV	0	2.0	6.4	11.3	16.4	22.0	27.8	33.9	39.7	
428	SQ	0	16	53	54	97	150	200	236	260	
429	SE	1408	1409	1410	1411	1412	1413	1414	1415	1415.9	
	*										
		HEC-1 INPUT									
		PAGE 11									
LINE	ID12345678910
430	KK	E24E28 ROUTE									
431	KM	Route combined flows from CPE24B in PECOS STORM DRAIN to CPE28B at Crismon									
432	KM	and Pecos									
433	KM	Pipe size selected based on equivalent size for two pipes									
434	RD	3970	0.0035	0.013		CIRC	9				
	*										
435	KK	E28B BASIN									
436	KM	Runoff from subbasin E28B									
437	KM	Modified as part of the Pecos Road DCR to move the eastern subbasin boundary									
438	KM	from Signal Butte to 222nd Street									
439	BA	0.418									
440	LG	0.22	0.15	8.36	0.10	48					
441	UI	0	52	154	268	350	512	598	430	321	232
442	UI	115	82	52	20	16	16	16	0	0	0
443	UI	0	0	0	0	0	0	0	0	0	0
444	UI	0	0	0	0	0	0	0	0	0	0
445	UI	0	0	0	0	0	0	0	0	0	0
	*										
446	KK	DIV28B DIVERT									
447	KM	Divert the required retention volume for the subbasin out of the model									
448	KM	Modified as part of the Pecos Road DCR from 51.3 to 39.9									
449	DT	RET28B	39.9	0.0							
450	DI	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
451	DQ	0.0	10000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	*										
452	KK	E29 BASIN									
453	KM	Runoff from subbasin E29									
454	KM	Modified as part of the Pecos Road DCR to move the eastern subbasin boundary									
455	KM	from Signal Butte to 222nd Street									
456	BA	0.754									
457	LG	0.15	0.25	5.85	0.26	55					
458	UI	0	84	212	400	516	675	1012	846	651	498
459	UI	368	191	141	88	53	26	26	26	0	0
460	UI	0	0	0	0	0	0	0	0	0	0
461	UI	0	0	0	0	0	0	0	0	0	0

```

462      UI      0      0      0      0      0      0      0      0      0      0
      *
463      KK  DIVE29  DIVERT
464      KM  Divert the required retention volume for the subbasin out of the model
465      KM  Modified as part of the Pecos Road DCR from 90.2 to 67.9
466      DT  RETE29   67.9   0.0
467      DI      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
468      DQ      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

1 HEC-1 INPUT PAGE 12

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

469      KK  CPE28B  COMBINE
470      KM  Combine routed flow from CPE24B with unretained runoff from subbasins E28B
471      KM  and E29 in the PECOS STORM DRAIN at Crismon and Pecos
472      HC      3      9.74
      *
    
```

```

473      KK  E28E31  ROUTE
474      KM  Route flows in the PECOS STORM DRAIN from CPE28B to CPE31 at Ellsworth and Pe
475      RD  5400  0.0035  0.013          CIRC      9
      *
    
```

```

476      KK      E31  BASIN
477      KM  Runoff from subbasin E31
478      BA  0.810
479      LG  0.15   0.25   4.80   0.39   55
480      UI      0      86      197      391      504      641      943      970      728      571
481      UI      441      296      151      126      86      37      26      26      26      0
482      UI      0      0      0      0      0      0      0      0      0      0
483      UI      0      0      0      0      0      0      0      0      0      0
484      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

```

485      KK  DIVE31  DIVERT
486      KM  Divert the required retention volume for the subbasin out of the model
487      KM  MODIFIED MAX VOLUME FROM 56.5 TO 68.9
488      DT  RETE31   68.9   0.0
489      DI      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
490      DQ      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

```

491      KK  CPE31A  COMBINE
492      KM  Combine routed flows from CPE28B with unretained runoff from subbasin E31 at
493      KM  in the PECOS CHANNEL at Ellsworth and Pecos
494      HC      2      10.55
      *
    
```

```

495      KK      E32  BASIN
496      KM  Runoff from subbasin E32
497      BA  0.246
498      LG  0.14   0.25   4.25   0.55   58
499      UI      0      72      238      387      535      337      190      78      37      15
500      UI      15      0      0      0      0      0      0      0      0      0
501      UI      0      0      0      0      0      0      0      0      0      0
502      UI      0      0      0      0      0      0      0      0      0      0
503      UI      0      0      0      0      0      0      0      0      0      0
      *
    
```

```

504      KK  DIVE32  DIVERT
505      KM  Divert the required retention volume for the subbasin out of the model
506      KM  MODIFIED MAX VOLUME FROM 17.2 TO 20.9
507      DT  RETE32   20.9   0.0
508      DI      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
509      DQ      0.0 10000.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0.0
      *
    
```

1 HEC-1 INPUT PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

510      KK  E32E31  ROUTE
511      KM  Route unretained runoff from subbasin E32 to CPE31
512      RS      5      FLOW
513      RC  0.025  0.060  0.025  3272  0.0028 1388.60
514      RX 100.00 110.00 128.00 149.80 160.00 191.50 209.20 210.00
515      RY 1388.3 1388.32 1388.32 1380.37 1380.17 1388.04 1388.39 1388.60
      *
    
```

```

516      KK  CPE31  COMBINE
517      KM  Combine unretained runoff from subbasin E32 with the flows from the PECOS
518      KM  CHANNEL at CPE31 - Ellsworth and Pecos
519      HC      2      10.80
      *
    
```

```

520      KK  E31E30  ROUTE
521      KM  Route runoff from CPE31 north in the Ellsworth Channel to CPE30
522      RS      5      FLOW
523      RC  0.025  0.045  0.025  4404  0.0008 1387.00
524      RX 100.00 107.00 112.50 144.90 175.10 201.50 225.90 244.00
    
```

```

525      RY 1386.1 1386.09 1386.09 1377.99 1377.99 1384.59 1385.08 1387.00
        *

526      KK E30B  BASIN
527      KM Runoff from subbasin E30B
528      BA 0.882
529      LG 0.24  0.15  8.40  0.09  47
530      UI 0      56      56      128  217  272  314  357  416  500
531      UI 668    683    552    475  416  355  303  261  191  124
532      UI 98     92     66     56   44   17   17   17   17   17
533      UI 17     17     0      0    0    0    0    0    0    0
534      UI 0      0      0      0    0    0    0    0    0    0
        *

535      KK DIV30B DIVERT
536      KM Divert the required retention volume for the subbasin out of the model
537      KM MODIFIED MAX VOLUME FROM 67.1 TO 81.9
538      DT RET30B 81.9  0.0
539      DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
540      DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
        *

541      KK CPE30 COMBINE
542      KM Combine routed flow from CPE31 in the Ellsworth Channel with unretained
543      KM runoff from subbasin E30B
544      HC 2 11.68
        *

545      KK E30E26 ROUTE
546      KM Route combined runoff from CPE30 to CPE26 in the Ellsworth Channel
547      RS 1 FLOW
548      RC 0.025 0.035 0.025 822 0.0005 1387.00
549      RX 100.00 105.00 108.50 149.90 220.10 251.30 279.10 285.10
550      RY 1387.0 1387.00 1386.66 1376.31 1376.31 1384.11 1384.66 1386.00
        *
    
```

1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

551      KK E26B  BASIN
552      KM Runoff from subbasin E26B
553      BA 0.259
554      LG 0.24  0.15  8.80  0.07  48
555      UI 0      38      145  222  320  448  315  222  139  65
556      UI 43     18      12   12   0    0    0    0    0    0
557      UI 0      0      0    0    0    0    0    0    0    0
558      UI 0      0      0    0    0    0    0    0    0    0
559      UI 0      0      0    0    0    0    0    0    0    0
        *

560      KK DIV26B DIVERT
561      KM Divert the required retention volume for the subbasin out of the model
562      KM MODIFIED MAX VOLUME FROM 20.1 TO 24.5
563      DT RET26B 24.5  0.0
564      DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
565      DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
        *

566      KK CPE26 COMBINE
567      KM Combined routed flows from CPE30 with unretained runoff from subbasin E26B
568      HC 2 11.94
        *

569      KK E26E33 ROUTE
570      KM Route combine flows from CPE26 to CPE33 in the Ellsworth Channel
571      RS 5 FLOW
572      RC 0.025 0.030 0.025 8929 0.0028 1379.67
573      RX 100.00 100.50 102.50 134.90 205.10 237.50 253.50 255.00
574      RY 1379.1 1379.12 1379.35 1371.25 1371.25 1379.35 1379.67 1379.67
        *

575      KK E33B  BASIN
576      KM Runoff from subbasin E33B
577      BA 0.851
578      LG 0.15  0.15  7.30  0.14  56
579      UI 0      117    409  651  892  1385  1087  793  558  278
580      UI 179    110    36   36   36   0    0    0    0    0
581      UI 0      0      0    0    0    0    0    0    0    0
582      UI 0      0      0    0    0    0    0    0    0    0
583      UI 0      0      0    0    0    0    0    0    0    0
        *

584      KK DIV33B DIVERT
585      KM Divert the required retention volume for the subbasin out of the model
586      KM MODIFIED MAX VOLUME FROM 66.8 TO 81.5
587      DT RET33B 81.5  0.0
588      DI 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
589      DQ 0.0 10000.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0
        *
    
```

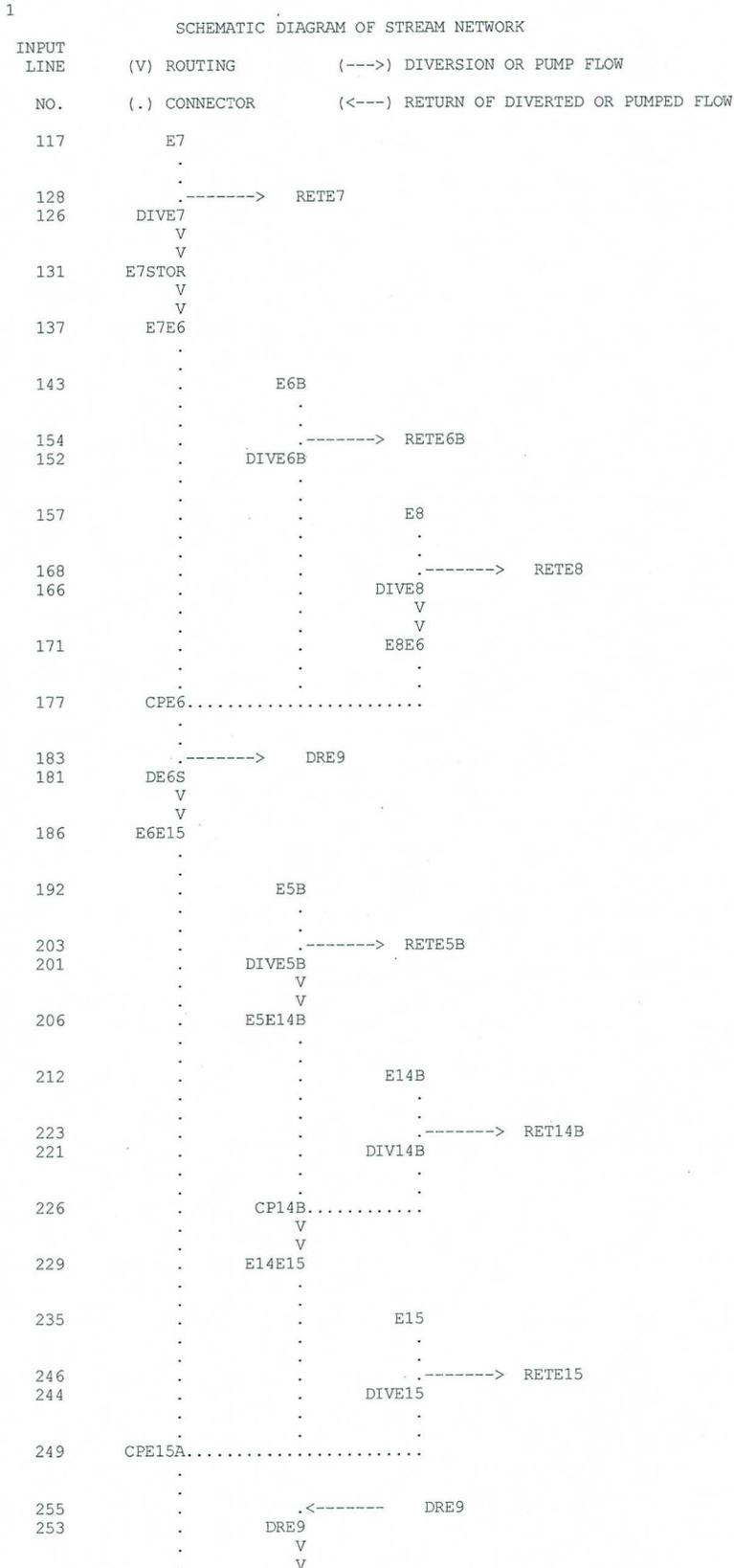
1

HEC-1 INPUT

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

590 KK CPE33B COMBINE
 591 KM Combine routed flows in the Ellsworth Channel from CPE26 with unretained
 592 KM runoff from subbasin E33B. Note this CP also receives flow from the
 593 KM Powerline model but that flow is not included in this model.
 594 HC 2 12.79
 *
 595 ZZ



```

256 . RTE6E9
. . .
262 . . . E9
. . .
273 . . . -----> RETE9
271 . . . DIVE9
. . .
276 . . . CPE9.....
. . .
282 . . . -----> DRR5
280 . . . DE9S
. . . V
. . . V
285 . . . E9E16
. . .
293 . . . <----- DRR5
291 . . . DRR5
. . .
294 . . . R5
. . .
305 . . . -----> RETR5
303 . . . DIVR5
. . .
308 . . . CPR5.....
. . . V
. . . V
312 . . . R5R8
. . .
318 . . . R8
. . .
329 . . . -----> RETR8
327 . . . DIVR8
. . .
332 . . . CPR8.....
. . . V
. . . V
335 . . . R8E16
. . .
341 . . . E16
. . .
352 . . . -----> RETE16
350 . . . DIVE16
. . .
355 . . . CPE16.....
. . . V
. . . V
359 . . . E16E15
. . .
365 . . . CPE15.....
. . . V
. . . V
370 . . . DETPB
. . . V
. . . V
379 . . . E1524B
. . .
383 . . . E25
. . .
397 . . . -----> RETE25
394 . . . DIVE25
. . .
400 . . . E24B
. . .
414 . . . -----> RET24B
411 . . . DIV24B
. . .
417 . . . CPE24B.....
. . . V
. . . V
421 . . . DET222
. . . V
. . . V
430 . . . E24E28
    
```


Pecos Road Channel and Basin Design Concept Report
DCR System Model
Future Conditions

DCR System Model: Storm drain from the Pecos Basin to the Ellsworth Channe

Prepared for the Flood Control District of Maricopa County
District Project Number FCD 2014C001-1

Prepared by Kimley-Horn and Associates, Inc.
Kimley Horn Project Number 091131024
January 2015

Model based on Alternative 1 of the East Mesa Area Drainage Master Plan Update (EMADMPU). The model was revised to include only those areas contributing to the Ellsworth Channel.

List of Changes:

- Basin DIVPB at Pecos Rd and Meridian was changed from a diversion card to a storage routing card with stage-storage-discharge data; the name was changed from DIVPB to DETPB to reflect the change.
- Routing reach from CPR9 to CPR8 was eliminated
- Powerline section of the model was deleted (all subbasins north of the future SR24 alignment).
- All subbasins south and east of R5 and R8 have been deleted.
- All comments from the East Mesa Area Drainage Master Plan Update that do pertain to the Ellsworth Channel model have been deleted.
- Area has been adjusted on HC cards to account for reduction in area due retention diversions.
- An additional proposed detention basin was modeled at 222nd Street with KK record of DET222.
- The subbasin boundary between Subbasins E28B and E24B and Subbasins E29 and E25 have been shifted from Signal Butte Road to 222nd Street to more accurately model flows upstream of detention basin DET222.
- For routing reaches with double pipes a single equivalent diameter pipe was modeled.

***** EAST MESA ADMPU *****

PROJECT: EAST MESA AREA DRAINAGE MASTER PLAN UPDATE
CLIENT: FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
PREPARED BY: ENTELLUS, INC.
PROJECT NO: FCD 2011C017 ENTELLUS 310.057
MODIFIED DATE: 9/12/2012
MODELER: RLJ

STORM: 100-YEAR 24-HOUR

DEVELOPMENT CONDITIONS: FUTURE LAND USE

INCREASED FUTURE RETENTION (2.19-->2.70 IN)

PROPOSED INFRASTRUCTURE: MOUNTAIN CHANNEL AND RETENTION BASIN
MERIDIAN CHANNEL
PECOS CHANNEL
MERIDIAN AND PECOS RETENTION BASIN
GERMANN CHANNEL

MODIFICATION 1: RETENTION VOLUMES WERE INCREASED TO
100-YEAR, 2-HOUR NOAA 2 RAINFALL WITH 80% EFFECTIVE
VOLUME WITHIN THE CITY OF MESA AND TOWN OF QUEEN CREEK FOR THE F
SUBBASINS:

E28B	E29	E30B
E31	E32	E33B

MODIFICATION 4: MERIDIAN CHANNEL (SOUTH OF PECOS): CPR8
ROUTED TO COMBINE NORTH UP MERIDIAN ROAD TO COMBINE
WITH CPE16 AND FOLLOW THE EXISTING FLOW PATH TO
PROPOSED RETENTION AT MERIDIAN AND PECOS.

MODIFICATION 5: PECOS CHANNEL (WEST OF MERIDIAN): CPE24B WAS MODIFIED TO
COMBINE WITH E25 AND WAS ROUTED ON PECOS ROAD. CPE29
WAS MODIFIED TO COMBINE WITH E29. NEW ROUTES WERE
DEFINED ON PECOS ROAD.

MODIFICATION 6: MERIDIAN AND PECOS OFFLINE RETENTION: ADDED DIVERSION
DIVPB AFTER CPE15 WITH A BYPASS FLOW OF 265 CFS

***** EAST MESA ADMPU *****

WARNING --- ROUTED OUTFLOW (513.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (503.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (497.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (489.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (489.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (509.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (499.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (490.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE
 WARNING --- ROUTED OUTFLOW (491.) IS GREATER THAN MAXIMUM OUTFLOW (487.) IN STORAGE-OUTFLOW TABLE

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 370 KK DETPB * STORAGE
 * *

374 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

375 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP STOR TYPE OF INITIAL CONDITION
 RSVRIC .00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

376 SV STORAGE .0 .7 8.3 25.2 45.8 66.9 88.6 110.9 133.8 157.2

377 SQ DISCHARGE 0. 12. 45. 58. 90. 120. 148. 167. 184. 199.

378 SE ELEVATION 1428.00 1429.00 1430.00 1431.00 1432.00 1433.00 1434.00 1435.00 1436.00 1437.00

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA .0 SQ MI

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	166.58-HR
196.	17.42	193.	143.	51.	22.
		(INCHES) .264	.781	.843	.848
		(AC-FT) 96.	284.	306.	308.

PEAK STORAGE + (AC-FT)	TIME (HR)	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	166.58-HR
153.	17.42	149.	96.	33.	14.

PEAK STAGE + (FEET)	TIME (HR)	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	166.58-HR
1436.80	17.42	1436.63	1434.25	1430.29	1428.99

CUMULATIVE AREA = 6.81 SQ MI

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HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 1.0 SQ MI

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	166.58-HR
194.	17.50	191.	141.	51.	22.
		(INCHES) .261	.769	.829	.834
		(AC-FT) 95.	279.	301.	303.

PEAK STORAGE TIME MAXIMUM AVERAGE STORAGE

	(AC-FT)	(HR)	6-HR	24-HR	72-HR	166.58-HR
	149.	17.50	145.	93.	32.	14.

PEAK STAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)				
	1436.65	17.50	1436.48	1434.15	1430.25	1428.97

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 5.0 SQ MI

PEAK FLOW	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)				
	185.	17.67	(CFS)	182.	133.	47.
			(INCHES)	.249	.725	.773
			(AC-FT)	90.	263.	281.
						282.

PEAK STORAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)				
	135.	17.67	132.	84.	29.	12.

PEAK STAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)				
	1436.07	17.67	1435.91	1433.74	1430.07	1428.89

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 10.0 SQ MI

PEAK FLOW	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)				
	173.	17.92	(CFS)	170.	122.	43.
			(INCHES)	.233	.668	.703
			(AC-FT)	85.	243.	255.
						255.

PEAK STORAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)				
	119.	17.92	116.	73.	25.	11.

PEAK STAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)				
	1435.35	17.92	1435.20	1433.24	1429.87	1428.81

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB
 TRANSPOSITION AREA 20.0 SQ MI

PEAK FLOW	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE FLOW		
+	(CFS)	(HR)				
	157.	18.33	(CFS)	154.	109.	38.
			(INCHES)	.211	.596	.619
			(AC-FT)	77.	216.	225.
						225.

PEAK STORAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STORAGE		
+	(AC-FT)	(HR)				
	99.	18.33	96.	61.	20.	9.

PEAK STAGE	TIME		6-HR	24-HR	72-HR	166.58-HR
				MAXIMUM AVERAGE STAGE		
+	(FEET)	(HR)				
	1434.47	18.42	1434.34	1432.65	1429.64	1428.71

CUMULATIVE AREA = 6.81 SQ MI

HYDROGRAPH AT STATION DETPB

		TRANSPOSITION AREA		30.0 SQ MI		
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	148.	18.67	145.	101.	35.	15.
		(CFS)				
		(INCHES)	.197	.553	.570	.570
		(AC-FT)	72.	201.	207.	207.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	89.	18.67	86.	54.	18.	8.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	1434.00	18.58	1433.88	1432.33	1429.52	1428.66
CUMULATIVE AREA =			6.81 SQ MI			

		HYDROGRAPH AT STATION		DETPB		
		TRANSPOSITION AREA		40.0 SQ MI		
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	139.	18.92	136.	96.	33.	14.
		(CFS)				
		(INCHES)	.186	.522	.536	.536
		(AC-FT)	67.	189.	195.	195.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	82.	18.92	79.	50.	17.	7.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	1433.68	18.92	1433.57	1432.13	1429.44	1428.62
CUMULATIVE AREA =			6.81 SQ MI			

		HYDROGRAPH AT STATION		DETPB		
		TRANSPOSITION AREA		50.0 SQ MI		
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	132.	19.17	129.	91.	31.	13.
		(CFS)				
		(INCHES)	.177	.497	.509	.509
		(AC-FT)	64.	181.	185.	185.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	76.	19.17	74.	46.	16.	7.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	1433.44	19.17	1433.34	1431.96	1429.38	1428.60
CUMULATIVE AREA =			6.81 SQ MI			

		HYDROGRAPH AT STATION		DETPB		
		TRANSPOSITION AREA		60.0 SQ MI		
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	128.	19.42	125.	88.	30.	13.
		(CFS)				
		(INCHES)	.171	.480	.491	.491
		(AC-FT)	62.	174.	178.	178.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	166.58-HR
+	73.	19.33	71.	44.	15.	6.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+ 1433.27	19.33	1433.18	1431.85	1429.34	1428.58

CUMULATIVE AREA = 6.81 SQ MI

INTERPOLATED HYDROGRAPH AT DETPB

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	166.58-HR	
+ 180.	17.75	177.	128.	45.	20.	
		(INCHES)	.242	.700	.742	.744
		(AC-FT)	88.	254.	269.	270.

CUMULATIVE AREA = 6.81 SQ MI

421 KK *****
 * DET222 * STORAGE
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425 KO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

HYDROGRAPH ROUTING DATA

426 RS STORAGE ROUTING
 NSTPS 1 NUMBER OF SUBREACHES
 ITYP STOR TYPE OF INITIAL CONDITION
 RSVRIC .00 INITIAL CONDITION
 X .00 WORKING R AND D COEFFICIENT

STATION	STORAGE	6-HR	24-HR	72-HR	166.58-HR	166.58-HR	166.58-HR	166.58-HR	166.58-HR	166.58-HR
427 SV	STORAGE	.0	2.0	6.4	11.3	16.4	22.0	27.8	33.9	39.7
428 SQ	DISCHARGE	0.	16.	53.	54.	97.	150.	200.	236.	260.
429 SE	ELEVATION	1408.00	1409.00	1410.00	1411.00	1412.00	1413.00	1414.00	1415.00	1415.90

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA .0 SQ MI

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	166.58-HR	
+ 239.	18.17	235.	171.	63.	27.	
		(INCHES)	.266	.774	.855	.859
		(AC-FT)	116.	339.	374.	376.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+ 35.	18.17	34.	25.	9.	4.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	166.58-HR
+ 1415.10	18.17	1414.97	1413.51	1410.13	1408.92

CUMULATIVE AREA = 8.20 SQ MI

HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 1.0 SQ MI

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	166.58-HR	
+ 237.	18.08	232.	168.	62.	27.	
		(INCHES)	.263	.762	.840	.844

	(AC-FT)	115.	333.	367.	369.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)				
34.	18.08	33.	25.	9.	4.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)				
1415.02	18.08	1414.89	1413.45	1410.10	1408.91
CUMULATIVE AREA =		8.20 SQ MI			

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 5.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)				
226.	18.17	(CFS)			
		221.	158.	57.	25.
		(INCHES)	.715	.781	.784
		(AC-FT)	110.	342.	343.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)				
32.	18.17	31.	23.	9.	4.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)				
1414.72	18.17	1414.59	1413.20	1409.97	1408.85
CUMULATIVE AREA =		8.20 SQ MI			

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 10.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)				
212.	18.25	(CFS)			
		207.	144.	52.	23.
		(INCHES)	.654	.708	.708
		(AC-FT)	103.	310.	310.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)				
30.	18.25	29.	22.	8.	3.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)				
1414.33	18.25	1414.20	1412.90	1409.83	1408.79
CUMULATIVE AREA =		8.20 SQ MI			

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 20.0 SQ MI

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
		6-HR	24-HR	72-HR	166.58-HR
+ (CFS)	(HR)				
193.	18.33	(CFS)			
		188.	127.	45.	20.
		(INCHES)	.578	.619	.619
		(AC-FT)	93.	271.	271.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (AC-FT)	(HR)				
27.	18.33	26.	20.	7.	3.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE		
		6-HR	24-HR	72-HR	166.58-HR
+ (FEET)	(HR)				
1413.86	18.33	1413.76	1412.53	1409.65	1408.71
CUMULATIVE AREA =		8.20 SQ MI			

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 30.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)					
+	180.	18.92	(CFS)	176.	118.	42.	18.
			(INCHES)	.199	.535	.568	.568
			(AC-FT)	87.	234.	248.	248.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR	
+	(AC-FT)	(HR)					
	26.	18.83	25.	18.	6.	3.	
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE 24-HR	72-HR	166.58-HR	
+	(FEET)	(HR)					
	1413.61	18.92	1413.52	1412.31	1409.55	1408.67	
CUMULATIVE AREA =			8.20 SQ MI				

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 40.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)					
+	170.	19.92	(CFS)	166.	111.	39.	17.
			(INCHES)	.188	.504	.532	.532
			(AC-FT)	82.	221.	233.	233.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR	
+	(AC-FT)	(HR)					
	24.	19.83	24.	17.	6.	3.	
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE 24-HR	72-HR	166.58-HR	
+	(FEET)	(HR)					
	1413.41	19.92	1413.31	1412.16	1409.48	1408.64	
CUMULATIVE AREA =			8.20 SQ MI				

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 50.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)					
+	163.	20.08	(CFS)	158.	106.	37.	16.
			(INCHES)	.179	.480	.504	.504
			(AC-FT)	78.	210.	220.	220.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR	
+	(AC-FT)	(HR)					
	23.	20.00	23.	17.	6.	3.	
PEAK STAGE	TIME		6-HR	MAXIMUM AVERAGE STAGE 24-HR	72-HR	166.58-HR	
+	(FEET)	(HR)					
	1413.25	20.08	1413.16	1412.02	1409.43	1408.62	
CUMULATIVE AREA =			8.20 SQ MI				

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HYDROGRAPH AT STATION DET222
 TRANSPOSITION AREA 60.0 SQ MI

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	166.58-HR	
+	(CFS)	(HR)					
+	157.	20.08	(CFS)	153.	102.	36.	15.
			(INCHES)	.173	.463	.484	.484
			(AC-FT)	76.	203.	212.	212.
PEAK STORAGE	TIME		6-HR	MAXIMUM AVERAGE STORAGE 24-HR	72-HR	166.58-HR	

+		E5E14B	89.	12.92	20.	7.	2.	.29
	HYDROGRAPH AT							
+		E14B	884.	12.25	109.	36.	12.	.53
	DIVERSION TO							
+		RET14B	884.	12.25	88.	24.	8.	.53
	HYDROGRAPH AT							
+		DIV14B	372.	12.50	37.	12.	4.	.53
	2 COMBINED AT							
+		CP14B	371.	12.50	57.	18.	6.	.81
	ROUTED TO							
+		E14E15	210.	12.67	56.	18.	6.	.81
	HYDROGRAPH AT							
+		E15	1096.	12.33	154.	51.	17.	.78
	DIVERSION TO							
+		RETE15	1096.	12.33	122.	34.	11.	.78
	HYDROGRAPH AT							
+		DIVE15	431.	12.67	54.	17.	6.	.78
	3 COMBINED AT							
+		CPE15A	638.	13.58	256.	87.	29.	4.29
	HYDROGRAPH AT							
+		DRE9	104.	13.00	3.	1.	0.	3.05
	ROUTED TO							
+		RTE6E9	26.	13.42	3.	1.	0.	3.05
	HYDROGRAPH AT							
+		E9	968.	12.42	147.	48.	16.	.72
	DIVERSION TO							
+		RETE9	968.	12.42	118.	33.	11.	.72
	HYDROGRAPH AT							
+		DIVE9	372.	12.75	49.	15.	5.	.72
	2 COMBINED AT							
+		CPE9	372.	12.75	52.	16.	5.	1.07
	DIVERSION TO							
+		DRR5	195.	12.75	9.	2.	1.	1.07
	HYDROGRAPH AT							
+		DE9S	176.	12.75	43.	14.	5.	1.07
	ROUTED TO							
+		E9E16	121.	13.25	41.	14.	5.	1.07
	HYDROGRAPH AT							
+		DRR5	195.	12.75	9.	2.	1.	1.07
	HYDROGRAPH AT							
+		R5	546.	12.50	72.	21.	7.	.50
	DIVERSION TO							
+		RETR5	4.	4.67	2.	1.	0.	.50
	HYDROGRAPH AT							
+		DIVR5	546.	12.50	72.	21.	7.	.50
	2 COMBINED AT							
+		CPR5	545.	12.50	81.	23.	8.	1.07
	ROUTED TO							
+		R5R8	472.	12.92	81.	23.	8.	1.07
	HYDROGRAPH AT							
+		R8	741.	12.42	115.	39.	13.	.55
	DIVERSION TO							
+		RETR8	741.	12.42	91.	25.	8.	.55
	HYDROGRAPH AT							
+		DIVR8	366.	12.67	42.	13.	4.	.55
	2 COMBINED AT							
+		CPR8	732.	12.67	119.	36.	12.	1.62
	ROUTED TO							
+		R8E16	649.	13.00	119.	36.	12.	1.62
	HYDROGRAPH AT							
+		E16	582.	12.33	79.	26.	9.	.40
	DIVERSION TO							

+		RETE16	582.	12.33	64.	18.	6.	.40
+	HYDROGRAPH AT	DIVE16	213.	12.58	26.	8.	3.	.40
+	3 COMBINED AT	CPE16	721.	13.00	180.	56.	19.	2.52
+	ROUTED TO	E16E15	679.	13.33	177.	56.	19.	2.52
+	2 COMBINED AT	CPE15	1161.	13.50	405.	136.	45.	6.81
+	ROUTED TO	DETPB	180.	17.75	177.	128.	45.	6.81
+	ROUTED TO	E1524B	180.	17.92	177.	128.	45.	6.81
+	HYDROGRAPH AT	E25	1554.	12.42	236.	77.	26.	1.18
+	DIVERSION TO	RETE25	1554.	12.42	205.	57.	19.	1.18
+	HYDROGRAPH AT	DIVE25	349.	12.92	64.	21.	7.	1.18
+	HYDROGRAPH AT	E24B	916.	12.33	126.	41.	14.	.58
+	DIVERSION TO	RET24B	916.	12.33	102.	28.	9.	.58
+	HYDROGRAPH AT	DIV24B	330.	12.67	41.	13.	4.	.58
+	3 COMBINED AT	CPE24B	352.	13.08	229.	153.	54.	8.20
+	ROUTED TO	DET222	216.	18.25	211.	148.	54.	8.20
+	ROUTED TO	E24E28	216.	18.33	211.	148.	54.	8.20
+	HYDROGRAPH AT	E28B	601.	12.42	88.	28.	9.	.42
+	DIVERSION TO	RET28B	601.	12.42	74.	20.	7.	.42
+	HYDROGRAPH AT	DIV28B	169.	12.83	24.	7.	2.	.42
+	HYDROGRAPH AT	E29	967.	12.42	150.	49.	16.	.75
+	DIVERSION TO	RETE29	967.	12.42	124.	34.	11.	.75
+	HYDROGRAPH AT	DIVE29	344.	12.83	47.	15.	5.	.75
+	3 COMBINED AT	CPE28B	359.	12.92	232.	163.	58.	9.74
+	ROUTED TO	E28E31	383.	13.08	232.	163.	58.	9.74
+	HYDROGRAPH AT	E31	964.	12.42	157.	52.	17.	.81
+	DIVERSION TO	RETE31	964.	12.42	125.	35.	12.	.81
+	HYDROGRAPH AT	DIVE31	402.	12.83	54.	17.	6.	.81
+	2 COMBINED AT	CPE31A	534.	13.08	258.	174.	62.	10.55
+	HYDROGRAPH AT	E32	404.	12.25	48.	16.	5.	.25
+	DIVERSION TO	RETE32	404.	12.25	38.	11.	4.	.25
+	HYDROGRAPH AT	DIVE32	136.	12.50	17.	5.	2.	.25
+	ROUTED TO							

+		E32E31	68.	12.92	.16.	5.	2.	.25
	2 COMBINED AT							
+		CPE31	561.	13.08	270.	178.	64.	10.80
	ROUTED TO							
+		E31E30	343.	13.67	263.	177.	64.	10.80
	HYDROGRAPH AT							
+		E30B	844.	12.83	186.	58.	19.	.88
	DIVERSION TO							
+		RET30B	844.	12.83	151.	41.	14.	.88
	HYDROGRAPH AT							
+		DIV30B	401.	13.33	55.	17.	6.	.88
	2 COMBINED AT							
+		CPE30	517.	13.67	299.	187.	67.	11.68
	ROUTED TO							
+		E30E26	483.	13.75	297.	187.	67.	11.68
	HYDROGRAPH AT							
+		E26B	415.	12.33	56.	18.	6.	.26
	DIVERSION TO							
+		RET26B	415.	12.33	45.	12.	4.	.26
	HYDROGRAPH AT							
+		DIV26B	146.	12.67	17.	5.	2.	.26
	2 COMBINED AT							
+		CPE26	492.	13.75	303.	189.	68.	11.94
	ROUTED TO							
+		E26E33	392.	14.50	294.	188.	68.	11.94
	HYDROGRAPH AT							
+		E33B	1304.	12.33	183.	59.	20.	.85
	DIVERSION TO							
+		RET33B	1304.	12.33	149.	41.	14.	.85
	HYDROGRAPH AT							
+		DIV33B	526.	12.67	57.	18.	6.	.85
	2 COMBINED AT							
+		CPE33B	416.	14.50	313.	197.	72.	12.79

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
 (FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME
							PEAK	TIME TO PEAK	
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR STORM = 1	STORM AREA (SQ MI) =			.00					
E1524B	MANE	5.00	196.00	1050.00	.85	5.00	196.00	1050.00	.85

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3081E+03 EXCESS= .0000E+00 OUTFLOW= .3081E+03 BASIN STORAGE= .9008E-02 PERCENT ERROR= .0

FOR STORM = 2	STORM AREA (SQ MI) =			1.00					
E1524B	MANE	5.00	193.74	1055.00	.83	5.00	193.74	1055.00	.83

CONTINUITY SUMMARY (AC-FT) - INFLOW= .3028E+03 EXCESS= .0000E+00 OUTFLOW= .3028E+03 BASIN STORAGE= .9008E-02 PERCENT ERROR= .0

FOR STORM = 3	STORM AREA (SQ MI) =			5.00					
E1524B	MANE	5.00	185.02	1065.00	.78	5.00	185.02	1065.00	.78

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2821E+03 EXCESS= .0000E+00 OUTFLOW= .2821E+03 BASIN STORAGE= .9008E-02 PERCENT ERROR= .0

FOR STORM = 4	STORM AREA (SQ MI) =			10.00					
E1524B	MANE	5.00	172.87	1085.00	.70	5.00	172.87	1085.00	.70

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2555E+03 EXCESS= .0000E+00 OUTFLOW= .2555E+03 BASIN STORAGE= .8899E-03 PERCENT ERROR= .0

FOR STORM = 5	STORM AREA (SQ MI) =			20.00					
E1524B	MANE	5.00	156.89	1110.00	.62	5.00	156.89	1110.00	.62

CONTINUITY SUMMARY (AC-FT) - INFLOW= .2247E+03 EXCESS= .0000E+00 OUTFLOW= .2247E+03 BASIN STORAGE= .9015E-03 PERCENT ERROR= .0

E28E31	MANE	5.00	567.60	775.00	.81	5.00	567.60	775.00	.81
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4206E+03 EXCESS= .0000E+00 OUTFLOW= .4205E+03 BASIN STORAGE= .9117E-02 PERCENT ERROR= .0									
FOR STORM = 2 STORM AREA (SQ MI) = 1.00									
E28E31	MANE	5.00	515.79	775.00	.80	5.00	515.79	775.00	.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4131E+03 EXCESS= .0000E+00 OUTFLOW= .4130E+03 BASIN STORAGE= .9117E-02 PERCENT ERROR= .0									
FOR STORM = 3 STORM AREA (SQ MI) = 5.00									
E28E31	MANE	5.00	505.95	780.00	.74	5.00	505.95	780.00	.74
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3837E+03 EXCESS= .0000E+00 OUTFLOW= .3836E+03 BASIN STORAGE= .9117E-02 PERCENT ERROR= .0									
FOR STORM = 4 STORM AREA (SQ MI) = 10.00									
E28E31	MANE	5.00	384.75	785.00	.67	5.00	384.75	785.00	.67
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3461E+03 EXCESS= .0000E+00 OUTFLOW= .3461E+03 BASIN STORAGE= .8492E-03 PERCENT ERROR= .0									
FOR STORM = 5 STORM AREA (SQ MI) = 20.00									
E28E31	MANE	5.00	222.87	795.00	.58	5.00	222.87	795.00	.58
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3015E+03 EXCESS= .0000E+00 OUTFLOW= .3015E+03 BASIN STORAGE= .8639E-03 PERCENT ERROR= .0									
FOR STORM = 6 STORM AREA (SQ MI) = 30.00									
E28E31	MANE	5.00	203.37	1095.00	.53	5.00	203.37	1095.00	.53
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2761E+03 EXCESS= .0000E+00 OUTFLOW= .2761E+03 BASIN STORAGE= .8687E-03 PERCENT ERROR= .0									
FOR STORM = 7 STORM AREA (SQ MI) = 40.00									
E28E31	MANE	5.00	191.23	1095.00	.50	5.00	191.23	1095.00	.50
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2582E+03 EXCESS= .0000E+00 OUTFLOW= .2582E+03 BASIN STORAGE= .8456E-03 PERCENT ERROR= .0									
FOR STORM = 8 STORM AREA (SQ MI) = 50.00									
E28E31	MANE	5.00	182.24	1200.00	.47	5.00	182.24	1200.00	.47
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2442E+03 EXCESS= .0000E+00 OUTFLOW= .2442E+03 BASIN STORAGE= .8659E-03 PERCENT ERROR= .0									
FOR STORM = 9 STORM AREA (SQ MI) = 60.00									
E28E31	MANE	5.00	176.60	1200.00	.45	5.00	176.60	1200.00	.45
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2345E+03 EXCESS= .0000E+00 OUTFLOW= .2345E+03 BASIN STORAGE= .8386E-03 PERCENT ERROR= .0									

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION E7STOR
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
PLAN 1	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1567.20	.00	27.	1.	.00	25.75	.00	
PLAN 2	ELEVATION	1566.00	1574.00	1574.00				
	STORAGE	0.	607.	607.				
	OUTFLOW	0.	104.	104.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	1567.17	.00	27.	1.	.00	25.75	.00	
PLAN 3		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				

	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1567.06	.00	24.	0.	.00	26.00	.00
PLAN 4			INITIAL VALUE	SPILLWAY CREST		TOP OF DAM		
	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.91	.00	21.	0.	.00	.00	.00
PLAN 5			INITIAL VALUE	SPILLWAY CREST		TOP OF DAM		
	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.72	.00	16.	0.	.00	.00	.00
PLAN 6			INITIAL VALUE	SPILLWAY CREST		TOP OF DAM		
	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.61	.00	14.	0.	.00	.00	.00
PLAN 7			INITIAL VALUE	SPILLWAY CREST		TOP OF DAM		
	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.53	.00	12.	0.	.00	.00	.00
PLAN 8			INITIAL VALUE	SPILLWAY CREST		TOP OF DAM		
	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.47	.00	11.	0.	.00	.00	.00
PLAN 9			INITIAL VALUE	SPILLWAY CREST		TOP OF DAM		
	ELEVATION	1566.00		1574.00		1574.00		
	STORAGE	0.		607.		607.		
	OUTFLOW	0.		104.		104.		
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	1566.43	.00	10.	0.	.00	.00	.00

Flood Control District of Maricopa County
 Drainage Design Management System
RAINFALL DATA
 Project Reference: PECOS RD - FUT UPDAT

ID	Method	Duration	2 Yr	5 Yr	10 Yr	25 Yr	50 Yr	100 Yr
DEFAULT	NOAA14	5 MIN	0.251	0.340	0.408	0.500	0.572	0.645
	NOAA14	10 MIN	0.383	0.518	0.621	0.762	0.871	0.981
	NOAA14	15 MIN	0.474	0.642	0.770	0.944	1.079	1.216
	NOAA14	30 MIN	0.639	0.865	1.037	1.272	1.453	1.638
	NOAA14	1 HOUR	0.791	1.070	1.283	1.574	1.799	2.027
	NOAA14	2 HOUR	0.897	1.193	1.422	1.731	1.971	2.219
	NOAA14	3 HOUR	0.944	1.239	1.472	1.797	2.055	2.324
	NOAA14	6 HOUR	1.126	1.438	1.686	2.025	2.293	2.572
	NOAA14	12 HOUR	1.278	1.611	1.874	2.231	2.505	2.785
	NOAA14	24 HOUR	1.547	1.982	2.330	2.809	3.184	3.579

Flood Control District of Maricopa County
 Drainage Design Management System
 SOILS

Area ID	Book Number	Map Unit	Soil ID	Area (sq mi)	Area (%)	XKSAT	Rock Percent (%)	Effective Rock (%)	Comments
Major Basin ID: 01									
E24B	645	1	6451	0.047	8.10	0.410	-	100	
	645	22	64522	0.350	60.20	0.040	-	100	
	645	75	64575	0.024	4.10	0.230	-	100	
	645	77	64577	0.058	9.90	0.050	-	100	
	645	112	645112	0.098	16.90	0.390	-	100	
	655	Mv	6554463	0.003	0.50	0.250	-	100	
	655	AnA	655204720	0.001	0.20	0.400	-	100	
E25	645	22	64522	0.001	0.00	0.040	-	100	
	645	75	64575	0.000	0.00	0.230	-	100	
	655	Co	6552449	0.226	19.10	0.040	-	100	
	655	Gf	6553231	0.005	0.40	0.250	-	100	
	655	Gm	6553245	0.369	31.30	0.250	-	100	
	655	Gn	6553247	0.119	10.10	0.040	-	100	
	655	Mv	6554463	0.250	21.20	0.250	-	100	
	655	AnA	655204720	0.210	17.80	0.400	-	100	
E28B	645	22	64522	0.236	56.50	0.040	-	100	
	645	75	64575	0.047	11.30	0.230	-	100	
	645	77	64577	0.075	18.00	0.050	-	100	
	645	78	64578	0.019	4.60	0.050	-	100	
	645	112	645112	0.039	9.40	0.390	-	100	
	655	Co	6552449	0.001	0.20	0.040	-	100	
E29	645	22	64522	0.001	0.10	0.040	-	100	
	645	75	64575	0.001	0.10	0.230	-	100	
	655	Co	6552449	0.167	22.20	0.040	-	100	
	655	Gf	6553231	0.226	30.00	0.250	-	100	
	655	Gm	6553245	0.302	40.10	0.250	-	100	
	655	Gn	6553247	0.018	2.30	0.040	-	100	
	655	Mv	6554463	0.027	3.60	0.250	-	100	
	655	Vf	6556231	0.011	1.50	1.200	-	100	

Flood Control District of Maricopa County
 Drainage Design Management System
LAND USE
 Project Reference: PECOS RD - FUT UPDAT

Sub Basin	Land Use Code	Area (sq mi)	Area (%)	Initial Loss (IA)	Percent Impervious (RTIMP)	Vegetation Cover (%)	DTHETA	Kn	Description
Major Basin ID: 01									
E24B	300	0.5365	92.2	0.15	55	60.0	NORMAL	0.030	General Industrial (Industrial where no detail available)
	610	0.0451	7.8	0.10	80	75.0	NORMAL	0.020	Transportation (Includes railroads, railyards, transit cente
		0.5816	100.0						
E25	300	1.1795	100.0	0.15	55	60.0	NORMAL	0.030	General Industrial (Industrial where no detail available)
		1.1795	100.0						
E28B	190	0.2939	70.3	0.25	45	50.0	NORMAL	0.050	Very High Density Residential - Multi Family (> 15 du per ac
	300	0.1156	27.7	0.15	55	60.0	NORMAL	0.030	General Industrial (Industrial where no detail available)
	610	0.0083	2.0	0.10	80	75.0	NORMAL	0.020	Transportation (Includes railroads, railyards, transit cente
		0.4178	100.0						
E29	300	0.7537	100.0	0.15	55	60.0	NORMAL	0.030	General Industrial (Industrial where no detail available)
		0.7537	100.0						

* Non default value

Flood Control District of Maricopa County
 Drainage Design Management System
 SUB BASINS

Area ID	Sub Basin Parameters								Rainfall Losses				
	Area (sq mi)	Length (mi)	Slope (ft/mi)	S-Graph	Lca (mi)	Lag (min)	Velocity (f/s)	Kn	IA (in)	DTHETA	PSIF (in)	XKSAT (in/hr)	RTIMP (%)
Major Basin ID: 01													
E24B	0.582	1.40	20.6	Valley	0.70	23.30	5.28	0.029	0.15	0.15	7.58	0.126	57
E25	1.180	1.66	15.8	Valley	0.83	28.90	5.06	0.030	0.15	0.25	5.85	0.250	55
E28B	0.418	1.04	25.1	Valley	0.52	27.10	3.36	0.044	0.22	0.15	8.36	0.095	48
E29	0.754	1.63	12.0	Valley	0.82	30.10	4.77	0.030	0.15	0.25	5.85	0.256	55

Project *Pecos Road Channel and Basin DCR*

Subject **Revised Retention Volume Calculations**

Designed by **MAW**

Date 10/29/2014

Project No. 091131024

Checked by

Date

District Project No: 2014C001

Objective: Calculate the updated retention volumes for the subbasins that were updated based on the location of the 222nd Street detention basin.

The updated retention volumes are estimated by calculating the retention volume for the portion of the area that is changing and then adding or subtracting that volume from the current retention volumes.

Change in Retention Volume

Subbasin ID	Current Area [sq mi]	Current Retention [ac-ft]	Retention per Area [ac-ft/sq mi]	Change in Area [sq mi]	Change in Retention [ac-ft]
E28B	0.539	51.3	95.2	0.120	11.4
E29	1.002	90.2	90.0	0.248	22.3

Updated Retention Volume Calculation

Subbasin ID	Current Retention [ac-ft]	Change in Retention [ac-ft]	Revised Retention [ac-ft]
E24B	44.4	11.4	55.8
E25	89.8	22.3	112.1
E28B	51.3	-11.4	39.9
E29	90.2	-22.3	67.9

Notes:

The current area and retention values were taken from the HEC-1 model from the East Mesa Area Drainage Master Plan Update (2014)

Kimley»Horn

Project **Pecos Road DCR**

Subject **Proposed Detention Basin Calculations**

Designed by **MAW**

Date 1/5/2015

Project No. 091131024

Checked by **LSM**

Date 1/5/2015

District Project No: 2014C001

Objective: to estimate the stage-storage-discharge relationship

Detention Basin - SWC Pecos/Meridian

Drains in 21.2 hours

Outlet Diameter 4.50 ft
Outlet Elevation 1428 ft

Outlet X-Sect Area 15.904 ft²
No. of Outlet Barrels 1
Outlet Pipe Slope 0.0032 ft/ft

Elevation [ft]	Surface Storage Area [ft ²]	Surface Storage Area [acre]	Average Area [acre]	Δ Elev [ft]	Δ Vol [ac-ft]	Σ Vol [ac-ft]	Δ Time to Drain [hr]	Q _{pipe} [cfs]
1428	-	-	0.75	1.0	0.7	0	1.5	0
1429	65,295	1.50	7.58	1.0	7.6	0.7	3.2	12
1430	595,321	13.67	16.90	1.0	16.9	8.3	4.0	45
1431	877,394	20.14	20.52	1.0	20.5	25.2	3.4	58
1432	910,727	20.91	21.15	1.0	21.1	45.8	2.4	90
1433	931,720	21.39	21.70	1.0	21.7	66.9	2.0	120
1434	958,877	22.01	22.29	1.0	22.3	88.6	1.7	148
1435	983,198	22.57	22.85	1.0	22.9	110.9	1.6	167
1436	1,007,682	23.13				133.8		184
Freeboard								
1437	1,032,328	23.70	23.42	1.0	23.4	157.2	1.5	199

Notes:

Q_{pipe} calculated using Mannings Equation, FHWA nomograph, and Orifice Equation

Outlet diameter is for a 54" orifice plate on a 60" outlet pipe

Kimley»Horn

Project *Pecos Road DCR*

Subject **Proposed Detention Basin Calculations**

Designed by **MAW**

Date 1/5/2015

Project No. 091131024

Checked by **LSM**

Date 1/5/2015

District Project No: 2014C001

Objective: to estimate the stage-storage-discharge relationship

Detention Basin - NEC Pecos/222nd Street

Drains in

7.7 hours

Outlet Diameter 5.50 ft

Outlet X-Sect Area 23.758 ft²

Outlet Elevation 1408 ft

No. of Outlet Barrels 1

Outlet Pipe Slope 0.0045 ft/ft

Elevation [ft]	Surface Storage Area [ft ²]	Surface Storage Area [acre]	Average Area [acre]	Δ Elev [ft]	Δ Vol [ac-ft]	Σ Vol [ac-ft]	Δ Time to Drain [hr]	Q _{pipe} [cfs]
1408	-	-	1.99	1.0	2.0	0	3.0	0
1409	173,539	3.98	4.36	1.0	4.4	2.0	1.3	16
1410	206,699	4.75	4.89	1.0	4.9	6.4	1.0	64
1411	219,731	5.04	5.20	1.0	5.2	11.3	0.8	54
1412	233,023	5.35	5.51	1.0	5.5	16.4	0.5	97
1413	246,574	5.66	5.82	1.0	5.8	22.0	0.4	150
1414	260,385	5.98	6.14	1.0	6.1	27.8	0.3	200
1415	274,454	6.30				33.9		236
Freeboard								
1415.9	287,339	6.60	6.45	0.9	5.8	39.7	0.3	260

Notes:

Q_{pipe} calculated using Mannings Equation, FHWA nomograph, and Orifice Equation

Worksheet for Meridian Channel - North Segment (upstream)

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.0016	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	13.00	ft
Discharge	371.00	ft ³ /s

Results

Normal Depth	2.97	ft
Flow Area	56.34	ft ²
Wetted Perimeter	26.30	ft
Hydraulic Radius	2.14	ft
Top Width	24.89	ft
Critical Depth	2.56	ft
Critical Slope	0.00279	ft/ft
Velocity	6.59	ft/s
Velocity Head	0.67	ft
Specific Energy	3.65	ft
Froude Number	0.77	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.97	ft
Critical Depth	2.56	ft
Channel Slope	0.0016	ft/ft

Worksheet for Meridian Channel - North Segment (upstream)

GVF Output Data

Critical Slope

0.00279 ft/ft

Cross Section for Meridian Channel - North Segment (upstream)

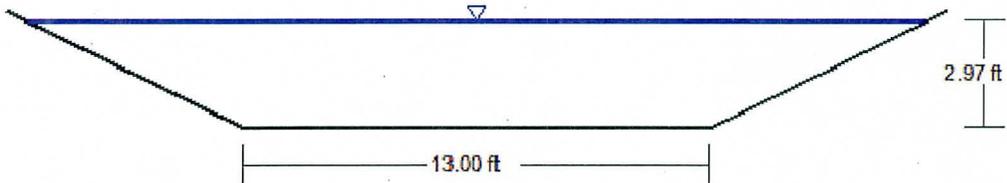
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.0016 ft/ft
Normal Depth	2.97 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	13.00 ft
Discharge	371.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Meridian Channel - North Segment (downstream)

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.0018	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	23.00	ft
Discharge	638.00	ft ³ /s

Results

Normal Depth	2.96	ft
Flow Area	85.59	ft ²
Wetted Perimeter	36.24	ft
Hydraulic Radius	2.36	ft
Top Width	34.84	ft
Critical Depth	2.66	ft
Critical Slope	0.00263	ft/ft
Velocity	7.45	ft/s
Velocity Head	0.86	ft
Specific Energy	3.82	ft
Froude Number	0.84	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.96	ft
Critical Depth	2.66	ft
Channel Slope	0.0018	ft/ft

Worksheet for Meridian Channel - North Segment (downstream)

GVF Output Data

Critical Slope

0.00263 ft/ft

Cross Section for Meridian Channel - North Segment (downstream)

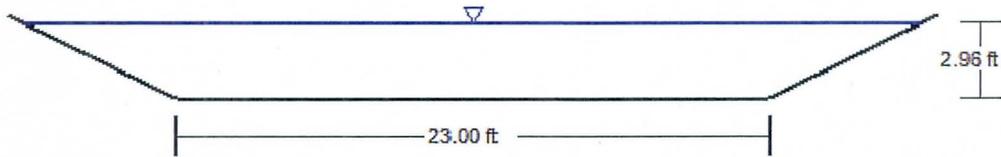
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.0018 ft/ft
Normal Depth	2.96 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	23.00 ft
Discharge	638.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Meridian Channel - South Segment (max slope)

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.0020	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	42.00	ft
Discharge	732.00	ft ³ /s

Results

Normal Depth	2.26	ft
Flow Area	104.91	ft ²
Wetted Perimeter	52.09	ft
Hydraulic Radius	2.01	ft
Top Width	51.02	ft
Critical Depth	2.04	ft
Critical Slope	0.00273	ft/ft
Velocity	6.98	ft/s
Velocity Head	0.76	ft
Specific Energy	3.01	ft
Froude Number	0.86	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.26	ft
Critical Depth	2.04	ft
Channel Slope	0.0020	ft/ft

Worksheet for Meridian Channel - South Segment (max slope)

GVF Output Data

Critical Slope

0.00273 ft/ft

Cross Section for Meridian Channel - South Segment (max slope)

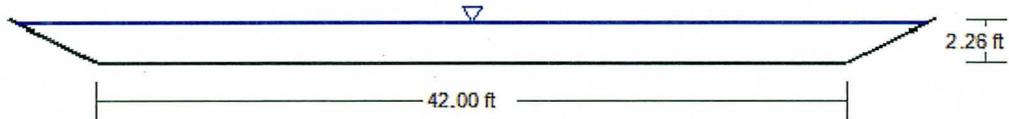
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015
Channel Slope	0.0020 ft/ft
Normal Depth	2.26 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	42.00 ft
Discharge	732.00 ft ³ /s

Cross Section Image



V: 1
H: 1

Worksheet for Meridian Channel - South Segment (min slope)

Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

Roughness Coefficient	0.015	
Channel Slope	0.0015	ft/ft
Left Side Slope	2.00	ft/ft (H:V)
Right Side Slope	2.00	ft/ft (H:V)
Bottom Width	42.00	ft
Discharge	732.00	ft ³ /s

Results

Normal Depth	2.44	ft
Flow Area	114.21	ft ²
Wetted Perimeter	52.90	ft
Hydraulic Radius	2.16	ft
Top Width	51.75	ft
Critical Depth	2.04	ft
Critical Slope	0.00273	ft/ft
Velocity	6.41	ft/s
Velocity Head	0.64	ft
Specific Energy	3.07	ft
Froude Number	0.76	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	2.44	ft
Critical Depth	2.04	ft
Channel Slope	0.0015	ft/ft

Worksheet for Meridian Channel - South Segment (min slope)

GVF Output Data

Critical Slope

0.00273 ft/ft

Cross Section for Meridian Channel - South Segment (min slope)

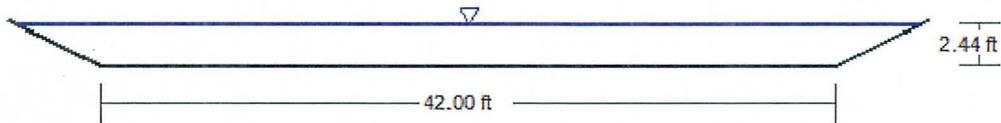
Project Description

Friction Method Manning Formula
Solve For Normal Depth

Input Data

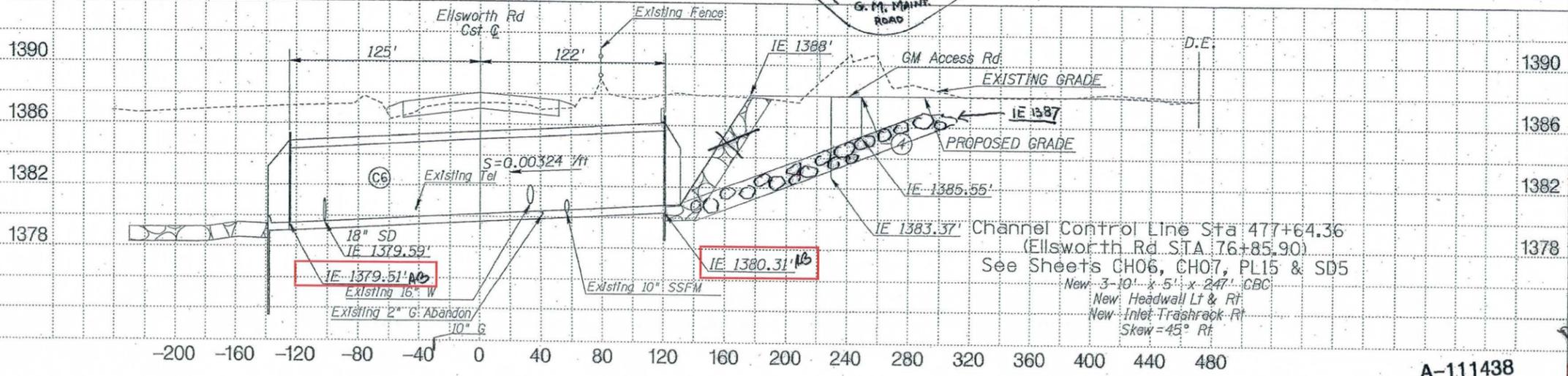
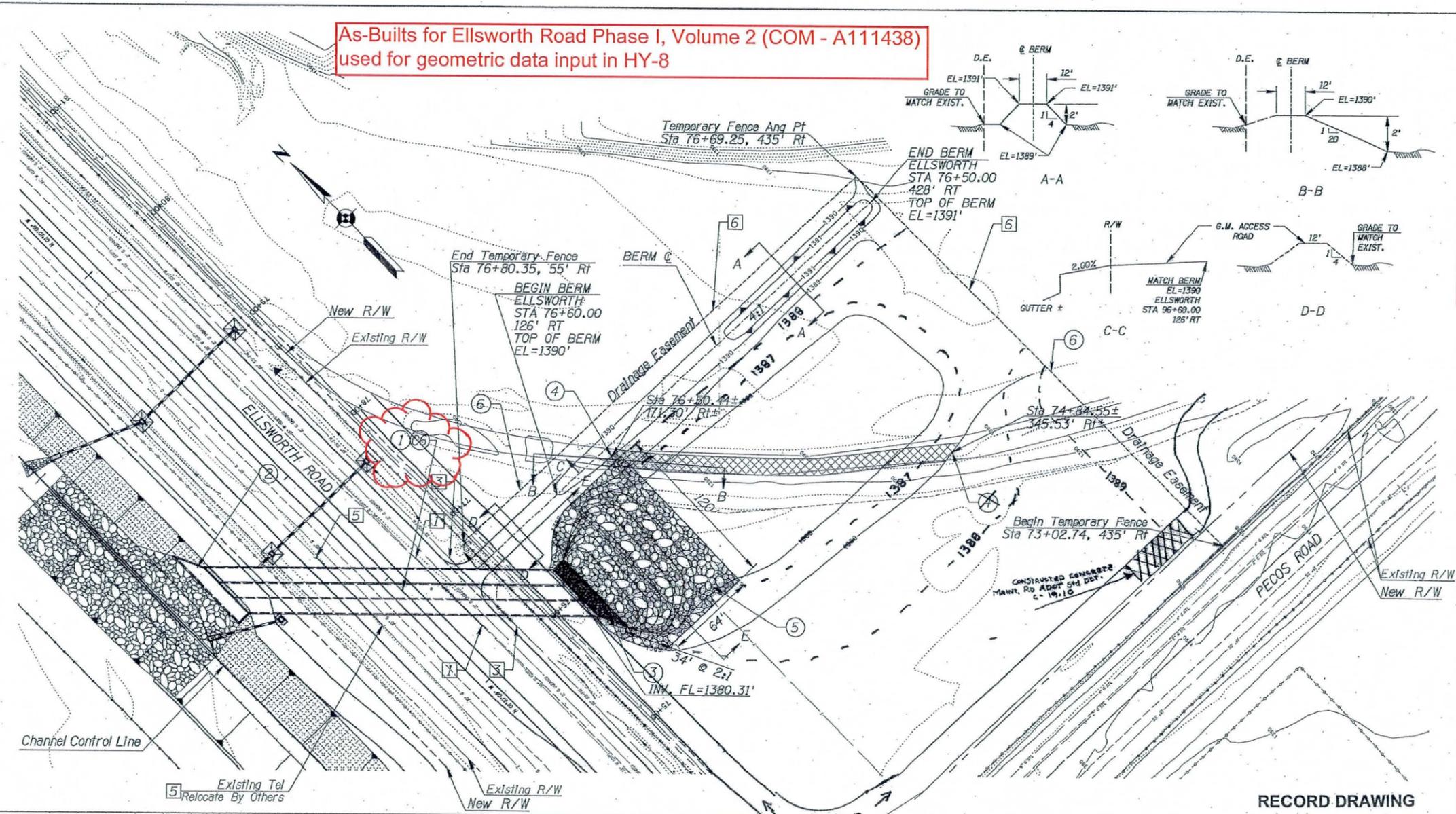
Roughness Coefficient	0.015
Channel Slope	0.0015 ft/ft
Normal Depth	2.44 ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	42.00 ft
Discharge	732.00 ft ³ /s

Cross Section Image



V: 1
H: 1

As-Builts for Ellsworth Road Phase I, Volume 2 (COM - A111438) used for geometric data input in HY-8



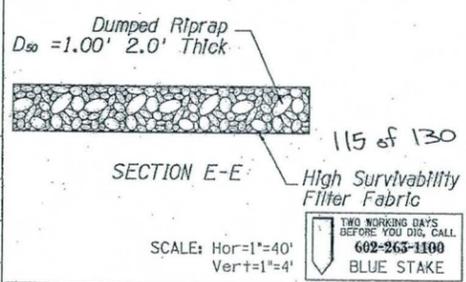
F.H.W.A. REGION	STATE	PROJECT NO.	SHEET NO.	TOTAL SHEETS	RECORD DRAWING
9	AZ	68927	115	130	

REMOVAL /RELOCATE

- 1 Sta 477+64.36, 23.00' Rt, Realign 16" Water Line Per COP Std Det P1370
 - 3 Relocate Existing 10" Sanitary Sewer Force Main.
 - 5 Relocate Existing Telephone.
 - 6 Remove Temporary Fencing, 747 Lf
- CONSTRUCTION
- 1 Sta 477+64.36, Construct 3-10' x 5' x 247' CBC Skew 45° Rt, Construct Inlet Headwall, Apron & Handrails per Structure Drawing Series S01 to S12 & Details
 - 2 Construct Outlet Headwall, Apron & Handrails per Structure Drawing Series S01 to S12 & Details, & Bank Armor, per Detail, Sheet CHD1
 - 3 Construct Trashrack, per Detail, Sheet CHD5
 - 4 Construct 2400 s.f. of Concrete Maintenance Road with Concrete walls per ADOT Std Det C-19.10
 - 5 Construct Dumped Riprap Scour Protection, D₅₀=1.00', Thickness=2.00' Per Dimensions And Section E-E This Sheet
 - 6 6' Temporary Chain Link fence, MAG Det. 160, 747 Lf Sta 73+02.74, 435' Rt to Sta 76+69.25, 345' Rt to Sta 76+80.35, 55' Rt

Structural Quantities

Item	Unit	(C6)
Structural Excavation	cu.yd.	1,834
Structural Backfill	cu.yd.	536
Structural Concrete	cu.yd.	849
Reinforcing Steel	lbs.	122,270
Galv. Pipe Handrail	ft.	131



SCALE: Hor=1"=40' Ver=1"=4'

TWO WORKING DAYS BEFORE YOU DIG, CALL 602-265-1100 BLUE STAKE

NO.	REVISION	BY	DATE

MARICOPA COUNTY
DEPARTMENT OF TRANSPORTATION
ENGINEERING DIVISION

ELLSWORTH ROAD
GERMANN RD TO RAY RD
PROJECT NO. 68927

DESIGNED	DATE
J. CHRISTOPH, R. DAVIES	04/15/05
DRAWN	DATE
S. CARLOCK	04/15/05
CHECKED	DATE
R. DAVIES	04/15/05

AMC Infrastructure Inc.
2001 WEST CAMELBACK ROAD, SUITE 300
PHOENIX, ARIZONA 85015
PHONE (602) 343-2400
FAX (602) 343-2459

CULVERT C6 DETAIL
CHANNEL CULVERT SHEETS

SHEET CHC5 OF CHC6

04/19/2005 10:22:10 AM s:\Plans\68927\chc\made\tp02_E.dgn

A-111438

TRACS NO.

HEC-RAS Plan: Final River: River Reach: Ellsworth Profile: Original

Reach	River Sta	Profile	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Ellsworth	17100	Original	600.00	1384.17	1390.46	1387.48	1390.58	0.000638	2.78	216.12	61.90	0.26
Ellsworth	17000	Original	600.00	1384.11	1390.40	1387.42	1390.51	0.000639	2.78	215.98	72.77	0.26
Ellsworth	16900	Original	600.00	1384.05	1390.33	1387.36	1390.45	0.000641	2.78	215.72	84.61	0.26
Ellsworth	16800	Original	600.00	1383.99	1390.27	1387.29	1390.39	0.000644	2.79	215.42	98.78	0.26
Ellsworth	16700	Original	600.00	1383.93	1390.20	1387.24	1390.32	0.000646	2.79	215.13	132.13	0.26
Ellsworth	16600	Original	600.00	1383.87	1390.14	1387.17	1390.26	0.000649	2.79	214.80	123.12	0.26
Ellsworth	16500	Original	600.00	1383.81	1390.07	1387.12	1390.19	0.000651	2.80	214.53	185.41	0.26
Ellsworth	16400	Original	600.00	1383.75	1390.01	1387.03	1390.13	0.000653	2.80	214.22	166.40	0.26
Ellsworth	16300	Original	600.00	1383.69	1389.94	1387.00	1390.06	0.000657	2.81	213.83	157.76	0.26
Ellsworth	16200	Original	600.00	1383.63	1389.87	1386.93	1390.00	0.000659	2.81	213.49	150.44	0.26
Ellsworth	16100	Original	600.00	1383.57	1389.81	1386.87	1389.93	0.000663	2.82	213.11	148.88	0.26
Ellsworth	16000	Original	600.00	1383.51	1389.74	1386.82	1389.86	0.000667	2.82	212.59	148.70	0.26
Ellsworth	15966.5	Original	600.00	1383.49	1389.71		1389.84	0.000990	2.83	212.27	59.17	0.26
Ellsworth	15947.5	Original	600.00	1383.48	1389.72	1386.03	1389.81	0.000497	2.44	246.18	64.09	0.19
Ellsworth	15937.5	Original	600.00	1383.47	1389.70	1385.74	1389.81	0.000068	2.66	225.22	65.44	0.19
Ellsworth	15920.67	Original	600.00	1383.46	1389.46	1386.31	1389.79	0.000352	4.58	130.97	21.83	0.33
Ellsworth	15895	Culvert										
Ellsworth	15870.67	Original	600.00	1383.42	1388.57		1389.01	0.000546	5.34	112.46	21.83	0.41
Ellsworth	15855.5	Original	600.00	1383.42	1388.76	1385.70	1388.92	0.000854	3.19	188.06	61.04	0.25
Ellsworth	15845.5	Original	600.00	1383.41	1388.77	1385.98	1388.91	0.000536	2.96	202.72	59.18	0.25
Ellsworth	15826.6	Original	600.00	1383.40	1388.66		1388.88	0.001445	3.77	158.99	51.45	0.38
Ellsworth	15809	Original	600.00	1383.43	1388.63		1388.85	0.001508	3.83	156.47	51.05	0.39
Ellsworth	15800	Original	600.00	1383.39	1388.61		1388.84	0.001491	3.82	157.14	51.16	0.38
Ellsworth	15700	Original	600.00	1383.33	1388.44		1388.68	0.001652	3.97	151.23	50.23	0.40
Ellsworth	15600	Original	600.00	1383.27	1388.23		1388.50	0.001878	4.16	144.12	49.08	0.43
Ellsworth	15550	Original	600.00	1383.24	1388.08		1388.38	0.003447	4.34	138.30	48.12	0.45
Ellsworth	15460	Original	600.00	1383.18	1387.66		1388.18	0.000744	5.77	103.92	27.67	0.53
Ellsworth	15450	Original	600.00	1381.86	1387.71	1384.91	1388.12	0.000376	5.16	116.31	109.54	0.39
Ellsworth	15350	Culvert										
Ellsworth	15192	Original	600.00	1380.41	1386.03	1383.69	1386.26	0.001558	3.89	154.36	54.31	0.33
Ellsworth	15100	Original	600.00	1380.33	1385.90	1383.64	1386.08	0.001825	3.43	175.18	53.91	0.33
Ellsworth	15000	Original	600.00	1380.25	1385.74	1383.55	1385.93	0.001188	3.51	171.12	53.30	0.34
Ellsworth	14900	Original	600.00	1380.17	1385.61	1383.48	1385.81	0.001236	3.56	168.62	52.93	0.35
Ellsworth	14800	Original	600.00	1380.09	1385.48	1383.40	1385.68	0.001293	3.62	165.81	52.51	0.36
Ellsworth	14700	Original	600.00	1380.01	1385.34	1383.32	1385.55	0.001362	3.69	162.60	52.02	0.37
Ellsworth	14600	Original	600.00	1379.93	1385.19	1383.23	1385.41	0.001448	3.78	158.90	51.43	0.38
Ellsworth	14579	Original	600.00	1379.90	1385.16	1383.21	1385.38	0.001450	3.78	158.81	51.41	0.38
Ellsworth	14569	Original	600.00	1379.90	1385.14		1385.36	0.001472	3.80	157.91	51.27	0.38
Ellsworth	14501	Original	600.00	1379.85	1385.03		1385.26	0.001556	3.88	154.64	50.76	0.39
Ellsworth	14491	Original	600.00	1379.84	1385.01	1383.15	1385.24	0.001566	3.89	154.29	50.70	0.39
Ellsworth	14451	Original	600.00	1379.81	1384.94	1383.12	1385.18	0.001622	3.94	152.26	50.38	0.40
Ellsworth	14400	Original	600.00	1379.77	1384.84	1383.06	1385.09	0.001700	4.01	149.62	49.97	0.41
Ellsworth	14300	Original	600.00	1379.69	1384.64	1382.99	1384.91	0.001900	4.18	143.50	48.99	0.43
Ellsworth	14200	Original	600.00	1379.61	1384.40	1382.91	1384.70	0.002202	4.42	135.79	47.71	0.46
Ellsworth	14100	Original	600.00	1379.53	1384.10	1382.85	1384.46	0.002722	4.78	125.41	45.94	0.51
Ellsworth	14000	Original	600.00	1379.45	1384.09	1381.74	1384.22	0.001116	2.84	211.15	64.94	0.28
Ellsworth	13900	Original	600.00	1379.37	1384.01	1381.66	1384.13	0.000713	2.85	210.61	64.88	0.28
Ellsworth	13800	Original	600.00	1379.29	1383.94	1381.57	1384.06	0.000707	2.84	211.20	64.95	0.28
Ellsworth	13700	Original	600.00	1379.21	1383.87	1381.49	1383.99	0.000702	2.83	211.80	78.22	0.28
Ellsworth	13600	Original	600.00	1379.13	1383.80	1381.41	1383.92	0.000695	2.82	212.55	78.27	0.28
Ellsworth	13500	Original	600.00	1379.05	1383.73	1381.34						0.27
Ellsworth	13400	Original	600.00	1378.97	1383.66	1381.26						0.27
Ellsworth	13300	Original	600.00	1378.89	1383.59	1381.17						0.27
Ellsworth	13200	Original	600.00	1378.81	1383.53	1381.08						0.27
Ellsworth	13100	Original										0.27
Ellsworth	13000	Original										0.27
Ellsworth	12900	Original										0.27
Ellsworth	12800	Original										0.26
Ellsworth	12700	Original										0.26
Ellsworth	12600	Original										0.26
Ellsworth	12500	Original										0.26
Ellsworth	12400	Original										0.26
Ellsworth	12300	Original										0.25
Ellsworth	12200	Original	600.00	1378.01	1382.91	1380.30						0.25
Ellsworth	12100	Original	600.00	1377.93	1382.85	1380.21	1382.96	0.000563	2.61	229.54	67.16	0.25
Ellsworth	12000	Original	600.00	1377.85	1382.80	1380.13	1382.90	0.000552	2.59	231.23	67.37	0.25

Culvert Location and Size	No.	Approx Sta
Pecos North 3-10' x 5' C.B.C	C-6	Roadway: 76+20 Channel: 477+00 RAS: 14100

Clip from Table 7 of the Final Drainage Report (W.O.#68927, May 2005 by AMEC) for Ellsworth Road Phase I - Germann Road to Ray Road drainage study and HEC-RAS model. The Proposed Conditions HEC-RAS model at RS 14100 was used to determine starting tailwater conditions for the HY-8 model.

HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 100 cfs

Design Flow: 542 cfs

Maximum Flow: 600 cfs

Table 1 - Summary of Culvert Flows at Crossing: Culvert C6

Headwater Elevation (ft)	Total Discharge (cfs)	C6 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
1384.11	100.00	100.00	0.00	1
1384.13	150.00	150.00	0.00	1
1384.16	200.00	200.00	0.00	1
1384.19	250.00	250.00	0.00	1
1384.23	300.00	300.00	0.00	1
1384.27	350.00	350.00	0.00	1
1384.33	400.00	400.00	0.00	1
1384.38	450.00	450.00	0.00	1
1384.45	500.00	500.00	0.00	1
1384.51	542.00	542.00	0.00	1
1384.61	600.00	600.00	0.00	1
1387.50	1485.31	1485.31	0.00	Overtopping

Rating Curve Plot for Crossing: Culvert C6

Total Rating Curve
Crossing: Culvert C6

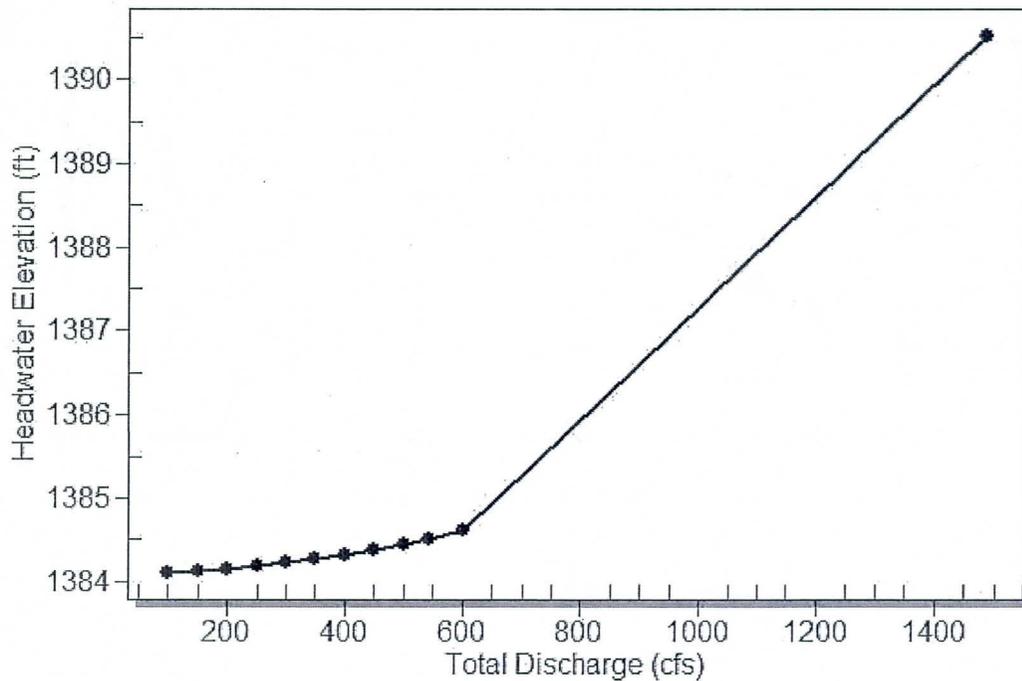
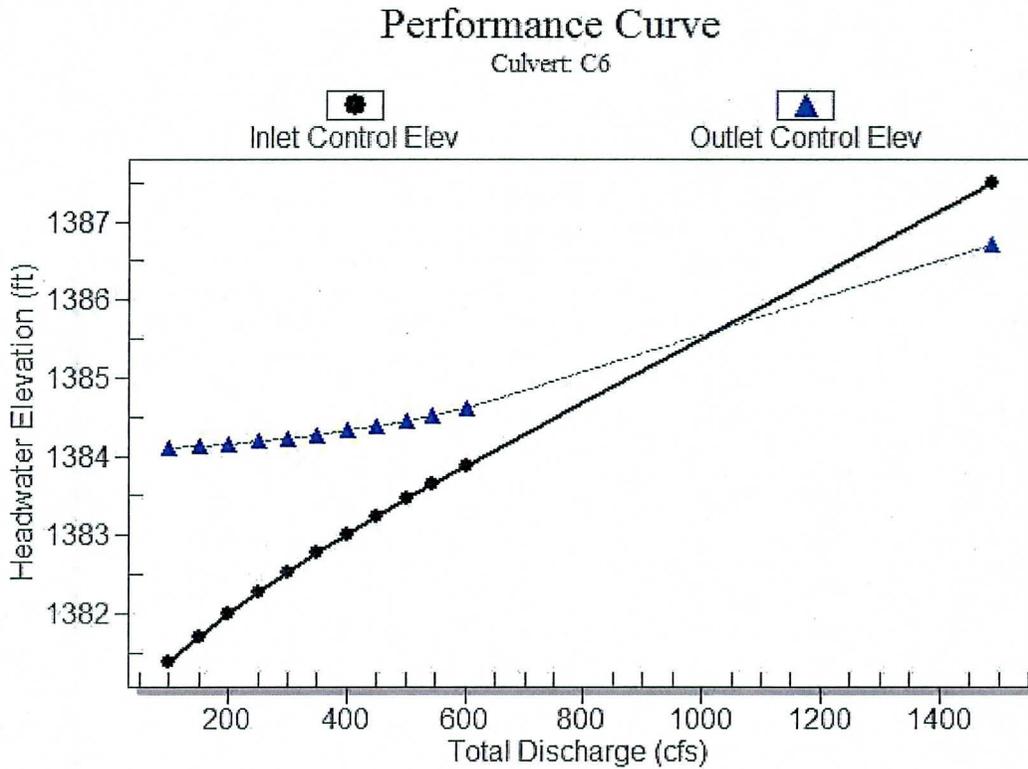


Table 2 - Culvert Summary Table: C6

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
100.00	100.00	1384.11	1.066	3.804	1-S1t	0.649	0.701	4.590	4.590	0.726	0.000
150.00	150.00	1384.13	1.396	3.822	1-S1t	0.860	0.919	4.590	4.590	1.089	0.000
200.00	200.00	1384.16	1.691	3.846	1-S1t	1.033	1.113	4.590	4.590	1.452	0.000
250.00	250.00	1384.19	1.963	3.878	1-S1t	1.194	1.292	4.590	4.590	1.816	0.000
300.00	300.00	1384.23	2.216	3.917	1-S1t	1.356	1.459	4.590	4.590	2.179	0.000
350.00	350.00	1384.27	2.456	3.962	1-S1t	1.495	1.617	4.590	4.590	2.542	0.000
400.00	400.00	1384.33	2.693	4.015	1-S1t	1.634	1.767	4.590	4.590	2.905	0.000
450.00	450.00	1384.38	2.922	4.075	1-S1t	1.772	1.912	4.590	4.590	3.268	0.000
500.00	500.00	1384.45	3.145	4.142	1-S1t	1.902	2.051	4.590	4.590	3.631	0.000
542.00	542.00	1384.51	3.328	4.204	1-S1t	2.007	2.164	4.590	4.590	3.936	0.000
600.00	600.00	1384.61	3.574	4.297	1-S1t	2.152	2.316	4.590	4.590	4.357	0.000

 Straight Culvert
 Inlet Elevation (invert): 1380.31 ft, Outlet Elevation (invert): 1379.51 ft
 Culvert Length: 247.00 ft, Culvert Slope: 0.0032

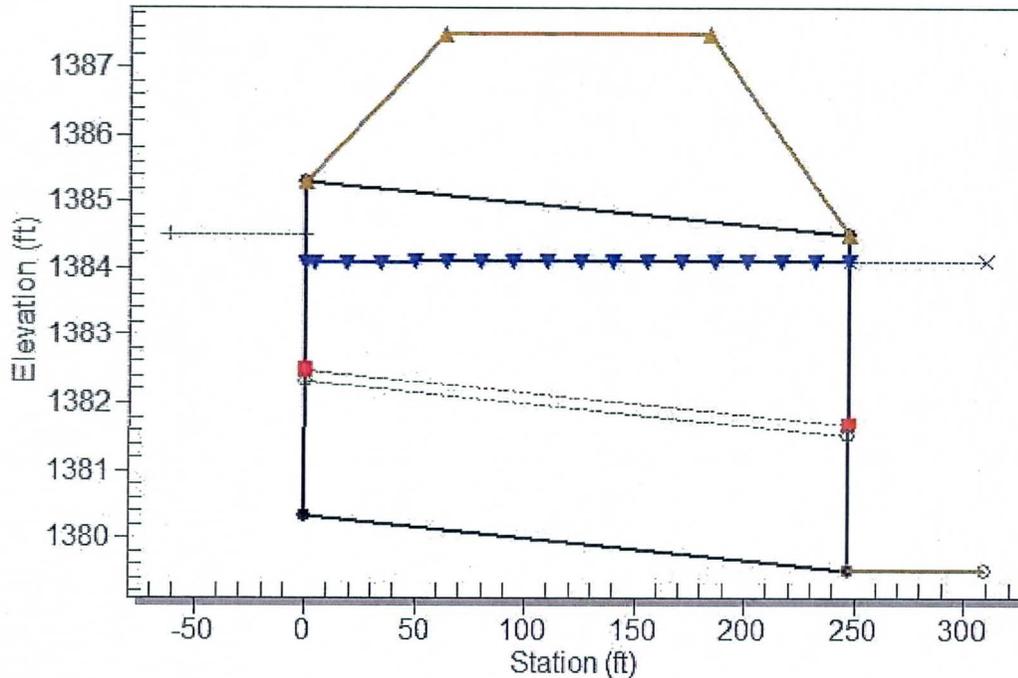
Culvert Performance Curve Plot: C6



Water Surface Profile Plot for Culvert: C6

Crossing - Culvert C6, Design Discharge - 542.0 cfs

Culvert - C6, Culvert Discharge - 542.0 cfs



Site Data - C6

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft

Inlet Elevation: 1380.31 ft

Outlet Station: 247.00 ft

Outlet Elevation: 1379.51 ft

Number of Barrels: 3

Culvert Data Summary - C6

Barrel Shape: Concrete Box

Barrel Span: 10.00 ft

Barrel Rise: 5.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: 1:1 Bevel (45° flare) Wingwall

Inlet Depression: NONE

Table 3 - Downstream Channel Rating Curve (Crossing: Culvert C6)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
100.00	1384.10	4.59
150.00	1384.10	4.59
200.00	1384.10	4.59
250.00	1384.10	4.59
300.00	1384.10	4.59
350.00	1384.10	4.59
400.00	1384.10	4.59
450.00	1384.10	4.59
500.00	1384.10	4.59
542.00	1384.10	4.59
600.00	1384.10	4.59

Tailwater Channel Data - Culvert C6

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 1384.10 ft

Roadway Data for Crossing: Culvert C6

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 40.00 ft

Crest Elevation: 1387.50 ft

Roadway Surface: Paved

Roadway Top Width: 120.00 ft

Pecos Channel - Pecos Outfall at Ellsworth (earthen w/ riprap)

Results

Critical Depth	1.71	ft
Critical Slope	0.01467	ft/ft
Velocity	3.57	ft/s
Velocity Head	0.20	ft
Specific Energy	3.28	ft
Froude Number	0.39	
Flow Type	Subcritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

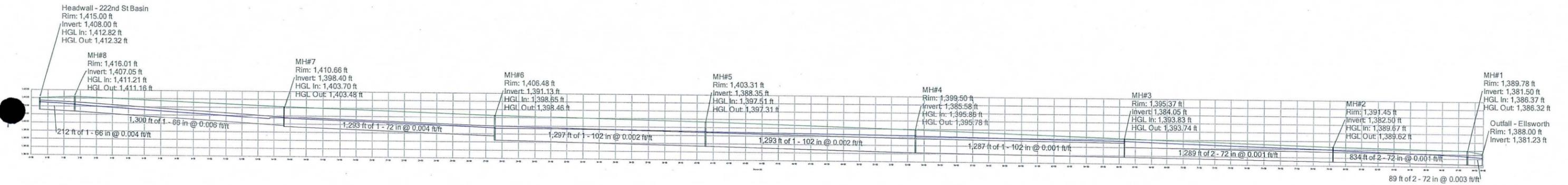
GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	3.08	ft
Critical Depth	1.71	ft
Channel Slope	0.0019	ft/ft
Critical Slope	0.01467	ft/ft

Normal depth in proposed storm drain outfall channel is less than headwater at Ellsworth culvert, so it was not used as the starting tailwater for the storm drain design.

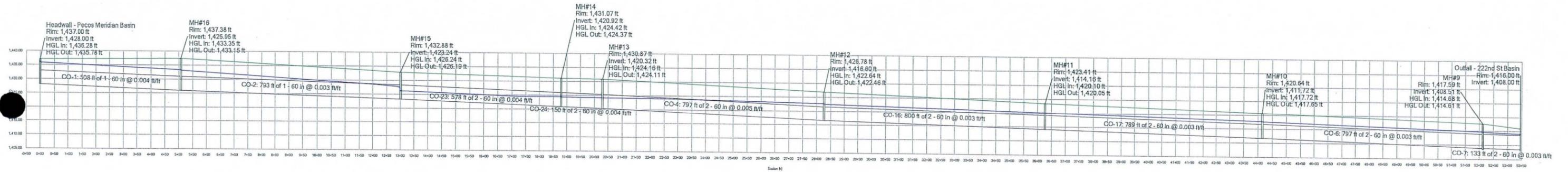
Profile Report

Engineering Profile - 222nd to Outfall Channel (DCR Drainage System.stsw)



Profile Report

Engineering Profile - Meridian to 222nd (DCR Drainage System.stsw)



FlexTable: Conduit Table

Label	Start Node	Stop Node	Diameter (in)	Length (Unified) (ft)	Total Flow (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Invert (U/S) (ft)	Invert (D/S) (ft)	Manning's n	Slope (ft/ft)	Velocity (ft/s)	Froude Number (Normal)
CO-1	Headwall - Pecos Meridian Basin	MH#16	60	508	180.00	1,435.78	1,433.35	1,428.00	1,425.95	0.013	0.004	9.17	0.723
CO-2	MH#16	MH#15	60	793	214.00	1,433.15	1,427.40	1,425.95	1,423.24	0.013	0.003	10.90	0.859
CO-23	MH#15	MH#14	60	578	214.00	1,426.19	1,424.42	1,423.24	1,420.92	0.013	0.004	8.94	0.430
CO-4	MH#13	MH#12	60	797	249.00	1,424.11	1,422.64	1,420.32	1,416.60	0.013	0.005	9.80	0.500
CO-16	MH#12	MH#11	60	800	283.00	1,422.46	1,420.10	1,416.60	1,414.16	0.013	0.003	7.21	0.568
CO-6	MH#10	MH#9	60	797	318.00	1,417.65	1,414.68	1,411.72	1,408.93	0.013	0.003	8.10	0.638
CO-7	MH#9	Outfall - 222nd St Basin	60	133	352.00	1,414.61	1,414.00	1,408.93	1,408.60	0.013	0.003	8.96	0.707
CO-8	Headwall - 222nd St Basin	MH#8	66	212	216.00	1,412.32	1,411.21	1,408.00	1,407.05	0.013	0.004	10.77	0.901
CO-25	MH#8	MH#7	66	1,300	216.00	1,411.16	1,403.70	1,407.05	1,398.90	0.013	0.006	12.47	1.194
CO-26	MH#7	MH#6	72	1,293	264.00	1,403.48	1,398.65	1,398.40	1,393.63	0.013	0.004	10.35	0.752
CO-11	MH#6	MH#5	102	1,297	311.00	1,398.46	1,397.51	1,391.13	1,388.35	0.013	0.002	9.23	0.813
CO-12	MH#5	MH#4	102	1,293	359.00	1,397.31	1,395.86	1,388.35	1,385.58	0.013	0.002	6.33	0.784
CO-13	MH#4	MH#3	102	1,287	417.00	1,395.78	1,393.83	1,385.58	1,384.05	0.013	0.001	7.35	0.444
CO-14	MH#3	MH#2	72	1,289	476.00	1,393.74	1,389.67	1,384.05	1,382.50	0.013	0.001	8.42	0.606
CO-15	MH#2	MH#1	72	834	505.00	1,389.62	1,386.37	1,382.50	1,381.50	0.013	0.001	8.93	0.643
CO-17	MH#11	MH#10	60	789	283.00	1,420.05	1,417.72	1,414.16	1,411.72	0.013	0.003	7.21	0.568
CO-20	MH#1	Outfall - Ellsworth	72	89	505.00	1,386.32	1,385.58	1,381.50	1,381.23	0.013	0.003	8.93	0.643
CO-24	MH#14	MH#13	60	150	249.00	1,424.37	1,424.16	1,420.92	1,420.32	0.013	0.004	9.22	0.500

FlexTable: Manhole Table

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Is Flooded?	Absolute Headloss (ft)
Headwall - 222nd St Basin	1,415.00	1,408.00	1,412.82	1,412.32	False	0.50
Headwall - Pecos Meridian Basin	1,437.00	1,428.00	1,436.28	1,435.78	False	0.50
MH#1	1,389.78	1,381.50	1,386.37	1,386.32	False	0.05
MH#2	1,391.45	1,382.50	1,389.67	1,389.62	False	0.05
MH#3	1,395.37	1,384.05	1,393.83	1,393.74	False	0.09
MH#4	1,399.50	1,385.58	1,395.86	1,395.78	False	0.08
MH#5	1,403.31	1,388.35	1,397.51	1,397.31	False	0.20
MH#6	1,406.48	1,391.13	1,398.65	1,398.46	False	0.19
MH#7	1,410.66	1,398.40	1,403.70	1,403.48	False	0.22
MH#8	1,416.01	1,407.05	1,411.21	1,411.16	False	0.05
MH#9	1,417.59	1,408.51	1,414.68	1,414.61	False	0.07
MH#10	1,420.64	1,411.72	1,417.72	1,417.65	False	0.07
MH#11	1,423.41	1,414.16	1,420.10	1,420.05	False	0.05
MH#12	1,426.78	1,416.60	1,422.64	1,422.46	False	0.18
MH#13	1,430.87	1,420.32	1,424.16	1,424.11	False	0.05
MH#14	1,431.07	1,420.92	1,424.42	1,424.37	False	0.05
MH#15	1,432.88	1,423.24	1,426.24	1,426.19	False	0.05
MH#16	1,437.38	1,425.95	1,433.35	1,433.15	False	0.20

Project *Pecos Road Basin and Channel DCR*
 Subject *Storm drain flows*
 Designed by **MAW** Date 11/3/2014 KH Project No. 091131024
 Checked by **LSM** Date 12/30/2014 District Ref. No. FCD2014C001-1

Objective: To prorate the flows for storm drain sizing using contributing drainage area

Calculate Prorated Flow

Location of HEC-1 Flow Change	HEC-1 ID	Storm Drain Flow ^a [cfs]	Overland Flow ^b [cfs]	Number of Quarter Mile Segments	Incremental Overland Flow ^c [cfs]
Discharge from Pecos/Meridian Basin	DETPB	180	--	--	--
222nd Street	CPE24B	352	172	5	34
Discharge from Pecos/222nd Street Basin	DET222	216	--	--	--
Crismon Road	CPE28B	359	143	3	48
Ellsworth Road	CPE31A	534	175	3	58

Notes:

- ^a Flow from HEC-1 ID that indicates the total flow in the storm drain at the HEC-1 flow change location.
- ^b Calculated by subtracting the current storm drain flow from the upstream storm drain flow.
- ^c Calculated by prorating the overland flow for each quarter mile segment of the HEC-1 flow change location.

Calculate Flow for Each Quarter Mile

Location of Storm Drain Flow Change	Upstream Storm Drain Flow [cfs]	Incremental Overland Flow [cfs]	Total Storm Drain flow [cfs]
Discharge from Pecos/Meridian Basin	180	--	180
1/4 mile west of Meridian Road	180	34	214
Mountain Road	214	34	249
1/4 mile west of Mountain Road	249	34	283
Signal Butte Road	283	34	318
222nd Street	318	34	352
Discharge from Pecos/222nd Street Basin	216	--	216
1/4 mile west of 222nd Street	216	48	264
1/4 east of Crismon Road	264	48	311
Crismon Road	311	48	359
1/4 mile west of Crismon Road	359	58	417
1/2 mile west of Crismon Road	417	58	476
1/4 east of Ellsworth Road	476	29	505
Ellsworth Road	505	29	534

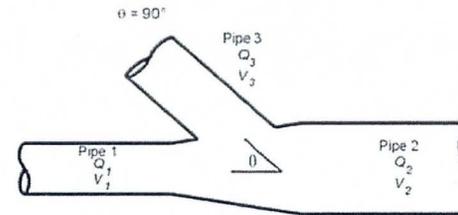
Project *Pecos Road Basin and Channel DCR*
 Subject *Junction Structure Losses*

Designed by **NAS**
 Checked by **LSM**

Date 1/5/2015 Job No. 091131024
 Date 1/6/2015 Client Ref. No. FCD2014C001-1

Objective: To determine the losses for junction structures throughout the Pecos Road pipe network per the Flood Control District guidelines

$$\frac{2(Q_2V_2 - Q_1V_1 - Q_3V_3\cos\theta)}{(A_1 + A_2)g} + V_1^2/2g - V_2^2/2g = h_j \quad (4.10b)$$



Junction ID	Pipe 1				Pipe 2				Pipe 3		h _j **
	Size	# Barrels	Flow	Velocity	Size	# Barrels	Flow	Velocity	Flow	Velocity*	
[-]	[in]	[-]	[cfs]	[ft/s]	[in]	[-]	[cfs]	[ft/s]	[cfs]	[ft/s]	[ft]
MH#1	72	2	513	9.07	72	2	513	9.07	-	9.07	0.05
MH#2	72	2	483	8.54	72	2	513	9.07	30.00	8.54	0.05
MH#3	72	2	425	7.52	72	2	483	8.54	58.00	7.52	0.09
MH#4	72	2	366	8.32	72	2	425	7.52	59.00	8.32	0.09
MH#5	60	2	315	9.03	72	2	366	8.32	51.00	9.03	0.11
MH#6	60	2	264	7.87	60	2	315	9.03	51.00	7.87	0.08
MH#7	60	2	264	6.72	60	2	264	7.87	-	6.72	0.05
MH#8	54	2	213	8.85	60	2	264	6.72	51.00	8.85	0.14
MH#9	54	2	213	6.70	54	2	213	8.85	-	6.70	0.05
MH#10	48	2	213	8.48	54	2	213	6.70	-	8.48	0.05
MH#11	60	2	320	8.15	60	2	355	8.48	35.00	8.15	0.07
MH#12	60	2	285	7.26	60	2	320	8.15	35.00	7.26	0.07
MH#13	60	2	285	7.26	60	2	285	7.26	-	7.26	0.05
MH#14	60	2	249	9.80	60	2	285	7.26	36.00	9.80	0.18
MH#15	60	2	214	8.93	60	2	249	9.80	35.00	8.93	(0.01)
MH#16	60	2	214	8.94	60	2	214	8.93	-	8.94	0.05
MH#17	60	1	214	10.90	60	2	214	8.94	-	10.90	0.05
MH#18	60	1	179	9.12	60	1	214	10.90	35.00	9.12	0.20

* Pipe 3 velocity was assumed to be the same as Pipe 1
 ** Equation for h_j assumed θ = 45 degrees, g = 32.2 ft/s/s

Kimley»Horn

Project: *Pecos Road DCR*

Subject: **Opinion of Probable Cost for Recommended Alternative**

Designed by: **NAS**

Date: 1/5/2014

KHA Project No: 091131024

Checked by: **ZRS**

Date: 1/8/2014

District Project No: 2014C001-1

Recommended Alternative

MAG Item Number	Description	Qty	Unit	Unit Price	Cost
Phase 1 Construction Items					
215.01100	Channel Excavation - Meridian North Channel	43,231	CY	\$ 6	\$ 259,400
215.01510	Earthwork for Retention Basins - Pecos/Meridian	370,874	CY	\$ 6	\$ 2,225,300
525.03217	Reinforced Concrete Channel, 6" Thick	4,041	CY	\$ 300	\$ 1,212,300
	Energy Dissipation Structure	1	EACH	\$ 20,000	\$ 20,000
Construction Subtotal					\$ 3,717,000
Phase 1 Potential Utility Relocation					
	Gas Line Relocation	1	EACH	\$ 30,000	\$ 30,000
Potential Utility Relocation Subtotal					\$ 30,000
	Right of Way Cost	43	AC	\$ 125,000	\$ 5,375,000
	Design Cost (10% of Construction Cost)				\$ 371,700
	Construction Admin and Contingency (20% of Construction Cost)				\$ 743,400
Phase 1 Total					\$ 10,237,000
Phase 2					
215.01100	Channel Excavation - Outfall Channel at Ellsworth	3,086	CY	\$ 6	\$ 18,600
215.01510	Earthwork for Retention Basins - Pecos/222nd	77,352	CY	\$ 6	\$ 464,200
220.10300	Riprap, D50=12"	1,826	CY	\$ 85	\$ 155,300
505.10150	Catch Basin, MAG Det. 535, Type F	15	EACH	\$ 4,500	\$ 67,500
523.10166	Headwall, MAG Det. 501, Straight Type, 66" Pipe	1	EACH	\$ 3,800	\$ 3,800
523.10272	Headwall, MAG Det. 501, Straight Type, 2-72" Pipe	1	EACH	\$ 4,200	\$ 4,200
618.20424	24" RGRCP, Class IV - Area Drain Laterals	600	LF	\$ 120	\$ 72,000
618.20466	66" RGRCP, Class IV	1,512	LF	\$ 190	\$ 287,300
618.20472	72" RGRCP, Class IV	5,717	LF	\$ 200	\$ 1,143,400
618.20502	102" RGRCP, Class IV	3,877	LF	\$ 300	\$ 1,163,100
625.01260	Storm Drain Manhole, MAG Det. 521 & 522	7	EACH	\$ 5,000	\$ 35,000
	Junction Structure	2	EACH	\$ 15,000	\$ 30,000
Construction Subtotal					\$ 3,444,400
Phase 2 Potential Utility Relocation					
	Water Line Relocation - 8"	1	EACH	\$ 20,000	\$ 20,000
	Water Line Relocation - 12"	1	EACH	\$ 25,000	\$ 25,000
Potential Utility Relocation Subtotal					\$ 45,000
	Right of Way Cost	10	AC	\$ 125,000	\$ 1,250,000
	Design Cost (10% of Construction Cost)				\$ 344,440
	Construction Admin and Contingency (20% of Construction Cost)				\$ 688,880
Phase 2 Total					\$ 5,773,000

Kimley»Horn

Project: *Pecos Road DCR*

Subject: **Opinion of Probable Cost for Recommended Alternative**

Designed by: **NAS**

Date: 1/5/2014

KHA Project No: 091131024

Checked by: **ZRS**

Date: 1/8/2014

District Project No: 2014C001-1

Phase 3						
505.10150	Catch Basin, MAG Det. 535, Type F	15	EACH	\$ 4,500	\$	67,500
523.10160	Headwall, MAG Det. 501, Straight Type, 60" Pipe	1	EACH	\$ 3,500	\$	3,500
523.10260	Headwall, MAG Det. 501, Straight Type, 2-60" Pipe	1	EACH	\$ 4,000	\$	4,000
618.20424	24" RGRCP, Class IV - Area Drain Laterals	600	LF	\$ 120	\$	72,000
618.20460	60" RGRCP, Class IV	9,389	LF	\$ 180	\$	1,690,100
625.01260	Storm Drain Manhole, MAG Det. 521 & 522	5	EACH	\$ 5,000	\$	25,000
	Junction Structure	5	EACH	\$ 15,000	\$	75,000
Construction Subtotal					\$	1,937,100
Phase 3 Potential Utility Relocation						
	Gas Line Relocation	2	EACH	\$ 30,000	\$	60,000
	Water Line Relocation - 4"/6"	2	EACH	\$ 15,000	\$	30,000
	Water Line Relocation - 12"	4	EACH	\$ 25,000	\$	100,000
	Water Line Relocation - 16"	1	EACH	\$ 30,000	\$	30,000
Potential Utility Relocation Subtotal					\$	220,000
	Right of Way Cost	0	AC	\$ 125,000	\$	-
	Design Cost (10% of Construction Cost)				\$	193,710
	Construction Admin and Contingency (20% of Construction Cost)				\$	387,420
Phase 3 Total					\$	2,738,000
Phase 4						
215.01100	Channel Excavation - Meridian South Channel	85,816	CY	\$ 6	\$	514,900
525.03217	Reinforced Concrete Channel, 6" Thick	8,312	CY	\$ 300	\$	2,493,600
	Energy Dissipation Structure	1	EACH	\$ 20,000	\$	20,000
Construction Subtotal					\$	3,028,500
Phase 4 Potential Utility Relocation						
	Electric Line Relocation	1	EACH	\$ 5,000	\$	5,000
Potential Utility Relocation Subtotal					\$	5,000
	Right of Way Cost	13	AC	\$ 125,000	\$	1,625,000
	Design Cost (10% of Construction Cost)				\$	302,850
	Construction Admin and Contingency (20% of Construction Cost)				\$	605,700
Phase 4 Total					\$	5,567,000
Construction Subtotal					\$	12,127,000
Potential Utility Relocation Subtotal					\$	300,000
Right of Way Subtotal					\$	8,250,000
Design Cost Subtotal					\$	1,213,000
Construction Admin and Contingency Subtotal					\$	2,425,000
Project Total					\$	24,315,000

Notes: Construction costs were determined from ADOT Estimated Engineering Construction Cost E2C2.

Utility relocation estimates based on typical relocation costs.

Riprap quantities were determined from standard cross sections in AutoCAD

Lateral pipe quantities and catch basin quantities were determined based on future developments along Pecos Road with an allowance of 40 ft of pipe per catch basin

Appendix G. Public Meetings

- Public Meeting 1
Notes, Sign-in Sheets, Comments
- Public Meeting 2
Invitation, Sign-in Sheets

NOTES

**FLOOD CONTROL DISTRICT OF MARICOPA COUNTY
PECOS ROAD CHANNEL AND BASIN DESIGN CONCEPT REPORT**

September 18, 2014

**Stakeholder Meeting #1
12:00 – 1:30 PM**

**CMC Steel
11444 E. Germann Rd., Mesa**

The meeting notes for the aforementioned project are attached for your information and use. If you believe that these notes do not accurately reflect your understanding of the conversations that took place or if major discussions are missing, please contact Laurie Marin at (602) 906-1369 within one week of these meeting notes being issued. Thanks to all who participated in the meeting.

Attendees:

See attached Sign-in Sheets

Handouts:

The following item(s) were provided to attendees or displayed as exhibits. These items are included as attachments to the meeting notes.

- Exhibits of Alternatives 1, 2, and 3
- Meeting Action Item Sheets

Presenters:

Mike Duncan, Flood Control District of Maricopa County
Laurie Marin, Kimley-Horn
Melanie Wadsworth, Kimley-Horn
Lance Webb, City of Mesa (for Q & A)
Stephen Ganstrom, City of Mesa (for Q & A)

Notes:

Mike began the meeting with a summary of the project, the purpose and location. Laurie discussed the general hydrology of the project area, and Melanie presented the components of each alternative. The meeting was then opened up for questions and input from the attendees.



- Q1 Is it possible to get copies of the maps?
A1 The District will distribute the maps.
- Q2 What if we don't want a channel on our property?
A2 Mike handed out comment forms at this point and asked attendees to write down any comments they had and we would take them into consideration.
- Q3 Pecos Road is a didn't used to be there before, why is flow there now?
A3 There was a discussion from residents about past conditions in the area. The statement was made that now there is a problem down Williams Field Road and down 222nd that didn't used to be there.
- Q4 How long has study been underway?
A4 The study has been underway since June and should be finished in December.
- Q5 Who decides on alternatives?
A5 The Flood Control District and the City of Mesa, with input from the consultant team and the local property owners and operators.
- Q6 Who is paying for this project?
A6 FCDMC
- Q7 Isn't there a rule or law that the upstream properties have to take care of their water so it doesn't affect downstream properties?
A7 No there is no such rule.
- Q8 How big was the storm event last Monday
A8 Lance: it was a 5-10 year event on Monday

The preference is #3 from meeting attendees

Stephen explained future development – the storm drain is an advantage for retention bleed off

- Q9 What is going to be developed in the Mesa proving grounds?
A9 Mesa said haven't seen a lot, subdivisions with retail

Fuji representative indicated they are not in favor of Alternative 1, they bought the NW corner of Pecos and Mountain.

The chemical company representative indicated they are opposed to anything on the north side



Q10 Are you leaning towards the storm drain option?

A10 Lance: Mesa pushed for the storm drain from an economic development standpoint, they wanted to know if it could be done, and what would it mean for corridor.

Q11 How will the water get into the storm drain?

A11 Many (30, 40) inlets have been estimated at this point to get the water into the storm drain.

Q12 Who is taking the lead on the project?

A12 FCDMC with Mesa

Lance and Stephen explained that Mesa has this project #1 or #2 on their priority list. There is a new focus on this area due to future development. Stormwater projects have historically been unpopular in Mesa so the City rolls stormwater projects into roadway projects.

Q13 When are projects submitted for review for funding?

A13 Answer not recorded.

Q14 Is there a timeframe if everything went perfectly?

A14 Maybe 4 years, if the City does a bond maybe 2-3 years, because if the City does a bond the funding percentage would change between the District and the City.

Lance and Stephen stated that the Economic Development group has been interested in this project. It is on their radar and they know they need to get drainage under control to help push development of the area forward.

Q15 How do "they" decide which projects get selected. What is it based on?

A15 Looking at City/District funding

Prioritization list from Mesa

There are currently several projects in NE Mesa, the McDowell and Ellsworth basin, this project

Comment from attendee: Every company is wanting to grow and create jobs

Q16 How is SR-24 is a factor in the design?

A16 If we put it in before SR-24 get 40-year protection, once SR-24 is complete it will be 100-year protection. It doesn't make sense to build it bigger now because it will go to waste when SR-24 is in.



Q17 Has Pinal County funded their piece?

A17 No answer given.

Q18 Is there any interim stuff to make it any better now?

A18 The improvements will likely be built in phases – it makes best sense to do the upstream basin but then a dedicated path for outflows is needed.

Q19 I have heard talks about building up Pecos and putting viaducts in?

A19 No answer given.

Discussion about the storm on Monday

Pecos was a river

It's been worse

The tire recycling place was 6 inches from having water in the facility

Q20 Are all developments in the area a zero discharge requirement? Like TRW Fuji?, etc.

A20 Answer not recorded.

The meeting was adjourned and attendees gave a strong unanimous indication that Alternative 3 was preferred by them. Comments were collected and are included as an attachment to these notes.



Meeting Attendees

1 of 3

Date: 09/18/2014 Time: 12:00 pm Number Present: 25

Meeting Title: PECOS ROAD CHANNEL AND BASIN D.C.R. - PRESENTATION OF ALTERNATIVES

Meeting Attendees :		
Name	Organization	Contact Phone/Email:
1. MIKE DUNCAN	F.C.D.M.C.	602-506-4732
2. Travis Watkins	MATHESON GAS	480-492-1912
3. Jerry Wright	MATHESON GAS	602-317-4310
4. Mike Taylor	CMC	480-396-7261
5. DAWN HELMS	CMC	480 987 3006
6. Charles Miner	CMC	480-399-3653
7. Don Mock	Mesa Wash Ranch	480-988-2521
8. Alan Prosen	CMC	480-280-5826
9. Abel Hernandez	CMC	214-876-9985
10. Georganna Lazear	Fuji	480-703-0532 (cell)
11. Rudy Komoros	TRW	480 722 6215
12. Monte De	CMC	480-286-6045
13. John Alston	Signa Butte Gardens	480-833-4488
14. PAT JOHN	CMC	480-396-7120
15. Rod Eudovs	Wilson Const	480-212-3238
16.		

NE Cor.
Galveston/
Mountain St.
1/2 acre



Meeting Attendees

2 of 3

Date: 09/18/2014 Time: 12:00 pm Number Present: _____

Meeting Title: PECOS ROAD CHANNEL AND BASIN D.C.R. - PRESENTATION OF ALTERNATIVES

Meeting Attendees :		
Name	Organization	Contact Phone/Email:
1. MIKE MAGRUDER	TKW	480 722 4174 MICHAEL.MAGRUDER@TKW.COM
2. KEN SMITH	SIGNAL BUTTE GRADING	KEN@SMITHSTONZONZON.COM 480 833 4488
3. Steve Tucker	Tucker Prop.	480-620-8683
4. Patricia Tretick	Waegel; ^{ELSA} ^{TRICK} ²⁰¹²	602-369-9222
5. Blythe Tretick	Estate	btretick@gmail.com
6. Stephen GRANZ/son	com	stephwbz@mesaaz.gov
7. Lance Webb	com	lance.webb@mesaaz.gov
8. Melanie Wedsworth	Kimley-Horn	melanie.wedsworth@kimley-horn.com
9. Laurie Marin	lll	laurie.marin@kimley-horn.com
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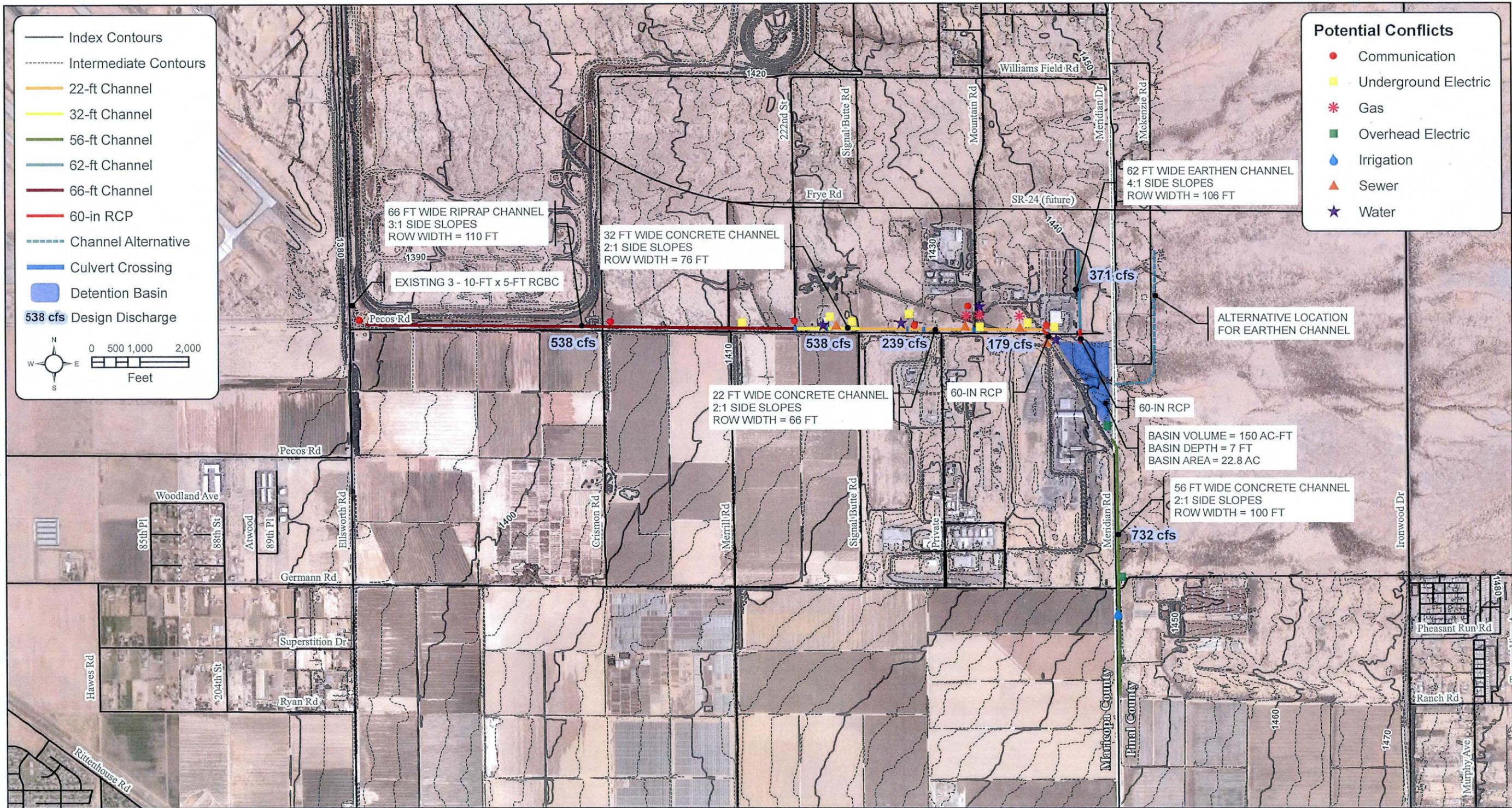
Meeting Attendees

3 of 3

Date: 09/18/2014 Time: 12:00 pm Number Present: _____

Meeting Title: PECOS ROAD CHANNEL AND BASIN D.C.R. - PRESENTATION OF ALTERNATIVES

Meeting Attendees :		
Name	Organization	Contact Phone/Email:
1. <i>Reece Bawden</i>	<i>AMERICAN PACIFIC</i>	<i>480-650-1441</i>
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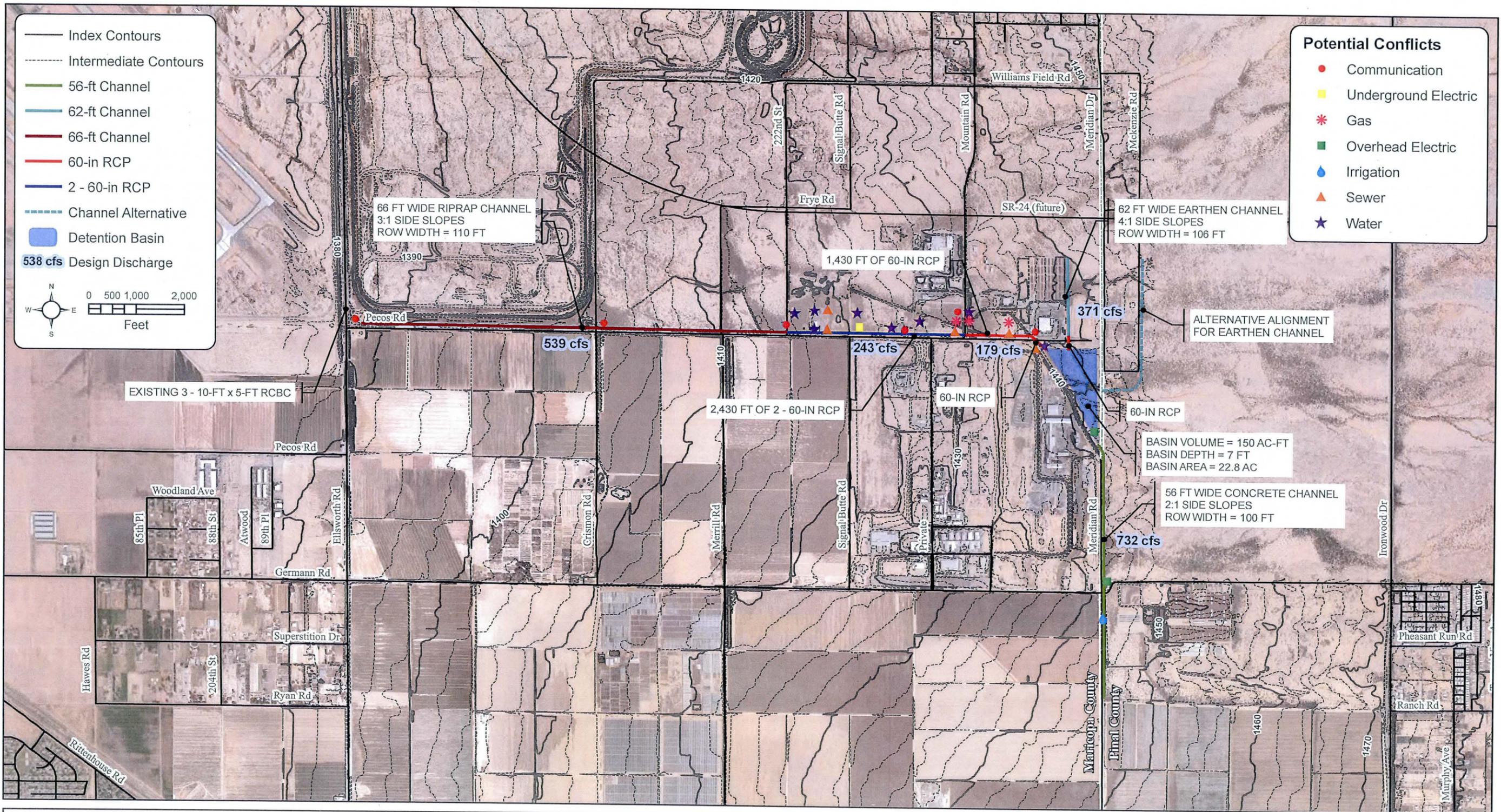


Kimley»Horn

Pecos Road Channel and
Basin Design Concept Report

Flood Control District of Maricopa County
City of Mesa

Alternative 1

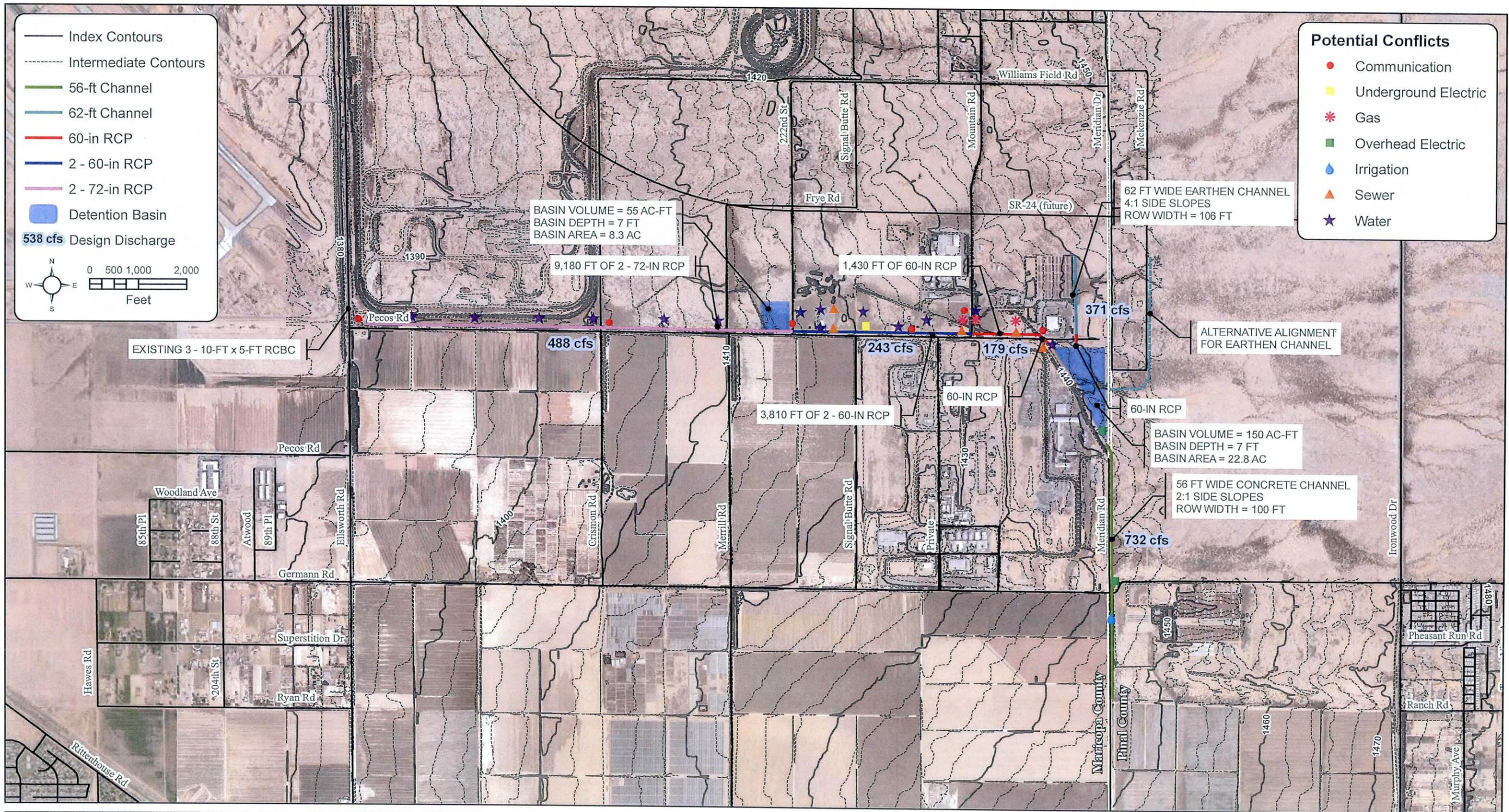


Kimley»Horn

Pecos Road Channel and Basin Design Concept Report

Flood Control District of Maricopa County
City of Mesa

Alternative 2



Kimley»Horn

Pecos Road Channel and Basin Design Concept Report

Flood Control District of Maricopa County
City of Mesa

Alternative 3



Meeting Action Items

10f3

Action Items		
Question/Follow-up	Who	By When
I AM FOR ALTERNATIVE 3!!!	KEN SMITH 480 833 4488 KENSMITHALFONLAW.COM	
"	John Alston 480-833-4198	
Want to see full explanation of All options w/ photos on your site	T Watkins 480-492-1912	
Alternative #3! Please post all info on your website	Georganna Lopez 480-703-0532 FEM	
Alternative #3!!	DAWN HOPKINS CELL OF AMERICA 480 987-3006	
ALT. #3	Red Eudais Wilson Const. 480-212-3238	
Alt #3 But move retention area off 22 nd St to West	Steve Tucker 480 620 8683	

Reviewed BY: (District PM) Maryland Duncan
 Reviewed BY: (Organization) Jane Webb
 CITY OF MESA

Date: 9-22-14
 Date: 9/22/14



Meeting Action Items

2 of 3

Action Items		
Question/Follow-up	Who	By When
We are not in favor of option 1 or 2. Negative impact to our usable property for development. Takes too much out of property if a concrete canal put in.	Gene Tokroaks 480-9829100 ext 102	MGC Pure Chemicals America Pecos + Mountain
Strongly against retention area on NW corner of 222 + Pecos. Takes too much of our property.	Tucker Prop 480 620 8683 8683	
Ditto above objection to retention adjacent to 222.	Naegoli Trust property on east side of 222	602 369-9222

Reviewed BY: (District PM) Michael Duncan

Date: 9-22-14

Reviewed BY: (Organization) James Webb
CITY OF MESA

Date: 9/22/14



Meeting Action Items

3 of 3

Action Items		
Question/Follow-up	Who	By When
WE ARE IN FAVOR OF OPTION 3	AMERICAN PACIFIC HOLDINGS	

[Handwritten signature]

Reviewed BY: (District PM) Michael Duran

Date: 9-22-14

Reviewed BY: (Organization) Jane Webb
CITY OF MESA

Date: 09/22/14



Flood Control District of Maricopa County

www.fcd.maricopa.gov

2801 West Durango Street
Phoenix, Arizona 85009
Phone: 602-506-1501
Fax: 602-506-4601

PROJECT/STUDY: *Pecos Road Corridor - Design Concept Report*

MEETING ANNOUNCEMENT: *Presentation of Preliminary (15%) Plans*

The Flood Control District of Maricopa County and the City of Mesa, along with Kimley-Horn and Associates, Inc., have developed preliminary plans for drainage improvements to address flooding issues along the three-mile segment of Pecos Road, from Ellsworth Road to the Meridian Road alignment.

The majority of the drainage improvements comprise underground storm drains along Pecos Road. East of the Meridian Road alignment, the improvements include two channels to collect stormwater runoff that approaches from the east. Also, two detention basins are included in the system to attenuate the storm flows.

We invite you to attend an upcoming meeting where the concepts of the preliminary, or 15%-level, plans will be presented:

Thursday, December 18, 2014
Noon – 12:40 pm
Fujifilm Electronic Materials
6550 South Mountain Road, Mesa, AZ,

This is approx. ¼ mile north of Pecos Rd., on the west side;
at a modular building at the south end of the parking lot.

If you are unable to attend and would like to obtain related information, or have any questions, please contact:

Mike Duncan, Project Manager
Flood Control District of Maricopa County
602-506-4732
mwd@mail.maricopa.gov

The City of Mesa contact is Lance Webb, Senior Civil Engineer, 480-644-2399,
lance.webb@mesaaz.gov



Meeting Attendees

Date: 12/18/2014 Time: 12:00 pm Number Present: _____

Meeting Title: PECOS ROAD CHANNEL AND BASIN D.C.R. - PRESENTATION OF 15% PLANS

Meeting Attendees :

Name	Organization	Contact Phone/Email:
1. MIKE MAGRUDER	TRW	MICHAEL MAGRUDER @ TRW.COM
2. DAVID JARVIS	APH, LLC	602-370-5525
3. Rick Decker	Investor	602-738-2371
4. Reece Bawden	APH LLC	480-650-1441
5. Rudy Komenda	TRW	RUDY.KOMENDA@TRW.COM 480 722 6215
6. LAURIE MARIN	Kimley-Horn	laurie.marin@kimley-horn.com 480 270 2677
7. Freddie Sanchez	Matheson Tri-Gas	fsanchez@mathesontri-gas.com 928 701 2447
8. NICK STAFFORD	KIMLEY-HORN	NICK.STAFFORD@KIMLEY-HORN.COM
9. Dana McBride	Mesa PID	DANA.McBride@MesaAZ.GOV (480) 644-5520
10. Anne Micci	Fujifilm	(480) 987-7033
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Meeting Attendees

Date: 12/18/2014 Time: 12:00 pm Number Present: _____

Meeting Title: PECOS ROAD CHANNEL AND BASIN D.C.R. - PRESENTATION OF 15% PLANS

Meeting Attendees :		
Name	Organization	Contact Phone/Email:
1. Charles Minter	CMC	480-399-3653
2. NEAL STODDARD	ALA	480-299-8658
3. JAMES Coffershey	Mesa Wash Ranch	602-677-2410
4. Blythe Trotter	Bruce Naegeli	602-369-9222
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Meeting Attendees

Date: 12/18/2014 Time: 12:00 pm Number Present: _____

Meeting Title: PECOS ROAD CHANNEL AND BASIN D.C.R. - PRESENTATION OF 15% PLANS

Meeting Attendees :		
Name	Organization	Contact Phone/Email:
1. Dawn Helms	CTRM	480 987 3006 DHELMS@CTRM.COM
2. Alan Jackson	CMC	Alan Jackson @ CMC, LLC 480-780-5870
3. Gene Tokraks	MPCA	480-987-9100 ext 102 gtokraks@mgcputc.com
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Appendix H. Conceptual Plans

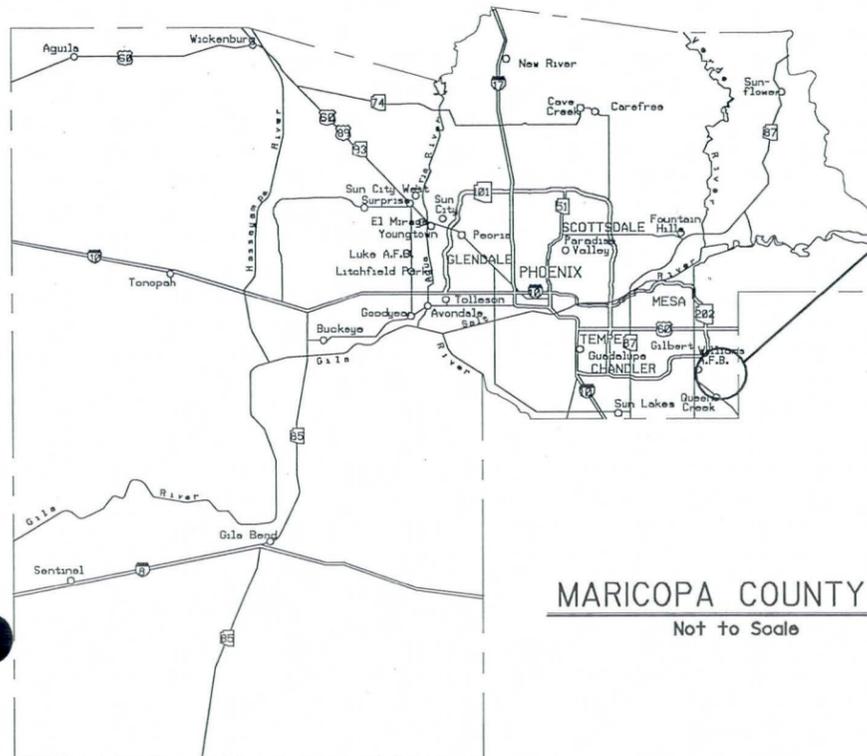
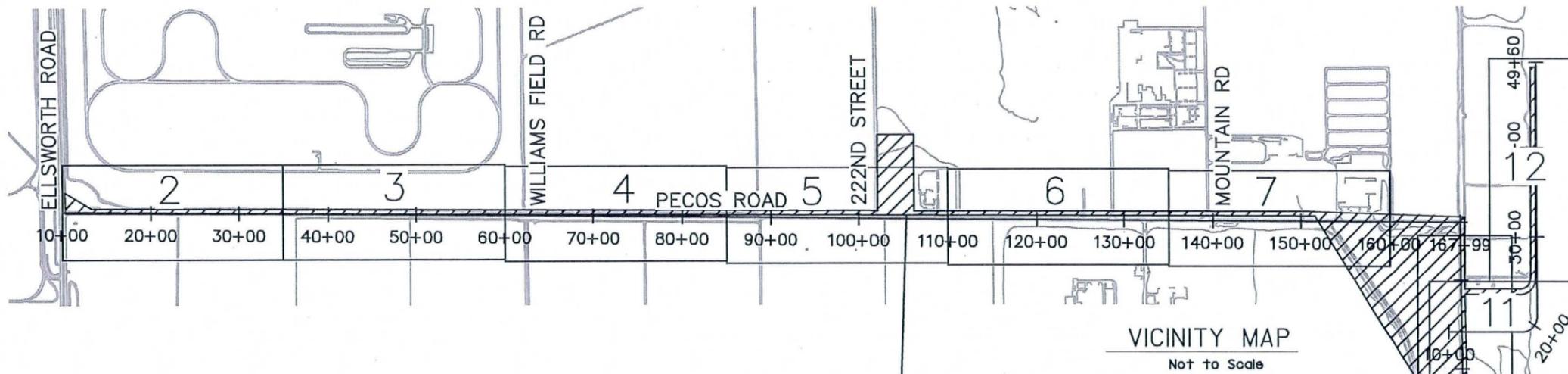


FLOOD CONTROL DISTRICT OF MARICOPA COUNTY

IN COOPERATION WITH KIMLEY-HORN
 CONCEPTUAL PLANS FOR THE CONSTRUCTION OF
 PECOS ROAD CHANNEL AND BASIN DRAINAGE IMPROVEMENTS

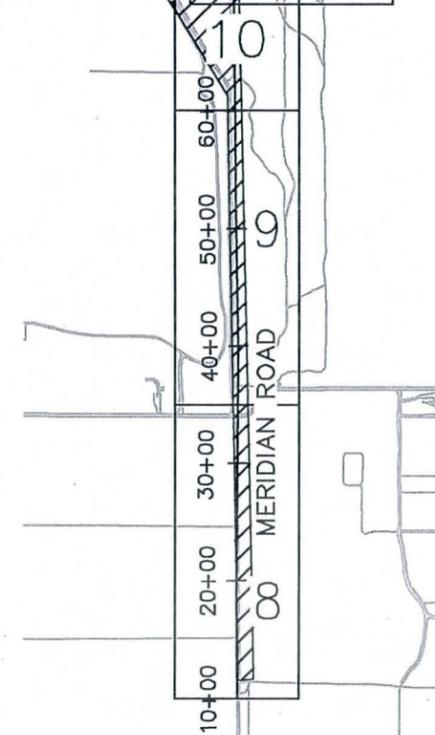
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FCD CONTRACT NO. 2014C001-1

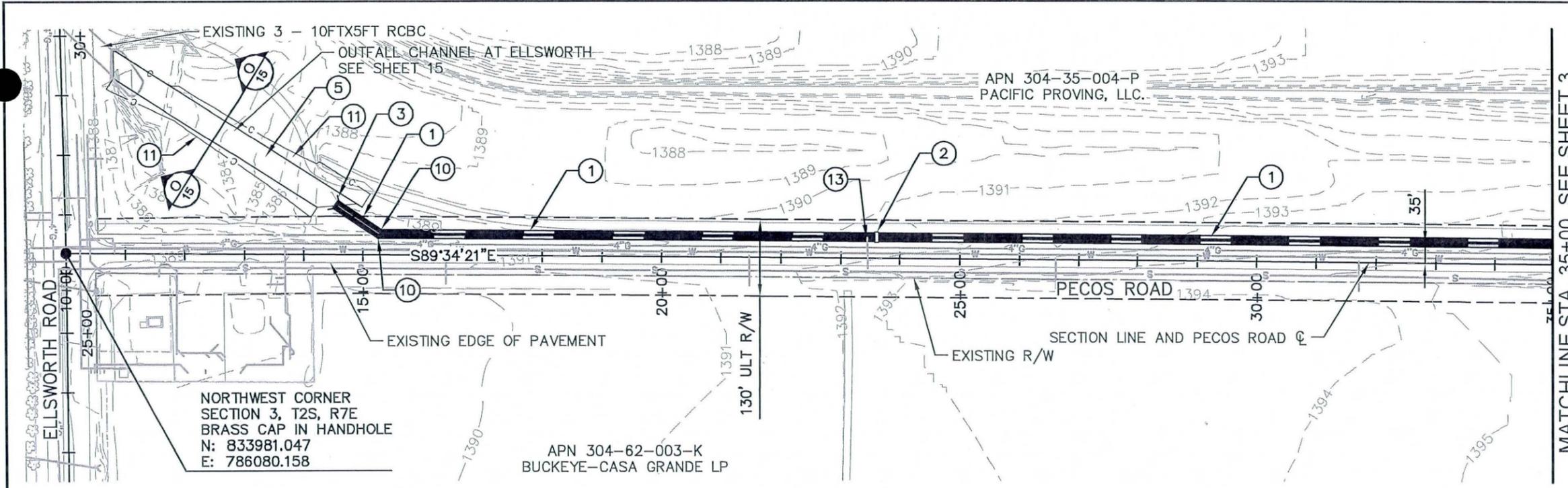


INDEX OF SHEETS

SHEET No.	SHEET TITLE
1	COVER SHEET
2-7	STORM DRAIN PLAN AND PROFILE
8-12	CHANNEL PLAN AND PROFILE
13-14	BASIN PLAN AND PROFILE
15	BASIN PROFILE AND TYPICAL CHANNEL SECTIONS



FLOOD CONTROL DISTRICT OF MARICOPA COUNTY	
ISSUE RECOMMENDED BY:	
PROJECT MANAGER	DATE
ISSUED FOR PUBLIC BIDDING BY:	
CHIEF ENGINEER & GENERAL MANAGER	DATE
BOARD OF DIRECTORS OF THE FLOOD CONTROL DISTRICT	
DENNY BARNEY - CHAIRMAN	
DISTRICT 1	DENNY BARNEY
DISTRICT 2	STEVE CHUCRI
DISTRICT 3	ANDY KUNASEK
DISTRICT 4	CLINT HICKMAN
DISTRICT 5	MARIE LOPEZ ROGERS

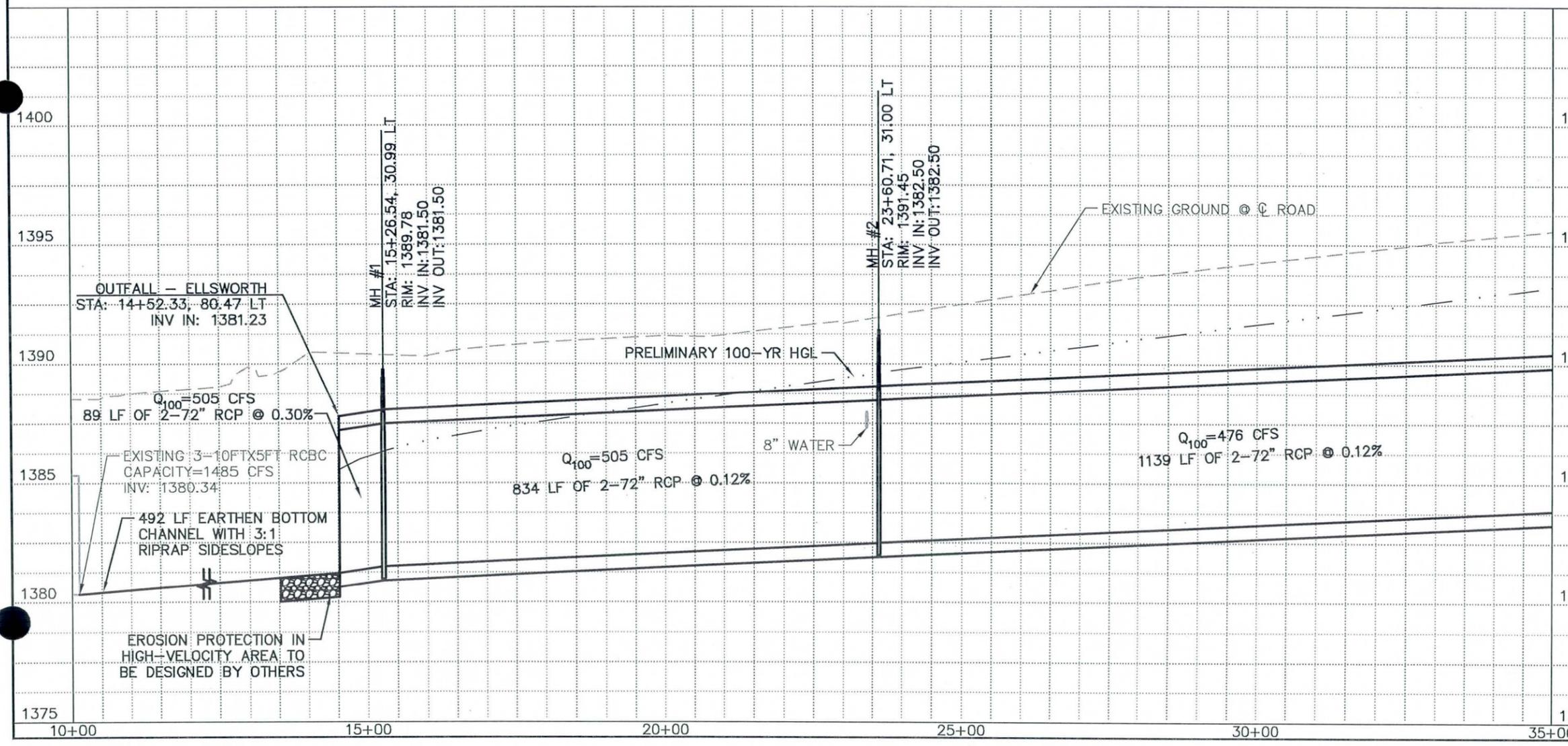


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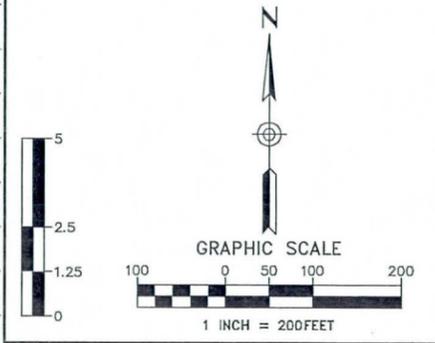
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○ CONSTRUCT ○

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①	2 - 72" RGRCP	2062	LF
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③	HEADWALL, MAG 501-3	1	EA
⑤	CHANNEL EXCAVATION	3086	CYD
⑩	MANHOLE, MAG 521&522	2	EA
⑪	RIPRAP, D ₅₀ =12"	1826	CYD
⑬	WATER LINE RELOCATION	1	EA



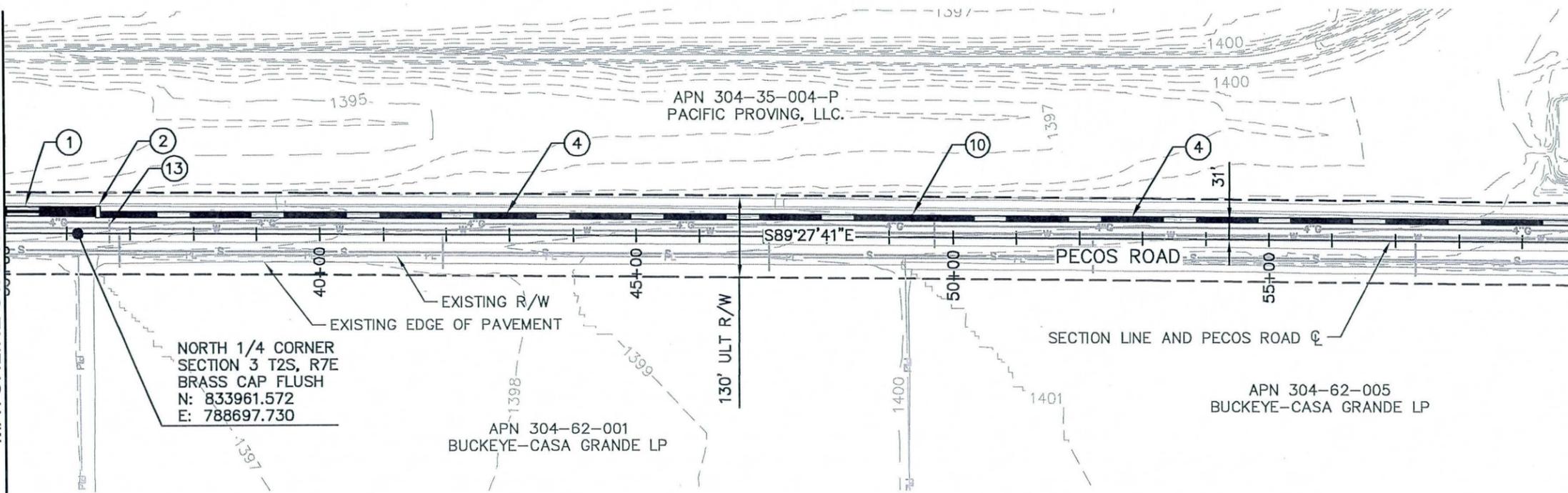
CALL THE NUMBER BEHIND THE SIGN
602-263-1100
1-800-STAKE-IT
(OUTSIDE MARICOPA COUNTY)



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	 FLOOD CONTROL DISTRICT OF MARICOPA COUNTY ENGINEERING DIVISION		
	PECOS ROAD CHANNEL AND BASIN DCR 442.03.20 FCD 2014C001-1		
		BY	DATE
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	DR: NAS		1/15
	CK: LSM		1/15
Kimley»Horn			
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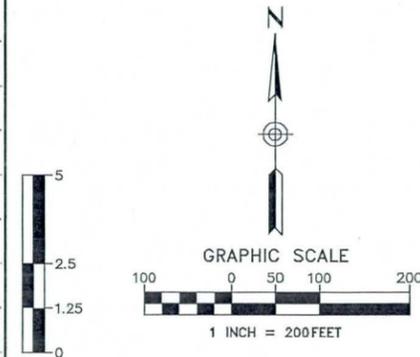
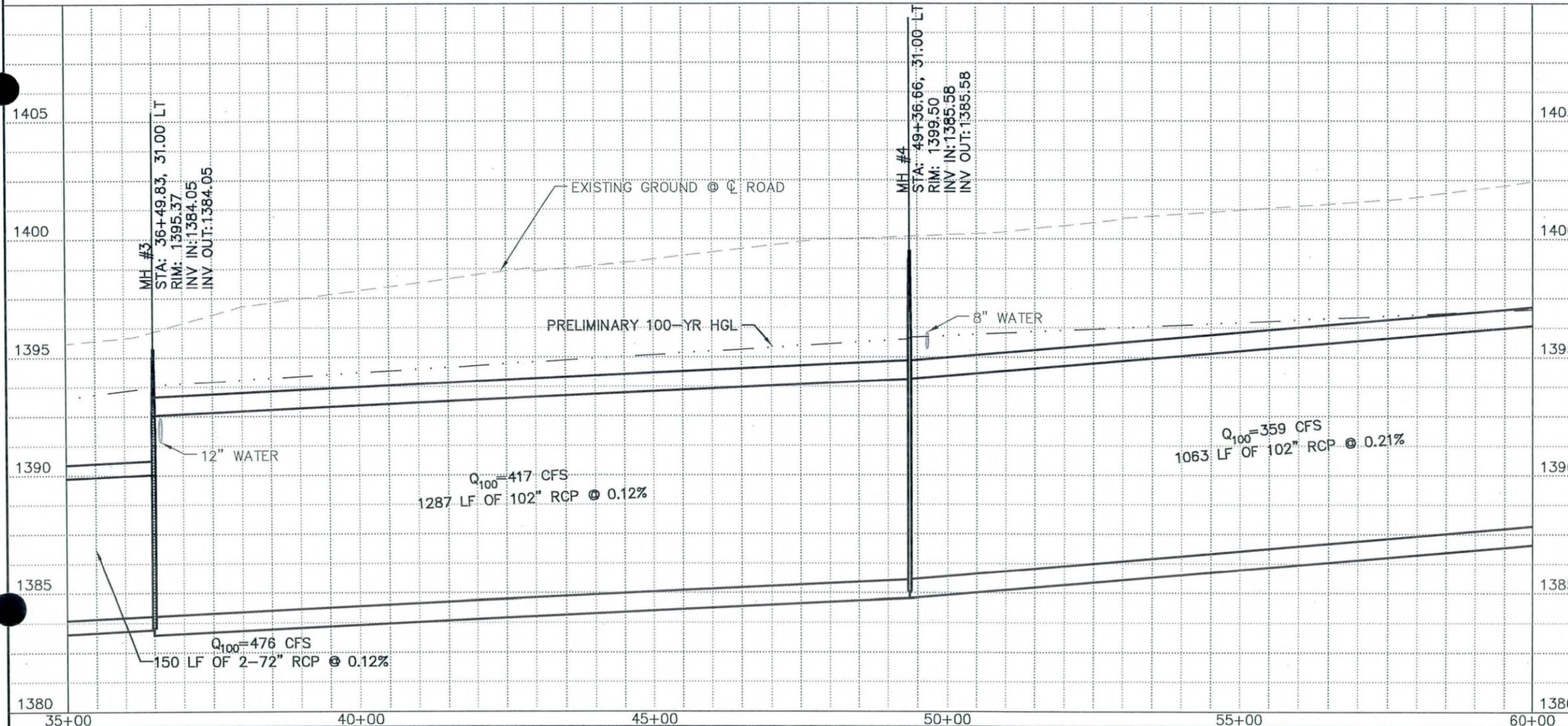
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④	102" RGRCP	2350	LF
⑩	MANHOLE, MAG 521&522	1	EA
⑬	WATER LINE RELOCATION	1	EA



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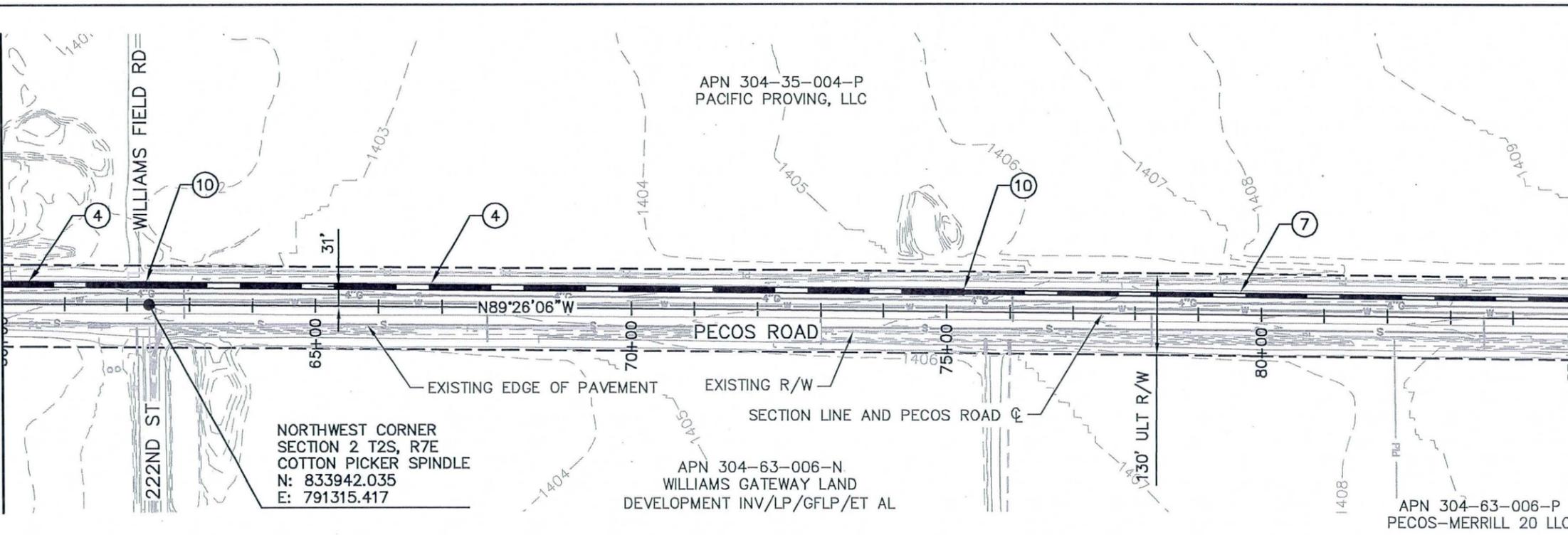
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OF MARICOPA COUNTY
ENGINEERING DIVISION
PECOS ROAD CHANNEL AND BASIN DCR
442.03.20
FCD 2014C001-1

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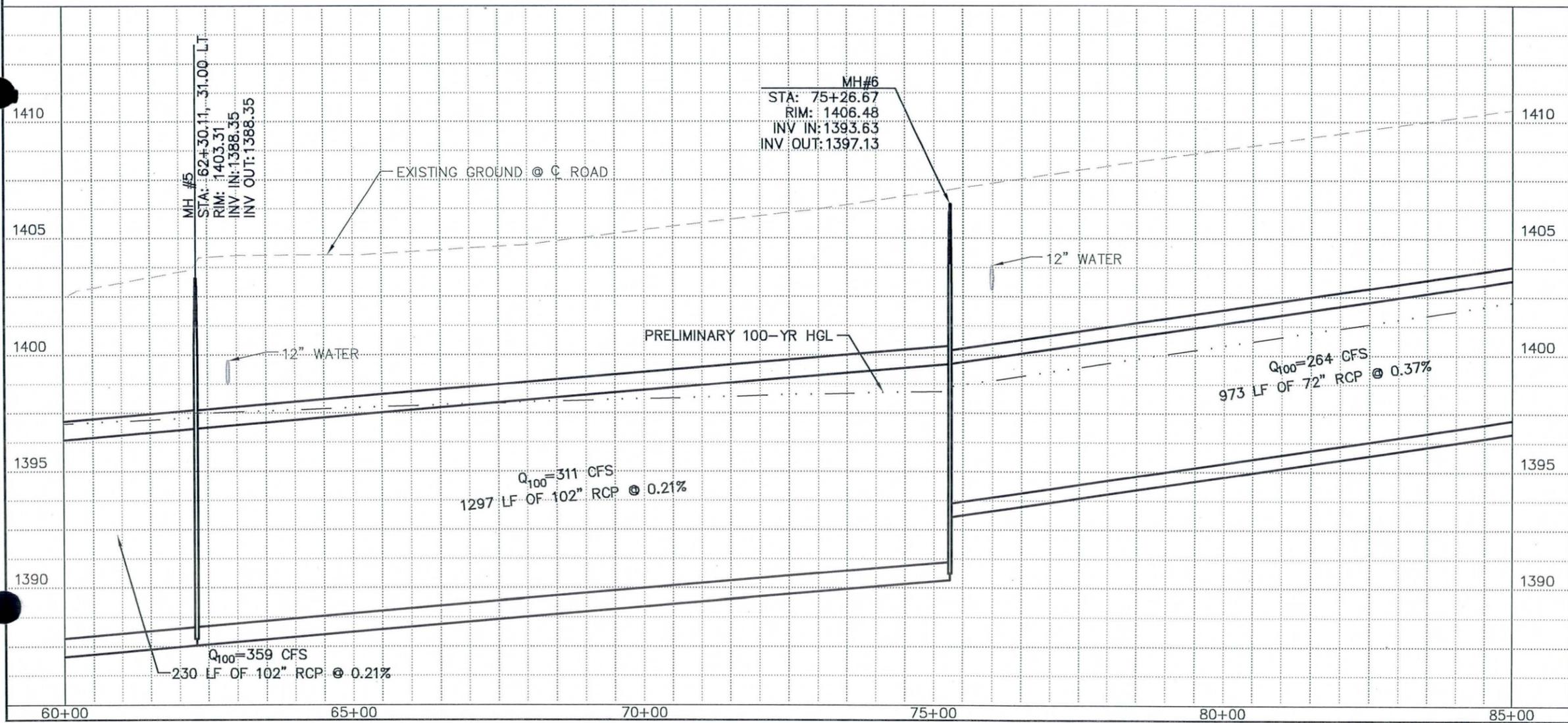
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⑦	72" RGRCP	973	LF
⑩	MANHOLE, MAG 521&522	2	EA

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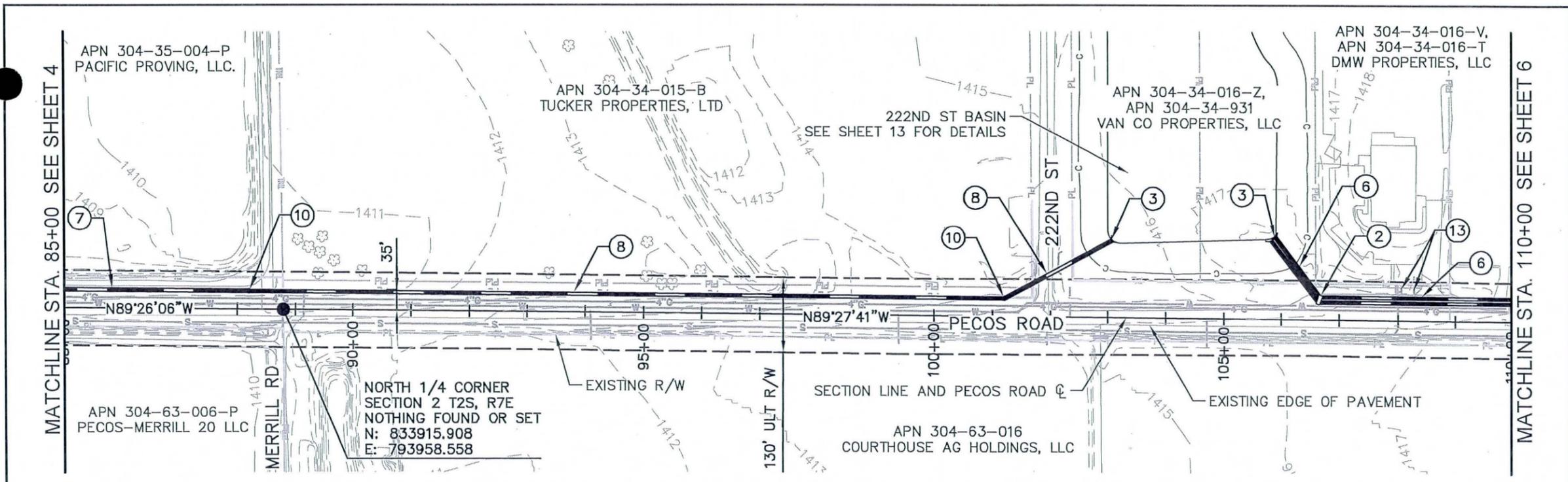
GRAPHIC SCALE

1 INCH = 200 FEET

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PECOS ROAD CHANNEL AND BASIN DCR
 442.03.20
 FCD 2014C001-1

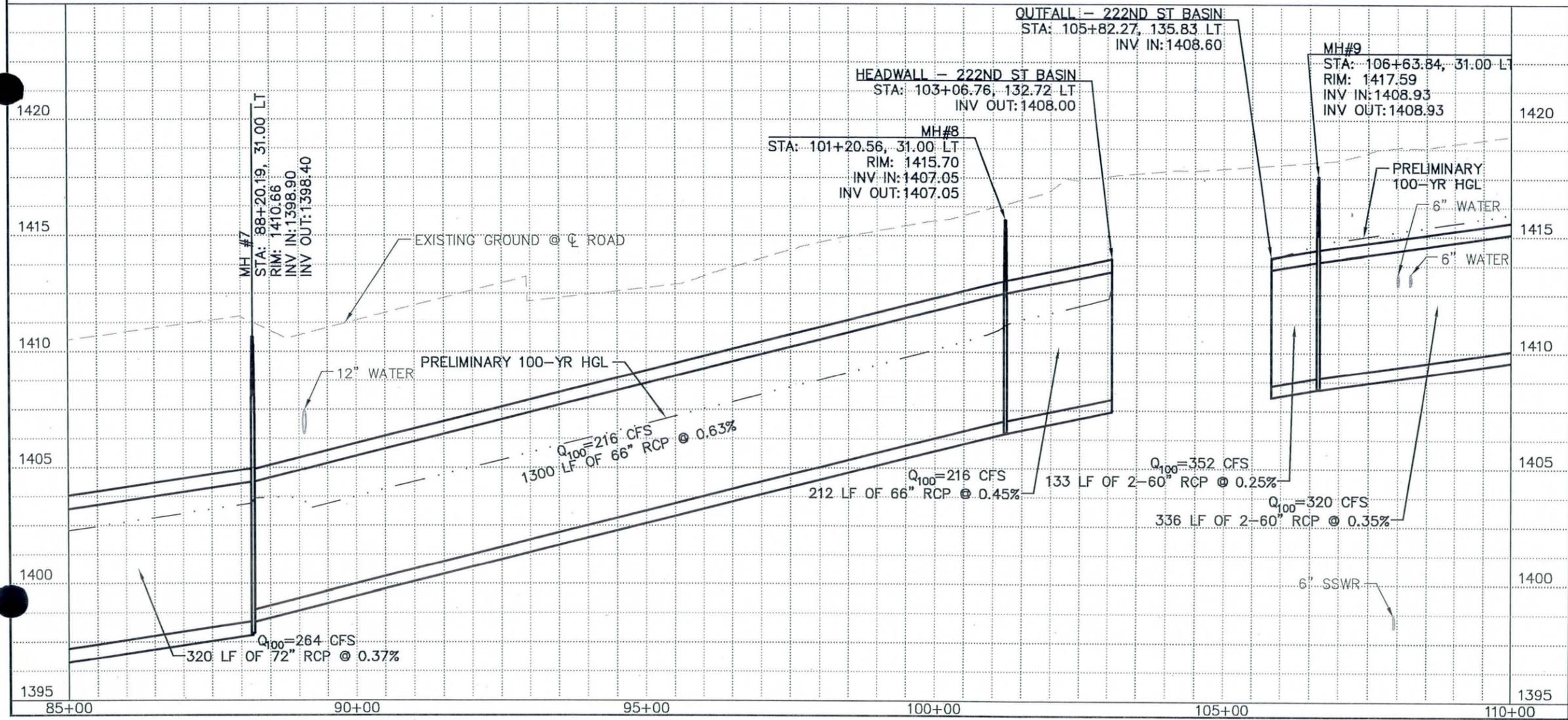
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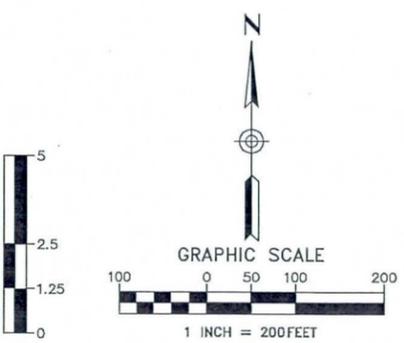
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○ CONSTRUCT ○

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③	HEADWALL, MAG 501-3	2	EA
⑥	2 - 60" RGRCP	469	LF
⑦	72" RGRCP	320	LF
⑧	66" RGRCP	1512	LF
⑩	MANHOLE, MAG 521&522	2	EA
⑬	WATER LINE RELOCATION	2	EA



CALL FOR NUMBER DATA BEFORE YOU BUY
602-263-1100
1-800-STAKE-IT
(COURTESY MARICOPA COUNTY)



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FLOOD CONTROL DISTRICT
OF MARICOPA COUNTY
ENGINEERING DIVISION

PECOS ROAD CHANNEL AND BASIN DCR
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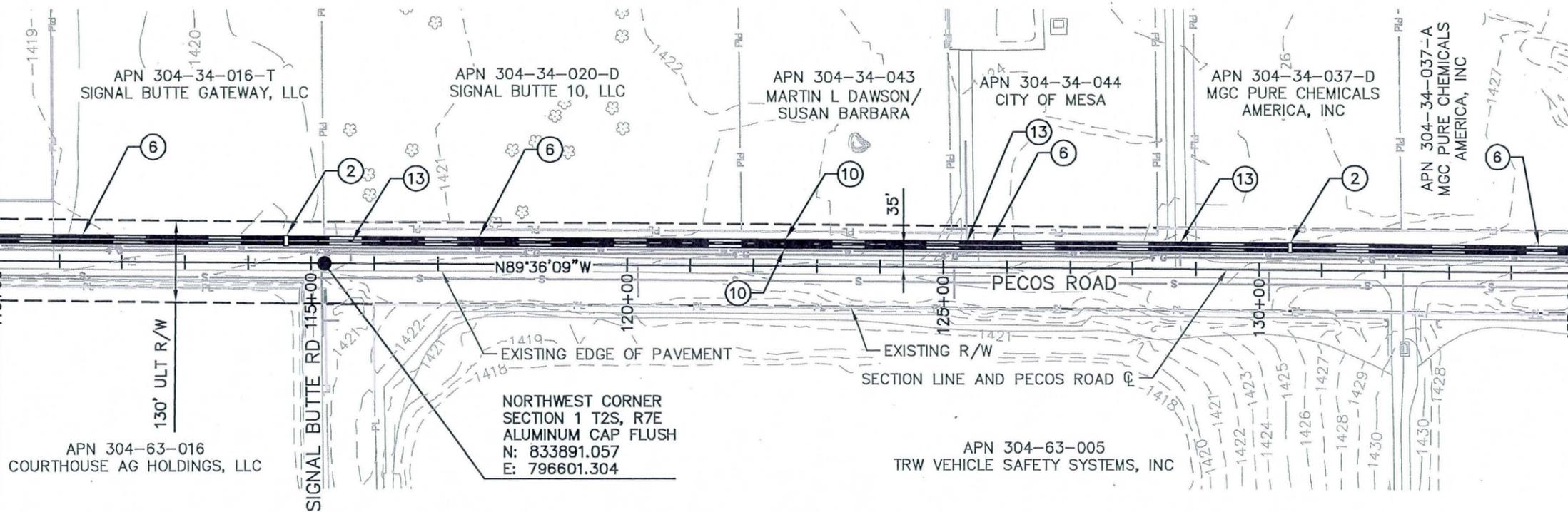
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Kimley»Horn

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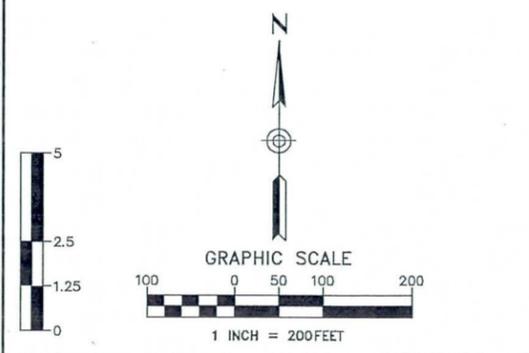
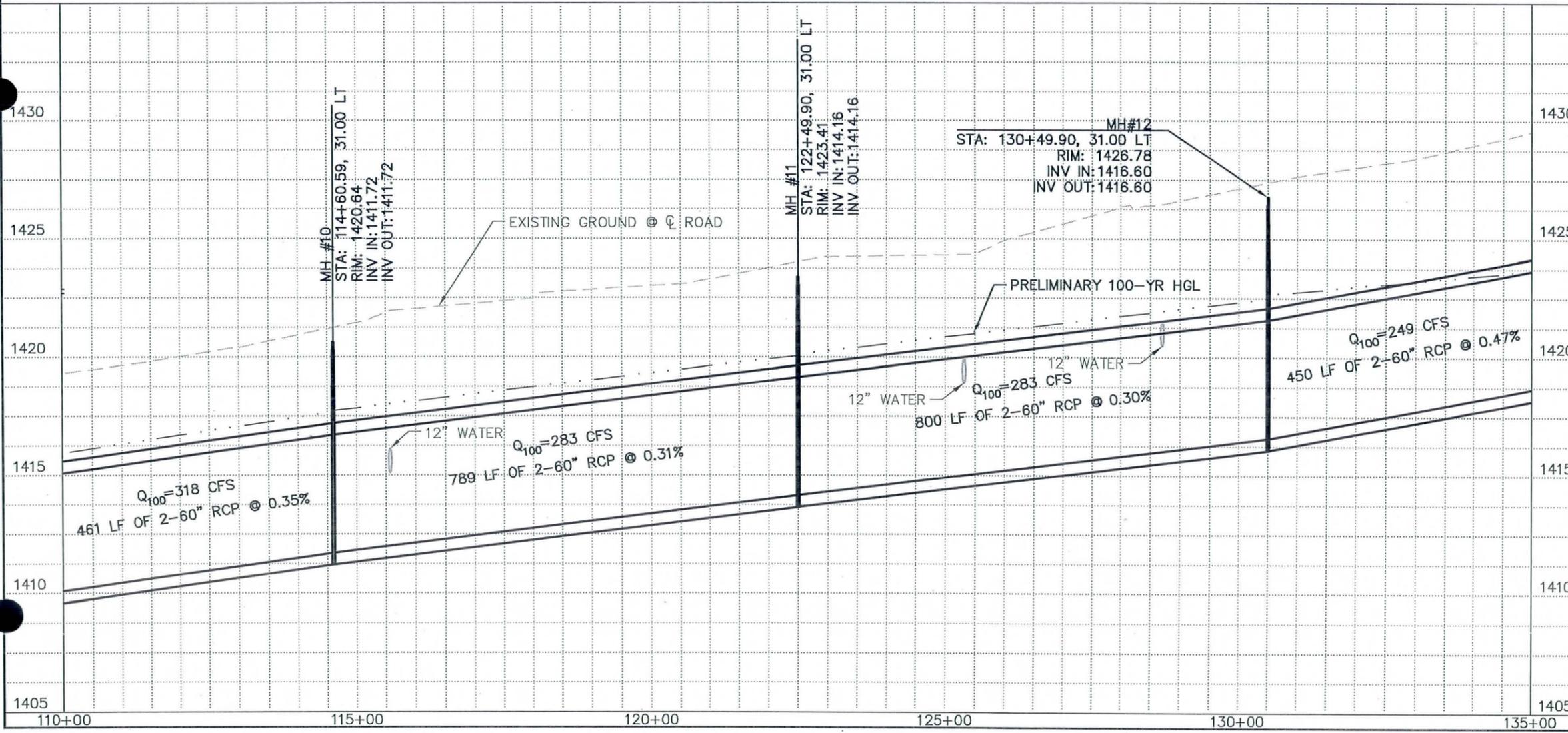
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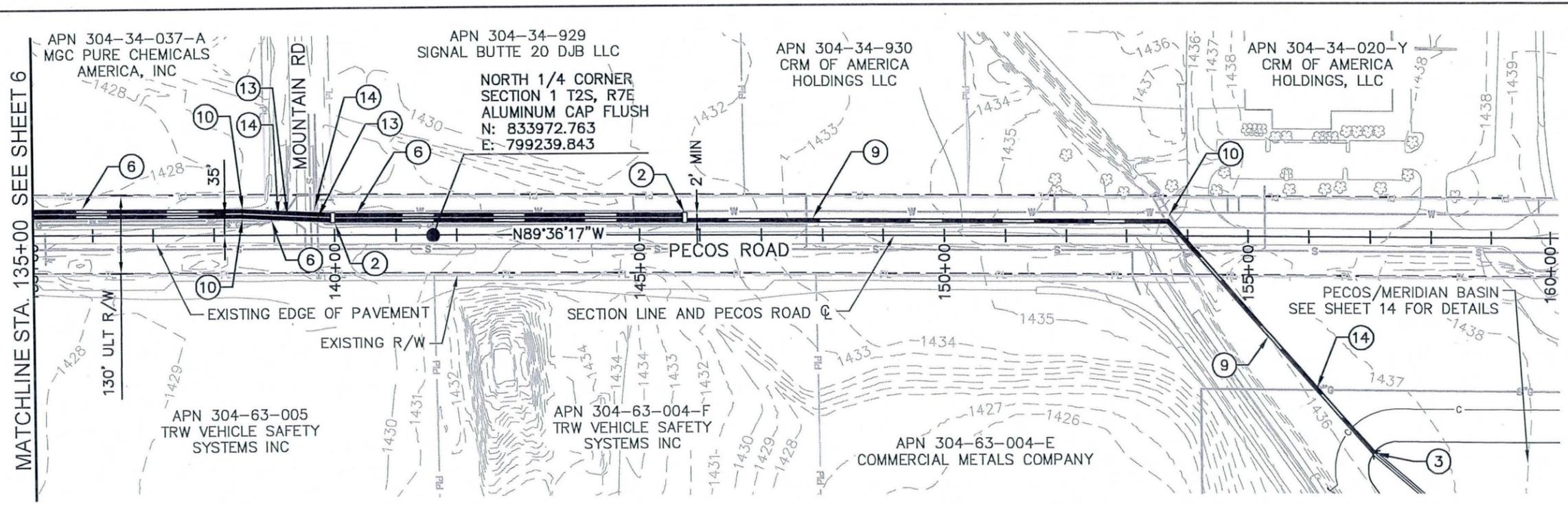


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⑬	WATER LINE RELOCATION	3	EA



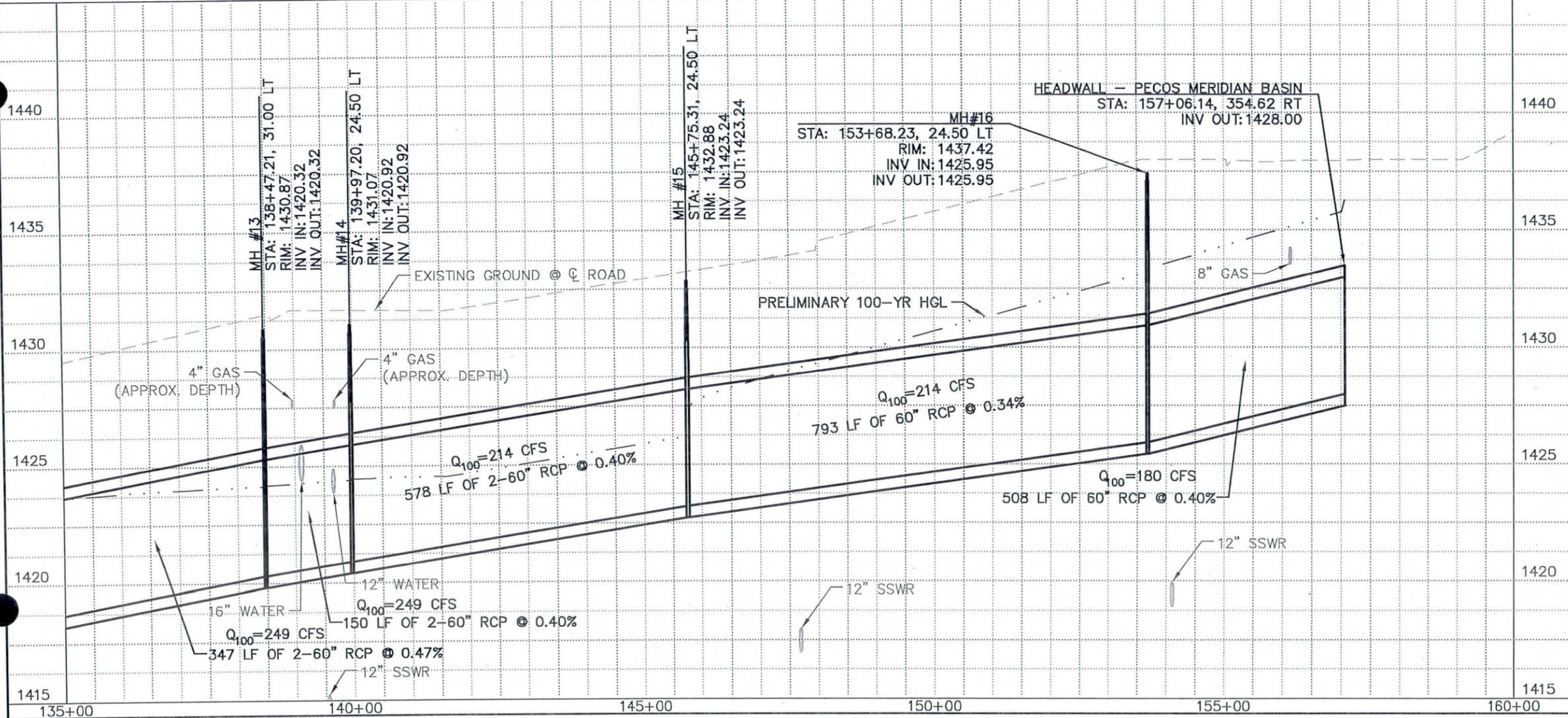
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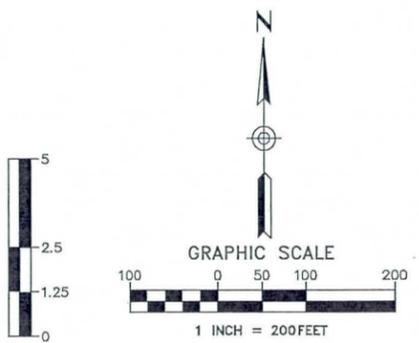
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⑨	60" RGRCP	1301	LF
⑩	MANHOLE, MAG 521&522	3	EA
⑬	WATER LINE RELOCATION	2	EA
⑭	GAS LINE RELOCATION	3	EA



CALL THE SPECIFIC AREA BEFORE YOU GO
602-263-1100
1-800-STAKE-IT
(EXTENDING MARKING SERVICE)



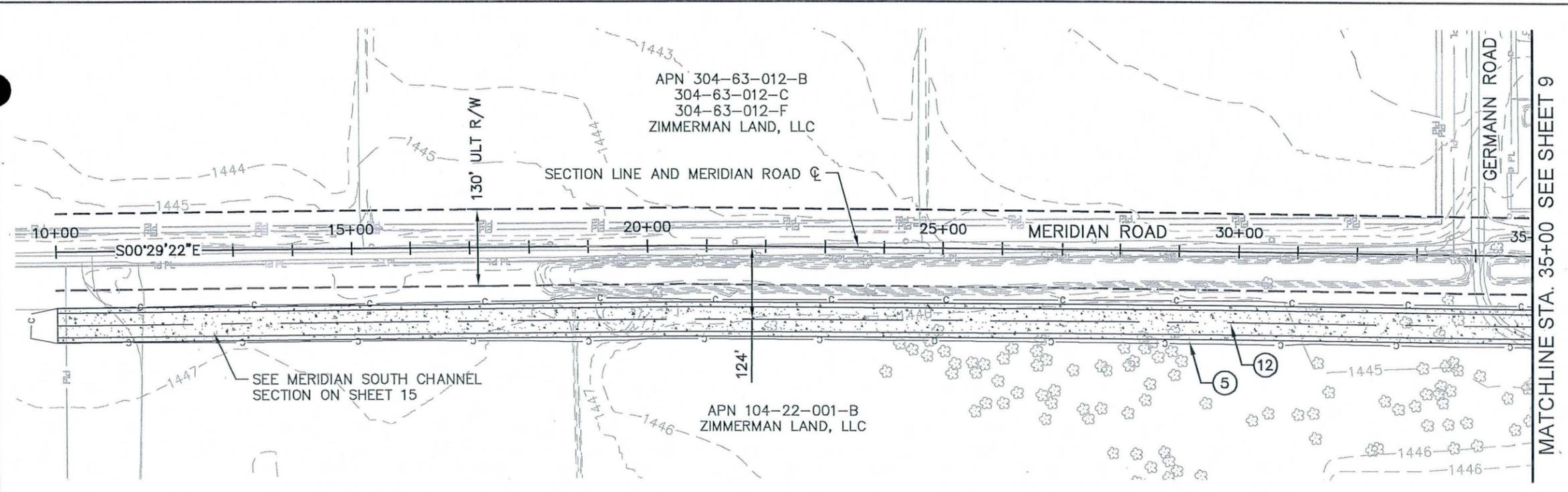
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FLOOD CONTROL DISTRICT OF MARICOPA COUNTY ENGINEERING DIVISION
PECOS ROAD CHANNEL AND BASIN DCR 442.03.20
FCD 2014C001-1

	BY	DATE
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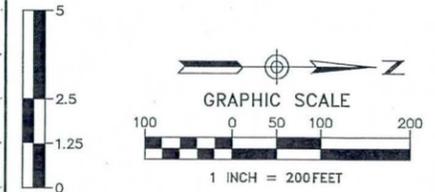
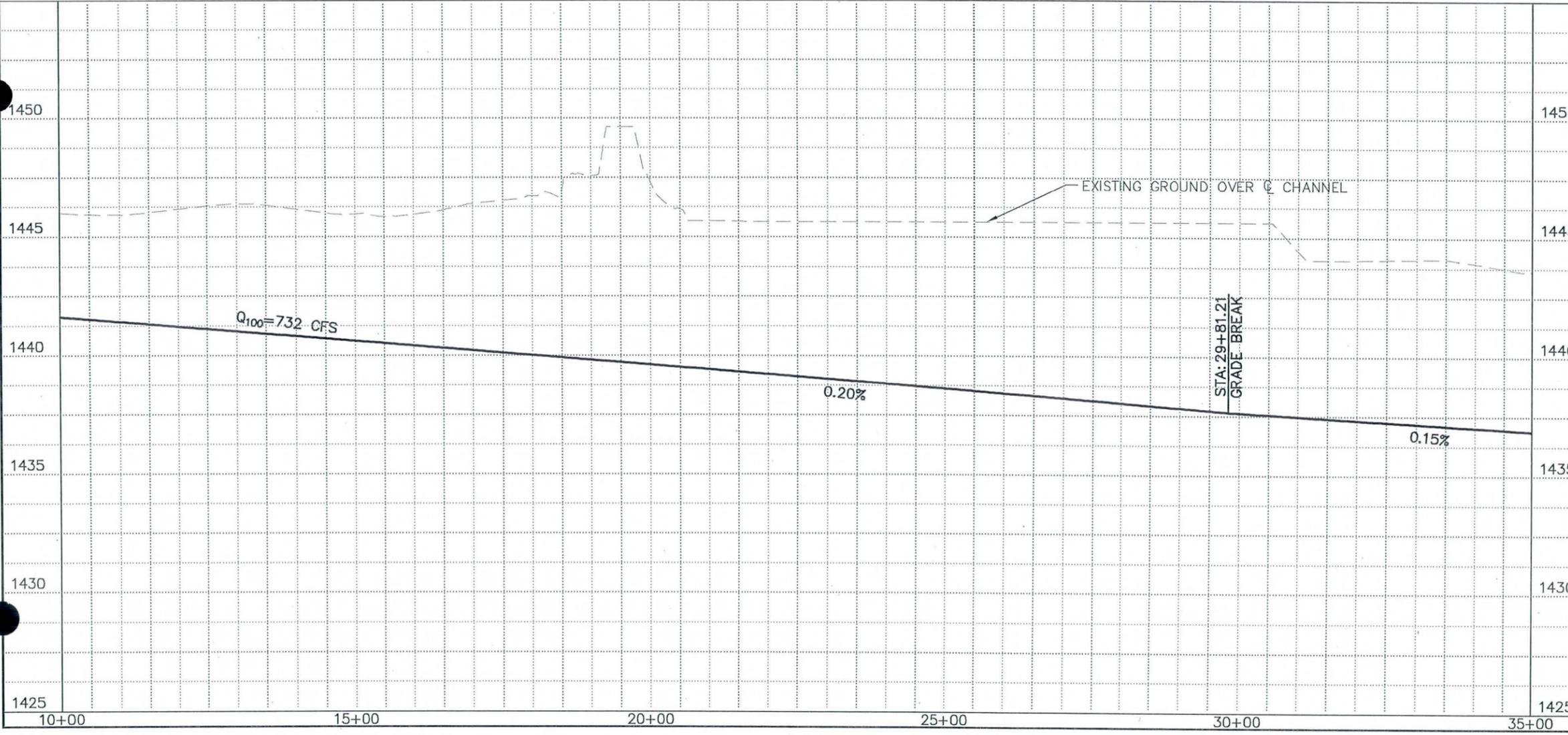
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MATCHLINE STA. 35+00 SEE SHEET 9

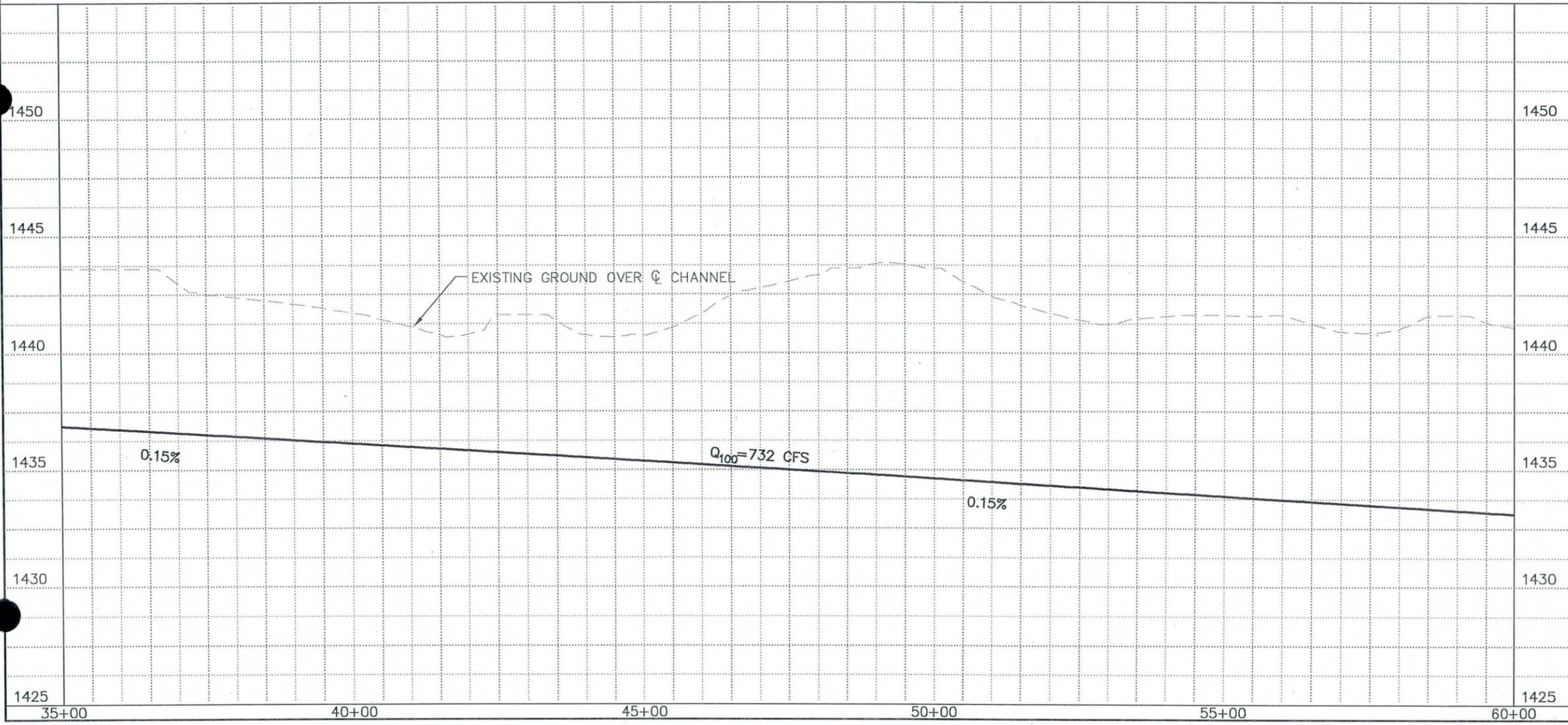
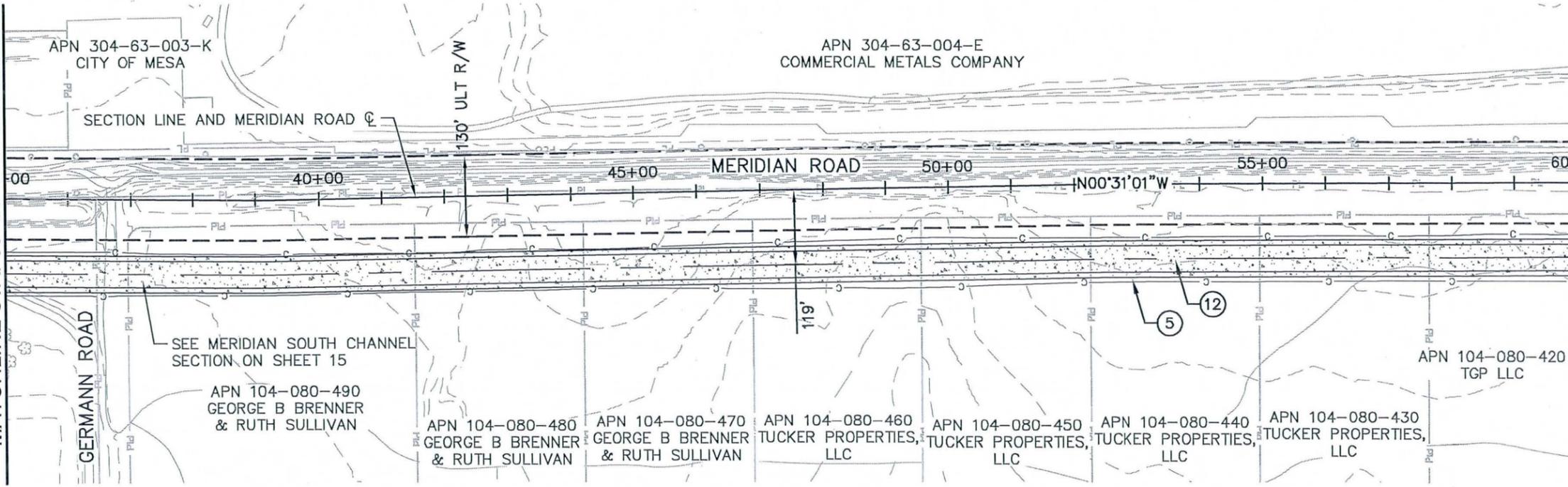
◻ REMOVE ◻			
○ CONSTRUCT ○			
NO	DESCRIPTION	QTY	UNIT
⑤	CHANNEL EXCAVATION	33833	CYD
⑫	REINFORCED CONCRETE	3617	CYD



3			
2			
1			
NO.	REVISION	BY	DATE
 FLOOD CONTROL DISTRICT OF MARICOPA COUNTY ENGINEERING DIVISION			
PECOS ROAD CHANNEL AND BASIN DCR 442.03.20 FCD 2014C001-1			
		BY	DATE
PRELIMINARY NOT FOR CONSTRUCTION		DES: MAW	1/15
		DR: NAS	1/15
		CK: LSM	1/15
Kimley»Horn			
DRAWING NO. DR07	PLAN AND PROFILE STA. 10+00 TO STA. 35+00	SHEET OF 8 15	

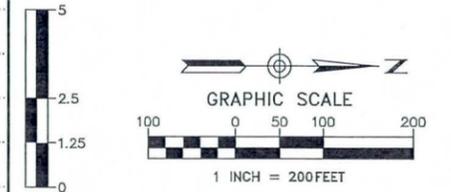
MATCHLINE STA. 35+00 SEE SHEET 8

MATCHLINE STA. 60+00 SEE SHEET 10



CONSTRUCT

NO	DESCRIPTION	QTY	UNIT
5	CHANNEL EXCAVATION	36318	CYD
12	REINFORCED CONCRETE	3617	CYD



NO.	REVISION	BY	DATE
3			
2			
1			

FLOOD CONTROL DISTRICT OF MARICOPA COUNTY ENGINEERING DIVISION

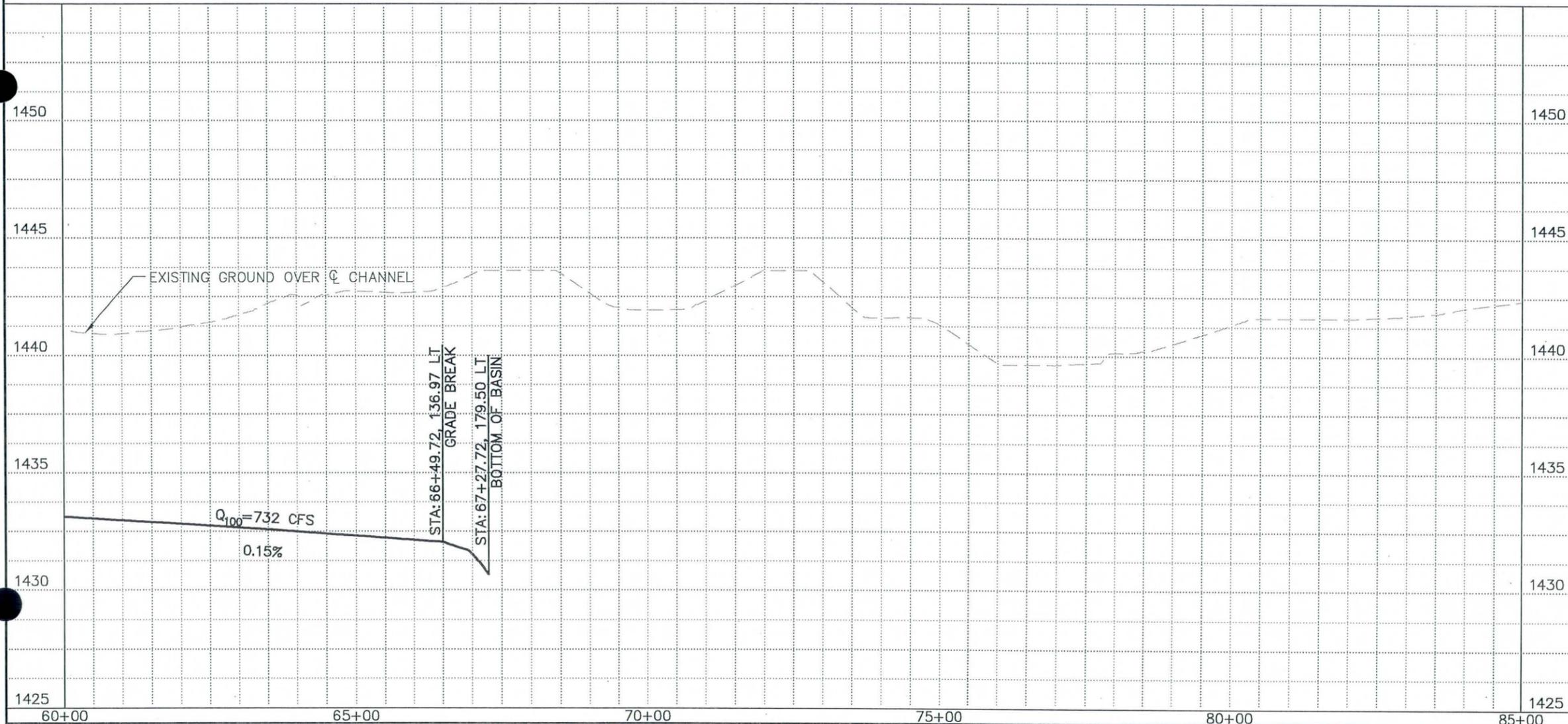
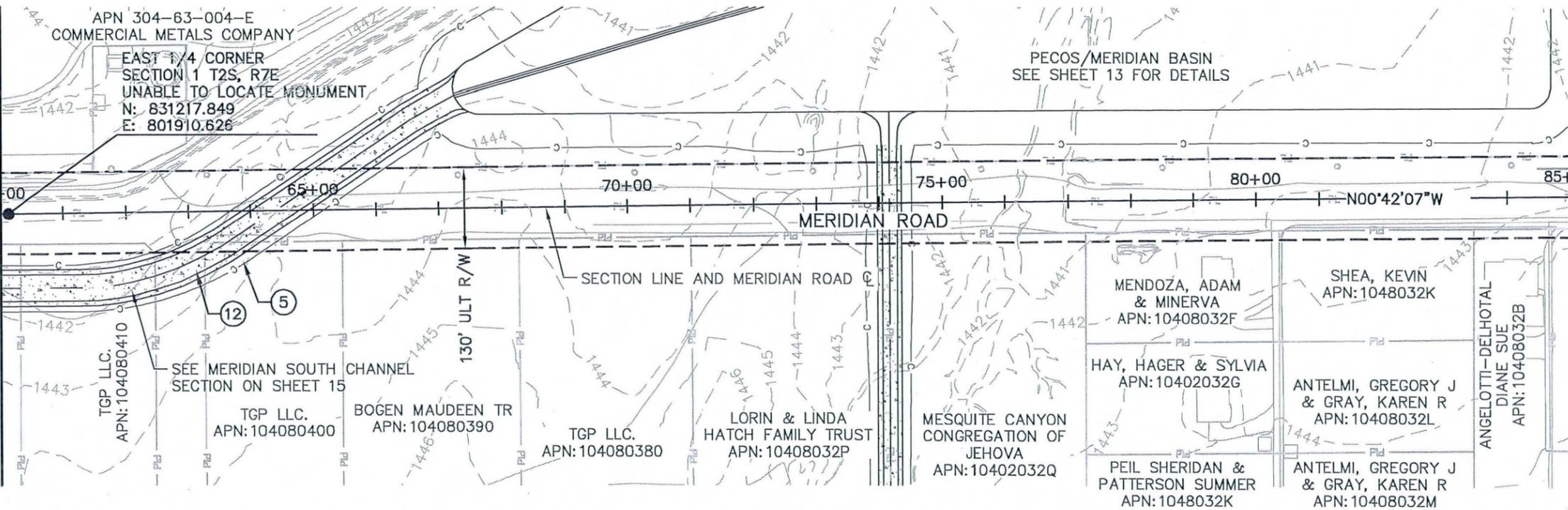
PECOS ROAD CHANNEL AND BASIN DCR 442.03.20 FCD 2014C001-1

	BY	DATE
DES:	MAW	1/15
DR:	NAS	1/15
CK:	LSM	1/15

Kimley»Horn

DRAWING NO.	PLAN AND PROFILE	SHEET OF
DR08	STA. 35+00 TO STA. 60+00	9 15

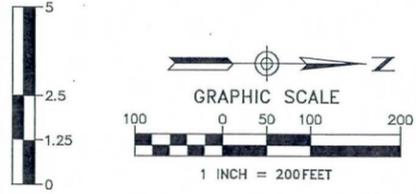
MATCHLINE STA. 60+00 SEE SHEET 9



REMOVE

CONSTRUCT

NO	DESCRIPTION	QTY	UNIT
5	CHANNEL EXCAVATION	15665	CYD
12	REINFORCED CONCRETE	1078	CYD



NO.	REVISION	BY	DATE
3			
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1			

FLOOD CONTROL DISTRICT
OF MARICOPA COUNTY
ENGINEERING DIVISION

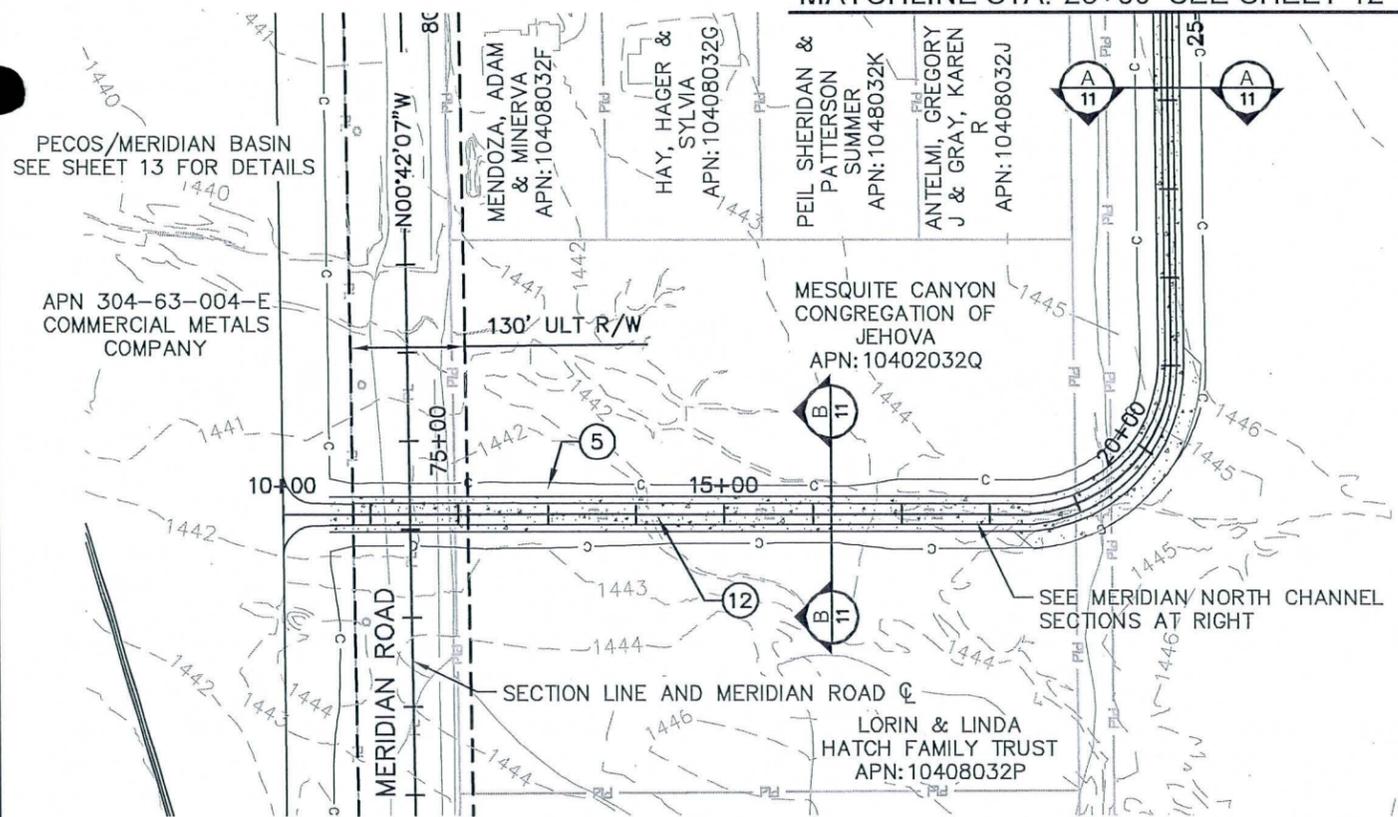
PECOS ROAD CHANNEL AND BASIN DCR
442.03.20
FCD 2014C001-1

	BY	DATE
DES:	MAW	1/15
DR:	NAS	1/15
CK:	LSM	1/15

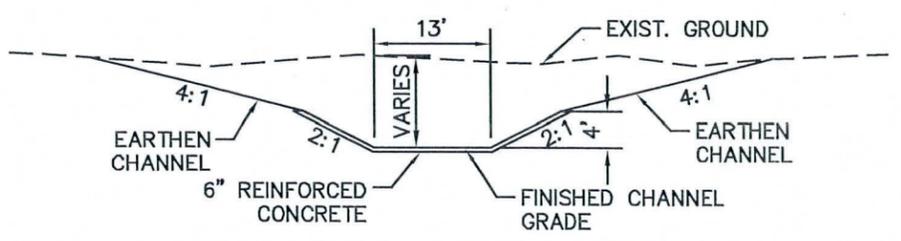
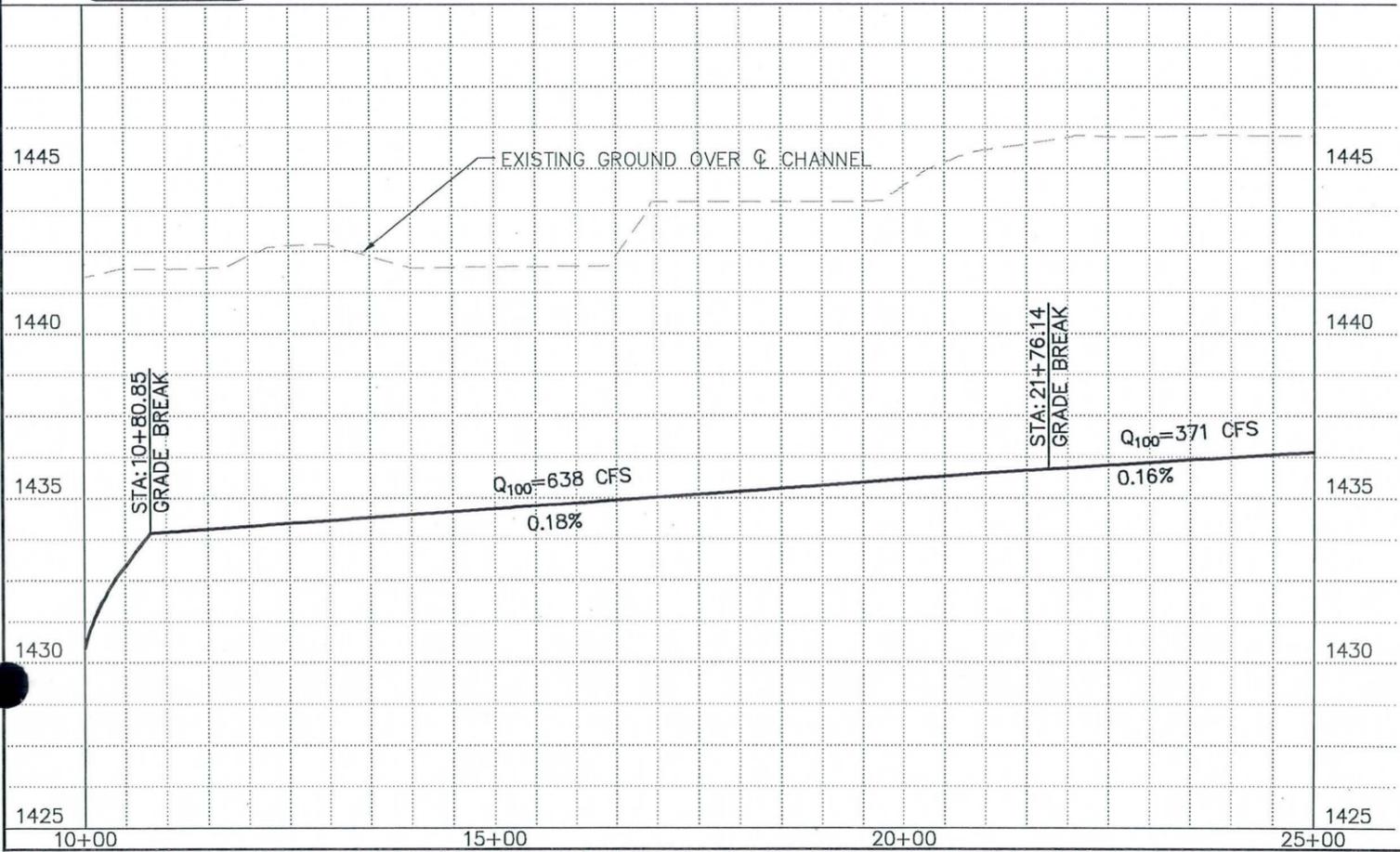
Kimley»Horn

DRAWING NO. DR09 PLAN AND PROFILE STA. 60+00 TO STA. 67+28 SHEET OF 10 15

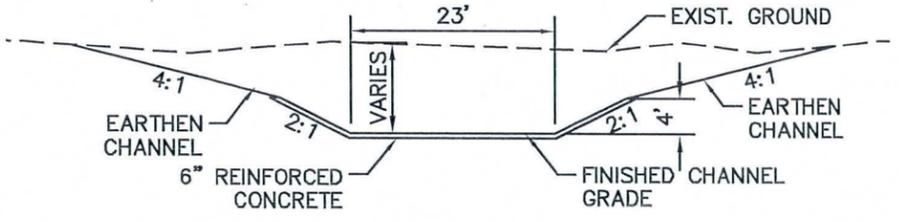
MATCHLINE STA. 25+00 SEE SHEET 12



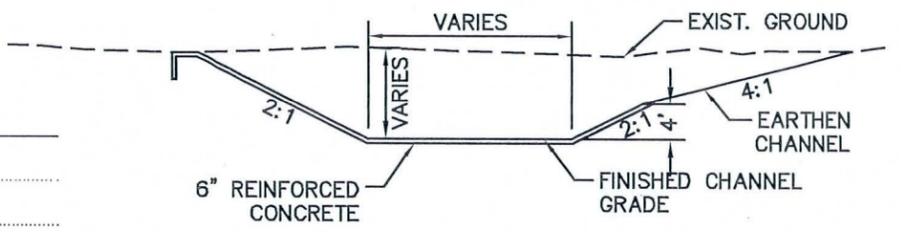
CALL THE NUMBER ON THE BACK OF THE STAKE
602-263-1100
1-800-STAKE-IT
(OUTSIDE MARICOPA COUNTY)



MERIDIAN NORTH CHANNEL - SECTION A-A
 STA: 21+02 TO 42+00
 SCALE: 1"=20'



MERIDIAN NORTH CHANNEL - SECTION B-B
 STA: 10+00 TO 18+45
 SCALE: 1"=20'

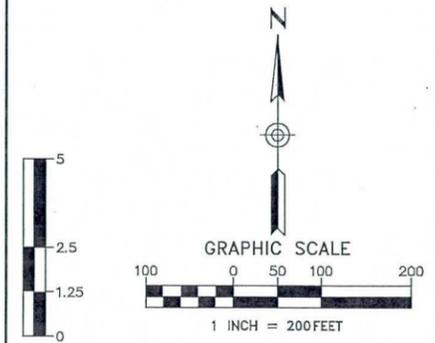


MERIDIAN NORTH CHANNEL - TRANSITION SECTION
 STA: 18+45 TO 21+02
 STA: 42+00 TO 49+60
 SCALE: 1"=20'

REMOVE

CONSTRUCT

NO	DESCRIPTION	QTY	UNIT
⑤	CHANNEL EXCAVATION	19146	CYD
⑫	REINFORCED CONCRETE	1583	CYD



NO.	REVISION	BY	DATE
3			
2			
1			

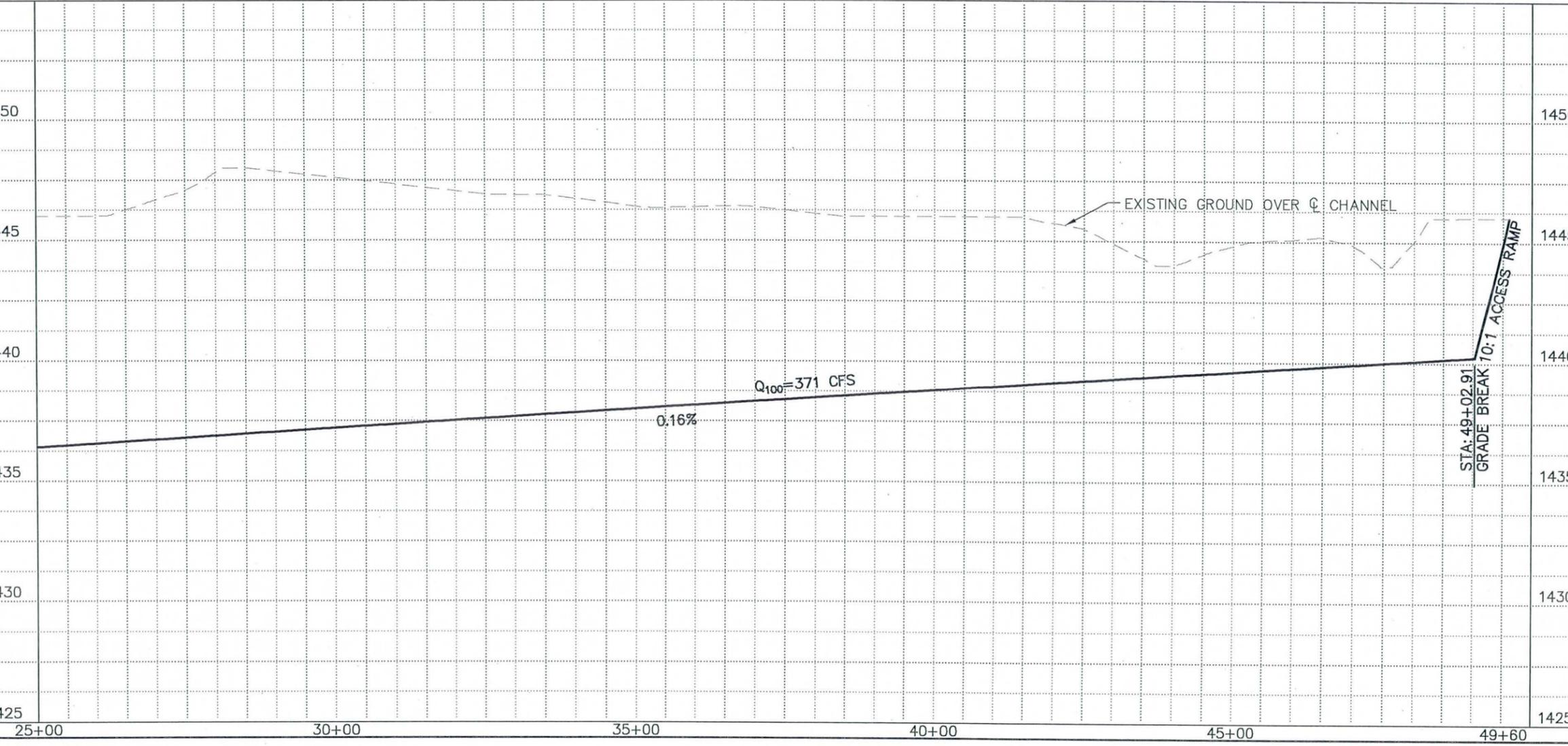
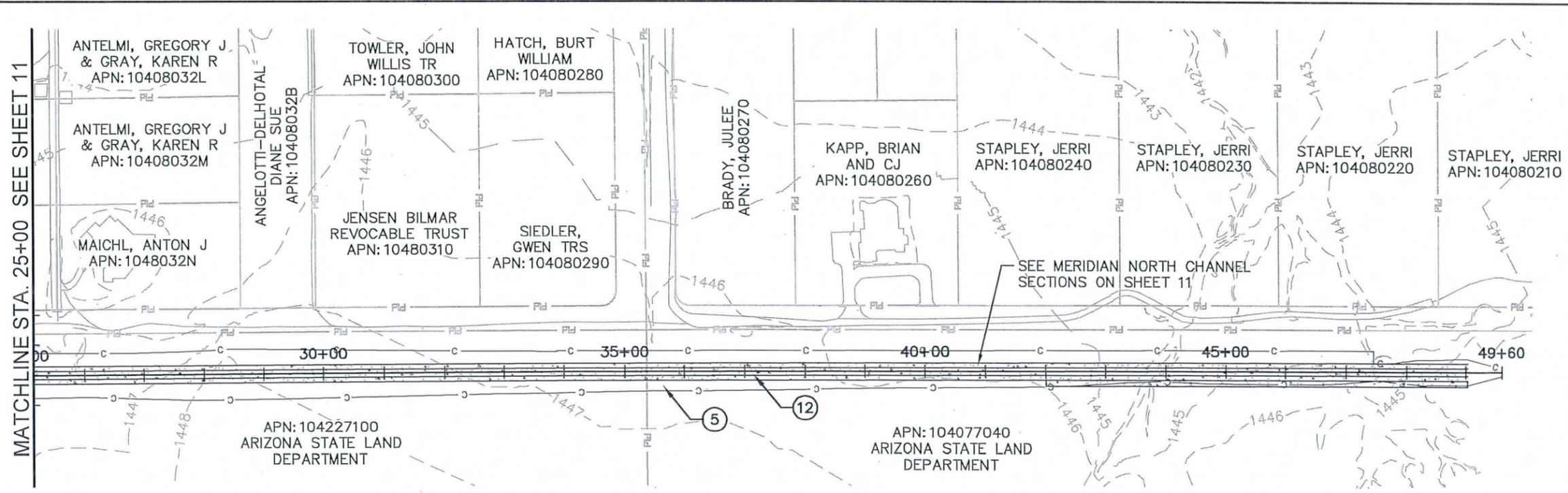
FLOOD CONTROL DISTRICT
 OF MARICOPA COUNTY
 ENGINEERING DIVISION

PECOS ROAD CHANNEL AND BASIN DCR
 442.03.20
 FCD 2014C001-1

	BY	DATE
DES:	MAW	1/15
DR:	NAS	1/15
CK:	LSM	1/15

Kimley»Horn

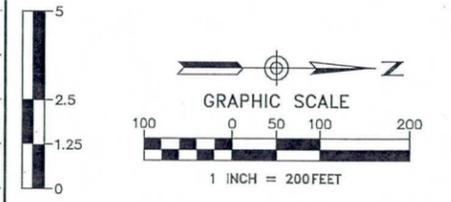
DRAWING NO.	PLAN AND PROFILE	SHEET OF
DR10	STA. 10+00 TO STA. 25+00	11 15



REMOVE

CONSTRUCT

NO	DESCRIPTION	QTY	UNIT
5	CHANNEL EXCAVATION	24085	CYD
12	REINFORCED CONCRETE	2205	CYD



NO.	REVISION	BY	DATE
3			
2			
1			

FLOOD CONTROL DISTRICT OF MARICOPA COUNTY ENGINEERING DIVISION

PECOS ROAD CHANNEL AND BASIN DCR 442.03.20 FCD 2014C001-1

	BY	DATE
DES:	MAW	1/15
DR:	NAS	1/15
CK:	LSM	1/15

PRELIMINARY NOT FOR CONSTRUCTION

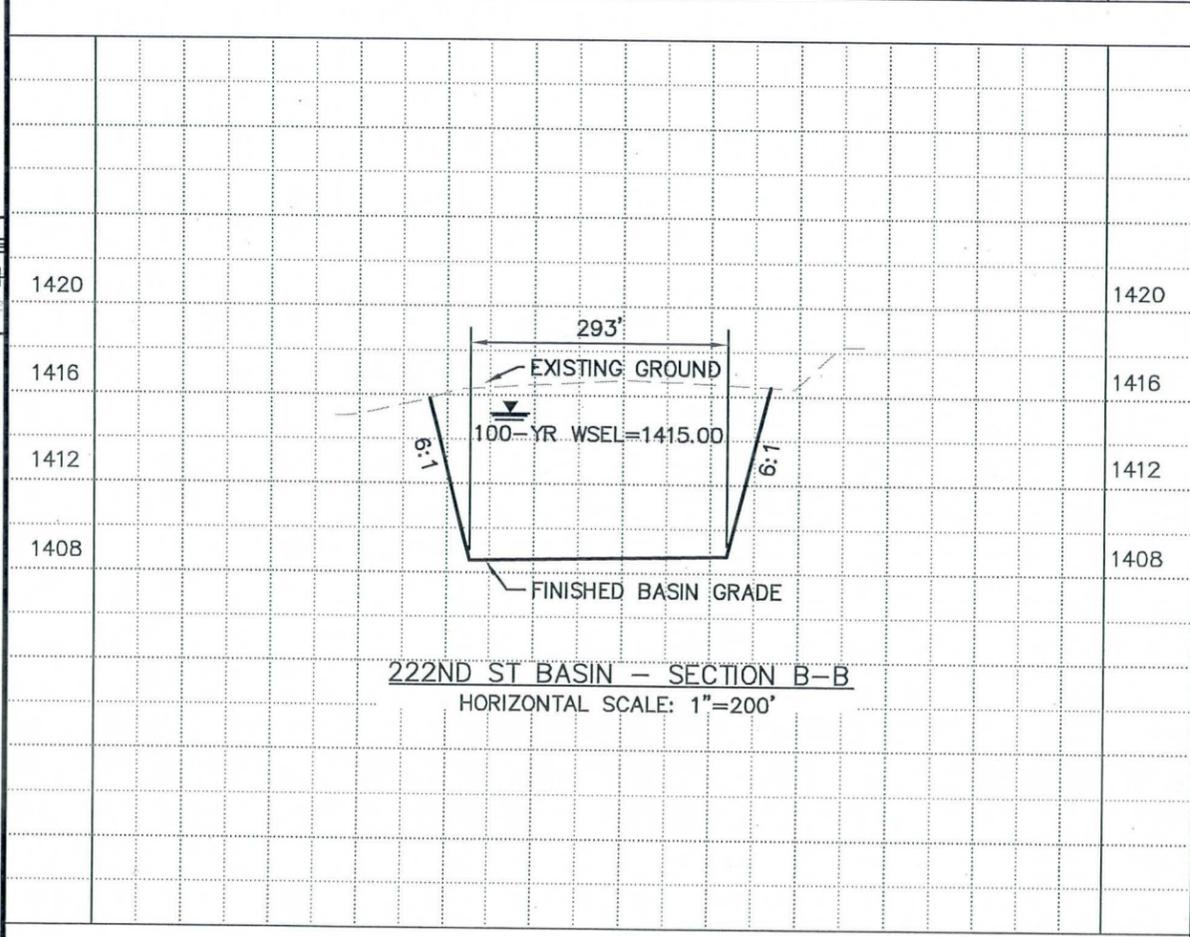
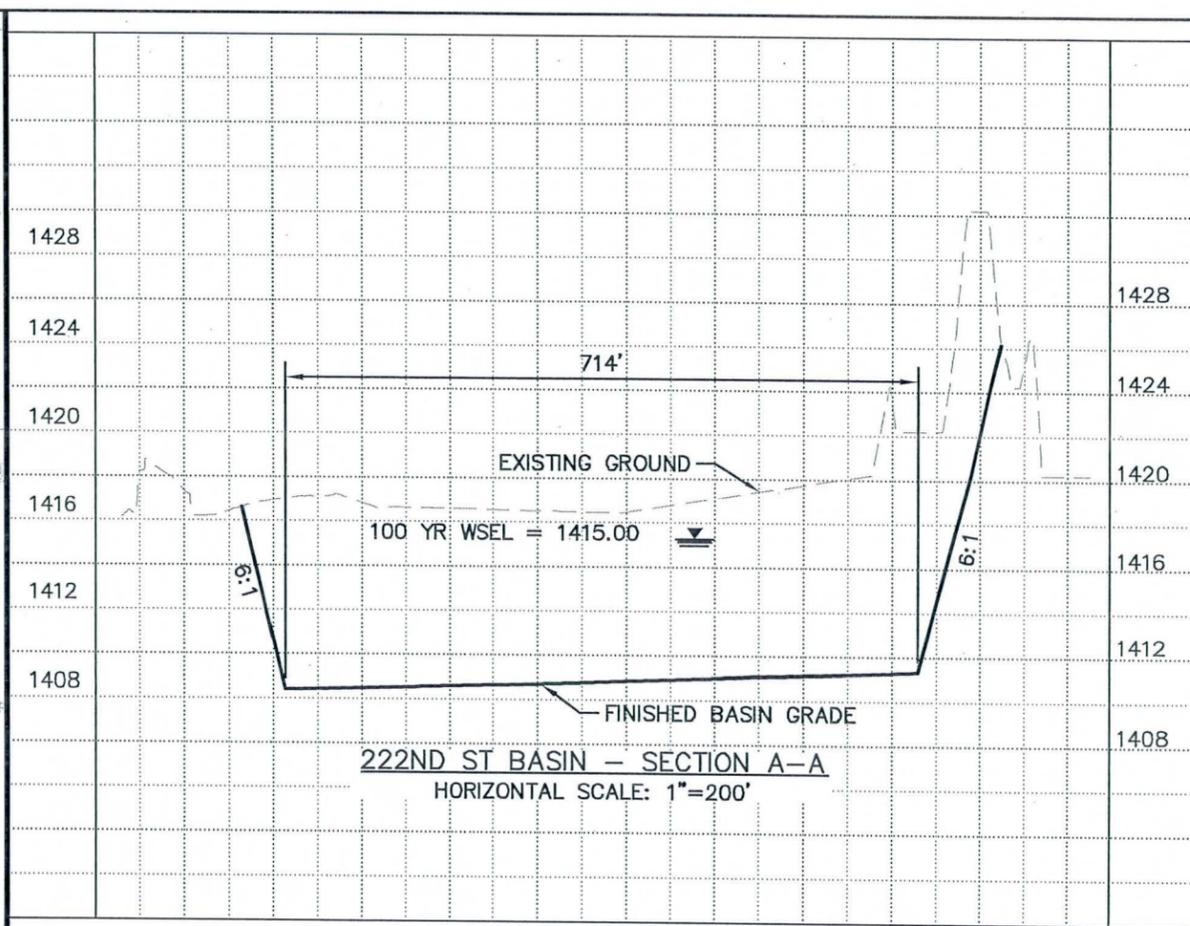
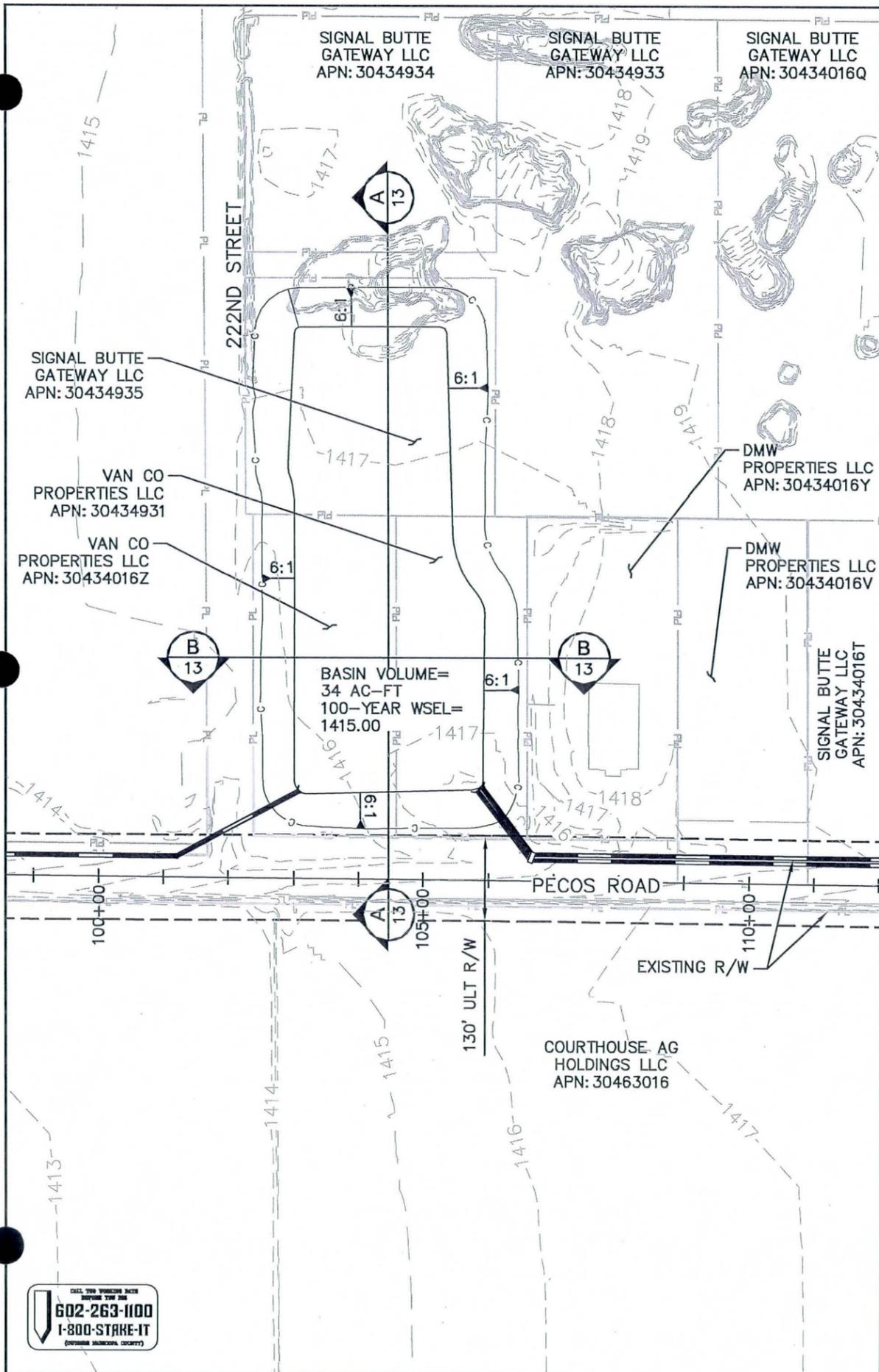
Kimley»Horn

DRAWING NO. DR11	PLAN AND PROFILE STA. 25+00 TO STA. 49+60	SHEET OF 12 15
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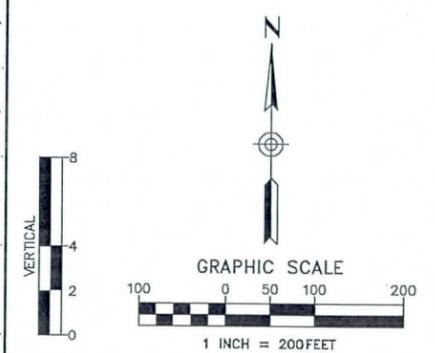
MATCHLINE STA. 25+00 SEE SHEET 11

SEE MERIDIAN NORTH CHANNEL SECTIONS ON SHEET 11

STA: 49+02.91
GRADE BREAK 10:1 ACCESS RAMP



REMOVE
 CONSTRUCT



3			
2			
1			
NO.	REVISION	BY	DATE

FLOOD CONTROL DISTRICT
 OF MARICOPA COUNTY
 ENGINEERING DIVISION
 PECOS ROAD CHANNEL AND BASIN DCR
 442.03.20
 FCD 2014C001-1

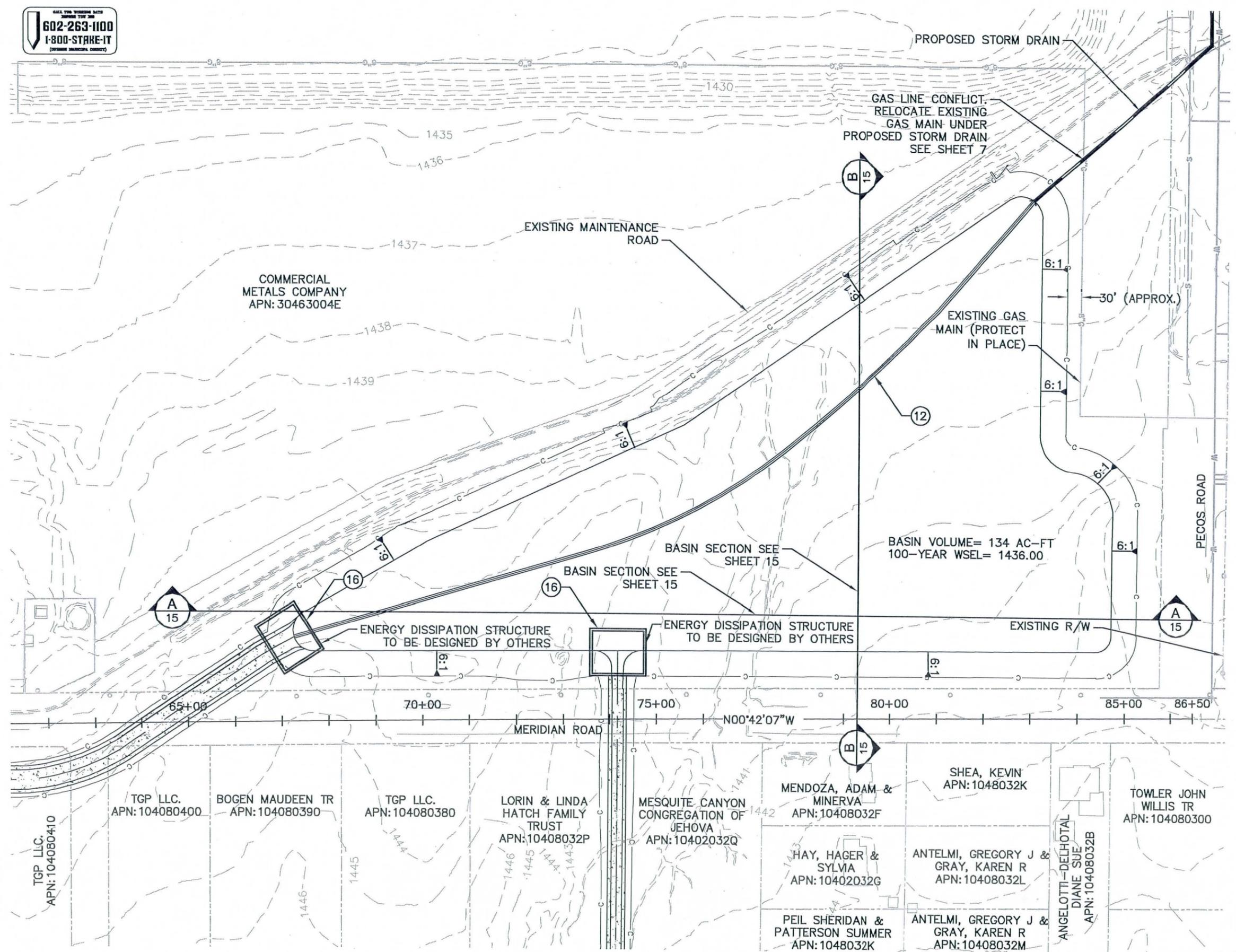
PRELIMINARY NOT FOR CONSTRUCTION	DES:	MAW	DATE	1/15
	DR:	NAS		1/15
	CK:	LSM		1/15

Kimley»Horn

DRAWING NO. DR12	BASIN DETAILS PECOS/222ND STREET BASIN	SHEET OF 13 15
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CALL THE WORKING DATE
 BEFORE THE JOB
602-263-1100
1-800-STRAKE-IT
(OUTSIDE MARICOPA COUNTY)

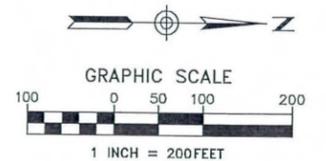
CALL THE TRADING PARTS
 BEFORE YOU BUY
602-263-1100
1-800-STAKE-IT
(OFFERING FINANCIAL SERVICES)



REMOVE

CONSTRUCT

NO	STATION TO STATION	QTY	UNIT
(12)	REINFORCED CONCRETE	253	CYD
(16)	ENERGY DISSIPATION STRUCTURE	2	EA



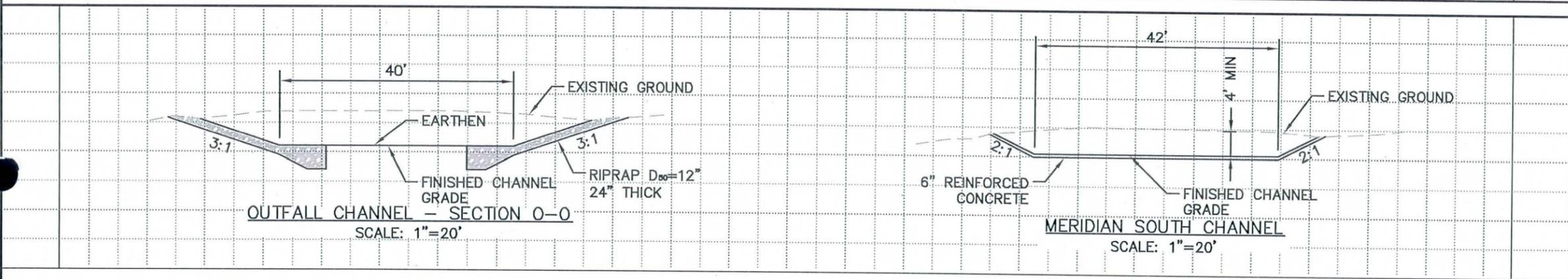
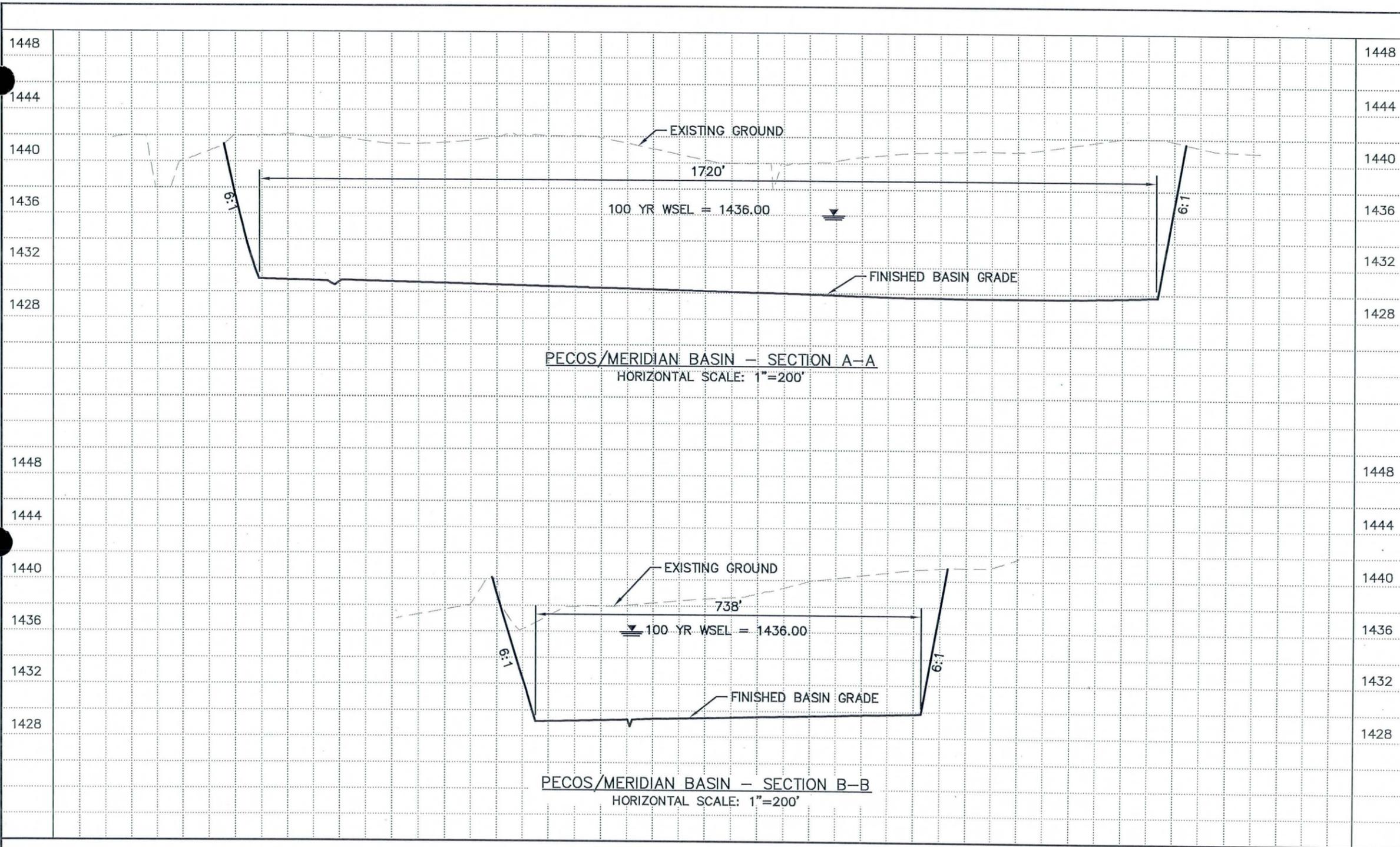
3			
2			
1			
NO.	REVISION	BY	DATE

FLOOD CONTROL DISTRICT
 OF MARICOPA COUNTY
 ENGINEERING DIVISION
 PECOS ROAD CHANNEL AND BASIN DCR
 442.03.20
 FCD 2014C001-1

	BY	DATE
DES:	MAW	1/15
DR:	NAS	1/15
CK:	LSM	1/15

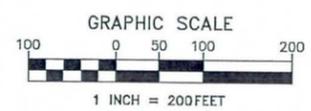
Kimley»Horn

DRAWING NO. DR13	BASIN DETAIL PECOS/MERIDIAN BASIN	SHEET OF 14 15
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REMOVE

CONSTRUCT



CALL TEO YOUNG LATE
MORNING 7:30 AM
602-263-1100
1-800-STAKE-IT
(OUTSIDE MARICOPA COUNTY)

3			
2			
1			
NO.	REVISION	BY	DATE

**FLOOD CONTROL DISTRICT
OF MARICOPA COUNTY
ENGINEERING DIVISION**

**PECOS ROAD CHANNEL AND BASIN DCR
442.03.20
FCD 2014C001-1**

PRELIMINARY NOT FOR CONSTRUCTION	DES:	MAW	DATE	1/15
	DR:	NAS		1/15
	CK:	LSM		1/15

Kimley»Horn

DRAWING NO. DR14	TYPICAL SECTIONS PECOS/222ND STREET BASIN	SHEET OF 15 15
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