

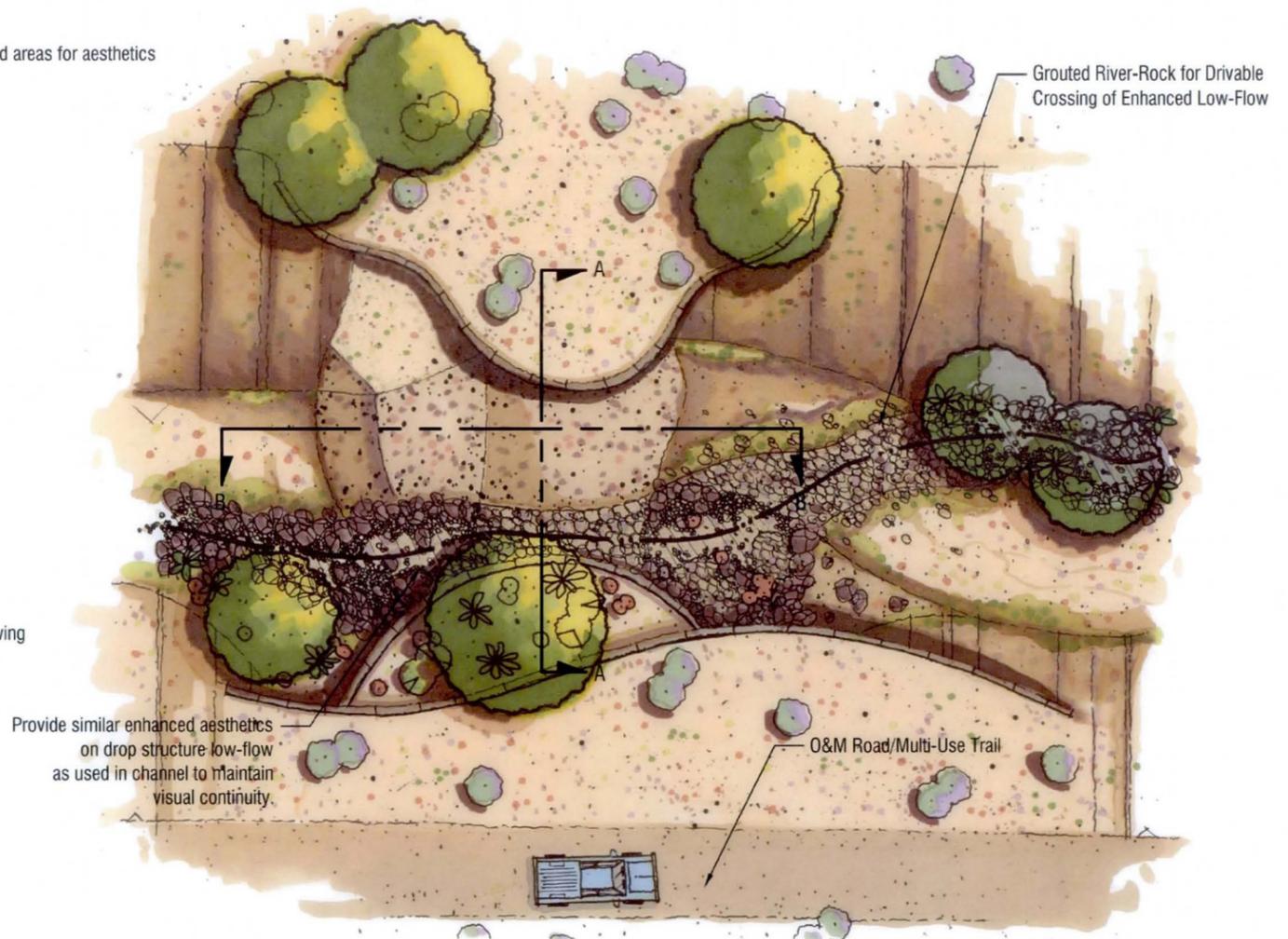
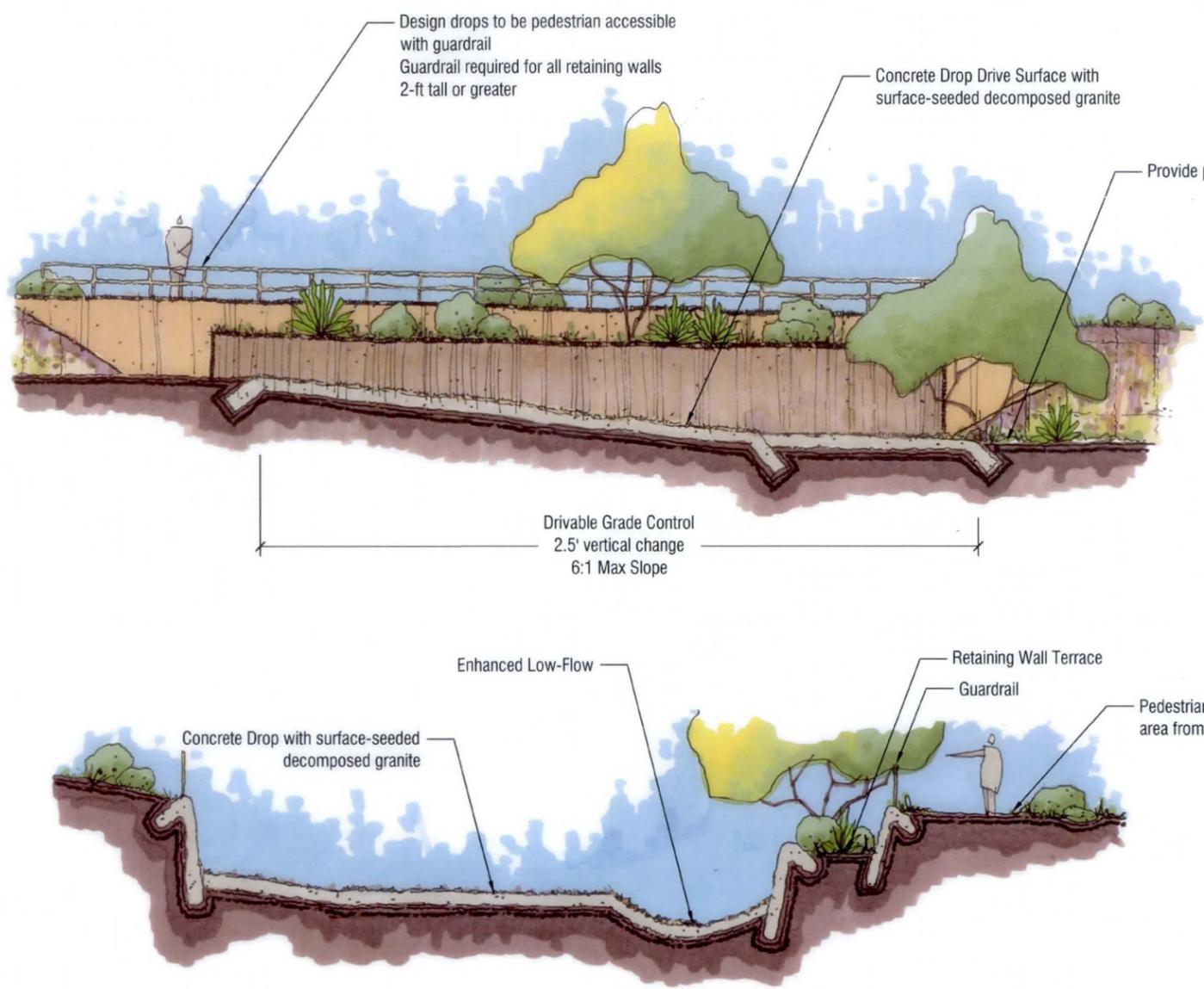


# White Tanks FRS No. 3 Outfall Channel

## Pre-Design Report

FCD 2009C012

January 29, 2010



201 West Indian School Road • Phoenix, AZ 85013 • (602) 252.8384



**TABLE OF CONTENTS**

1	Introduction .....	1	5.4	Retaining Walls .....	16
1.1	Stakeholders .....	3	5.5	Landscape Integration .....	17
1.2	Purpose .....	3	5.5.1	Natural Form Channel .....	18
1.3	Value Analysis and Value Engineering .....	3	5.5.2	Meandered Trapezoidal Channel .....	19
1.4	Authority for Study .....	3	5.5.3	Restricted Open Channel .....	20
1.5	Location of Study .....	3	5.5.4	Hardened Channel .....	21
2	Design Considerations .....	4	6	Reach Evaluation .....	22
2.1	Introduction .....	4	6.1	Reaches 6 and 7 .....	22
2.2	FRS#3 Remediation Project .....	4	6.1.1	Alternative 6/7A .....	22
2.3	Jackrabbit Trail and Jackrabbit Parkway .....	5	6.1.2	Alternative 6/7B .....	22
2.4	Buckeye Park and Ride .....	5	6.1.3	Alternative 6/7C .....	22
2.5	Buckeye Sewer Improvement Project .....	5	6.1.4	Alternative 6/7D .....	22
2.6	Operations and Maintenance Road .....	5	6.1.5	Alternative 6/7E .....	22
2.7	Channel Scour and Erosion Protection .....	6	6.1.6	Alternative 6/7F .....	22
2.8	Side Drainage Inlets .....	6	6.2	Reach 9 .....	29
2.9	Culvert Crossings .....	7	6.2.1	Alternative 9A .....	29
2.10	Reach 6 .....	7	6.2.2	Alternative 9B .....	29
2.11	Reach 7 .....	7	6.2.3	Alternative 9C .....	29
2.12	Reach 9 .....	7	6.2.4	Alternative 9D .....	29
2.12.1	Principal Spillway Channel .....	7	6.2.5	Alternative 9E .....	29
2.12.2	Emergency Spillway .....	7	6.2.6	Alternative 9F .....	29
2.12.3	Earth Fissures and Subsidence .....	8	6.2.7	Alternative 9G .....	29
2.12.4	Principal Spillway Wasteway .....	8	6.3	Cost Comparison .....	37
3	Hydrology .....	9	7	Conclusions and Recommendations .....	39
3.1	Existing Conditions with Project in Place .....	9	8	References .....	40
3.2	Future Conditions with Project in Place .....	9			
3.3	Probable Maximum Flood (PMF) for FRS#3 .....	10			
4	Hydraulics .....	11			
4.1	Sedimentation and Scour Analysis .....	11			
4.1.1	Soil Data .....	11			
4.1.2	Equilibrium Slope .....	11			
4.2	Culvert Hydraulics .....	11			
4.3	Wasteway Flows to Beardsley Canal and Wash .....	12			
5	Design Elements .....	14			
5.1	Culverts .....	14			
5.2	Pipe Options .....	14			
5.3	Grade Control Structures .....	15			



EXPIRES 3/31/2012



**TABLE OF CONTENTS (Continued)**

Figure 1	Location and Vicinity Map .....	1	Table 1	HEC-1 Model and Design Discharges .....	10
Figure 2	Project Schematic Map .....	2	Table 2	Land Cost Comparison .....	37
Figure 3	Buckeye Park and Ride Palm Lane Entrance .....	5	Table 3	Reach Evaluation Cost Comparison, 30% Design Report Cost Estimates .....	38
Figure 4	Typical Grade Control Structure Looking Upstream in the Channel.....	6	Table 4	Reach Evaluation Cost Comparison, 2010 Land Cost Estimates .....	38
Figure 5	Cross-Section through Grade Control Structure.....	6			
Figure 6	Wasteway Flow Inundation Area .....	13	Appendix A	Product Literature.....	A-1
Figure 7	Con-Span and Bebo Pre-Case Culvert Options .....	14	Appendix B	FRS No. 3 Outlet Design Capacity Memorandum.....	B-1
Figure 8	HDPE Welded Seam Pipe .....	14	Appendix C	Hydrologic Modeling .....	C-1
Figure 9	ArmorFlex Used for Spillway and Grade Control Structure .....	15	C.1	Schematic Maps .....	C-1
Figure 10	ArmorFlex Block.....	15	C.2	Future Conditions with Project in Place, 10-Year for FRS#3 Area.....	C-4
Figure 11	ArmorFlex Installation Cross-Section .....	15	C.3	Future Conditions with Project in Place, 10-Year for Jackrabbit Corridor .....	C-11
Figure 12	Terraced Keystone Wall System .....	16	C.4	Existing Conditions with Project in Place, 100-Year for FRS#3 Area .....	C-15
Figure 13	Straight-Faced and Tri-Plane Variants of Keystone Block System .....	16	C.5	Existing Conditions with Project in Place, 100-Year for Jackrabbit Corridor.....	C-22
Figure 14	Natural Form Channel.....	18	C.6	Existing Conditions with Project in Place, 10-Year for FRS#3 Area .....	C-32
Figure 15	Meandered Trapezoidal Channel .....	19	C.7	Existing Conditions with Project in Place, 10-Year for Jackrabbit Corridor.....	C-39
Figure 16	Restricted Open Channel .....	20	Appendix D	Culvert Hydraulic Calculations .....	D-1
Figure 17	Hardened Channel.....	21	Appendix E	Equilibrium Slope Calculation .....	E-1
Figure 18	Alternative 6/7A .....	23	Appendix F	Cost Estimate.....	F-1
Figure 19	Alternative 6/7B .....	24	Appendix G	Value Engineering Memorandum by Jacobs.....	G-2
Figure 20	Alternative 6/7C .....	25	Appendix H	Wasteway Flow HEC-RAS Model.....	H-2
Figure 21	Alternative 6/7D .....	26	Appendix J	Comparison of Flo2D Grid vs. Aerial Mapping .....	J-2
Figure 22	Alternative 6/7E.....	27			
Figure 23	Alternative 6/7F.....	28			
Figure 24	Alternative 9A.....	30			
Figure 25	Alternative 9B.....	31			
Figure 26	Alternative 9C .....	32			
Figure 27	Alternative 9D .....	33			
Figure 28	Alternative 9E.....	34			
Figure 29	Alternative 9F.....	35			
Figure 30	Alternative 9G .....	36			
Figure 31	Schematic Map for FRS#3 Area HEC-1 Model .....	C-1			
Figure 32	Schematic Map for Jackrabbit Corridor HEC-1 Model, Existing Condition with Project in Place.....	C-2			
Figure 33	Schematic Map for Jackrabbit Corridor HEC-1 Model, Future Condition with Project in Place .....	C-3			



EXPIRES 3/31/2012



## 1 INTRODUCTION

Hoskin•Ryan Consultants, Inc. (HRC), has been contracted by the Flood Control District of Maricopa County (District) to prepare final design for the White Tanks FRS No. 3 (FRS#3) Outfall Channel project. The District is in the process of performing rehabilitation to FRS#3, including a new Principal Spillway that discharges adjacent to the Beardsley Canal. The project provides a channel along the Jackrabbit Trail corridor, to convey the Principal Spillway flows from FRS#3 to FRS#4. The outfall channel will extend south from the Principal Spillway of FRS#3 to the existing FRS#4 inlet channel north of McDowell Road, and will lie within the Town of Buckeye and unincorporated Maricopa County.

The goals of the project include:

- Provide an outfall for the FRS#3 Principal Spillway flows.
- Intercept and convey the 100-year flood flows reaching the channel to the planned outfall at FRS#4.
- Reduce the effective FEMA 100-year floodplain along Jackrabbit Trail.
- Accommodate the future widening of Jackrabbit Trail.
- Design the facilities to complement the existing and planned future setting through implementation of context sensitive planning and design.
- Provide an opportunity to implement trail linkage as part of the Maricopa County Regional Trail System.

The existing FRS#4 inlet channel is a concrete-lined channel which extends from south of Interstate 10 (I-10) to north of McDowell Road. North of the existing concrete-lined channel, the existing Jackrabbit Channel and Wash are a series of unlined channels and ditches of varying dimensions and capacities. Between Missouri Avenue and the Bethany Home Road alignment, natural drainage patterns continue across the Jackrabbit Trail alignment from west to east. From the Bethany Home Road alignment north to FRS#3, the predominant land slope is east towards the Beardsley Canal.

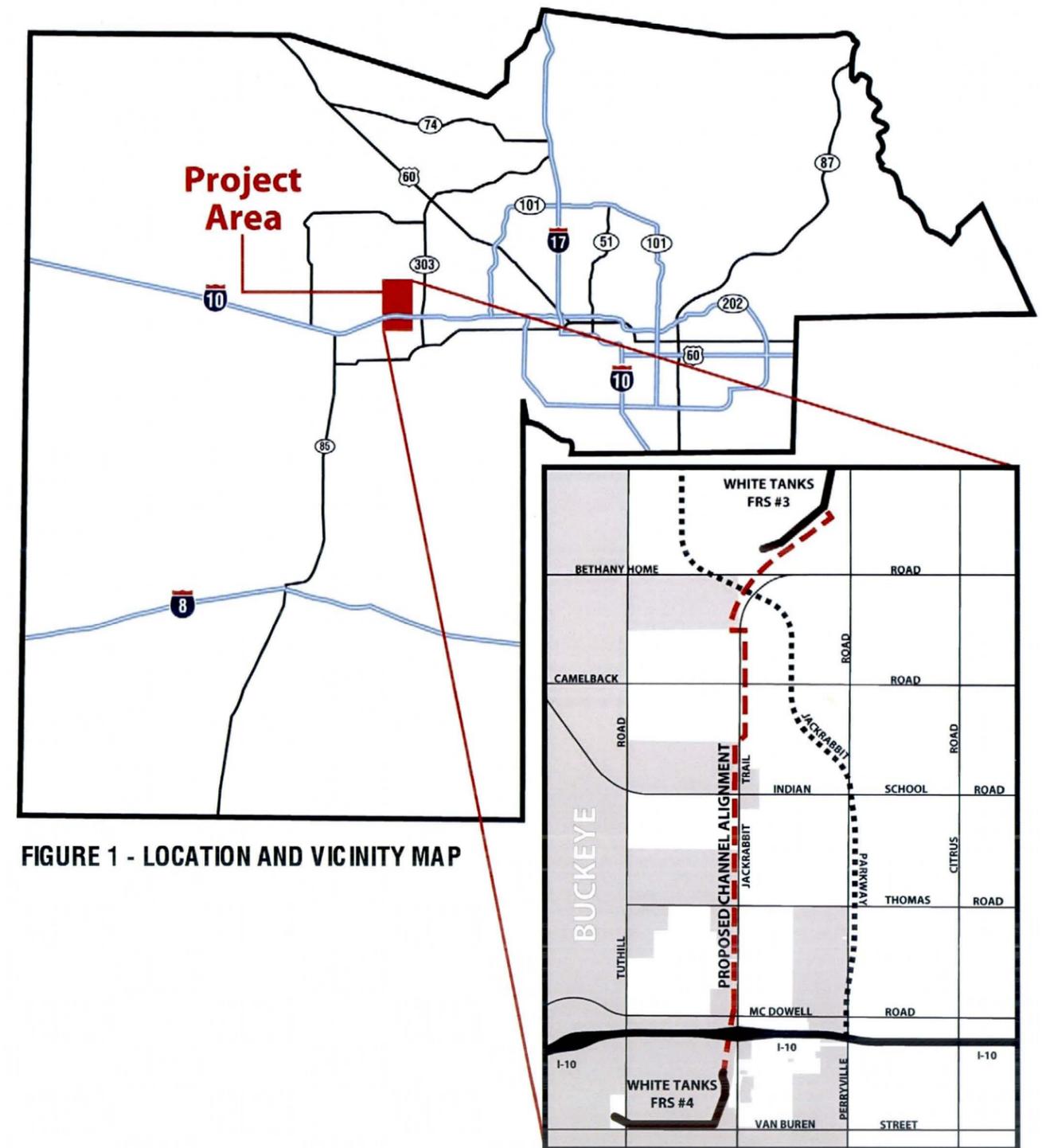


FIGURE 1 - LOCATION AND VICINITY MAP

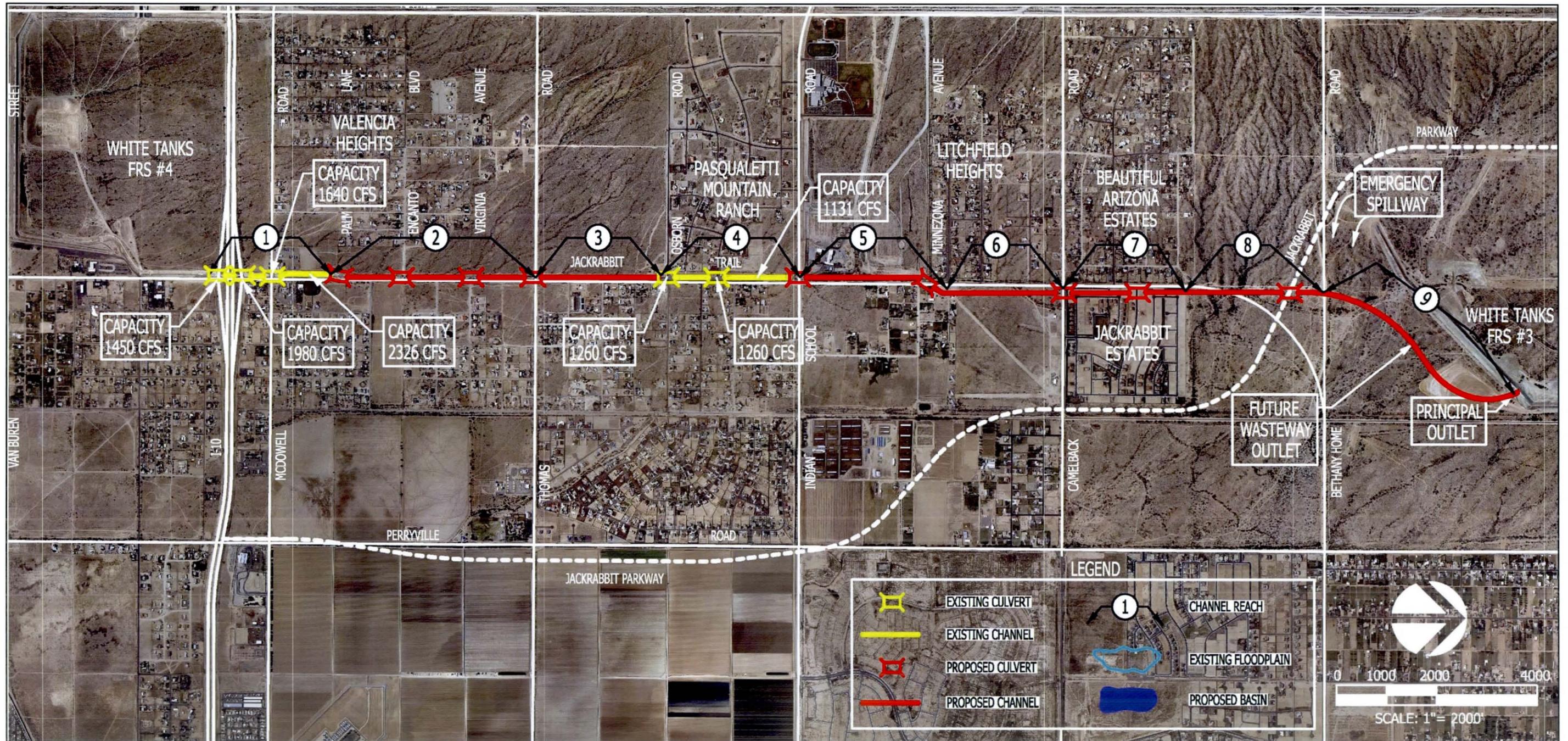


FIGURE 2 – PROJECT SCHEMATIC MAP



## 1.1 Stakeholders

On-going projects and interested stakeholders include the District, the Arizona Department of Transportation (ADOT), Maricopa County Department of Transportation (MCDOT), the Town of Buckeye, the Maricopa County Municipal Water Conservation District (MWD), existing developments such as Jackrabbit Estates (Arryo Mountain Estates), Beautiful Arizona Estates, Pasqualetti Ranch, and Litchfield Heights, and private development interests such as DMB White Tanks (Verrado, north of Indian School Road) and SouthWest Value Partners (north of Missouri Avenue).

## 1.2 Purpose

The *Design Report and 30% Plans* for the White Tanks FRS#3 Outfall Channel project (Figure 1) were completed on June 30, 2009 (Refs. 34, 35) and form the basis for the final design. This Pre-Design Report documents the re-evaluation of several alternative channel alignments and design approaches that were highlighted as a part of a Value Analysis conducted by the District.

This report is submitted in conjunction with a *Landscape Architecture Pre-Design Report* (Ref. 12). The 30% Plans were prepared without the guidance of a landscape architect, therefore it is the intent of the Landscape Pre-Design to identify methods to incorporate landscape materials, aesthetic structural treatments and trail connectivity into the project.

Results from this report will be incorporated into the Final Design Plans and Reports, as applicable.

## 1.3 Value Analysis and Value Engineering Review

A Value Analysis was conducted for the entire project limits. The purpose of the Value Analysis was to identify alternative design concepts that may have been overlooked in the planning and engineering stages of the project. Results from the Value Analysis are documented in a separate report (Ref. 40). Many different ideas and concepts were developed over the three-day Value Analysis session. Members of the Value Analysis team voted on ideas of merit; a shortlisted group of concepts was further developed, and cost estimates were prepared.

These concepts were presented to a panel of District personnel and some were eliminated because they did not meet the original intent of the project or they appeared unfeasible due to schedule or inter-agency conflicts.

In addition to the Value Analysis Session conducted by the District, Jacobs prepared a Value Engineering review of the 30% Plans; a copy of the resulting memorandum is included in Appendix G. The main recommendations from the Value Engineering review include potentially using HDPE pipe within Reach 9, and arch culverts within Reach 6.

## 1.4 Authority for Study

A detailed Scope of Work was formulated as a part of the contract and proposal process. The Flood Control District of Maricopa County's contract number is FCD 2009C012. The official Notice to Proceed date is October 22, 2009. The District Project Manager is Gary Wesch, P.E.

## 1.5 Location of Study

The main area of interest lies along Jackrabbit Trail between FRS#3 and FRS#4, from approximately Roosevelt Street to Glendale Avenue, and includes the jurisdictions of the Town of Buckeye and unincorporated Maricopa County. The immediate watershed area contributing to the channel extends west to Tuthill Road, and north to FRS#3. Additionally, the watershed area includes all areas, which drain into the FRS#3 from the White Tanks Mountains, east to the Perryville Road alignment and north to McMicken Dam, near the Cactus Road alignment.



## 2 DESIGN CONSIDERATIONS

### 2.1 Introduction

The White Tanks Flood Retarding Structure No. 3 (FRS#3) Outfall Channel will provide an outfall for the FRS#3 Principal Spillway flows. This conveyance channel will extend south from the Principal Spillway at FRS#3 to the existing FRS#4 inlet channel north of McDowell Road. The District recently constructed a new Principal Spillway for FRS#3 at the east end of the dam, and has a design for a new emergency spillway at the west end.

The channel alignment will meander, where possible, to maintain a pleasing aesthetic view, and will serve as a multi-use trail connection. The Design Report and 30% Plans were prepared by Hoskin-Ryan for the District (Refs. 34, 35). The project was broken into nine reaches, each with its own channel cross-section and right-of-way requirements. The Final Design phase will use the 30% Design Plans as the basis for design.

The 30% Design was based upon accepting the full discharge from the Principal Spillway located at the east end of FRS#3. In order to provide flexibility for the dam operations for both FRS#3 and FRS#4, a wasteway was shown which would allow releases from the Principal Spillway to be directed southward along the west side of the Beardsley Canal. Prior to the Value Analysis, District staff decided that a single 48-inch gated outlet from the Principal Spillway could meet these needs (See Appendix B).

The Outfall Channel will be designed to convey 285 cfs that occurs at an elevation head of 1,216 feet (NAVD 88). This is the outflow from a single 48-inch pipe (west pipe) under maximum head from the Probable Maximum Flood (PMF). The wasteway flows from the east pipe will be for a discharge of 221 cfs through the 48-inch gated outlet. This flow will occur when the water surface elevation is at the crest elevation of the emergency spillway.

The FRS#4 inlet channel is a concrete-lined channel which extends from south of I-10 to north of McDowell Road. North of the existing concrete-lined channel, the Jackrabbit Channel is a series of unlined channels and ditches of varying dimensions and capacities. Between Missouri Avenue and the Bethany Home

Road alignment, natural drainage patterns continue across the Jackrabbit Trail alignment from west to east. North of the Bethany Home Road alignment, the predominant land slope is to the east, towards the Beardsley Canal. An overchute structure just south of Bethany Home Road conveys runoff, which originates on District property, across the canal.

### 2.2 FRS#3 Remediation Project

The District has recently completed improvements to the FRS#3 dam as a part of the Phase 1 Dam Remediation (Ref. 52). The modifications included strengthening of the dam to mitigate for the potential of a subsidence and fissure zone through the area. Other improvements included the installation of a new Principal Spillway at the east end of the FRS. The Principal Spillway consists of two 48-inch diameter gated pipe outlets and a riser tower connected to the western pipe. Currently, these pipes would discharge floodwaters along the west side of the Beardsley Canal. The floodwater would flow southward until it crosses the Beardsley Canal at an existing overchute south of Bethany Home Road.

A stockpile of dirt excavated from the FRS#3 North Inlet Channel contains an estimated 500,000 cubic yards of soil. This material, along with additional excavation from within the channel, will be used for landscape mounding and screening of the dam. Design of the Phase 2 Dam Remediation Plans (Ref. 53) is complete and the project bid in early 2010. The Phase 2 plans include structure modifications to the west end of FRS#3 and grading for a new emergency spillway. The improved emergency spillway will contain the PMF flows and train them toward the southeast.

EPG prepared Landscape Design Plans (Ref. 53) that included mounding to help conceal the FRS from view from the future Jackrabbit Parkway and Jackrabbit Trail/Bethany Home Road. These plans might be adapted for use on the Reach 9 section of the Outfall Channel. The free form shape of the grading will help to break up the straight-engineered lines of the dam. Variable sideslopes on both sides of the channel in this reach will be evaluated.



### 2.3 Jackrabbit Trail and Jackrabbit Parkway

A recent study by MCDOT (Refs. 10, 11) proposed a new highway, referred to as the Jackrabbit Parkway, which follows an alignment along Perryville Road and then crosses Jackrabbit Trail north of Missouri Avenue. This parkway will be considered in the Final Design; however, no improvements will be made since the exact alignment has not been established. In another MCDOT study, the right-of-way width for the Jackrabbit Trail was identified as 130 feet in width; however, Jackrabbit Trail is currently termed as a "Road of Regional Significance" (RRS) by MCDOT, which means that a right-of-way width of 140 feet is desirable. Planning studies by MCDOT indicate that the Jackrabbit Parkway will ultimately assume this designation and therefore Jackrabbit Trail will be re-classified.

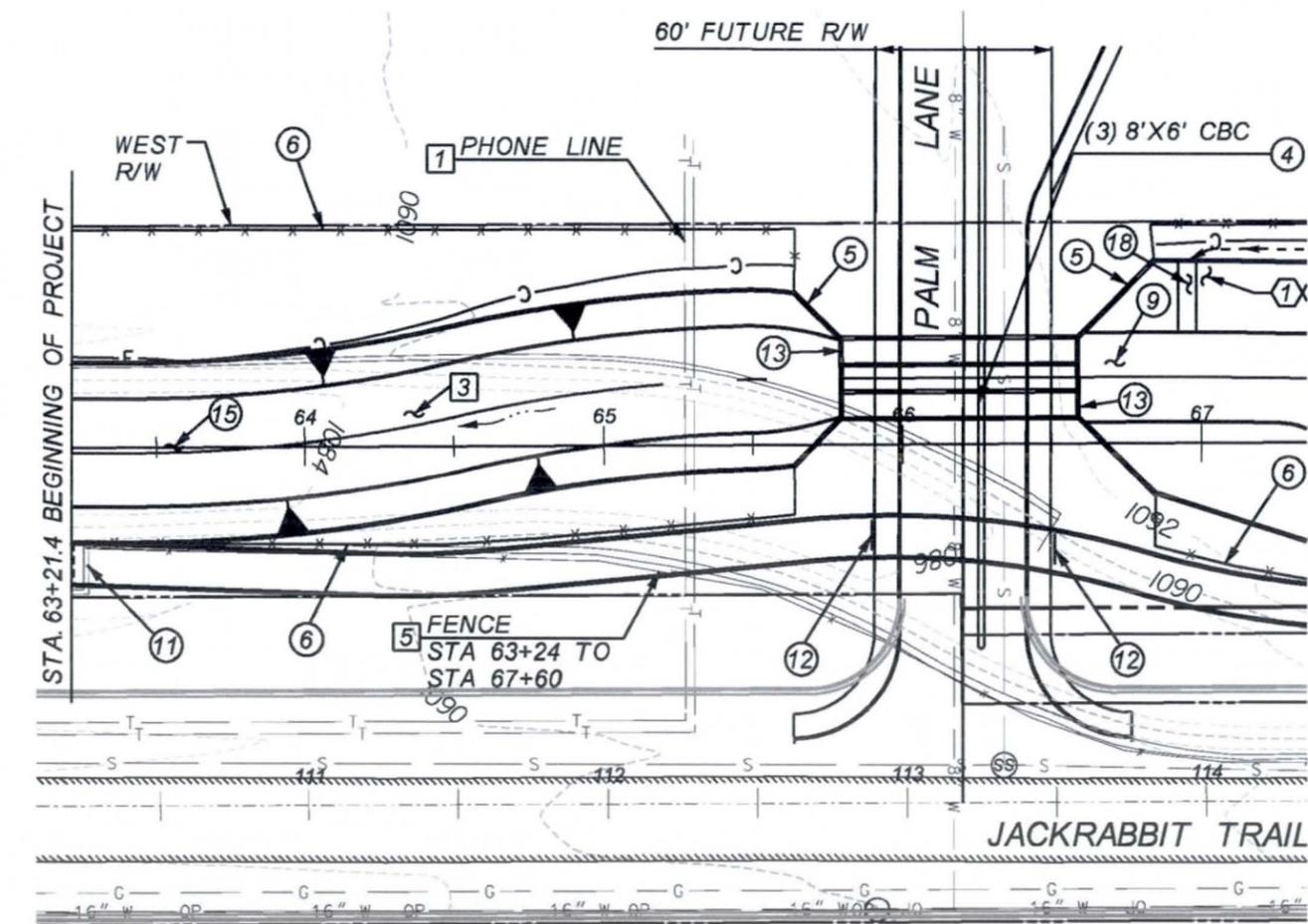


FIGURE 3 – BUCKEYE PARK AND RIDE PALM LANE ENTRANCE

A procedural step by the Town of Buckeye is necessary to remove the designation of RRS. Discussions should be held with the Town of Buckeye and MCDOT to resolve the ultimate requirements.

### 2.4 Buckeye Park and Ride

The Town of Buckeye plans to solicit proposals to prepare design plans for a new Park and Ride facility. This 5-acre site will be located on a 6.88-acre parcel (MCR 502-34-017L) on the northwest corner of Jackrabbit Trail and Palm Lane. Palm Lane, which does not currently exist, will be constructed with the Park and Ride project. A new culvert crossing will be necessary along with a segment of concrete channel at the outlet. The District is in the process of forming an Intergovernmental Agreement (IGA) with Buckeye to coordinate the design and construction of the culvert and channel. Some temporary channel improvements will be necessary at the upstream end of the culvert.

### 2.5 Buckeye Sewer Improvement Project

Final Design Plans are complete and construction is underway for a sewer extension within Jackrabbit Trail from approximately Roosevelt Street to 1,300 feet north of Indian School Road. The new 12- to 15-inch sewer line will intercept future lateral extensions to the west. Sewer lateral extensions should be designed with each culvert crossing of the major side streets. A future extension of this line from Indian School Road north to Bethany Home Road should be considered in the Final Design.

### 2.6 Operations and Maintenance Road

Where right-of-way will not be too constrained, the Operations and Maintenance (O&M) road will meander to align with the sideslope contours and will be placed at the top of channel slope on both sides of the channel. The O&M road will also serve as the Multi-Use Trail for the project and will provide a connection to the Maricopa Regional Trail, Segment 35 (Ref. 37). Fencing, gates, or removable bollards will be used to limit access to the



channel and yet still maintain the trail use. Decomposed granite, with a stabilizer to reduce erosion and dust, may be used to help blend to the surroundings.

## 2.7 Channel Scour and Erosion Protection

The natural slope along the existing Jackrabbit Channel alignment is steep enough to cause flow velocities in excess of 3 feet per second. Drop structures of 2.5 feet in height were specified in the 30% Design Plans (Refs. 34, 35) providing an overall design bed slope of 0.0010 ft/ft. They are shown as a sloped concrete transition set at a maximum slope of 20 percent, allowing maintenance vehicles to drive between channel segments. The District's O&M personnel have indicated that access ramps are an important feature and that the grade should not exceed a slope of 6:1. In the 30% Design, a riprap transition was proposed downstream of each grade control structure, to force a hydraulic jump and slow the flow velocity. The rock riprap may pose a challenge to the passage of maintenance vehicles.

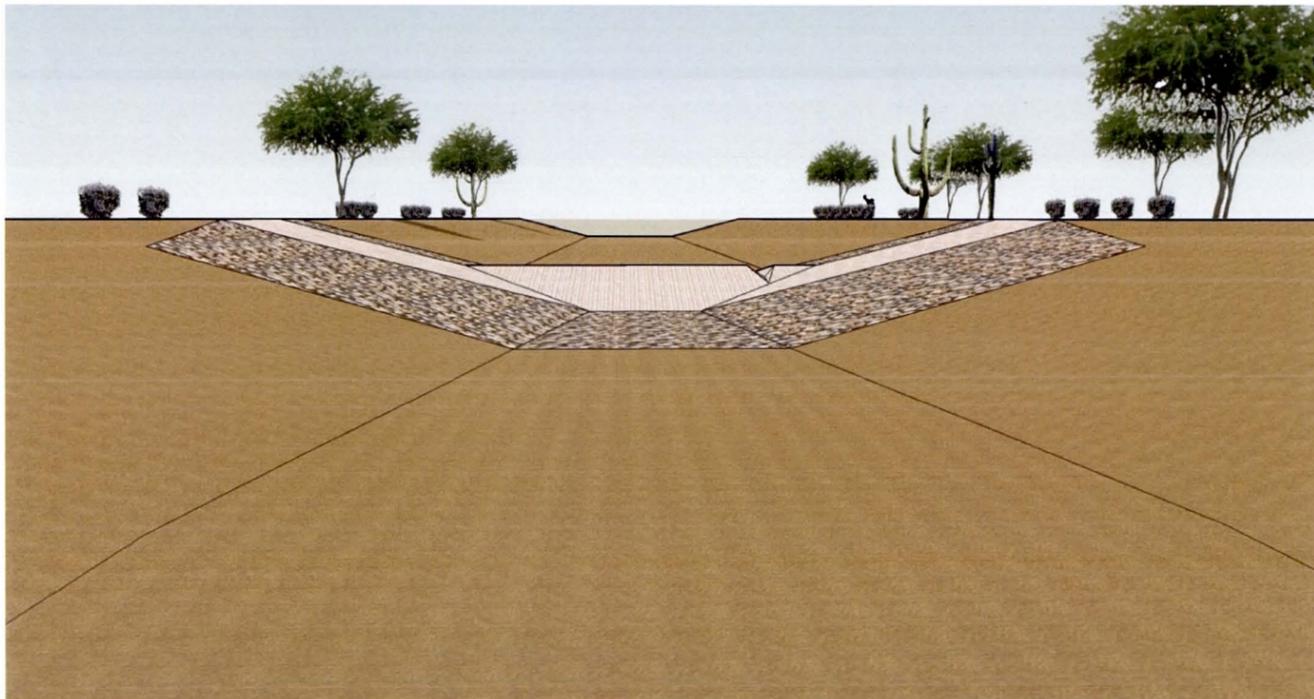


FIGURE 4 – TYPICAL GRADE CONTROL STRUCTURE LOOKING UPSTREAM IN THE CHANNEL

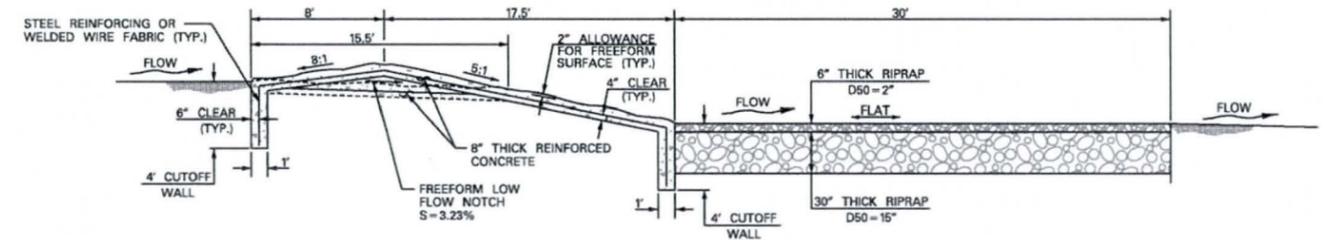


FIGURE 5 – CROSS-SECTION THROUGH GRADE CONTROL STRUCTURE

A low flow thalweg (notch) will be provided in the weir crest to allow smaller flows to pass without affecting the maintenance vehicle path. Additionally, the position of the low flow thalweg along the weir crest may be varied from structure to structure, allowing the low flows to create a more natural meandering wash appearance along the length of the channel.

Landscape and aesthetic treatments will be incorporated into the Final Design. Boulders, colored concrete, aggregate surfaces and form liners will be explored as options to improve the appearance of these structures. The earthen banks of the channel will be protected from rill erosion with gravel mulch and hydro seeding.

## 2.8 Side Drainage Inlets

Local washes and drainage from the west enter the current channel along Jackrabbit Trail. This drainage will be handled in a manner that eliminates erosion and prevents migration outside of District property. The 30% Design shows the use of concrete spillways to control erosion. Other methods will be explored that can minimize structures and be compatible with adjacent properties. The spillways will be designed to coincide with the grade control structures, where possible, to minimize the use of concrete and riprap. Alternative measures will be explored for a range of design flows.



## 2.9 Culvert Crossings

Culverts will be used where the channel alignment crosses roads. District policy does not allow for funding of the culvert construction to the full build-out length, therefore the culverts will be built to accommodate the existing roadway or right-of-way widths. Grade control structures will be built at most culvert inlets in order to reduce the need for grade control structures.

## 2.10 Reach 6

Within the Litchfield Heights subdivision, several washes collect from watersheds to the west and combine in a drainage channel on the west side of Jackrabbit Road. This drainage collects behind berms that parallel Jackrabbit Road and is conveyed south through two concrete box culverts. Future widening of Jackrabbit Trail may interrupt the channel and culverts. A means to intercept this drainage and convey it within the new channel is desirable. Additional conveyance capacity should help reduce the existing floodplain in the area.

At approximately Jackrabbit Trail and Minnezona Avenue, two existing earthen channels merge with the culvert structure. Flowline elevation differences between the three channels require the design of a complex junction structure. The 30% Design proposed two energy-dissipating structures at this location. Alternatives for Reach 6 are explored further in Section 6.1 of this report.

## 2.11 Reach 7

The right-of-way width available within Reach 7 limits the amount of channel meander and bottom width. According to the 30% Design, an existing screen wall that separates Jackrabbit Estates from Jackrabbit Trail will be removed. Removal of the theme wall around the project would cause disruption of the existing landscape and irrigation systems. In places, the right-of-way is not wide enough to accommodate a full maintenance road; therefore, the use of the local streets within the subdivision was proposed.

In a meeting with the HOA and Shea Homes (developer of the project), it appears that there is reluctance for the new channel to be integrated into the development. The HOA appears to prefer to wall the development from the

channel. Other alternatives to reduce the impact on this development should be pursued and are discussed in Section 6.1 of this report.

## 2.12 Reach 9

### 2.12.1 Principal Spillway Channel

Reach 9 lays between the FRS#3 Principal Spillway and the Bethany Home Road alignment. A coordination meeting with ADWR and NRCS indicated that their approval would not be necessary if there is no impact to the operation of the dam structure. The design as presented in the 30% Design Plans will need to meet USACE and FEMA criteria for levee design, CFR 65.10. The 30% Design Plans show an earth embankment along the south bank. This embankment will need to be designed in accordance with the USACE's levee requirements, and therefore a minimum of 3 feet of freeboard should be provided for the 100-year event. The north bank will not require the same freeboard but should slope toward the channel. Landscape mounds will be placed in a manner similar to that shown for the FRS#3 rehabilitation project (Ref. 51) in order to mask the appearance of the dam. Alternative design options for this reach will be explored, including widening of the berms to remove the restrictions placed on the design by classification as a dam or levee.

### 2.12.2 Emergency Spillway

The 30% Design Plans show the channel crosses under the emergency spillway via a concrete box culvert. The design of this box culvert needs to be integrated into the spillway training dike design which will be built with the Phase 2 Dam Remediation (Ref. 53). Since the culvert will interrupt the training dikes which will be built, methods to protect against erosion will need to be explored. The NRCS approved SITES model for the emergency spillway will need to be revised.



### 2.12.3 Earth Fissures and Subsidence

A geotechnical investigation performed by AMEC (Ref. 2) as part of the dam remediation project indicates that there is the potential for subsidence and fissures in the area of FRS#3. If subsidence or fissuring were to occur, the channel in Reach 9 could be vulnerable. Subsidence risks are discussed further in the Geotechnical Report for this project (Ref.61). The 30% Design Plans included a contingency item for the inclusion of a hardened structure into the Outfall Channel project. Reach 9 Alternatives are discussed further in Section 6.2 of this report.

### 2.12.4 Principal Spillway Wasteway

The Structures Management Branch required the inclusion of a wasteway for the Principal Spillway. The wasteway structure currently shown on the 30% Design Plans consists of a spillway and a gated structure within the Reach 9 channel. Operating conditions for the wasteway might occur if the downstream outfall channel is not complete, or if FRS#4 is unable to accept additional discharge.

Since preparation of the 30% Design Plans, the Structures Management Branch recommends that the wasteway is eliminated. Instead, it is proposed to direct the eastern outlet pipe toward the Beardsley Canal wash and the western pipe to the outfall channel. An evaluation of the impact to the Beardsley Canal wash downstream of the Principal Outlet is included in Section 4.3 of this report.



### 3 HYDROLOGY

HEC-1 models were prepared for the existing conditions and “future conditions with project-in-place.” The existing conditions model was created in December 2009 and was based upon the *Loop303/White Tanks ADMPU Area Hydrologic Analysis* (the ADMPU AHA) submitted by HDR on September 4, 2009. The future conditions model was prepared in June 2009 for the *White Tanks FRS No.3 Outfall Channel 30% Design Report* (Refs. 34, 35), and was based upon the ADMPU AHA submitted by HDR on March 9, 2009. HRC reviewed the ADMPU AHA models and has confirmed that the recent updates do not affect the validity of the models previously prepared.

#### 3.1 Existing Conditions with Project in Place

Existing conditions models for the 10-year and 100-year storm events were created based upon the “existing conditions with CIP” model (ECIP-MB2.dat) of the ADMPU AHA. Modifications made by HRC include updates to NOAA 14 precipitation, the stage-storage-discharge curve of FRS3, retention volumes, and routing channel geometries.

To reflect the precipitation difference between the “mountain terrain” and “range terrain,” the watershed of Major Basin 02 in the ADMPU AHA was divided into two basins. The FRS#3 major basin covers the watershed area upstream of White Tanks FRS#3, with a 100-year point precipitation of 4.016 inches and a 10-year point precipitation of 2.572 inches. The Jackrabbit Corridor major basin covers the watershed area downstream of FRS#3, with a 100-year point precipitation of 3.661 inches and a 10-year point precipitation of 2.353 inches. Separate HEC-1 models were created for each major basin. HEC-DSS was employed for data transfer between the two models.

The stage-storage-discharge curve for the “future condition,” which is defined as the condition with the Principal Spillway open and the gated outlet closed, was used to update the ADMPU AHA model for FRS#3

storage routing. Additional information regarding this update is documented in the *White Tanks FRS No.3 Outfall Channel 30% Design Report* (Refs. 34, 35).

A retention volume of 12.5 acre-feet was applied to the Pasqualetti Mountain Ranch in the ADMPU AHA model. The Final Plat indicates on-lot retention; however, the current development does not appear to provide on-lot retention, and does not have room for significant retention storage. It is not clear whether on-lot retention will be required for future phase, therefore, to be conservative, the retention diversion was removed from the model.

The channel proposed by the Preliminary Design Plans prepared by Gannett-Fleming (Ref. 30) was used for channel routing in the ADMPU AHA model. Updates were made to reflect the channel geometry proposed by the 30% Design Report (Refs. 34, 35).

The computed existing conditions discharges along proposed channel are shown in Table 1.

#### 3.2 Future Conditions with Project in Place

A future conditions model for the 10-year storm event was created based upon the “future condition with CIP” model (Future\_CIP\_MB02.dat) of the ADMPU AHA. Modifications made by HRC include updates to land use types, retention volumes, NOAA 14 precipitation, and routing channel geometries. Additional information regarding the updates is documented in the *White Tanks FRS No.3 Outfall Channel 30% Design Report* (Refs. 34, 35). The computed future conditions discharges along the proposed channel are shown in Table 1.



Table 1: HEC-1 Model and Design Discharges

Reach	Existing Conditions			Future Conditions			Design Discharge
	Concentration Point	100-Year	10-Year	Concentration Point	100-Year	10-Year	
Reach 1	CPW37	1065	346	CPW38	1549	397	1549
Reach 2	CPW36	935	286	CPW37A	648	222	700
Reach 3	CPW36	935	286	CPW36	670	241	700
Reach 4	CPW35	853	294	CPW35	701	302	700
Reach 5	CPW33	792	293	CPW33	795	360	800
Reach 6	CPW33	792	293	CPW33	795	360	800
Reach 7	CPW28A	511	211	CPW28A	664	81	700
Reach 8	CPW28A	522	211	CPW28A	664	81	700
Reach 9	CPW21A	187	54	CPW21A	218	87	285

### 3.3 Probable Maximum Flood (PMF) for FRS#3

The Natural Resource Conservation Services (NRCS) developed Probable Maximum Flood (PMF) hydrographs for various Probable Maximum Precipitations (PMP) using TR-20. The TR-20 model prepared by NRCS was updated by URS for the *FRS3 Remediation Project* (Refs. 49, 50). The FRS#3 reservoir routing results for future conditions indicate that the 6-hour local PMP will cause a maximum reservoir elevation of 1216 feet (NAVD 88), with a corresponding Principal Spillway discharge of 284 cfs. Therefore, the design discharge for Reach 9 was set at 285 cfs.



## 4 HYDRAULICS

Soils information collected during the *White Tanks FRS No.3 Outfall Channel 30% Design Report* (Refs. 34, 35) indicates that a sandy loam covers the project alignment. Based upon guidelines in the District Hydraulics Manual (Ref. 17), a maximum design velocity of 3 feet per second was selected for the unlined portions of the channel. Alternatives other than an unlined channel were identified for Reaches 6, 7, and 9 during the Value Analysis Session held by the District. This report documents the hydraulic analysis for these alternatives.

### 4.1 Sedimentation and Scour Analysis

Although the non-erosive velocity method was selected as the criteria for the 30% design, it is also recognized that the equilibrium slope method documented in the District's *River Mechanics Manual* (Ref. 29) is potentially applicable. This report documents the equilibrium slope calculations performed using available soil data.

At each tributary, the sediment yield was calculated using the District's DDMSW program (beta version 4.5.3). The DDMSW program calculates wash load using the Modified Universal Soil Loss Equation (MUSLE) method and bed load using the Zeller-Fullerton equation, as documented in the District's *River Mechanics Manual* (Ref. 29). The results are provided in Appendix E. Sediment-trapping basins will be designed to capture sediments conveyed by major tributary washes approaching the channel from the west.

#### 4.1.1 Soil Data

Alpha Geotechnical and Materials, Inc., geotechnical subconsultant for this project, has collected 60 soil samples along the proposed channel alignment, 5 soil samples at the stockpile, and 12 soil samples within the sandy bottom of the Jackrabbit Wash (Ref. 61). This information will be used to determine the equilibrium slope for the channel for both clearwater and sediment laden discharges. The grain size distribution from the laboratory tests indicates that the soil at the design depth of the channel

generally contains about 30% silt, while the soil sample from the existing wash sandy bottom contains less than 10% silt (Ref. 61). The equilibrium slope analysis and sediment yield calculations were conducted using the grain size distribution of the existing wash sandy bottom sample ( $D_{84}=4.0\text{mm}$ ,  $D_{50}=1.2\text{mm}$ , and  $D_{14}=0.2\text{mm}$ ), as this is the existing equilibrium state of the wash.

#### 4.1.2 Equilibrium Slope

Per discussion with District staff, the channel was designed based on the permissible velocity of 3 feet per second. Equilibrium slope analysis using the Schoklitsch equation was used to verify the channel design slope for clearwater flows. For lower discharge flows, sediment will trap behind the FRS, however, at full discharge, the outlet pipes may carry sediments. The channel or pipe slope from the Principal Spillway, west along the Reach 9 segment, will be steepened by an additional one foot (from 0.10% to 0.129%) to allow for the potential of future differential subsidence as identified by Geological Consultants, Inc. (Ref.61). The PMF outflow of 285 cfs from the west Principal Spillway, or the 10-year flow from the HEC-1 models, whichever is larger, was used for the equilibrium slope analysis for each reach. The results are provided in Appendix E.

### 4.2 Channel Hydraulics

The hydraulic performance of alternatives for Reaches 6, 7, and 9 were analyzed using FlowMaster and Dodson Hydrocalc (Appendix D). The channel, pipes and culverts have been sized properly to convey the design flows.

In the 30% design, a Manning's 'n' of 0.035 was selected for un-lined earthen channel, and the channel slope was identified to be 0.1% to achieve a non-erosive velocity of 3 feet per second. One of the landscape scenarios could potentially lead to a Manning's 'n' of 0.050 when vegetation is fully established. Accordingly, the channel slope could theoretically be increased to 0.2% for an earthen channel with a non-erosive velocity of 3 feet



per second. With the increase of channel slope, six of 19 drop structures between Reach 2 and Reach 6 could be eliminated. However, it is recognized that Manning's 'n' will vary with the growth of the landscape vegetation and its impact on channel hydraulics need further investigation. The channel will be designed for post-construction and full-growth conditions.

The sensitivity of flow velocities on channel slopes and Manning's roughness was evaluated for Reaches 2 and 3. A narrow cross-section with a 30-foot channel bottom and 4:1 side slope and a wide cross-section with a 44-foot channel bottom and 6:1 sideslope were selected for analysis. The results indicate that the flow velocity will fall below 3 fps for a design channel slope of 0.1% with  $0.025 < n < 0.035$  and for a design channel slope of 0.2% with  $0.035 < n < 0.050$ . The results are included in Appendix E.

#### 4.3 Wasteway Flows to Beardsley Canal and Wash

One of the two Principal Spillway pipes (east pipe) will remain for use as an emergency wasteway. This wasteway will be used if the operation of FRS#4 does not allow a discharge, if construction of the outfall channel is incomplete, or if an earth fissure develops. This project maps the inundation effects which could result from a discharge of 221 cfs from the gated outlet when the water surface elevation in the FRS #3 reservoir reaches the crest of the emergency spillway, i.e. 1,212 feet (NAVD 88). The potential flood inundation area occurs along the west side of the Beardsley Canal, southward toward an overchute that is located south of Bethany Home Road.

A steady flow HEC-RAS model was prepared using cross-section geometry obtained from the one-foot aerial mapping prepared by Cooper Aerial in December 2009 (Appendix H). Cross-sections were located along the wash every 200 feet except at the Beardsley Canal overchute and where trails cross the wash. Ineffective flow areas were identified at some cross-sections where water could pond. Due to the density of the vegetation, a Manning's 'n' roughness coefficient of 0.045 was chosen for the entire wash along the Beardsley Canal. The results from the HEC-RAS model were used to delineate the floodplain shown in Figure 6.

The principal spillway inundation area was mapped by JE Fuller using Flo2D, as part of the FRS#3 Emergency Action Plan EAP) study (Ref. 62). The EAP indicates that the flow of 221 cfs would not be contained within the Beardsley Wash and would overtop Beardsley Canal. To resolve the difference in results, a sample of the Flo2D grid was compared with the aerial mapping (Appendix J). The 50'x50' square grid used in the Flo2D model does not provide sufficient precision to represent the Beardsley Wash, whose total width is approximately 50 feet. The Flo2D model underestimated the existing wash capacity and, as a result, overtopping of the Beardsley Canal was predicted. The HEC-RAS model provides a more accurate model of the wash capacity and shows that overtopping of the canal will not occur.



FIGURE 6 – WASTEWAY FLOW INUNDATION AREA



## 5 DESIGN ELEMENTS

The 30% Design Plans were prepared without input from a landscape architect and were based upon the need for a functional channel system. During the Value Analysis, several design elements were discussed that could improve the aesthetics and maintenance of the channel and structures. Landscape concepts have been developed in conjunction with EPG and are further discussed in the *Landscape Architecture Pre-Design Report* (Ref. 12).

### 5.1 Culverts

The 30% Design Plans proposed ADOT concrete box culvert throughout the project in the size range of 2-10' x 6' and 3-10' x 6' were proposed in the 30% Design Plans. A minimum height of 6-feet is recommended by MCDOT due to maintenance access. These structures have gained popular support from municipalities throughout the country and are universally used.

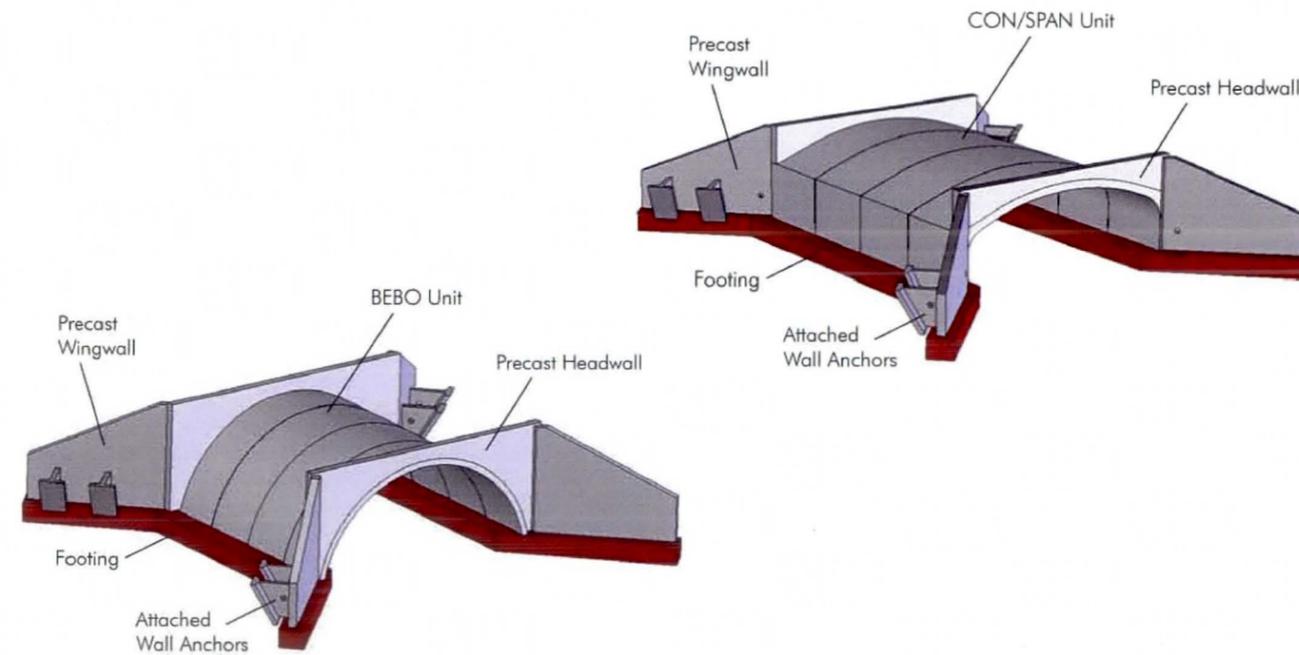


FIGURE 7 – CON-SPAN AND BEBO PRE-CAST CULVERT OPTIONS

During the Value Analysis, the use of a pre-manufactured culvert system was proposed. The use of these may have some benefits over a cast-in-place culvert system. The road network in this area is fragmented and there are houses that may only have one paved point of access. Prolonged shutdowns of roads could be a significant challenge. Pre-cast units have an advantage because they are manufactured off-site and can reduce road closure times. Installation takes less time and there is no concrete cure time to be concerned about.

Pre-cast arch units available from Contech present an alternative that can create a more aesthetic structure economically (Appendix A). The two pre-cast units presented here are the Con-Span and the BEBO unit. Product information from Contech is provided in Appendix A. Initial price quotes from Contech (Appendix A) show a price of \$670/LF for (1) 16'x6' Con/SPAN Precast Arch Culvert installed versus \$1121/LF presented in the 30% Design for a (2) 8'x6' CBC, and \$754/LF for (1) 24'x6' Con/SPAN Precast Arch Culvert installed versus \$1604/LF presented in the 30% Design for a (3) 8'x6' CBC. Pre-cast wingwalls are an option and since they are made to order, formliners and colored concrete can be specified.

### 5.2 Pipe Options

The design discharge for the outfall channel within Reach 9 will be reduced to 285cfs from its original 560 cfs. With a lower design discharge, a pipe option for Reach 9, including underneath the emergency spillway, may be more economically feasible. Since Reach 9 lies within a subsidence and fissure risk zone (Ref. 2), there is the potential for long-term differential settlement.



FIGURE 8 – HDPE WELDED SEAM PIPE



At the Value Analysis workshop, the use of a welded seam HDPE pipe was suggested. Contech has a product called DuroMaxx that has a steel ribbed reinforcement that minimizes pipe deflection. Duromaxx is available in sizes up to 72-inches in diameter. The estimated installed price for 72-inch diameter Duromaxx pipe is \$186/LF. A competing product is Weholite, a profile wall pipe. Product information for both can be found in Appendix A.

### 5.3 Grade Control Structures

The 30% Design shows nineteen (19) grade control structures within Reach 2 to Reach 6. The O&M Division at the District has indicated a desire to be able to drive along the length of the channel. The 30% Design Plans show the use of a sloped concrete grade control structure with a downslope face of 5:1 and a vertical grade change of 2.5 feet. Each grade control structure also has a 30-foot long riprap section to help reduce the flow velocity and to contain the hydraulic jump that will occur. Loose rock riprap of sufficient size to withstand the flow velocities expected will be difficult to traverse with vehicles and may require frequent maintenance.

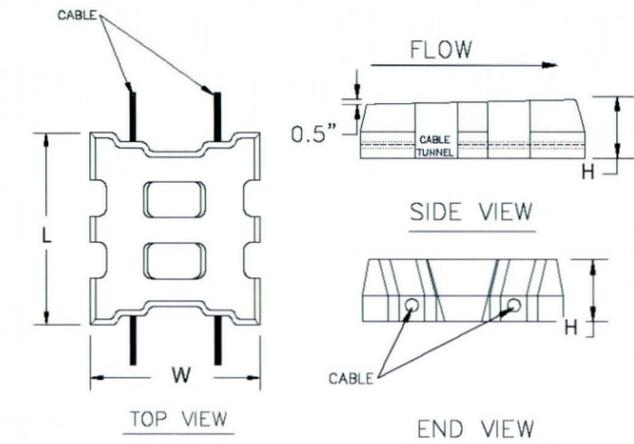


FIGURE 10 – ARMORFLEX BLOCK

An alternative product from Contech that might be usable in this application is called ArmorFlex. This articulated concrete block is tied together with cables to provide a uniform drivable surface. This product could be used in conjunction with the concrete grade control, or it could also be used for the grade control and side drainage spillways. This block is available to order with an integral colored concrete. Block can be open or closed cell and should use a filter fabric below an aggregate base. Cost of ArmorFlex installed is estimated at \$9.04/SF compared to 3-feet of rock riprap at \$7.77/SF and concrete spillway at \$12.41/SF.



FIGURE 9 – ARMORFLEX USED FOR SPILLWAY AND GRADE CONTROL STRUCTURE

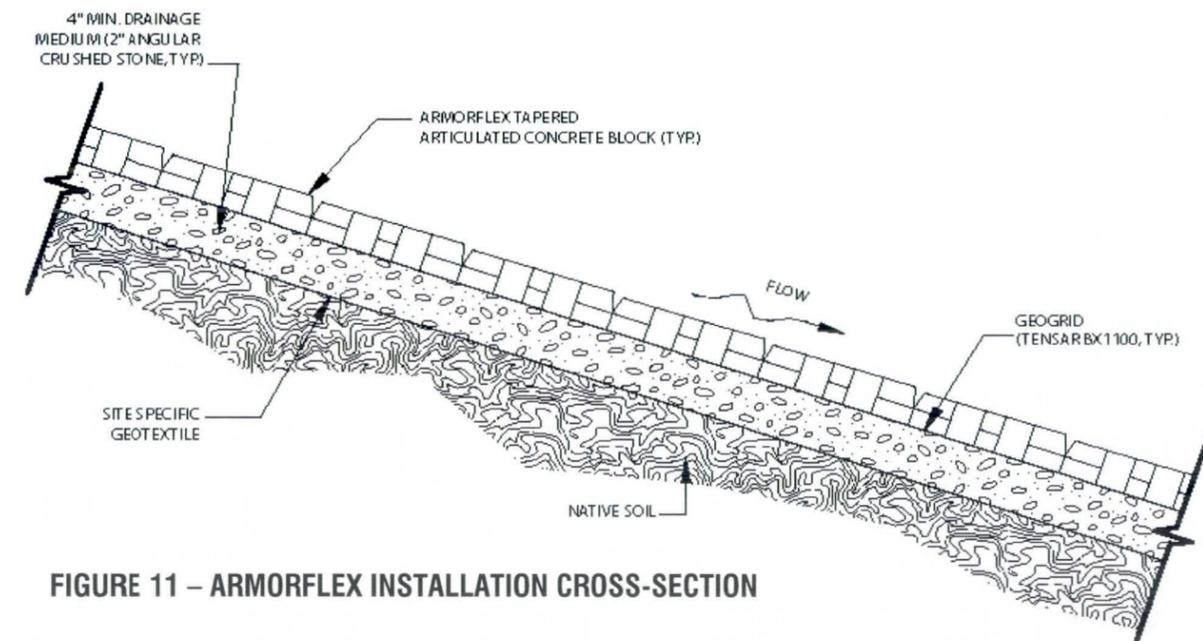


FIGURE 11 – ARMORFLEX INSTALLATION CROSS-SECTION

#### 5.4 Retaining Walls

Where the right-of-way is narrower than desirable to meet the landscape and aesthetic goals of the project, the use of retaining walls may be necessary and is referred to as a “Restricted Channel” (Ref. 12). In addition, in certain locations such as at Jackrabbit Estates or Pasqualetti Mountain Ranch, an O&M road will not fit within the available right-of-way. In order to allow for a channel with variable sideslopes and meander, retaining walls should be considered. Retaining walls should be kept below 2.0-feet in order to avoid the need for fall protection. The 30% Design considered the use of formed cast-in-place concrete retaining walls. Gabion basket retaining walls were discussed at the Value Analysis meeting, however, the O&M Division indicated that they cause maintenance problems and can be subject to vandalism.



FIGURE 12 – TERRACED KEYSTONE WALL SYSTEM



FIGURE 13 – STRAIGHT-FACED AND TRI-PLANE VARIANTS OF KEYSTONE BLOCK SYSTEM

An alternative that was discussed was the use of a dry stack gravity wall system such as Keystone. These types of products allow for significant height of retaining wall with a variety of stone and color finishes.

Another alternative would be to use a colored gunite concrete laid at a 1:1 slope. The surface could be kept rough and the aggregate exposed, and the need for wire mesh could possibly be avoided using a “Fibermesh” mixture of cement and fiberglass. A variable texture can be introduced with a coarse mix design, and it could be scalloped to look like the layers of caliche in the area if done with skill. The relative cost of these alternatives was estimated as follows:

- Formed cast-in-place concrete retaining wall = \$132/LF
- Keystone Block = \$56/LF
- Pneumatically-placed mortar (gunite) = \$34/LF
- Gabion basket (3x3) = \$37/LF



## 5.5 Landscape Integration

Based upon the channel corridor's land context, the landscape design theme for this project is Desert Sonoran. This theme lends itself to a low maintenance low water use landscape that will fit with the natural desert. It is the team's desire to create a conveyance channel that mimics that found within a natural wash system. Natural washes tend to meander, erode, have soft banks and have predominant vegetation along the low flow wash banks. Overbank areas are typically less densely vegetated and differ in plant species. Further discussion of landforms and concepts are provided in the *Landscape Architecture Pre-Design Report* prepared by EPG (Ref. 12).

Four different channel concepts are discussed in the LA Pre-Design Report as follows:

- Natural Form Channel
- Meandered Trapezoidal Channel
- Restricted Open Channel
- Hardened Channel



### 5.5.1 Natural Form Channel

This would consist of a meandered low-flow channel located within a shallow floodplain area with flat-sloped overbank areas. The entire floodplain would be accommodated within the right-of-way using a depressed trapezoidal section. The low-flow channel would be approximately one foot in depth with erodible banks and would be allowed to erode and meander within the overbank areas. As would be typical of many desert washes, vegetation would follow the thread of the low-flow, and thus the fully-grown channel Manning's n value would need to be designed to be high enough to allow the freeboard requirements to be maintained after the vegetation becomes mature.

velocities. The 30% Design was based upon the use of an 'n' value of 0.035 and resulted in nineteen (19) grade control structures with a bed slope of 0.0010 ft/ft. By increasing the 'n' value to 0.050, the same velocity can be held with a bed slope of 0.0020 ft/ft. This bed slope helps to eliminate six (6) grade control structures. The optimum bed slope will be evaluated for a range of flow conditions from a low 'n' value after completion of construction, to a fully-grown in condition. The channel hydraulics will be assessed for a range of flows given the various stages of vegetative growth and the varying soils and locations of caliche as identified by geological Consultants, Inc. and Alpha Geotechnical.

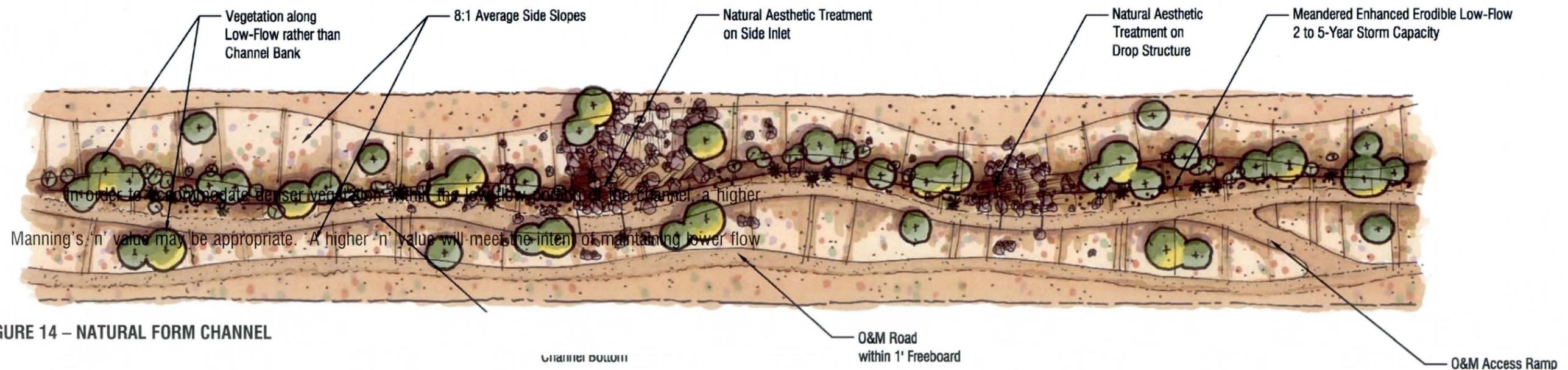


FIGURE 14 – NATURAL FORM CHANNEL



### 5.5.2 Meandered Trapezoidal Channel

The meandered open channel concept is based upon the 30% Design Plans configuration. The channel consists of a uniform bottom width trapezoidal channel section that meanders within a straight right-of-way and thus results in either variable sideslopes or in the top of bank location. The vegetation within this concept is located along the top of bank outside of the freeboard zone and within a landscape setback, where available. A low flow could still be incorporated into this concept.

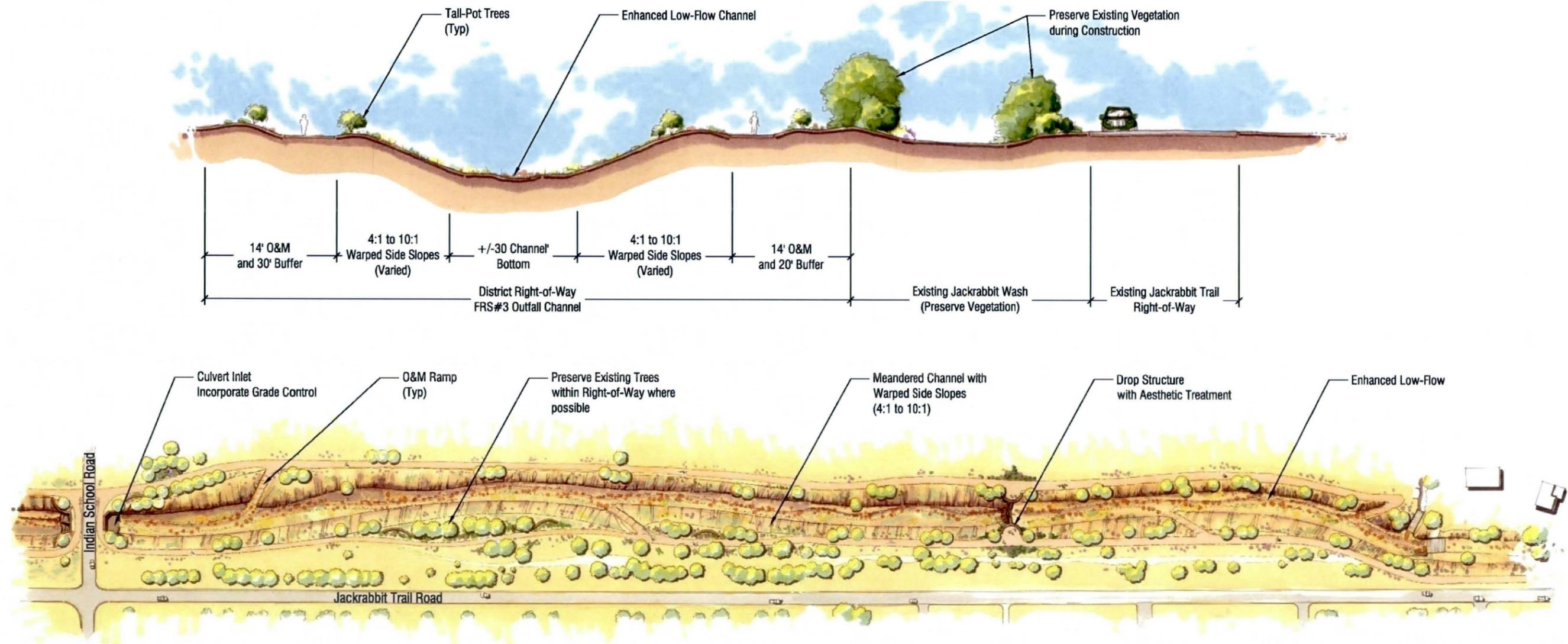


FIGURE 15 – MEANDERED TRAPEZOIDAL CHANNEL



### 5.5.3 Restricted Open Channel

With the Restricted Open Channel concept, the right-of-way width is considered less than optimum (Reaches 2, 3, 4 & 7) which makes the incorporation of meanders and landscape setbacks more difficult. This can be countered to some extent with the inclusion of retaining walls that would vary in location (alternating sides of channel), and in length. Retaining walls would occur more predominantly downstream of grade control structures where the channel depth increases and causes a “pinching-in” of the channel. Retaining wall options are discussed further in Section 5.4 of this report.

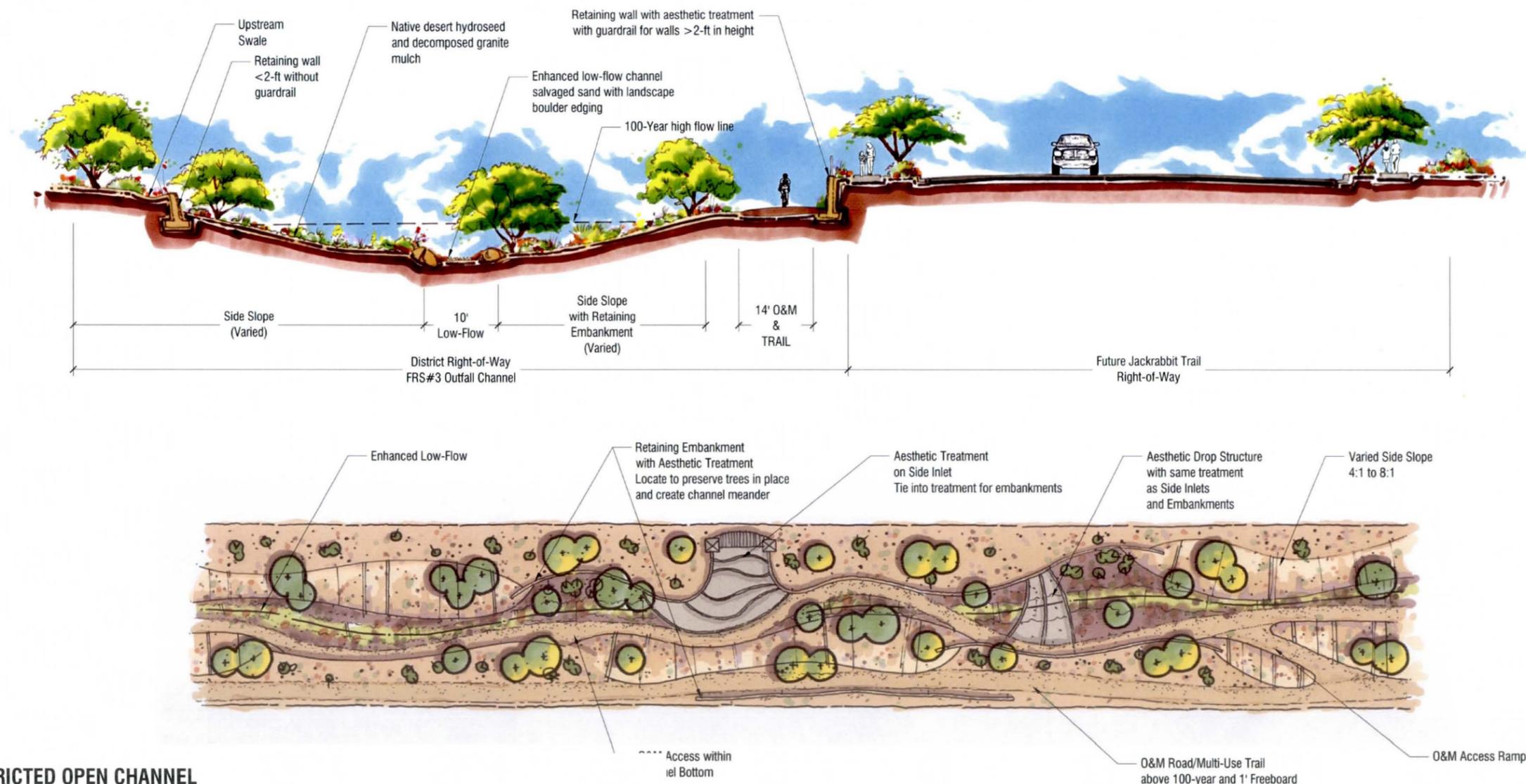


FIGURE 16 – RESTRICTED OPEN CHANNEL



#### 5.5.4 Hardened Channel

A hardened channel would not typically fit into the context of a Sonoran Natural Desert theme, however, its use is considered for Reach 7 through the Jackrabbit Estates. Here, the right-of-way is restricted by several factors including street knuckles, depth of channel, and existing landscape and perimeter walls to the subdivision.

Preliminary discussion with the Jackrabbit Estates HOA indicates a reluctance to assume landscape maintenance responsibilities for a Natural Sonoran Desert theme. If the existing perimeter walls and landscape could remain intact and the channel built within the narrow confines of the existing lots, then the remainder of the open space could be walled from the subdivision and used for vegetative screening. The Jackrabbit Estates HOA may be more willing to maintain the landscape if it is similar to that which exists today.

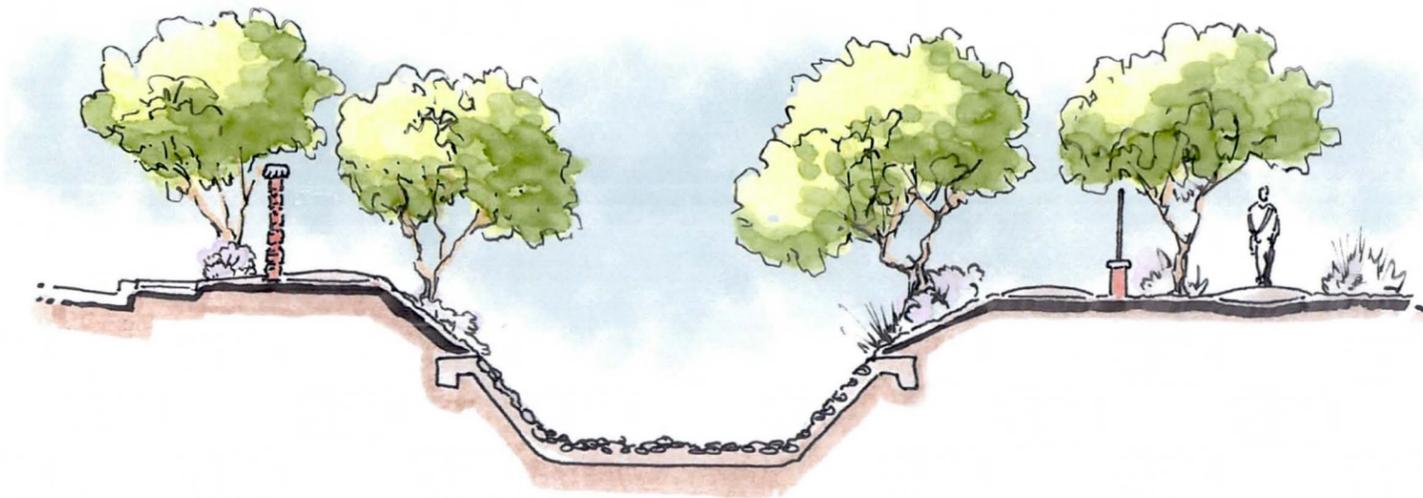


FIGURE 17 – HARDENED CHANNEL



## 6 REACH EVALUATION

Prior to the commencement of the Final Design, a Value Analysis session was held to review the 30% Design Plans (Refs. 34, 35). Many different design concepts were discussed during this session and additional alternatives were conceived for Reaches 6, 7 and 9. Each of these Alternatives is discussed below:

### 6.1 Reaches 6 and 7

Reach 6 extends from an outfall on the west side of Jackrabbit Trail, near Sells Road, north to Camelback Road. The 30% Design Plans show that the channel within Reach 6 lies on the east side of Jackrabbit Trail within a property referred to as Missionary Wings. Reach 7 extends from Camelback Road, north through the Jackrabbit Estates subdivision on the east side of Jackrabbit Trail to the Missouri Road alignment.

Because of discussions at the Value Analysis session and PAAC 1 meeting several other alternatives were evaluated as discussed herein.

#### 6.1.1 Alternative 6/7A

Alternative 6/7A is the plan presented in the *Design Report and 30% Plans* (Refs. 34, 35).

#### 6.1.2 Alternative 6/7B

Alternative 6/7B represents the 30% Design Alternative within these two reaches with the addition of a cross-drainage culvert north of Meadowbrook Avenue. This culvert will alleviate siltation upstream of Meadowbrook Avenue and the cost was added to the Baseline Alternative. Additional retaining walls may be necessary within Reach 7 (Jackrabbit Estates) in order to provide additional channel meander and to allow for continuous maintenance road. The Restricted Open Channel landscape concept is discussed in further detail in the *Landscape Architecture Pre-Design Report* (Ref. 12).

#### 6.1.3 Alternative 6/7C

Alternative 6/7C consists of a closed conduit along the full length of Reach 6 and 7 to replace the open channel through Jackrabbit Estates and avoid the need for right-of-way acquisition through the Missionary Wings property. This alternative would still require side drainage inlets along the west side of Jackrabbit Trail.

#### 6.1.4 Alternative 6/7D

Alternative 6D consists of construction of an open channel on vacant land located on the west side of Jackrabbit Trail and a culvert through Litchfield Heights to replace existing undersized culverts across Minnezona Avenue and Meadowbrook Avenue. Within Reach 7, this alternative would be the same as Alternative 7B.

#### 6.1.5 Alternative 6/7E

Alternative 6E would be the same as Alternative 6B. Within Reach 7, the open channel shown in Alternative 7A would be replaced with an underground conduit.

#### 6.1.6 Alternative 6/7F

Alternative 6F would be the same as Alternative 6B. Within Reach 7, the earthen channel would be replaced with a concrete-lined channel with minimum freeboard requirements. The Restricted Open Channel landscape concept is discussed in further detail in the *Landscape Architecture Pre-Design Report* (Ref. 12).

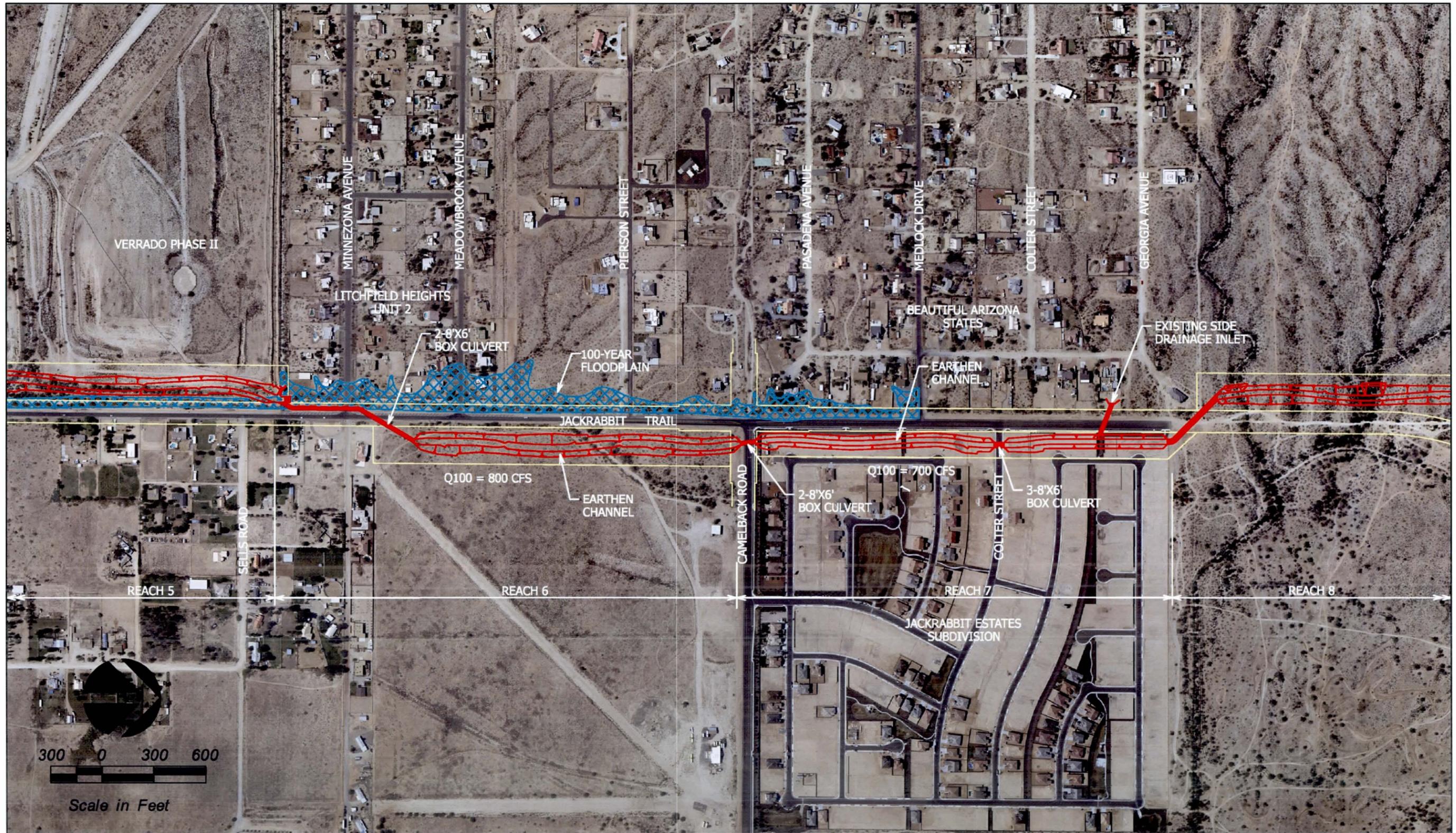


FIGURE 18 – ALTERNATIVE 6/7A

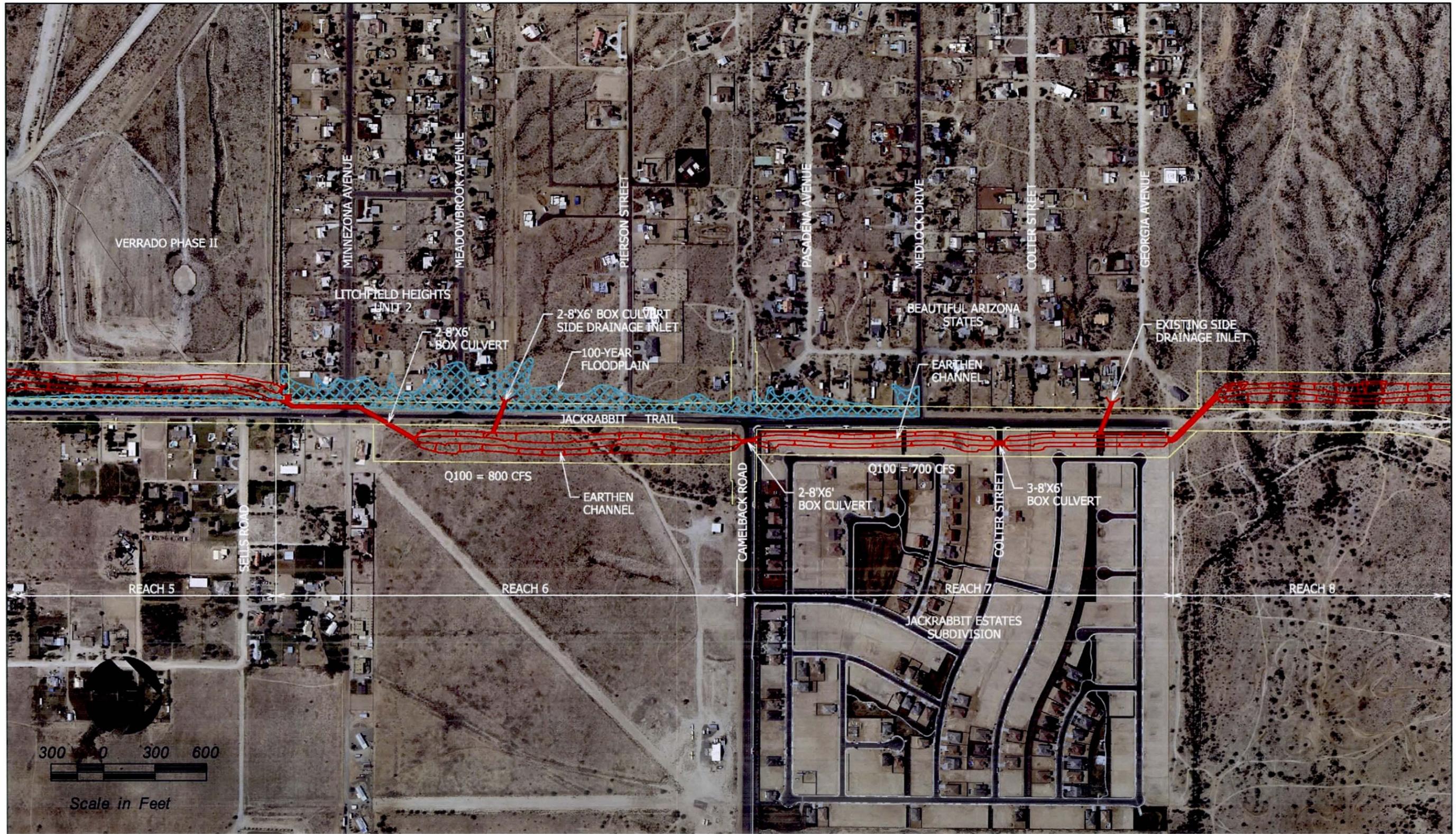


FIGURE 19 – ALTERNATIVE 6/7B

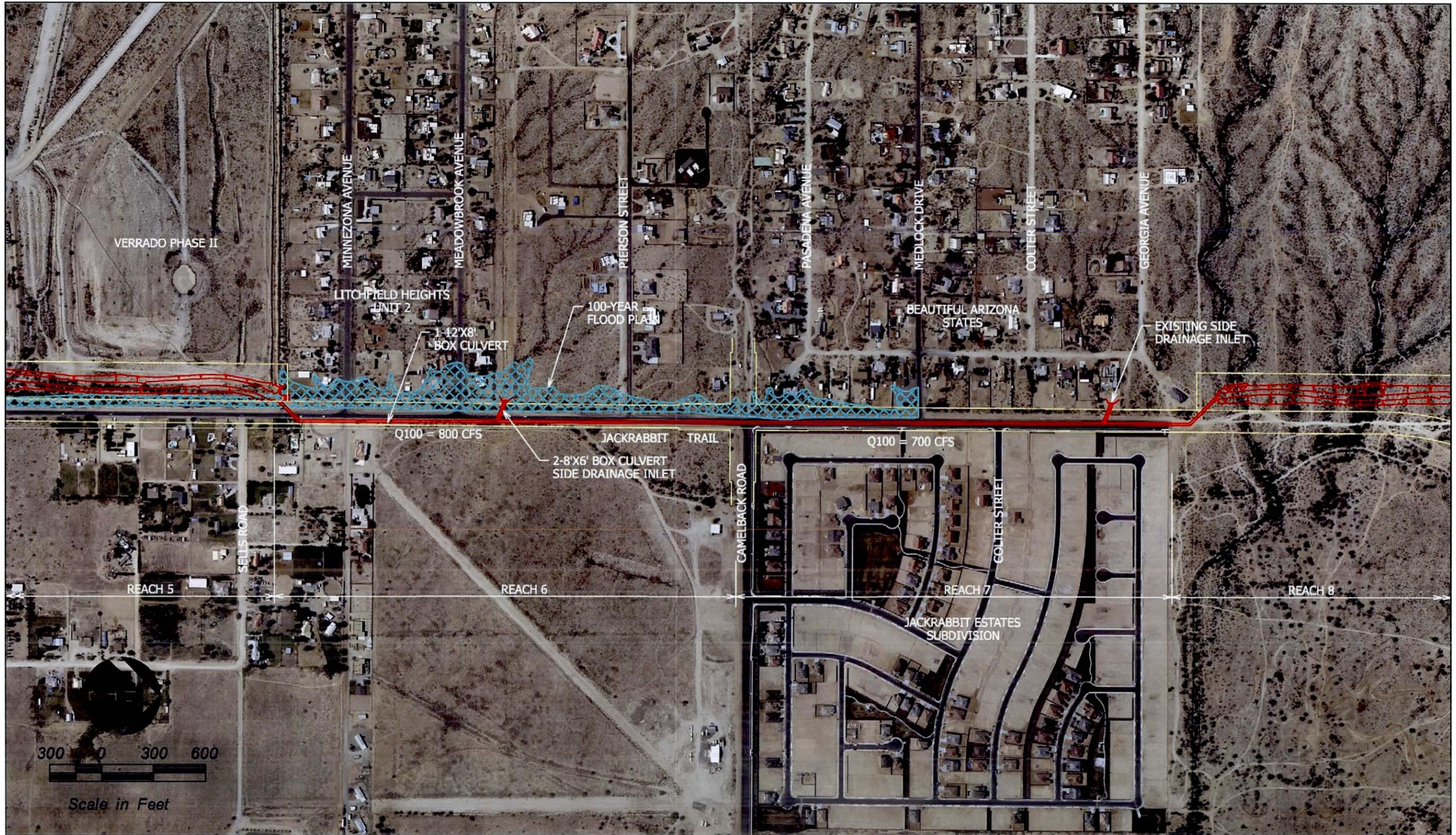


FIGURE 20 – ALTERNATIVE 6/7C

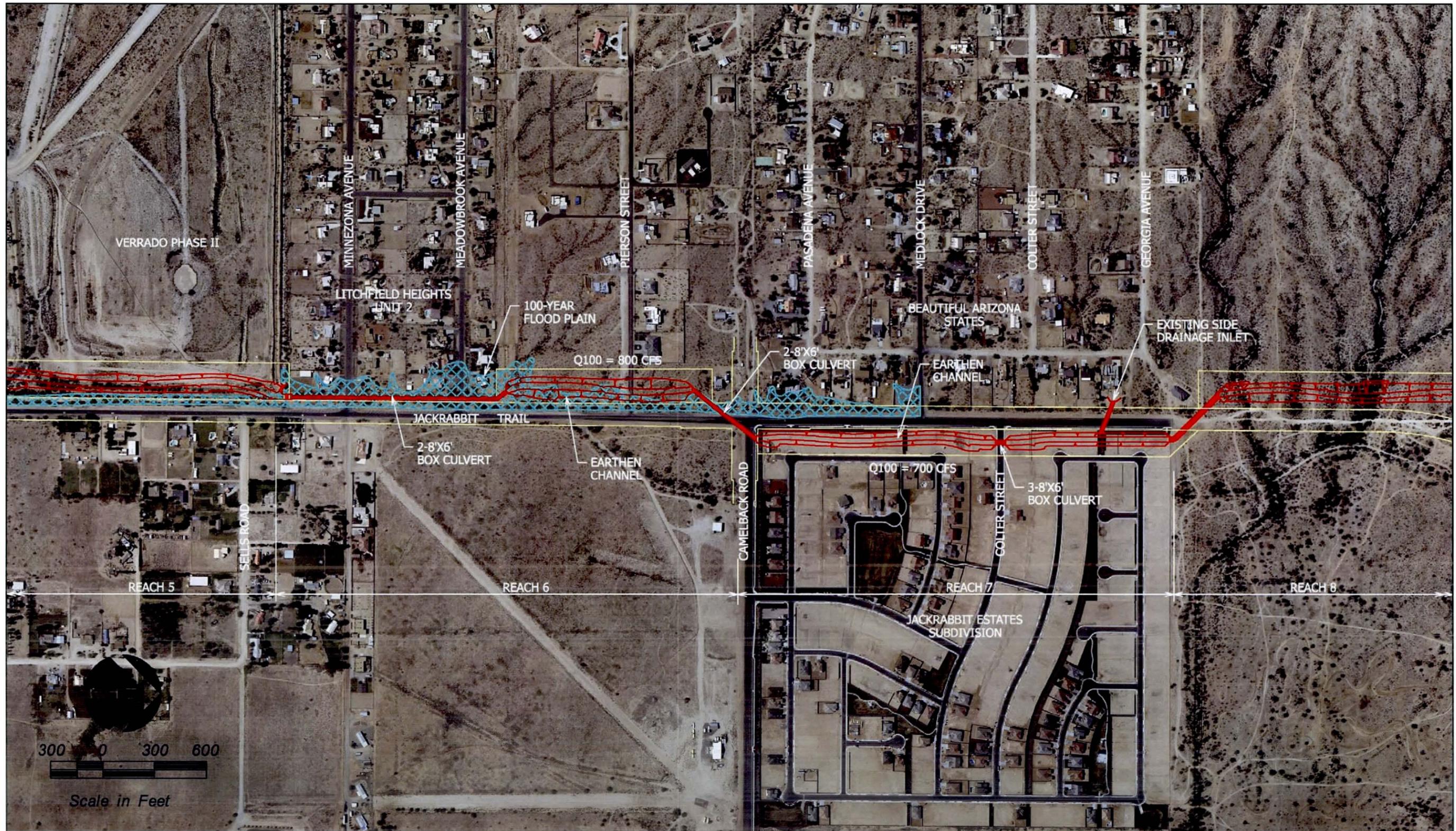


FIGURE 21 – ALTERNATIVE 6/7D

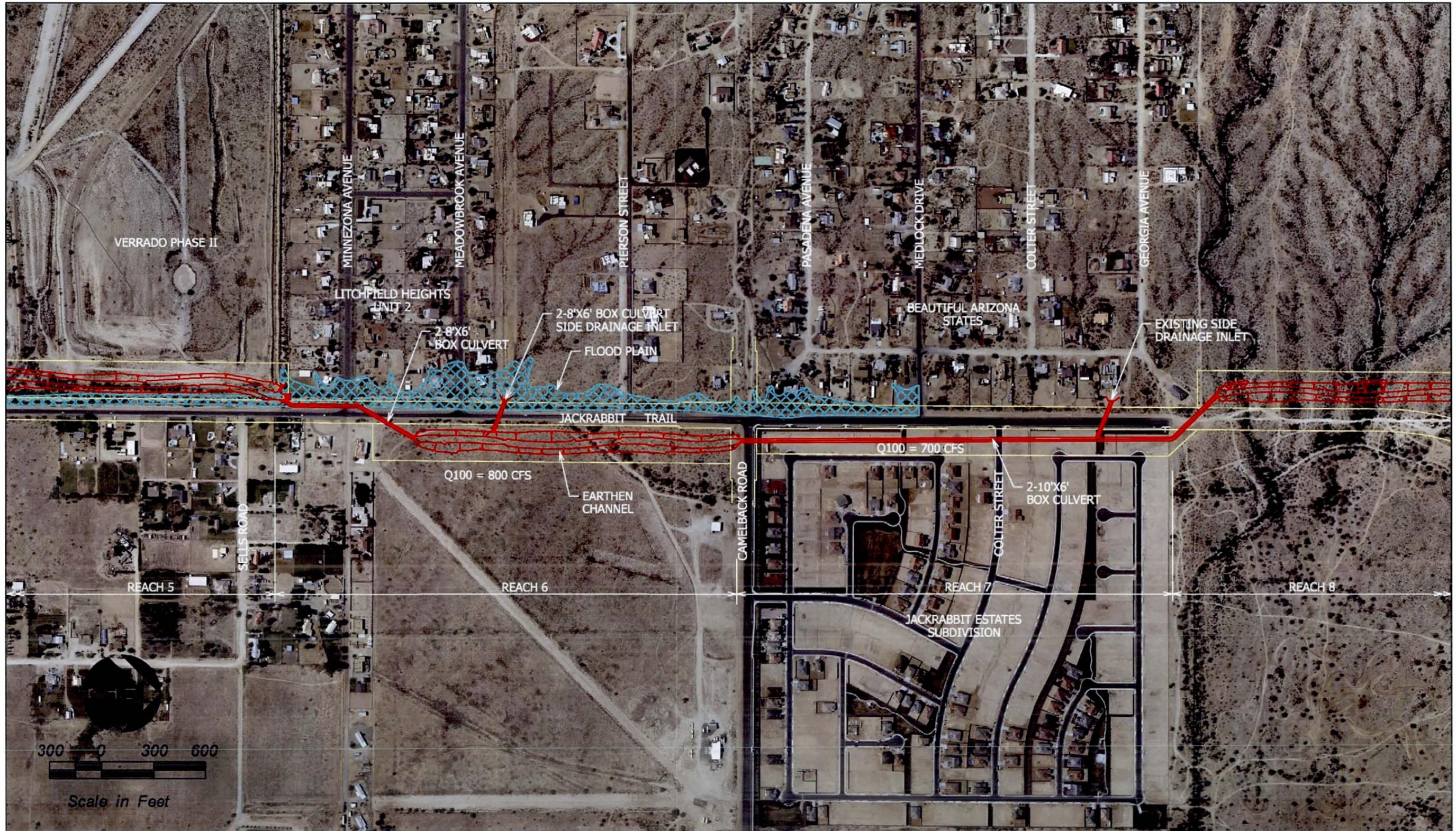


FIGURE 22 – ALTERNATIVE 6/7E

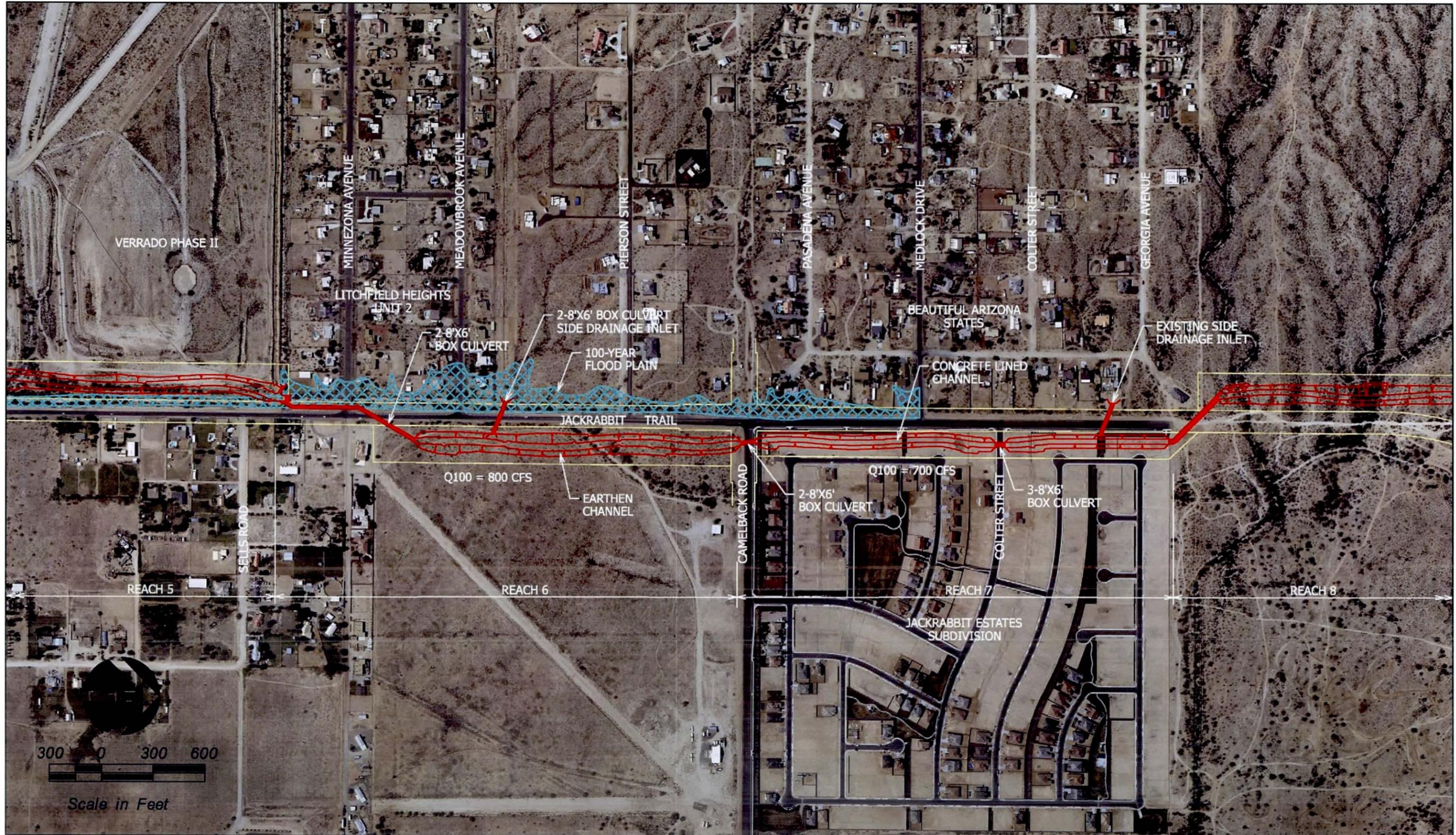


FIGURE 23 – ALTERNATIVE 6/7F



## 6.2 Reach 9

Reach 9 extends from the Principal Spillway in a southwesterly direction toward the emergency spillway, and then south across the emergency spillway to Bethany Home Road. The design discharge for this reach has decreased from the PMF flow of 560 cfs to 285 cfs. The Principal Spillway consists of two 48-inch diameter gated pipes which currently outlet to a channel along the west side of the Beardsley Canal. One of the two pipes (west pipe) will be directed into the Outfall Channel, thus allowing flexibility to discharge from FRS#3 to either location. Aesthetic berming for Reach 9 is illustrated in the LA Pre-Design Report (Ref. 12). The location of this berming will be refined during the Final Design stage to ensure that flow from the emergency spillway is not impeded. In addition, assessment of the emergency spillway flows may necessitate extension of the left training dike and re-evaluation of the NRCS approved SITES model. Reference will be made to the EAP inundation map during the Final Design (Ref. 62).

### 6.2.1 Alternative 9A

Alternative 9A represents the 30% Design Alternative which includes an earthen channel and raised embankment, wasteway spillway and gates to the Beardsley Canal wash, and allowance for a hardened channel lining, and concrete box culverts underneath the emergency spillway. Alternative 9A is no longer under consideration.

### 6.2.2 Alternative 9B

Alternative 9B is the revised Baseline Alternative and consists of the same earthen channel as Alternative 9A except that it will be designed to handle a flow of 285 cfs and will be connected to the westerly Principal Spillway pipe. Subsidence monitoring replaces the hardened channel, and the culvert size underneath the emergency spillway will be reduced in size. The existing east pipe of the Principal Spillway would act as a wasteway and discharge to the Beardsley Canal wash.

### 6.2.3 Alternative 9C

Alternative 9C follows the same alignment as Alternative 9B except that a single pressure pipe connects to the westerly outlet pipe and outlets near Bethany Home Road, south of the emergency spillway. Alternative 9C is no longer under consideration due to concerns about its effect on the operational characteristics of the dam and the delays that could result from reviews through ADWR and NRCS.

### 6.2.4 Alternative 9D

Alternative 9D consists of a sedimentation basin at the outlet from the Principal Spillway and two 72-inch diameter HDPE pipes that would drain southwesterly along the same alignment as Alternative 9B. The existing east pipe of the Principal Spillway would act as a wasteway and discharge to the Beardsley Canal wash.

### 6.2.5 Alternative 9E

Alternative 9E consists of an organic shaped detention basin downstream of the Principal Spillway, and then a conduit under the emergency spillway. This alternative is similar to that produced for the Phase II Remediation Plans and the landscape grading plans prepared by EPG (Ref. 53). The existing east pipe of the Principal Spillway would act as a wasteway and discharge to the Beardsley Canal wash.

### 6.2.6 Alternative 9F

Alternative 9F consists of a single pipe across the dam along the Jackrabbit Trail alignment. The Principal Spillway would remain and be used as a wasteway option. Due to concerns about a jack and bore process under the dam, and agency reviews and delays, this alternative was eliminated.

### 6.2.7 Alternative 9G

Alternative 9G consists of a single pipe or pipes around the west end of the dam. The Principal Spillway would remain and used as a wasteway option. Due to concerns about agency reviews and delays, this alternative was eliminated.

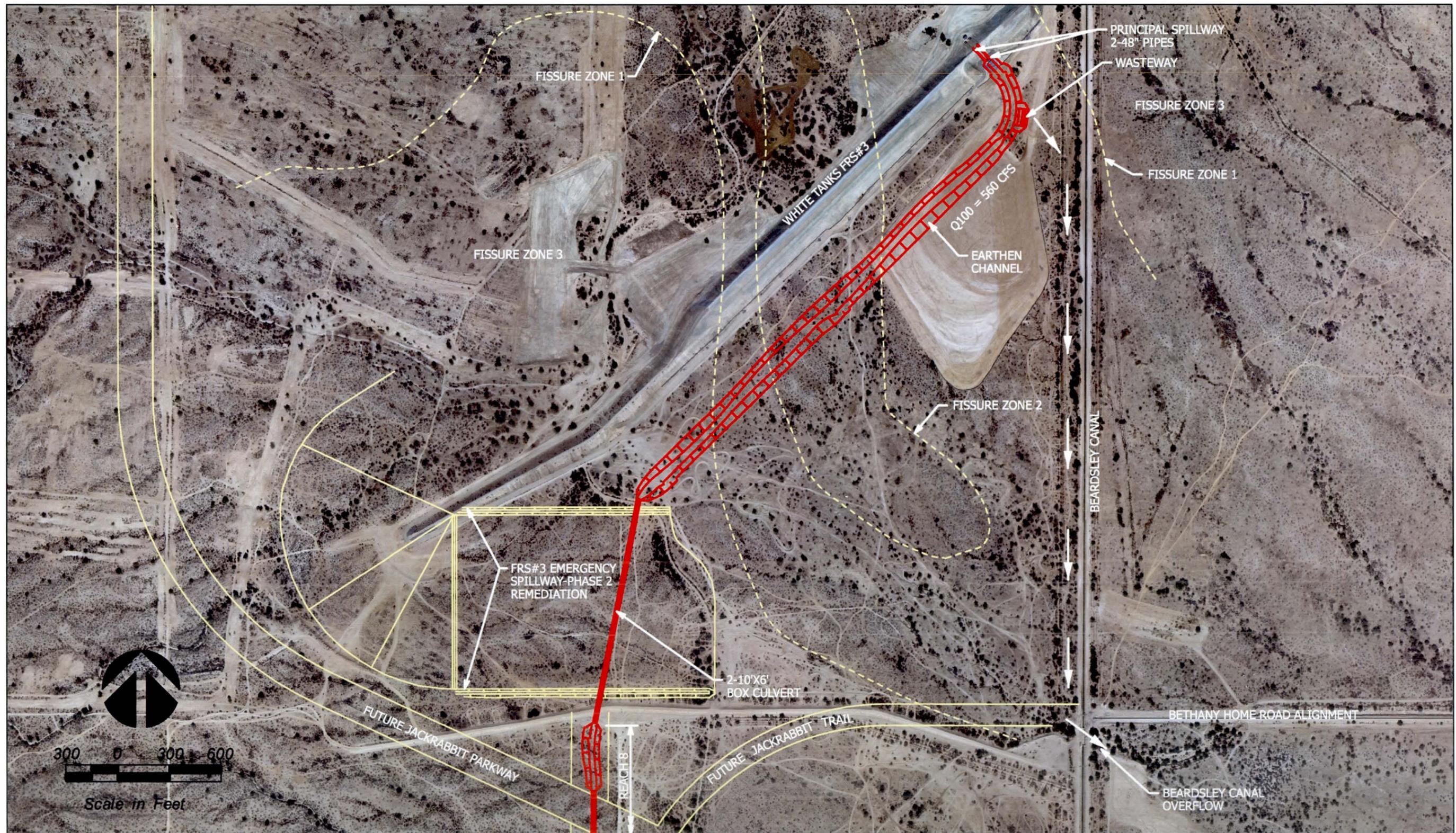


FIGURE 24 – ALTERNATIVE 9A

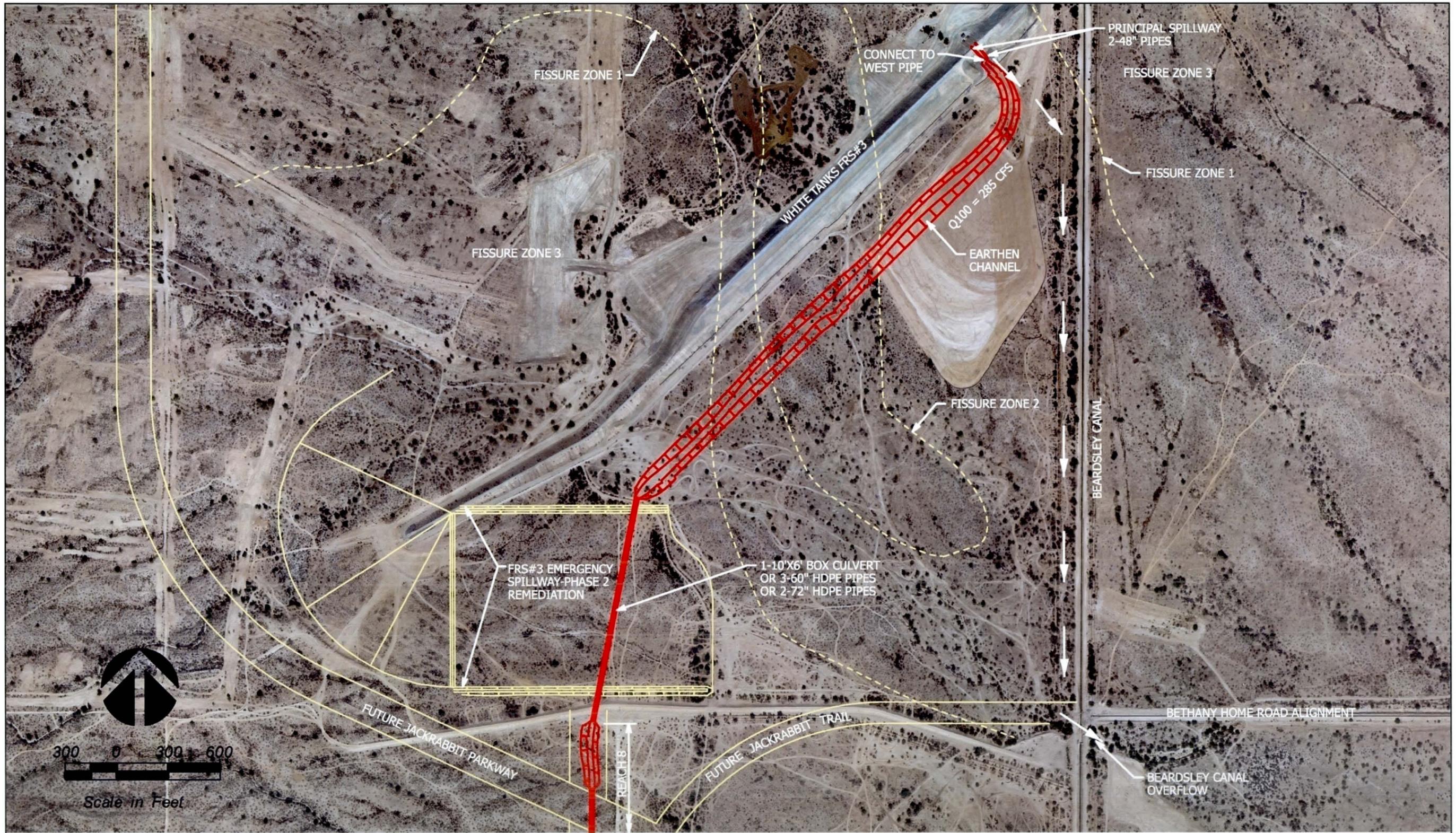


FIGURE 25 – ALTERNATIVE 9B

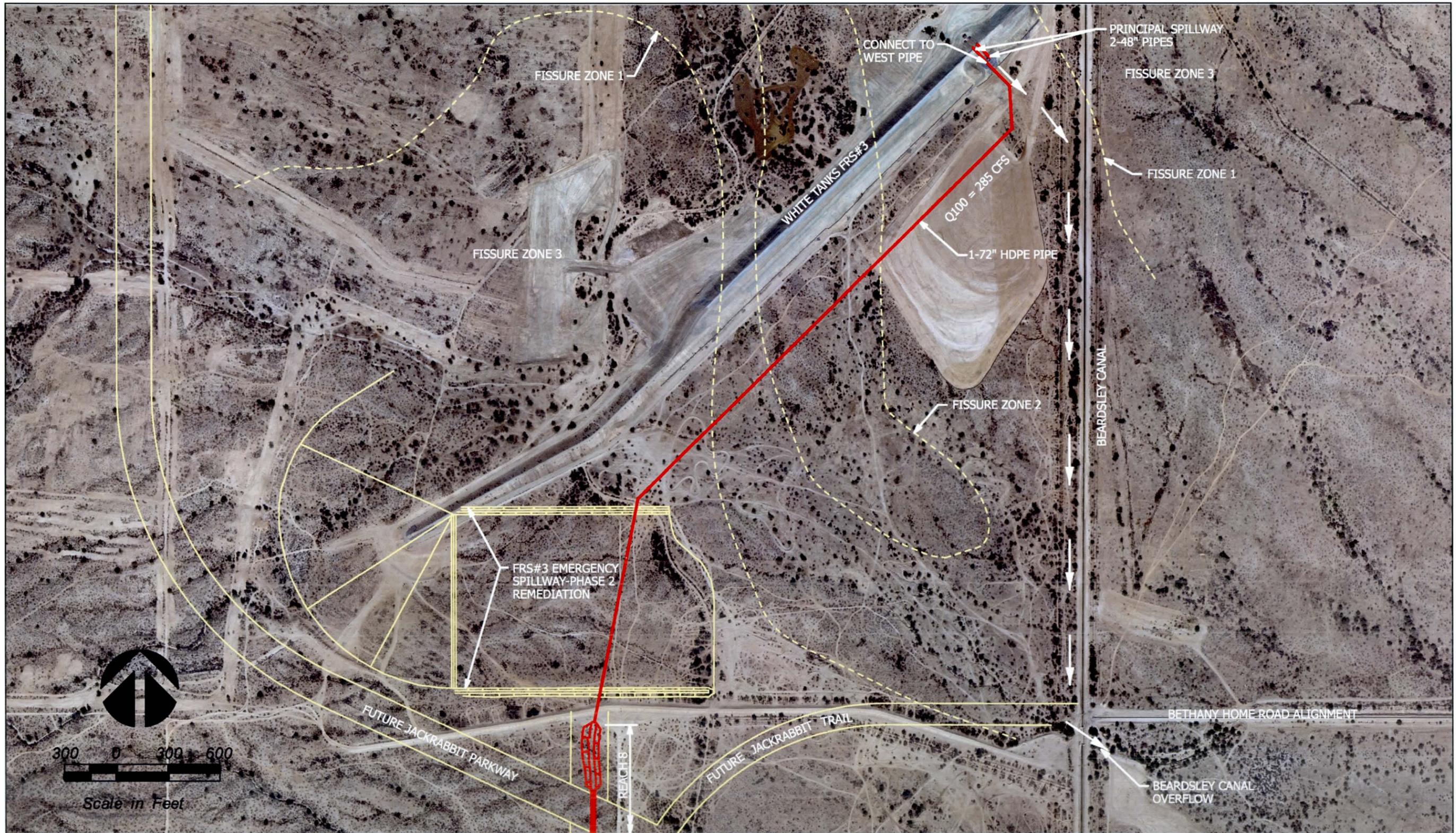


FIGURE 26 – ALTERNATIVE 9C

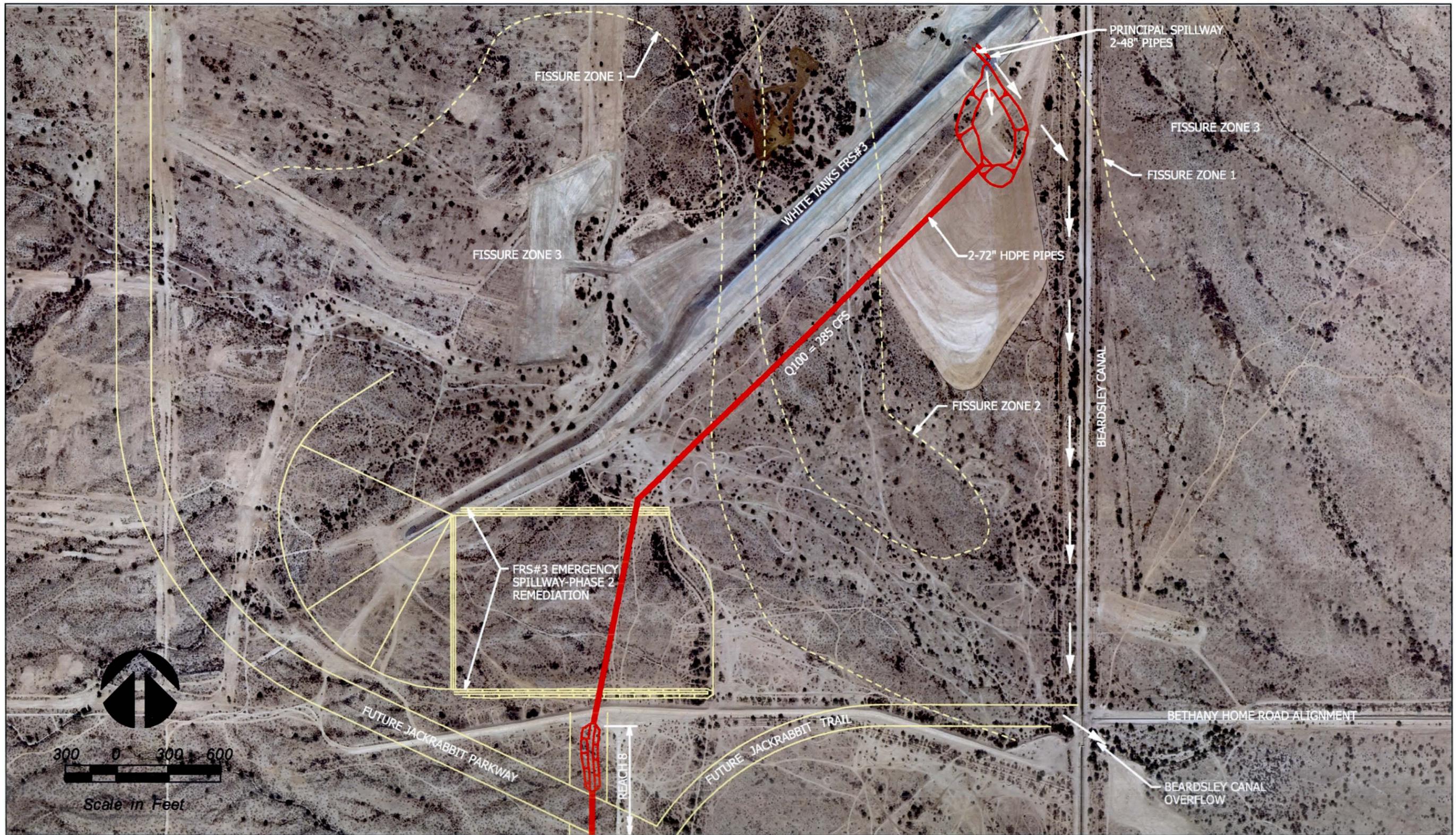


FIGURE 27 – ALTERNATIVE 9D

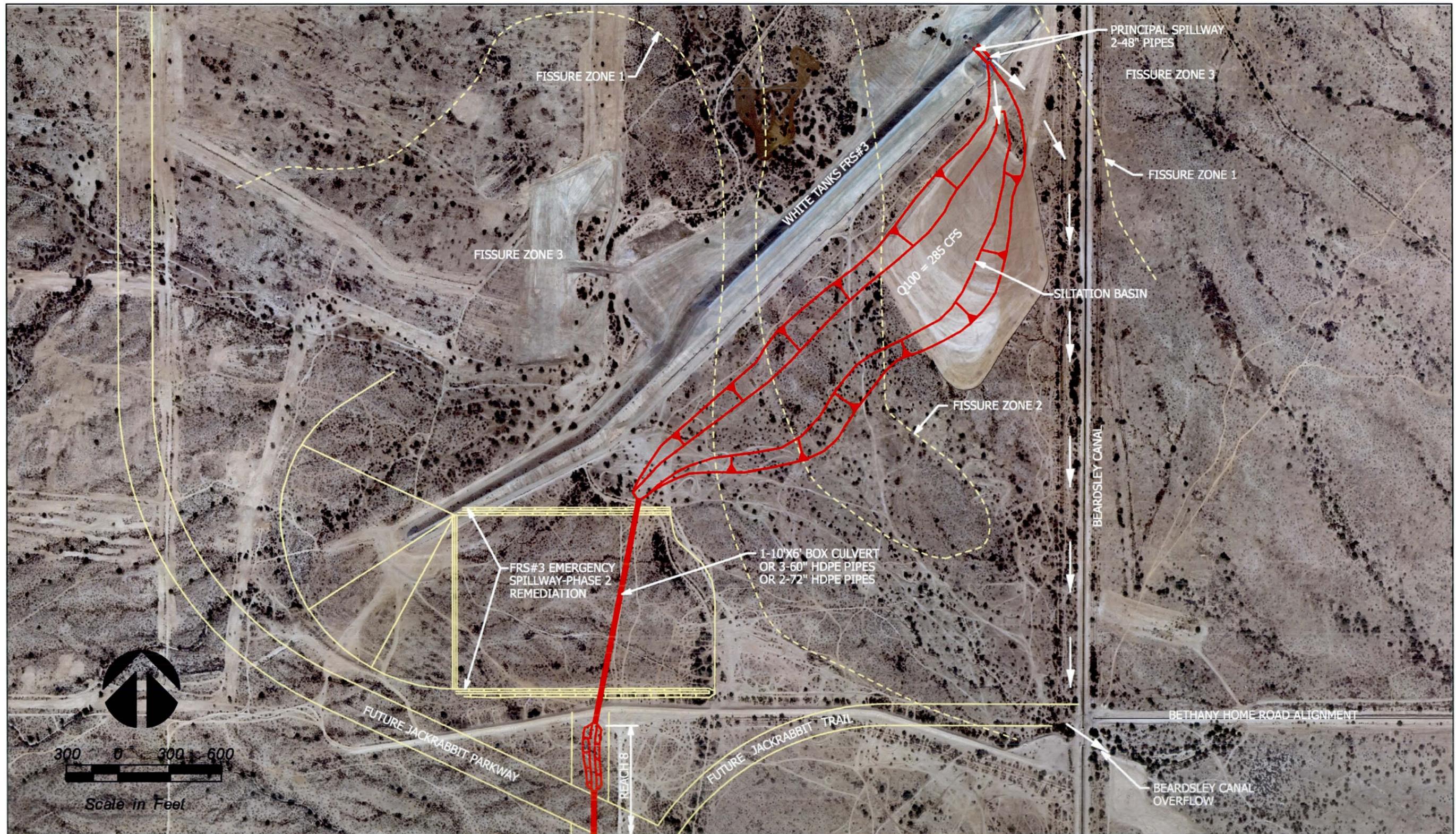


FIGURE 28 – ALTERNATIVE 9E

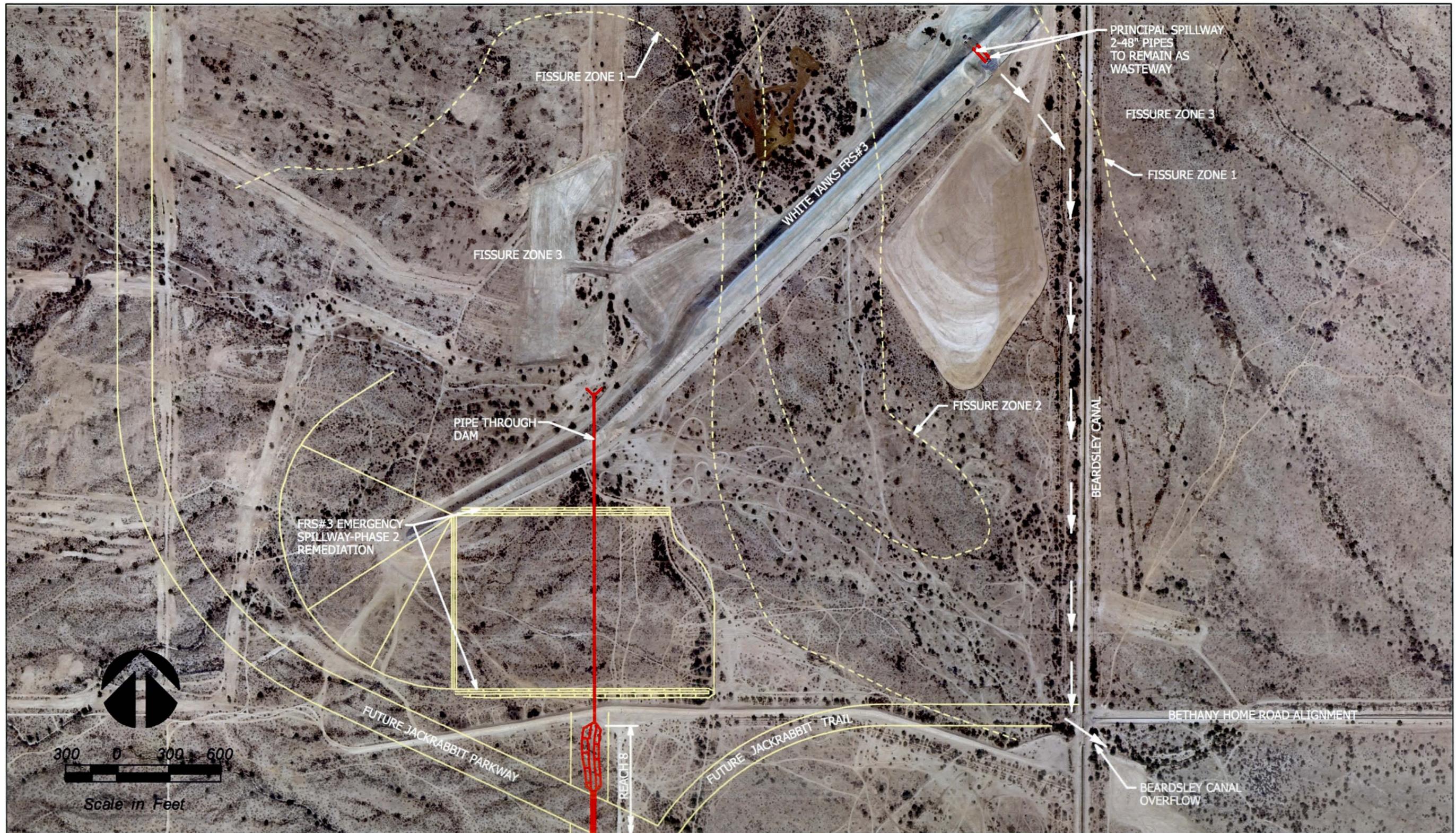


FIGURE 29 – ALTERNATIVE 9F



FIGURE 30 – ALTERNATIVE 9G



### 6.3 Cost Comparison

Cost estimates and quantity summaries for the 30% Design were prepared for the project by reach and by plan sheet in the *30% Design Report* (Refs. 34, 35). The unit prices used in the 30% Design Report were used for the comparison of alternatives within this report. Following completion of the 30% Design Plans and Report, several decisions were made that affect the basis of comparison. In order to make sure that the Alternatives presented in this report were evaluated relative to the same level of protection and cost, a Baseline Alternative was developed. The Baseline Alternative is the 30% Design adjusted as follows:

- Channel within Reach 9 sized for 1/2 Principal Spillway flow (285 cfs)
- Culvert across emergency spillway reduced to single barrel box culvert from double barrel culvert
- Wasteway eliminated, outlet structure modification added
- Hardened Channel allowance removed
- Earthwork for Reach 9 is unchanged
- The cost of aesthetic berming in Reach 9 was not included
- Culvert across Jackrabbit Trail at Minnezona added
- All unit prices and contingencies remain the same as the 30% Design
- Operations and Maintenance costs are not included
- Additional costs due to hard dig into caliche layer are not included

Since the 30% Design Report was prepared, land prices may have declined and could result in an overall decrease in project cost. The land unit prices presented in the 30% Design and those estimated for 2010 are compared in Table 2.

Table 2: Land Cost Comparison

Category	30% Design Report Values	2010 Estimated Values
Platted Parcel	\$205,000 per acre	\$60,000 per acre
Unplatted Parcel	\$152,500 per acre	\$40,000 per acre



Table 3: Reach Evaluation Cost Comparison, 30% Design Report Cost Estimates

Reach	Alternative	Reach Cost*	Difference from Baseline	Least Cost
6	Alt 6A (30% Design)	\$3,913,070	(\$328,866)	
	<b>Alt 6B (Baseline)</b>	<b>\$4,241,936</b>	<b>\$0</b>	
	Alt 6C	\$4,104,888	(\$137,048)	
	Alt 6D	\$3,611,941	(\$629,995)	**
	Alt 6E	\$4,241,936	\$0	
	Alt 6F	\$4,241,936	\$0	
7	Alt 7A (30% Design)	\$1,172,339	\$0	
	<b>Alt 7B (Baseline)</b>	<b>\$1,172,339</b>	<b>\$0</b>	**
	Alt 7C	\$3,652,382	\$2,480,043	
	Alt 7D	\$1,172,339	\$0	
	Alt 7E	\$5,646,173	\$4,473,834	
	Alt 7F	\$2,849,023	\$1,676,684	
9	Alt 9A (30% Design)	\$4,223,440	\$1,625,398	
	<b>Alt 9B (Baseline)</b>	<b>\$2,598,042</b>	<b>\$0</b>	
	Alt 9D	\$2,414,391	(\$183,651)	**
	Alt 9E	\$2,924,342	\$326,300	

\* Using land costs from the 30% Design Report (Ref. 34) see Table 2.

Table 4: Reach Evaluation Cost Comparison, 2010 Land Cost Estimates

Reach	Alternative	Reach Cost*	Difference from Baseline	Least Cost
6	Alt 6A (30% Design)	\$2,778,893	(\$328,866)	
	<b>Alt 6B (Baseline)</b>	<b>\$3,107,759</b>	<b>\$0</b>	
	Alt 6C	\$4,104,888	\$997,129	
	Alt 6D	\$2,968,441	(\$139,318)	**
	Alt 6E	\$3,107,759	\$0	
	Alt 6F	\$3,107,759	\$0	
7	Alt 7A (30% Design)	\$1,172,339	\$0	
	<b>Alt 7B (Baseline)</b>	<b>\$1,172,339</b>	<b>\$0</b>	**
	Alt 7C	\$3,652,382	\$2,480,043	
	Alt 7D	\$1,172,339	\$0	
	Alt 7E	\$5,646,173	\$4,473,834	
	Alt 7F	\$2,849,023	\$1,676,684	
9	Alt 9A (30% Design)	\$4,223,440	\$1,625,398	
	<b>Alt 9B (Baseline)</b>	<b>\$2,598,042</b>	<b>\$0</b>	
	Alt 9D	\$2,414,391	(\$183,651)	**
	Alt 9E	\$2,924,342	\$326,300	

\* Using 2010 land costs estimates provided by the District, See Table 2.

Using the unit land prices presented in Table 2, a reach-by-reach comparison was prepared for each alternative as presented in Table 3 and Table 4. A comparison of Table 3 costs indicates that a combination of Alternatives 6D, 7B, and 9D result in the best cost solution. Using the 2010 unit land prices, as presented in Table 4, the lowest cost solution remains the same, however, the gap narrows.

For each of the Alternatives presented, changes in design concepts associated with the use of different landscape treatments, aesthetic berming, retaining walls, and preservation of existing landscape features are not included in the comparative cost estimates. These design costs will be accounted for with the 60% submittal.



## 7 CONCLUSIONS AND RECOMMENDATIONS

This *Pre-Design Report* accompanies the *Landscape Architecture Pre-Design Report* (Ref. 12). The purpose of the LA Pre-Design Report is to present concepts for the integration of aesthetic treatments and a connection to the Maricopa Trail. This report provides an evaluation of these concepts and re-evaluates alternatives for Reaches 6, 7 and 9 in response to ideas generated from the Value Analysis meeting.

Final Design is ongoing, and decisions reached from this Pre-Design Report will be integrated into the 60% Design Plans and 30% Landscape Design Plans.

### Reach 6

The Baseline cost increased over that from the 30% Design due to the inclusion of an additional culvert across Jackrabbit Trail north of Minnezona Avenue. The addition of a means to intercept drainage from the north and west is recommended. This will help to reduce the 100-year floodplain within the Litchfield Heights subdivision.

Alternatives 6C and 6D both reduce the overall project cost due to a reduction in the right-of-way acquisition costs. Use of a collection channel on the west side of Jackrabbit Trail is preferred over the Baseline Alternative because it will provide for collection of street drainage and incoming silts. The three-channel convergence upstream of Sells Drive would be avoided, and future MCDOT widening of Jackrabbit Trail on the west side would be accommodated.

Right-of-way acquisition has commenced for all land parcels identified on the 30% Design Plans. Due to project goals for construction commencement and the completion of land acquisition prior to the end of the fiscal year, the Baseline Alternative is recommended.

### Reach 7

Within Reach 7, the least cost solution is the Baseline Alternative presented in the 30% Design Plans. This alternative would require the removal of existing landscape improvements along the frontage of Jackrabbit Estates. Construction of a new perimeter wall to the east of the channel is not included since Jackrabbit Estates was compensated as part of the District's land acquisition settlement. In addition, it is desirable to keep the O&M road within the District's right-of-way, therefore, additional retaining walls are recommended along the length of Reach 7. Alternative 7B is recommended.

### Reach 9

Within Reach 9, the least cost alternative is 9D. This alternative included (2) 72-inch diameter HDPE pipes from the Principal Spillway, across the emergency spillway and across Bethany Home Road to Reach 8. This alternative avoids the need to build a FEMA certified levee embankment across the fissure risk zone. Because of the long-term risk of subsidence, it is recommended to increase the fall along the pipe's length by 1.0 foot to accommodate future potential differential subsidence. Monitoring of long-term movement will require periodic measurements to the pipe invert at benchmark manhole locations.

A comparison of the costs for pipe and channel alternatives show that they are similar and would not be a reason for selection of one alternative over another. O&M costs, safety concerns and FEMA levee certification should be overriding decision factors.

### Summary Cost

Implementation of Alternatives 6D, 7B, and 9D would result in a total project cost of approximately \$21,400,771 compared to the Baseline cost of \$22,214,417 (assuming the land costs do not decrease). Implementation of Landscape Design Elements as discussed in Section 5 and the LA Pre-Design Report is recommended following receipt of the Geotechnical Investigation and further review with District staff.

*9B is cheaper if 2-72" HDPE is used instead of 10x6 PCB*



## 8 REFERENCES

1. AMEC Infrastructure, Inc., *Jackrabbit Trail (195<sup>th</sup> Avenue) Design Concept Report, Yuma Road to Thomas Road*, prepared for Maricopa County Department of Transportation, Engineering Division, MCDOT Work Order No. 69039, January 2004.
2. AMEC Infrastructure, Inc., *White Tanks FRS No. 3 Preliminary Geotechnical Report, Contract FCD 2003C014, Work Assignment No. 1*, December 2004.
3. Arizona Water Company, *Water Distribution Quarter Section Maps*, October 19, 1981.
4. CMX, *Zanjero Trails Parcel 34 Conceptual Site Plan*, Draft, March 30, 2009.
5. CMX, *Zanjero Trails RUPD/CUPD-PAD Zone Change Request, Proposed Zoning Map*, April 2006.
6. Coe and Van Loo, *Verrado Agua Fria Irrigation Pump Station No. 1*, September 19, 2004, As-Built July 8, 2005.
7. Coe and Van Loo, *Verrado Indian School Road Well*, March 7, 2003, As-Built January 9, 2004.
8. Coe and Van Loo, *Zone 3S Booster Pump Station, Agua Fria Plant Booster Station No. 9*, April 5, 2003, As-Built January 9, 2004.
9. Dodson & Associates, Inc., *HydroCalc*, Version 1.2a for Windows, 1996.
10. DMJM Harris / AECOM, *Jackrabbit Trail Access Control and Corridor Improvement Study, Interstate-10 to Bell Road, Volume I Final Report*, October 2008.
11. DMJM Harris / AECOM, *Jackrabbit Trail Access Control and Corridor Improvement Study, Interstate-10 to Bell Road, Volume II Appendices*, October 2008.
12. EPG, Inc., in association with Hoskin-Ryan Consultants, Inc., *White Tanks FRS No. 3 Outfall Channel Final Design, FCD 2009C012, Landscape Architecture Pre-Design Report*, December 17, 2009.
13. EPG, Inc., in association with Hoskin-Ryan Consultants, Inc., *White Tanks FRS No. 3 Outfall Channel Final Design, FCD 2009C012, Site Analysis Report*, November 20, 2009.
14. Flood Control District of Maricopa County, *Aesthetic and Multiple-Use Design Guidelines for Flood Control Structures*, January 5, 2005.
15. Flood Control District of Maricopa County, *Computer Aided Drafting & Design Data Delivery Specifications*, Rev. 1.0, January 2000.
16. Flood Control District of Maricopa County, *Consultant Guidelines, Incorporated by Reference for Consultant Services Contracts*, Third Edition, Revision 1, December 1, 2003.
17. Flood Control District of Maricopa County, *Drainage Design Manual for Maricopa County, Arizona, Hydraulics*, Draft September 2003.
18. Flood Control District of Maricopa County, *Drainage Design Manual for Maricopa County, Arizona, Hydrology*, Draft November 2003.
19. Flood Control District of Maricopa County, *Drainage Policies and Standards for Maricopa County, Arizona*, January 11, 2007.
20. Flood Control District of Maricopa County, *Flood Protection Methods*, November 6, 2006.
21. Flood Control District of Maricopa County, *Flood Protection Structures Types Handbook*, April 1, 2008.
22. Flood Control District of Maricopa County, *FY 08/09 0.8-ft Orthophotography Tiles for the White Tanks FRS No. 3 Outfall Channel Project Area in Tif Format*, February 11, 2009, Date of Photography October-December 2008.
23. Flood Control District of Maricopa County, *FY 08/09 1-ft Orthophotography Tiles for the White Tanks FRS No. 3 Outfall Channel Project Area in Tif Format*, March 5, 2009, Date of Photography October-December 2008.
24. Flood Control District of Maricopa County, *GIS Data for the White Tanks FRS No. 3 Outfall Channel Project Area in Various Formats*, Project 2007-C016 Assignment #4, February 12, 2009.
25. Flood Control District of Maricopa County, *Landscape Aesthetics and Multi-Use Consultant Handbook*, April 2003.
26. Flood Control District of Maricopa County, *Landscape Design Themes Handbook*, July 27, 2007.
27. Flood Control District of Maricopa County, *Mission, Vision, Goals, and Objectives for Planning Studies*, February 12, 2007.
28. Flood Control District of Maricopa County, *Policy for the Treatment and Landscaping for Flood Control Projects*, December 16, 1992.
29. Flood Control District of Maricopa County, *River Mechanics Manual for DDMSW*, Draft, September 2009.
30. Gannett Fleming, *White Tanks FRS No. 3 Outfall Channel Project, Preliminary Design Report*, December 2008.
31. Haestad Methods, Inc., *FlowMaster*, Version 5.17, 1995.
32. HDR, *Loop 303/White Tanks ADMPU Area Hydrologic Analysis*, March 2009.
33. Hoskin-Ryan Consultants, Inc., *On-Call Contract FCD 2007C016, Work Assignment No. 4, White Tanks FRS No. 3 Outfall Channel, Survey Report*, March 19, 2009.
34. Hoskin-Ryan Consultants, Inc., *White Tanks FRS No. 3 Outfall Channel 30% Design Report, FCD 2007C016 Assignment 4, Volume I – Design Report and 30% Plans*, June 30, 2009.
35. Hoskin-Ryan Consultants, Inc., *White Tanks FRS No. 3 Outfall Channel 30% Design Report, FCD 2007C016 Assignment 4, Volume II – Appendices*, June 30, 2009.
36. KVL Consultants, Inc., for Flood Control District of Maricopa County, *Drainage Design Management System for Windows*, Version 3.5.4, April 1, 2008.
37. Maricopa County Trails Commission, *Maricopa County Regional Trail System Plan*, adopted 2004.
38. Morrison Maierle, Inc., *Off-Site Water Plans for Jackrabbit Estates*, March 29, 2005, As-Built October 11, 2007.
39. Phillips, Jeff V., and Saeid Tadayon, United States Geological Survey, in association with Flood Control District of Maricopa County, *Selection of Manning's Roughness Coefficient for Natural and*



- Constructed Vegetated and Non-Vegetated Channels, and Vegetation Maintenance Plan Guidelines for Vegetated Channels in Central Arizona*, Scientific Investigations Report 2006-5108, 2007.
40. SiteTek Financial Arts, Inc., *Value Analysis Workshop, November 3-5, 2009, 30% Design Phase White Tanks FRS III Outfall Channel, Value Analysis Draft Report*, November 9, 2009.
41. Thomsen, B.W. and Hjalmarson, H.W., with U. S. Geological Survey, Water Resources Division, for Flood Control District of Maricopa County, *Estimated Manning's Roughness Coefficients for Stream Channels and Flood Plains in Maricopa County, Arizona*, April 1991.
42. Town of Buckeye, *Transportation Design Manual, DM202*, May 2007.
43. United Engineering Group, *Water Plans for Jackrabbit Estates*, April 12, 2005, As-Built September 7, 2006.
44. United States Army Corps of Engineers, *Hydrologic Engineering Center, HEC-1 Flood Hydrograph Package*, Version 4.1, June 1998.
45. United States Army Corps of Engineers, *Hydrologic Engineering Center, HEC-RAS River Analysis System*, Version 4.0.0, March 2008.
46. URS, *Loop 303 Corridor/White Tanks Area Drainage Master Plan Update, Volume IV: Level III Area Drainage Master Plan Update Report, Final*, FCD Contract 99-40, February 2005.
47. URS, *Loop 303 Corridor/White Tanks Area Drainage Master Plan Update, Volume V: Existing Condition Hydrology Technical Data Notebook*, August 2004.
48. URS, *Loop 303 Corridor/White Tanks Area Drainage Master Plan Update, Volume V: Future Condition Hydrology Technical Data Notebook*, January 2005.
49. URS, *Design Report, White Tanks FRS No. 3 Remediation Project – Phase 1, Volume 1*, March 23, 2005.
50. URS, *Design Report, White Tanks FRS No. 3 Remediation Project – Phase 1, Volume 2*, March 23, 2005.
51. URS, *Geotechnical Data Report, White Tanks FRS No. 3 Remediation Project*, March 23, 2005.
52. URS, *White Tanks FRS No. 3 Remediation Project – Phase 1: Embankment Fill Plan and Outlet Works Channel Plan and Profile, PCN 470.04.30, FCD Contract No. 2004C017*, March 2005.
53. URS, *White Tanks FRS No. 3 Remediation Project – Phase 2, PCN 470.04.30, FCD Contract No. 2008C031*, March 3, 2009.
54. WLB Group, *White Tanks/Agua Fria Area Drainage Master Study*, 1994.
55. Wood, Patel and Associates, Inc., *Indian School Road Utilities, Verrado*, February 17, 2003, As-Built February 9, 2004.
56. Wood, Patel and Associates, Inc., *Nonpotable Waterline Plan, Sells Road to Indian School Road*, November 1, 2004, As-Built March 11, 2005.
57. Wood, Patel and Associates, Inc., *Offsite Water Transmission Main, Verrado*, April 17, 2003, As-Built October 22, 2003.
58. Wood, Patel and Associates, Inc., *Verrado Planning Unit Drainage Plan for Portions of Planning Units II and IV (Phase 3 South and Phase 3 East), and Update to Master Drainage Plan*, August 22, 2006.
59. Wood, Patel and Associates, Inc., *White Tanks FRS No. 4 Rehabilitation Project*, December 2008.
60. Simon, Li & Associates, *Design Manual for Engineering Analysis of Fluvial Systems*, 1985.
61. Alpha Geotechnical and Materials, Inc., *Geotechnical Exploration, White Tanks FRS No.3 Outfall Channel Between White Tanks FRS No.3 and White Tanks FRS No. 4, Maricopa County, Arizona, Draft* January 2010.
62. J.E. Fuller Hydrology and Geomorphology, Inc., *Emergency Action Plan Final report for White Tanks FRS #3*, October 2009.



**APPENDIX A PRODUCT LITERATURE**



## Precast Details

**Buried Structure vs. Bridge-at-Grade**

**DESIGN SPECIFICATIONS**  
 AASHTO:  
 Standard Specifications for Highway Bridges - Section 16.8  
 LRFD Bridge Design Specifications - Section 12.14

**MANUFACTURING SPECIFICATIONS**  
 ASTM C1504

**Base Slab**

**Strip Footing**

**Footing Details**

Strip Footing

Pedestal Wall Footing

Multi Cell Pier Footing

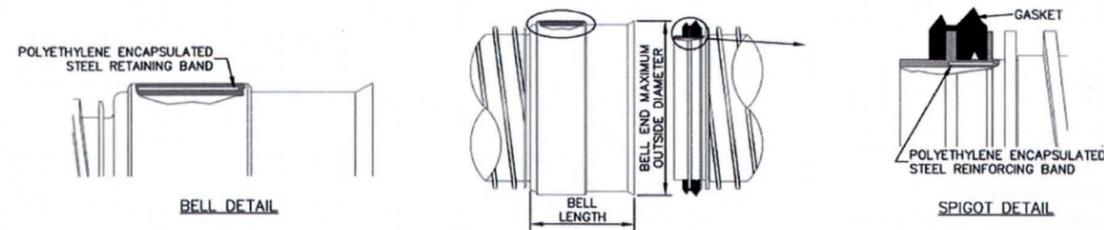
**Significant Economic Advantages are Gained from Precast Wingwalls through:**

- Narrower Footings
- Thinner Walls
- Reduced Excavation





### Joint Details – The Design Behind the Performance



## DuroMaxx™ – The Next Generation of Drainage Pipe

### DuroMaxx Environmental Benefits

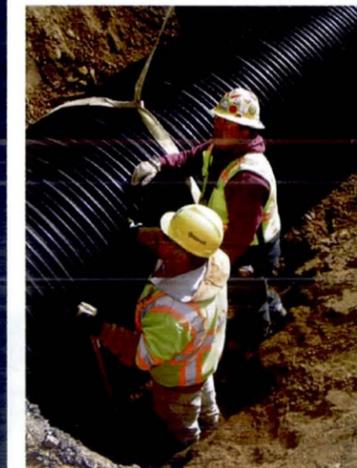
DuroMaxx consumes 35% less of the natural resources required to produce AASHTO M294 pipe. Steel reinforcing ribs in the profile wall provide the structural integrity for the pipe. These ribs are made out of steel with recycled content levels ranging from 55-80%. DuroMaxx pipe is eligible for LEED credits in a variety of the U.S. Green Building Council's categories for sustainable sites, water efficiency and landscaping, and materials and resources.

CONTECH Construction Products Inc. provides site solutions for the civil engineering industry. CONTECH's portfolio includes bridges, drainage, retaining walls, sanitary sewer, stormwater, erosion control and soil stabilization products.

For more information, call one of CONTECH's Regional Offices located in the following cities:

- |                                |                     |
|--------------------------------|---------------------|
| <b>Ohio (Corporate Office)</b> | <b>513-645-7000</b> |
| California (San Bernardino)    | 909-885-8800        |
| Colorado (Denver)              | 303-431-8999        |
| Florida (Tampa)                | 727-544-8811        |
| Georgia (Atlanta)              | 770-409-0814        |
| Indiana (Indianapolis)         | 317-842-7766        |
| Kansas (Kansas City)           | 913-906-9200        |
| Maryland (Baltimore)           | 410-740-8490        |
| Oregon (Portland)              | 503-258-3180        |
| Texas (Dallas)                 | 972-590-2000        |

Visit our web site: [www.contech-cpi.com](http://www.contech-cpi.com)  
800.338.1122



NOTHING IN THIS CATALOG SHOULD BE CONSTRUED AS AN EXPRESSED WARRANTY OR AN IMPLIED WARRANTY OF MERCHANTABILITY OR FITNESS FOR ANY PARTICULAR PURPOSE. SEE THE CONTECH STANDARD CONDITIONS OF SALE (VIEWABLE AT [WWW.CONTECH-CPI.COM/COS](http://WWW.CONTECH-CPI.COM/COS)) FOR MORE INFORMATION.

DuroMaxx is supported by Plastream technology.



©2009 CONTECH CONSTRUCTION PRODUCTS, INC.  
All rights reserved. Printed in USA.



Knowledge. Solutions. Service.

## Key Performance Advantages

### High Strength Steel Rib

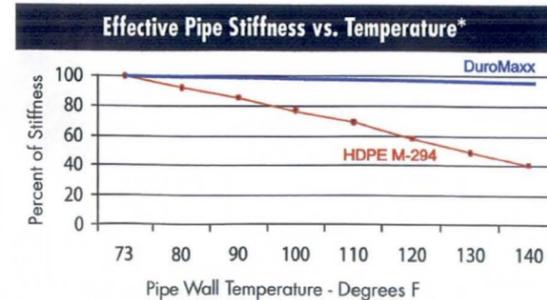
**The strength of steel with the durability of plastic**  
It's the ideal combination of materials that makes DuroMaxx an exceptional pipe. Steel reinforcing ribs provide the strength. High-Density Polyethylene Resin (HDPE) provides the durability. The combination of materials results in an extraordinarily strong and durable pipe. CONTECH design engineers also provide DuroMaxx with a smooth inner wall for outstanding hydraulics. DuroMaxx provides the properties you can count on for long term service and performance in the most demanding environments. Finally, a drainage product that is engineered for service and long life.

#### High Strength Steel for Lifelong Performance

DuroMaxx steel rib profile wall construction will not creep or buckle. The built-in capacity of the high strength steel eliminates concerns that have long plagued open profile wall pipe. Today, it is possible to design with confidence to meet the structural demands of the most difficult storm drain projects, ensuring long-term performance.

#### Effects of Temperature

All flexible pipes must be designed to have adequate pipe stiffness to resist handling, installation and construction loads. The required stiffness must be sufficient to minimize deflection, ensuring a successful installation. Published pipe stiffness levels are measured at 73°F in a laboratory. The actual or apparent field pipe stiffness due to the effects of sunlight and a modest 80° temperature will produce results that are very different in the field – where it counts with a pipe wall temperature in excess of 110°. This results in a loss of pipe stiffness greater than 30% for a non-reinforced open profile polyethylene pipe. Steel-reinforced DuroMaxx pipe loses less than 1% of its stiffness under the same conditions.



\*The information in this graph is an average stiffness loss observed over several diameters of one AASHRO M294 HDPE profile wall product.

### High Stress Rated Resins

**High Performance Resins for Lifelong Performance**  
Predictable service life demands predictable material properties. CONTECH engineers have designed DuroMaxx with high quality stress rated materials that provide predictable engineering properties. DuroMaxx will not experience the dreaded cracking and delamination that has undermined HDPE pipe supplier credibility. CONTECH's decision to manufacture DuroMaxx using stress rated resins was a choice made to support the professional engineer and to avoid further negative experiences for the contractor. Shouldn't you demand similar Hydrostatic Design Basis (HDB) stress rated materials from your supplier?

### Low Head Water Tight Joints

#### High Performance Low Head Joints

The integrated bell and spigot DuroMaxx design achieves a level of performance that sets it apart from conventional storm drain products. The DuroMaxx joint is designed to meet the highest standards of performance for storm drains for the added assurance often required but not cost effectively available to the engineer. DuroMaxx bell and spigots are designed to achieve 15 psi when tested in the laboratory in accordance with ASTM D3212. DuroMaxx Water Tight (WT) sets a new industry standard for joint performance.

#### Longer Lengths: Fewer Joints

DuroMaxx pipe is manufactured in standard lengths of 20 feet with bell and spigot joints – resulting in fewer joints to assemble on site and faster installation rates for the contractor. If your project requires custom lengths, DuroMaxx can be provided in plain end or with bell and spigot joints.



## Applications

#### Drainage Pipe

DuroMaxx drainage pipe is ideally suited for the collection and removal of gravity flow stormwater from residential developments, industrial sites and urban projects. Anywhere the need to move water exists, DuroMaxx meets that need.

#### Subsoil Drainage Pipes

DuroMaxx can also be produced as perforated pipe for subsoil drainage applications. Used to collect and transfer subsurface water through ground seepage into the pipeline, DuroMaxx perforated pipe can eliminate the need for open drainage channels.

#### Stormwater Detention Systems

Detention systems are used to regulate stormwater flow through main pipelines by acting as a buffer during peak loads. DuroMaxx systems are designed to contain the water and slowly release it into the main system over a period of time. These systems are often custom made to water tight specifications in order to suit the project requirements. DuroMaxx systems can incorporate a wide range of fittings such as bends, risers, bulk headed ends and inlet/outlet pipes. The systems can be custom manufactured to individual lengths in sizes and configurations that can be economically transported and assembled on site. The light weight and ease of handling of the sections, even large diameters, allows easy placement and installation of pipe and other structures on site.

DuroMaxx is an engineered polyethylene steel composite pipe with a rib profile outer wall and a smooth internal surface. Suitable for drainage and detention applications, DuroMaxx is extruded using virgin high-density polyethylene, which is embedded with ribs of high yield steel. This composite structure creates a pipe with exceptional strength and a relatively low material mass, that is manufactured in accordance with and meets ASTM F2562 for steel reinforced thermoplastic ribbed pipe.

## Applications and Savings

### Savings

#### Higher Flow Rates

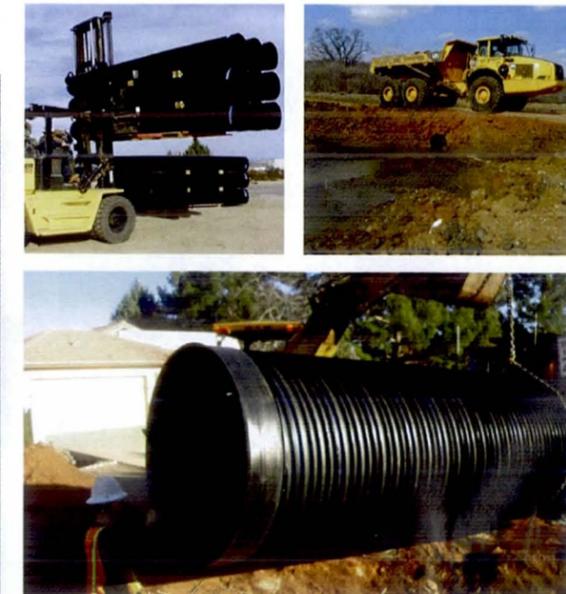
Higher flow rates are achieved with a smooth polyethylene water way wall thereby providing the engineer with the design option to reduce the pipeline diameter, saving money overall.

#### Lighter Weight

DuroMaxx pipe is light weight which means it can be easily and quickly handled and installed, often eliminating the need to use heavy construction equipment. As the two main cost drivers to install water conveyance products are manpower and machinery, DuroMaxx provides the opportunity to save in both, resulting in less overall spending. The longer lengths and easy joint assembly are just some of the DuroMaxx installation advantages. For the nationally accepted installation standard, reference the ASTM D2321 or contact your local CONTECH representative for the DuroMaxx installation guide.

#### Fittings

DuroMaxx pipe is compatible with a full range of fabricated fittings such as elbows, tees, wyes, slope junctions and reducers. Both standard and custom fittings can be readily fabricated from sections of the pipe.





**ENGINEERS ESTIMATE**

Page 1 of 1

Date: 12/8/09  
Client: Hoskin/Ryan  
Contact: Paul Hoskin  
PROJECT: FRS NO.3 Outfall Channel

Quote: 1  
Territory:  
Reply to: John Bacigalupi  
602-377-5347

This estimate is a comparison of CON/SPAN equivalents to Cast in Place Box Culvert structures- (CBC).

Item No.	Approx. Quantity	Description	Unit Price	Unit	Unit Total
1	825	CON/SPAN Precast Arch Culvert-16' x 6'	\$504.00	LF	\$415,800.00
		Precast-16' span x 6' rise replaces (2)8'x6' CBC			
1A	825	Foundations and Installation of Precast	\$166.00	LF	\$136,950.00
		Includes excavation/foundations/erection			
<b>1Total</b>	<b>1</b>	<b>Total Installed Cost of Precast Option 1</b>	<b>\$670.00</b>	<b>LF</b>	<b>\$552,750.00</b>
2	63	CON/SPAN Precast Arch Culvert-24' x 6'	\$567.00	LF	\$35,721.00
		Precast -24' span x 6' rise replaces (3)8'x6' CBC			
2A	63	Foundations and Installation of Precast	\$187.00	LF	\$11,781.00
		Includes excavation/foundations/erection			
<b>2T</b>	<b>1</b>	<b>Total Installed Cost of Precast Option 2</b>	<b>\$754.00</b>	<b>LF</b>	<b>\$47,502.00</b>
			<b>(tax not included) TOTAL</b>		

Unless documentation of tax exempt status is provided, tax will be added to invoiced price.

**Notes**

1. Installation of precast is by others
2. Design is included
3. Quantities above based on estimated quantities. Buyer must verify quantity at unit price above at time of order.
4. On site consultation is provided during installation
5. Prices are F.O.B. plant, freight allowed to jobsite with purchaser to unload at a truck accessible delivery point.

PAYMENT TERMS ARE 1/2%-10, NET 30 DAYS FROM DATE OF INVOICE UNLESS MATERIAL IS OTHERWISE NOTED AS NONSTANDARD ABOVE. IF NONSTANDARD, PAYMENT TERMS ARE 1/3 AT ORDER ACCEPTANCE AND PRIOR TO START OF PRODUCTION, 2/3 NET 30 DAYS FROM DATE OF INVOICE. THIS OFFER IS SUBJECT TO CREDIT APPROVAL. PRICES QUOTED APPLY ONLY TO THE REFERENCED PROJECT AND ARE IN EFFECT FOR 30 DAYS FROM THE DATE OF THIS QUOTATION. SELLER RESERVES THE RIGHT TO ADJUST PRICES AFTER 30 DAYS FROM THE DATE OF QUOTATION BUT THE CONTECH COS REMAIN APPLICABLE. PRICES ARE BASED ON ESTIMATED QUANTITIES SHOWN. IF A DIFFERENT QUANTITY IS PURCHASED, CONTECH RESERVES THE RIGHT TO ADJUST PRICES. THIS QUOTATION CONTAINS THE ENTIRE AGREEMENT WITH RESPECT TO THE PURCHASE AND SALE OF THE PRODUCTS DESCRIBED AND SUPERSEDES ALL PREVIOUS COMMUNICATIONS. BUYER'S SIGNATURE BELOW, DIRECTION TO MANUFACTURE, OR ACCEPTANCE OF DELIVERY OF GOODS DESCRIBED ABOVE, SHALL BE DEEMED AN ACCEPTANCE OF THE CONTECH COS. SELLER EXPRESSLY REJECTS ANY OTHER TERMS AND CONDITIONS. PRICES ARE F.O.B. ORIGIN WITH FREIGHT ALLOWED TO THE JOBSITE WITH UNLOADING BY OTHERS AT A TRUCK ACCESSIBLE LOCATION.

**ACCEPTANCE**

WE HEREBY ORDER THE DESCRIBED MATERIAL SUBJECT TO THE TERMS AND CONDITIONS OF THIS QUOTATION AND IN THE CONTECH CONDITIONS OF SALE INCLUDED HERewith AND VIEWABLE AT [www.contech-cpi.com/cos](http://www.contech-cpi.com/cos).

Company: \_\_\_\_\_  
By: \_\_\_\_\_  
Title: \_\_\_\_\_ Date: \_\_\_\_\_

**CONTECH CONSTRUCTION PRODUCTS INC.**

By: John Bacigalupi  
Title: **District Manager**



## The lightweight pipe that takes a heavier load

Weholite® pipe is large diameter, profile wall pipe made from high-density polyethylene (HDPE) resin. Designed for gravity and low-pressure applications, Weholite's raw material properties have been combined with patented structural wall technology to create a lightweight engineered pipe with superior loading capacity. It is used to convey liquids or air, under ground or above ground, in low-pressure applications.

### Lighter. Stronger. Chemical Resistant.

Weholite pipe is much lighter than similarly sized concrete pipe. Combine this with longer manufacturing lengths and Weholite allows you to achieve savings in labour and equipment.

Weholite HDPE pipe will not corrode, tuberculate or support biological growth, making it the material of choice in harsh chemical environments. It is inert to salt water and the chemicals likely to be present in sanitary sewage effluent.

Like all HDPE pipe, Weholite has a smooth ID that maintains its flow capability over time. The low Manning's roughness factor of 0.01 remains constant, even after years of use.

### Easier to Transport. Easier to Install.

#### Leak Proof.

Weholite pipe is much easier to handle and install than heavier, rigid concrete or metallic pipe. This means potential cost savings during the construction process. It is structurally designed to withstand an impact, especially in cold weather installations when other pipes are prone to cracks and breaks.

Weholite pipe is usually joined by a thermal fusion process (extrusion welding) to form a joint that is as strong as the pipe itself. Extrusion welding eliminates potential leak points every 8-20 feet commonly found with concrete, PVC and ductile iron pipe. Since fused joints are self-restraining, costly thrust restraints or thrust blocks may not be required.

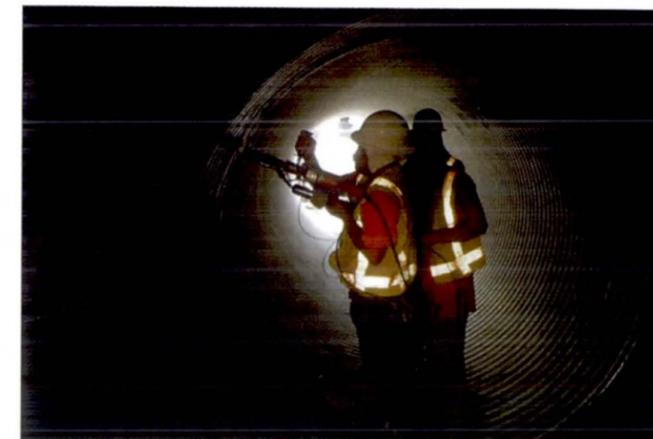


Extrusion welded Weholite pipe is leak proof. The properties of HDPE pipe and the thermal fusion method of joining produces a continuous pipeline, eliminating the risk of leakage caused by shifting unstable soils. A continuous Weholite pipeline eliminates the joint infiltration and exfiltration problems experienced with other pipe materials.

### Cost Effective. Permanent.

Weholite pipe offers distinct chemical and physical advantages over concrete or iron pipe. It can be bent to a radius 200 times the nominal pipe diameter to eliminate many fittings required for directional changes in piping systems made from other materials. In addition, the flexibility of Weholite pipe makes it well suited for dynamic soils and areas prone to earthquakes.

Weholite is cost effective in both the short and long term. The fact that it is lightweight makes it easier to transport and install. The fact that it is leak proof and fatigue resistant means years of maintenance free use. The Plastics Pipe Institute conservatively estimates the service life for HDPE pipe to be 50-100 years.



### Weholite Advantages

- ◆ *Lightweight*
- ◆ *Impact Resistant*
- ◆ *Corrosion Resistant*
- ◆ *Chemical Resistant*
- ◆ *Fatigue Resistant*
- ◆ *Leak Proof*
- ◆ *Flexible*
- ◆ *Long Life*
- ◆ *Environmentally Friendly*



# Technical Info

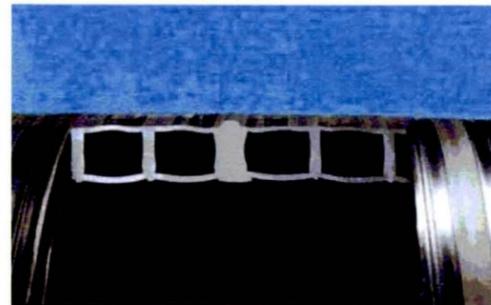
## The Weholite Structure

Weholite pipe is manufactured with a unique profile design that takes advantage of structural shape efficiencies to provide a product that is suitable for a wide range of loading conditions. The structure is the optimal solution when comparing performance versus weight.

### Material Properties

#### Weholite Pipe is Corrosion and Chemical Resistant

Weholite pipe will not corrode, tuberculate or support biological growth. It is the material of choice in harsh chemical environments. Weholite has a smooth ID and maintains its flow capability over time - Mannings n Factor remains 0.010, even after years of use.



#### Weholite Pipe is Flexible and Fatigue Resistant

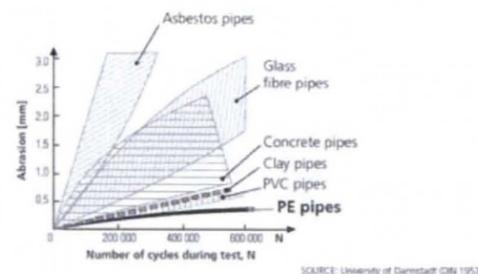
Weholite can be bent to a radius 200 times the nominal pipe diameter. This can eliminate many fittings required for directional changes compared to piping systems made from other materials. In addition, the flexibility of Weholite makes it well suited for dynamic soils and areas prone to earthquake.

#### Weholite Pipe is Lightweight and Impact Resistant

Weholite is much easier to handle and install than heavier, rigid metallic or concrete pipe, allowing for cost advantages in the construction process. Structurally, it is better suited to withstand an impact than other pipe materials, especially in cold weather installations when other pipes like PVC are prone to cracks and breaks.

#### Weholite Pipe Abrasion resistance

Weholite pipes show superior abrasion-resistant qualities compared to traditional pipeline materials. This is proven by the fact that HDPE pipes have been the first choice for the mining industry during many decades.



Size (inch)	Item		Dimensions	
	Class	Spec	Avg. OD (inch)	Avg. ID* (inch)
66	160	F894	72.4	66.0
66	250	F894	73.8	66.0
72	100	F894	78.4	72.0
72	160	F894	79.1	72.0
72	250	F894	80.5	72.0
78	100	F894	84.4	78.0
78	160	F894	85.8	78.0
78	250	F894	86.5	78.0
84	100	F894	90.3	84.0
84	160	F894	91.8	84.0
84	250	F894	93.2	84.0
90	160	F894	97.8	90.0
90	250	F894	99.2	90.0
90	400	F894	100.6	90.0
96	160	F894	104.5	96.0
96	250	F894	105.9	96.0
96	400	F894	107.4	96.0
108	160	F894	117.2	108.0
108	250	F894	118.6	108.0
108	400	F894	120.8	108.0
120	160	F894	129.9	120.0
120	250	F894	131.3	120.0
120	400	F894	134.2	120.0
132	160	F894**	141.6	132.0

Standard Inventory Product

\*Minimum ID is 1% less than Average ID

\*\*Pipe complies entirely with ASTM F894 with the exception of the nominal OD value.

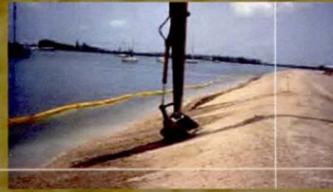
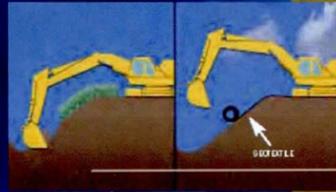
**Note:** This dimensional table for Weholite pipe contains a range of product sizes and stiffness classes. The specification associated with each of these items is ASTM F894. Pipe sizes 48" and smaller are available in lower stiffness classes that do not comply with the minimum waterway wall thickness requirement of ASTM F894. If the analysis using our online tools indicates that one of these lower stiffness items is suitable, the standard that will be indicated on all documentation is NONF894. The items comply in all respects with ASTM F894 except the waterway wall.





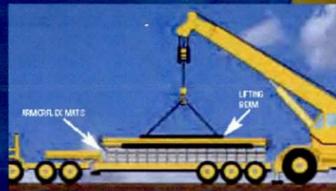
ARMORFLEX® INSTALLATION

ArmorFlex arrives on-site as a system of factory-assembled mats. ArmorFlex is placed on a site specific geotextile which has been placed on a prepared subgrade using conventional construction equipment.



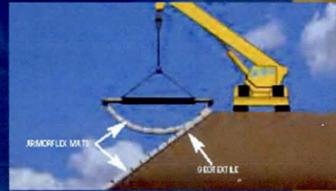
SITE PREPARATION

Mats are supplied on 42-foot trailers, up to 1600 square feet per truck.



DELIVERY & UNLOADING

Mats can be handled with a spreader bar which is provided by Armortec with the initial load.



INSTALLING & LIFTING DEVICE

Permanent anchorage can be achieved by connecting the mat cables to patented anchors such as "Helix" or "Duckbill".

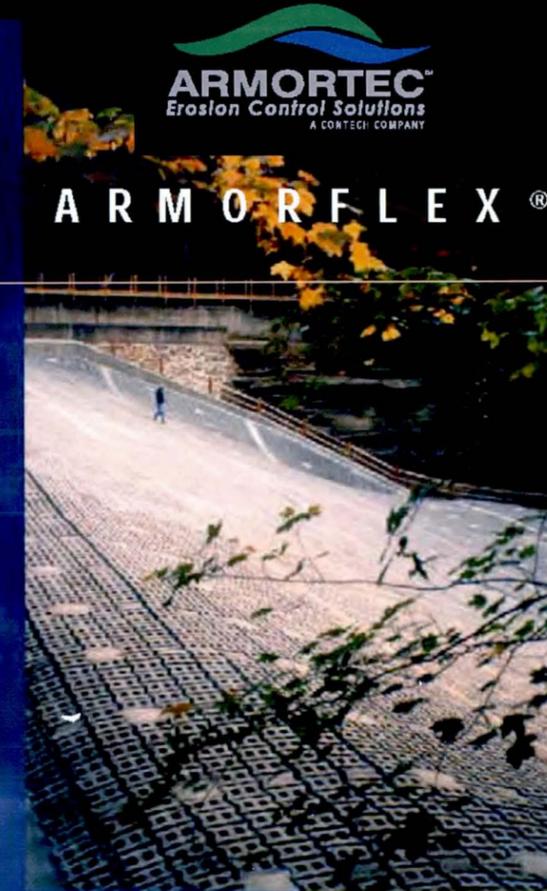
Mats subject to wave attack should be blinded with a sand/gravel mixture. Above normal waterline mats may be topsoiled and seeded to give a "green" effect.



BACKFILL & VEGETATION

Proper toe trench requires a minimum of 2 rows of block buried below predicated soil depth.

Mats subject to wave attack are required to have a bedding layer of crushed stone or gravel.



ARTICULATING CONCRETE BLOCK REVETMENT SYSTEM

APPLICATIONS

- CHANNEL LINING • RIVERBANK PROTECTION
- DRAINAGE DITCH LINING • PIPELINE PROTECTION
- BOAT RAMPS • RESERVOIR SLOPE PROTECTION
- LAKE SHORELINE PROTECTION
- BRIDGE ABUTMENT PROTECTION
- DIKS AND LEVY PROTECTION
- DAM CRESTS AND SPILLWAYS
- WEIRS AND OVERFLOW CHANNELS

OTHER ARMORTEC® BROCHURES

- ARMORLOC • A-JACKS COASTAL
- A-JACKS STREAMBANK & SCOUR
- ARMORTEC MULTI-PRODUCT
- ARMORFLEX HAND PLACED • ARMORFLEX OS
- ARMORWEDGE



AUTHORIZED AGENT

ARMORTEC is a subsidiary of

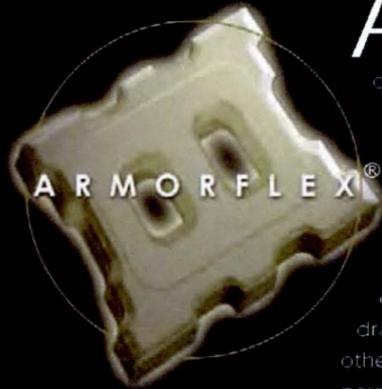


9025 Centre Pointe Drive  
Suite 400  
West Chester, OH 45069  
Toll Free (866) 551-8325  
www.contechess.com  
www.armortecsoftware.com

ARMORTEC, INC. doing business in Florida as ARMORTEC EROSION CONTROL SOLUTIONS, INC. © 2007 ARMORTEC. All Rights Reserved. AAF06



EROSION CONTROL SOLUTIONS



**A**rmorFlex is a flexible, interlocking matrix of concrete blocks of uniform size, shape and weight connected by a series of cables which pass longitudinally through preformed ducts in each block. ArmorFlex is installed over site specific filter fabric on a prepared surface. ArmorFlex revetment systems combine the favorable aspects of lightweight blankets and meshes, such as porosity, flexibility, vegetation encouragement and habitat enhancement with nonerrodible, self-weight and high tractive force resistance of a rigid lining.

ArmorFlex has proven to be an aesthetic and functional alternative to dumped stone riprap, gabions, structural concrete and other heavy-duty, durable erosion protection systems. ArmorFlex is easy to install, therefore, can dramatically reduce overall project costs. More specifically, when compared to other systems, life-cycle costs have been reduced because ArmorFlex is a permanent system and saves on subsequent maintenance expenses.



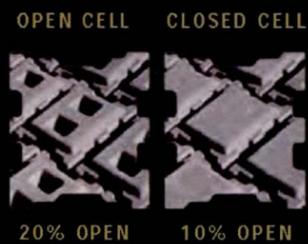
### ARMORFLEX® BLOCK SPECIFICATIONS

STANDARD CLASS  
CONCRETE BLOCK  
OPEN AREA 20%

CONCRETE BLOCK CLASS	OPEN/CLOSED CELL	NOMINAL DIMENSIONS			GROSS AREA/ (sq. ft.)	BLOCK WEIGHT		OPEN AREA %
		L	W	H		lbs.	lbs./sq. ft.	
30s	Open	13.0	11.6	4.75	0.98	31-36	32-37	20
50s	Open	13.0	11.6	6.00	0.98	45-52	45-53	20
40	Open	17.4	15.5	4.75	1.77	62-71	35-40	20
50	Open	17.4	15.5	6.00	1.77	81-94	46-53	20
70	Open	17.4	15.5	8.50	1.77	120-138	68-78	20
40L	Open	17.4	23.6	4.75	2.58	90-106	35-41	20
70L	Open	17.4	23.6	8.50	2.58	173-201	67-78	20
45s	Closed	13.0	11.6	4.75	0.98	39-45	40-45	10
55s	Closed	13.0	11.6	6.00	0.98	53-61	54-62	10
45	Closed	17.4	15.5	4.75	1.77	78-89	43-50	10
55	Closed	17.4	15.5	6.00	1.77	94-108	53-61	10
85	Closed	17.4	15.5	8.50	1.77	145-167	82-98	10
45L	Closed	17.4	23.6	4.75	2.58	108-126	42-49	10
85L	Closed	17.4	23.6	8.50	2.58	209-243	81-94	10
<b>High Velocity Application Block Classes</b>								
40-T	Open	17.4	15.5	4.75	1.77	62-71	35-40	20
50-T	Open	17.4	15.5	6.00	1.77	81-94	46-53	20
70-T	Open	17.4	15.5	8.50	1.77	120-138	68-78	20

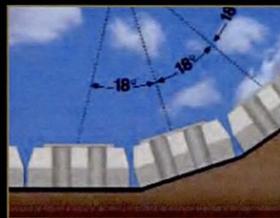
Note: Please see your local sales representative for regional block availability.

### BLOCK STYLES



When placed on a site specific filter fabric, the permeability of the revetment system relieves hydrostatic pressure in the subgrade. The system's capability for soil retention prevents leaching of subsols throughout the installation.

### FLEXIBILITY



ArmorFlex blocks are interconnected by flexible cables, providing articulation between adjacent blocks. Block walls are designed with beveled side walls to allow for flexibility in all directions.

### FEATURES & BENEFITS

- STABILITY
- FLEXIBILITY
- PERFORMANCE
- COST-EFFECTIVE
- VEGETATION
- PERMEABILITY
- EASY TO INSTALL



### MINIMUM PHYSICAL REQUIREMENTS

MIN. DENSITY (IN AIR) LBS/FT <sup>3</sup>		MIN. COMPRESSIVE STRENGTH PSI		MAX. WATER ABSORPTION LBS/FT <sup>3</sup>	
AVE. OF 3 UNITS	INDIVIDUAL UNIT	AVE. OF 3 UNITS	INDIVIDUAL UNIT	AVE. OF 3 UNITS	INDIVIDUAL UNIT
130	125	4,000	3,500	9.1	11.7

\*Unit weight and density values may vary due to availability of local materials.

### DAMS, SPILLWAYS, AND HIGH VELOCITY CHANNELS



ArmorFlex T-Series

ArmorFlex unique Tapered block design offers superior protection for embankment dams, spillways, and high velocity channels and chutes. The essential design component of the ArmorFlex Tapered system is a 0.5-inch taper that virtually eliminates destabilizing impact flow forces, thereby providing higher factors of safety. The ArmorFlex Tapered block system has been successfully tested under hydraulic jump conditions at Colorado State University.

### RESEARCH AND DESIGN

Since 1980, Armortec has initiated and participated in a wide range of research projects to evaluate the performance of ArmorFlex, including the following:

- Tetrattech model tests - California, U.S.A.
- Wave Attack Tests, Report No. M1910 - Delft Hydraulics Laboratory, 1982
- "Large-Scale model study of ArmorFlex slope protection" Tekmarine, Inc., May, 1984
- "Design for Reinforced Grass Waterways," - CIRIA Report 116, 1987
- "Minimizing Embankment Damage During Overtopping Flows," FHWA Report-RD-88-181 prepared by Simons, U and Associates, Inc, November 1988
- "Hydraulic Stability of Articulated Concrete Block Revetment Systems During Overtopping Flow," FHWA Report-RD-89-199 prepared by Simons, U and Associates, Inc., July 1989
- ArmorFlex Overtopping Test, prepared by Ayers Associates, Inc.

### RESEARCH PROVEN PERFORMANCE

Armortec has carried out extensive research into wave and open channel flow conditions on ArmorFlex in the United States and the Netherlands. Design manuals and computer programs are available to assist in the proper ArmorFlex block selection for your hydraulic conditions.



Dam Overtopping Tests



### ArmorFlex® (not to scale)

**Open Cell Block**      **Close Cell Block**

**TOP VIEW**      **TOP VIEW**

**SIDE VIEW**      **END VIEW**

**TOP VIEW**      **SIDE VIEW**      **END VIEW**

**Tapered Series**

**Tapered Series - Cross Section**

4" MIN DRAINAGE MEDIUM (2" ANGULAR CRUSHED STONE, TYP.)  
ARMORWEDGE TAPERED ARTICULATED CONCRETE BLOCK (TYP.)  
GEOGRID (TENSAR B1100, TYP.)  
SITE SPECIFIC GEOTEXTILE  
NATIVE SOIL  
TAPERED BLOCK TYPICAL CROSS SECTION  
NOT TO SCALE

**Top of Slope - Standard Detail**

BACKFILL WITH 4000 PSI GROUT CONCRETE OR APPROVED EQUAL  
2 UNIT MIN.  
AREA OF COVERAGE  
SITE SPECIFIC GEOTEXTILE  
Existing Subgrade  
1" MIN.

ArmorFlex Unit Specification								
Concrete Block Class	Open/Closed Cell	Nominal Dimensions			Block Weight		Open Area %	
		L	W	H	sq. ft.	lbs/sq. ft.		
30s	Open	13.0	11.6	4.75	0.98	31-36	32-37	20
50s	Open	13.0	11.6	6.00	0.98	45-52	45-53	20
40	Open	17.4	15.5	4.75	1.77	62-71	35-40	20
50	Open	17.4	15.5	6.00	1.77	81-94	46-53	20
70	Open	17.4	15.5	8.50	1.77	120-138	68-78	20
40L	Open	17.4	23.6	4.75	2.58	90-106	35-41	20
70L	Open	17.4	23.6	8.50	2.58	173-201	67-78	20
45s	Closed	13.0	11.6	4.75	0.98	39-45	40-45	10
55s	Closed	13.0	11.6	6.00	0.98	53-61	54-62	10
45	Closed	17.4	15.5	4.75	1.77	78-89	43-50	10
55	Closed	17.4	15.5	6.00	1.77	94-108	53-61	10
85	Closed	17.4	15.5	8.50	1.77	145-167	82-98	10
45L	Closed	17.4	23.6	4.75	2.58	108-126	42-49	10
85L	Closed	17.4	23.6	8.50	2.58	209-243	81-94	10
High Velocity Application Block Classes								
40-T	Open	17.4	15.5	4.75	1.77	62-71	35-40	20
50-T	Open	17.4	15.5	6.00	1.77	81-94	46-53	20
70-T	Open	17.4	15.5	8.50	1.77	120-138	68-78	20

### ArmorFlex® cont. (not to scale)

**Typical Mat**

REVESTMENT CABLE  
REVESTMENT CABLE SLEEVE  
REVESTMENT WASHER  
REVESTMENT CABLE SLEEVE  
REVESTMENT WASHER  
N.T.S.

### A-Jacks® (not to scale)

**A-Jacks Placement Profile**

**A-Jacks Unit**

A-Jacks Unit Specification					
A-JACKS	L (IN)	T (IN)/H (IN)	C (IN)	VOL (FT <sup>3</sup> )	WT (LBS)
AJ-24	24	4	1.84	0.56	78
AJ-48	48	7.36	3.68	4.49	629
AJ-72	72	11.04	5.52	15.14	2,120
AJ-96	96	14.72	7.396	35.87	5,022
AJ-120	120	18.40	9.20	70.69	9,699

### ArmorWedge® (not to scale)

**Side View - Typical Block**

ArmorWedge Unit Specification					
UNIT DIMENSION	UNIT WEIGHT (LBS)	SYSTEM WEIGHT (LBS)	UNIT COVERAGE (SF)	COMPRESSIVE STRENGTH (PSI)	MAXIMUM ABSORPTION (LBS/FT <sup>2</sup> )
12x18	40-52	36-40	1.1875	4000	12



APPENDIX B – FRS No. 3 Outlet Design Capacity Memorandum



**Flood Control District**  
of Maricopa County

PROJECT MEMORANDUM

**Date:** November 16, 2009

**To:** Gary Wesch, P.E.  
Project Manager

**From:** Michael Greenslade, P.E.  
Project Manager

**Subject:** White Tanks FRS No. 3 Outlet Design Capacity

In your e-mail of November 3, 2009 you requested clarification regarding the design outlet capacity for White Tanks FRS No. 3. You indicated that your meeting notes reference a capacity of 230 cfs which corresponds to the capacity when the reservoir water surface elevation is at the crest of the auxiliary (emergency) spillway. In order to clearly understand the channel capacity needed for discharges through the principal spillway the design and the operational procedures for the interim and future conditions must be understood. For reference in this discussion, the discharge rating curve for the principal spillway and gated outlet (Table 14-2) from the White Tanks No. 3 Phase 1 design is attached.

The principal spillway consists of two 48" pipes of which one is connected to a stand alone gated outlet and the other is connected to an NRCS riser which includes a bypass gated outlet. With the NRCS riser currently capped (interim condition), the 48" pipe connected to the NRCS riser can be utilized via the bypass gated outlet. The capping of the NRCS riser was done so that uncontrolled flows through the principal spillway would not occur until outlet channels had been constructed and uncontrolled flows could be safely discharged (ultimate future condition). The ultimate future condition is defined as follows:

- The overall rehabilitation of White Tanks FRS No. 3 and White Tanks FRS No. 4 is completed,
- The outlet channel from White Tanks No. 3 to White Tanks No. 4 has been constructed,
- The outlet channel from White Tanks No. 4 has been constructed, and
- The earth fissure risk at White Tanks No. 3 has either been reduced due to additional studies or mitigated through design.

While the 30% design for the outlet channel assumed a capacity utilizing both the 48" pipes with the principal spillway uncapped (537 cfs) a review of the original design intent and preferred operational procedures indicates that a capacity significantly less is needed. Future operation in the ultimate future condition defined above assumes the principal spillway (right 48" pipe) is uncapped and connected to the outlet channel. The stand alone gated outlet (left 48" pipe) should not be



White Tanks FRS No. 3 Outlet Design Capacity  
November 16, 2009  
Page 2 of 2

connected to the outlet channel and therefore its capacity ignored for the outlet channel design. The purpose for not connecting the stand alone gated outlet to the outlet channel is that operationally this outlet will only be utilized if there is a condition where the outlet channel should not be utilized as discussed below:

- Following construction of the White Tanks FRS No. 3 outlet channel and under certain flooding conditions there may be a need to prohibit flows from White Tanks FRS No. 3 to the outlet channel prior to construction completion of the White Tanks FRS No. 4 outlet channel. Under these flooding conditions, the stand alone gated outlet would only be utilized after implementation of the District's emergency action plan (EAP).
- A condition where the stand alone gated outlet might be utilized in the ultimate future condition is one where a hazard exists within the earth fissure risk zone such that discharges into the outlet channel would create a dam safety concern to White Tanks FRS No. 3 and discharges should be directed away from the earth fissure risk zone. Under this condition, the stand alone gated outlet would only be utilized after implementation of the District's EAP.

**Recommendations**

Based on the planned operational procedures and ultimate future condition the outlet channel should be designed for the discharge associated with the principal spillway uncapped. Under this condition, a maximum discharge of **284 cfs** will occur when the water surface elevation is at its maximum (PMF elevation) which is 1,216 feet (NAVD 88).

The design for any structure to accommodate the stand alone gated outlet should be for a maximum discharge of 253 cfs that will occur during operation of this structure at a maximum water surface elevation discussed above. Typically, the stand alone gated outlet will not be operated until spillway flows have ceased but to ensure the outlet channel design capacity is not exceeded the maximum discharge should be utilized for design.

Furthermore, the design of the conveyance system through the emergency spillway should be such that failure will not occur during spillway flows and the calculated scour resulting from those flows. The analysis should include modifications to the final approved SITES models to account for the conveyance system.

TABLE 14-2  
Outlet Works Discharge Rating Curve

Elevation (feet) (NAVD 88)	Future Condition (Principal Spillway Open)			Interim Condition & Future Condition (Principal Spillway Closed)		
	Discharge (cfs)			Discharge (cfs)		
	Gated Outlet (48-inch)	Principal Spillway <sup>1</sup> (48-inch)	Combined	Gated Outlet (48-inch)	Gated Principal Spillway Bypass outlet (48-inch)	Combined
1,197	-	-	-	-	-	-
1,199	24	-	24	24	24	48
1,201	87	76	163	87	87	174
1,203	123	181	304	123	123	246
1,205	150	201	351	150	150	300
1,207	173	218	391	173	173	346
1,209	194	234	428	194	194	388
1,211	212	249	461	212	212	424
1,212	221	257	478	221	221	442
1,213	229	264	493	229	229	458
1,214	237	270	507	237	237	474
1,215	245	277	522	245	245	490
1,216	253	284	537	253	253	506
1,217	260	290	550	260	260	520
1,218	267	296	563	267	267	534

Notes:

1. Principal spillway crest elevation is set at 1,200 ft (NAVD 88).





### APPENDIX C – HYDROLOGIC MODELING

#### C.1 SCHEMATIC MAPS

SCHEMATIC MAP FOR FRS#3 AREA HEC-1 MODEL  
ADOPTED FROM LOOP 303/WHITE TANKS ADMPU AREA HYDROLOGIC ANALYSIS (HDR,2009)

-  SUB-BASIN
-  DIVERSION
-  RETENTION
-  CHANNEL ROUTING
-  CONCENTRATION POINT
-  STORAGE ROUTING



FIGURE 31 – SCHEMATIC MAP FOR FRS#3 AREA HEC-1 MODEL

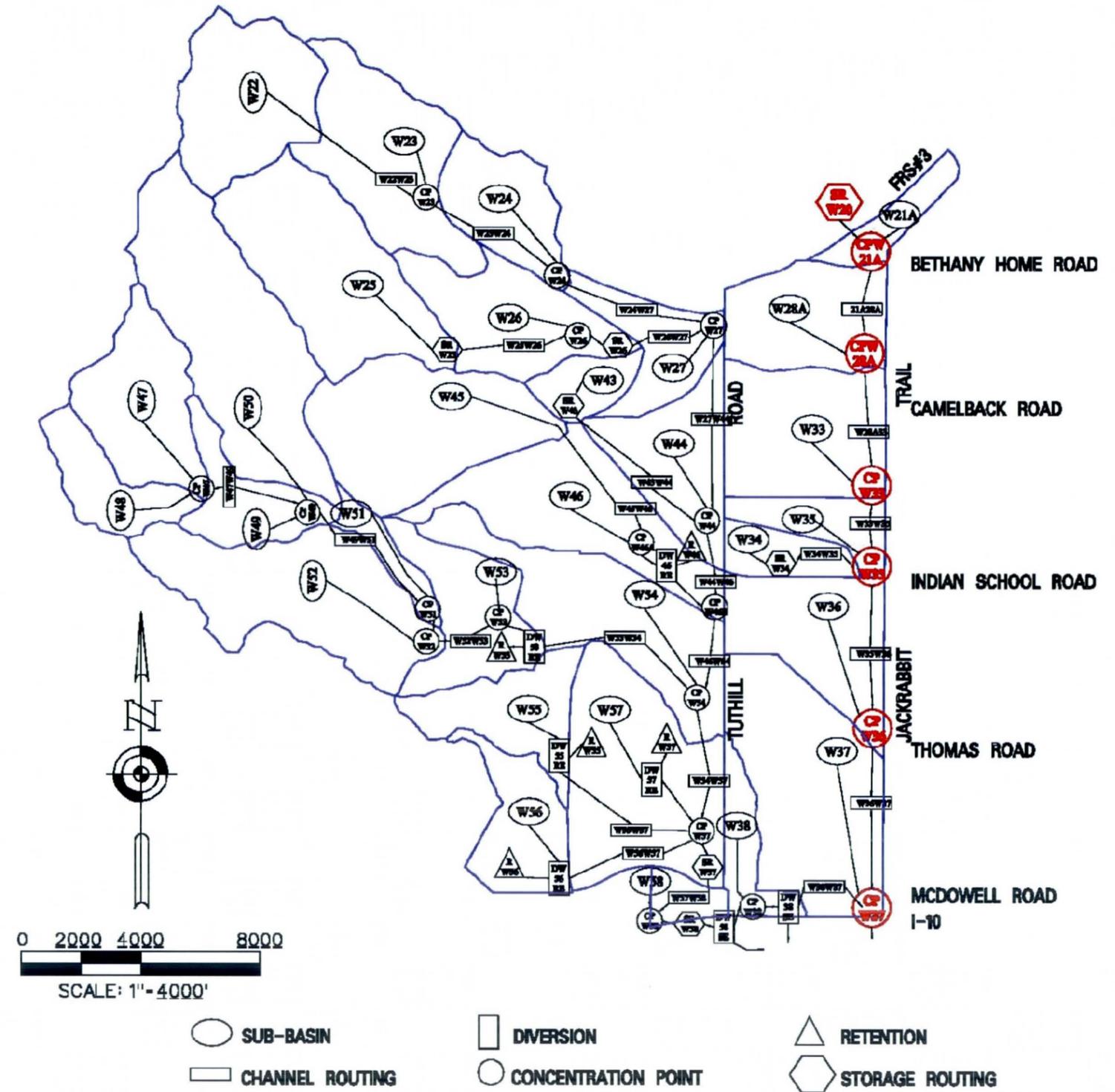


FIGURE 32 – SCHEMATIC MAP FOR JACKRABBIT CORRIDOR HEC-1 MODEL,  
EXISTING CONDITION WITH PROJECT IN PLACE

SCHEMATIC MAP FOR JACKRABBIT CORRIDOR HEC-1 MODEL  
WITH PROJECT-IN-PLACE

UPDATE BASED ON LOOP 303/WHITE TANKS ADMPU AREA HYDROLOGIC ANALYSIS (HDR,2009)









196	KK	W09W10	ROUTE																	
197	RS	1	FLOW	-1																
198	RC	0.035	0.022	0.035	11134	0.0683	0.00													
199	RX	100.00	137.00	172.00	192.00	220.00	230.00	284.00	338.00											
200	RY	1990.0	1975.00	1960.00	1950.00	1950.00	1960.00	1975.00	1990.00											
	*																			

201	KK	W10	BASIN																	
202	BA	1.338																		
203	LG	0.10	0.25	3.95	0.40	25														
204	UI	0	395	1548	2646	1783	1282	874	611	394	273									
205	UI	184	135	70	52	53	53	0	0	0	0									
206	UI	0	0	0	0	0	0	0	0	0	0									
207	UI	0	0	0	0	0	0	0	0	0	0									
208	UI	0	0	0	0	0	0	0	0	0	0									
	*																			

209	KK	CPW10	COMBINE																	
210	HC	2	3.137																	
	*																			

211	KK	W11	BASIN																	
212	BA	0.812																		
213	LG	0.10	0.25	3.95	0.40	25														
214	UI	0	275	1046	1697	1048	762	488	340	214	147									
215	UI	93	65	34	34	34	0	0	0	0	0									
216	UI	0	0	0	0	0	0	0	0	0	0									
217	UI	0	0	0	0	0	0	0	0	0	0									
218	UI	0	0	0	0	0	0	0	0	0	0									
	*																			

219	KK	CPW11	COMBINE																	
220	HC	2	3.949																	
	*																			

221	KK	W11W12	ROUTE																	
222	RS	6	FLOW	-1																
223	RC	0.035	0.022	0.035	21182	0.0205	0.00													
224	RX	100.00	107.00	114.00	125.00	140.00	154.00	244.00	334.00											
225	RY	1310.0	1309.00	1308.00	1306.00	1305.90	1308.00	1309.00	1310.00											
	*																			

226	KK	W12	BASIN																	
227	BA	1.805																		
228	LG	0.18	0.25	4.60	0.46	14														
229	UI	0	176	316	723	1114	1380	1905	1487	1091	947									
230	UI	808	705	564	448	406	338	262	222	192	151									
231	UI	137	103	85	87	64	34	34	34	34	34									
232	UI	33	34	0	0	0	0	0	0	0	0									
233	UI	0	0	0	0	0	0	0	0	0	0									
	*																			

1 HEC-1 INPUT PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

234	KK	CPW12	COMBINE																	
235	HC	3	11.547																	
	*																			

236	KK	W12W13	ROUTE																	
237	RS	1	FLOW	-1																
238	RC	0.022	0.022	0.022	2059	0.0121	0.00													
239	RX	100.00	107.00	124.00	130.00	159.00	165.00	177.00	183.00											
240	RY	1230.0	1228.00	1224.00	1222.00	1221.90	1224.00	1228.00	1230.00											
	*																			

241	KK	W13	BASIN																	
242	BA	1.584																		
243	LG	0.21	0.25	4.90	0.36	14														
244	UI	0	163	322	742	1082	1371	1809	1158	947	811									
245	UI	694	579	443	387	335	252	205	181	140	125									
246	UI	91	80	80	46	31	32	31	31	31	32									
247	UI	31	0	0	0	0	0	0	0	0	0									
248	UI	0	0	0	0	0	0	0	0	0	0									
	*																			

249	KK	CPW13	COMBINE																	
250	HC	2	13.131																	
	*																			

251	KK	W13W16	ROUTE																	
252	RS	3	FLOW	-1																
253	RC	0.035	0.022	0.035	6232	0.0042	0.00													
254	RX	100.00	167.00	178.00	189.00	218.00	228.00	239.00	250.00											
255	RY	1216.0	1214.00	1212.00	1210.00	1209.90	1212.00	1214.00	1216.00											
	*																			

256	KK	W15	BASIN																	
257	BA	1.227																		
258	LG	0.25	0.25	4.55	0.40	24														
259	UI	0	140	338	725	1009	1399	1252	848	726	601									
260	UI	489	377	321	260	195	162	134	109	82	68									
261	UI	70	31	27	27	27	27	27	26	0	0									
262	UI	0	0	0	0	0	0	0	0	0	0									
263	UI	0	0	0	0	0	0	0	0	0	0									
	*																			

264	KK	DW15RE	DIVERT																	
265	DT	W15R	91.9	0.0																
266	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0									
267	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0									
	*																			

268	KK	W14	BASIN																	
269	BA	1.582																		
270	LG	0.14	0.25	5.20	0.37	19														
271	UI	0	330	1263	2143	2612	1581	1214	868	644	451									
272	UI	324	238	167	134	76	52	52	53	0	0									
273	UI	0	0	0	0	0	0	0	0	0	0									

HEC-1 INPUT PAGE 8

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

274	UI	0	0	0	0	0	0	0	0	0	0									
275	UI	0	0	0	0	0	0	0	0	0	0									
	*																			

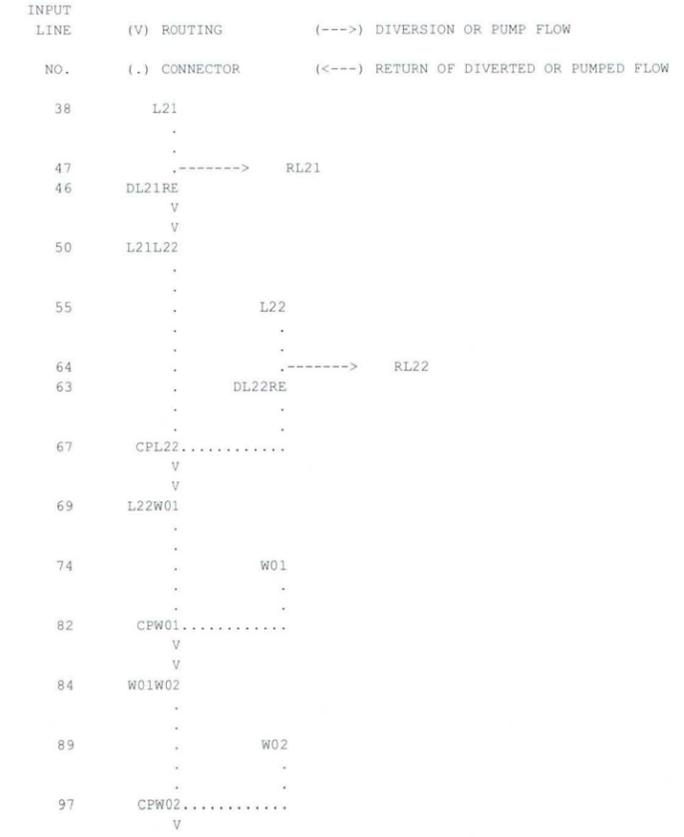
276	KK	W14W15	ROUTE																	
277	RS	1	FLOW	-1																
278	RC	0.025	0.025	0.025	7308	0.0104	0.00													
279	RX	100.00	105.00	109.00	125.00	135.00	151.00	155.00	160.00											



306	RY	1000.0	999.50	999.00	995.00	995.10	999.00	999.50	1000.00											
307	KK	W18	BASIN																	
308	BA	1.260																		
309	LG	0.24	0.25	4.40	0.44	46														
310	UI	0	7025	2342	356	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
311	UI	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
312	UI	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
HEC-1 INPUT																				
LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10									
313	UI	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
314	UI	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
315	KK	DW18RE	DIVERT																	
316	DT	W18R	94.3	0.0																
317	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
318	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
319	KK	W17	BASIN																	
320	BA	1.497																		
321	LG	0.28	0.25	4.30	0.43	24														
322	UI	0	266	1071	1806	2464	1531	1172	893	631	493									
323	UI	334	263	187	126	121	49	47	47	47	0									
324	UI	0	0	0	0	0	0	0	0	0	0									
325	UI	0	0	0	0	0	0	0	0	0	0									
326	UI	0	0	0	0	0	0	0	0	0	0									
327	KK	W17W18	ROUTE																	
328	RS	1	FLOW	-1																
329	RC	0.045	0.035	0.045	8559	0.0257	0.00													
330	RX	100.00	140.00	150.00	156.00	194.00	216.00	255.00	342.00											
331	RY	1302.0	1300.00	1298.00	1296.00	1295.90	1298.00	1300.00	1302.00											

358	LG	0.26	0.25	4.10	0.54	25														
359	UI	0	138	365	765	1050	1503	993	779	662	534									
360	UI	409	332	276	203	166	136	105	82	67	65									
361	UI	27	26	27	26	27	26	0	0	0	0									
362	UI	0	0	0	0	0	0	0	0	0	0									
363	UI	0	0	0	0	0	0	0	0	0	0									
364	KK	DW20RE	DIVERT																	
365	DT	W20R	85.2	0.0																
366	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0									
367	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0									
368	KK	CPW20	COMBINE																	
369	HC	4	21.522																	
370	KK	SRW20	STORAGE																	
371	KM	STAGE-STORAGE-DISCHARGE CURVE FROM URS DESIGN OF FRS#3 OUTLET STRUCTURE																		
372	KM	THE DISCHARGE INCLUDING OUTFLOW FROM PRINCIPAL AND EMERGENCY SPILLWAY,																		
373	KM	AS WELL AS INFILTRATION																		
374	RS	1	STOR	-1																
375	SV	44.8	388	585	846	1002	2045	3218	3557	4693	6510									
376	SQ	0.02	0.17	4.5	187	203	276	330	2936	24545	70439									
377	SE	1188	1198	1200	1202	1203	1208	1212	1213	1216	1220									
378	KK	OUTFL																		
379	KM	SEPRATE OUTFLOW FROM INFILTRATION																		
380	ZW	A=WT B=FRS3 C=FLOW																		
381	DT	INFL																		
382	DI	0	4.5	86	203	330	2936	24545	70439											
383	DQ	0	4.5	10	22	73	79	96	121											
384	ZZ																			

SCHEMATIC DIAGRAM OF STREAM NETWORK



351	KK	W19W20	ROUTE																	
352	RS	1	FLOW	-1																
353	RC	0.025	0.025	0.025	3790	0.0158	0.00													
354	RX	100.00	105.00	109.00	125.00	135.00	151.00	155.00	160.00											
355	RY	1000.0	999.50	999.00	995.00	995.10	999.00	999.50	1000.00											
356	KK	W20	BASIN																	
357	BA	1.137																		

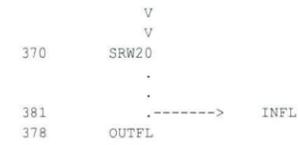


```

99      V
      W02W05
104      .
      .      W03
      .      V
      .      V
112      .      W03W04
      .
      .      .      W04
      .      .
125      .      CPW04.....
      .      V
      .      V
127      .      W04W05
      .
      .      .      W05
      .      .
140      CPW05.....
      .      V
      .      V
142      SRW05
      .      V
      .      V
148      W05W12
      .
      .      .      W06
      .      .
161      .      .      W07
      .      .
169      .      CPW07.....
      .      V
      .      V
171      .      W07W08
      .
      .      .      W08
      .      .
184      .      CPW08.....
      .
      .      .      W09
      .      .
194      .      CPW09.....
      .      V
      .      V
196      .      W09W10
      .
      .      .      W10
      .      .
201      .      .      CPW10.....
      .      .
211      .      .      W11
      .      .
219      .      CPW11.....
      .      V
      .      V
221      .      W11W12
      .
      .      .      W12
      .      .
226      .      .      CPW12.....
      .      V
      .      V
234      .      W12W13
236
  
```

```

241      .      .      W13
      .      .
249      CPW13.....
      .      V
      .      V
251      W13W16
      .
      .      .      W15
      .      .
256      .      .      W15R
      .      .      .
265      .      .      .      W14
264      .      .      .      V
      .      .      .      V
      .      .      .      W14W15
276      .      .      .
      .      .      .
281      .      CPW15.....
      .      V
      .      V
283      .      W15W16
      .
      .      .      W16
      .      .
288      .      .      .      W16R
297      .      .      .      .
296      .      .      .      .
      .      .      .      .
300      CPW16.....
      .      V
      .      V
302      W16W20
      .
      .      .      W18
      .      .
307      .      .      .      W18R
316      .      .      .      .
315      .      .      .      .
      .      .      .      .
319      .      .      .      W17
      .      .      .      V
      .      .      .      V
327      .      .      .      W17W18
      .      .      .
      .      .      .      CPW18.....
332      .      .      .      V
      .      .      .      V
334      .      W18W20
      .
      .      .      W19
      .      .
339      .      .      .      RW19
348      .      .      .      .
347      .      .      .      .
      .      .      .      .
      .      .      .      .
351      .      .      .      W19W20
      .      .      .
      .      .      .      W20
356      .      .      .      .
      .      .      .      .
365      .      .      .      .
364      .      .      .      .
      .      .      .      .
      .      .      .      .
368      CPW20.....
  
```



RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	L21	80.	13.58	31.	9.	3.	.52		
DIVERSION TO	RL21	80.	13.58	31.	9.	3.	.52		
HYDROGRAPH AT	DL21RE	0.	.00	0.	0.	0.	.52		
ROUTED TO	L21L22	0.	.00	0.	0.	0.	.52		
HYDROGRAPH AT	L22	21.	14.75	10.	2.	1.	.36		
DIVERSION TO	RL22	21.	14.75	10.	2.	1.	.36		
HYDROGRAPH AT	DL22RE	0.	.00	0.	0.	0.	.36		
2 COMBINED AT	CPL22	0.	.00	0.	0.	0.	.89		
ROUTED TO	L22W01	0.	.00	0.	0.	0.	.89		
HYDROGRAPH AT	W01	37.	13.00	9.	2.	1.	.19		
2 COMBINED AT	CPW01	37.	13.00	8.	2.	1.	1.08		
ROUTED TO	W01W02	35.	13.25	8.	2.	1.	1.08		
HYDROGRAPH AT	W02	193.	12.42	27.	8.	3.	.39		
2 COMBINED AT	CPW02	194.	12.42	35.	10.	3.	1.47		
ROUTED TO	W02W05	179.	12.58	35.	10.	3.	1.47		
HYDROGRAPH AT	W03	965.	12.33	142.	45.	15.	1.97		
ROUTED TO	W03W04	729.	12.67	142.	45.	15.	1.97		
HYDROGRAPH AT	W04	1086.	12.33	164.	51.	17.	2.03		
2 COMBINED AT	CPW04	1497.	12.42	304.	95.	32.	4.01		
ROUTED TO	W04W05	1432.	12.58	304.	95.	32.	4.01		
HYDROGRAPH AT	W05	216.	12.33	21.	6.	2.	.32		

+	3 COMBINED AT	CPW05	1681.	12.58	358.	111.	37.	5.79
+	ROUTED TO	SRW05	1655.	12.67	358.	111.	37.	5.79
+	ROUTED TO	W05W12	1593.	12.75	358.	111.	37.	5.79
+	HYDROGRAPH AT	W06	561.	12.17	53.	17.	6.	.71
+	HYDROGRAPH AT	W07	447.	12.08	57.	20.	7.	.31
+	2 COMBINED AT	CPW07	992.	12.17	110.	37.	12.	1.02
+	ROUTED TO	W07W08	934.	12.17	110.	37.	12.	1.02
+	HYDROGRAPH AT	W08	490.	12.08	39.	12.	4.	.44
+	2 COMBINED AT	CPW08	1397.	12.17	148.	48.	16.	1.46
+	HYDROGRAPH AT	W09	442.	12.08	47.	16.	5.	.34
+	2 COMBINED AT	CPW09	1807.	12.17	194.	64.	21.	1.80
+	ROUTED TO	W09W10	1512.	12.25	194.	64.	21.	1.80
+	HYDROGRAPH AT	W10	1133.	12.17	116.	35.	12.	1.34
+	2 COMBINED AT	CPW10	2578.	12.25	309.	99.	33.	3.14
+	HYDROGRAPH AT	W11	716.	12.17	71.	22.	7.	.81
+	2 COMBINED AT	CPW11	3247.	12.17	379.	120.	40.	3.95
+	ROUTED TO	W11W12	2332.	12.67	378.	120.	40.	3.95
+	HYDROGRAPH AT	W12	778.	12.42	117.	34.	11.	1.80
+	3 COMBINED AT	CPW12	4296.	12.67	838.	261.	87.	11.55
+	ROUTED TO	W12W13	4269.	12.67	838.	261.	87.	11.55
+	HYDROGRAPH AT	W13	762.	12.42	109.	32.	11.	1.58
+	2 COMBINED AT	CPW13	4666.	12.67	936.	289.	97.	13.13
+	ROUTED TO	W13W16	4547.	12.83	936.	289.	97.	13.13
+	HYDROGRAPH AT	W15	674.	12.33	100.	31.	10.	1.23
+	DIVERSION TO	W15R	674.	12.33	100.	31.	10.	1.23
+	HYDROGRAPH AT	DW15RE	0.	.00	0.	0.	0.	1.23
+	HYDROGRAPH AT	W14	1120.	12.25	119.	36.	12.	1.58



+	ROUTED TO	W14W15	876.	12.33	119.	35.	12.	1.58
+	2 COMBINED AT	CPW15	871.	12.33	119.	35.	12.	2.81
+	ROUTED TO	W15W16	758.	12.50	119.	35.	12.	2.81
+	HYDROGRAPH AT	W16	347.	12.42	41.	12.	4.	.53
+	DIVERSION TO	W16R	347.	12.42	41.	12.	4.	.53
+	HYDROGRAPH AT	DW16RE	0.	.00	0.	0.	0.	.53
+	3 COMBINED AT	CPW16	4956.	12.83	1034.	318.	107.	16.47
+	ROUTED TO	W16W20	4940.	12.83	1034.	318.	107.	16.47
+	HYDROGRAPH AT	W18	1778.	12.08	140.	46.	15.	1.26
+	DIVERSION TO	W18R	1778.	12.08	140.	46.	15.	1.26
+	HYDROGRAPH AT	DW18RE	2.	22.42	1.	0.	0.	1.26
+	HYDROGRAPH AT	W17	1020.	12.25	119.	37.	12.	1.50
+	ROUTED TO	W17W18	735.	12.42	119.	37.	12.	1.50
+	2 COMBINED AT	CPW18	732.	12.42	118.	37.	12.	2.76
+	ROUTED TO	W18W20	656.	12.58	118.	36.	12.	2.76
+	HYDROGRAPH AT	W19	1610.	12.17	212.	74.	25.	1.16
+	DIVERSION TO	RW19	1597.	12.08	151.	44.	15.	1.16
+	HYDROGRAPH AT	DW19RE	768.	12.33	99.	31.	10.	1.16
+	ROUTED TO	W19W20	624.	12.42	98.	31.	10.	1.16
+	HYDROGRAPH AT	W20	603.	12.33	88.	28.	9.	1.14
+	DIVERSION TO	W20R	603.	12.33	88.	28.	9.	1.14
+	HYDROGRAPH AT	DW20RE	0.	.00	0.	0.	0.	1.14
+	4 COMBINED AT	CPW20	5555.	12.83	1203.	374.	125.	21.52
+	ROUTED TO	SRW20	91.	22.17	91.	74.	35.	21.52
+	DIVERSION TO	INFL	11.	21.75	11.	9.	7.	21.52
+	HYDROGRAPH AT	OUTFL	81.	22.17	80.	64.	28.	21.52



C.3 FUTURE CONDITIONS WITH PROJECT IN PLACE, 10-YEAR FOR JACKRABBIT CORRIDOR

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 02DEC09 TIME 11:04:20 *
*****
  
```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
  
```

```

X X XXXXXXX XXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXX X
X X X X X
X X X X X
X X XXXXXXX XXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID FUTURE CONDITION 10-YEAR 24HOUR EVENT
2 ID PRECIPITATION FROM DDMSW
3 ID WHITE TANKS AREA, WATERSHED CONTRIBUTING TO FRS#3
4 ID PREPARED BY HOSKIN RYAN CONSULTANTS EXCLUSIVELY FOR
5 ID FRS#3 OUTLET CHANNEL DESIGN, 12-02-2009
6 ID BASED ON HDR HEC-1 MODEL OF FUTURE CONDITION WITH CIP
7 ID MODIFICATIONS INCLUDE:
8 ID (1) UPDATE WITH AVERAGE RAINFALL DEPTH FOR JACKRABBIT CORRIDOR
9 ID (2) CHANGE BASIN W21A TO UNDEVELOPMENT CONDITION
10 ID (3) ADD RETENTION DIVERSION FOR W28A
11 ID (4) REMOVE RETENTION DIVERSION FOR W33
12 ID (5) UPDATE VERRADO DEVELOPMENT FOR W34 AND W35
13 ID (6) UPDATE RETENTION FOR W36 AND W37 (ARROYO SECO DEVELOPMENT)
14 ID (7) DIVIDE BASIN W37 INTO W37A AND W37B
15 ID (8) UPDATE PROPOSED CHANNEL ALONG JACKRABBIT TRAIL
16 ID *****
17 ID Flood Control District of Maricopa County
18 ID FU_CIP_MB02 - Loop 303/ White Tanks ADMFU AHA
19 ID Major Basin: 02
20 ID 100 Year - Return Period
21 ID 24 Hour Storm
22 ID Multiple Storms
23 ID Unit Hydrograph: S-Graph
24 ID 03/08/2009
25 IT 5 1JAN99 1200 2000
26 IN 15
27 IO 5
*DIAGRAM
*
28 JD 2.353 0.0001
29 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
30 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
31 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
32 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
33 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
34 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
35 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
36 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
37 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
  
```

```

38 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
39 JD 2.235 10.0
*
40 KK WT3
41 KM OUTFLOW FROM WT FRS#3 OUTLET
42 BA 21.52
43 KO 5
44 ZR =QI A=WT B=FRS3 C=FLOW
*
HEC-1 INPUT PAGE 2
  
```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
45 KK W21A BASIN
46 KM FCD PROPERTY ADJACENT TO EMERGENCY AND PRINCIPAL SPILLWAY, NO LAND DEVELOPMEN
47 KM IN FUTURE
48 ZW A=WT B=W21A C=FLOW
49 BA 0.199
50 LG 0.35 0.35 4.35 0.40 0 0 0 0 0 0
51 UI 0 38 150 260 315 274 179 117 75 49
52 UI 30 23 8 8 9 0 0 0 0 0
53 UI 0 0 0 0 0 0 0 0 0 0
54 UI 0 0 0 0 0 0 0 0 0 0
55 UI 0 0 0 0 0 0 0 0 0 0
*
  
```

```

56 KK CPW21A COMBINE
57 ZW A=WT B=CPW21A C=FLOW
58 HC 2 0.199
*
  
```

```

59 KK 21A28A ROUTE
60 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=30FT, SIDE SLOPE 6:1
61 ZW A=WT B=21A28A C=FLOW
62 RS 4 FLOW -1
63 RC 0.045 0.035 0.045 3560 0.0010
64 RX 100 110 120 150 180 210 220 230
65 RY 1001 1000 1000 995 995 1000 1000 1001
*
  
```

```

66 KK W28A BASIN
67 BA 0.642
68 LG 0.26 0.25 4.55 0.41 22
69 UI 0 85 281 456 611 978 845 622 457 266
70 UI 145 96 47 26 26 27 0 0 0 0
71 UI 0 0 0 0 0 0 0 0 0 0
72 UI 0 0 0 0 0 0 0 0 0 0
73 UI 0 0 0 0 0 0 0 0 0 0
*
  
```

```

74 KK DW28AR
75 KM FUTURE DEVELOPMENT ON 301AC VACANT LAND OF MARACAY, 80% RETENTION VOLUME ASSU
76 KM (C=0.65) (P=2.3 IN)
77 ZW A=WT B=DW28AR C=FLOW
78 DT RW28A 30.0
79 DI 0 10000
80 DQ 0 10000
*
  
```

```

81 KK CPW28A COMBINE
82 ZW A=WT B=CPW28A C=FLOW
83 HC 2 0.841
*
HEC-1 INPUT PAGE 3
  
```

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
84 KK W28A33 ROUTE
85 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 4:1
86 ZW A=WT B=W28A33 C=FLOW
87 RS 5 FLOW -1
88 RC 0.045 0.035 0.045 4336 0.0010
89 RX 100 110 120 140 180 200 210 220
90 RY 1001 1000 1000 995 995 1000 1000 1001
*
  
```

```

91 KK W33 BASIN
  
```



92 ZW A=WT B=W33 C=FLOW  
 93 BA 0.839  
 94 LG 0.30 0.25 4.00 0.55 15  
 95 UI 0 96 254 469 595 819 1172 911 714 530  
 96 UI 367 191 142 97 37 29 30 29 0 0  
 97 UI 0 0 0 0 0 0 0 0 0 0  
 98 UI 0 0 0 0 0 0 0 0 0 0  
 99 UI 0 0 0 0 0 0 0 0 0 0  
 \*

100 KK CPW33 COMBINE  
 101 ZW A=WT B=CPW33 C=FLOW  
 102 HC 2 1.68  
 \*

103 KK W33W35 ROUTE  
 104 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 6:1  
 105 ZW A=WT B=W33W35 C=FLOW  
 106 RS 3 FLOW -1  
 107 RC 0.045 0.035 0.045 2658 0.0010  
 108 RX 100 110 116 152 192 228 240 250  
 109 RY 1001 1000 1000 994 994 1000 1000 1001  
 \*

\* UPDATE VERRADO DEVELOPMENT AT INDIAN SCHOOL AND JACKRABBIT TRAIL RD  
 \* PER VERRADO MASTER DRAINAGE PLAN PREPARED BY WOOD PATEL. THE SCHOOL  
 \* SITE (~0.184 SQ MI) COULD RETAIN 100-YR 24-HR RAINFALL, THEREFORE IS  
 \* REMOVED FROM HEC-1 MODEL AS NON-CONTRIBUTING AREA, PER VERRADO MDP.  
 \*

110 KK W34  
 111 KM THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN  
 112 KM L= .78 Lca= .35 S= 69.7 Kn= .054 LAG= 21  
 113 KM PHOENIX VALLEY S-GRAPH WAS USED FOR THIS BASIN  
 114 BA .238  
 115 LG .25 .25 3.95 .58 31  
 116 UI 40 161 238 384 397 267 176 80 48 22  
 117 UI 12 12 0. 0. 0. 0. 0. 0. 0. 0.  
 118 UI 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 \*

HEC-1 INPUT PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

119 KK W35  
 120 KM THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN  
 121 KM L= 0.860 Lca= .32 S= 49.2 Kn= .054 LAG= 23  
 122 KM PHOENIX VALLEY S-GRAPH WAS USED FOR THIS BASIN  
 123 BA .089  
 124 LG .25 .25 3.95 .57 25  
 125 UI 13 50 75 108 155 108 76 50 22 14  
 126 UI 7. 4. 4. 0. 0. 0. 0. 0. 0. 0.  
 127 UI 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 \*

128 KK CP35R  
 129 KM ADD HYDROGRAPHS AT SRW35  
 130 HC 2  
 \*

131 KK SRW35  
 132 KM RET BASIN AT CP30 - 54' WEIR OUTFALL  
 133 ZW A=WT B=SRW35 C=FLOW  
 134 RS 1 STOR 0 0  
 135 SV 0 3.67 7.67 12.21 17.26 19.89 22.59 25.36 28.21  
 136 SE 1153 1154 1155 1156 1157 1157.5 1158 1158.5 1159  
 137 SQ 0.1 0.11 0.12 0.13 0.14 0.15 0.15 50.21 142.02  
 \*

138 KK CPW35  
 139 KM ADD HYDROGRAPHS AT JACKRABBIT TRAIL AND INDIAN SCHOOL RD  
 140 ZW A=WT B=CPW35 C=FLOW  
 141 HC 2  
 \*

142 KK W35W36 ROUTE  
 143 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 4:1  
 144 ZW A=WT B=W35W36 C=FLOW  
 145 RS 7 FLOW -1  
 146 RC 0.045 0.035 0.045 6051 0.0010

147 RX 100 110 116 140 180 204 220 230  
 148 RY 1001 1000 1000 994 994 1000 1000 1001  
 \*

149 KK W36 BASIN  
 150 BA 0.720  
 151 LG 0.30 0.25 4.00 0.55 15  
 152 UI 0 75 166 331 432 543 773 886 660 517  
 153 UI 403 292 150 125 75 48 23 23 23 23  
 154 UI 0 0 0 0 0 0 0 0 0 0  
 155 UI 0 0 0 0 0 0 0 0 0 0  
 156 UI 0 0 0 0 0 0 0 0 0 0  
 \*

HEC-1 INPUT PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

157 KK DW36RE DIVERT  
 158 KM ARROYO SECO FUTURE DEVELOPMENT HOLDS 127AC VACANT LAND IN BASIN W36. ASSUME 8  
 159 KM 100-YEAR 2-HOUR RETENTION. (C=0.65) (P=2.3IN). PASSQUALITY MOUNTAIN RANCH  
 160 KM PROVIDES A DETENTION BASIN OF NEGLIGIBLE SIZE AND NO RETENTION.  
 161 ZW A=WT B=DW36RE C=FLOW  
 162 DT RW36 12.7  
 163 DI 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0  
 164 DQ 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0  
 \*

165 KK CPW36 COMBINE  
 166 ZW A=WT B=CPW36 C=FLOW  
 167 HC 2 2.911  
 \*

168 KK W36W37 ROUTE  
 169 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=30FT, SIDE SLOPE 5:1  
 170 ZW A=WT B=W36W37 C=FLOW  
 171 RS 5 FLOW -1  
 172 RC 0.045 0.035 0.045 4527 0.0010  
 173 RX 100 110 120 150 180 210 220 230  
 174 RY 1001 1000 1000 994 994 1000 1000 1001  
 \*

175 KK W37A  
 176 KM LG VARIABLE VALUES FROM HDR MODEL.  
 177 KM THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN  
 178 KM L= 1.9 Lca= 1.0 S= 60.1 Kn= .034 LAG= 28.5  
 179 KM PHOENIX VALLEY S-GRAPH WAS USED FOR THIS BASIN  
 180 BA .63  
 181 LG .29 .25 4.30 .48 19.00  
 182 UI 74. 203. 370. 478. 657. 903. 674. 517. 388. 244.  
 183 UI 128. 96. 62. 23. 23. 23. 23. 0. 0. 0.  
 184 UI 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 \*

185 KK DW37AR DIVERT  
 186 KM ARROYO SECO FUTURE DEVELOPMENT HOLDS 162AC VACANT LAND IN BASIN W37A. ASSUME  
 187 KM 80% 100-YEAR 2-HOUR RETENTION. (C=0.65) (P=2.3IN). THE SOUTH SUBDIVISION IN  
 188 KM BASIN W37A DOES NOT PROVIDE RETENTION.  
 189 ZW A=WT B=DW37AR C=FLOW  
 190 DT RW37A 16.1  
 191 DI 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0  
 192 DQ 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0  
 \*

193 KK CPW37A COMBINE  
 194 ZW A=WT B=CPW37A C=FLOW  
 195 HC 2 3.541  
 \*

HEC-1 INPUT PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

196 KK W37B  
 197 KM LG VARIABLE VALUES FROM HDR MODEL.  
 198 KM THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN  
 199 KM L= 2.0 Lca= 1.0 S= 59.2 Kn= .034 LAG= 28.7  
 200 KM PHOENIX VALLEY S-GRAPH WAS USED FOR THIS BASIN  
 201 BA .67  
 202 LG .29 .25 4.30 .48 19.00

1

1

1



203	UI	79.	214.	390.	503.	686.	962.	720.	553.	416.	270.
204	UI	137.	105.	69.	24.	24.	24.	24.	0.	0.	0.
205	UI	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
*											
206	KK	DW37BR DIVERT									
207	KM	ARROYO SECO FUTURE DEVELOPMENT HOLDS 30AC VACANT LAND IN BASIN W37B. ASSUME									
208	KM	80% 100-YEAR 2-HOUR RETENTION. (C=0.65) (P=2.3IN). THE SOUTH SUBDIVIION IN									
209	KM	BASIN W37B DOES NOT PROVIDE RETENTION.									
210	ZW	A=WT B=DW37BR C=FLOW									
211	DT	RW37B 3.0									
212	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0
213	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0
*											
214	KK	CPW37B COMBINE									
215	ZW	A=WT B=CPW37B C=FLOW									
216	HC	2 4.214									
*											
217	KK	W37W38 ROUTE									
218	ZW	A=WT B=W37W38 C=FLOW									
219	RS	1 FLOW -1									
220	RC	0.015	0.015	0.015	833	0.0015	0.00				
221	RX	100.00	105.00	109.00	125.00	135.00	151.00	155.00	160.00		
222	RY	1000.0	999.50	999.00	995.00	995.10	999.00	999.50	1000.00		
*											
223	KK	W38 BASIN									
224	BA	0.163									
225	LG	0.10	0.25	4.15	0.59	84					
226	UI	0	72	224	403	305	162	58	21	11	0
227	UI	0	0	0	0	0	0	0	0	0	0
228	UI	0	0	0	0	0	0	0	0	0	0
229	UI	0	0	0	0	0	0	0	0	0	0
230	UI	0	0	0	0	0	0	0	0	0	0
*											
231	KK	DW38RE DIVERT									
232	KM	ASSUME 80% 100-YEAR 2-HOUR RETENTION. (C=0.65) (P=2.3IN).									
233	ZW	A=WT B=DW38RE C=FLOW									
234	DT	W38R 10.4 0.0									
235	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0
236	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0
*											

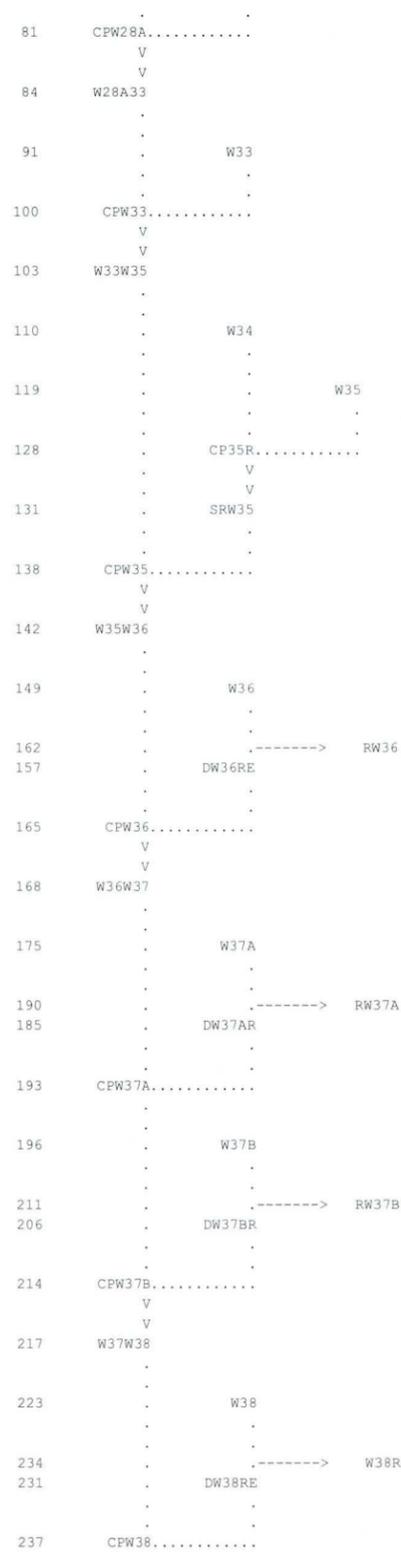
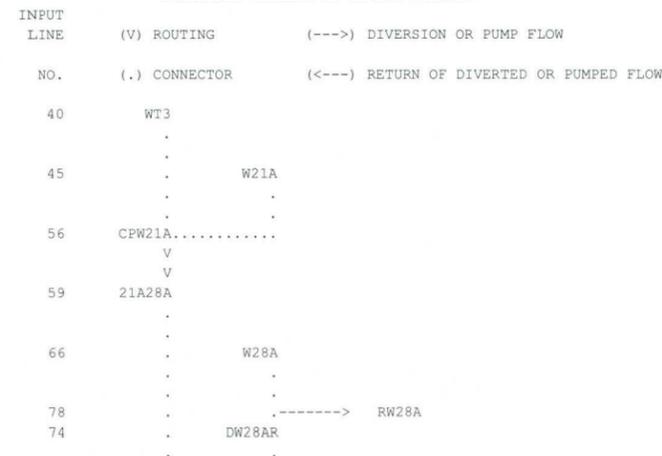
HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

237	KK	CPW38 COMBINE									
238	ZW	A=WT B=CPW38 C=FLOW									
239	HC	2 4.377									
*											
240	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK





RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT								
+	WT3	81.	22.17	80.	64.	28.	21.52		
+	HYDROGRAPH AT								
+	W21A	87.	12.25	7.	2.	1.	.20		
+	2 COMBINED AT								
+	CPW21A	87.	12.25	80.	64.	29.	.20		
+	ROUTED TO								
+	21A28A	81.	22.67	80.	64.	29.	.20		
+	HYDROGRAPH AT								
+	W28A	372.	12.33	44.	13.	5.	.64		
+	DIVERSION TO								
+	RW28A	372.	12.33	44.	13.	5.	.64		
+	HYDROGRAPH AT								
+	DW28AR	0.	.00	0.	0.	0.	.64		
+	2 COMBINED AT								
+	CPW28A	81.	22.67	80.	64.	29.	.84		
+	ROUTED TO								
+	W28A33	81.	23.25	80.	64.	29.	.84		
+	HYDROGRAPH AT								
+	W33	363.	12.42	44.	13.	4.	.84		
+	2 COMBINED AT								
+	CPW33	360.	12.42	82.	70.	33.	1.68		
+	ROUTED TO								
+	W33W35	302.	12.67	82.	70.	33.	1.68		
+	HYDROGRAPH AT								
+	W34	153.	12.25	18.	6.	2.	.24		
+	HYDROGRAPH AT								
+	W35	52.	12.25	6.	2.	1.	.09		
+	2 COMBINED AT								
+	CP35R	205.	12.25	24.	8.	3.	.33		
+	ROUTED TO								
+	SRW35	0.	21.33	0.	0.	0.	.33		
+	2 COMBINED AT								
+	CPW35	302.	12.67	82.	70.	33.	2.01		
+	ROUTED TO								
+	W35W36	219.	13.33	82.	69.	33.	2.01		
+	HYDROGRAPH AT								
+	W36	293.	12.50	38.	11.	4.	.72		
+	DIVERSION TO								
+	RW36	278.	12.42	23.	6.	2.	.72		
+	HYDROGRAPH AT								
+	DW36RE	207.	12.67	18.	5.	2.	.72		
+	2 COMBINED AT								
+	CPW36	241.	13.25	83.	73.	35.	2.91		
+	ROUTED TO								
+	W36W37	213.	13.75	83.	73.	35.	2.91		
+	HYDROGRAPH AT								
+	W37A	312.	12.33	39.	12.	4.	.63		

+	DIVERSION TO	RW37A	312.	12.33	30.	8.	3.	.63
+	HYDROGRAPH AT	DW37AR	122.	12.67	12.	4.	1.	.63
+	2 COMBINED AT	CPW37A	222.	13.75	84.	75.	36.	3.54
+	HYDROGRAPH AT	W37B	330.	12.33	41.	13.	4.	.67
+	DIVERSION TO	RW37B	8.	10.58	4.	2.	1.	.67
+	HYDROGRAPH AT	DW37BR	330.	12.33	41.	11.	4.	.67
+	2 COMBINED AT	CPW37B	329.	12.33	112.	84.	40.	4.21
+	ROUTED TO	W37W38	321.	12.33	112.	84.	40.	4.21
+	HYDROGRAPH AT	W38	198.	12.17	25.	9.	3.	.16
+	DIVERSION TO	W38R	198.	12.17	18.	5.	2.	.16
+	HYDROGRAPH AT	DW38RE	92.	12.33	11.	3.	1.	.16
+	2 COMBINED AT	CPW38	397.	12.33	122.	87.	41.	4.38

\*\*\* NORMAL END OF HEC-1 \*\*\*



C.4 EXISTING CONDITIONS WITH PROJECT IN PLACE, 100-YEAR FOR FRS#3 AREA

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 05DEC09 TIME 14:12:37 *
*****

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID WHITE TANKS AREA, WATERSHED CONTRIBUTING TO FRS#3
2 ID PREPARED BY HOSKIN RYAN CONSULTANTS EXCLUSIVELY FOR
3 ID FRS#3 OUTLET CHANNEL DESIGN, 12-05-2009
4 ID BASED ON HDR LOOP303/WHITE TANKS ADMPU AHA (09-04-09)
5 ID HEC-1 MODEL OF EXISTING CONDITION W/ CIP
6 ID MODIFICATIONS INCLUDE:
7 ID (1) UPDATE WITH AVERAGE RAINFALL DEPTH FOR FRS#3 WATERSHED ONLY
8 ID (2) UPDATE THE STAGE-STORAGE-DISCHARGE CURVE BASED ON URS DESIGN
9 ID OF FRS#3 PRINCIPAL AND EMERGENCY SPILLWAY (DISCHARGE
10 ID INCLUDING INFILTRATION)
11 ID (3) SEPARATE FRS#3 OUTFLOW AND INFILTRATION
12 ID *****
13 ID Flood Control District of Maricopa County
14 ID L303_EX_CIP_MB02 - Loop 303/ White Tanks ADMPU AHA
15 ID 100 YEAR
16 ID 24 Hour Storm
17 ID Unit Hydrograph: S-Graph
18 ID 08/18/2009
19 ID FCDMC CONTRACT 2007C031
20 ID BY HDR ENGINEERING (#79902)
21 ID EXISTING CONDITIONS WITH CIP-AUGUST 2009
22 ID MAJOR BASIN 02
23 ID FILE NAME: ECIP-MB2.DAT
24 IT 5 1JAN99 1200 2000
25 IN 15
26 IO 5
*DIAGRAM
*
27 JD 4.016 0.0001
28 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
29 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
30 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
31 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
32 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
33 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
34 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
35 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
36 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
37 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000

```

```

38 JD 3.815 10.0
39 JD 3.614 30.0
*
40 KK L21BASIN
41 KM BASIN BOUNDARY FROM MCMICKEN DAM ON THE WEST AND THE
42 KM BEARDSLEY CSR ON THE EAST
43 BA 0.525
44 LG 0.34 0.32 4.55 0.37 1
45 UI 0 20 20 20 21 58 70 88 109 125
46 UI 140 158 170 180 187 193 193 194 187 179
47 UI 172 150 140 123 113 101 93 83 76 70
48 UI 61 56 51 45 40 38 34 31 32 22
49 UI 21 21 20 14 14 14 13 14 11 5
*

```

HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
50 KK DL21REDIVERT
51 KM Mass grading and Storage along canal
52 DT RL21 57.3 0.0
53 DI 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
54 DQ 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
*
55 KK L21L22ROUTE
56 KM Cross-section: Cross-section determined from A-team survey
57 KM Manning's N Value: earth w/sparse trees and brush, ponding against canal
58 RS 1 FLOW
59 RC 0.032 0.032 0.032 8793 0.0020 0.00
60 RX 100.00 101.00 107.00 117.00 169.00 409.00 512.00 513.00
61 RY 1328.1 1328.00 1326.00 1324.00 1324.10 1326.00 1328.00 1328.10
*

```

```

62 KK L22BASIN
63 KM BASIN BOUNDARY FROM MCMICKEN DAM ON THE WEST AND THE
64 KM BEARDSLEY CSR ON THE EAST
65 BA 0.362
66 LG 0.34 0.34 4.35 0.39 0
67 UI 0 19 19 21 56 79 101 124 144 162
68 UI 170 183 184 177 172 154 133 117 103 89
69 UI 78 68 59 52 43 38 36 29 28 20
70 UI 20 18 13 13 13 12 5 5 4 5
71 UI 5 4 5 4 5 5 4 0 0 0
*

```

```

72 KK DL22REDIVERT
73 KM Storage along canal
74 DT RL22 15.6 0.0
75 DI 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
76 DQ 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
*

```

```

77 KK CPL22COMBINE
78 HC 2 0.887
*

```

```

79 KK L22W01ROUTE
80 KM Cross-section: Cross-section determined from 1991 topo
81 KM Manning's N Value: earth w/ sparse trees and brush
82 RS 4 FLOW
83 RC 0.032 0.032 0.032 3159 0.0063 0.00
84 RX 100.00 101.00 102.00 115.00 128.00 140.00 141.00 142.00
85 RY 1320.2 1320.10 1320.00 1314.00 1314.10 1320.00 1320.10 1320.20
*

```

```

86 KK W01BASIN
87 KM BASIN BOUNDARY FROM FRS#3 ON THE WEST AND THE BEARDSLEY CSR ON THE EAST
88 BA 0.191
89 LG 0.34 0.34 3.95 0.40 0
90 UI 0 38 144 258 304 262 170 110 71 44
91 UI 29 21 8 7 8 0 0 0 0 0
*

```

HEC-1 INPUT PAGE 3

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
92 UI 0 0 0 0 0 0 0 0 0 0
93 UI 0 0 0 0 0 0 0 0 0 0

```



```

94  UI  0  0  0  0  0  0  0  0  0  0  0
   *
95  KK  CPW01COMBINE
96  HC  2  1.078
   *
97  KK  W01W02ROUTE
98  KM  Cross-section: Estimated 3' deep and 4:1 side slopes
99  KM  width based on aerial
100 KM  Manning's N Value: natural desert wash w/ vegetation
101 RS  1  FLOW
102 RC  0.035  0.035  0.035  2650  0.0053  0.00
103 RX  100.00  111.00  122.00  139.00  162.00  182.00  191.00  200.00
104 RY  1290.5  1290.25  1290.00  1286.00  1286.10  1290.00  1290.25  1290.50
   *
105 KK  W02BASIN
106 KM  BASIN BOUNDARY FROM 1990 TOPO, ALL FLOW TO SOUTH
107 KM  MCMICKEN DAM ON THE WEST AND THE BEARDSLEY CSR ON THE EAST
108 BA  0.394
109 LG  0.35  0.35  4.65  0.32  0
110 UI  0  56  195  370  497  530  435  300  209  145
111 UI  99  70  46  38  14  13  14  13  0  0
112 UI  0  0  0  0  0  0  0  0  0  0
113 UI  0  0  0  0  0  0  0  0  0  0
114 UI  0  0  0  0  0  0  0  0  0  0
   *
115 KK  CPW02COMBINE
116 HC  2  1.472
   *
117 KK  W02W05ROUTE
118 KM  Cross-section: Natural Desert Wash w/ vegetation
119 RS  1  FLOW
120 RC  0.035  0.035  0.035  2214  0.0045  0.00
121 RX  100.00  106.00  112.00  119.00  135.00  137.00  138.00  141.00
122 RY  1280.0  1278.00  1277.00  1276.00  1275.90  1277.00  1278.00  1280.00
   *
123 KK  W03BASIN
124 KM  BASIN BOUNDARY FROM 1990 TOPO
125 BA  1.971
126 LG  0.35  0.35  4.00  0.47  20
127 UI  0  145  146  415  653  907  1064  1233  1685  1257
128 UI  947  849  756  672  606  522  442  374  341  315
129 UI  263  217  186  167  159  119  113  107  71  72
130 UI  70  71  37  27  28  28  28  28  28  28
131 UI  27  29  27  0  0  0  0  0  0  0
   *
132 KK  W03W04ROUTE
133 KM  Cross-section: Side slopes and width based on aerial and topo
134 KM  Manning's N Value: natural desert wash w/ vegetation
135 RS  3  FLOW
136 RC  0.035  0.035  0.035  18417  0.0490  0.00
137 RX  100.00  140.00  180.00  210.00  235.00  305.00  345.00  385.00
138 RY  1511.0  1510.50  1510.00  1502.00  1502.10  1510.00  1511.00  1512.00
   *
139 KK  W04BASIN
140 KM  BASIN BOUNDARY FROM 1990 TOPO
141 BA  2.034
142 LG  0.35  0.35  4.60  0.34  10
143 UI  0  144  147  379  620  881  1032  1176  1561  1470
144 UI  998  876  788  702  637  566  477  407  357  335
145 UI  304  239  203  188  158  157  113  111  105  72
146 UI  71  71  71  40  28  28  27  28  28  28
147 UI  28  28  27  28  0  0  0  0  0  0
   *
148 KK  CPW04COMBINE
149 HC  2  4.005
   *

```

```

150 KK  W04W05ROUTE
151 KM  Cross-section: Estimated 3' deep and 4:1 side slopes
152 KM  width based on aerial / Manning's N Value: clean straight earth
153 RS  2  FLOW
154 RC  0.035  0.035  0.035  5298  0.0098  0.00
155 RX  100.00  120.00  140.00  160.00  174.00  214.00  234.00  254.00
156 RY  1313.0  1312.50  1312.00  1308.00  1308.10  1312.00  1312.50  1313.00
   *
157 KK  W05BASIN
158 KM  BASIN BOUNDARY FROM 1990 TOPO AND BEARDSLEY CSR
159 BA  0.316
160 LG  0.35  0.35  4.25  0.42  0
161 UI  0  32  62  147  214  282  302  300  260  199
162 UI  153  119  90  67  54  40  32  22  22  9
163 UI  7  8  8  8  8  0  0  0  0  0
164 UI  0  0  0  0  0  0  0  0  0  0
165 UI  0  0  0  0  0  0  0  0  0  0
   *
166 KK  CPW05COMBINE
167 HC  3  5.793
   *
168 KK  DW05SEDIVERT
169 KM  North Inlet Channel Divert from L303M3LA.OUT model given to HDR by
170 KM  FCDMC 05062009
171 DT  DW05S  0.0  0.0
172 DI  600.0  800.0  1000.0  1200.0  1400.0  1600.0  2000.0  2400.0  2715.0  2800.0
173 DQ  105.0  163.0  361.0  498.0  640.0  792.0  1100.0  1437.0  1605.0  1630.0
   *
174 KK  W0512ARROUTE
175 KM  White Tanks FRS#3 North Inlet Channel South
176 KM  Channel plans FCD Contract No 2007C021
177 KM  Cholla Wash
178 RS  3  FLOW
179 RC  0.050  0.030  0.050  5306  0.0083  0.00
180 RX  1010.0  1015.00  1020.00  1050.00  1100.00  1275.00  1580.00  1750.00
181 RY  1251.0  1249.00  1249.00  1245.00  1244.90  1250.00  1250.00  1254.00
   *
182 KK  W06BASIN
183 KM  BASIN BOUNDARY FROM 1990 TOPO
184 BA  0.707
185 LG  0.35  0.35  4.30  0.41  18
186 UI  0  103  362  675  987  837  576  461  363  257
187 UI  217  150  119  90  72  49  48  20  20  19
188 UI  20  20  0  0  0  0  0  0  0  0
189 UI  0  0  0  0  0  0  0  0  0  0
190 UI  0  0  0  0  0  0  0  0  0  0
   *
191 KK  W07BASIN
192 KM  BASIN BOUNDARY FROM 1990 TOPO
193 BA  0.312
194 LG  0.35  0.35  4.25  0.42  19
195 UI  0  65  253  428  510  316  236  171  126  89
196 UI  63  46  33  26  14  11  10  10  0  0
197 UI  0  0  0  0  0  0  0  0  0  0
198 UI  0  0  0  0  0  0  0  0  0  0
199 UI  0  0  0  0  0  0  0  0  0  0
   *
200 KK  CPW07COMBINE
201 HC  2  1.019
   *
202 KK  W07W08ROUTE
203 KM  Cross-section: Based on aerial and topo
204 KM  Manning's N Value: Natural Desert wash w/ vegetation
205 KM  N value modified to slow velocity
206 RS  1  FLOW
207 RC  0.045  0.040  0.045  5589  0.0796  0.00
208 RX  100.00  136.00  173.00  197.00  234.00  254.00  298.00  342.00
209 RY  2880.0  2865.00  2850.00  2840.00  2840.00  2850.00  2865.00  2880.00

```

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10



210	KK	W08BASIN
211	KM	BASIN BOUNDARY FROM 1990 TOPO
212	BA	0.446
213	LG	0.35 0.35 3.95 0.40 20
214	UI	0 156 587 941 577 413 262 183 117 78
215	UI	49 32 19 19 19 0 0 0 0 0
216	UI	0 0 0 0 0 0 0 0 0 0
217	UI	0 0 0 0 0 0 0 0 0 0

HEC-1 INPUT PAGE 6

LINE	ID	1	2	3	4	5	6	7	8	9	10
218	UI	0	0	0	0	0	0	0	0	0	0

219	KK	CPW08COMBINE
220	HC	2 1.465

221	KK	W09BASIN
222	KM	BASIN BOUNDARY FROM 1990 TOPO
223	BA	0.335
224	LG	0.35 0.35 3.95 0.40 20
225	UI	0 125 468 716 427 304 193 127 85 53
226	UI	37 19 14 15 0 0 0 0 0 0
227	UI	0 0 0 0 0 0 0 0 0 0
228	UI	0 0 0 0 0 0 0 0 0 0
229	UI	0 0 0 0 0 0 0 0 0 0

230	KK	CPW09COMBINE
231	HC	2 1.8

232	KK	W09W10ROUTE
233	KM	Cross-section: Based on aerial and topo
234	KM	Manning's N Value: Natural Desert wash w/ vegetation
235	KM	N value modified to slow velocity
236	RS	1 FLOW
237	RC	0.045 0.040 0.045 11134 0.0683 0.00
238	RX	100.00 137.00 172.00 192.00 220.00 230.00 284.00 338.00
239	RY	1990.0 1975.00 1960.00 1950.00 1950.00 1960.00 1975.00 1990.00

240	KK	W10BASIN
241	KM	BASIN BOUNDARY FROM 1990 TOPO
242	BA	1.338
243	LG	0.35 0.35 3.95 0.40 20
244	UI	0 153 376 806 1108 1572 1334 920 794 647
245	UI	533 402 350 278 212 175 141 119 85 75
246	UI	75 29 30 30 29 30 29 0 0 0
247	UI	0 0 0 0 0 0 0 0 0 0
248	UI	0 0 0 0 0 0 0 0 0 0

249	KK	CPW10COMBINE
250	HC	2 3.138

251	KK	W11BASIN
252	KM	BASIN BOUNDARY FROM 1990 TOPO
253	BA	0.812
254	LG	0.35 0.35 3.95 0.40 20
255	UI	0 100 272 567 759 1098 696 556 469 375
256	UI	285 236 190 141 116 92 77 52 48 39
257	UI	20 19 19 19 20 0 0 0 0 0
258	UI	0 0 0 0 0 0 0 0 0 0

HEC-1 INPUT PAGE 7

LINE	ID	1	2	3	4	5	6	7	8	9	10
259	UI	0	0	0	0	0	0	0	0	0	0

260	KK	CPW11COMBINE
261	HC	2 3.95

262	KK	W11W12ROUTE
263	KM	Cross-section: Based on aerial and topo
264	KM	Manning's N Value: Natural Desert wash w/ vegetation
265	RS	8 FLOW
266	RC	0.045 0.035 0.045 21182 0.0205 0.00
267	RX	100.00 110.30 290.50 304.40 319.20 330.60 344.60 569.70
268	RY	1312.0 1310.00 1308.00 1306.00 1305.90 1308.00 1310.00 1312.00

269	KK	W12BASIN
270	KM	BASIN BOUNDARY FROM 1990 TOPO AND BEARDSLEY CSR
271	BA	1.868
272	LG	0.34 0.34 4.60 0.34 3
273	UI	0 125 126 289 490 706 847 961 1170 1474
274	UI	1002 820 727 654 604 537 483 418 353 310
275	UI	293 266 221 193 160 148 139 120 96 96
276	UI	83 61 61 61 61 37 24 24 24 24
277	UI	24 25 24 24 24 24 24 0 0 0

278	KK	DW05SERETRIEVE
279	KM	Flow traveling down North Inlet Channel
280	DR	DW05S

281	KK	W0512BROUTE
282	KM	White Tanks FRS#3 North Inlet Channel South
283	KM	Channel plans FCD Contract No 2007C021
284	KM	N value modified to mimic slowing of velocity by drop structures
285	RS	2 FLOW
286	RC	0.035 0.035 0.035 5494 0.0170 0.00
287	RX	100.00 120.00 135.00 165.00 220.00 300.00 315.00 379.00
288	RY	1244.7 1239.65 1239.50 1232.00 1231.90 1239.50 1239.65 1255.65

289	KK	CPW12COMBINE
290	HC	4 11.61

291	KK	W12W13ROUTE
292	KM	From NIC South Channel Plans at Sta. 535+00
293	RS	1 FLOW
294	RC	0.032 0.032 0.032 2062 0.0051 0.00
295	RX	100.00 120.00 162.50 205.00 355.00 397.50 440.00 460.00
296	RY	1218.4 1218.18 1211.10 1203.98 1204.45 1211.53 1218.65 1218.85

HEC-1 INPUT PAGE 8

LINE	ID	1	2	3	4	5	6	7	8	9	10
------	----	---	---	---	---	---	---	---	---	---	----

297	KK	W13BASIN
298	KM	BASIN BOUNDARY FROM 1990 TOPO AND BEARDSLEY CSR
299	BA	1.584
300	LG	0.35 0.35 4.90 0.29 3
301	UI	0 107 108 254 430 622 734 838 1035 1255
302	UI	820 689 615 557 511 445 405 352 287 261
303	UI	248 223 176 154 137 121 119 90 83 83
304	UI	59 52 53 53 48 21 20 21 20 21
305	UI	20 21 21 20 21 21 0 0 0 0

306	KK	CPW13COMBINE
307	HC	2 13.194

308	KK	W13W16ROUTE
309	KM	From NIC South Channel Plans
310	KM	at Sta. 523+00
311	RS	2 FLOW
312	RC	0.032 0.032 0.032 6257 0.0051 0.00
313	RX	100.00 115.00 162.00 209.10 359.10 435.90 465.00 480.00
314	RY	1216.9 1216.77 1208.93 1201.09 1203.09 1215.09 1223.54 1223.69

315	KK	W15BASIN
316	KM	BASIN BOUNDARY FROM 1990 TOPO
317	BA	1.227
318	LG	0.35 0.35 4.55 0.35 0
319	UI	0 98 112 315 498 652 757 975 1045 671



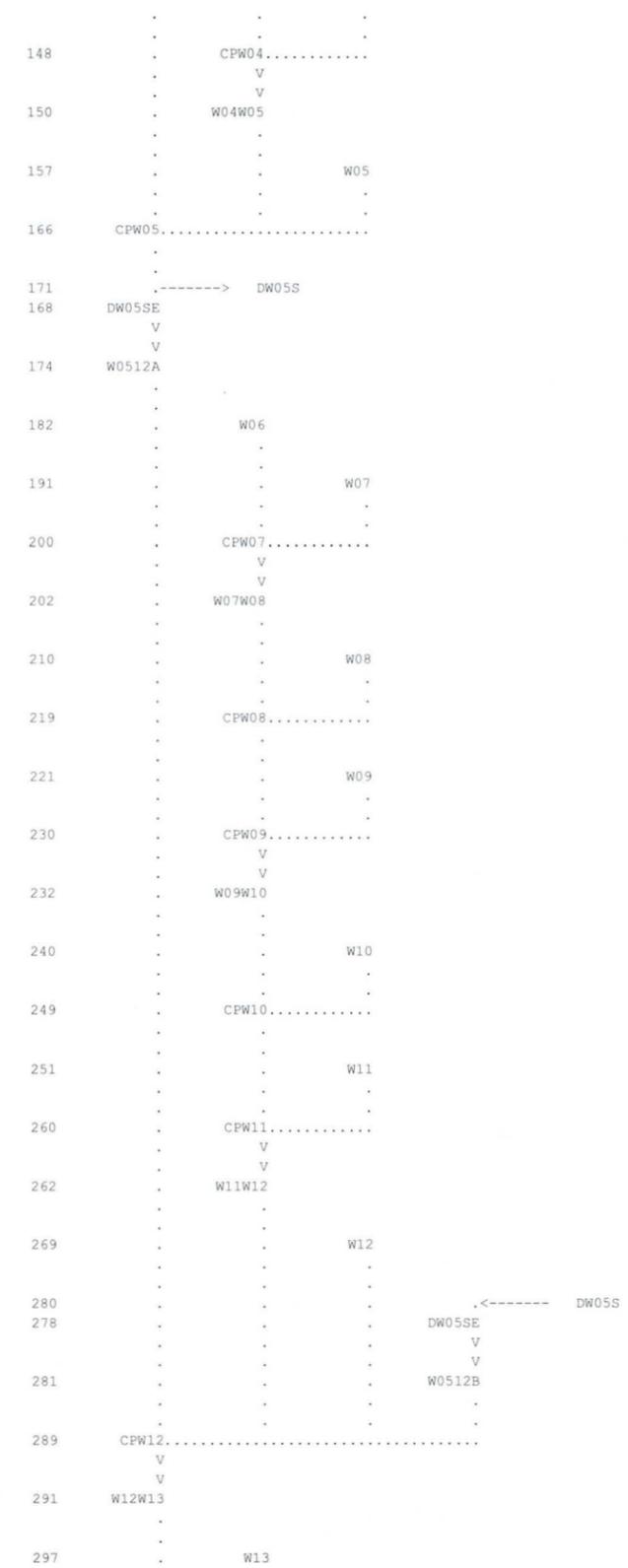
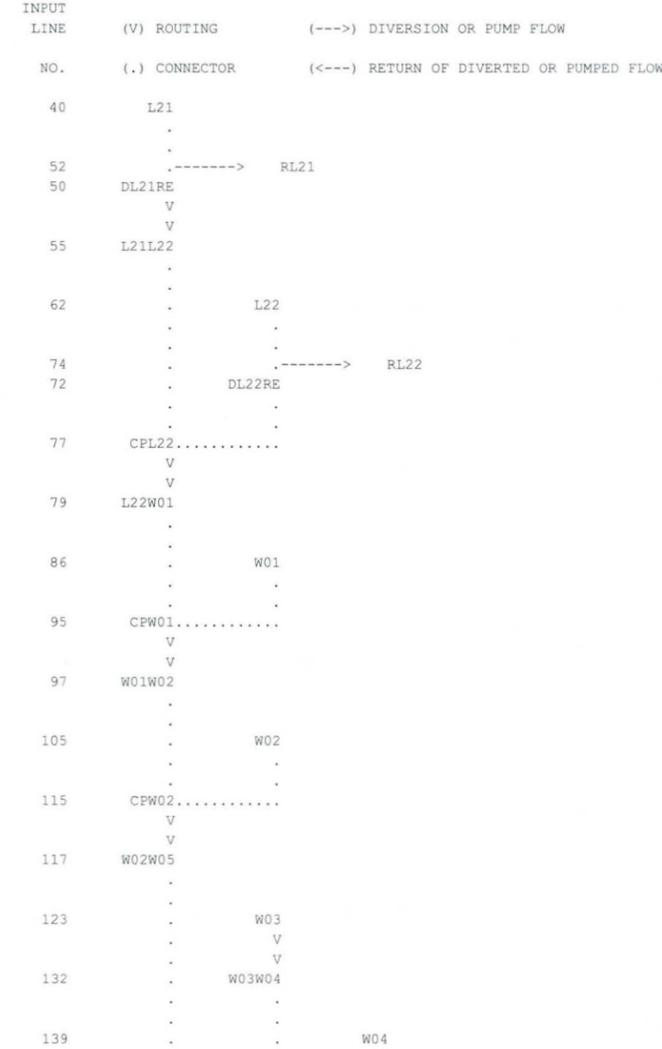
320	UI	578	523	457	400	352	284	245	227	196	161
321	UI	128	117	107	86	75	70	49	48	47	43
322	UI	19	18	19	19	19	19	18	19	19	0
323	UI	0	0	0	0	0	0	0	0	0	0
*											
324	KK W14BASIN										
325	KM BASIN BOUNDARY FROM 1990 TOPO										
326	BA	1.582									
327	LG	0.35	0.37	5.20	0.25	3					
328	UI	0	165	333	776	1104	1420	1804	1142	948	811
329	UI	682	567	431	386	320	242	201	182	128	124
330	UI	82	80	79	32	32	32	31	32	32	32
331	UI	0	0	0	0	0	0	0	0	0	0
332	UI	0	0	0	0	0	0	0	0	0	0
*											
333	KK W14W15ROUTE										
334	KM Cross-section: Based on aerial and topo										
335	KM Manning's N Value: Natural Desert wash w/ vegetation										
336	RS	3 FLOW									
337	RC	0.035	0.035	0.035	7308	0.0104	0.00				
338	RX	100.00	130.00	150.00	184.00	210.00	226.00	246.00	276.00		
339	RY	1280.0	1276.00	1274.00	1270.00	1269.90	1274.00	1276.00	1280.00		
*											
HEC-1 INPUT											
LINE	ID	1	2	3	4	5	6	7	8	9	10
340	KK	CPW15COMBINE									
341	HC	2 2.809									
*											
342	KK W15W16ROUTE										
343	KM Cross-section: Based on aerial and topo										
344	KM Manning's N Value: Natural Desert wash w/ vegetation										
345	RS	1 FLOW									
346	RC	0.035	0.035	0.035	2750	0.0087	0.00				
347	RX	100.00	135.00	232.00	328.00	360.00	498.00	635.00	735.00		
348	RY	1202.0	1200.00	1199.00	1198.00	1197.90	1199.00	1200.00	1202.00		
*											
349	KK W16BASIN										
350	KM BASIN BOUNDARY FROM BEARDSLEY CSR, THE FRS#4 AND 1990 TOPO										
351	BA	0.530									
352	LG	0.22	0.22	4.55	0.33	0					
353	UI	0	61	148	318	464	562	575	509	384	282
354	UI	211	157	115	87	65	42	42	15	14	15
355	UI	15	15	0	0	0	0	0	0	0	0
356	UI	0	0	0	0	0	0	0	0	0	0
357	UI	0	0	0	0	0	0	0	0	0	0
*											
358	KK CPW16COMBINE										
359	HC	3 16.534									
*											
360	KK W16W20ROUTE										
361	KM Cross-section: Based on aerial and topo										
362	KM Manning's N Value: clean earth; straight										
363	RS	1 FLOW									
364	RC	0.022	0.022	0.022	3633	0.0130	0.00				
365	RX	100.00	113.00	127.00	136.00	245.00	272.00	318.00	384.00		
366	RY	1186.0	1184.00	1182.00	1180.00	1179.90	1182.00	1184.00	1186.00		
*											
367	KK W18BASIN										
368	KM BASIN BOUNDARY FROM 1990 TOPO										
369	BA	1.260									
370	LG	0.35	0.35	4.40	0.38	8					
371	UI	0	38	38	38	38	38	99	112	147	168
372	UI	200	230	242	261	278	296	307	348	390	440
373	UI	461	337	285	264	241	228	223	213	202	195
374	UI	185	177	171	161	152	148	137	130	119	110
375	UI	100	97	93	90	89	86	79	81	68	62
*											
376	KK W17BASIN										
377	KM BASIN BOUNDARY FROM 1990 TOPO										

378	BA	1.497									
379	LG	0.35	0.35	4.30	0.41	18					
380	UI	0	169	396	865	1197	1639	1571	1038	892	737
381	UI	607	469	398	324	247	201	173	131	110	82
HEC-1 INPUT											
LINE	ID	1	2	3	4	5	6	7	8	9	10
382	UI	83	52	32	33	32	32	33	32	0	0
383	UI	0	0	0	0	0	0	0	0	0	0
384	UI	0	0	0	0	0	0	0	0	0	0
*											
385	KK W17W18ROUTE										
386	KM Cross-section: Based on aerial and topo										
387	KM Manning's N Value: natural desert wash w/ vegetation										
388	KM and heavy vegetation										
389	RS	2 FLOW									
390	RC	0.045	0.035	0.045	8559	0.0257	0.00				
391	RX	100.00	140.00	150.00	156.00	194.00	216.00	255.00	342.00		
392	RY	1302.0	1300.00	1298.00	1296.00	1295.90	1298.00	1300.00	1302.00		
*											
393	KK CPW18COMBINE										
394	HC	2 2.757									
*											
395	KK W18W20ROUTE										
396	KM Cross-section: Estimated 3' deep, side slopes and width based										
397	KM on aerial / Manning's N Value: natural desert wash w/ vegetation										
398	RS	5 FLOW									
399	RC	0.035	0.035	0.035	6914	0.0058	0.00				
400	RX	100.00	155.00	170.00	210.00	216.00	256.00	276.00	336.00		
401	RY	1249.0	1248.25	1248.00	1245.00	1245.10	1248.00	1248.25	1249.00		
*											
402	KK W19BASIN										
403	KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
404	KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
405	BA	1.158									
406	LG	0.35	0.35	3.88	0.42	20					
407	UI	0	241	939	1587	1896	1172	876	636	467	328
408	UI	236	172	119	99	51	39	39	39	0	0
409	UI	0	0	0	0	0	0	0	0	0	0
410	UI	0	0	0	0	0	0	0	0	0	0
411	UI	0	0	0	0	0	0	0	0	0	0
*											
412	KK SRW19STORAGE										
413	KM Master Drainage Plan for the Caterpillar Property (Basin #16)										
414	KO										
415	RS	1 STOR									
416	SV	1.00	31.00	114.00	270.00	502.00	807.00	1319.00	1388.00	1460.00	
417	SQ										
418	SE	1198.0	1200.00	1210.00	1220.00	1230.00	1240.00	1250.00	1260.00	1261.00	1262.00
419	ST										
*											
HEC-1 INPUT											
LINE	ID	1	2	3	4	5	6	7	8	9	10
420	KK W19W20ROUTE										
421	KM Cross-section: Estimated 4' deep and 3:1 side slopes, width based										
422	KM on aerial / Manning's N Value: earth with sparse trees and shrubs										
423	RS	1 FLOW									
424	RC	0.032	0.032	0.032	3790	0.0158	0.00				
425	RX	100.00	120.00	140.00	152.00	158.00	170.00	190.00	210.00		
426	RY	1240.5	1240.25	1240.00	1236.00	1236.00	1240.00	1240.25	1240.50		
*											
427	KK W20BASIN										
428	KM BASIN BOUNDARY FROM WHITE TANKS #4 FRS, S-S-D CURVES										
429	KM FROM JAN 2009 FCDMC, AND FROM 1990 TOPO										
430	BA	1.137									
431	LG	0.29	0.29	4.10	0.44	0					
432	UI	0	104	165	390	618	777	969	1101	712	596
433	UI	525	458	389	315	265	233	199	157	131	115
434	UI	98	80	71	51	50	51	26	19	20	20
435	UI	20	20	20	20	20	0	0	0	0	0



436	UI	0	0	0	0	0	0	0	0	0	0	0	0	0
437	KK	CPW20COMBINE												
438	HC	4	21.586											
439	KK	SRW20 STORAGE												
440	KM	STAGE-STORAGE-DISCHARGE CURVE FROM URS DESIGN OF FRS#3 OUTLET STRUCTURE												
441	KM	THE DISCHARGE INCLUDING OUTFLOW FROM PRINCIPAL AND EMERGENCY SPILLWAY,												
442	KM	AS WELL AS INFILTRATION												
443	RS	1	STOR	-1										
444	SV	44.8	388	585	846	1002	2045	3218	3557	4693	6510			
445	SQ	0.02	0.17	4.5	187	203	276	330	2936	24545	70439			
446	SE	1188	1198	1200	1202	1203	1208	1212	1213	1216	1220			
447	KK	OUTFL												
448	KM	SEPRATE OUTFLOW FROM INFILTRATION												
449	ZW	A=WT B=FRS3 C=FLOW												
450	DT	INFL												
451	DI	0	4.5	86	203	330	2936	24545	70439					
452	DQ	0	4.5	10	22	73	79	96	121					
453	ZZ													

1 SCHEMATIC DIAGRAM OF STREAM NETWORK





OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	L21	195.	13.25	57.	14.	5.	.52	
+	DIVERSION TO	RL21	195.	13.25	57.	14.	5.	.52	
+	HYDROGRAPH AT	DL21RE	0.	.00	0.	0.	0.	.52	
+	ROUTED TO	L21L22	0.	.00	0.	0.	0.	.52	
+	HYDROGRAPH AT	L22	175.	12.92	38.	10.	3.	.36	
+	DIVERSION TO	RL22	175.	12.92	31.	8.	3.	.36	
+	HYDROGRAPH AT	DL22RE	56.	13.75	7.	2.	1.	.36	
+	2 COMBINED AT	CPL22	56.	13.75	7.	2.	1.	.89	
+	ROUTED TO	L22W01	41.	14.08	7.	2.	1.	.89	
+	HYDROGRAPH AT	W01	252.	12.25	21.	5.	2.	.19	
+	2 COMBINED AT	CPW01	249.	12.25	27.	7.	2.	1.08	
+	ROUTED TO	W01W02	196.	12.33	27.	7.	2.	1.08	
+	HYDROGRAPH AT	W02	461.	12.33	44.	11.	4.	.39	
+	2 COMBINED AT	CPW02	652.	12.33	70.	18.	6.	1.47	
+	ROUTED TO	W02W05	608.	12.42	70.	18.	6.	1.47	
+	HYDROGRAPH AT	W03	1384.	12.58	267.	79.	26.	1.97	
+	ROUTED TO	W03W04	1195.	12.83	267.	79.	26.	1.97	
+	HYDROGRAPH AT	W04	1411.	12.58	257.	70.	23.	2.03	
+	2 COMBINED AT	CPW04	2341.	12.67	520.	148.	50.	4.01	
+	ROUTED TO	W04W05	2211.	12.83	520.	148.	50.	4.01	
+	HYDROGRAPH AT	W05	269.	12.42	32.	8.	3.	.32	
+	3 COMBINED AT	CPW05	2517.	12.75	619.	173.	58.	5.79	
+	DIVERSION TO	DW05S	1499.	12.75	310.	96.	32.	5.79	
+	HYDROGRAPH AT	DW05SE	1018.	12.75	309.	77.	26.	5.79	
+	ROUTED TO	W0512A	990.	12.92	309.	77.	26.	5.79	
+	HYDROGRAPH AT	W06	817.	12.25	97.	28.	9.	.71	
+	HYDROGRAPH AT	W07	403.	12.25	43.	13.	4.	.31	
+	2 COMBINED AT	CPW07	1215.	12.25	139.	40.	13.	1.02	

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES





C.5 EXISTING CONDITIONS WITH PROJECT IN PLACE, 100-YEAR FOR JACKRABBIT CORRIDOR

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 09DEC09 TIME 13:37:21 *
*****
  
```

```

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
  
```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID WHITE TANKS AREA, WATERSHED CONTRIBUTING TO FRS#3
2 ID PREPARED BY HOSKIN RYAN CONSULTANTS EXCLUSIVELY FOR
3 ID FRS#3 OUTLET CHANNEL DESIGN, 12-09-2009
4 ID BASED ON HDR LOOP303/WHITE TANKS ADMPU AHA (09-04-09)
5 ID HEC-1 MODEL OF EXISTING CONDITIONS WITH CIP
6 ID MODIFICATIONS INCLUDE:
7 ID (1) UPDATE WITH AVERAGE RAINFALL DEPTH FOR JACKRABBIT CORRIDOR
8 ID (2) UPDATE THE PROPOSED CHANNEL DESIGN
9 ID (3) DELETE RETENTION OF PASQUELETTI TO REFLECT EXIST CONDITIONS
10 ID
11 ID *****
12 ID Flood Control District of Maricopa County
13 ID L303_EX_CIP_MB02 - Loop 303/ White Tanks ADMPU AHA
14 ID 100 YEAR
15 ID 24 Hour Storm
16 ID Unit Hydrograph: S-Graph
17 ID 08/18/2009
18 ID FCDMC CONTRACT 2007C031
19 ID BY HDR ENGINEERING (#79902)
20 ID EXISTING CONDITIONS WITH CIP-AUGUST 2009
21 ID MAJOR BASIN 02
22 ID FILE NAME: ECIP-MB2.DAT
23 IT 5 1JAN99 1200 2000
24 IN 15
25 IO 5
*DIAGRAM
*
26 JD 3.661 0.0001
27 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
28 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
29 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
30 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
31 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
32 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
33 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
34 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
35 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
36 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
37 JD 3.478 10.0
  
```

1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
50 UI 0 19 35 81 123 161 180 182 168 133
51 UI 102 82 62 49 38 30 21 18 13 13
52 UI 5 5 4 5 5 5 0 0 0 0
53 UI 0 0 0 0 0 0 0 0 0 0
54 UI 0 0 0 0 0 0 0 0 0 0
*
55 KK CPW21ACOMBINE
56 ZW A=CIP B=CPW21A C=FLOW
57 HC 2 0.199
*
58 KK 21A28A ROUTE
59 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=30FT, SIDE SLOPE 6:1
60 ZW A=CIP B=21A28A C=FLOW
61 RS 4 FLOW -1
62 RC 0.045 0.035 0.045 3560 0.0010
63 RX 100 110 120 150 180 210 220 230
64 RY 1001 1000 1000 995 995 1000 1000 1001
*
65 KK W28ABASIN
66 KM Boundary based on Preliminary Design Plans for
67 KM White Tanks FRS #3 Outfall Channel dated
68 KM 12-08-2008 prepared by Gannett Fleming
69 BA 0.642
70 LG 0.34 0.32 4.55 0.35 1
71 UI 0 65 127 296 444 573 621 609 524 407
72 UI 308 239 181 135 110 80 64 45 44 16
73 UI 17 16 16 16 16 0 0 0 0 0
74 UI 0 0 0 0 0 0 0 0 0 0
75 UI 0 0 0 0 0 0 0 0 0 0
*
76 KK CPW28ACOMBINE
77 ZW A=CIP B=CPW28A C=FLOW
78 HC 2 0.841
*
79 KK W28A33 ROUTE
80 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 4:1
81 ZW A=CIP B=W28A33 C=FLOW
82 RS 5 FLOW -1
83 RC 0.045 0.035 0.045 4336 0.0010
84 RX 100 110 120 140 180 200 210 220
85 RY 1001 1000 1000 995 995 1000 1000 1001
*
86 KK W33BASIN
87 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN
88 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO
89 ZW A=CIP B=W33 C=FLOW
90 BA 0.839
91 LG 0.31 0.27 4.00 0.47 4
92 UI 0 92 207 460 670 834 886 810 641 473
HEC-1 INPUT
PAGE 3
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
93 UI 361 275 195 155 114 85 63 52 23 22
  
```

1



94	UI	23	22	23	0	0	0	0	0	0	0
95	UI	0	0	0	0	0	0	0	0	0	0
96	UI	0	0	0	0	0	0	0	0	0	0
*											
97	KK CPW33COMBINE										
98	ZW	A=CIP B=CPW33 C=FLOW									
99	HC	2	1.68								
*											
100	KK W33W35 ROUTE										
101	KM	PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 6:1									
102	ZW	A=CIP B=W33W35 C=FLOW									
103	RS	3	FLOW	-1							
104	RC	0.045	0.035	0.045	2658	0.0010					
105	RX	100	110	116	152	192	228	240	250		
106	RY	1001	1000	1000	994	994	1000	1000	1001		
*											
107	KK W35BASIN										
108	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
109	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
110	BA	0.283									
111	LG	0.32	0.34	3.71	0.47	4					
112	UI	0	33	83	180	257	312	308	268	201	146
113	UI	108	80	58	43	33	22	19	8	8	8
114	UI	8	8	0	0	0	0	0	0	0	0
115	UI	0	0	0	0	0	0	0	0	0	0
116	UI	0	0	0	0	0	0	0	0	0	0
*											
117	KK W34BASIN										
118	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
119	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
120	BA	0.228									
121	LG	0.32	0.31	3.74	0.46	20					
122	UI	0	33	131	238	312	316	236	162	111	74
123	UI	52	34	23	13	9	8	9	0	0	0
124	UI	0	0	0	0	0	0	0	0	0	0
125	UI	0	0	0	0	0	0	0	0	0	0
126	UI	0	0	0	0	0	0	0	0	0	0
*											
127	KK SRW34STORAGE										
128	KM	Master Drainage Plan for the Caterpillar Property (Basin #29)									
129	KO										
130	RS	1	STOR								
131	SV	0.99	12.73	23.45	36.25	50.68	54.76	59.33	83.20		
132	SQ	88.00 6226.00									
133	SE	1164.5	1166.00	1170.00	1172.00	1174.00	1176.00	1177.50	1178.00	1180.00	
134	ST										
*											
HEC-1 INPUT											
LINE	ID	1	2	3	4	5	6	7	8	9	10
135	KK W34W35ROUTE										
136	KM	Cross-section: Estimated 3' deep and 4:1 side slopes, width based on									
137	KM	aerial. Manning's N Value: clean straight earth									
138	RS	1	FLOW	-1							
139	RC	0.022	0.022	0.022	813	0.0111	0.00				
140	RX	100.00	104.00	108.00	120.00	132.00	144.00	152.00	160.00		
141	RY	1166.2	1166.10	1166.00	1160.00	1160.10	1162.00	1162.10	1162.20		
*											
142	KK CPW35COMBINE										
143	ZW	A=CIP B=CPW35 C=FLOW									
144	HC	3	2.191								
*											
145	KK W35W36 ROUTE										
146	KM	PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 4:1									
147	ZW	A=CIP B=W35W36 C=FLOW									
148	RS	7	FLOW	-1							
149	RC	0.045	0.035	0.045	6051	0.0010					
150	RX	100	110	116	140	180	204	220	230		
151	RY	1001	1000	1000	994	994	1000	1000	1001		
*											

152	KK W36BASIN										
153	KM	Boundary based on Aerial, topo, and Preliminary									
154	KM	Design Plans for White Tanks FRS #3 Outfall Channel									
155	KM	dated 12-08-2008 prepared by Gannett Fleming									
156	BA	0.720									
157	LG	0.31	0.28	4.00	0.47	4					
158	UI	0	65	101	247	385	507	591	617	609	513
159	UI	409	329	255	204	160	126	102	76	64	45
160	UI	45	25	16	16	15	16	16	16	0	0
161	UI	0	0	0	0	0	0	0	0	0	0
162	UI	0	0	0	0	0	0	0	0	0	0
*											
163	KK CPW36COMBINE										
164	ZW	A=CIP B=CPW36 C=FLOW									
165	HC	2	2.911								
*											
166	KK W36W37 ROUTE										
167	KM	PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=30FT, SIDE SLOPE 5:1									
168	ZW	A=CIP B=W36W37 C=FLOW									
169	RS	5	FLOW	-1							
170	RC	0.045	0.035	0.045	4527	0.0010					
171	RX	100	110	120	150	180	210	220	230		
172	RY	1001	1000	1000	994	994	1000	1000	1001		
*											
HEC-1 INPUT											
LINE	ID	1	2	3	4	5	6	7	8	9	10
173	KK W37BASIN										
174	KM	WESTERN LIMIT DEFINED BY JACKRABBIT WASH									
175	KM	CAPACITY APPROX 12,000 CFS, VALENCIA HEIGHTS									
176	BA	1.210									
177	LG	0.32	0.31	4.20	0.44	4					
178	UI	0	96	112	318	497	664	822	897	937	893
179	UI	777	643	515	421	344	278	221	186	148	115
180	UI	104	69	66	63	23	24	23	24	23	24
181	UI	24	0	0	0	0	0	0	0	0	0
182	UI	0	0	0	0	0	0	0	0	0	0
*											
183	KK W22BASIN										
184	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
185	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
186	BA	0.782									
187	LG	0.35	0.35	4.15	0.44	19					
188	UI	0	237	914	1559	1035	751	503	352	228	158
189	UI	107	80	37	31	31	31	0	0	0	0
190	UI	0	0	0	0	0	0	0	0	0	0
191	UI	0	0	0	0	0	0	0	0	0	0
192	UI	0	0	0	0	0	0	0	0	0	0
*											
193	KK W22W23ROUTE										
194	KM	Cross-section: Based on aerial and topo									
195	KM	Manning's N Value: pavement and natural desert wash w/ vegetation									
196	RS	1	FLOW	-1							
197	RC	0.035	0.013	0.035	4866	0.0719	0.00				
198	RX	100.00	112.00	113.00	126.00	439.00	477.00	496.00	515.00		
199	RY	1820.0	1815.00	1810.00	1800.00	1799.90	1810.00	1815.00	1820.00		
*											
200	KK W23BASIN										
201	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
202	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
203	BA	0.897									
204	LG	0.35	0.35	4.35	0.40	18					
205	UI	0	236	906	1581	1306	885	636	424	309	204
206	UI	145	98	80	33	34	33	33	0	0	0
207	UI	0	0	0	0	0	0	0	0	0	0
208	UI	0	0	0	0	0	0	0	0	0	0
209	UI	0	0	0	0	0	0	0	0	0	0
*											
210	KK CPW23COMBINE										
211	HC	2	1.679								
*											
HEC-1 INPUT											



LINE	ID	1	2	3	4	5	6	7	8	9	10	
212	KK	W23W24ROUTE										
213	KM	Cross-section: Based on aerial and topo										
214	KM	Manning's N Value: natural desert wash w/ vegetation										
215	RS	1 FLOW										
216	RC	0.045	0.035	0.045	5335	0.0367	0.00					
217	RX	100.00	120.00	140.00	180.00	220.00	240.00	260.00	280.00			
218	RY	1462.0	1461.00	1460.00	1450.00	1450.10	1460.00	1461.00	1462.00			
219	KK	W24BASIN										
220	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
221	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
222	BA	0.475										
223	LG	0.35	0.35	4.90	0.29	14						
224	UI	0	88	342	575	788	483	372	280	201	154	
225	UI	104	82	60	39	38	15	14	15	15	0	
226	UI	0	0	0	0	0	0	0	0	0	0	
227	UI	0	0	0	0	0	0	0	0	0	0	
228	UI	0	0	0	0	0	0	0	0	0	0	
229	KK	CPW24COMBINE										
230	HC	2 2.154										
231	KK	W24W27ROUTE										
232	KM	Cross-section: Based on aerial and topo										
233	KM	Manning's N Value: natural desert wash w/ vegetation										
234	RS	1 FLOW										
235	RC	0.035	0.035	0.035	5873	0.0289	0.00					
236	RX	100.00	120.00	140.00	160.00	180.00	200.00	220.00	240.00			
237	RY	1094.0	1092.00	1090.00	1084.00	1084.10	1090.00	1090.25	1090.50			
238	KK	W25BASIN										
239	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
240	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
241	BA	1.099										
242	LG	0.35	0.35	4.80	0.30	8						
243	UI	0	143	438	866	1174	1490	915	737	620	467	
244	UI	358	307	216	171	140	110	76	71	53	27	
245	UI	28	28	27	28	0	0	0	0	0	0	
246	UI	0	0	0	0	0	0	0	0	0	0	
247	UI	0	0	0	0	0	0	0	0	0	0	
248	KK	SRW25STORAGE										
249	KM	Verrado on-line storage basin (WoodPatel ID SR20)										
250	KO											
251	RS	1 STOR										
252	SV	1.05	9.43	26.91	54.31	92.89	138.67	176.47	190.08	219.05		
253	SQ	265.00 1377.00										
254	SE	1443.0	1446.00	1450.00	1454.00	1458.00	1462.00	1466.00	1469.00	1472.00		
255	ST											
	*											
		HEC-1 INPUT										
		PAGE 7										
LINE	ID	1	2	3	4	5	6	7	8	9	10	
256	KK	W25W26ROUTE										
257	KM	Cross-section: Based on aerial and topo										
258	KM	Manning's N Value: natural desert wash w/ vegetation										
259	RS	1 FLOW										
260	RC	0.035	0.035	0.035	6978	0.0178	0.00					
261	RX	100.00	120.00	140.00	156.00	176.00	192.00	212.00	232.00			
262	RY	1451.5	1451.25	1451.00	1447.00	1447.10	1451.00	1451.25	1451.50			
263	KK	W26BASIN										
264	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
265	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
266	BA	0.682										
267	LG	0.33	0.37	6.20	0.17	15						
268	UI	0	86	245	500	680	926	574	465	390	304	
269	UI	231	197	152	110	95	69	59	43	42	21	

270	UI	17	16	17	16	17	0	0	0	0	0	
271	UI	0	0	0	0	0	0	0	0	0	0	
272	UI	0	0	0	0	0	0	0	0	0	0	
	*											
273	KK	CPW26COMBINE										
274	HC	2 1.781										
	*											
275	KK	SRW26STORAGE										
276	KM	Verrado on-line storage basin (WoodPatel ID SR21 and PH 6 Golf)										
277	KO											
278	RS	1 STOR										
279	SV	0.68	20.68	57.58	95.91	102.34	117.65	130.00				
280	SQ	265.00 1377.00 2000.00										
281	SE	1319.0	1320.00	1330.00	1340.00	1347.00	1348.00	1350.00	1351.00			
282	ST											
	*											
283	KK	W26W27ROUTE										
284	KM	Cross-section: based on topo and aerial										
285	KM	Manning's N Value: natural desert wash w/ vegetation										
286	RS	1 FLOW										
287	RC	0.035	0.035	0.035	3484	0.0172	0.00					
288	RX	100.00	120.00	140.00	152.00	168.00	180.00	200.00	220.00			
289	RY	1298.5	1298.25	1298.00	1294.00	1294.10	1298.00	1298.25	1298.50			
	*											
290	KK	W27BASIN										
291	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
292	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
293	BA	0.411										
294	LG	0.32	0.37	5.80	0.20	11						
295	UI	0	76	296	498	681	418	323	241	174	133	
296	UI	91	71	51	34	33	13	13	13	13	0	
297	UI	0	0	0	0	0	0	0	0	0	0	
298	UI	0	0	0	0	0	0	0	0	0	0	
299	UI	0	0	0	0	0	0	0	0	0	0	
	*											
		HEC-1 INPUT										
		PAGE 8										
LINE	ID	1	2	3	4	5	6	7	8	9	10	
300	KK	CPW27COMBINE										
301	HC	3 4.345										
	*											
302	KK	W27W44ROUTE										
303	KM	Cross-section: Clean straight earth										
304	RS	1 FLOW										
305	RC	0.022	0.022	0.022	7169	0.0098	0.00					
306	RX	100.00	182.00	270.00	288.00	318.00	329.00	333.00	338.00			
307	RY	1256.0	1254.00	1250.00	1248.00	1248.00	1250.00	1254.00	1256.00			
	*											
308	KK	W43BASIN										
309	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
310	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
311	BA	0.209										
312	LG	0.20	0.28	3.48	0.55	61						
313	UI	0	971	508	111	0	0	0	0	0	0	
314	UI	0	0	0	0	0	0	0	0	0	0	
315	UI	0	0	0	0	0	0	0	0	0	0	
316	UI	0	0	0	0	0	0	0	0	0	0	
317	UI	0	0	0	0	0	0	0	0	0	0	
	*											
318	KK	SRW43STORAGE										
319	KM	Verrado on-line storage basin (WLB) (WoodPatel ID SR23)										
320	KO											
321	RS	1 STOR										
322	SV	6.04	20.38	53.82	120.38	216.24	325.98	455.42	606.10	645.49		
323	SQ											
324	SE	1272.0	1276.00	1280.00	1284.00	1288.00	1292.00	1296.00	1300.00	1305.00		
325	ST											
	*											
326	KK	W43W44ROUTE										
327	KM	Cross-section: Side slopes and width based on aerial and topo										



328 KM Manning's N Value: natural desert wash w/ vegetation  
 329 RS 1 FLOW  
 330 RC 0.035 0.035 0.035 8415 0.0125 0.00  
 331 RX 100.00 145.00 180.00 210.00 220.00 245.00 270.00 295.00  
 332 RY 1266.0 1264.00 1262.00 1258.00 1258.00 1262.00 1265.50 1266.00  
 \*

333 KK W44BASIN  
 334 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 335 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 336 BA 0.598  
 337 LG 0.35 0.35 4.90 0.29 0  
 338 UI 0 55 89 214 334 438 500 527 506 421  
 339 UI 332 266 206 162 127 99 82 59 48 37  
 340 UI 37 13 14 13 14 13 14 0 0 0  
 341 UI 0 0 0 0 0 0 0 0 0 0  
 342 UI 0 0 0 0 0 0 0 0 0 0  
 \*

HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

343 KK CPW44COMBINE  
 344 HC 3 5.153  
 \*

345 KK W44W46ROUTE  
 346 KM Cross-section: Estimated 2' deep, side slopes and width based on aerial  
 347 KM and topo. Manning's N Value: earth w/ sparse trees and shrubs  
 348 RS 1 FLOW  
 349 RC 0.032 0.032 0.032 1706 0.0070 0.00  
 350 RX 100.00 116.00 132.00 162.00 192.00 252.00 272.00 292.00  
 351 RY 1216.0 1215.00 1214.00 1208.00 1208.10 1210.00 1211.00 1212.00  
 \*

352 KK W45BASIN  
 353 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 354 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 355 BA 1.035  
 356 LG 0.35 0.33 7.30 0.11 3  
 357 UI 0 136 414 824 1120 1399 860 697 573 441  
 358 UI 336 286 202 161 130 104 71 67 47 26  
 359 UI 26 26 26 26 0 0 0 0 0 0  
 360 UI 0 0 0 0 0 0 0 0 0 0  
 361 UI 0 0 0 0 0 0 0 0 0 0  
 \*

362 KK W45W46ROUTE  
 363 KM Cross-section: Based on aerial and topo  
 364 KM Manning's N Value: natural desert wash w/ vegetation  
 365 RS 4 FLOW  
 366 RC 0.035 0.035 0.035 9372 0.0125 0.00  
 367 RX 100.00 160.00 205.00 265.00 285.00 310.00 345.00 385.00  
 368 RY 1274.0 1270.00 1268.00 1262.00 1262.10 1272.00 1275.50 1276.00  
 \*

369 KK W46BASIN  
 370 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 371 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 372 BA 0.926  
 373 LG 0.27 0.29 6.40 0.18 16  
 374 UI 0 88 165 367 477 592 749 1082 916 727  
 375 UI 580 459 331 180 148 97 75 27 27 27  
 376 UI 28 27 0 0 0 0 0 0 0 0  
 377 UI 0 0 0 0 0 0 0 0 0 0  
 378 UI 0 0 0 0 0 0 0 0 0 0  
 \*

379 KK CPW46ACOMBINE  
 380 HC 2 1.961  
 \*

HEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

381 KK DW46REDIVERT  
 382 KM Master Drainage Plan for the Caterpillar Property (Basin #27)  
 383 DT RW46 0.0 0.0

384 DI 0.0 35.0 98.0 179.0 276.0 520.0 888.0 1339.0 1859.0 2439.0  
 385 DQ 0.0 0.0 0.0 0.0 0.0 135.0 382.0 701.0 1080.0 1509.0  
 \*

386 KK CPW46BCOMBINE  
 387 HC 2 7.114  
 \*

388 KK W46W54ROUTE  
 389 KM Cross-section: side slopes, width based on aerial and topo  
 390 KM Manning's N Value: natural desert wash w/ vegetation  
 391 RS 1 FLOW  
 392 RC 0.035 0.035 0.035 3908 0.0397 0.00  
 393 RX 100.00 112.00 124.00 140.00 160.00 190.00 220.00 240.00  
 394 RY 1194.5 1194.00 1190.00 1184.00 1184.10 1186.00 1190.00 1190.50  
 \*

395 KK W47BASIN  
 396 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 397 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 398 BA 0.666  
 399 LG 0.35 0.35 3.95 0.40 20  
 400 UI 0 96 349 638 936 788 540 432 340 243  
 401 UI 202 142 111 83 66 47 43 19 19 18  
 402 UI 19 18 0 0 0 0 0 0 0 0  
 403 UI 0 0 0 0 0 0 0 0 0 0  
 404 UI 0 0 0 0 0 0 0 0 0 0  
 \*

405 KK W48BASIN  
 406 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 407 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 408 BA 0.353  
 409 LG 0.35 0.35 3.95 0.40 20  
 410 UI 0 57 232 395 573 367 281 216 157 124  
 411 UI 85 65 48 36 28 20 10 11 11 11  
 412 UI 0 0 0 0 0 0 0 0 0 0  
 413 UI 0 0 0 0 0 0 0 0 0 0  
 414 UI 0 0 0 0 0 0 0 0 0 0  
 \*

415 KK CPW47COMBINE  
 416 HC 2 1.019  
 \*

417 KK W47W49ROUTE  
 418 KM Cross-section: Based on aerial and topo  
 419 KM Manning's N Value: natural desert wash w/ vegetation  
 420 RS 1 FLOW  
 421 RC 0.035 0.035 0.035 5077 0.0414 0.00  
 422 RX 100.00 150.00 190.00 210.00 235.00 255.00 275.00 310.00  
 HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

423 RY 1740.0 1720.00 1710.00 1707.00 1708.00 1714.00 1730.00 1740.00  
 \*

424 KK W50BASIN  
 425 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 426 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 427 BA 1.345  
 428 LG 0.35 0.35 4.25 0.42 19  
 429 UI 0 122 193 458 725 898 1129 1321 842 706  
 430 UI 619 546 461 378 312 278 240 189 156 135  
 431 UI 120 93 88 60 60 59 35 24 23 24  
 432 UI 23 24 24 23 23 0 0 0 0 0  
 433 UI 0 0 0 0 0 0 0 0 0 0  
 \*

434 KK W49BASIN  
 435 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN  
 436 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO  
 437 BA 0.385  
 438 LG 0.35 0.35 3.95 0.40 20  
 439 UI 0 67 265 450 633 398 302 232 166 129  
 440 UI 89 70 48 35 31 16 12 12 12 11  
 441 UI 0 0 0 0 0 0 0 0 0 0  
 442 UI 0 0 0 0 0 0 0 0 0 0  
 443 UI 0 0 0 0 0 0 0 0 0 0

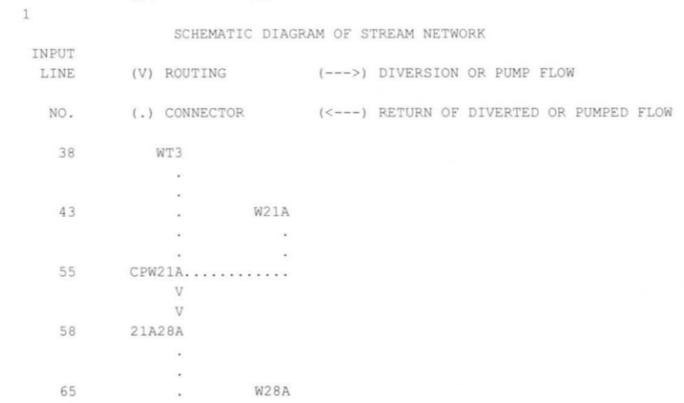
PAGE 11



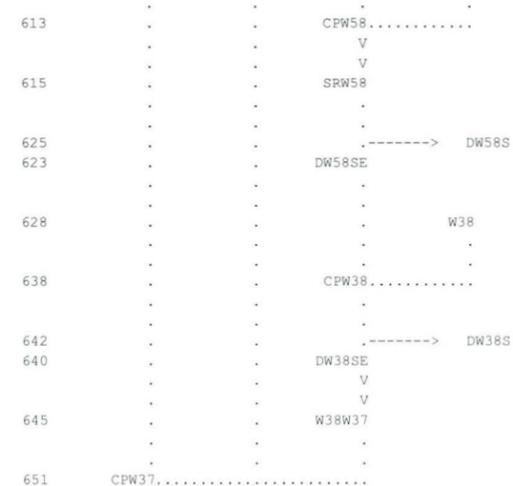
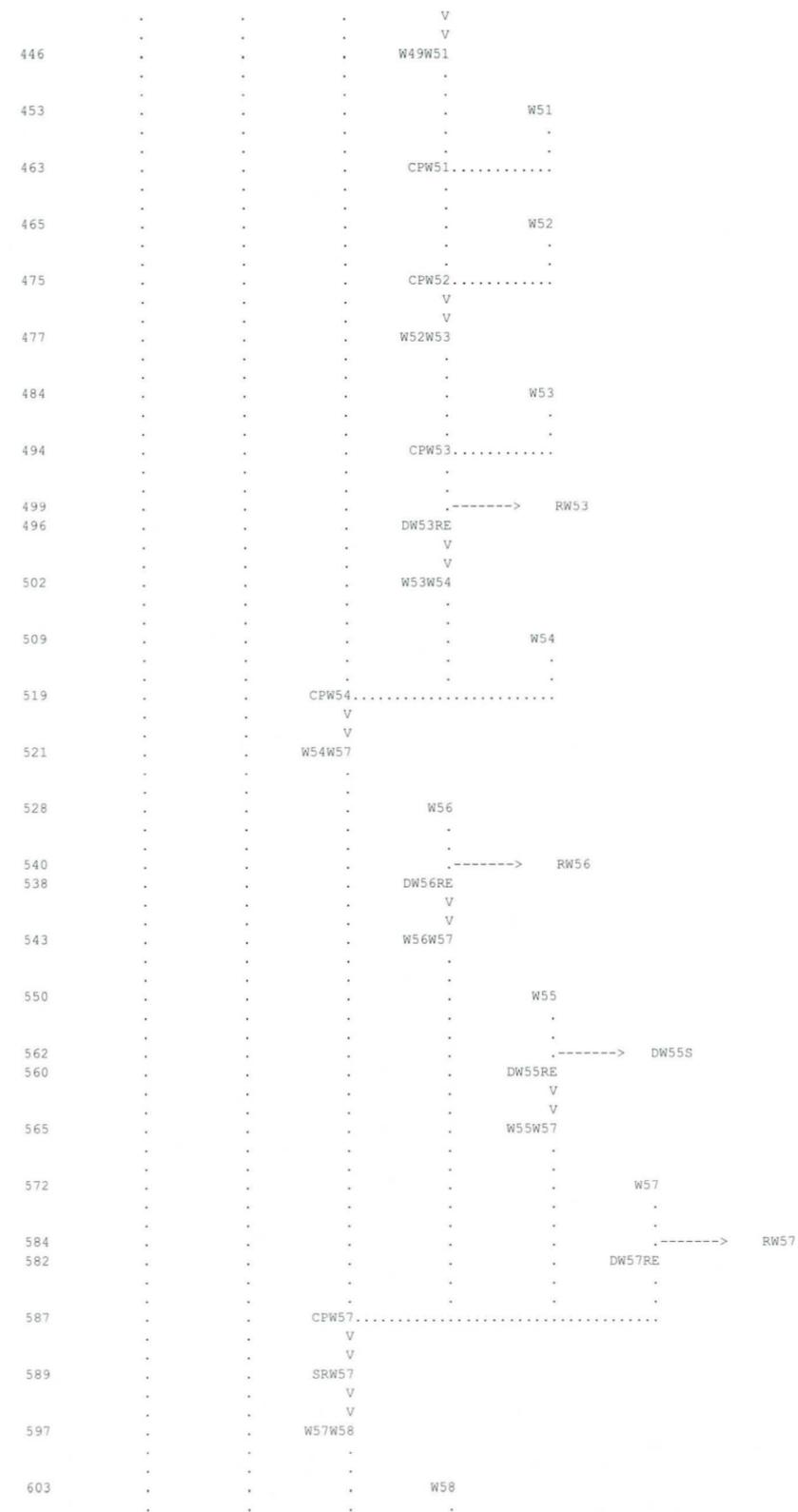


556	UI	120	92	67	51	38	29	15	15	15	15	
557	UI	0	0	0	0	0	0	0	0	0	0	
558	UI	0	0	0	0	0	0	0	0	0	0	
559	UI	0	0	0	0	0	0	0	0	0	0	
*												
560	KK DW55REDIVERT											
561	KM Verado GOB5											
562	DT	DW55S	0.0	0.0								
563	DI	0.0	55.0	101.0	537.0	1297.0	2269.0	4708.0	7684.0	11074.0	0.0	
564	DQ	0.0	0.0	0.0	382.0	1080.0	1984.0	4269.0	7072.0	10310.0	0.0	
*												
565	KK W55W57ROUTE											
566	KM Cross-section: Estimated 2' deep and 4:1 side slopes, width											
567	KM based on aerial / Manning's N Value: natural desert wash w/ vegetation											
568	RS	4	FLOW									
569	RC	0.035	0.035	0.035	5747	0.0096	0.00					
570	RX	100.00	110.00	120.00	136.00	156.00	172.00	192.00	212.00			
571	RY	1136.5	1136.25	1136.00	1134.00	1134.10	1136.00	1136.25	1136.50			
*												
572	KK W57BASIN											
573	KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN											
574	KM WOOD/PATEL, 2006 MODIFIED SLIGHTLY TO MATCH NEW TOPO											
575	BA	1.161										
576	LG	0.27	0.29	4.65	0.37	19						
577	UI	0	138	388	695	889	1284	1641	1231	946	700	
578	UI	409	239	166	101	43	43	42	0	0	0	
579	UI	0	0	0	0	0	0	0	0	0	0	
580	UI	0	0	0	0	0	0	0	0	0	0	
581	UI	0	0	0	0	0	0	0	0	0	0	
*												
HEC-1 INPUT												
LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10	
582	KK DW57REDIVERT											
583	KM Master Drainage Plan for the Caterpillar Property (Basin #42)											
584	DT	RW57	21.6	0.0								
585	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0	
586	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0	
*												
587	KK CPW57COMBINE											
588	HC	4	14.788									
*												
589	KK SRW57STORAGE											
590	KM Verrado SR42											
591	KO											
592	RS	1	STOR									
593	SV	24.40	29.60	35.70	42.00	48.50	55.20	62.20	69.30	76.70		
594	SQ				368.00	1040.00	1912.00	2944.00	4114.00	5410.00		
595	SE	1084.0	1090.00	1091.00	1092.00	1093.00	1094.00	1095.00	1096.00	1097.00	1098.00	
596	ST											
*												
597	KK W57W58ROUTE											
598	KM Cross-section: Taken from aerial and topo											
599	RS	1	FLOW									
600	RC	0.022	0.022	0.022	1236	0.0067	0.00					
601	RX	100.00	115.50	121.80	142.00	179.30	191.30	199.60	207.80			
602	RY	1072.0	1070.00	1064.00	1062.00	1061.90	1064.00	1065.00	1066.00			
*												
603	KK W58BASIN											
604	KM BASIN BOUNDARY VARIES FROM VERRADO DEVEL.COND.PLAN WOOD/PATEL 2006											
605	KM NEW 2' CI TOPO OBTAINED 2008											
606	BA	0.131										
607	LG	0.30	0.33	4.65	0.35	18						
608	UI	0	25	101	176	208	180	117	75	48	32	
609	UI	19	14	5	5	6	0	0	0	0	0	
610	UI	0	0	0	0	0	0	0	0	0	0	
611	UI	0	0	0	0	0	0	0	0	0	0	
612	UI	0	0	0	0	0	0	0	0	0	0	
*												
613	KK CPW58COMBINE											

614	HC	2	14.919									
*												
615	KK SRW58STORAGE											
616	KM Storage based on new topo section calculations											
617	KO											
618	RS	1	STOR									
619	SV	0.17	2.57	5.40	13.08	31.52	47.89	64.25	111.96	171.81		
620	SQ		784.10	2217.60	3099.20	3799.80	4122.90	4540.00	6878.80	112249.90		
621	SE	1084.0	1086.00	1088.00	1090.00	1092.00	1094.00	1095.00	1096.00	1098.00	1100.00	
622	ST											
*												
HEC-1 INPUT												
LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10	
623	KK DW58SEDIVERT											
624	KM Divert is stage storage on 4-10x8 boxes under I-10. Diverted flow goes s											
625	DT	DW58S	0.0	0.0								
626	DI	0.0	100.0	2000.0	4100.0	4200.0	5000.0	6000.0	7000.0	8000.0	9000.0	
627	DQ	0.0	100.0	2000.0	4100.0	4195.5	4606.7	4833.2	4983.7	5102.6	5203.3	
*												
628	KK W38BASIN											
629	KM BASIN BOUNDARY FORMED BY MCDOWELL, I-10, JACKRABBIT											
630	KM AND TUTHILL, DETAILED I-10 TOPO AND CULVERT INFO											
631	BA	0.251										
632	LG	0.32	0.32	4.65	0.33	7						
633	UI	0	30	77	163	235	279	279	236	174	127	
634	UI	93	68	51	36	27	20	14	7	7	8	
635	UI	7	0	0	0	0	0	0	0	0	0	
636	UI	0	0	0	0	0	0	0	0	0	0	
637	UI	0	0	0	0	0	0	0	0	0	0	
*												
638	KK CPW38COMBINE											
639	HC	2	15.17									
*												
640	KK DW38SEDIVERT											
641	KM Full flow capacity of culverts under I-10 is diverted flow											
642	DT	DW38S	0.0	0.0								
643	DI	0.0	100.0	200.0	300.0	400.0	467.0	500.0	800.0	1000.0	10000.0	
644	DQ	0.0	100.0	200.0	300.0	400.0	467.0	467.0	467.0	467.0	467.0	
*												
645	KK W38W37ROUTE											
646	KM Cross section based from 1990 topo, Manning's N Value: clean earth											
647	RS	3	FLOW									
648	RC	0.022	0.022	0.022	2849	0.0053	0.00					
649	RX	100.00	204.00	440.00	608.00	687.00	700.00	736.00	759.00			
650	RY	1083.0	1082.00	1080.00	1078.00	1078.00	1080.00	1082.00	1083.00			
*												
651	KK CPW37COMBINE											
652	ZW	A=CIP B=CPW37 C=FLOW										
653	HC	3	19.291									
*												
654	ZZ											







RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	WT3	187.	17.00	186.	180.	99.	21.52	
+	HYDROGRAPH AT	W21A	139.	12.42	17.	4.	1.	.20	
+	2 COMBINED AT	CPW21A	187.	17.00	186.	180.	101.	.20	
+	ROUTED TO	21A28A	187.	17.42	186.	180.	100.	.20	
+	HYDROGRAPH AT	W28A	508.	12.42	61.	16.	5.	.64	
+	2 COMBINED AT	CPW28A	511.	12.42	200.	186.	105.	.84	
+	ROUTED TO	W28A33	445.	12.83	195.	185.	105.	.84	
+	HYDROGRAPH AT	W33	685.	12.42	81.	21.	7.	.84	
+	2 COMBINED AT	CPW33	792.	12.58	258.	201.	112.	1.68	
+	ROUTED TO	W33W35	764.	12.75	255.	200.	112.	1.68	
+	HYDROGRAPH AT	W35	233.	12.33	26.	7.	2.	.28	
+	HYDROGRAPH AT	W34	255.	12.25	28.	8.	3.	.23	
+	ROUTED TO	SRW34	0.	.00	0.	0.	0.	.23	
+	ROUTED TO	W34W35	0.	.00	0.	0.	0.	.23	
+	3 COMBINED AT	CPW35	853.	12.67	275.	205.	114.	2.19	



+	ROUTED TO	W35W36	804.	13.17	268.	204.	114.	2.19	+	3 COMBINED AT	CPW44	2572.	12.50	359.	101.	34.	5.15
+	HYDROGRAPH AT	W36	496.	12.50	69.	18.	6.	.72	+	ROUTED TO	W44W46	2548.	12.50	359.	101.	34.	5.15
+	2 COMBINED AT	CPW36	935.	13.08	315.	216.	119.	2.91	+	HYDROGRAPH AT	W45	1151.	12.25	134.	34.	11.	1.03
+	ROUTED TO	W36W37	888.	13.42	311.	215.	119.	2.91	+	ROUTED TO	W45W46	994.	12.58	134.	34.	11.	1.03
+	HYDROGRAPH AT	W37	736.	12.58	113.	30.	10.	1.21	+	HYDROGRAPH AT	W46	957.	12.50	130.	37.	12.	.93
+	HYDROGRAPH AT	W22	961.	12.17	92.	27.	9.	.78	+	2 COMBINED AT	CPW46A	1918.	12.50	263.	71.	24.	1.96
+	ROUTED TO	W22W23	934.	12.25	92.	27.	9.	.78	+	DIVERSION TO	RW46	1124.	12.50	108.	27.	9.	1.96
+	HYDROGRAPH AT	W23	1064.	12.17	106.	31.	10.	.90	+	HYDROGRAPH AT	DW46RE	794.	12.50	155.	44.	15.	1.96
+	2 COMBINED AT	CPW23	1968.	12.25	198.	58.	19.	1.68	+	2 COMBINED AT	CPW46B	3331.	12.50	512.	144.	48.	7.11
+	ROUTED TO	W23W24	1783.	12.25	198.	58.	19.	1.68	+	ROUTED TO	W46W54	3283.	12.58	512.	144.	48.	7.11
+	HYDROGRAPH AT	W24	547.	12.25	57.	16.	5.	.47	+	HYDROGRAPH AT	W47	692.	12.25	83.	24.	8.	.67
+	2 COMBINED AT	CPW24	2320.	12.25	254.	74.	25.	2.15	+	HYDROGRAPH AT	W48	389.	12.25	44.	13.	4.	.35
+	ROUTED TO	W24W27	2107.	12.33	254.	74.	25.	2.15	+	2 COMBINED AT	CPW47	1077.	12.25	127.	37.	12.	1.02
+	HYDROGRAPH AT	W25	1037.	12.25	120.	32.	11.	1.10	+	ROUTED TO	W47W49	998.	12.33	127.	37.	12.	1.02
+	ROUTED TO	SRW25	0.	.00	0.	0.	0.	1.10	+	HYDROGRAPH AT	W50	971.	12.42	160.	47.	16.	1.35
+	ROUTED TO	W25W26	0.	.00	0.	0.	0.	1.10	+	HYDROGRAPH AT	W49	430.	12.25	48.	14.	5.	.38
+	HYDROGRAPH AT	W26	714.	12.33	92.	26.	9.	.68	+	3 COMBINED AT	CPW49	2214.	12.33	332.	98.	33.	2.75
+	2 COMBINED AT	CPW26	710.	12.33	91.	26.	9.	1.78	+	ROUTED TO	W49W51	2034.	12.50	332.	98.	33.	2.75
+	ROUTED TO	SRW26	0.	.00	0.	0.	0.	1.78	+	HYDROGRAPH AT	W51	143.	12.33	13.	3.	1.	.15
+	ROUTED TO	W26W27	0.	.00	0.	0.	0.	1.78	+	2 COMBINED AT	CPW51	2144.	12.42	345.	101.	34.	2.90
+	HYDROGRAPH AT	W27	495.	12.25	51.	14.	5.	.41	+	HYDROGRAPH AT	W52	850.	12.42	117.	32.	11.	1.12
+	3 COMBINED AT	CPW27	2525.	12.33	303.	87.	29.	4.34	+	2 COMBINED AT	CPW52	2980.	12.42	459.	132.	44.	4.02
+	ROUTED TO	W27W44	2142.	12.50	302.	87.	29.	4.34	+	ROUTED TO	W52W53	2758.	12.50	459.	132.	44.	4.02
+	HYDROGRAPH AT	W43	467.	12.08	41.	14.	5.	.21	+	HYDROGRAPH AT	W53	791.	12.17	57.	15.	5.	.57
+	ROUTED TO	SRW43	0.	.00	0.	0.	0.	.21	+	2 COMBINED AT	CPW53	2902.	12.50	514.	147.	49.	4.59
+	ROUTED TO	W43W44	0.	.00	0.	0.	0.	.21	+	DIVERSION TO	RW53	665.	12.50	59.	15.	5.	4.59
+	HYDROGRAPH AT	W44	440.	12.50	58.	14.	5.	.60	+	HYDROGRAPH AT							



+		DW53RE	2237.	12.50	455.	132.	44.	4.59
	ROUTED TO							
+		W53W54	2116.	12.67	455.	132.	44.	4.59
	HYDROGRAPH AT							
+		W54	957.	12.42	122.	35.	12.	.98
	3 COMBINED AT							
+		CPW54	6076.	12.58	1082.	309.	104.	12.68
	ROUTED TO							
+		W54W57	5911.	12.67	1081.	309.	104.	12.68
	HYDROGRAPH AT							
+		W56	558.	12.25	39.	10.	3.	.45
	DIVERSION TO							
+		RW56	558.	12.25	39.	10.	3.	.45
	HYDROGRAPH AT							
+		DW56RE	0.	.00	0.	0.	0.	.45
	ROUTED TO							
+		W56W57	0.	.00	0.	0.	0.	.45
	HYDROGRAPH AT							
+		W55	507.	12.25	56.	16.	5.	.50
	DIVERSION TO							
+		DW55S	355.	12.25	24.	6.	2.	.50
	HYDROGRAPH AT							
+		DW55RE	151.	12.25	31.	10.	3.	.50
	ROUTED TO							
+		W55W57	136.	12.58	31.	10.	3.	.50
	HYDROGRAPH AT							
+		W57	1251.	12.42	148.	43.	14.	1.16
	DIVERSION TO							
+		RW57	559.	12.08	37.	11.	4.	1.16
	HYDROGRAPH AT							
+		DW57RE	1251.	12.42	121.	32.	11.	1.16
	4 COMBINED AT							
+		CPW57	6785.	12.58	1228.	350.	117.	14.79
	ROUTED TO							
+		SRW57	6604.	12.67	1228.	334.	111.	14.79
	ROUTED TO							
+		W57W58	6575.	12.67	1228.	334.	111.	14.79
	HYDROGRAPH AT							
+		W58	166.	12.25	17.	5.	2.	.13
	2 COMBINED AT							
+		CPW58	6608.	12.67	1243.	338.	113.	14.92
	ROUTED TO							
+		SRW58	5281.	12.92	1244.	338.	113.	14.92
	DIVERSION TO							
+		DW58S	4670.	12.92	1207.	329.	110.	14.92
	HYDROGRAPH AT							
+		DW58SE	611.	12.92	37.	9.	3.	14.92
	HYDROGRAPH AT							
+		W38	237.	12.33	27.	7.	2.	.25
	2 COMBINED AT							
+		CPW38	657.	12.92	63.	16.	5.	15.17
	DIVERSION TO							
+		DW38S	467.	12.83	58.	15.	5.	15.17

+	HYDROGRAPH AT	DW38SE	190.	12.92	5.	1.	0.	15.17
	ROUTED TO							
+		W38W37	78.	13.17	5.	1.	0.	15.17
	3 COMBINED AT							
+		CPW37	1065.	13.25	406.	240.	129.	19.29

\*\*\* NORMAL END OF HEC-1 \*\*\*



C.6 EXISTING CONDITIONS WITH PROJECT IN PLACE, 10-YEAR FOR FRS#3 AREA

```

1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 10DEC09 TIME 15:52:37
*
*****
  
```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
  
```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X
XXXXXXXX XXXX X XXXXX X
X X X X X
X X X X X
X X XXXXXXX XXXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID WHITE TANKS AREA, WATERSHED CONTRIBUTING TO FRS#3
2 ID PREPARED BY HOSKIN RYAN CONSULTANTS EXCLUSIVELY FOR
3 ID FRS#3 OUTLET CHANNEL DESIGN, 12-05-2009
4 ID BASED ON HDR LOOP303/WHITE TANKS ADMPU AHA (09-04-09)
5 ID HEC-1 MODEL OF EXISTING CONDITION W/ CIP
6 ID MODIFICATIONS INCLUDE:
7 ID (1) UPDATE WITH AVERAGE RAINFALL DEPTH FOR FRS#3 WATERSHED ONLY
8 ID (2) UPDATE THE STAGE-STORAGE-DISCHARGE CURVE BASED ON URS DESIGN
9 ID OF FRS#3 PRINCIPAL AND EMERGENCY SPILLWAY (DISCHARGE
10 ID INCLUDING INFILTRATION)
11 ID (3) SEPARATE FRS#3 OUTFLOW AND INFILTRATION
12 ID *****
13 ID Flood Control District of Maricopa County
14 ID L303_EX_CIP_MB02 - Loop 303/ White Tanks ADMPU AHA
15 ID 100 YEAR
16 ID 24 Hour Storm
17 ID Unit Hydrograph: S-Graph
18 ID 08/18/2009
19 ID FCDMC CONTRACT 2007C031
20 ID BY HDR ENGINEERING (#79902)
21 ID EXISTING CONDITIONS WITH CIP-AUGUST 2009
22 ID MAJOR BASIN 02
23 ID FILE NAME: ECIP-MB2.DAT
24 IT 5 1JAN99 1200 2000
25 IN 15
26 IO 5
*DIAGRAM
*
27 JD 2.572 0.0001
28 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
29 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
30 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
31 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
32 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
33 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
34 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
35 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
36 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
37 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
  
```

```

38 JD 2.443 10.0
39 JD 2.315 30.0
*
40 KK L21BASIN
41 KM BASIN BOUNDARY FROM MCMICKEN DAM ON THE WEST AND THE
42 KM BEARDSLEY CSR ON THE EAST
43 BA 0.525
44 LG 0.34 0.32 4.55 0.37 1
45 UI 0 20 20 20 21 58 70 88 109 125
46 UI 140 158 170 180 187 193 193 194 187 179
47 UI 172 150 140 123 113 101 93 83 76 70
48 UI 61 56 51 45 40 38 34 31 32 22
49 UI 21 21 20 14 14 14 13 14 11 5
*
  
```

1 HEC-1 INPUT PAGE 2

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
50 KK DL21REDIVERT
51 KM Mass grading and Storage along canal
52 DT RL21 57.3 0.0
53 DI 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
54 DQ 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
*
55 KK L21L2ROUTE
56 KM Cross-section: Cross-section determined from A-team survey
57 KM Manning's N Value: earth w/sparse trees and brush, ponding against canal
58 RS 1 FLOW
59 RC 0.032 0.032 0.032 8793 0.0020 0.00
60 RX 100.00 101.00 107.00 117.00 169.00 409.00 512.00 513.00
61 RY 1328.1 1328.00 1326.00 1324.00 1324.10 1326.00 1328.00 1328.10
*
  
```

```

62 KK L22BASIN
63 KM BASIN BOUNDARY FROM MCMICKEN DAM ON THE WEST AND THE
64 KM BEARDSLEY CSR ON THE EAST
65 BA 0.362
66 LG 0.34 0.34 4.35 0.39 0
67 UI 0 19 19 21 56 79 101 124 144 162
68 UI 170 183 184 177 172 154 133 117 103 89
69 UI 78 68 59 52 43 38 36 29 28 20
70 UI 20 18 13 13 13 12 5 5 4 5
71 UI 5 4 5 4 5 5 4 0 0 0
*
72 KK DL22REDIVERT
73 KM Storage along canal
74 DT RL22 15.6 0.0
75 DI 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
76 DQ 0.0 500.0 5000.0 50000.0 0.0 0.0 0.0 0.0 0.0 0.0
*
  
```

```

77 KK CPL22COMBINE
78 HC 2 0.887
*
79 KK L22W01ROUTE
80 KM Cross-section: Cross-section determined from 1991 topo
81 KM Manning's N Value: earth w/ sparse trees and brush
82 RS 4 FLOW
83 RC 0.032 0.032 0.032 3159 0.0063 0.00
84 RX 100.00 101.00 102.00 115.00 128.00 140.00 141.00 142.00
85 RY 1320.2 1320.10 1320.00 1314.00 1314.10 1320.00 1320.10 1320.20
*
  
```

```

86 KK W01BASIN
87 KM BASIN BOUNDARY FROM FRS#3 ON THE WEST AND THE BEARDSLEY CSR ON THE EAST
88 BA 0.191
89 LG 0.34 0.34 3.95 0.40 0
90 UI 0 38 144 258 304 262 170 110 71 44
91 UI 29 21 8 7 8 0 0 0 0 0
*
  
```

1 HEC-1 INPUT PAGE 3

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
92 UI 0 0 0 0 0 0 0 0 0 0
93 UI 0 0 0 0 0 0 0 0 0 0
  
```



```

94  UI 0 0 0 0 0 0 0 0 0 0
95  KK CPW01COMBINE
96  HC 2 1.078
*

97  KK W01W02ROUTE
98  KM Cross-section: Estimated 3' deep and 4:1 side slopes
99  KM width based on aerial
100 KM Manning's N Value: natural desert wash w/ vegetation
101 RS 1 FLOW
102 RC 0.035 0.035 0.035 2650 0.0053 0.00
103 RX 100.00 111.00 122.00 139.00 162.00 182.00 191.00 200.00
104 RY 1290.5 1290.25 1290.00 1286.00 1286.10 1290.00 1290.25 1290.50
*

105 KK W02BASIN
106 KM BASIN BOUNDARY FROM 1990 TOPO, ALL FLOW TO SOUTH
107 KM MCMICKEN DAM ON THE WEST AND THE BEARDSLEY CSR ON THE EAST
108 BA 0.394
109 LG 0.35 0.35 4.65 0.32 0
110 UI 0 56 195 370 497 530 435 300 209 145
111 UI 99 70 46 38 14 13 14 13 0 0
112 UI 0 0 0 0 0 0 0 0 0 0
113 UI 0 0 0 0 0 0 0 0 0 0
114 UI 0 0 0 0 0 0 0 0 0 0
*

115 KK CPW02COMBINE
116 HC 2 1.472
*

117 KK W02W05ROUTE
118 KM Cross-section: Natural Desert Wash w/ vegetation
119 RS 1 FLOW
120 RC 0.035 0.035 0.035 2214 0.0045 0.00
121 RX 100.00 106.00 112.00 119.00 135.00 137.00 138.00 141.00
122 RY 1280.0 1278.00 1277.00 1276.00 1275.90 1277.00 1278.00 1280.00
*

123 KK W03BASIN
124 KM BASIN BOUNDARY FROM 1990 TOPO
125 BA 1.971
126 LG 0.35 0.35 4.00 0.47 20
127 UI 0 145 146 415 653 907 1064 1233 1685 1257
128 UI 947 849 756 672 606 522 442 374 341 315
129 UI 263 217 186 167 159 119 113 107 71 72
130 UI 70 71 37 27 28 28 28 28 28 28
131 UI 27 29 27 0 0 0 0 0 0 0
*

132 KK W03W04ROUTE
133 KM Cross-section: Side slopes and width based on aerial and topo
134 KM Manning's N Value: natural desert wash w/ vegetation
135 RS 3 FLOW
136 RC 0.035 0.035 0.035 18417 0.0490 0.00
137 RX 100.00 140.00 180.00 210.00 235.00 305.00 345.00 385.00
138 RY 1511.0 1510.50 1510.00 1502.00 1502.10 1510.00 1511.00 1512.00
*

139 KK W04BASIN
140 KM BASIN BOUNDARY FROM 1990 TOPO
141 BA 2.034
142 LG 0.35 0.35 4.60 0.34 10
143 UI 0 144 147 379 620 881 1032 1176 1561 1470
144 UI 998 876 788 702 637 566 477 407 357 335
145 UI 304 239 203 188 158 157 113 111 105 72
146 UI 71 71 71 40 28 28 27 28 28 28
147 UI 28 28 27 28 0 0 0 0 0 0
*

148 KK CPW04COMBINE
149 HC 2 4.005
*

```

```

150 KK W04W05ROUTE
151 KM Cross-section: Estimated 3' deep and 4:1 side slopes
152 KM width based on aerial / Manning's N Value: clean straight earth
153 RS 2 FLOW
154 RC 0.035 0.035 0.035 5298 0.0098 0.00
155 RX 100.00 120.00 140.00 160.00 174.00 214.00 234.00 254.00
156 RY 1313.0 1312.50 1312.00 1308.00 1308.10 1312.00 1312.50 1313.00
*

157 KK W05BASIN
158 KM BASIN BOUNDARY FROM 1990 TOPO AND BEARDSLEY CSR
159 BA 0.316
160 LG 0.35 0.35 4.25 0.42 0
161 UI 0 32 62 147 214 282 302 300 260 199
162 UI 153 119 90 67 54 40 32 22 22 9
163 UI 7 8 8 8 8 0 0 0 0 0
164 UI 0 0 0 0 0 0 0 0 0 0
165 UI 0 0 0 0 0 0 0 0 0 0
*

166 KK CPW05COMBINE
167 HC 3 5.793
*

168 KK DW05SEDIWERT
169 KM North Inlet Channel Divert from L303M3LA.OUT model given to HDR by
170 KM FCDMC 05062009
171 DT DW05S 0.0 0.0
172 DI 600.0 800.0 1000.0 1200.0 1400.0 1600.0 2000.0 2400.0 2715.0 2800.0
173 DQ 105.0 163.0 361.0 498.0 640.0 792.0 1100.0 1437.0 1605.0 1630.0
*

174 KK W0512AROUTE
175 KM White Tanks FRS#3 North Inlet Channel South
176 KM Channel plans FCD Contract No 2007C021
177 KM Cholla Wash
178 RS 3 FLOW
179 RC 0.050 0.030 0.050 5306 0.0083 0.00
180 RX 1010.0 1015.00 1020.00 1050.00 1100.00 1275.00 1580.00 1750.00
181 RY 1251.0 1249.00 1249.00 1245.00 1244.90 1250.00 1250.00 1254.00
*

182 KK W06BASIN
183 KM BASIN BOUNDARY FROM 1990 TOPO
184 BA 0.707
185 LG 0.35 0.35 4.30 0.41 18
186 UI 0 103 362 675 987 837 576 461 363 257
187 UI 217 150 119 90 72 49 48 20 20 19
188 UI 20 20 0 0 0 0 0 0 0 0
189 UI 0 0 0 0 0 0 0 0 0 0
190 UI 0 0 0 0 0 0 0 0 0 0
*

191 KK W07BASIN
192 KM BASIN BOUNDARY FROM 1990 TOPO
193 BA 0.312
194 LG 0.35 0.35 4.25 0.42 19
195 UI 0 65 253 428 510 316 236 171 126 89
196 UI 63 46 33 26 14 11 10 10 0 0
197 UI 0 0 0 0 0 0 0 0 0 0
198 UI 0 0 0 0 0 0 0 0 0 0
199 UI 0 0 0 0 0 0 0 0 0 0
*

200 KK CPW07COMBINE
201 HC 2 1.019
*

202 KK W07W08ROUTE
203 KM Cross-section: Based on aerial and topo
204 KM Manning's N Value: Natural Desert wash w/ vegetation
205 KM N value modified to slow velocity
206 RS 1 FLOW
207 RC 0.045 0.040 0.045 5589 0.0796 0.00
208 RX 100.00 136.00 173.00 197.00 234.00 254.00 298.00 342.00
209 RY 2880.0 2865.00 2850.00 2840.00 2840.00 2850.00 2865.00 2880.00

```

1

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1

HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10



210 KK W08BASIN  
 211 KM BASIN BOUNDARY FROM 1990 TOPO  
 212 BA 0.446  
 213 LG 0.35 0.35 3.95 0.40 20  
 214 UI 0 156 587 941 577 413 262 183 117 78  
 215 UI 49 32 19 19 19 0 0 0 0 0  
 216 UI 0 0 0 0 0 0 0 0 0 0  
 217 UI 0 0 0 0 0 0 0 0 0 0  
 \*  
 HEC-1 INPUT

PAGE 6

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 218 UI 0 0 0 0 0 0 0 0 0 0  
 \*  
 219 KK CPW08COMBINE  
 220 HC 2 1.465  
 \*  
 221 KK W09BASIN  
 222 KM BASIN BOUNDARY FROM 1990 TOPO  
 223 BA 0.335  
 224 LG 0.35 0.35 3.95 0.40 20  
 225 UI 0 125 468 716 427 304 193 127 85 53  
 226 UI 37 19 14 15 0 0 0 0 0 0  
 227 UI 0 0 0 0 0 0 0 0 0 0  
 228 UI 0 0 0 0 0 0 0 0 0 0  
 229 UI 0 0 0 0 0 0 0 0 0 0  
 \*  
 230 KK CPW09COMBINE  
 231 HC 2 1.8  
 \*

232 KK W09W10ROUTE  
 233 KM Cross-section: Based on aerial and topo  
 234 KM Manning's N Value: Natural Desert wash w/ vegetation  
 235 KM N value modified to slow velocity  
 236 RS 1 FLOW  
 237 RC 0.045 0.040 0.045 11134 0.0683 0.00  
 238 RX 100.00 137.00 172.00 192.00 220.00 230.00 284.00 338.00  
 239 RY 1990.0 1975.00 1960.00 1950.00 1950.00 1960.00 1975.00 1990.00  
 \*

240 KK W10BASIN  
 241 KM BASIN BOUNDARY FROM 1990 TOPO  
 242 BA 1.338  
 243 LG 0.35 0.35 3.95 0.40 20  
 244 UI 0 153 376 806 1108 1572 1334 920 794 647  
 245 UI 533 402 350 278 212 175 141 119 85 75  
 246 UI 75 29 30 30 29 30 29 0 0 0  
 247 UI 0 0 0 0 0 0 0 0 0 0  
 248 UI 0 0 0 0 0 0 0 0 0 0  
 \*

249 KK CPW10COMBINE  
 250 HC 2 3.138  
 \*

251 KK W11BASIN  
 252 KM BASIN BOUNDARY FROM 1990 TOPO  
 253 BA 0.812  
 254 LG 0.35 0.35 3.95 0.40 20  
 255 UI 0 100 272 567 759 1098 696 556 469 375  
 256 UI 285 236 190 141 116 92 77 52 48 39  
 257 UI 20 19 19 19 19 20 0 0 0 0  
 258 UI 0 0 0 0 0 0 0 0 0 0  
 \*  
 HEC-1 INPUT

PAGE 7

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 259 UI 0 0 0 0 0 0 0 0 0 0  
 \*  
 260 KK CPW11COMBINE  
 261 HC 2 3.95  
 \*

262 KK W11W12ROUTE  
 263 KM Cross-section: Based on aerial and topo  
 264 KM Manning's N Value: Natural Desert wash w/ vegetation  
 265 RS 8 FLOW  
 266 RC 0.045 0.035 0.045 21182 0.0205 0.00  
 267 RX 100.00 110.30 290.50 304.40 319.20 330.60 344.60 569.70  
 268 RY 1312.0 1310.00 1308.00 1306.00 1305.90 1308.00 1310.00 1312.00  
 \*

269 KK W12BASIN  
 270 KM BASIN BOUNDARY FROM 1990 TOPO AND BEARDSLEY CSR  
 271 BA 1.868  
 272 LG 0.34 0.34 4.60 0.34 3  
 273 UI 0 125 126 289 490 706 847 961 1170 1474  
 274 UI 1002 820 727 654 604 537 483 418 353 310  
 275 UI 293 266 221 193 160 148 139 120 96 96  
 276 UI 83 61 61 61 61 37 24 24 24 24  
 277 UI 24 25 24 24 24 24 24 0 0 0  
 \*

278 KK DW05SERETRIEVE  
 279 KM Flow traveling down North Inlet Channel  
 280 DR DW05S  
 \*

281 KK W0512BROUTE  
 282 KM White Tanks FRS#3 North Inlet Channel South  
 283 KM Channel plans FCD Contract No 2007C021  
 284 KM N value modified to mimic slowing of velocity by drop structures  
 285 RS 2 FLOW  
 286 RC 0.035 0.035 0.035 5494 0.0170 0.00  
 287 RX 100.00 120.00 135.00 165.00 220.00 300.00 315.00 379.00  
 288 RY 1244.7 1239.65 1239.50 1232.00 1231.90 1239.50 1239.65 1255.65  
 \*

289 KK CPW12COMBINE  
 290 HC 4 11.61  
 \*

291 KK W12W13ROUTE  
 292 KM From NIC South Channel Plans at Sta. 535+00  
 293 RS 1 FLOW  
 294 RC 0.032 0.032 0.032 2062 0.0051 0.00  
 295 RX 100.00 120.00 162.50 205.00 355.00 397.50 440.00 460.00  
 296 RY 1218.4 1218.18 1211.10 1203.98 1204.45 1211.53 1218.65 1218.85  
 \*

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
 297 KK W13BASIN  
 298 KM BASIN BOUNDARY FROM 1990 TOPO AND BEARDSLEY CSR  
 299 BA 1.584  
 300 LG 0.35 0.35 4.90 0.29 3  
 301 UI 0 107 108 254 430 622 734 838 1035 1255  
 302 UI 820 689 615 557 511 445 405 352 287 261  
 303 UI 248 223 176 154 137 121 119 90 83 83  
 304 UI 59 52 53 53 48 21 20 21 20 21  
 305 UI 20 21 21 20 21 21 0 0 0 0  
 \*

306 KK CPW13COMBINE  
 307 HC 2 13.194  
 \*

308 KK W13W16ROUTE  
 309 KM From NIC South Channel Plans  
 310 KM at Sta. 523+00  
 311 RS 2 FLOW  
 312 RC 0.032 0.032 0.032 6257 0.0051 0.00  
 313 RX 100.00 115.00 162.00 209.10 359.10 435.90 465.00 480.00  
 314 RY 1216.9 1216.77 1208.93 1201.09 1203.09 1215.09 1223.54 1223.69  
 \*

315 KK W15BASIN  
 316 KM BASIN BOUNDARY FROM 1990 TOPO  
 317 BA 1.227  
 318 LG 0.35 0.35 4.55 0.35 0  
 319 UI 0 98 112 315 498 652 757 975 1045 671

1

1

PAGE 8



320	UI	578	523	457	400	352	284	245	227	196	161
321	UI	128	117	107	86	75	70	49	48	47	43
322	UI	19	18	19	19	19	19	18	19	19	0
323	UI	0	0	0	0	0	0	0	0	0	0

324	KK	W14BASIN									
325	KM	BASIN BOUNDARY FROM 1990 TOPO									
326	BA	1.582									
327	LG	0.35	0.37	5.20	0.25	3					
328	UI	0	165	333	776	1104	1420	1804	1142	948	811
329	UI	682	567	431	386	320	242	201	182	128	124
330	UI	82	80	79	32	32	32	32	31	32	32
331	UI	0	0	0	0	0	0	0	0	0	0
332	UI	0	0	0	0	0	0	0	0	0	0

333	KK	W14W15ROUTE									
334	KM	Cross-section: Based on aerial and topo									
335	KM	Manning's N Value: Natural Desert wash w/ vegetation									
336	RS	3 FLOW									
337	RC	0.035	0.035	0.035	7308	0.0104	0.00				
338	RX	100.00	130.00	150.00	184.00	210.00	226.00	246.00	276.00		
339	RY	1280.0	1276.00	1274.00	1270.00	1269.90	1274.00	1276.00	1280.00		

HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

340	KK	CPW15COMBINE									
341	HC	2 2.809									

342	KK	W15W16ROUTE									
343	KM	Cross-section: Based on aerial and topo									
344	KM	Manning's N Value: Natural Desert wash w/ vegetation									
345	RS	1 FLOW									
346	RC	0.035	0.035	0.035	2750	0.0087	0.00				
347	RX	100.00	135.00	135.00	232.00	328.00	360.00	498.00	635.00	735.00	
348	RY	1202.0	1200.00	1199.00	1198.00	1197.90	1199.00	1200.00	1202.00		

349	KK	W16BASIN									
350	KM	BASIN BOUNDARY FROM BEARDSLEY CSR, THE FRS#4 AND 1990 TOPO									
351	BA	0.530									
352	LG	0.22	0.22	4.55	0.33	0					
353	UI	0	61	148	318	464	562	575	509	384	282
354	UI	211	157	115	87	65	42	42	15	14	15
355	UI	15	15	0	0	0	0	0	0	0	0
356	UI	0	0	0	0	0	0	0	0	0	0
357	UI	0	0	0	0	0	0	0	0	0	0

358	KK	CPW16COMBINE									
359	HC	3 16.534									

360	KK	W16W20ROUTE									
361	KM	Cross-section: Based on aerial and topo									
362	KM	Manning's N Value: clean earth; straight									
363	RS	1 FLOW									
364	RC	0.022	0.022	0.022	3633	0.0130	0.00				
365	RX	100.00	113.00	127.00	136.00	245.00	272.00	318.00	384.00		
366	RY	1186.0	1184.00	1182.00	1180.00	1179.90	1182.00	1184.00	1186.00		

367	KK	W18BASIN									
368	KM	BASIN BOUNDARY FROM 1990 TOPO									
369	BA	1.260									
370	LG	0.35	0.35	4.40	0.38	8					
371	UI	0	38	38	38	38	38	99	112	147	168
372	UI	200	230	242	261	278	296	307	348	390	440
373	UI	461	337	285	264	241	228	223	213	202	195
374	UI	185	177	171	161	152	148	137	130	119	110
375	UI	100	97	93	90	89	86	79	81	68	62

376	KK	W17BASIN									
377	KM	BASIN BOUNDARY FROM 1990 TOPO									

378	BA	1.497									
379	LG	0.35	0.35	4.30	0.41	18					
380	UI	0	169	396	865	1197	1639	1571	1038	892	737
381	UI	607	469	398	324	247	201	173	131	110	82

HEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

382	UI	83	52	32	33	32	32	33	32	0	0
383	UI	0	0	0	0	0	0	0	0	0	0
384	UI	0	0	0	0	0	0	0	0	0	0

385	KK	W17W18ROUTE									
386	KM	Cross-section: Based on aerial and topo									
387	KM	Manning's N Value: natural desert wash w/ vegetation									
388	KM	and heavy vegetation									
389	RS	2 FLOW									
390	RC	0.045	0.035	0.045	8559	0.0257	0.00				
391	RX	100.00	140.00	150.00	156.00	194.00	216.00	255.00	342.00		
392	RY	1302.0	1300.00	1298.00	1296.00	1295.90	1298.00	1300.00	1302.00		

393	KK	CPW18COMBINE									
394	HC	2 2.757									

395	KK	W18W20ROUTE									
396	KM	Cross-section: Estimated 3' deep, side slopes and width based									
397	KM	on aerial / Manning's N Value: natural desert wash w/ vegetation									
398	RS	5 FLOW									
399	RC	0.035	0.035	0.035	6914	0.0058	0.00				
400	RX	100.00	155.00	170.00	210.00	216.00	256.00	276.00	336.00		
401	RY	1249.0	1248.25	1248.00	1245.00	1245.10	1248.00	1248.25	1249.00		

402	KK	W19BASIN									
403	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
404	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
405	BA	1.158									
406	LG	0.35	0.35	3.88	0.42	20					
407	UI	0	241	939	1587	1896	1172	876	636	467	328
408	UI	236	172	119	99	51	39	39	39	0	0
409	UI	0	0	0	0	0	0	0	0	0	0
410	UI	0	0	0	0	0	0	0	0	0	0
411	UI	0	0	0	0	0	0	0	0	0	0

412	KK	SRW19STORAGE									
413	KM	Master Drainage Plan for the Caterpillar Property (Basin #16)									
414	KO										
415	RS	1 STOR									
416	SV	1.00	31.00	114.00	270.00	502.00	807.00	1319.00	1388.00	1460.00	
417	SQ										
418	SE	1198.0	1200.00	1210.00	1220.00	1230.00	1240.00	1250.00	1260.00	1261.00	1262.00
419	ST										

HEC-1 INPUT

PAGE 11

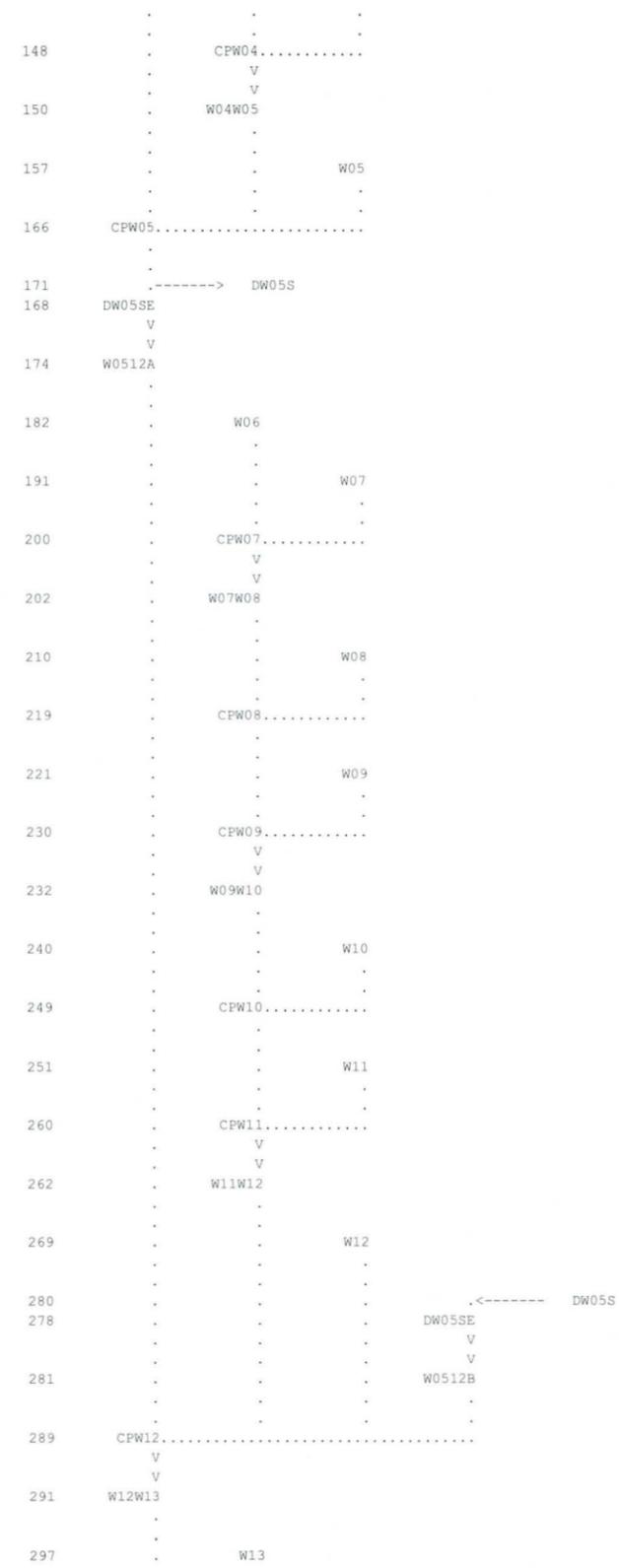
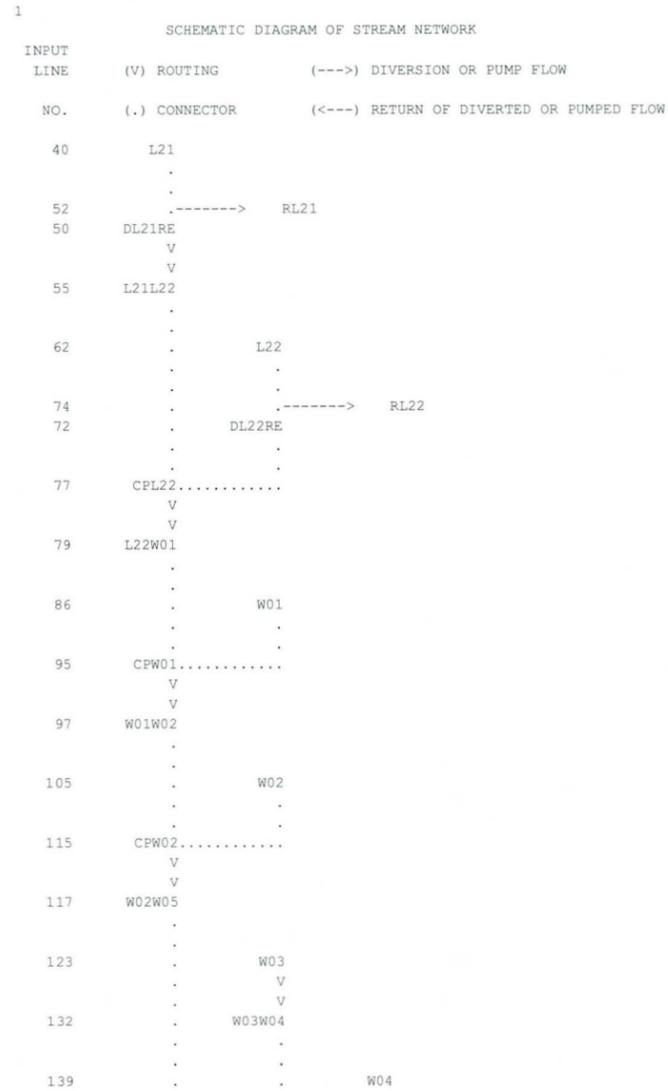
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

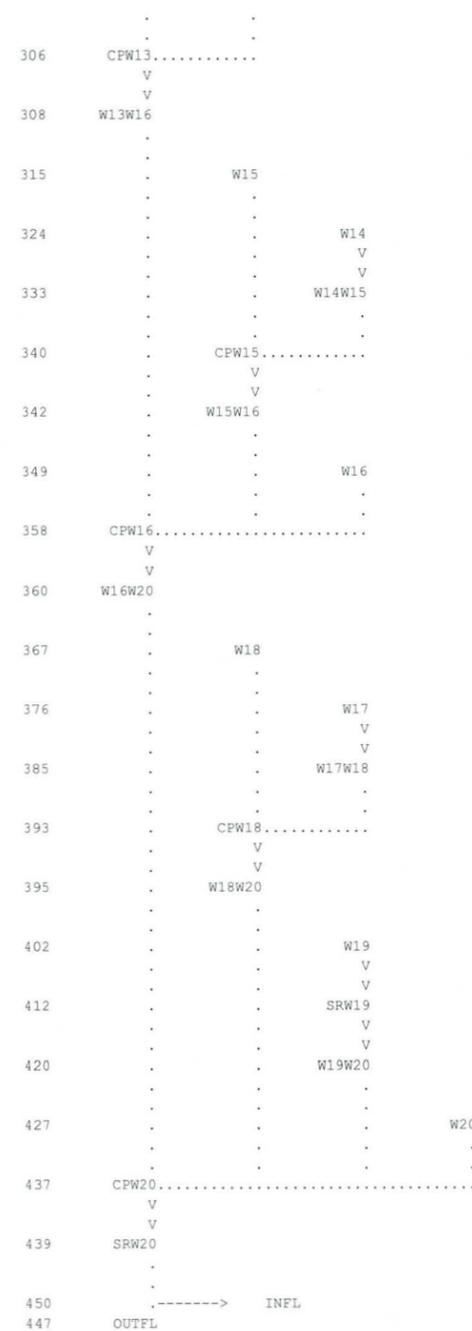
420	KK	W19W20ROUTE									
421	KM	Cross-section: Estimated 4' deep and 3:1 side slopes, width based									
422	KM	on aerial / Manning's N Value: earth with sparse trees and shrubs									
423	RS	1 FLOW									
424	RC	0.032	0.032	0.032	3790	0.0158	0.00				
425	RX	100.00	120.00	140.00	152.00	158.00	170.00	190.00	210.00		
426	RY	1240.5	1240.25	1240.00	1236.00	1236.00	1240.00	1240.25	1240.50		

427	KK	W20BASIN									
428	KM	BASIN BOUNDARY FROM WHITE TANKS #4 FRS, S-S-D CURVES									
429	KM	FROM JAN 2009 FCDMC, AND FROM 1990 TOPO									
430	BA	1.137									
431	LG	0.29	0.29	4.10	0.44	0					
432	UI	0	104	165	390	618	777	969	1101	712	596
433	UI	525	458	389	315	265	233	199	157	131	115
434	UI	98	80	71	51	50	51	26	19	20	20
435	UI	20	20	20	20	20	0	0	0	0	0



436	UI	0	0	0	0	0	0	0	0	0	0	0	0	0
437	KK	CPW20COMBINE												
438	HC	4	21.586											
439	KK	SRW20 STORAGE												
440	KM	STAGE-STORAGE-DISCHARGE CURVE FROM URS DESIGN OF FRS#3 OUTLET STRUCTURE												
441	KM	THE DISCHARGE INCLUDING OUTFLOW FROM PRINCIPAL AND EMERGENCY SPILLWAY,												
442	KM	AS WELL AS INFILTRATION												
443	RS	1	STOR	-1										
444	SV	44.8	388	585	846	1002	2045	3218	3557	4693	6510			
445	SQ	0.02	0.17	4.5	187	203	276	330	2936	24545	70439			
446	SE	1188	1198	1200	1202	1203	1208	1212	1213	1216	1220			
447	KK	OUTFL												
448	KM	SEPRATE OUTFLOW FROM INFILTRATION												
449	ZW	A=WT B=FRS3 C=FLOW												
450	DT	INFL												
451	DI	0	4.5	86	203	330	2936	24545	70439					
452	DQ	0	4.5	10	22	73	79	96	121					
453	ZZ													





RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	L21	81.	13.25	24.	6.	2.	.52	

+	DIVERSION TO	RL21	81.	13.25	24.	6.	2.	.52
+	HYDROGRAPH AT	DL21RE	0.	.00	0.	0.	0.	.52
+	ROUTED TO	L21L22	0.	.00	0.	0.	0.	.52
+	HYDROGRAPH AT	L22	72.	12.92	15.	4.	1.	.36
+	DIVERSION TO	RL22	72.	12.92	15.	4.	1.	.36
+	HYDROGRAPH AT	DL22RE	0.	.00	0.	0.	0.	.36
+	2 COMBINED AT	CPL22	0.	.00	0.	0.	0.	.89
+	ROUTED TO	L22W01	0.	.00	0.	0.	0.	.89
+	HYDROGRAPH AT	W01	112.	12.25	8.	2.	1.	.19
+	2 COMBINED AT	CPW01	111.	12.25	8.	2.	1.	1.08
+	ROUTED TO	W01W02	75.	12.42	8.	2.	1.	1.08
+	HYDROGRAPH AT	W02	209.	12.33	18.	5.	2.	.39
+	2 COMBINED AT	CPW02	274.	12.33	26.	7.	2.	1.47
+	ROUTED TO	W02W05	240.	12.42	26.	7.	2.	1.47
+	HYDROGRAPH AT	W03	658.	12.58	132.	41.	14.	1.97
+	ROUTED TO	W03W04	525.	12.92	132.	41.	14.	1.97
+	HYDROGRAPH AT	W04	651.	12.58	118.	33.	11.	2.03
+	2 COMBINED AT	CPW04	999.	12.67	248.	74.	25.	4.01
+	ROUTED TO	W04W05	940.	12.92	248.	74.	25.	4.01
+	HYDROGRAPH AT	W05	110.	12.42	13.	3.	1.	.32
+	3 COMBINED AT	CPW05	1066.	12.83	286.	83.	28.	5.79
+	DIVERSION TO	DW05S	406.	12.83	110.	39.	13.	5.79
+	HYDROGRAPH AT	DW05SE	660.	12.83	176.	44.	15.	5.79
+	ROUTED TO	W0512A	649.	13.08	176.	44.	15.	5.79
+	HYDROGRAPH AT	W06	387.	12.25	47.	14.	5.	.71
+	HYDROGRAPH AT	W07	194.	12.25	21.	6.	2.	.31
+	2 COMBINED AT	CPW07	578.	12.25	68.	21.	7.	1.02





C.7 EXISTING CONDITIONS WITH PROJECT IN PLACE, 10-YEAR FOR JACKRABBIT CORRIDOR

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 10DEC09 TIME 15:53:08 *
*****

*****
* U.S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****
  
```

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1

```

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID WHITE TANKS AREA, WATERSHED CONTRIBUTING TO FRS#3
2 ID PREPARED BY HOSKIN RYAN CONSULTANTS EXCLUSIVELY FOR
3 ID FRS#3 OUTLET CHANNEL DESIGN, 12-09-2009
4 ID BASED ON HDR LOOP303/WHITE TANKS ADMPU AHA (09-04-09)
5 ID HEC-1 MODEL OF EXISTING CONDITIONS WITH CIP
6 ID MODIFICATIONS INCLUDE:
7 ID (1) UPDATE WITH AVERAGE RAINFALL DEPTH FOR JACKRABBIT CORRIDOR
8 ID (2) UPDATE THE PROPOSED CHANNEL DESIGN
9 ID (3) DELETE RETENTION OF PASQUELETTI TO REFLECT EXIST CONDITIONS
10 ID
11 ID *****
12 ID Flood Control District of Maricopa County
13 ID L303 EX_CIP_MB02 - Loop 303/ White Tanks ADMPU AHA
14 ID 100 YEAR
15 ID 24 Hour Storm
16 ID Unit Hydrograph: S-Graph
17 ID 08/18/2009
18 ID FCDMC CONTRACT 2007C031
19 ID BY HDR ENGINEERING (#79902)
20 ID EXISTING CONDITIONS WITH CIP-AUGUST 2009
21 ID MAJOR BASIN 02
22 ID FILE NAME: ECIP-MB2.DAT
23 IT 5 1JAN99 1200 2000
24 IN 15
25 IO 5
*DIAGRAM
*
26 JD 2.353 0.0001
27 PC 0.000 0.002 0.005 0.008 0.011 0.014 0.017 0.020 0.023 0.026
28 PC 0.029 0.032 0.035 0.038 0.041 0.044 0.048 0.052 0.056 0.060
29 PC 0.064 0.068 0.072 0.076 0.080 0.085 0.090 0.095 0.100 0.105
30 PC 0.110 0.115 0.120 0.126 0.133 0.140 0.147 0.155 0.163 0.172
31 PC 0.181 0.191 0.203 0.218 0.236 0.257 0.283 0.387 0.663 0.707
32 PC 0.735 0.758 0.776 0.791 0.804 0.815 0.825 0.834 0.842 0.849
33 PC 0.856 0.863 0.869 0.875 0.881 0.887 0.893 0.898 0.903 0.908
34 PC 0.913 0.918 0.922 0.926 0.930 0.934 0.938 0.942 0.946 0.950
35 PC 0.953 0.956 0.959 0.962 0.965 0.968 0.971 0.974 0.977 0.980
36 PC 0.983 0.986 0.989 0.992 0.995 0.998 1.000
37 JD 2.235 10.0
  
```

```

*
38 KK WT3
39 KM OUTFLOW FROM WT FRS#3 OUTLET
40 BA 21.52
41 KO 5
42 ZR =QI A=WT B=FRS3 C=FLOW
*
43 KK W21ABASIN
44 KM Boundary based on Preliminary Design Plans for
45 KM White Tanks FRS #3 Outfall Channel dated
46 KM 12-08-2008 prepared by Gannett Fleming
47 ZW A=CIP B=W21A C=FLOW
48 BA 0.199
49 LG 0.35 0.35 4.35 0.40 0
HEC-1 INPUT
*
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
50 UI 0 19 35 81 123 161 180 182 168 133
51 UI 102 82 62 49 38 30 21 18 13 13
52 UI 5 5 4 5 5 5 0 0 0 0
53 UI 0 0 0 0 0 0 0 0 0 0
54 UI 0 0 0 0 0 0 0 0 0 0
*
55 KK CPW21ACOMBINE
56 ZW A=CIP B=CPW21A C=FLOW
57 HC 2 0.199
*
58 KK 21A28A ROUTE
59 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=30FT, SIDE SLOPE 6:1
60 ZW A=CIP B=21A28A C=FLOW
61 RS 4 FLOW -1
62 RC 0.045 0.035 0.045 3560 0.0010
63 RX 100 110 120 150 180 210 220 230
64 RY 1001 1000 1000 995 995 1000 1000 1001
*
65 KK W28ABASIN
66 KM Boundary based on Preliminary Design Plans for
67 KM White Tanks FRS #3 Outfall Channel dated
68 KM 12-08-2008 prepared by Gannett Fleming
69 BA 0.642
70 LG 0.34 0.32 4.55 0.35 1
71 UI 0 65 127 296 444 573 621 609 524 407
72 UI 308 239 181 135 110 80 64 45 44 16
73 UI 17 16 16 16 16 0 0 0 0 0
74 UI 0 0 0 0 0 0 0 0 0 0
75 UI 0 0 0 0 0 0 0 0 0 0
*
76 KK CPW28ACOMBINE
77 ZW A=CIP B=CPW28A C=FLOW
78 HC 2 0.841
*
79 KK W28A33 ROUTE
80 KM PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 4:1
81 ZW A=CIP B=W28A33 C=FLOW
82 RS 5 FLOW -1
83 RC 0.045 0.035 0.045 4336 0.0010
84 RX 100 110 120 140 180 200 210 220
85 RY 1001 1000 1000 995 995 1000 1000 1001
*
86 KK W33BASIN
87 KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN
88 KM WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO
89 ZW A=CIP B=W33 C=FLOW
90 BA 0.839
91 LG 0.31 0.27 4.00 0.47 4
92 UI 0 92 207 460 670 834 886 810 641 473
HEC-1 INPUT
*
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
93 UI 361 275 195 155 114 85 63 52 23 22
  
```

PAGE 2

PAGE 3



94	UI	23	22	23	0	0	0	0	0	0	0
95	UI	0	0	0	0	0	0	0	0	0	0
96	UI	0	0	0	0	0	0	0	0	0	0
*											
97	KK	CPW33COMBINE									
98	ZW	A=CIP B=CPW33 C=FLOW									
99	HC	2 1.68									
*											
100	KK	W33W35 ROUTE									
101	KM	PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 6:1									
102	ZW	A=CIP B=W33W35 C=FLOW									
103	RS	3 FLOW -1									
104	RC	0.045	0.035	0.045	2658	0.0010					
105	RX	100	110	116	152	192	228	240	250		
106	RY	1001	1000	1000	994	994	1000	1000	1001		
*											
107	KK	W35BASIN									
108	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
109	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
110	BA	0.283									
111	LG	0.32	0.34	3.71	0.47	4					
112	UI	0	33	83	180	257	312	308	268	201	146
113	UI	108	80	58	43	33	22	19	8	8	8
114	UI	8	8	0	0	0	0	0	0	0	0
115	UI	0	0	0	0	0	0	0	0	0	0
116	UI	0	0	0	0	0	0	0	0	0	0
*											
117	KK	W34BASIN									
118	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
119	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
120	BA	0.228									
121	LG	0.32	0.31	3.74	0.46	20					
122	UI	0	33	131	238	312	316	236	162	111	74
123	UI	52	34	23	13	9	8	9	0	0	0
124	UI	0	0	0	0	0	0	0	0	0	0
125	UI	0	0	0	0	0	0	0	0	0	0
126	UI	0	0	0	0	0	0	0	0	0	0
*											
127	KK	SRW34STORAGE									
128	KM	Master Drainage Plan for the Caterpillar Property (Basin #29)									
129	KO										
130	RS	1 STOR									
131	SV	0.99	12.73	23.45	36.25	50.68	54.76	59.33	83.20		
132	SQ							88.00	6226.00		
133	SE	1164.5	1166.00	1170.00	1172.00	1174.00	1176.00	1177.50	1178.00	1180.00	
134	ST										
*											
HEC-1 INPUT											
PAGE 4											
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10											
135	KK	W34W35ROUTE									
136	KM	Cross-section: Estimated 3' deep and 4:1 side slopes, width based on									
137	KM	aerial. Manning's N Value: clean straight earth									
138	RS	1 FLOW									
139	RC	0.022	0.022	0.022	813	0.0111	0.00				
140	RX	100.00	104.00	108.00	120.00	132.00	144.00	152.00	160.00		
141	RY	1166.2	1166.10	1166.00	1160.00	1160.10	1162.00	1162.10	1162.20		
*											
142	KK	CPW35COMBINE									
143	ZW	A=CIP B=CPW35 C=FLOW									
144	HC	3 2.191									
*											
145	KK	W35W36 ROUTE									
146	KM	PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=40FT, SIDE SLOPE 4:1									
147	ZW	A=CIP B=W35W36 C=FLOW									
148	RS	7 FLOW -1									
149	RC	0.045	0.035	0.045	6051	0.0010					
150	RX	100	110	116	140	180	204	220	230		
151	RY	1001	1000	1000	994	994	1000	1000	1001		
*											

152	KK	W36BASIN									
153	KM	Boundary based on Aerial, topo, and Preliminary									
154	KM	Design Plans for White Tanks FRS #3 Outfall Channel									
155	KM	dated 12-08-2008 prepared by Gannett Fleming									
156	BA	0.720									
157	LG	0.31	0.28	4.00	0.47	4					
158	UI	0	65	101	247	385	507	591	617	609	513
159	UI	409	329	255	204	160	126	102	76	64	45
160	UI	45	25	16	16	15	16	16	16	0	0
161	UI	0	0	0	0	0	0	0	0	0	0
162	UI	0	0	0	0	0	0	0	0	0	0
*											
163	KK	CPW36COMBINE									
164	ZW	A=CIP B=CPW36 C=FLOW									
165	HC	2 2.911									
*											
166	KK	W36W37 ROUTE									
167	KM	PROPOSED JACKRABBIT CHANNEL, BOTTOM WIDTH=30FT, SIDE SLOPE 5:1									
168	ZW	A=CIP B=W36W37 C=FLOW									
169	RS	5 FLOW -1									
170	RC	0.045	0.035	0.045	4527	0.0010					
171	RX	100	110	120	150	180	210	220	230		
172	RY	1001	1000	1000	994	994	1000	1000	1001		
*											
HEC-1 INPUT											
PAGE 5											
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10											
173	KK	W37BASIN									
174	KM	WESTERN LIMIT DEFINED BY JACKRABBIT WASH									
175	KM	CAPACITY APPROX 12,000 CFS, VALENCIA HEIGHTS									
176	BA	1.210									
177	LG	0.32	0.31	4.20	0.44	4					
178	UI	0	96	112	318	497	664	822	897	937	893
179	UI	777	643	515	421	344	278	221	186	148	115
180	UI	104	69	66	63	23	24	23	24	23	24
181	UI	24	0	0	0	0	0	0	0	0	0
182	UI	0	0	0	0	0	0	0	0	0	0
*											
183	KK	W22BASIN									
184	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
185	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
186	BA	0.782									
187	LG	0.35	0.35	4.15	0.44	19					
188	UI	0	237	914	1559	1035	751	503	352	228	158
189	UI	107	80	37	31	31	31	0	0	0	0
190	UI	0	0	0	0	0	0	0	0	0	0
191	UI	0	0	0	0	0	0	0	0	0	0
192	UI	0	0	0	0	0	0	0	0	0	0
*											
193	KK	W22W23ROUTE									
194	KM	Cross-section: Based on aerial and topo									
195	KM	Manning's N Value: pavement and natural desert wash w/ vegetation									
196	RS	1 FLOW									
197	RC	0.035	0.013	0.035	4866	0.0719	0.00				
198	RX	100.00	112.00	113.00	126.00	439.00	477.00	496.00	515.00		
199	RY	1820.0	1815.00	1810.00	1800.00	1799.90	1810.00	1815.00	1820.00		
*											
200	KK	W23BASIN									
201	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
202	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
203	BA	0.897									
204	LG	0.35	0.35	4.35	0.40	18					
205	UI	0	236	906	1581	1306	885	636	424	309	204
206	UI	145	98	80	33	34	33	0	0	0	0
207	UI	0	0	0	0	0	0	0	0	0	0
208	UI	0	0	0	0	0	0	0	0	0	0
209	UI	0	0	0	0	0	0	0	0	0	0
*											
210	KK	CPW23COMBINE									
211	HC	2 1.679									
*											
HEC-1 INPUT											
PAGE 6											
LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10											



LINE	ID	1	2	3	4	5	6	7	8	9	10	
212	KK	W23W24ROUTE										
213	KM	Cross-section: Based on aerial and topo										
214	KM	Manning's N Value: natural desert wash w/ vegetation										
215	RS	1 FLOW										
216	RC	0.045	0.035	0.045	5335	0.0367	0.00					
217	RX	100.00	120.00	140.00	180.00	220.00	240.00	260.00	280.00			
218	RY	1462.0	1461.00	1460.00	1450.00	1450.10	1460.00	1461.00	1462.00			
219	KK	W24BASIN										
220	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
221	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
222	BA	0.475										
223	LG	0.35	0.35	4.90	0.29	14						
224	UI	0	88	342	575	788	483	372	280	201	154	
225	UI	104	82	60	39	38	15	14	15	15	0	
226	UI	0	0	0	0	0	0	0	0	0	0	
227	UI	0	0	0	0	0	0	0	0	0	0	
228	UI	0	0	0	0	0	0	0	0	0	0	
229	KK	CPW24COMBINE										
230	HC	2 2.154										
231	KK	W24W27ROUTE										
232	KM	Cross-section: Based on aerial and topo										
233	KM	Manning's N Value: natural desert wash w/ vegetation										
234	RS	1 FLOW										
235	RC	0.035	0.035	0.035	5873	0.0289	0.00					
236	RX	100.00	120.00	140.00	160.00	180.00	200.00	220.00	240.00			
237	RY	1094.0	1092.00	1090.00	1084.00	1084.10	1090.00	1090.25	1090.50			
238	KK	W25BASIN										
239	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
240	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
241	BA	1.099										
242	LG	0.35	0.35	4.80	0.30	8						
243	UI	0	143	438	866	1174	1490	915	737	620	467	
244	UI	358	307	216	171	140	110	76	71	53	27	
245	UI	28	28	27	28	0	0	0	0	0	0	
246	UI	0	0	0	0	0	0	0	0	0	0	
247	UI	0	0	0	0	0	0	0	0	0	0	
248	KK	SRW25STORAGE										
249	KM	Verrado on-line storage basin (WoodPatel ID SR20)										
250	KO											
251	RS	1 STOR										
252	SV	1.05	9.43	26.91	54.31	92.89	138.67	176.47	190.08	219.05		
253	SQ	265.00 1377.00										
254	SE	1443.0	1446.00	1450.00	1454.00	1458.00	1462.00	1466.00	1469.00	1470.00	1472.00	
255	ST											
	*											
		HEC-1 INPUT										
LINE	ID	1	2	3	4	5	6	7	8	9	10	
256	KK	W25W26ROUTE										
257	KM	Cross-section: Based on aerial and topo										
258	KM	Manning's N Value: natural desert wash w/ vegetation										
259	RS	1 FLOW										
260	RC	0.035	0.035	0.035	6978	0.0178	0.00					
261	RX	100.00	120.00	140.00	156.00	176.00	192.00	212.00	232.00			
262	RY	1451.5	1451.25	1451.00	1447.00	1447.10	1451.00	1451.25	1451.50			
263	KK	W26BASIN										
264	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
265	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
266	BA	0.682										
267	LG	0.33	0.37	6.20	0.17	15						
268	UI	0	86	245	500	680	926	574	465	390	304	
269	UI	231	197	152	110	95	69	59	43	42	21	

270	UI	17	16	17	16	17	0	0	0	0	0	
271	UI	0	0	0	0	0	0	0	0	0	0	
272	UI	0	0	0	0	0	0	0	0	0	0	
	*											
273	KK	CPW26COMBINE										
274	HC	2 1.781										
	*											
275	KK	SRW26STORAGE										
276	KM	Verrado on-line storage basin (WoodPatel ID SR21 and PH 6 Golf)										
277	KO											
278	RS	1 STOR										
279	SV	0.68	20.68	57.58	95.91	102.34	117.65	130.00				
280	SQ	265.00 1377.00 2000.00										
281	SE	1319.0	1320.00	1330.00	1340.00	1347.00	1348.00	1350.00	1351.00			
282	ST											
	*											
283	KK	W26W27ROUTE										
284	KM	Cross-section: based on topo and aerial										
285	KM	Manning's N Value: natural desert wash w/ vegetation										
286	RS	1 FLOW										
287	RC	0.035	0.035	0.035	3484	0.0172	0.00					
288	RX	100.00	120.00	140.00	152.00	168.00	180.00	200.00	220.00			
289	RY	1298.5	1298.25	1298.00	1294.00	1294.10	1298.00	1298.25	1298.50			
	*											
290	KK	W27BASIN										
291	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
292	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
293	BA	0.411										
294	LG	0.32	0.37	5.80	0.20	11						
295	UI	0	76	296	498	681	418	323	241	174	133	
296	UI	91	71	51	34	33	13	13	13	13	0	
297	UI	0	0	0	0	0	0	0	0	0	0	
298	UI	0	0	0	0	0	0	0	0	0	0	
299	UI	0	0	0	0	0	0	0	0	0	0	
	*											
		HEC-1 INPUT										
LINE	ID	1	2	3	4	5	6	7	8	9	10	
300	KK	CPW27COMBINE										
301	HC	3 4.345										
	*											
302	KK	W27W44ROUTE										
303	KM	Cross-section: Clean straight earth										
304	RS	1 FLOW										
305	RC	0.022	0.022	0.022	7169	0.0098	0.00					
306	RX	100.00	182.00	270.00	288.00	318.00	329.00	333.00	338.00			
307	RY	1256.0	1254.00	1250.00	1248.00	1248.00	1250.00	1254.00	1256.00			
	*											
308	KK	W43BASIN										
309	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
310	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO										
311	BA	0.209										
312	LG	0.20	0.28	3.48	0.55	61						
313	UI	0	971	508	111	0	0	0	0	0	0	
314	UI	0	0	0	0	0	0	0	0	0	0	
315	UI	0	0	0	0	0	0	0	0	0	0	
316	UI	0	0	0	0	0	0	0	0	0	0	
317	UI	0	0	0	0	0	0	0	0	0	0	
	*											
318	KK	SRW43STORAGE										
319	KM	Verrado on-line storage basin (WLB) (WoodPatel ID SR23)										
320	KO											
321	RS	1 STOR										
322	SV	6.04	20.38	53.82	120.38	216.24	325.98	455.42	606.10	645.49		
323	SQ	265.00 1377.00 2000.00										
324	SE	1272.0	1276.00	1280.00	1284.00	1288.00	1292.00	1296.00	1300.00	1304.00	1305.00	
325	ST											
	*											
326	KK	W43W44ROUTE										
327	KM	Cross-section: Side slopes and width based on aerial and topo										



328	KM	Manning's N Value: natural desert wash w/ vegetation									
329	RS	1	FLOW								
330	RC	0.035	0.035	0.035	8415	0.0125	0.00				
331	RX	100.00	145.00	180.00	210.00	220.00	245.00	270.00	295.00		
332	RY	1266.0	1264.00	1262.00	1258.00	1258.00	1262.00	1265.50	1266.00		
	*										
333	KK	W44BASIN									
334	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
335	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
336	BA	0.598									
337	LG	0.35	0.35	4.90	0.29	0					
338	UI	0	55	89	214	334	438	500	527	506	421
339	UI	332	266	206	162	127	99	82	59	48	37
340	UI	37	13	14	13	14	13	14	0	0	0
341	UI	0	0	0	0	0	0	0	0	0	0
342	UI	0	0	0	0	0	0	0	0	0	0
	*										

HEC-1 INPUT

PAGE 9

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

343	KK	CPW44COMBINE									
344	HC	3	5.153								
	*										

345	KK	W44W46ROUTE									
346	KM	Cross-section: Estimated 2' deep, side slopes and width based on aerial									
347	KM	and topo. Manning's N Value: earth w/ sparse trees and shrubs									
348	RS	1	FLOW								
349	RC	0.032	0.032	0.032	1706	0.0070	0.00				
350	RX	100.00	116.00	132.00	162.00	192.00	252.00	272.00	292.00		
351	RY	1216.0	1215.00	1214.00	1208.00	1208.10	1210.00	1211.00	1212.00		
	*										

352	KK	W45BASIN									
353	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
354	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
355	BA	1.035									
356	LG	0.35	0.33	7.30	0.11	3					
357	UI	0	136	414	824	1120	1399	860	697	573	441
358	UI	336	286	202	161	130	104	71	67	47	26
359	UI	26	26	26	26	0	0	0	0	0	0
360	UI	0	0	0	0	0	0	0	0	0	0
361	UI	0	0	0	0	0	0	0	0	0	0
	*										

362	KK	W45W46ROUTE									
363	KM	Cross-section: Based on aerial and topo									
364	KM	Manning's N Value: natural desert wash w/ vegetation									
365	RS	4	FLOW								
366	RC	0.035	0.035	0.035	9372	0.0125	0.00				
367	RX	100.00	160.00	205.00	265.00	285.00	310.00	345.00	385.00		
368	RY	1274.0	1270.00	1268.00	1262.00	1262.10	1272.00	1275.50	1276.00		
	*										

369	KK	W46BASIN									
370	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
371	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
372	BA	0.926									
373	LG	0.27	0.29	6.40	0.18	16					
374	UI	0	88	165	367	477	592	749	1082	916	727
375	UI	580	459	331	180	148	97	75	27	27	27
376	UI	28	27	0	0	0	0	0	0	0	0
377	UI	0	0	0	0	0	0	0	0	0	0
378	UI	0	0	0	0	0	0	0	0	0	0
	*										

379	KK	CPW46COMBINE									
380	HC	2	1.961								
	*										

HEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

381	KK	DW46REDIVERT									
382	KM	Master Drainage Plan for the Caterpillar Property (Basin #27)									
383	DT	RW46	0.0	0.0							

384	DI	0.0	35.0	98.0	179.0	276.0	520.0	888.0	1339.0	1859.0	2439.0
385	DQ	0.0	0.0	0.0	0.0	0.0	135.0	382.0	701.0	1080.0	1509.0
	*										

386	KK	CPW46COMBINE									
387	HC	2	7.114								
	*										

388	KK	W46W54ROUTE									
389	KM	Cross-section: side slopes, width based on aerial and topo									
390	KM	Manning's N Value: natural desert wash w/ vegetation									
391	RS	1	FLOW								
392	RC	0.035	0.035	0.035	3908	0.0397	0.00				
393	RX	100.00	112.00	124.00	140.00	160.00	190.00	220.00	240.00		
394	RY	1194.5	1194.00	1190.00	1184.00	1184.10	1186.00	1190.00	1190.50		
	*										

395	KK	W47BASIN									
396	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
397	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
398	BA	0.666									
399	LG	0.35	0.35	3.95	0.40	20					
400	UI	0	96	349	638	936	788	540	432	340	243
401	UI	202	142	111	83	66	47	43	19	19	18
402	UI	19	18	0	0	0	0	0	0	0	0
403	UI	0	0	0	0	0	0	0	0	0	0
404	UI	0	0	0	0	0	0	0	0	0	0
	*										

405	KK	W48BASIN									
406	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
407	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
408	BA	0.353									
409	LG	0.35	0.35	3.95	0.40	20					
410	UI	0	57	232	395	573	367	281	216	157	124
411	UI	85	65	48	36	28	20	10	11	11	11
412	UI	0	0	0	0	0	0	0	0	0	0
413	UI	0	0	0	0	0	0	0	0	0	0
414	UI	0	0	0	0	0	0	0	0	0	0
	*										

415	KK	CPW47COMBINE									
416	HC	2	1.019								
	*										

417	KK	W47W49ROUTE									
418	KM	Cross-section: Based on aerial and topo									
419	KM	Manning's N Value: natural desert wash w/ vegetation									
420	RS	1	FLOW								
421	RC	0.035	0.035	0.035	5077	0.0414	0.00				
422	RX	100.00	150.00	190.00	210.00	235.00	255.00	275.00	310.00		
		HEC-1 INPUT									

PAGE 11

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

423	RY	1740.0	1720.00	1710.00	1707.00	1708.00	1714.00	1730.00	1740.00		
	*										

424	KK	W50BASIN									
425	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
426	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
427	BA	1.345									
428	LG	0.35	0.35	4.25	0.42	19					
429	UI	0	122	193	458	725	898	1129	1321	842	706
430	UI	619	546	461	378	312	278	240	189	156	135
431	UI	120	93	88	60	60	59	35	24	23	24
432	UI	23	24	24	23	23	0	0	0	0	0
433	UI	0	0	0	0	0	0	0	0	0	0
	*										

434	KK	W49BASIN									
435	KM	BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN									
436	KM	WOOD/PATEL (2006) MODIFIED SLIGHTLY TO MATCH 1990 2' CI TOPO									
437	BA	0.385									
438	LG	0.35	0.35	3.95	0.40	20					
439	UI	0	67	265	450	633	398	302	232	166	129
440	UI	89	70	48	35	31	16	12	12	12	11
441	UI	0	0	0	0	0	0	0	0	0	0
442	UI	0	0	0	0	0	0	0	0	0	0
443	UI	0	0	0	0	0	0	0	0	0	0
	*										

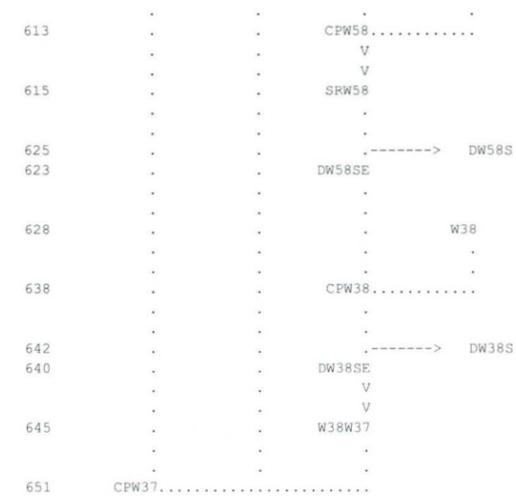
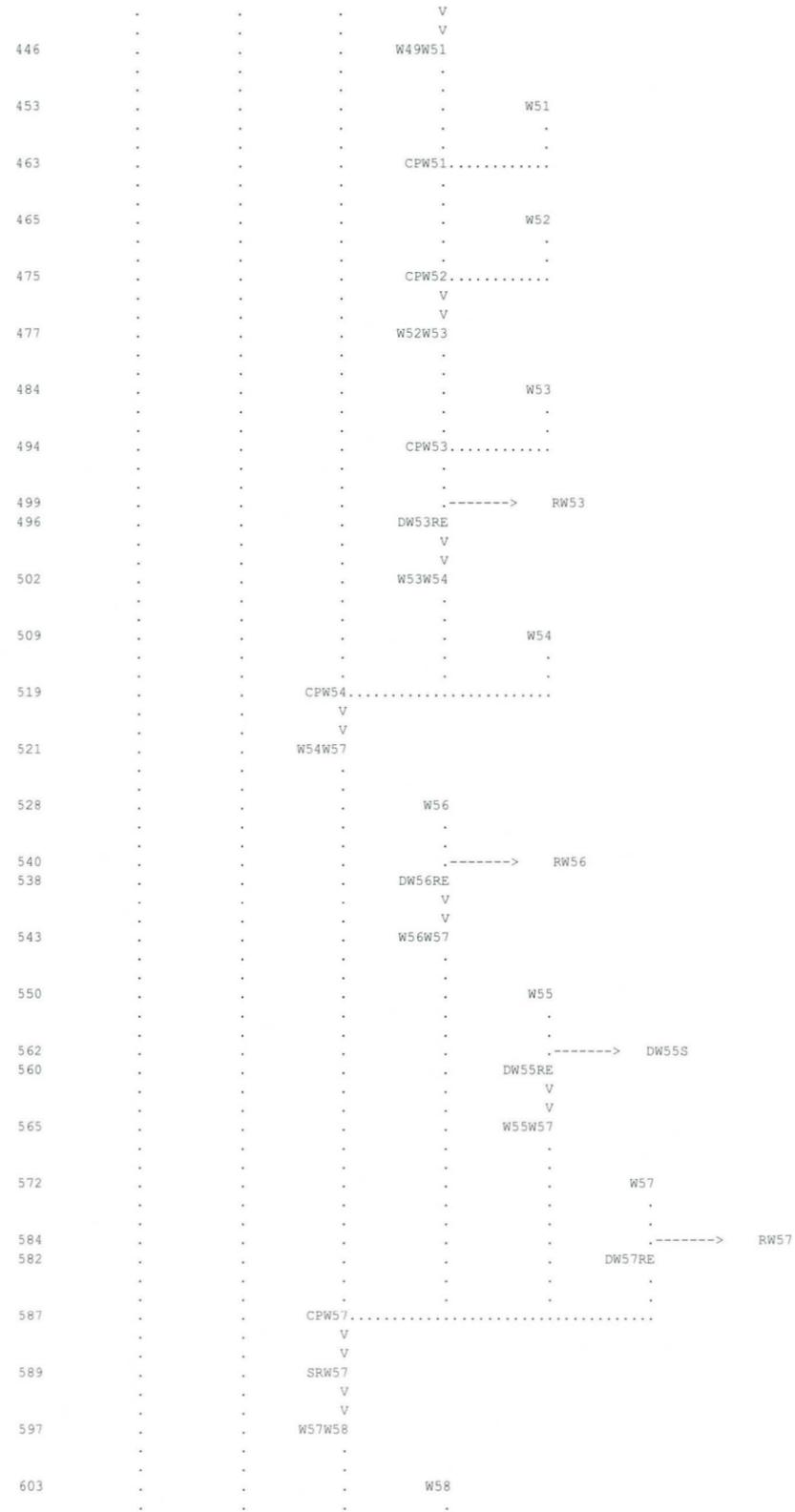




556	UI	120	92	67	51	38	29	15	15	15	15
557	UI	0	0	0	0	0	0	0	0	0	0
558	UI	0	0	0	0	0	0	0	0	0	0
559	UI	0	0	0	0	0	0	0	0	0	0
*											
560	KK DW55REDIVERT										
561	KM Verado GOB5										
562	DT	DW55S	0.0	0.0							
563	DI	0.0	55.0	101.0	537.0	1297.0	2269.0	4708.0	7684.0	11074.0	0.0
564	DQ	0.0	0.0	0.0	382.0	1080.0	1984.0	4269.0	7072.0	10310.0	0.0
*											
565	KK W55W57ROUTE										
566	KM Cross-section: Estimated 2' deep and 4:1 side slopes, width										
567	KM based on aerial / Manning's N Value: natural desert wash w/ vegetation										
568	RS	4	FLOW								
569	RC	0.035	0.035	0.035	5747	0.0096	0.00				
570	RX	100.00	110.00	120.00	136.00	156.00	172.00	192.00	212.00		
571	RY	1136.5	1136.25	1136.00	1134.00	1134.10	1136.00	1136.25	1136.50		
*											
572	KK W57BASIN										
573	KM BASIN BOUNDARY FROM VERRADO DEVELOPED CONDITIONS DRAINAGE PLAN										
574	KM WOOD/PATEL, 2006 MODIFIED SLIGHTLY TO MATCH NEW TOPO										
575	BA	1.161									
576	LG	0.27	0.29	4.65	0.37	19					
577	UI	0	138	388	695	889	1284	1641	1231	946	700
578	UI	409	239	166	101	43	43	42	0	0	0
579	UI	0	0	0	0	0	0	0	0	0	0
580	UI	0	0	0	0	0	0	0	0	0	0
581	UI	0	0	0	0	0	0	0	0	0	0
*											
HEC-1 INPUT											
PAGE 15											
LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
582	KK DW57REDIVERT										
583	KM Master Drainage Plan for the Caterpillar Property (Basin #42)										
584	DT	RW57	21.6	0.0							
585	DI	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0
586	DQ	0.0	500.0	5000.0	50000.0	0.0	0.0	0.0	0.0	0.0	0.0
*											
587	KK CPW57COMBINE										
588	HC	4	14.788								
*											
589	KK SRW57STORAGE										
590	KM Verrado SR42										
591	KO										
592	RS	1	STOR								
593	SV	24.40	29.60	35.70	42.00	48.50	55.20	62.20	69.30	76.70	
594	SQ				368.00	1040.00	1912.00	2944.00	4114.00	5410.00	
595	SE	1084.0	1090.00	1091.00	1092.00	1093.00	1094.00	1095.00	1096.00	1097.00	1098.00
596	ST										
*											
597	KK W57W58ROUTE										
598	KM Cross-section: Taken from aerial and topo										
599	RS	1	FLOW								
600	RC	0.022	0.022	0.022	1236	0.0067	0.00				
601	RX	100.00	115.50	121.80	142.00	179.30	191.30	199.60	207.80		
602	RY	1072.0	1070.00	1064.00	1062.00	1061.90	1064.00	1065.00	1066.00		
*											
603	KK W58BASIN										
604	KM BASIN BOUNDARY VARIES FROM VERRADO DEVEL.COND.PLAN WOOD/PATEL 2006										
605	KM NEW 2' CI TOPO OBTAINED 2008										
606	BA	0.131									
607	LG	0.30	0.33	4.65	0.35	18					
608	UI	0	25	101	176	208	180	117	75	48	32
609	UI	19	14	5	5	6	0	0	0	0	0
610	UI	0	0	0	0	0	0	0	0	0	0
611	UI	0	0	0	0	0	0	0	0	0	0
612	UI	0	0	0	0	0	0	0	0	0	0
*											
613	KK CPW58COMBINE										

614	HC	2	14.919								
*											
615	KK SRW58STORAGE										
616	KM Storage based on new topo section calculations										
617	KO										
618	RS	1	STOR								
619	SV	0.17	2.57	5.40	13.08	31.52	47.89	64.25	111.96	171.81	
620	SQ		784.10	2217.60	3099.20	3799.80	4122.90	4540.00	6878.80	112249.90	
621	SE	1084.0	1086.00	1088.00	1090.00	1092.00	1094.00	1095.00	1096.00	1098.00	1100.00
622	ST										
*											
HEC-1 INPUT											
PAGE 16											
LINE	ID	.....1	.....2	.....3	.....4	.....5	.....6	.....7	.....8	.....9	.....10
623	KK DW58SEDIVERT										
624	KM Divert is stage storage on 4-10x8 boxes under I-10. Diverted flow goes s										
625	DT	DW58S	0.0	0.0							
626	DI	0.0	100.0	2000.0	4100.0	4200.0	5000.0	6000.0	7000.0	8000.0	9000.0
627	DQ	0.0	100.0	2000.0	4100.0	4195.5	4606.7	4833.2	4983.7	5102.6	5203.3
*											
628	KK W38BASIN										
629	KM BASIN BOUNDARY FORMED BY MCDOWELL, I-10, JACKRABBIT										
630	KM AND TUTHILL, DETAILED I-10 TOPO AND CULVERT INFO										
631	BA	0.251									
632	LG	0.32	0.32	4.65	0.33	7					
633	UI	0	30	77	163	235	279	279	236	174	127
634	UI	93	68	51	36	27	20	14	7	7	8
635	UI	7	0	0	0	0	0	0	0	0	0
636	UI	0	0	0	0	0	0	0	0	0	0
637	UI	0	0	0	0	0	0	0	0	0	0
*											
638	KK CPW38COMBINE										
639	HC	2	15.17								
*											
640	KK DW38SEDIVERT										
641	KM Full flow capacity of culverts under I-10 is diverted flow										
642	DT	DW38S	0.0	0.0							
643	DI	0.0	100.0	200.0	300.0	400.0	467.0	500.0	800.0	1000.0	10000.0
644	DQ	0.0	100.0	200.0	300.0	400.0	467.0	467.0	467.0	467.0	467.0
*											
645	KK W38W37ROUTE										
646	KM Cross section based from 1990 topo, Manning's N Value: clean earth										
647	RS	3	FLOW								
648	RC	0.022	0.022	0.022	2849	0.0053	0.00				
649	RX	100.00	204.00	440.00	608.00	687.00	700.00	736.00	759.00		
650	RY	1083.0	1082.00	1080.00	1078.00	1078.00	1080.00	1082.00	1083.00		
*											
651	KK CPW37COMBINE										
652	ZW A=CIP B=CPW37 C=FLOW										
653	HC	3	19.291								
*											
654	ZZ										
SCHEMATIC DIAGRAM OF STREAM NETWORK											
INPUT	(V) ROUTING	(--->)	DIVERSION OR PUMP FLOW								
LINE	(.) CONNECTOR	(<---)	RETURN OF DIVERTED OR PUMPED FLOW								
NO.	WT3										
43		W21A									
55	CPW21A	.....									
58	21A28A										
65		W28A									





RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
	HYDROGRAPH AT	WT3	13.	27.33	12.	9.	3.	21.52		
	HYDROGRAPH AT	W21A	54.	12.50	7.	2.	1.	.20		
	2 COMBINED AT	CPW21A	54.	12.50	12.	9.	4.	.20		
	ROUTED TO	21A28A	32.	13.17	12.	9.	4.	.20		
	HYDROGRAPH AT	W28A	212.	12.42	25.	6.	2.	.64		
	2 COMBINED AT	CPW28A	211.	12.42	31.	15.	6.	.84		
	ROUTED TO	W28A33	155.	13.00	31.	15.	6.	.84		
	HYDROGRAPH AT	W33	293.	12.42	34.	9.	3.	.84		
	2 COMBINED AT	CPW33	293.	12.42	64.	23.	9.	1.68		
	ROUTED TO	W33W35	251.	12.75	64.	23.	9.	1.68		
	HYDROGRAPH AT	W35	96.	12.42	11.	3.	1.	.28		
	HYDROGRAPH AT	W34	120.	12.25	14.	4.	1.	.23		
	ROUTED TO	SRW34	0.	.00	0.	0.	0.	.23		
	ROUTED TO	W34W35	0.	.00	0.	0.	0.	.23		
	3 COMBINED AT	CPW35	294.	12.67	74.	25.	10.	2.19		
	ROUTED TO									





+	ROUTED TO	W53W54	1055.	12.75	238.	71.	24.	4.59
+	HYDROGRAPH AT	W54	469.	12.50	61.	18.	6.	.98
+	3 COMBINED AT	CPW54	2777.	12.67	556.	164.	55.	12.68
+	ROUTED TO	W54W57	2667.	12.75	556.	164.	55.	12.68
+	HYDROGRAPH AT	W56	230.	12.25	16.	4.	1.	.45
+	DIVERSION TO	RW56	230.	12.25	16.	4.	1.	.45
+	HYDROGRAPH AT	DW56RE	0.	.00	0.	0.	0.	.45
+	ROUTED TO	W56W57	0.	.00	0.	0.	0.	.45
+	HYDROGRAPH AT	W55	226.	12.25	27.	8.	3.	.50
+	DIVERSION TO	DW55S	109.	12.25	5.	1.	0.	.50
+	HYDROGRAPH AT	DW55RE	116.	12.25	21.	7.	2.	.50
+	ROUTED TO	W55W57	105.	12.67	21.	7.	2.	.50
+	HYDROGRAPH AT	W57	614.	12.42	74.	22.	7.	1.16
+	DIVERSION TO	RW57	571.	12.33	39.	11.	4.	1.16
+	HYDROGRAPH AT	DW57RE	567.	12.50	42.	12.	4.	1.16
+	4 COMBINED AT	CPW57	2988.	12.75	615.	182.	61.	14.79
+	ROUTED TO	SRW57	2897.	12.83	606.	165.	55.	14.79
+	ROUTED TO	W57W58	2899.	12.83	605.	165.	55.	14.79
+	HYDROGRAPH AT	W58	80.	12.25	8.	2.	1.	.13
+	2 COMBINED AT	CPW58	2907.	12.83	611.	167.	56.	14.92
+	ROUTED TO	SRW58	2803.	12.92	611.	167.	56.	14.92
+	DIVERSION TO	DW58S	2803.	12.92	611.	167.	56.	14.92
+	HYDROGRAPH AT	DW58SE	0.	.00	0.	0.	0.	14.92
+	HYDROGRAPH AT	W38	106.	12.42	12.	3.	1.	.25
+	2 COMBINED AT	CPW38	102.	12.42	12.	3.	1.	15.17
+	DIVERSION TO	DW38S	102.	12.42	12.	3.	1.	15.17
	HYDROGRAPH AT							

+		DW38SE	0.	.00	0.	0.	0.	15.17
+	ROUTED TO	W38W37	0.	.00	0.	0.	0.	15.17
+	3 COMBINED AT	CPW37	346.	12.75	139.	42.	16.	19.29

\*\*\* NORMAL END OF HEC-1 \*\*\*



**APPENDIX D – CULVERT HYDRAULIC CALCULATIONS**

**ALTERNATIVE 9B – Earthen channel Reach 9**

**Worksheet for Reach 9 - 285cfs**

Project Description

Friction Method                   Manning Formula  
 Solve For                         Normal Depth

Input Data

Roughness Coefficient             0.035  
 Channel Slope                     0.00100 ft/ft  
 Left Side Slope                   4.00 ft/ft (H:V)  
 Right Side Slope                  4.00 ft/ft (H:V)  
 Bottom Width                     20.00 ft  
 Discharge                         285.00 ft<sup>3</sup>/s

Results

Normal Depth                     3.47 ft  
 Flow Area                         117.75 ft<sup>2</sup>  
 Wetted Perimeter                 48.65 ft  
 Top Width                         47.79 ft  
 Critical Depth                    1.65 ft  
 Critical Slope                    0.01654 ft/ft  
 Velocity                         2.42 ft/s  
 Velocity Head                    0.09 ft  
 Specific Energy                  3.57 ft  
 Froude Number                   0.27

Flow Type                         Subcritical

GVF Input Data

Downstream Depth                0.00 ft  
 Length                            0.00 ft  
 Number Of Steps                 0

GVF Output Data

Upstream Depth                   0.00 ft  
 Profile Description  
 Profile Headloss                 0.00 ft  
 Downstream Velocity             Infinity ft/s  
 Upstream Velocity                Infinity ft/s  
 Normal Depth                     3.47 ft  
 Critical Depth                    1.65 ft  
 Channel Slope                    0.00100 ft/ft  
 Critical Slope                    0.01654 ft/ft

**ALTERNATIVE 9B – (1) 10'x6' CBC under emergency spillway**

BOX CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 5, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Span (ft)	10.0
Culvert Rise (ft)	6.0
FHWA Chart Number	9
FHWA Scale Number (Type of Culvert Entrance)	1
Manning's Roughness Coefficient (n-value)	0.013
Entrance Loss Coefficient of Culvert Opening	0.2
Culvert Length (ft)	1,320.0
Invert Elevation at Downstream end of Culvert (ft)	1,182.97
Invert Elevation at Upstream end of Culvert (ft)	1,185.61
Culvert Slope (ft/ft)	0.002
Starting Flow Rate (cfs)	285.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	285.0
Starting Tailwater Depth (ft)	4.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	4.0

COMPUTATION RESULTS							
Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
285.0	4.0	4.76	4.73	3.46	2.93	3.46	8.23

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281)440-3787, Fax: (281)440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.



**Alternative 9C – (1) 72-inch Pipe (pressure flow)**

PIPE CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 14, 2009

DESCRIPTION	PROGRAM INPUT DATA	VALUE
Culvert Diameter (ft)		6.0
FHWA Chart Number		2
FHWA Scale Number (Type of Culvert Entrance)		1
Manning's Roughness Coefficient (n-value)		0.01
Entrance Loss Coefficient of Culvert Opening		0.5
Culvert Length (ft)		4,800.0
Invert Elevation at Downstream end of Culvert (ft)		1,090.0
Invert Elevation at Upstream end of Culvert (ft)		1,094.8
Culvert Slope (ft/ft)		0.001
Starting Flow Rate (cfs)		285.0
Incremental Flow Rate (cfs)		0.0
Ending Flow Rate (cfs)		285.0
Starting Tailwater Depth (ft)		3.0
Incremental Tailwater Depth (ft)		0.0
Ending Tailwater Depth (ft)		3.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
285.0	3.0	7.99	14.11	6.0	4.62	4.62	12.2

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.

**Alternative 9D – (3) 60-inch Pipes**

PIPE CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 5, 2009

DESCRIPTION	PROGRAM INPUT DATA	VALUE
Culvert Diameter (ft)		5.0
FHWA Chart Number		2
FHWA Scale Number (Type of Culvert Entrance)		1
Manning's Roughness Coefficient (n-value)		0.01
Entrance Loss Coefficient of Culvert Opening		0.5
Culvert Length (ft)		4,800.0
Invert Elevation at Downstream end of Culvert (ft)		1,090.0
Invert Elevation at Upstream end of Culvert (ft)		1,094.8
Culvert Slope (ft/ft)		0.001
Starting Flow Rate (cfs)		95.0
Incremental Flow Rate (cfs)		0.0
Ending Flow Rate (cfs)		95.0
Starting Tailwater Depth (ft)		3.0
Incremental Tailwater Depth (ft)		0.0
Ending Tailwater Depth (ft)		3.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater (ft) Inlet Control	Headwater (ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
95.0	3.0	4.08	4.55	3.66	2.77	3.0	7.72

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.



**Alternative 9D – (2) 72-inch Pipes**

PIPE CULVERT ANALYSIS  
COMPUTATION OF CULVERT PERFORMANCE CURVE

December 5, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Diameter (ft)	6.0
FHWA Chart Number	2
FHWA Scale Number (Type of Culvert Entrance)	1
Manning's Roughness Coefficient (n-value)	0.01
Entrance Loss Coefficient of Culvert Opening	0.5
Culvert Length (ft)	4,800.0
Invert Elevation at Downstream end of Culvert (ft)	1,090.0
Invert Elevation at Upstream end of Culvert (ft)	1,094.8
Culvert Slope (ft/ft)	0.001
Starting Flow Rate (cfs)	143.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	143.0
Starting Tailwater Depth (ft)	3.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	3.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
143.0	3.0	4.75	5.24	4.14	3.25	3.25	9.16

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
All Rights Reserved.

**Alternative 9E – Pipe Under Emergency Spillway, (3) 60-inch Pipes**

PIPE CULVERT ANALYSIS  
COMPUTATION OF CULVERT PERFORMANCE CURVE

December 5, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Diameter (ft)	5.0
FHWA Chart Number	1
FHWA Scale Number (Type of Culvert Entrance)	2
Manning's Roughness Coefficient (n-value)	0.013
Entrance Loss Coefficient of Culvert Opening	0.5
Culvert Length (ft)	1,320.0
Invert Elevation at Downstream end of Culvert (ft)	1,182.97
Invert Elevation at Upstream end of Culvert (ft)	1,185.61
Culvert Slope (ft/ft)	0.002
Starting Flow Rate (cfs)	95.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	95.0
Starting Tailwater Depth (ft)	3.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	3.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
95.0	3.0	4.07	4.45	3.43	2.77	3.0	7.72

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
All Rights Reserved.



**Alternative 9E – Pipe Under Emergency Spillway, (2) 72-inch Pipes**

PIPE CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 5, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Diameter (ft)	6.0
FHWA Chart Number	1
FHWA Scale Number (Type of Culvert Entrance)	2
Manning's Roughness Coefficient (n-value)	0.013
Entrance Loss Coefficient of Culvert Opening	0.5
Culvert Length (ft)	1,320.0
Invert Elevation at Downstream end of Culvert (ft)	1,182.97
Invert Elevation at Upstream end of Culvert (ft)	1,185.61
Culvert Slope (ft/ft)	0.002
Starting Flow Rate (cfs)	143.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	143.0
Starting Tailwater Depth (ft)	3.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	3.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
143.0	3.0	4.74	5.16	3.89	3.25	3.25	9.16

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.

**Alternative 9F – (1) 60-inch Pipe Across Dam or Under Emergency Spillway**

PIPE CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 14, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Diameter (ft)	5.0
FHWA Chart Number	2
FHWA Scale Number (Type of Culvert Entrance)	1
Manning's Roughness Coefficient (n-value)	0.01
Entrance Loss Coefficient of Culvert Opening	0.5
Culvert Length (ft)	1,900.0
Invert Elevation at Downstream end of Culvert (ft)	1,183.0
Invert Elevation at Upstream end of Culvert (ft)	1,200.0
Culvert Slope (ft/ft)	0.0089
Starting Flow Rate (cfs)	15.0
Incremental Flow Rate (cfs)	30.0
Ending Flow Rate (cfs)	285.0
Starting Tailwater Depth (ft)	3.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	3.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
15.0	3.0	1.42	0.0	0.74	1.07	0.74	8.33
45.0	3.0	2.59	0.0	1.27	1.88	1.27	11.52
75.0	3.0	3.5	0.0	1.65	2.45	1.65	13.32
105.0	3.0	4.33	0.0	1.97	2.92	1.97	14.61
135.0	3.0	5.14	0.0	2.27	3.33	2.27	15.61
165.0	3.0	6.19	0.0	2.54	3.68	2.54	16.43
195.0	3.0	7.17	0.0	2.82	3.99	2.82	17.11
225.0	3.0	8.4	0.0	3.09	4.25	3.09	17.66
255.0	3.0	9.82	0.0	3.37	4.45	3.37	18.1
285.0	3.0	11.41	0.0	3.67	4.61	3.67	18.43

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.



**Alternative 6/7A – (2) 8'X6' CBC to receive side drainage (Q100=556cfs) from SF14**

BOX CULVERT ANALYSIS  
COMPUTATION OF CULVERT PERFORMANCE CURVE

December 11, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Span (ft)	8.0
Culvert Rise (ft)	6.0
FHWA Chart Number	9
FHWA Scale Number (Type of Culvert Entrance)	1
Manning's Roughness Coefficient (n-value)	0.013
Entrance Loss Coefficient of Culvert Opening	0.2
Culvert Length (ft)	200.0
Invert Elevation at Downstream end of Culvert (ft)	1,177.14
Invert Elevation at Upstream end of Culvert (ft)	1,178.14
Culvert Slope (ft/ft)	0.005
Starting Flow Rate (cfs)	278.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	278.0
Starting Tailwater Depth (ft)	4.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	4.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
278.0	4.0	5.43	0.0	3.0	3.35	3.0	11.58

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com

**Alternative 6/7B – (1) 12'X8' CBC for Reaches 6 and 7 with a 2-foot drop inlet**

BOX CULVERT ANALYSIS  
COMPUTATION OF CULVERT PERFORMANCE CURVE

December 11, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Span (ft)	12.0
Culvert Rise (ft)	8.0
FHWA Chart Number	9
FHWA Scale Number (Type of Culvert Entrance)	1
Manning's Roughness Coefficient (n-value)	0.013
Entrance Loss Coefficient of Culvert Opening	0.2
Culvert Length (ft)	5,360.0
Invert Elevation at Downstream end of Culvert (ft)	1,160.24
Invert Elevation at Upstream end of Culvert (ft)	1,178.14
Culvert Slope (ft/ft)	0.0033
Starting Flow Rate (cfs)	700.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	700.0
Starting Tailwater Depth (ft)	4.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	4.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
700.0	4.0	7.67	0.0	4.65	4.73	4.65	12.55

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
All Rights Reserved.



**Alternative 6/7C – (2) 8’X6’ CBC Reaches 6 and 7 with a 2-foot drop inlet**

BOX CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 12, 2009

DESCRIPTION	PROGRAM INPUT DATA	VALUE
Culvert Span (ft)		8.0
Culvert Rise (ft)		6.0
FHWA Chart Number		9
FHWA Scale Number (Type of Culvert Entrance)		1
Manning's Roughness Coefficient (n-value)		0.013
Entrance Loss Coefficient of Culvert Opening		0.2
Culvert Length (ft)		300.0
Invert Elevation at Downstream end of Culvert (ft)		1,172.91
Invert Elevation at Upstream end of Culvert (ft)		1,174.41
Culvert Slope (ft/ft)		0.005
Starting Flow Rate (cfs)		350.0
Incremental Flow Rate (cfs)		0.0
Ending Flow Rate (cfs)		350.0
Starting Tailwater Depth (ft)		4.0
Incremental Tailwater Depth (ft)		0.0
Ending Tailwater Depth (ft)		4.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
350.0	4.0	6.33	0.0	3.55	3.9	3.55	12.32

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281)440-3787, Fax: (281)440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.

**Alternative 6/7C – (2) 8’X6’ CBC at Reach 7, west of Jackrabbit Trail, with a 2.5-foot drop inlet**

BOX CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 12, 2009

DESCRIPTION	PROGRAM INPUT DATA	VALUE
Culvert Span (ft)		8.0
Culvert Rise (ft)		6.0
FHWA Chart Number		9
FHWA Scale Number (Type of Culvert Entrance)		1
Manning's Roughness Coefficient (n-value)		0.013
Entrance Loss Coefficient of Culvert Opening		0.2
Culvert Length (ft)		900.0
Invert Elevation at Downstream end of Culvert (ft)		1,160.24
Invert Elevation at Upstream end of Culvert (ft)		1,162.74
Culvert Slope (ft/ft)		0.0028
Starting Flow Rate (cfs)		400.0
Incremental Flow Rate (cfs)		0.0
Ending Flow Rate (cfs)		400.0
Starting Tailwater Depth (ft)		4.0
Incremental Tailwater Depth (ft)		0.0
Ending Tailwater Depth (ft)		4.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
400.0	4.0	6.92	6.84	4.9	4.27	4.9	10.2

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281)440-3787, Fax: (281)440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.



**Alternative 6/7D – (2) 10'X8' CBC for Reach 7 with a 2-foot drop inlet**

BOX CULVERT ANALYSIS  
 COMPUTATION OF CULVERT PERFORMANCE CURVE

December 11, 2009

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Span (ft)	10.0
Culvert Rise (ft)	6.0
FHWA Chart Number	9
FHWA Scale Number (Type of Culvert Entrance)	1
Manning's Roughness Coefficient (n-value)	0.013
Entrance Loss Coefficient of Culvert Opening	0.2
Culvert Length (ft)	2,746.0
Invert Elevation at Downstream end of Culvert (ft)	1,174.41
Invert Elevation at Upstream end of Culvert (ft)	1,178.14
Culvert Slope (ft/ft)	0.0014
Starting Flow Rate (cfs)	350.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	350.0
Starting Tailwater Depth (ft)	4.0
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	4.0

COMPUTATION RESULTS

Flow Rate (cfs)	Tailwater Depth (ft)	Headwater Inlet Control (ft)	Headwater Outlet Control (ft)	Normal Depth (ft)	Critical Depth (ft)	Depth at Outlet (ft)	Outlet Velocity (fps)
350.0	4.0	5.46	5.7	4.63	3.36	4.0	8.75

HYDROCALC Hydraulics for Windows, Version 1.2a Copyright (c) 1996  
 Dodson & Associates, Inc., 5629 FM 1960 West, Suite 314, Houston, TX 77069  
 Phone: (281) 440-3787, Fax: (281) 440-4742, Email: software@dodson-hydro.com  
 All Rights Reserved.

**Alternative 6/7E – Concrete channel Reach 7**

**Worksheet for Reach 7 Concrete Channel**

Project Description

Friction Method                      Manning Formula  
 Solve For                                Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.00100 ft/ft
Left Side Slope	2.00 ft/ft (H:V)
Right Side Slope	2.00 ft/ft (H:V)
Bottom Width	15.00 ft
Discharge	700.00 ft <sup>3</sup> /s

Results

Normal Depth	4.13 ft
Flow Area	95.94 ft <sup>2</sup>
Wetted Perimeter	33.45 ft
Top Width	31.50 ft
Critical Depth	3.47 ft
Critical Slope	0.00192 ft/ft
Velocity	7.30 ft/s
Velocity Head	0.83 ft
Specific Energy	4.95 ft
Froude Number	0.74

Flow Type                                Subcritical

GVF Input Data

Downstream Depth	0.00 ft
Length	0.00 ft
Number Of Steps	0

GVF Output Data

Upstream Depth	0.00 ft
Profile Description	
Profile Headloss	0.00 ft
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	4.13 ft
Critical Depth	3.47 ft
Channel Slope	0.00100 ft/ft
Critical Slope	0.00192 ft/ft

Bentley Systems, Inc. Haestad Methods Solution Center

Bentley FlowMaster [08.01.071.00]

12/11/2009 4:03:17 PM    27 Siemens Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Page 1 of 1



## APPENDIX E – EQUILIBRIUM SLOPE CALCULATION

### WT03 Equilibrium Slopes

Reference: The Flood Control District of Maricopa County, River Mechanics Manual for DDMSW (Draft), September 2009

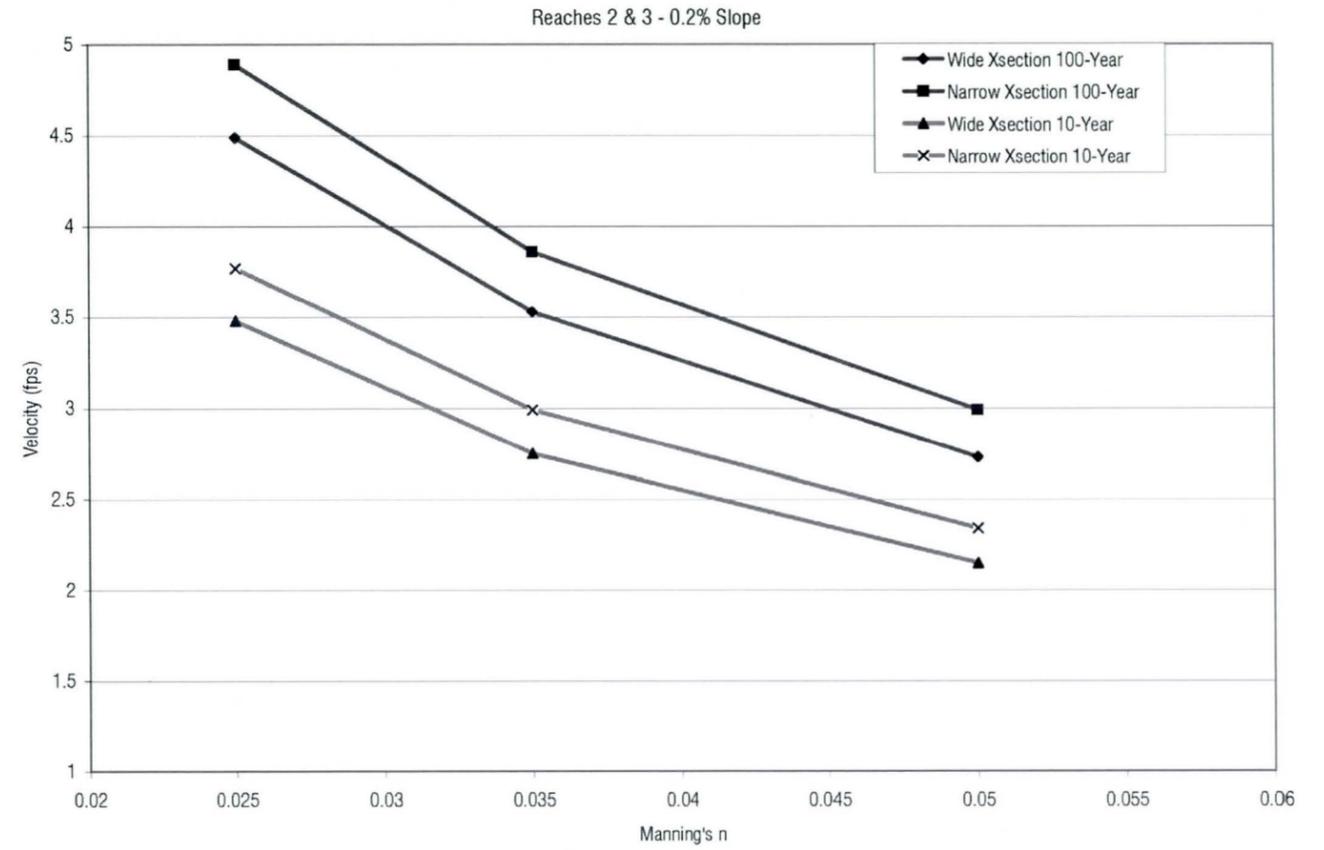
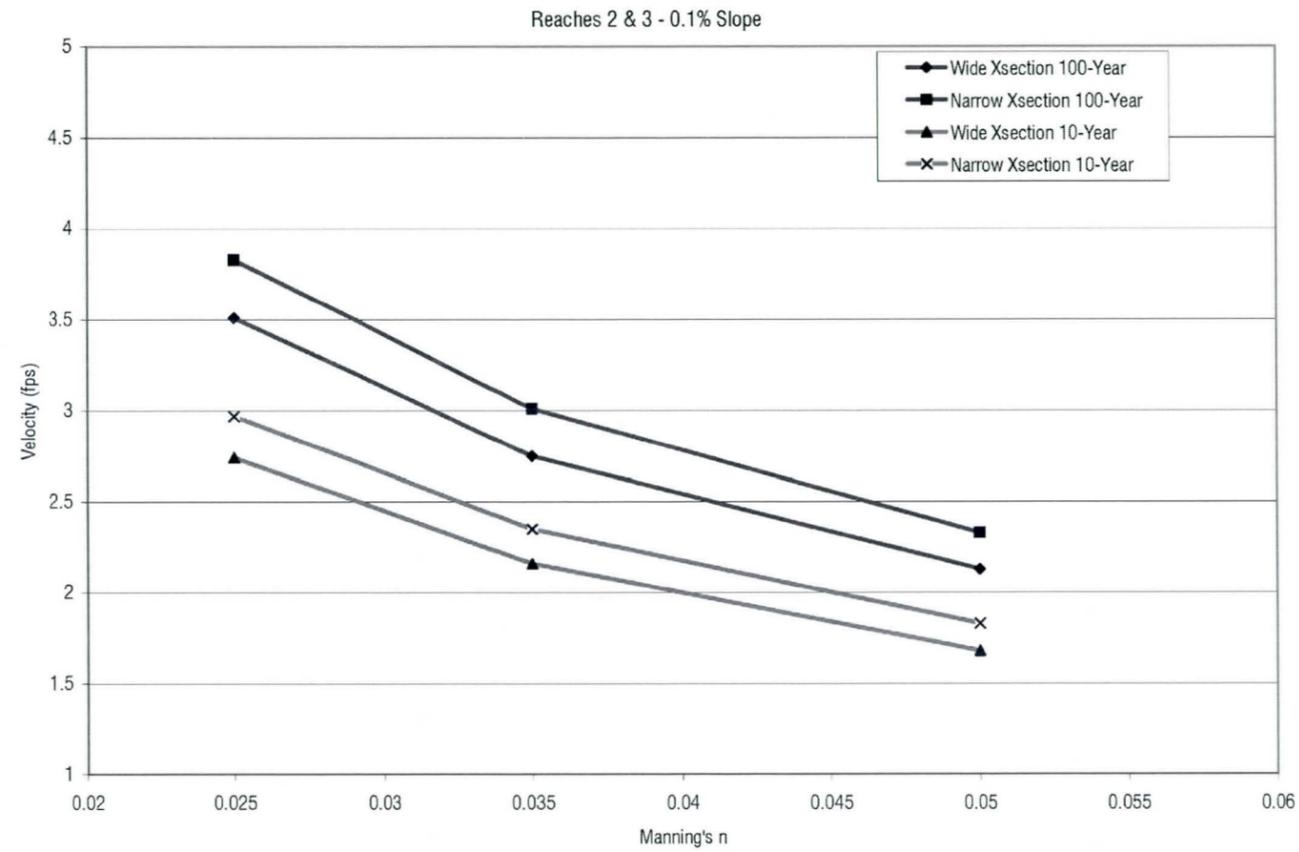
#### Clear-Water Flow

The Schoklitsch equation was used for the equilibrium slope for clear-water flow.

$$S_L = K \left( \frac{DB}{Q} \right)^{3/4}$$

where,  $S_L$  is equilibrium slope (ft/ft),  $K = 0.00174$ ,  $Q$  is 10-year event discharge (cfs),  $D = D_{50}$  (mm), and  $B$  is channel width (ft).

<b>Reach 9</b>	Trapezoidal Channel	Bottom Width = 20 ft	Side Slope= 4 :1	$n = 0.025$	
PMF	$Q = 285$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 33.1$ ft	$h = 3.3$ ft	$S_L = 0.0004$ ft/ft
<b>Reach 8</b>	Trapezoidal Channel	Bottom Width = 30 ft	Side Slope= 4 :1	$n = 0.025$	
PMF	$Q = 285$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 41$ ft	$h = 2.8$ ft	$S_L = 0.0005$ ft/ft
<b>Reach 7</b>	Trapezoidal Channel	Bottom Width = 30 ft	Side Slope= 4 :1	$n = 0.025$	
PMF	$Q = 285$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 41$ ft	$h = 2.8$ ft	$S_L = 0.0005$ ft/ft
<b>Reach 6</b>	Trapezoidal Channel	Bottom Width = 40 ft	Side Slope= 4 :1	$n = 0.025$	
Future Condition	$Q_{10} = 360$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 51.1$ ft	$h = 2.8$ ft	$S_L = 0.0005$ ft/ft
Existing Condition	$Q_{10} = 293$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 49.6$ ft	$h = 2.4$ ft	$S_L = 0.0005$ ft/ft
<b>Reach 5</b>	Trapezoidal Channel	Bottom Width = 40 ft	Side Slope= 4 :1	$n = 0.025$	
Future Condition	$Q_{10} = 360$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 51.1$ ft	$h = 2.8$ ft	$S_L = 0.0005$ ft/ft
Existing Condition	$Q_{10} = 293$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 49.6$ ft	$h = 2.4$ ft	$S_L = 0.0005$ ft/ft
<b>Reach 4</b>	Trapezoidal Channel	Bottom Width = 50 ft	Side Slope= 4 :1	$n = 0.025$	
Future Condition	$Q_{10} = 302$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 58.6$ ft	$h = 2.1$ ft	$S_L = 0.0006$ ft/ft
Existing Condition	$Q_{10} = 294$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 58.4$ ft	$h = 2.1$ ft	$S_L = 0.0006$ ft/ft
<b>Reach 3</b>	Trapezoidal Channel	Bottom Width = 30 ft	Side Slope= 4 :1	$n = 0.025$	
Future Condition	$Q_{10} = 241$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 39.8$ ft	$h = 2.5$ ft	$S_L = 0.0005$ ft/ft
Existing Condition	$Q_{10} = 286$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 41$ ft	$h = 2.8$ ft	$S_L = 0.0005$ ft/ft
<b>Reach 2</b>	Trapezoidal Channel	Bottom Width = 30 ft	Side Slope= 4 :1	$n = 0.025$	
Future Condition	$Q_{10} = 222$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 39.3$ ft	$h = 2.3$ ft	$S_L = 0.0005$ ft/ft
Existing Condition	$Q_{10} = 286$ cfs	$D_{50} = 1.2$ mm	$B = A/h = 41$ ft	$h = 2.8$ ft	$S_L = 0.0005$ ft/ft





**APPENDIX F – COST ESTIMATE**



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS  
ALTERNATIVE 6/7A AND 9A (30% DESIGN)**

1/27/2010

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
<b>GENERAL CONDITIONS</b>										
105-1	PARTNERING ALLOWANCE	LS					1	1	\$15,000.00	\$15,000
107-1	AZDPES/SWPPP PERMITS	LS					1	1	\$100,000.00	\$100,000
107-2	PUBLIC INFORMATION & NOTIFICATION ALLOWANCE	LS					1	1	\$20,000.00	\$20,000
107-3	PROJECT SIGNS ALLOWANCE	EA					1	1	\$5,000.00	\$5,000
107-4	WATER MANAGEMENT	LS					1	1	\$55,884.74	\$55,885
107-5	VANDALISM ALLOWANCE	LS					1	1	\$25,000.00	\$25,000
							\$220,885			
<b>EARTHWORK</b>										
201-1	CLEARING AND GRUBBING	LS					1	1	\$288,562.50	\$288,563
202-1	MOBILIZATION	LS					1	1	\$110,034.84	\$110,035
211-1	FILL CONSTRUCTION (DITCHES, FARM ROAD AND OVERBANK)	CY	1,864	150	625	57,639		109,234	\$7.00	\$764,638
211-2	FINAL AESTHETIC GRADING	LS					1	1	\$227,496.40	\$227,496
215-1	CHANNEL EXCAVATION	CY	46,736	63,919	92,535	68,038		470,589	\$3.00	\$1,411,767
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	20	0	151	0		459	\$45.00	\$20,655
220-2	PLAIN RIPRAP (D <sub>50</sub> = 12")	CY	324	196	1,311	20		3,038	\$70.00	\$212,660
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	562	0	748			6,017	\$75.00	\$451,275
230-1	GRAVEL MULCH	SY	37,711	27,513	44,512	31,284		251,884	\$4.00	\$1,007,535
230-2	HYDROSEEDING	AC	9	7.29	10.97	11.23		69	\$6,000.00	\$412,630
			\$426,044	\$360,338	\$680,485	\$801,502	\$626,094			
<b>STREETS &amp; RELATED WORK</b>										
310-1	ABC MAINTENANCE ROAD & RAMP (4-INCH)	SY	7,504	3,077	8,098	6,535		49,082	\$4.63	\$227,252
336-1	TEMPORARY PAVEMENT REPLACEMENT (2" A.C.)	SY	0	0	0	0		996	\$20.00	\$19,924
336-2	PERMANENT PAVEMENT REPLACEMENT (3" A.C.)	SY	274	322	0	0		682	\$30.00	\$20,467
340-1	CONCRETE VERTICAL CURB & GUTTER, MAG STD DET 220, TYPE 'A'	LF	0	36	0	0		36	\$19.00	\$684
340-2	CONCRETE ROLL CURB & GUTTER, MAG STD DET 220, TYPE 'C'	LF	0	80	0	0		80	\$17.00	\$1,360
340-3	CONCRETE SIDEWALK, MAG STD DET 230	SF	0	1,004	0	0		1,004	\$15.00	\$15,060
340-4	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-1	SF	0	144	0	0		144	\$15.00	\$2,160
340-5	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-2	SF	0	576	0	0		576	\$15.00	\$8,640
350-1	REMOVE EXISTING WIRE FENCE	LF	0	0	0	175		3,832	\$1.00	\$3,832
350-2	REMOVE PAVEMENT	SY	0	0	0	0		1,739	\$7.00	\$12,171
350-3	BURIED TRASH REMOVAL ALLOWANCE	LS					1	1	\$50,000.00	\$50,000
350-4	REMOVE CONCRETE CURB & GUTTER	LF	0	236	0	0		236	\$6.00	\$1,416
350-5	REMOVE GROUTED RIPRAP	SY	0	0	0	0		4,597	\$18.92	\$86,952
350-6	REMOVE EXISTING BLOCK WALL, RETAINIGN WALL	LF	0	3,711	0	0		4,057	\$8.00	\$32,456
350-7	REMOVE EXISTING CONCRETE LINED CHANNEL	SY	0	0	0	0		2,920	\$18.92	\$55,232
350-8	REMOVE EXISTING CONCRETE SIDEWALK	SY	0	112	0	0		112	\$18.92	\$2,110
			\$42,977	\$85,014	\$37,495	\$30,432	\$50,000			
<b>RIGHT-OF-WAY AND TRAFFIC CONTROL</b>										
401-1	MISCELLANEOUS TRAFFIC CONTROL	LS					1	1	\$100,000.00	\$100,000
412-1	4 STRAND SMOOTH WIRE FENCE	LF	3,488	4,460	4,714	3,471		35,902	\$5.00	\$179,510
421-1	INSTALL GATE	EA	0	0	0	1		1	\$1,000.00	\$1,000
			\$17,440	\$22,300	\$23,570	\$18,355	\$100,000			
<b>STRUCTURES</b>										
505-1	CONCRETE CHANNEL LINING (7" THICK)	SF	0	0	0	0		17,476	\$10.80	\$188,784
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	826	85	0	0		911	\$1,121.25	\$1,021,459
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	58	393	0		721	\$1,604.20	\$1,156,628
505-4	CONCRETE BOX CULVERT TYPE E (1 BARREL 10' x 6'), ADOT B-02.20	LF	0	0	0	1,320		1,320	\$1,475.50	\$1,947,660
505-5	CONCRETE BOX CULVERT INLET HEADWALL, ADOT B-04.30	EA	1	2	1	1		10	\$8,801.00	\$88,010



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS  
ALTERNATIVE 6/7A AND 9A (30% DESIGN)**

1/27/2010

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	1	2	2	0		10	\$14,768.00	\$147,680
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000
505-19	WASTEWAY STRUCTURE	CY	0	0	0	202		202	\$500.00	\$101,000
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	3		3	\$50,000.00	\$150,000
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					1	1	\$2,225,826.96	\$2,225,827
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850
			\$1,167,497	\$316,393	\$900,308	\$2,219,311	\$2,231,383			
	<b>SUBTOTAL CONSTRUCTION ITEMS</b>		\$1,653,958	\$784,045	\$1,641,857	\$3,069,600	\$3,228,361			\$14,434,827
	Relocation and/or Removal of Existing Utilities		\$82,698	\$39,202	\$82,093	\$153,480	\$161,418		5%	\$721,741
	Engineering Contingencies for Unknown Items		\$82,698	\$39,202	\$82,093	\$153,480	\$161,418		5%	\$721,741
	<b>TOTAL CONSTRUCTION COST</b>		\$1,819,353	\$862,450	\$1,806,043	\$3,376,560	\$3,551,197			\$15,878,310
	Landscaping as Aesthetic Treatment		\$155,829	\$113,690	\$183,934	\$129,275	\$0	52	\$20,000	\$1,040,842
	Non-Landscaping Aesthetic Treatment		\$72,774	\$34,498	\$72,242	\$135,062	\$142,048		4%	\$635,132
	<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>		\$2,047,957	\$1,010,637	\$2,062,218	\$3,640,897	\$3,693,245			\$17,554,284
	Engineering and Landscape Design		\$204,796	\$101,064	\$206,222	\$364,090	\$369,324		10%	\$1,755,428
	Construction Administration		\$122,877	\$60,638	\$123,733	\$218,454	\$221,595		6%	\$1,053,257
	<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>		\$2,375,630	\$1,172,339	\$2,392,173	\$4,223,440	\$4,284,164			\$20,362,969
	Required FCDMC Right-of-Way Acquisition - Undeveloped Property	AC	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
	Required FCDMC Right-of-Way Acquisition - Platted Property	AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
	<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		\$1,537,440	\$0	\$1,999,107	\$0	\$0	35.70		\$6,101,742
	<b>TOTAL PROJECT COST</b>		\$3,913,070	\$1,172,339	\$4,391,280	\$4,223,440	\$4,284,164			\$26,464,711



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS  
 ALTERNATIVE 6/7B AND 9B (BASELINE)**

1/27/2010

FCD 2009C012  
 PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
 HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
<b>GENERAL CONDITIONS</b>										
105-1	PARTNERING ALLOWANCE	LS					1	1	\$15,000.00	\$15,000
107-1	AZDPES/SWPPP PERMITS	LS					1	1	\$100,000.00	\$100,000
107-2	PUBLIC INFORMATION & NOTIFICATION ALLOWANCE	LS					1	1	\$20,000.00	\$20,000
107-3	PROJECT SIGNS ALLOWANCE	EA					1	1	\$5,000.00	\$5,000
107-4	WATER MANAGEMENT	LS					1	1	\$55,884.74	\$55,885
107-5	VANDALISM ALLOWANCE	LS					1	1	\$25,000.00	\$25,000
							\$220,885			
<b>EARTHWORK</b>										
201-1	CLEARING AND GRUBBING	LS					1	1	\$288,562.50	\$288,563
202-1	MOBILIZATION	LS					1	1	\$110,034.84	\$110,035
211-1	FILL CONSTRUCTION (DITCHES, FARM ROAD AND OVERBANK)	CY	1,864	150	625	57,639		109,234	\$7.00	\$764,638
211-2	FINAL AESTHETIC GRADING	LS					1	1	\$227,496.40	\$227,496
215-1	CHANNEL EXCAVATION	CY	46,736	63,919	92,535	68,038		470,589	\$3.00	\$1,411,767
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	20	0	151	0		459	\$45.00	\$20,655
220-2	PLAIN RIPRAP (D <sub>50</sub> = 12")	CY	324	196	1,311	20		3,038	\$70.00	\$212,660
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	562	0	748			6,017	\$75.00	\$451,275
230-1	GRAVEL MULCH	SY	37,711	27,513	44,512	31,284		251,884	\$4.00	\$1,007,535
230-2	HYDROSEEDING	AC	9	7.29	10.97	11.23		69	\$6,000.00	\$412,630
			\$426,044	\$360,338	\$680,485	\$801,502	\$626,094			
<b>STREETS &amp; RELATED WORK</b>										
310-1	ABC MAINTENANCE ROAD & RAMP (4-INCH)	SY	7,504	3,077	8,098	6,535		49,082	\$4.63	\$227,252
336-1	TEMPORARY PAVEMENT REPLACEMENT (2" A.C.)	SY	0	0	0	0		996	\$20.00	\$19,924
336-2	PERMANENT PAVEMENT REPLACEMENT (3" A.C.)	SY	274	322	0	0		682	\$30.00	\$20,467
340-1	CONCRETE VERTICAL CURB & GUTTER, MAG STD DET 220, TYPE 'A'	LF	0	36	0	0		36	\$19.00	\$684
340-2	CONCRETE ROLL CURB & GUTTER, MAG STD DET 220, TYPE 'C'	LF	0	80	0	0		80	\$17.00	\$1,360
340-3	CONCRETE SIDEWALK, MAG STD DET 230	SF	0	1,004	0	0		1,004	\$15.00	\$15,060
340-4	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-1	SF	0	144	0	0		144	\$15.00	\$2,160
340-5	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-2	SF	0	576	0	0		576	\$15.00	\$8,640
350-1	REMOVE EXISTING WIRE FENCE	LF	0	0	0	175		3,832	\$1.00	\$3,832
350-2	REMOVE PAVEMENT	SY	0	0	0	0		1,739	\$7.00	\$12,171
350-3	BURIED TRASH REMOVAL ALLOWANCE	LS					1	1	\$50,000.00	\$50,000
350-4	REMOVE CONCRETE CURB & GUTTER	LF	0	236	0	0		236	\$6.00	\$1,416
350-5	REMOVE GROUTED RIPRAP	SY	0	0	0	0		4,597	\$18.92	\$86,952
350-6	REMOVE EXISTING BLOCK WALL, RETAINIGN WALL	LF	0	3,711	0	0		4,057	\$8.00	\$32,456
350-7	REMOVE EXISTING CONCRETE LINED CHANNEL	SY	0	0	0	0		2,920	\$18.92	\$55,232
350-8	REMOVE EXISTING CONCRETE SIDEWALK	SY	0	112	0	0		112	\$18.92	\$2,110
			\$42,977	\$85,014	\$37,495	\$30,432	\$50,000			
<b>RIGHT-OF-WAY AND TRAFFIC CONTROL</b>										
401-1	MISCELLANEOUS TRAFFIC CONTROL	LS					1	1	\$100,000.00	\$100,000
412-1	4 STRAND SMOOTH WIRE FENCE	LF	3,488	4,460	4,714	3,471		35,902	\$5.00	\$179,510
421-1	INSTALL GATE	EA	0	0	0	1		1	\$1,000.00	\$1,000
			\$17,440	\$22,300	\$23,570	\$18,355	\$100,000			
<b>STRUCTURES</b>										
505-1	CONCRETE CHANNEL LINING (7" THICK)	SF	0	0	0	0		17,476	\$10.80	\$188,784
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	1,026	85	0	0		1,111	\$1,121.25	\$1,245,709
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	58	393	0		721	\$1,604.20	\$1,156,628
505-4	CONCRETE BOX CULVERT TYPE E (1 BARREL 10' x 6'), ADOT B-02.20	LF	0	0	0	1,320		1,320	\$737.75	\$973,830
505-5	CONCRETE BOX CULVERT INLET HEADWALL, ADOT B-04.30	EA	2	2	1	1		11	\$8,801.00	\$96,811



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS  
ALTERNATIVE 6/7B AND 9B (BASELINE)**

1/27/2010

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY											
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT	
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	2	2	2	0		11	\$14,768.00	\$162,448	
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500	
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000	
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000	
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556	
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500	
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000	
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500	
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500	
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000	
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500	
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000	
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000	
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0	
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500	
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0	
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010	
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0	
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000	
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000	
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850	
			\$1,415,316	\$316,393	\$900,308	\$994,481	\$5,556				
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			<b>\$1,901,777</b>	<b>\$784,045</b>	<b>\$1,641,857</b>	<b>\$1,844,770</b>	<b>\$1,002,534</b>			<b>\$11,231,989</b>	
Relocation and/or Removal of Existing Utilities			\$95,089	\$39,202	\$82,093	\$92,238	\$50,127		5%	\$561,599	
Engineering Contingencies for Unknown Items			\$95,089	\$39,202	\$82,093	\$92,238	\$50,127		5%	\$561,599	
<b>TOTAL CONSTRUCTION COST</b>			<b>\$2,091,954</b>	<b>\$862,450</b>	<b>\$1,806,043</b>	<b>\$2,029,247</b>	<b>\$1,102,787</b>			<b>\$12,355,188</b>	
Landscaping as Aesthetic Treatment			\$155,829	\$113,690	\$183,934	\$129,275	\$0	52	\$20,000	\$1,040,842	
Non-Landscaping Aesthetic Treatment			\$83,678	\$34,498	\$72,242	\$81,170	\$44,111		4%	\$494,208	
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			<b>\$2,331,462</b>	<b>\$1,010,637</b>	<b>\$2,062,218</b>	<b>\$2,239,691</b>	<b>\$1,146,899</b>			<b>\$13,890,237</b>	
Engineering and Landscape Design			\$233,146	\$101,064	\$206,222	\$223,969	\$114,690		10%	\$1,389,024	
Construction Administration			\$139,888	\$60,638	\$123,733	\$134,381	\$68,814		6%	\$833,414	
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			<b>\$2,704,496</b>	<b>\$1,172,339</b>	<b>\$2,392,173</b>	<b>\$2,598,042</b>	<b>\$1,330,403</b>			<b>\$16,112,675</b>	
Required FCDMC Right-of-Way Acquisition - Undeveloped Property			AC	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property			AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>			<b>AC</b>	<b>10.08</b>	<b>0.00</b>	<b>13.11</b>	<b>0.00</b>	<b>0.00</b>	<b>35.70</b>		<b>\$6,101,742</b>
<b>TOTAL PROJECT COST</b>			<b>\$4,241,936</b>	<b>\$1,172,339</b>	<b>\$4,391,280</b>	<b>\$2,598,042</b>	<b>\$1,330,403</b>			<b>\$22,214,417</b>	

Handwritten calculations:  
 2.598  
 - 1.974 (10x6RCB)  
 -----  
 0.624  
 + 0.370  
 -----  
 1.094  
 1320 x 2 x 140



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**  
**ALTERNATIVE 6/7C**

1/27/2010

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY											
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT	
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	1	0	1	0		7	\$14,768.00	\$103,376	
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500	
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000	
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000	
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556	
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500	
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000	
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500	
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500	
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000	
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500	
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000	
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000	
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0	
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500	
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0	
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010	
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0	
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000	
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000	
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850	
			\$3,019,802	\$2,643,914	\$885,540	\$994,481	\$5,556				
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			<b>\$3,093,266</b>	<b>\$2,752,278</b>	<b>\$1,627,089</b>	<b>\$1,844,770</b>	<b>\$1,002,534</b>			<b>\$14,376,943</b>	
Relocation and/or Removal of Existing Utilities			\$154,663	\$137,614	\$81,354	\$92,238	\$50,127		5%	\$718,847	
Engineering Contingencies for Unknown Items			\$154,663	\$137,614	\$81,354	\$92,238	\$50,127		5%	\$718,847	
<b>TOTAL CONSTRUCTION COST</b>			<b>\$3,402,593</b>	<b>\$3,027,505</b>	<b>\$1,789,798</b>	<b>\$2,029,247</b>	<b>\$1,102,787</b>			<b>\$15,814,637</b>	
Landscaping as Aesthetic Treatment			\$0	\$0	\$183,934	\$129,275	\$0	39	\$20,000	\$771,323	
Non-Landscaping Aesthetic Treatment			\$136,104	\$121,100	\$71,592	\$81,170	\$44,111		4%	\$632,585	
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			<b>\$3,538,697</b>	<b>\$3,148,606</b>	<b>\$2,045,324</b>	<b>\$2,239,691</b>	<b>\$1,146,899</b>			<b>\$17,218,546</b>	
Engineering and Landscape Design			\$353,870	\$314,861	\$204,532	\$223,969	\$114,690		10%	\$1,721,855	
Construction Administration			\$212,322	\$188,916	\$122,719	\$134,381	\$68,814		6%	\$1,033,113	
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			<b>\$4,104,888</b>	<b>\$3,652,382</b>	<b>\$2,372,576</b>	<b>\$2,598,042</b>	<b>\$1,330,403</b>			<b>\$19,973,513</b>	
Required FCDMC Right-of-Way Acquisition - Undeveloped Property			AC	0.00	0.00	13.11	0.00	0.00	13.11	\$152,500.00	\$1,999,107
Required FCDMC Right-of-Way Acquisition - Platted Property			AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>			<b>AC</b>	<b>0.00</b>	<b>0.00</b>	<b>13.11</b>	<b>0.00</b>	<b>0.00</b>	<b>25.62</b>		<b>\$4,564,302</b>
<b>TOTAL PROJECT COST</b>			<b>\$4,104,888</b>	<b>\$3,652,382</b>	<b>\$4,371,682</b>	<b>\$2,598,042</b>	<b>\$1,330,403</b>			<b>\$24,537,815</b>	



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 6/7D**

FCD 2009C012

PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.

HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
<b>GENERAL CONDITIONS</b>										
105-1	PARTNERING ALLOWANCE	LS					1	1	\$15,000.00	\$15,000
107-1	AZDPES/SWPPP PERMITS	LS					1	1	\$100,000.00	\$100,000
107-2	PUBLIC INFORMATION & NOTIFICATION ALLOWANCE	LS					1	1	\$20,000.00	\$20,000
107-3	PROJECT SIGNS ALLOWANCE	EA					1	1	\$5,000.00	\$5,000
107-4	WATER MANAGEMENT	LS					1	1	\$55,884.74	\$55,885
107-5	VANDALISM ALLOWANCE	LS					1	1	\$25,000.00	\$25,000
							\$220,885			
<b>EARTHWORK</b>										
201-1	CLEARING AND GRUBBING	LS					1	1	\$288,562.50	\$288,563
202-1	MOBILIZATION	LS					1	1	\$110,034.84	\$110,035
211-1	FILL CONSTRUCTION (DITCHES, FARM ROAD AND OVERBANK)	CY	1,864	150	625	57,639		109,234	\$7.00	\$764,638
211-2	FINAL AESTHETIC GRADING	LS					1	1	\$227,496.40	\$227,496
215-1	CHANNEL EXCAVATION	CY	32,715	63,919	92,535	68,038		456,568	\$3.00	\$1,369,705
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	20	0	151	0		459	\$45.00	\$20,655
220-2	PLAIN RIPRAP (D <sub>50</sub> = 12")	CY	324	196	1,311	20		3,038	\$70.00	\$212,660
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	562	0	748			6,017	\$75.00	\$451,275
230-1	GRAVEL MULCH	SY	26,397	27,513	44,512	31,284		240,570	\$4.00	\$962,282
230-2	HYDROSEEDING	AC	7	7.29	10.97	11.23		66	\$6,000.00	\$395,765
			\$321,864	\$360,338	\$680,485	\$801,502	\$626,094			
<b>STREETS &amp; RELATED WORK</b>										
310-1	ABC MAINTENANCE ROAD & RAMP (4-INCH)	SY	7,504	3,077	8,098	6,535		49,082	\$4.63	\$227,252
336-1	TEMPORARY PAVEMENT REPLACEMENT (2" A.C.)	SY	0	0	0	0		996	\$20.00	\$19,924
336-2	PERMANENT PAVEMENT REPLACEMENT (3" A.C.)	SY	274	322	0	0		682	\$30.00	\$20,467
340-1	CONCRETE VERTICAL CURB & GUTTER, MAG STD DET 220, TYPE 'A'	LF	0	36	0	0		36	\$19.00	\$684
340-2	CONCRETE ROLL CURB & GUTTER, MAG STD DET 220, TYPE 'C'	LF	0	80	0	0		80	\$17.00	\$1,360
340-3	CONCRETE SIDEWALK, MAG STD DET 230	SF	0	1,004	0	0		1,004	\$15.00	\$15,060
340-4	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-1	SF	0	144	0	0		144	\$15.00	\$2,160
340-5	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-2	SF	0	576	0	0		576	\$15.00	\$8,640
350-1	REMOVE EXISTING WIRE FENCE	LF	0	0	0	175		3,832	\$1.00	\$3,832
350-2	REMOVE PAVEMENT	SY	0	0	0	0		1,739	\$7.00	\$12,171
350-3	BURIED TRASH REMOVAL ALLOWANCE	LS					1	1	\$50,000.00	\$50,000
350-4	REMOVE CONCRETE CURB & GUTTER	LF	0	236	0	0		236	\$6.00	\$1,416
350-5	REMOVE GROUTED RIPRAP	SY	0	0	0	0		4,597	\$18.92	\$86,952
350-6	REMOVE EXISTING BLOCK WALL, RETAINIGN WALL	LF	0	3,711	0	0		4,057	\$8.00	\$32,456
350-7	REMOVE EXISTING CONCRETE LINED CHANNEL	SY	0	0	0	0		2,920	\$18.92	\$55,232
350-8	REMOVE EXISTING CONCRETE SIDEWALK	SY	0	112	0	0		112	\$18.92	\$2,110
			\$42,977	\$85,014	\$37,495	\$30,432	\$50,000			
<b>RIGHT-OF-WAY AND TRAFFIC CONTROL</b>										
401-1	MISCELLANEOUS TRAFFIC CONTROL	LS					1	1	\$100,000.00	\$100,000
412-1	4 STRAND SMOOTH WIRE FENCE	LF	3,488	4,460	4,714	3,471		35,902	\$5.00	\$179,510
421-1	INSTALL GATE	EA	0	0	0	1		1	\$1,000.00	\$1,000
			\$17,440	\$22,300	\$23,570	\$18,355	\$100,000			
<b>STRUCTURES</b>										
505-1	CONCRETE CHANNEL LINING (7" THICK)	SF	0	0	0	0		17,476	\$10.80	\$188,784
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	1,200	85	0	0		1,285	\$1,121.25	\$1,440,806
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	58	393	0		721	\$1,604.20	\$1,156,628
505-4	CONCRETE BOX CULVERT TYPE E (1 BARREL 10' x 6'), ADOT B-02.20	LF	0	0	0	1,320		1,320	\$737.75	\$973,830
505-5	CONCRETE BOX CULVERT INLET HEADWALL, ADOT B-04.30	EA	1	2	1	1		10	\$8,801.00	\$88,010



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 6/7D**

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	1	2	1	0		9	\$14,768.00	\$132,912
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850
			\$1,586,844	\$316,393	\$885,540	\$994,481	\$5,556			
	<b>SUBTOTAL CONSTRUCTION ITEMS</b>		\$1,969,125	\$784,045	\$1,627,089	\$1,844,770	\$1,002,534			\$11,284,570
	Relocation and/or Removal of Existing Utilities		\$98,456	\$39,202	\$81,354	\$92,238	\$50,127		5%	\$564,228
	Engineering Contingencies for Unknown Items		\$98,456	\$39,202	\$81,354	\$92,238	\$50,127		5%	\$564,228
	<b>TOTAL CONSTRUCTION COST</b>		\$2,166,038	\$862,450	\$1,789,798	\$2,029,247	\$1,102,787			\$12,413,027
	Landscaping as Aesthetic Treatment		\$109,080	\$113,690	\$183,934	\$129,275	\$0	50	\$20,000	\$994,093
	Non-Landscaping Aesthetic Treatment		\$86,642	\$34,498	\$71,592	\$81,170	\$44,111		4%	\$496,521
	<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>		\$2,361,760	\$1,010,637	\$2,045,324	\$2,239,691	\$1,146,899			\$13,903,641
	Engineering and Landscape Design		\$236,176	\$101,064	\$204,532	\$223,969	\$114,690		10%	\$1,390,364
	Construction Administration		\$141,706	\$60,638	\$122,719	\$134,381	\$68,814		6%	\$834,218
	<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>		\$2,739,641	\$1,172,339	\$2,372,576	\$2,598,042	\$1,330,403			\$16,128,223
	Required FCDMC Right-of-Way Acquisition - Undeveloped Property	AC	5.72	0.00	13.11	0.00	0.00	18.83	\$152,500.00	\$2,871,407
	Required FCDMC Right-of-Way Acquisition - Platted Property	AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
	<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		\$872,300	\$0	\$1,999,107	\$0	\$0	31.34		\$5,436,602
	<b>TOTAL PROJECT COST</b>		\$3,611,941	\$1,172,339	\$4,371,682	\$2,598,042	\$1,330,403			\$21,564,825



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 2010 LAND COST ESTIMATES**

1/29/2010

**ALTERNATIVE 6/7E**

FCD 2009C012

PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.

HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
<b>GENERAL CONDITIONS</b>										
105-1	PARTNERING ALLOWANCE	LS					1	1	\$15,000.00	\$15,000
107-1	AZDPES/SWPPP PERMITS	LS					1	1	\$100,000.00	\$100,000
107-2	PUBLIC INFORMATION & NOTIFICATION ALLOWANCE	LS					1	1	\$20,000.00	\$20,000
107-3	PROJECT SIGNS ALLOWANCE	EA					1	1	\$5,000.00	\$5,000
107-4	WATER MANAGEMENT	LS					1	1	\$55,884.74	\$55,885
107-5	VANDALISM ALLOWANCE	LS					1	1	\$25,000.00	\$25,000
							\$220,885			
<b>EARTHWORK</b>										
201-1	CLEARING AND GRUBBING	LS					1	1	\$288,562.50	\$288,563
202-1	MOBILIZATION	LS					1	1	\$110,034.84	\$110,035
211-1	FILL CONSTRUCTION (DITCHES, FARM ROAD AND OVERBANK)	CY	1,864	150	625	57,639		109,234	\$7.00	\$764,638
211-2	FINAL AESTHETIC GRADING	LS					1	1	\$227,496.40	\$227,496
215-1	CHANNEL EXCAVATION	CY	46,736	0	92,535	68,038		406,670	\$3.00	\$1,220,010
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	20	0	151	0		459	\$45.00	\$20,655
220-2	PLAIN RIPRAP (D <sub>50</sub> = 12")	CY	324	196	1,311	20		3,038	\$70.00	\$212,660
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	562	0	748			6,017	\$75.00	\$451,275
230-1	GRAVEL MULCH	SY	37,711	0	44,512	31,284		224,371	\$4.00	\$897,483
230-2	HYDROSEEDING	AC	9	0	10.97	11.23		61	\$6,000.00	\$368,870
			\$426,044	\$14,770	\$680,485	\$801,502	\$626,094			
<b>STREETS &amp; RELATED WORK</b>										
310-1	ABC MAINTENANCE ROAD & RAMP (4-INCH)	SY	7,504	3,077	8,098	6,535		49,082	\$4.63	\$227,252
336-1	TEMPORARY PAVEMENT REPLACEMENT (2" A.C.)	SY	0	0	0	0		996	\$20.00	\$19,924
336-2	PERMANENT PAVEMENT REPLACEMENT (3" A.C.)	SY	274	322	0	0		682	\$30.00	\$20,467
340-1	CONCRETE VERTICAL CURB & GUTTER, MAG STD DET 220, TYPE 'A'	LF	0	36	0	0		36	\$19.00	\$684
340-2	CONCRETE ROLL CURB & GUTTER, MAG STD DET 220, TYPE 'C'	LF	0	80	0	0		80	\$17.00	\$1,360
340-3	CONCRETE SIDEWALK, MAG STD DET 230	SF	0	1,004	0	0		1,004	\$15.00	\$15,060
340-4	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-1	SF	0	144	0	0		144	\$15.00	\$2,160
340-5	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-2	SF	0	576	0	0		576	\$15.00	\$8,640
350-1	REMOVE EXISTING WIRE FENCE	LF	0	0	0	175		3,832	\$1.00	\$3,832
350-2	REMOVE PAVEMENT	SY	0	0	0	0		1,739	\$7.00	\$12,171
350-3	BURIED TRASH REMOVAL ALLOWANCE	LS					1	1	\$50,000.00	\$50,000
350-4	REMOVE CONCRETE CURB & GUTTER	LF	0	236	0	0		236	\$6.00	\$1,416
350-5	REMOVE GROUTED RIPRAP	SY	0	0	0	0		4,597	\$18.92	\$86,952
350-6	REMOVE EXISTING BLOCK WALL, RETAINIGN WALL	LF	0	3,711	0	0		4,057	\$8.00	\$32,456
350-7	REMOVE EXISTING CONCRETE LINED CHANNEL	SY	0	0	0	0		2,920	\$18.92	\$55,232
350-8	REMOVE EXISTING CONCRETE SIDEWALK	SY	0	112	0	0		112	\$18.92	\$2,110
			\$42,977	\$85,014	\$37,495	\$30,432	\$50,000			
<b>RIGHT-OF-WAY AND TRAFFIC CONTROL</b>										
401-1	MISCELLANEOUS TRAFFIC CONTROL	LS					1	1	\$100,000.00	\$100,000
412-1	4 STRAND SMOOTH WIRE FENCE	LF	3,488	4,460	4,714	3,471		35,902	\$5.00	\$179,510
421-1	INSTALL GATE	EA	0	0	0	1		1	\$1,000.00	\$1,000
			\$17,440	\$22,300	\$23,570	\$18,355	\$100,000			
<b>STRUCTURES</b>										
505-1	CONCRETE CHANNEL LINING (7" THICK)	SF	0	0	0	0		17,476	\$10.80	\$188,784
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	1,026	0	0	0		1,026	\$1,121.25	\$1,150,403
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	0	393	0		663	\$1,604.20	\$1,063,585
505-4	CONCRETE BOX CULVERT TYPE E (2 BARREL 10' x 6'), ADOT B-02.20	LF	0	2,746	0	0		2,746	\$1,475.50	\$4,051,723
	CONCRETE BOX CULVERT TYPE E (1 BARREL 10' x 6'), ADOT B-02.20	LF	0	0		1,320		1,320	\$737.75	\$973,830
505-5	CONCRETE BOX CULVERT INLET HEADWALL, ADOT B-04.30	EA	2	0	1	1		9	\$8,801.00	\$79,209



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 2010 LAND COST ESTIMATES**  
**ALTERNATIVE 6/7E**

1/29/2010

FCD 2009C012  
 PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
 HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	2	0	2	0		9	\$14,768.00	\$132,912
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850
			\$1,415,316	\$4,132,628	\$900,308	\$994,481	\$5,556			
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			<b>\$1,901,777</b>	<b>\$4,254,712</b>	<b>\$1,641,857</b>	<b>\$1,844,770</b>	<b>\$1,002,534</b>			<b>\$14,702,656</b>
Relocation and/or Removal of Existing Utilities			\$95,089	\$212,736	\$82,093	\$92,238	\$50,127		5%	\$735,133
Engineering Contingencies for Unknown Items			\$95,089	\$212,736	\$82,093	\$92,238	\$50,127		5%	\$735,133
<b>TOTAL CONSTRUCTION COST</b>			<b>\$2,091,954</b>	<b>\$4,680,183</b>	<b>\$1,806,043</b>	<b>\$2,029,247</b>	<b>\$1,102,787</b>			<b>\$16,172,922</b>
Landscaping as Aesthetic Treatment			\$155,829	\$0	\$183,934	\$129,275	\$0	46	\$20,000	\$927,152
Non-Landscaping Aesthetic Treatment			\$83,678	\$187,207	\$72,242	\$81,170	\$44,111		4%	\$646,917
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			<b>\$2,331,462</b>	<b>\$4,867,391</b>	<b>\$2,062,218</b>	<b>\$2,239,691</b>	<b>\$1,146,899</b>			<b>\$17,746,990</b>
Engineering and Landscape Design			\$233,146	\$486,739	\$206,222	\$223,969	\$114,690		10%	\$1,774,699
Construction Administration			\$139,888	\$292,043	\$123,733	\$134,381	\$68,814		6%	\$1,064,819
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			<b>\$2,704,496</b>	<b>\$5,646,173</b>	<b>\$2,392,173</b>	<b>\$2,598,042</b>	<b>\$1,330,403</b>			<b>\$20,586,509</b>
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	10.08	0.00	13.11	0.00	0.00	23.19	\$40,000.00	\$927,619
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	0.00	12.51	\$60,000.00	\$750,789
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		<b>AC</b>	<b>10.08</b>	<b>0.00</b>	<b>13.11</b>	<b>0.00</b>	<b>0.00</b>	<b>35.70</b>		<b>\$1,678,408</b>
<b>TOTAL PROJECT COST</b>			<b>\$3,107,759</b>	<b>\$5,646,173</b>	<b>\$2,916,529</b>	<b>\$2,598,042</b>	<b>\$1,330,403</b>			<b>\$22,264,916</b>



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 6/7F**

FCD 2009C012

PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.

HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
<b>GENERAL CONDITIONS</b>										
105-1	PARTNERING ALLOWANCE	LS					1	1	\$15,000.00	\$15,000
107-1	AZDPES/SWPPP PERMITS	LS					1	1	\$100,000.00	\$100,000
107-2	PUBLIC INFORMATION & NOTIFICATION ALLOWANCE	LS					1	1	\$20,000.00	\$20,000
107-3	PROJECT SIGNS ALLOWANCE	EA					1	1	\$5,000.00	\$5,000
107-4	WATER MANAGEMENT	LS					1	1	\$55,884.74	\$55,885
107-5	VANDALISM ALLOWANCE	LS					1	1	\$25,000.00	\$25,000
							\$220,885			
<b>EARTHWORK</b>										
201-1	CLEARING AND GRUBBING	LS					1	1	\$288,562.50	\$288,563
202-1	MOBILIZATION	LS					1	1	\$110,034.84	\$110,035
211-1	FILL CONSTRUCTION (DITCHES, FARM ROAD AND OVERBANK)	CY	1,864	150	625	57,639		109,234	\$7.00	\$764,638
211-2	FINAL AESTHETIC GRADING	LS					1	1	\$227,496.40	\$227,496
215-1	CHANNEL EXCAVATION	CY	46,736	63,919	92,535	68,038		470,589	\$3.00	\$1,411,767
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	20	0	151	0		459	\$45.00	\$20,655
220-2	PLAIN RIPRAP (D <sub>50</sub> = 12")	CY	324	196	1,311	20		3,038	\$70.00	\$212,660
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	562	0	748			6,017	\$75.00	\$451,275
230-1	GRAVEL MULCH	SY	37,711	0	44,512	31,284		224,371	\$4.00	\$897,483
230-2	HYDROSEEDING	AC	9	0	10.97	11.23		61	\$6,000.00	\$368,870
			\$426,044	\$206,527	\$680,485	\$801,502	\$626,094			
<b>STREETS &amp; RELATED WORK</b>										
310-1	ABC MAINTENANCE ROAD & RAMP (4-INCH)	SY	7,504	3,077	8,098	6,535		49,082	\$4.63	\$227,252
336-1	TEMPORARY PAVEMENT REPLACEMENT (2" A.C.)	SY	0	0	0	0		996	\$20.00	\$19,924
336-2	PERMANENT PAVEMENT REPLACEMENT (3" A.C.)	SY	274	322	0	0		682	\$30.00	\$20,467
340-1	CONCRETE VERTICAL CURB & GUTTER, MAG STD DET 220, TYPE 'A'	LF	0	36	0	0		36	\$19.00	\$684
340-2	CONCRETE ROLL CURB & GUTTER, MAG STD DET 220, TYPE 'C'	LF	0	80	0	0		80	\$17.00	\$1,360
340-3	CONCRETE SIDEWALK, MAG STD DET 230	SF	0	1,004	0	0		1,004	\$15.00	\$15,060
340-4	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-1	SF	0	144	0	0		144	\$15.00	\$2,160
340-5	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-2	SF	0	576	0	0		576	\$15.00	\$8,640
350-1	REMOVE EXISTING WIRE FENCE	LF	0	0	0	175		3,832	\$1.00	\$3,832
350-2	REMOVE PAVEMENT	SY	0	0	0	0		1,739	\$7.00	\$12,171
350-3	BURIED TRASH REMOVAL ALLOWANCE	LS					1	1	\$50,000.00	\$50,000
350-4	REMOVE CONCRETE CURB & GUTTER	LF	0	236	0	0		236	\$6.00	\$1,416
350-5	REMOVE GROUTED RIPRAP	SY	0	0	0	0		4,597	\$18.92	\$86,952
350-6	REMOVE EXISTING BLOCK WALL, RETAINIGN WALL	LF	0	3,711	0	0		4,057	\$8.00	\$32,456
350-7	REMOVE EXISTING CONCRETE LINED CHANNEL	SY	0	0	0	0		2,920	\$18.92	\$55,232
350-8	REMOVE EXISTING CONCRETE SIDEWALK	SY	0	112	0	0		112	\$18.92	\$2,110
			\$42,977	\$85,014	\$37,495	\$30,432	\$50,000			
<b>RIGHT-OF-WAY AND TRAFFIC CONTROL</b>										
401-1	MISCELLANEOUS TRAFFIC CONTROL	LS					1	1	\$100,000.00	\$100,000
412-1	4 STRAND SMOOTH WIRE FENCE	LF	3,488	4,460	4,714	3,471		35,902	\$5.00	\$179,510
421-1	INSTALL GATE	EA	0	0	0	1		1	\$1,000.00	\$1,000
			\$17,440	\$22,300	\$23,570	\$18,355	\$100,000			
<b>STRUCTURES</b>										
505-1	CONCRETE CHANNEL LINING (7" THICK)	SF	0	140,400	0	0		157,876	\$10.80	\$1,705,451
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	1,026	85	0	0		1,111	\$1,121.25	\$1,245,709
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	58	393	0		721	\$1,604.20	\$1,156,628
505-4	CONCRETE BOX CULVERT TYPE E (1 BARREL 10' x 6'), ADOT B-02.20	LF	0	0	0	1,320		1,320	\$737.75	\$973,830
505-5	CONCRETE BOX CULVERT INLET HEADWALL, ADOT B-04.30	EA	2	2	1	1		11	\$8,801.00	\$96,811



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 6/7F**

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY											
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT	
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	2	2	2	0		11	\$14,768.00	\$162,448	
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500	
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000	
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000	
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556	
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500	
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000	
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500	
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500	
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000	
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500	
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000	
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000	
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0	
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500	
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0	
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010	
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0	
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000	
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000	
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850	
			\$1,415,316	\$1,833,060	\$900,308	\$994,481	\$5,556				
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			\$1,901,777	\$2,146,901	\$1,641,857	\$1,844,770	\$1,002,534			\$12,594,844	
Relocation and/or Removal of Existing Utilities			\$95,089	\$107,345	\$82,093	\$92,238	\$50,127		5%	\$629,742	
Engineering Contingencies for Unknown Items			\$95,089	\$107,345	\$82,093	\$92,238	\$50,127		5%	\$629,742	
<b>TOTAL CONSTRUCTION COST</b>			\$2,091,954	\$2,361,591	\$1,806,043	\$2,029,247	\$1,102,787			\$13,854,329	
Landscaping as Aesthetic Treatment			\$155,829	\$0	\$183,934	\$129,275	\$0	46	\$20,000	\$927,152	
Non-Landscaping Aesthetic Treatment			\$83,678	\$94,464	\$72,242	\$81,170	\$44,111		4%	\$554,173	
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			\$2,331,462	\$2,456,054	\$2,062,218	\$2,239,691	\$1,146,899			\$15,335,654	
Engineering and Landscape Design			\$233,146	\$245,605	\$206,222	\$223,969	\$114,690		10%	\$1,533,565	
Construction Administration			\$139,888	\$147,363	\$123,733	\$134,381	\$68,814		6%	\$920,139	
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			\$2,704,496	\$2,849,023	\$2,392,173	\$2,598,042	\$1,330,403			\$17,789,359	
Required FCDMC Right-of-Way Acquisition - Undeveloped Property			AC	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property			AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>			AC	10.08	0.00	13.11	0.00	0.00	35.70		\$6,101,742
<b>TOTAL PROJECT COST</b>			\$4,241,936	\$2,849,023	\$4,391,280	\$2,598,042	\$1,330,403			\$23,891,101	



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 9D**

FCD 2009C012

HOSKIN-RYAN CONSULTANTS, INC.

PCN 470.04.32

HRC 09-077-01

**QUANTITY SUMMARY**

ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
<b>GENERAL CONDITIONS</b>										
105-1	PARTNERING ALLOWANCE	LS					1	1	\$15,000.00	\$15,000
107-1	AZDPES/SWPPP PERMITS	LS					1	1	\$100,000.00	\$100,000
107-2	PUBLIC INFORMATION & NOTIFICATION ALLOWANCE	LS					1	1	\$20,000.00	\$20,000
107-3	PROJECT SIGNS ALLOWANCE	EA					1	1	\$5,000.00	\$5,000
107-4	WATER MANAGEMENT	LS					1	1	\$55,884.74	\$55,885
107-5	VANDALISM ALLOWANCE	LS					1	1	\$25,000.00	\$25,000
							\$220,885			
<b>EARTHWORK</b>										
201-1	CLEARING AND GRUBBING	LS					1	1	\$288,562.50	\$288,563
202-1	MOBILIZATION	LS					1	1	\$110,034.84	\$110,035
211-1	FILL CONSTRUCTION (DITCHES, FARM ROAD AND OVERBANK)	CY	1,864	150	625	42,772		94,367	\$7.00	\$660,571
211-2	FINAL AESTHETIC GRADING	LS					1	1	\$227,496.40	\$227,496
215-1	CHANNEL EXCAVATION	CY	46,736	63,919	92,535	10,886		413,437	\$3.00	\$1,240,311
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	20	0	151	0		459	\$45.00	\$20,655
220-2	PLAIN RIPRAP (D <sub>50</sub> = 12")	CY	324	196	1,311	0		3,018	\$70.00	\$211,260
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	582	0	748			6,017	\$75.00	\$451,275
230-1	GRAVEL MULCH	SY	37,711	27,513	44,512	5,006		225,605	\$4.00	\$902,419
230-2	HYDROSEEDING	AC	9	7.29	10.97	0.58		58	\$6,000.00	\$348,750
			\$426,044	\$360,338	\$680,485	\$355,583	\$626,094			
<b>STREETS &amp; RELATED WORK</b>										
310-1	ABC MAINTENANCE ROAD & RAMP (4-INCH)	SY	7,504	3,077	8,098	6,535		49,082	\$4.63	\$227,252
336-1	TEMPORARY PAVEMENT REPLACEMENT (2" A.C.)	SY	0	0	0	0		996	\$20.00	\$19,924
336-2	PERMANENT PAVEMENT REPLACEMENT (3" A.C.)	SY	274	322	0	0		682	\$30.00	\$20,467
340-1	CONCRETE VERTICAL CURB & GUTTER, MAG STD DET 220, TYPE 'A'	LF	0	36	0	0		36	\$19.00	\$684
340-2	CONCRETE ROLL CURB & GUTTER, MAG STD DET 220, TYPE 'C'	LF	0	80	0	0		80	\$17.00	\$1,360
340-3	CONCRETE SIDEWALK, MAG STD DET 230	SF	0	1,004	0	0		1,004	\$15.00	\$15,060
340-4	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-1	SF	0	144	0	0		144	\$15.00	\$2,160
340-5	CONCRETE DRIVEWAY ENTRANCE, MAG STD DET 250-2	SF	0	576	0	0		576	\$15.00	\$8,640
350-1	REMOVE EXISTING WIRE FENCE	LF	0	0	0	175		3,832	\$1.00	\$3,832
350-2	REMOVE PAVEMENT	SY	0	0	0	0		1,739	\$7.00	\$12,171
350-3	BURIED TRASH REMOVAL ALLOWANCE	LS				0	1	1	\$50,000.00	\$50,000
350-4	REMOVE CONCRETE CURB & GUTTER	LF	0	236	0	0		236	\$6.00	\$1,416
350-5	REMOVE GROUTED RIPRAP	SY	0	0	0	0		4,597	\$18.92	\$86,952
350-6	REMOVE EXISTING BLOCK WALL, RETAINIGN WALL	LF	0	3,711	0	0		4,057	\$8.00	\$32,456
350-7	REMOVE EXISTING CONCRETE LINED CHANNEL	SY	0	0	0	0		2,920	\$18.92	\$55,232
350-8	REMOVE EXISTING CONCRETE SIDEWALK	SY	0	112	0	0		112	\$18.92	\$2,110
			\$42,977	\$85,014	\$37,495	\$30,432	\$50,000			
<b>RIGHT-OF-WAY AND TRAFFIC CONTROL</b>										
401-1	MISCELLANEOUS TRAFFIC CONTROL	LS				0	1	1	\$100,000.00	\$100,000
412-1	4 STRAND SMOOTH WIRE FENCE	LF	3,488	4,460	4,714	3,471		35,902	\$5.00	\$179,510
421-1	INSTALL GATE	EA	0	0	0	0		0	\$1,000.00	\$0
			\$17,440	\$22,300	\$23,570	\$17,355	\$100,000			
<b>STRUCTURES</b>										
505-1	CONCRETE CHANNEL LINING (7" THICK)	SF	0	0	0	0		17,476	\$10.80	\$188,784
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	1,026	85	0	0		1,111	\$1,121.25	\$1,245,709
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	58	393	0		721	\$1,604.20	\$1,156,628
505-4	2-72" DUROMAXX HDPE PIPES TO REPLACE CONCRETE BOX CULVERT	LF	0	0	0	9,600		9,600	\$140.00	\$1,344,000
505-5	CONCRETE BOX CULVERT INLET HEADWALL, ADOT B-04.30	EA	2	2	1	1		11	\$8,801.00	\$96,811
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	2	2	2	0		11	\$14,768.00	\$162,448



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 9D**

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0
	MANHOLES	EA				8		8	\$4,160.00	\$33,280
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850
			\$1,415,316	\$316,393	\$900,308	\$1,397,931	\$5,556			
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			<b>\$1,901,777</b>	<b>\$784,045</b>	<b>\$1,641,857</b>	<b>\$1,801,301</b>	<b>\$1,002,534</b>			<b>\$11,188,520</b>
Relocation and/or Removal of Existing Utilities			\$95,089	\$39,202	\$82,093	\$90,065	\$50,127		5%	\$559,426
Engineering Contingencies for Unknown Items			\$95,089	\$39,202	\$82,093	\$90,065	\$50,127		5%	\$559,426
<b>TOTAL CONSTRUCTION COST</b>			<b>\$2,091,954</b>	<b>\$862,450</b>	<b>\$1,806,043</b>	<b>\$1,981,431</b>	<b>\$1,102,787</b>			<b>\$12,307,372</b>
Landscaping as Aesthetic Treatment			\$155,829	\$113,690	\$183,934	\$20,684	\$0	47	\$20,000	\$932,251
Non-Landscaping Aesthetic Treatment			\$83,678	\$34,498	\$72,242	\$79,257	\$44,111		4%	\$492,295
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			<b>\$2,331,462</b>	<b>\$1,010,637</b>	<b>\$2,062,218</b>	<b>\$2,081,372</b>	<b>\$1,146,899</b>			<b>\$13,731,918</b>
Engineering and Landscape Design			\$233,146	\$101,064	\$206,222	\$208,137	\$114,690		10%	\$1,373,192
Construction Administration			\$139,888	\$60,638	\$123,733	\$124,882	\$68,814		6%	\$823,915
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			<b>\$2,704,496</b>	<b>\$1,172,339</b>	<b>\$2,392,173</b>	<b>\$2,414,391</b>	<b>\$1,330,403</b>			<b>\$15,929,025</b>
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		<b>AC</b>	<b>10.08</b>	<b>0.00</b>	<b>13.11</b>	<b>0.00</b>	<b>0.00</b>	<b>35.70</b>		<b>\$6,101,742</b>
<b>TOTAL PROJECT COST</b>			<b>\$4,241,936</b>	<b>\$1,172,339</b>	<b>\$4,391,280</b>	<b>\$2,414,391</b>	<b>\$1,330,403</b>			<b>\$22,030,767</b>

*P39 says \$21,800,771*



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 9E**

FCD 2009C012  
PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.  
HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	2	2	2	0		11	\$14,768.00	\$162,448
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			\$1,415,316	\$316,393	\$900,308	\$994,481	\$5,556			
Relocation and/or Removal of Existing Utilities			\$95,089	\$39,202	\$82,093	\$104,533	\$50,127		5%	\$573,894
Engineering Contingencies for Unknown Items			\$95,089	\$39,202	\$82,093	\$104,533	\$50,127		5%	\$573,894
<b>TOTAL CONSTRUCTION COST</b>			\$2,091,954	\$862,450	\$1,806,043	\$2,299,721	\$1,102,787			\$12,625,663
Landscaping as Aesthetic Treatment			\$155,829	\$113,690	\$183,934	\$129,275	\$0	52	\$20,000	\$1,040,842
Non-Landscaping Aesthetic Treatment			\$83,678	\$34,498	\$72,242	\$91,989	\$44,111		4%	\$505,027
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			\$2,331,462	\$1,010,637	\$2,062,218	\$2,520,985	\$1,146,899			\$14,171,531
Engineering and Landscape Design			\$233,146	\$101,064	\$206,222	\$252,098	\$114,690		10%	\$1,417,153
Construction Administration			\$139,888	\$60,638	\$123,733	\$151,259	\$68,814		6%	\$850,292
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			\$2,704,496	\$1,172,339	\$2,392,173	\$2,924,342	\$1,330,403			\$16,438,976
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		AC	10.08	0.00	13.11	0.00	0.00	35.70		\$6,101,742
<b>TOTAL PROJECT COST</b>			\$4,241,936	\$1,172,339	\$4,391,280	\$2,924,342	\$1,330,403			\$22,540,718



**WHITE TANKS FRS#3 OUTLET CHANNEL - COST ESTIMATE BY REACH, USING 30% DESIGN REPORT LAND COSTS**

1/27/2010

**ALTERNATIVE 9E**

FCD 2009C012

PCN 470.04.32

HOSKIN-RYAN CONSULTANTS, INC.

HRC 09-077-01

QUANTITY SUMMARY										
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
505-6	CONCRETE BOX CULVERT OUTLET HEADWALL, ADOT B-04.30	EA	2	2	2	0		11	\$14,768.00	\$162,448
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	0		154	\$500.00	\$77,000
505-10	CONCRETE TEST PANELS - 10' x 10' x 6"	EA					3	3	\$1,851.85	\$5,556
505-11	CONCRETE SIDE FLOW SPILLWAY, (10' BOTTOM WIDTH) TYPE1	CY	0	0	0	0		35	\$500.00	\$17,500
505-12	CONCRETE SIDE FLOW SPILLWAY, (20' BOTTOM WIDTH) TYPE2	CY	0	0	0	0		80	\$500.00	\$40,000
505-13	CONCRETE SIDE FLOW SPILLWAY, (30' BOTTOM WIDTH) TYPE3	CY	0	0	0	0		65	\$500.00	\$32,500
505-14	CONCRETE SIDE FLOW SPILLWAY, (40' BOTTOM WIDTH) TYPE4	CY	0	0	0	0		63	\$500.00	\$31,500
505-15	CONCRETE SIDE FLOW SPILLWAY, (50' BOTTOM WIDTH) TYPE5	CY	0	0	140	0		140	\$500.00	\$70,000
505-16	CONCRETE SIDE FLOW SPILLWAY, (80' BOTTOM WIDTH) TYPE6	CY	0	0	251	0		251	\$500.00	\$125,500
505-17	CONCRETE DROP INLET STRUCTURE, (3-8'X6' BOX CULVERT) TYPE 1	CY	0	0	0	0		80	\$500.00	\$40,000
505-18	CONCRETE DROP INLET STRUCTURE, (2-8'X6' BOX CULVERT) TYPE 2	CY	14	14	0	0		28	\$500.00	\$14,000
505-19	WASTEWAY STRUCTURE	CY	0	0	0	0		0	\$500.00	\$0
505-20	FLOW JUNCTION STRUCTURE	CY	137	0	0	0		137	\$500.00	\$68,500
505-21	SLIDE GATE STRUCTURE	EA	0	0	0	0		0	\$50,000.00	\$0
505-22	GROUTED RIPRAP DOWNDRAIN	EA	0	6	4	0		27	\$1,630.00	\$44,010
505-23	ALLOWANCE FOR HARDENED STRUCTURE WITHIN FISSURE ZONE	LS					0	0	\$2,225,826.96	\$0
510-1	RETAINING WALL, 2' TO 3'	LF	0	300	100	0		400	\$40.00	\$16,000
515-1	BOLLARDS, MAG STD DET 140, TYPE 2 REMOVABLE	EA	12	21	9	3		96	\$1,000.00	\$96,000
520-1	STEEL SAFETY RAIL, MAG STD DET 145, TYPE 1	LF	617	415	220	118		2,398	\$75.00	\$179,850
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			\$1,415,316	\$316,393	\$900,308	\$994,481	\$5,556			
Relocation and/or Removal of Existing Utilities			\$95,089	\$39,202	\$82,093	\$104,533	\$50,127		5%	\$573,894
Engineering Contingencies for Unknown Items			\$95,089	\$39,202	\$82,093	\$104,533	\$50,127		5%	\$573,894
<b>TOTAL CONSTRUCTION COST</b>			\$2,091,954	\$862,450	\$1,806,043	\$2,299,721	\$1,102,787			\$12,625,663
Landscaping as Aesthetic Treatment			\$155,829	\$113,690	\$183,934	\$129,275	\$0	52	\$20,000	\$1,040,842
Non-Landscaping Aesthetic Treatment			\$83,678	\$34,498	\$72,242	\$91,989	\$44,111		4%	\$505,027
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			\$2,331,462	\$1,010,637	\$2,062,218	\$2,520,985	\$1,146,899			\$14,171,531
Engineering and Landscape Design			\$233,146	\$101,064	\$206,222	\$252,098	\$114,690		10%	\$1,417,153
Construction Administration			\$139,888	\$60,638	\$123,733	\$151,259	\$68,814		6%	\$850,292
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			\$2,704,496	\$1,172,339	\$2,392,173	\$2,924,342	\$1,330,403			\$16,438,976
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		AC	10.08	0.00	13.11	0.00	0.00	35.70		\$6,101,742
<b>TOTAL PROJECT COST</b>			\$4,241,936	\$1,172,339	\$4,391,280	\$2,924,342	\$1,330,403			\$22,540,718

*Duplicates F-16?*



**Project Cost with CBC versus Arch Culverts**

CONCRETE BOX CULVERTS THROUGHOUT PROJECT																
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 1	REACH 2	REACH 3	REACH 4	REACH 5	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT	
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	0	0	0	0	0	826	85	0	0		911	\$1,121.25	\$1,021,459	
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	162	50	0	58	0	58	393	0		721	\$1,604.20	\$1,156,628	
505-4	CONCRETE BOX CULVERT TYPE E (2 BARREL 10' x 6'), ADOT B-02.20	LF	0	0	0	0	0	0	0	0	1,320		1,320	\$1,475.50	\$1,947,660	
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			\$255,148	\$1,757,019	\$825,242	\$336,568	\$883,030	\$1,653,958	\$784,045	\$1,641,857	\$3,069,600	\$3,228,361			\$14,434,827	
Relocation and/or Removal of Existing Utilities			\$12,757	\$87,851	\$41,262	\$16,828	\$44,152	\$82,698	\$39,202	\$82,093	\$153,480	\$161,418			5%	\$721,741
Engineering Contingencies for Unknown Items			\$12,757	\$87,851	\$41,262	\$16,828	\$44,152	\$82,698	\$39,202	\$82,093	\$153,480	\$161,418			5%	\$721,741
<b>TOTAL CONSTRUCTION COST</b>			\$280,663	\$1,932,721	\$907,766	\$370,225	\$971,333	\$1,819,353	\$862,450	\$1,806,043	\$3,376,560	\$3,551,197			\$15,878,310	
Landscaping as Aesthetic Treatment			\$6,175	\$160,292	\$87,381	\$30,207	\$174,060	\$155,829	\$113,690	\$183,934	\$129,275	\$0		52	\$20,000	\$1,040,842
Non-Landscaping Aesthetic Treatment			\$11,227	\$77,309	\$36,311	\$14,809	\$38,853	\$72,774	\$34,498	\$72,242	\$135,062	\$142,048			4%	\$635,132
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			\$298,064	\$2,170,322	\$1,031,457	\$415,240	\$1,184,246	\$2,047,957	\$1,010,637	\$2,062,218	\$3,640,897	\$3,693,245			\$17,554,284	
Engineering and Landscape Design			\$29,806	\$217,032	\$103,146	\$41,524	\$118,425	\$204,796	\$101,064	\$206,222	\$364,090	\$369,324			10%	\$1,755,428
Construction Administration			\$17,884	\$130,219	\$61,897	\$24,914	\$71,055	\$122,877	\$60,638	\$123,733	\$218,454	\$221,595			6%	\$1,053,257
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			\$345,755	\$2,517,573	\$1,196,490	\$481,679	\$1,373,725	\$2,375,630	\$1,172,339	\$2,392,173	\$4,223,440	\$4,284,164			\$20,362,969	
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	0.00	0.00	0.00	0.00	0.00	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547	
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	12.51	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195	
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		AC	0.00	0.00	0.00	0.00	12.51	10.08	0.00	13.11	0.00	0.00	35.70		\$6,101,742	
<b>TOTAL PROJECT COST</b>			\$345,755	\$2,517,573	\$1,196,490	\$481,679	\$3,938,921	\$3,913,070	\$1,172,339	\$4,391,280	\$4,223,440	\$4,284,164			\$26,464,711	

CONSPAN ARCH CULVERTS THROUGHOUT PROJECT																
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 1	REACH 2	REACH 3	REACH 4	REACH 5	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT	
505-2	CONCRETE BOX CULVERT TYPE A (2 BARREL 8' x 6'), ADOT B-02.20	LF	0	0	0	0	0	826	85	0	0		911	\$670.00	\$610,370	
505-3	CONCRETE BOX CULVERT TYPE B (3 BARREL 8' x 6'), ADOT B-02.30	LF	0	162	50	0	58	0	58	393	0		721	\$754.00	\$543,634	
505-4	CONCRETE BOX CULVERT TYPE E (2 BARREL 10' x 6'), ADOT B-02.20	LF	0	0	0	0	0	0	0	0	1,320		1,320	\$1,475.50	\$1,947,660	
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			\$255,148	\$1,619,287	\$782,732	\$336,568	\$833,718	\$1,281,225	\$696,377	\$1,307,729	\$3,069,600	\$3,228,361			\$13,410,744	
Relocation and/or Removal of Existing Utilities			\$12,757	\$80,964	\$39,137	\$16,828	\$41,686	\$84,061	\$34,819	\$65,386	\$153,480	\$161,418			5%	\$670,537
Engineering Contingencies for Unknown Items			\$12,757	\$80,964	\$39,137	\$16,828	\$41,686	\$84,061	\$34,819	\$65,386	\$153,480	\$161,418			5%	\$670,537
<b>TOTAL CONSTRUCTION COST</b>			\$280,663	\$1,781,215	\$861,005	\$370,225	\$917,090	\$1,409,348	\$766,015	\$1,438,501	\$3,376,560	\$3,551,197			\$14,751,819	
Landscaping as Aesthetic Treatment			\$6,175	\$160,292	\$87,381	\$30,207	\$174,060	\$155,829	\$113,690	\$183,934	\$129,275	\$0		52	\$20,000	\$1,040,842
Non-Landscaping Aesthetic Treatment			\$11,227	\$71,249	\$34,440	\$14,809	\$36,684	\$56,374	\$30,641	\$57,540	\$135,062	\$142,048			4%	\$590,073
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			\$298,064	\$2,012,756	\$982,826	\$415,240	\$1,127,834	\$1,621,551	\$910,345	\$1,679,975	\$3,640,897	\$3,693,245			\$16,382,733	
Engineering and Landscape Design			\$29,806	\$201,276	\$98,283	\$41,524	\$112,783	\$162,155	\$91,035	\$167,998	\$364,090	\$369,324			10%	\$1,638,273
Construction Administration			\$17,884	\$120,765	\$58,970	\$24,914	\$67,670	\$97,293	\$54,621	\$100,799	\$218,454	\$221,595			6%	\$982,964
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			\$345,755	\$2,334,797	\$1,140,078	\$481,679	\$1,308,287	\$1,880,999	\$1,056,001	\$1,948,771	\$4,223,440	\$4,284,164			\$19,003,970	
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	0.00	0.00	0.00	0.00	0.00	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547	
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	12.51	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195	
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		AC	0.00	0.00	0.00	0.00	12.51	10.08	0.00	13.11	0.00	0.00	35.70		\$6,101,742	
<b>TOTAL PROJECT COST</b>			\$345,755	\$2,334,797	\$1,140,078	\$481,679	\$3,873,482	\$3,418,439	\$1,056,001	\$3,947,878	\$4,223,440	\$4,284,164			\$25,105,712	



**Project Cost with RipRap and Concrete Grade Control Structures versus ArmorFlex Grade Control Structures**

RIPRAP AT GRADE CONTROL STRUCTURES															
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 1	REACH 2	REACH 3	REACH 4	REACH 5	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
220-1	PLAIN RIPRAP (D <sub>50</sub> = 2")	CY	0	170	60	42	16	20	0	151	0		459	\$45.00	\$20,655
220-3	PLAIN RIPRAP (D <sub>50</sub> = 15")	CY	0	2,619	1,285	522	281	562	0	748			6,017	\$75.00	\$451,275
505-7	CONCRETE GRADE CONTROL STRUCTURE, (30'-10' BOTTOM WIDTH TRANSITION) TYPE 1	CY	0	609	342	0	0	0	0	0	0		951	\$500.00	\$475,500
505-8	CONCRETE GRADE CONTROL STRUCTURE, (40'-20' BOTTOM WIDTH TRANSITION) TYPE 2	CY	0	0	0	0	84	168	0	0	0		252	\$500.00	\$126,000
505-9	CONCRETE GRADE CONTROL STRUCTURE, (50'-30' BOTTOM WIDTH TRANSITION) TYPE 3	CY	0	0	0	154	0	0	0	0	0		154	\$500.00	\$77,000
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			<b>\$255,148</b>	<b>\$1,757,019</b>	<b>\$825,242</b>	<b>\$336,568</b>	<b>\$883,030</b>	<b>\$1,653,958</b>	<b>\$784,045</b>	<b>\$1,641,857</b>	<b>\$3,069,600</b>	<b>\$3,228,361</b>			<b>\$14,434,827</b>
Relocation and/or Removal of Existing Utilities			\$12,757	\$87,851	\$41,262	\$16,828	\$44,152	\$82,698	\$39,202	\$82,093	\$153,480	\$161,418		5%	\$721,741
Engineering Contingencies for Unknown Items			\$12,757	\$87,851	\$41,262	\$16,828	\$44,152	\$82,698	\$39,202	\$82,093	\$153,480	\$161,418		5%	\$721,741
<b>TOTAL CONSTRUCTION COST</b>			<b>\$280,663</b>	<b>\$1,932,721</b>	<b>\$907,766</b>	<b>\$370,225</b>	<b>\$971,333</b>	<b>\$1,819,353</b>	<b>\$862,450</b>	<b>\$1,806,043</b>	<b>\$3,376,560</b>	<b>\$3,551,197</b>			<b>\$15,878,310</b>
Landscaping as Aesthetic Treatment			\$6,175	\$160,292	\$87,381	\$30,207	\$174,060	\$155,829	\$113,690	\$183,934	\$129,275	\$0	52	\$20,000	\$1,040,842
Non-Landscaping Aesthetic Treatment			\$11,227	\$77,309	\$36,311	\$14,809	\$38,853	\$72,774	\$34,498	\$72,242	\$135,062	\$142,048		4%	\$635,132
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			<b>\$298,064</b>	<b>\$2,170,322</b>	<b>\$1,031,457</b>	<b>\$415,240</b>	<b>\$1,184,246</b>	<b>\$2,047,957</b>	<b>\$1,010,637</b>	<b>\$2,062,218</b>	<b>\$3,640,897</b>	<b>\$3,693,245</b>			<b>\$17,554,284</b>
Engineering and Landscape Design			\$29,806	\$217,032	\$103,146	\$41,524	\$118,425	\$204,796	\$101,064	\$206,222	\$364,090	\$369,324		10%	\$1,755,428
Construction Administration			\$17,884	\$130,219	\$61,887	\$24,914	\$71,055	\$122,877	\$60,638	\$123,733	\$218,454	\$221,595		6%	\$1,053,257
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			<b>\$345,755</b>	<b>\$2,517,573</b>	<b>\$1,196,490</b>	<b>\$481,679</b>	<b>\$1,373,725</b>	<b>\$2,375,630</b>	<b>\$1,172,339</b>	<b>\$2,392,173</b>	<b>\$4,223,440</b>	<b>\$4,284,164</b>			<b>\$20,362,969</b>
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	0.00	0.00	0.00	0.00	0.00	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	12.51	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		<b>AC</b>	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	<b>12.51</b>	<b>10.08</b>	<b>0.00</b>	<b>13.11</b>	<b>0.00</b>	<b>0.00</b>	<b>35.70</b>		<b>\$6,101,742</b>
<b>TOTAL PROJECT COST</b>			<b>\$345,755</b>	<b>\$2,517,573</b>	<b>\$1,196,490</b>	<b>\$481,679</b>	<b>\$3,938,921</b>	<b>\$3,913,070</b>	<b>\$1,172,339</b>	<b>\$4,391,280</b>	<b>\$4,223,440</b>	<b>\$4,284,164</b>			<b>\$26,464,711</b>

ARMORFLEX AT GRADE CONTROL STRUCTURES															
ITEM NO.	ITEM DESCRIPTION	UNIT	REACH 1	REACH 2	REACH 3	REACH 4	REACH 5	REACH 6	REACH 7	REACH 8	REACH 9	LUMP SUM ITEMS	TOTAL QUANTITY	UNIT PRICE	TOTAL AMOUNT
220-1	ARMORFLEX TO REPLACE RIPRAP	SF	0	9,105	3,230	2,270	836	1,672	0	8,132	0		25,245	\$9.04	\$228,215
220-3	ARMORFLEX TO REPLACE RIPRAP	SF	0	28,239	13,860	5,640	3,033	6,066	0	8,132			64,970	\$9.04	\$587,329
505-7	ARMORFLEX TO REPLACE GRADE CONTROL STRUCTURE	SF	0	16,794	9,330	0	0	0	0	0	0		26,124	\$9.04	\$236,161
505-8	ARMORFLEX TO REPLACE GRADE CONTROL STRUCTURE	SF	0	0	0	0	2,262	4,524	0	0	0		6,786	\$9.04	\$61,345
505-9	ARMORFLEX TO REPLACE GRADE CONTROL STRUCTURE	SF	0	0	0	4,294	0	0	0	0	0		4,294	\$9.04	\$38,818
	CONCRETE GRADE CONTROL STRUCTURE CUTOFF WALL	CY	0	195	112	46	28	56	0	0			437	\$500.00	\$218,500
<b>SUBTOTAL CONSTRUCTION ITEMS</b>			<b>\$255,148</b>	<b>\$1,835,352</b>	<b>\$850,003</b>	<b>\$351,852</b>	<b>\$888,659</b>	<b>\$1,665,756</b>	<b>\$784,045</b>	<b>\$1,725,989</b>	<b>\$3,069,600</b>	<b>\$3,228,361</b>			<b>\$14,654,765</b>
Relocation and/or Removal of Existing Utilities			\$12,757	\$91,768	\$42,500	\$17,593	\$44,433	\$83,288	\$39,202	\$86,299	\$153,480	\$161,418		5%	\$732,738
Engineering Contingencies for Unknown Items			\$12,757	\$91,768	\$42,500	\$17,593	\$44,433	\$83,288	\$39,202	\$86,299	\$153,480	\$161,418		5%	\$732,738
<b>TOTAL CONSTRUCTION COST</b>			<b>\$280,663</b>	<b>\$2,018,887</b>	<b>\$935,004</b>	<b>\$387,037</b>	<b>\$977,525</b>	<b>\$1,832,332</b>	<b>\$862,450</b>	<b>\$1,898,588</b>	<b>\$3,376,560</b>	<b>\$3,551,197</b>			<b>\$16,120,241</b>
Landscaping as Aesthetic Treatment			\$6,175	\$160,292	\$87,381	\$30,207	\$174,060	\$155,829	\$113,690	\$183,934	\$129,275	\$0	52	\$20,000	\$1,040,842
Non-Landscaping Aesthetic Treatment			\$11,227	\$80,755	\$37,400	\$15,481	\$39,101	\$73,293	\$34,498	\$75,944	\$135,062	\$142,048		4%	\$644,810
<b>TOTAL CONSTRUCTION AND LANDSCAPE COST</b>			<b>\$298,064</b>	<b>\$2,259,934</b>	<b>\$1,059,785</b>	<b>\$432,725</b>	<b>\$1,190,686</b>	<b>\$2,061,454</b>	<b>\$1,010,637</b>	<b>\$2,158,465</b>	<b>\$3,640,897</b>	<b>\$3,693,245</b>			<b>\$17,805,893</b>
Engineering and Landscape Design			\$29,806	\$225,993	\$105,978	\$43,273	\$119,069	\$206,145	\$101,064	\$215,846	\$364,090	\$369,324		10%	\$1,780,589
Construction Administration			\$17,884	\$135,596	\$63,587	\$25,964	\$71,441	\$123,687	\$60,638	\$129,508	\$218,454	\$221,595		6%	\$1,068,354
<b>TOTAL CONSTRUCTION, LANDSCAPE, AND CONTINGENCIES COST</b>			<b>\$345,755</b>	<b>\$2,621,524</b>	<b>\$1,229,350</b>	<b>\$501,961</b>	<b>\$1,381,196</b>	<b>\$2,391,287</b>	<b>\$1,172,339</b>	<b>\$2,503,819</b>	<b>\$4,223,440</b>	<b>\$4,284,164</b>			<b>\$20,654,835</b>
Required FCDMC Right-of-Way Acquisition - Undeveloped Property		AC	0.00	0.00	0.00	0.00	0.00	10.08	0.00	13.11	0.00	0.00	23.19	\$152,500.00	\$3,536,547
Required FCDMC Right-of-Way Acquisition - Platted Property		AC	0.00	0.00	0.00	0.00	12.51	0.00	0.00	0.00	0.00	0.00	12.51	\$205,000.00	\$2,565,195
<b>TOTAL REQUIRED RIGHT-OF-WAY ACQUISITION</b>		<b>AC</b>	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	<b>0.00</b>	<b>12.51</b>	<b>10.08</b>	<b>0.00</b>	<b>13.11</b>	<b>0.00</b>	<b>0.00</b>	<b>35.70</b>		<b>\$6,101,742</b>
<b>TOTAL PROJECT COST</b>			<b>\$345,755</b>	<b>\$2,621,524</b>	<b>\$1,229,350</b>	<b>\$501,961</b>	<b>\$3,946,391</b>	<b>\$3,928,727</b>	<b>\$1,172,339</b>	<b>\$4,502,926</b>	<b>\$4,223,440</b>	<b>\$4,284,164</b>			<b>\$26,756,577</b>



APPENDIX G – VALUE ENGINEERING MEMORANDUM BY JACOBS

**Memorandum**

101 North First Avenue  
Suite 3100  
Phoenix, AZ 85003-1902 USA  
602.253.1200 Fax 602.253.1202



**Memorandum**

(Continued)

Page 2 of 2

---

**Date** November 2, 2009 - Draft, Revised November 11, 2009

**To** Paul Hoskin (HRC), Kristyn Van Meter (HRC)

**From** Chris Miranda (JEG)

**Cc:** Brad Olbert (JEG), File

**Subject** Update on review of White Tanks FRS No. 3 Outfall Channel - 30% Plans

---

As per our scope of work, I want to update you on our progress on the review of the 30% plans. Through our review we have developed a few questions and that we believe would need to be reviewed and revised either in the Design Report or within the plans.

The items summarized below are based on our review of the 30% plans and the design report.

- Drop structure review
  - The design report states that the grades shall be a maximum of 20%, Volume I, P. 18. However, our review of the plans show the some drop structures having grades from 23% to 55%. All of the locations are located upstream and adjacent to proposed Box Culverts. If the grades at these locations are to be excluded the text should state so. Will users of the channel bottom be expecting a 20% grade at each location? Can using a deeper Box Culvert pass maintenance vehicles and avoid many of the channel ramps?
- Adverse Grades
  - The adverse grade proposed for the drop structures has a 20% grade on the downstream side and a 12.5% adverse grade on the upstream side. The total grade break is 32.5%. Initially maintenance vehicles may hang up on the crest. Suggest backfilling upstream to flatten the slope. This will happen eventually with sediment buildup. At that point the channel will have an adverse grade to it other than the low flow channel. The adverse crest is there to reduce the velocity of the channel flow to prevent channel erosion. Are we doubling up with protection? The upstream riprap provides a similar function. Would removing the adverse crest reduce the cost of the structure?
- Channel velocities
  - Within Vol. I, p.15, 16, and 18 of the design report, the channel velocities are stated to be above 3 fps, 3.5 fps, and 4 fps. However, the report discusses a maximum velocity of 3.0 fps for earth channels of sandy loam soils with vegetation. Midpoint sections might show velocities consistently above 3.0 fps. Need to check sediment transport equations for the sediment in the area to best determine the channel size.
- Gravel Mulch vs. Aggregate Base Course
  - Within Vol. I, p.19 of the design report, it states that the O&M road shall have gravel mulch but on sheet 51 of 55 within the plans shows the O&M road having 4-inches of ABC. ABC should be used in lieu of gravel mulch.

- Gravel Mulch
  - Gravel Mulch on sheet 5 of 55 within the plans is shown being used on the top of the banks as well as the sideslopes of the channel. This may not be a very aesthetic use of materials.

Additionally, through our review we have looked at a few items that can be discussed within the Value Engineering Meetings, set for November 3<sup>rd</sup> – 5<sup>th</sup>.

- Closed conduit HDPE pipe through Reach 9.
  - Please find the attached information from Contech and ISCO within Appendix A.
- Closed conduit from a portion of Reach 8 through Reach 6.
  - Please find the attached information on Conspan, from Contech and a Reinforced Concrete Box Culvert within Appendix B.
- Use of sediment traps to reduce the sediment bed load.
- Review of O&M needs for channel and type of vehicles to be used.



**APPENDIX H – WASTEWAY FLOW HEC-RAS MODEL**

HEC-RAS Version 4.0.0 March 2008  
 U.S. Army Corps of Engineers  
 Hydrologic Engineering Center  
 609 Second Street  
 Davis, California

```

X   X XXXXXX   XXXX   XXXX   XX   XXXX
X   X X       X   X   X   X   X   X
X   X X       X       X   X   X   X
XXXXXXXX XXXX   X     XXX XXXX XXXXXX XXXX
X   X X       X       X   X   X   X   X
X   X X       X   X   X   X   X   X
X   X XXXXXX   XXXX   X   X   X   X XXXXX
  
```

\*\*\*\*\*

PROJECT DATA  
 Project Title: Beardsley Wash  
 Project File : Beardsley.prj  
 Run Date and Time: 1/28/2010 4:17:33 PM

Project in English units

Project Description:  
 Project: Beardsley Wash PMF Floodplain  
 Hoskin Ryan  
 Consultants  
 12/28/2009

Cross-section geometries obtained from the aerial  
 mapping prepared by Cooper Aerial on 12/22/2009  
 Wash center line lies on  
 Station 1000 at each cross-section  
 Datum: NAVD 88

\*\*\*\*\*

PLAN DATA

Plan Title: PMF  
 Plan File : G:\Projects\09\09-077 WTO3 Final\01 - 30% Design\Hydro\HEC-RAS\Beardsley.p01

Geometry Title: Beardsley Wash  
 Geometry File : G:\Projects\09\09-077 WTO3 Final\01 - 30% Design\Hydro\HEC-RAS\Beardsley.g01

Flow Title : PMF  
 Flow File : G:\Projects\09\09-077 WTO3 Final\01 - 30% Design\Hydro\HEC-RAS\Beardsley.f01

Plan Summary Information:  
 Number of: Cross Sections = 28 Multiple Openings = 0  
 Culverts = 0 Inline Structures = 0  
 Bridges = 0 Lateral Structures = 0

Computational Information  
 Water surface calculation tolerance = 0.01  
 Critical depth calculation tolerance = 0.01  
 Maximum number of iterations = 20  
 Maximum difference tolerance = 0.3  
 Flow tolerance factor = 0.001

Computation Options  
 Critical depth computed only where necessary  
 Conveyance Calculation Method: At breaks in n values only  
 Friction Slope Method: Average Conveyance  
 Computational Flow Regime: Subcritical Flow

\*\*\*\*\*

FLOW DATA

Flow Title: PMF  
 Flow File : G:\Projects\09\09-077 WTO3 Final\01 - 30% Design\Hydro\HEC-RAS\Beardsley.f01

Flow Data (cfs)  
 \*\*\*\*\*  
 \* River Reach RS \* PF 1 \*  
 \* Beardsley Wash 9 5800 \* 1 \*  
 \* Beardsley Wash 9 5200 \* 221 \*  
 \*\*\*\*\*

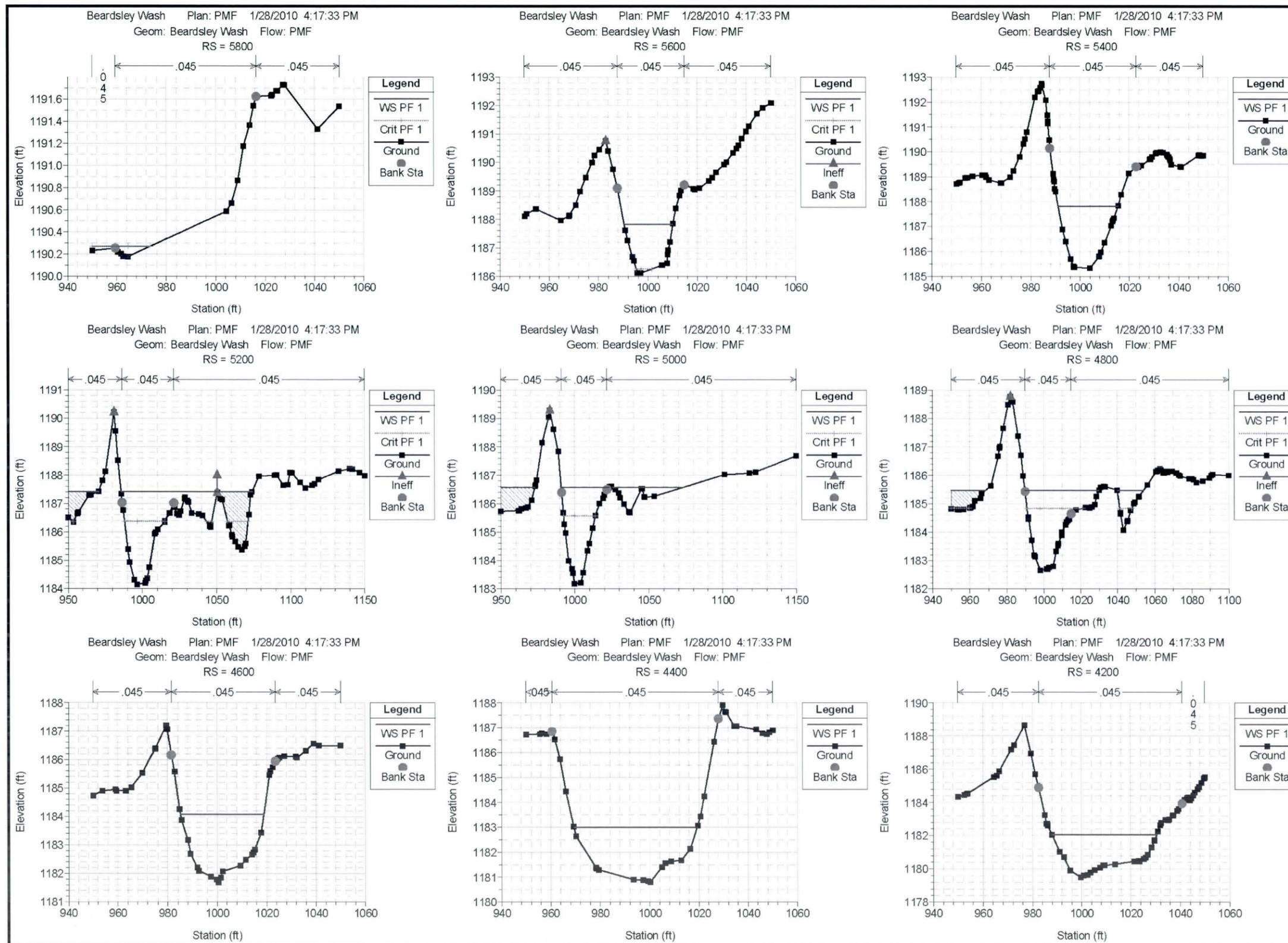
Boundary Conditions  
 \*\*\*\*\*  
 \* River Reach Profile \* Upstream Downstream \*  
 \*\*\*\*\*  
 \* Beardsley Wash 9 PF 1 \* Normal S = 0.005 \*  
 \*\*\*\*\*

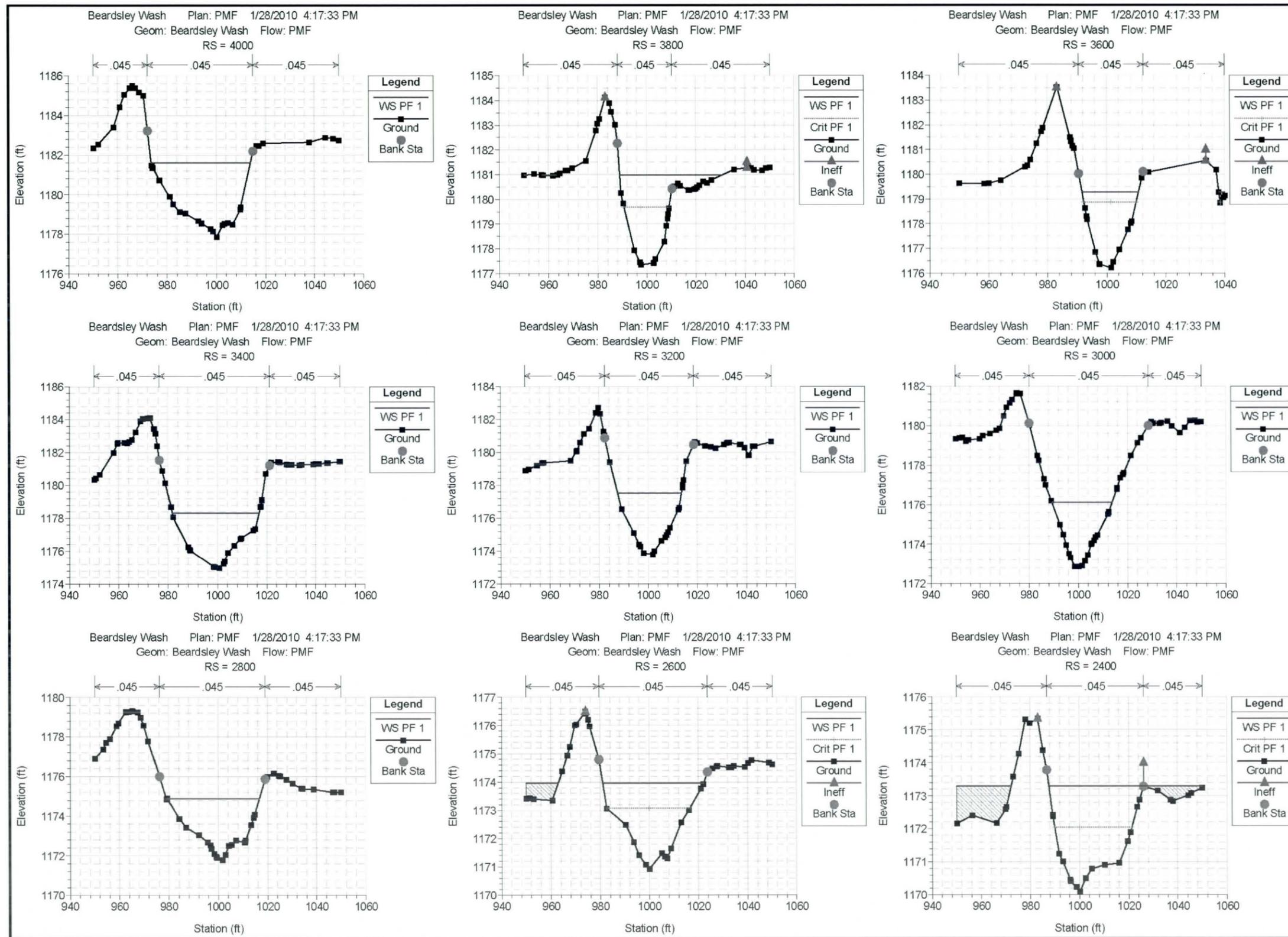
\*\*\*\*\*

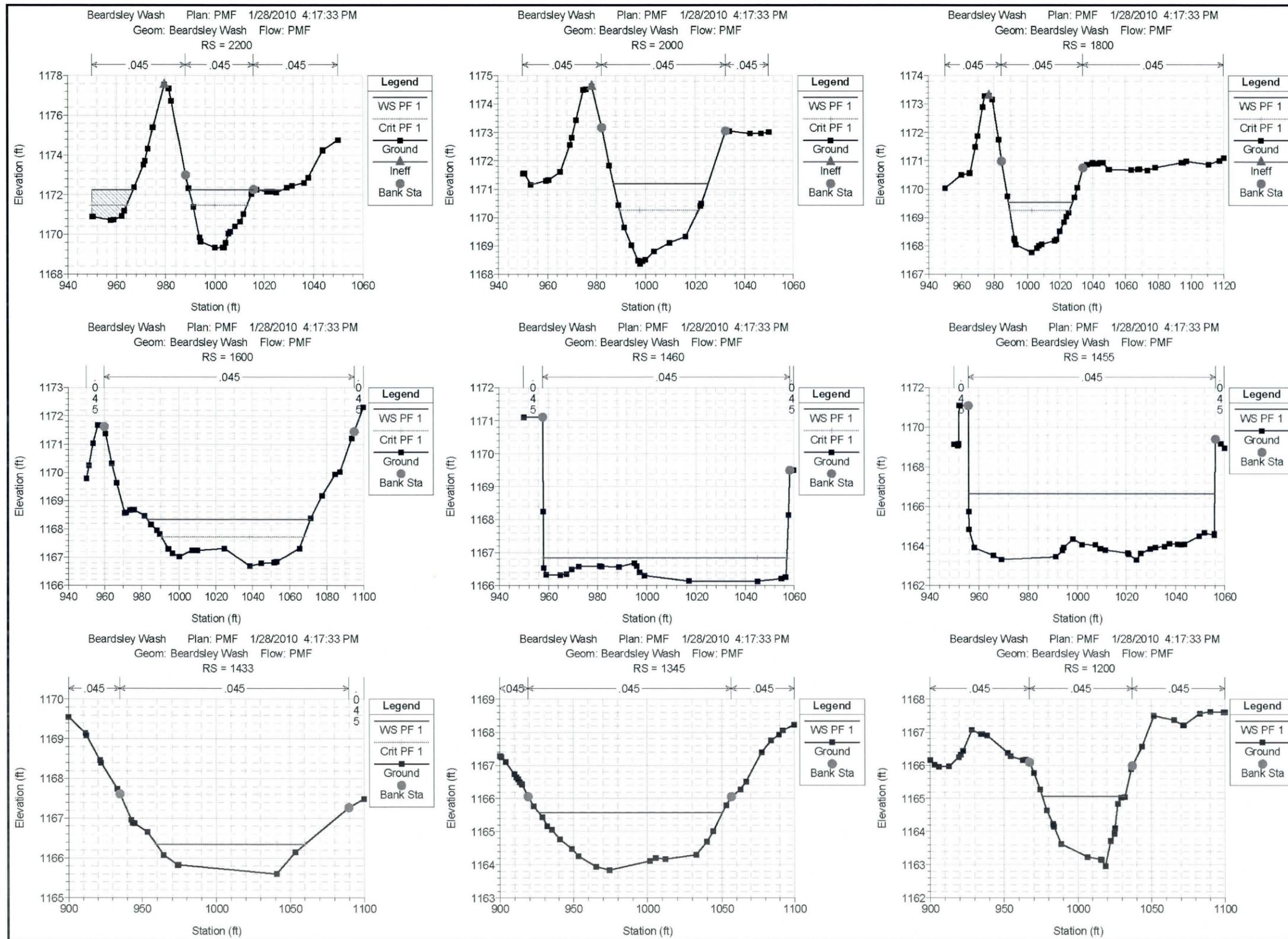
SUMMARY OF MANNING'S N VALUES

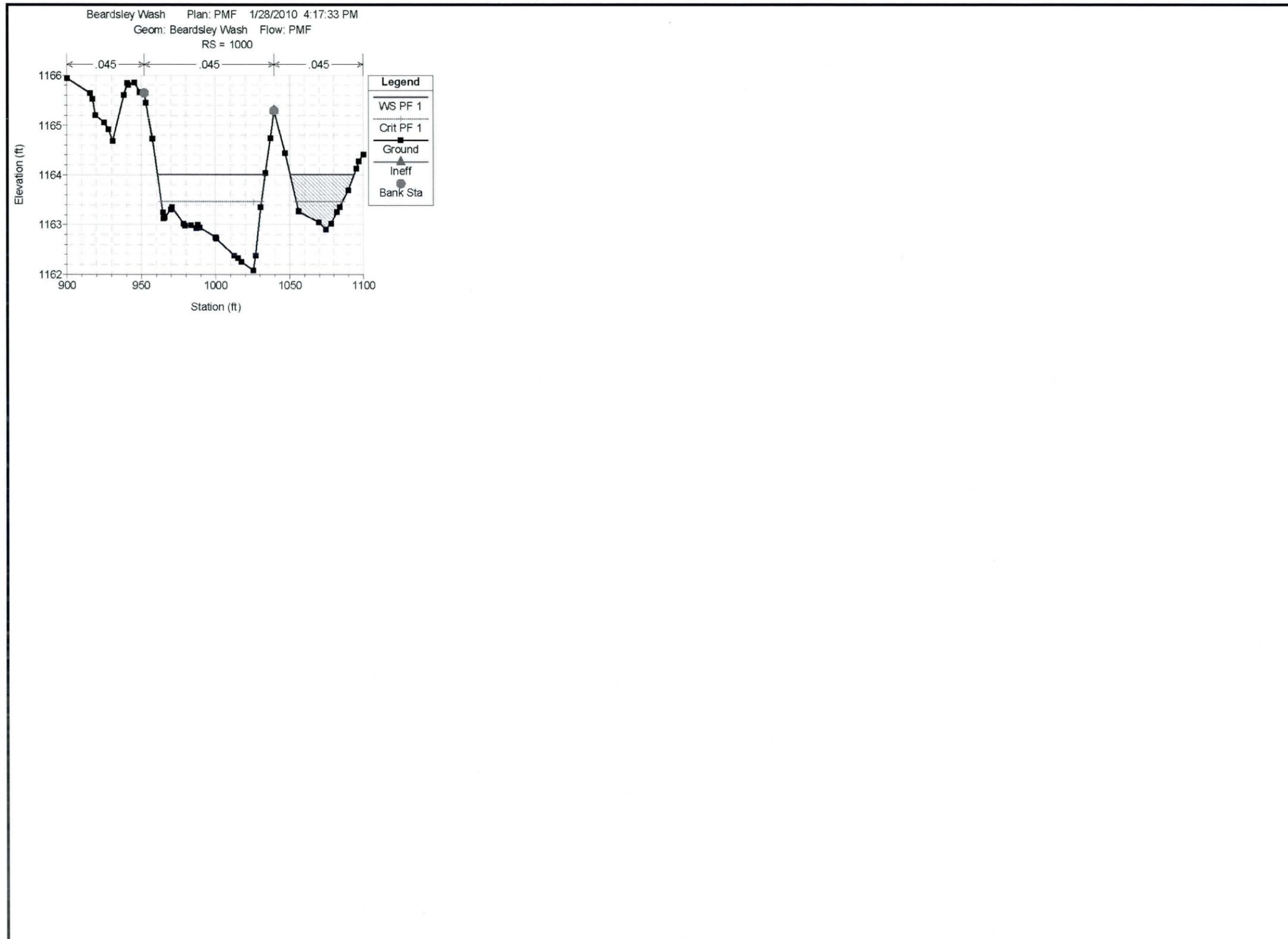
River:Beardsley Wash  
 \*\*\*\*\*  
 \* Reach \* River Sta. \* n1 \* n2 \* n3 \*  
 \*\*\*\*\*  
 \*9 \* 5800 \* .045\* .045\* .045\*  
 \*9 \* 5600 \* .045\* .045\* .045\*  
 \*9 \* 5400 \* .045\* .045\* .045\*  
 \*9 \* 5200 \* .045\* .045\* .045\*  
 \*9 \* 5000 \* .045\* .045\* .045\*  
 \*9 \* 4800 \* .045\* .045\* .045\*  
 \*9 \* 4600 \* .045\* .045\* .045\*  
 \*9 \* 4400 \* .045\* .045\* .045\*  
 \*9 \* 4200 \* .045\* .045\* .045\*  
 \*9 \* 4000 \* .045\* .045\* .045\*  
 \*9 \* 3800 \* .045\* .045\* .045\*  
 \*9 \* 3600 \* .045\* .045\* .045\*  
 \*9 \* 3400 \* .045\* .045\* .045\*  
 \*9 \* 3200 \* .045\* .045\* .045\*  
 \*9 \* 3000 \* .045\* .045\* .045\*  
 \*9 \* 2800 \* .045\* .045\* .045\*  
 \*9 \* 2600 \* .045\* .045\* .045\*  
 \*9 \* 2400 \* .045\* .045\* .045\*  
 \*9 \* 2200 \* .045\* .045\* .045\*  
 \*9 \* 2000 \* .045\* .045\* .045\*  
 \*9 \* 1800 \* .045\* .045\* .045\*  
 \*9 \* 1600 \* .045\* .045\* .045\*  
 \*9 \* 1460 \* .045\* .045\* .045\*  
 \*9 \* 1455 \* .045\* .045\* .045\*  
 \*9 \* 1433 \* .045\* .045\* .045\*  
 \*9 \* 1345 \* .045\* .045\* .045\*  
 \*9 \* 1200 \* .045\* .045\* .045\*  
 \*9 \* 1000 \* .045\* .045\* .045\*  
 \*\*\*\*\*

\*\*\*\*\*











APPENDIX J – COMPARISON OF FLO2D GRID VS. AERIAL MAPPING

